

# **APPENDIX B**

## **Channel Stabilization Measures**

# OVERVIEW OF VARIOUS CHANNEL STABILIZATION MEASURES

## INTRODUCTION

Channel stabilization measures are structures used to control the vertical and horizontal alignment of a channel. For example, riprap is commonly used for bank protection to control lateral channel shifting. Grade control or drop structures are often used to control vertical incision (degradation) and are typically constructed of concrete or driven sheet pile. However, other less common channel stabilization methods and construction techniques are often useful, and in some cases more appropriate for a given situation. The following information provides an overview of channel stabilization measures and provides an introduction to some of the measures recommended for Cottonwood Creek.

## BANK PROTECTION

Common alternatives for bank protection in urban areas can be classified as flexible revetment, rigid revetment, and spur fields. Flexible and rigid revetments have been widely used for channel linings in urban areas. Spur fields are less common in urban areas, but have been widely used in rural areas, particularly by the transportation and road engineering community.

### Flexible Revetment Bank Protection

Common flexible revetments include dumped rock riprap and rock-and-wire mattress and gabions. Dumped rock riprap has been widely used for bank protection (**Figure 1**). Rock riprap protection is flexible and local damage is easily repaired. Successful design depends on adequate rock size and gradation, an appropriate filter between the underlying soil and riprap, and proper construction practices.

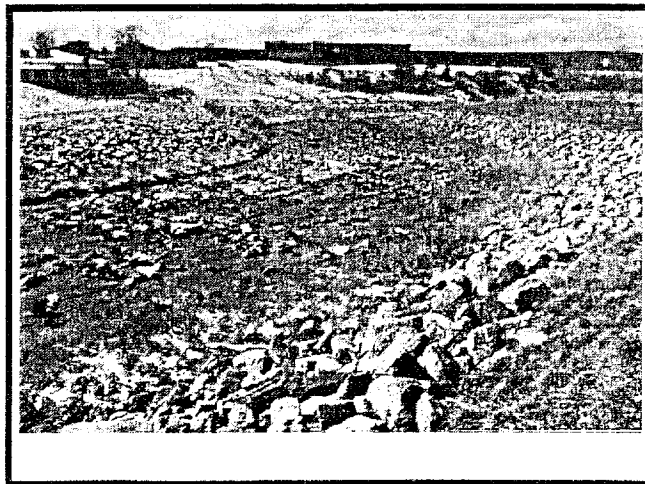


Figure 1. Dumped riprap bank protection, Cottonwood Creek, Colorado.

When only the channel banks are protected, adequate toe-down (burial into the channel bottom) must be provided to prevent failure by scour along the toe of slope. Rock riprap is often effectively used to provide toe protection along a bankline that is otherwise natural (e.g., a prudent line channel). Riprap placed along the toe of slope, with adequate toe-down, can prevent undercutting of the bank and potential bank mass failures.

The economic use of rock-and-wire products is favored by an arid climate, availability of stones of cobble size, and unavailability of rock for dumped rock riprap (FHWA 1991). Corrosion of wire mesh is slow in arid climates and ephemeral streams do not subject the wire to continuous abrasion. **Figure 2** shows a gabion wall constructed to protect the outside of a bend on the Black Arroyo, New Mexico. Where large rock is not available, the use of rock-and-wire products may be advantageous in spite of the eventual corrosion or abrasion of the wire. However, gabion walls are labor intensive to build and subject to vandalism (in urban areas the wire mesh has been cut or broken open and the rocks thrown into the channel).



Figure 2. Gabion wall on Black Arroyo, New Mexico.

## Rigid Revetment Bank Protection

Common rigid revetment includes concrete paving and soil cement. Concrete paving minimizes channel size, but is typically the most expensive lining alternative. When used for bank lining only, adequate toe-down must be provided to prevent undermining. **Figure 3** illustrates a concrete trapezoidal channel under construction, terminating with a concrete drop structure at the downstream confluence (Unser Boulevard channel, New Mexico). The aesthetic appearance of concrete lining can be improved using tinted concrete; however, the smooth, flat appearance of a concrete lining generally does not blend well in a natural, or naturalistic, channel environment.

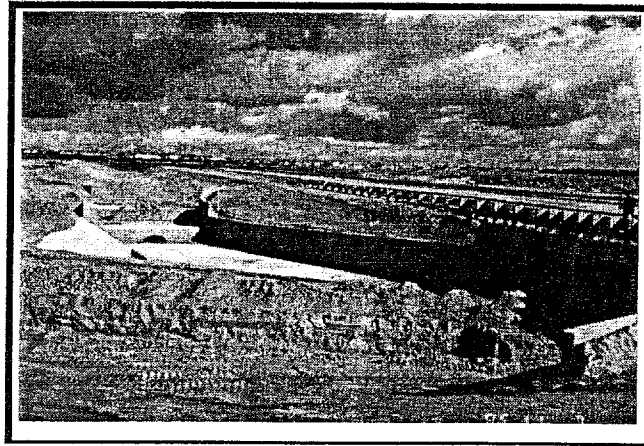


Figure 3. Concrete trapezoidal channel under construction.

Soil cement is a highly compacted mixture of soil (usually sand), Portland cement and water. The placement and compaction of soil cement is accomplished by conventional highway construction equipment and methods. The resulting product has an appearance, texture and color similar to that of the native bank materials (Hansen and Lynch 1995). A stair-step construction is typically used, with each lift about 8 ft wide and about 12 inches thick before compaction (6-8 inches thick after compaction). To provide a smoother edge, the soil cement can be trimmed at the end of each days placement; however, in many cases the added roughness of the stair-step edge is beneficially hydraulically, and the steps provide a means for people and animals to climb out of a channel, which can be a desirable emergency safety measure in urban areas.

**Figure 4** illustrates stair-step soil cement bank protection on the outside of a bend on Calabacillas Arroyo, New Mexico, and **Figure 5** shows soil cement protection of both banks on Sand Creek, Colorado. Unlike other types of bank revetment, where milder slopes are desirable, soil cement in a stair-step construction can be used on steeper slopes (i.e., typically one-to-one), which reduces channel excavation costs. For many applications, soil cement is generally more aesthetically pleasing than other types of revetment and has roughness characteristics more comparable to those of the native bank materials.

### Spur Field Bank Protection

Spurs are permeable or impermeable structures that project from the bank into the channel (FHWA 1991). Spurs may be used to alter flow direction, induce deposition or reduce flow velocity. Spurs may protect a stream bank at less cost than riprap revetment, and by deflecting current away from the bank and causing deposition, they may more effectively protect banks from erosion than revetment (Richardson and Simons 1984). Multiple spurs are typically designed to create a spur field along a bankline (**Figure 6**), with the overall design a function of permeability, orientation, spacing, height, shape, length, construction materials and stream environment (FHWA 1991). In contrast to bank revetment, which stabilizes the bankline but does not change the erosive flow conditions, a spur field can be used to control the problem by diverting flow back into the middle of channel and allowing a bank line to recover by sediment deposition and revegetation.

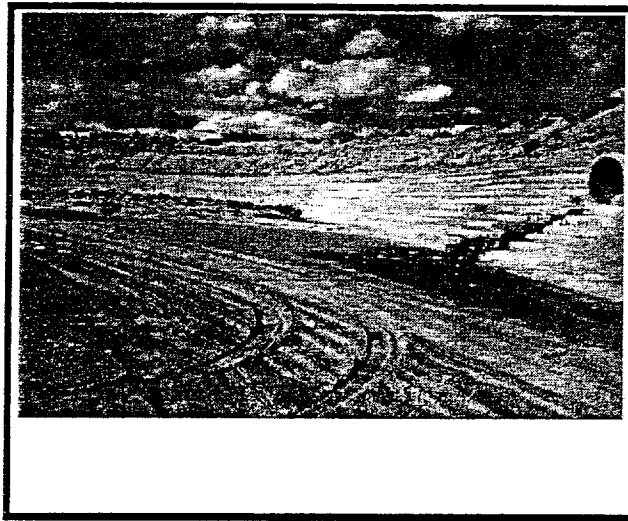


Figure 4. Soil cement bank protection, Calabacillas Arroyo.

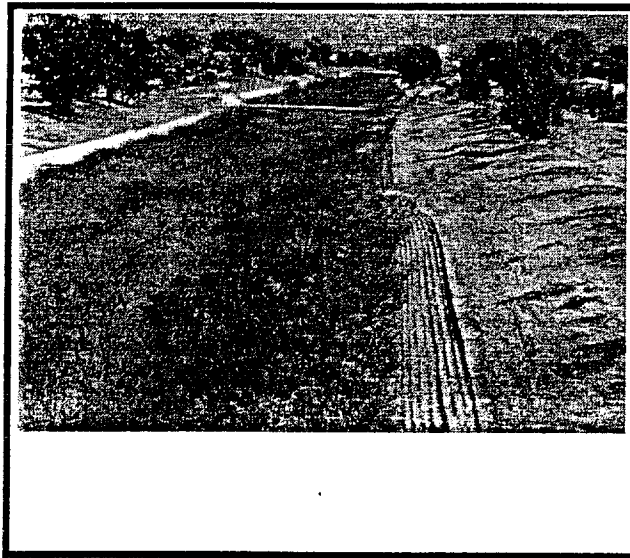


Figure 5. Soil cement bank protection, Sand Creek, Colorado



Figure 6. Spur view along the outside of a bend.

## GRADE CONTROL PROTECTION

Grade control or vertical channel protection can range from simple rock riprap structures, to soil cement structures, to large concrete structures with baffled aprons and stilling basins. The terms grade control structure and drop structure are often used interchangeably; however, it can be useful to define a grade control structure as a structure that maintains the existing grade (with an invert typically at the existing channel/terrace bottom), and a drop structure as a structure used to lower the existing grade (by using an invert elevated above the natural channel/terrace bottom).

Success with riprap drop structures has been varied. In the Denver area, the use of riprap drop structures has been discouraged by the Denver Urban Drainage and Flood Control District, based on a comprehensive evaluation of the performance of existing riprap drop structures (McLaughlin Water Engineers 1986).

Soil cement drop structures have been effective in the southwest, with designs ranging from a straight drop to curvilinear and stepped drops. **Figure 7** illustrates a stepped soil cement drop structure on La Barranca Arroyo, New Mexico, and **Figure 8** shows a curvilinear soil cement drop structure on Calabacillas Arroyo, New Mexico.

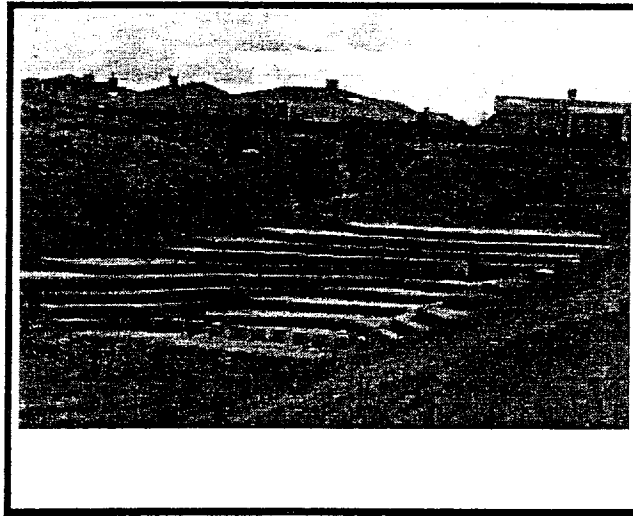


Figure 7. Stepped soil-cement drop structure, La Barranca Arroyo, New Mexico.



Figure 8. Curvilinear soil cement drop structure, Cabacillas Arroyo, New Mexico.

Properly designed concrete drops are effective and can accommodate large drop heights with significant energy dissipation, but these type of structures are typically quite expensive. Often, a more economical and aesthetically pleasing design can be achieved by using multiple soil cement drops of lower height. **Figure 9** illustrates a small concrete grade control structure on Black's Arroyo, New Mexico. Concrete drop structures that are not much more than a retaining wall often fail, as illustrated by **Figure 10**. In contrast, this type of failure is rarely seen on stair-step soil cement drop structures due to the large mass of soil cement used in construction.



Figure 9. Concrete grade control structure, Black Arroyo, New Mexico.

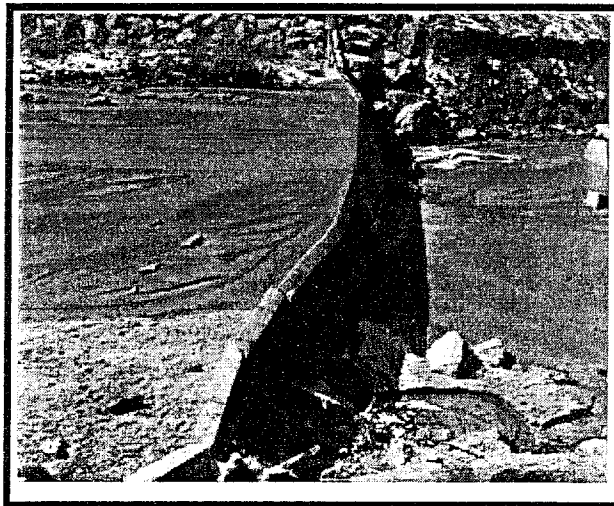


Figure 10. Failing grade control structure, Cottonwood Creek, Colorado.

The durability of soil cement drop structures under perennial flow conditions is a concern, where the soil cement is exposed to slow but progressive erosion by year-round flow. Under these conditions it may be advisable to cap the soil cement structure with roller-compacted concrete (RCC). RCC uses a processed/graded aggregate and has a higher compressive strength than soil cement, but is constructed using similar techniques. RCC has been used for dam embankment overtopping protection and has functioned well under long term flow conditions (McLean and Hansen 1993).



# APPENDIX C

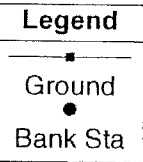
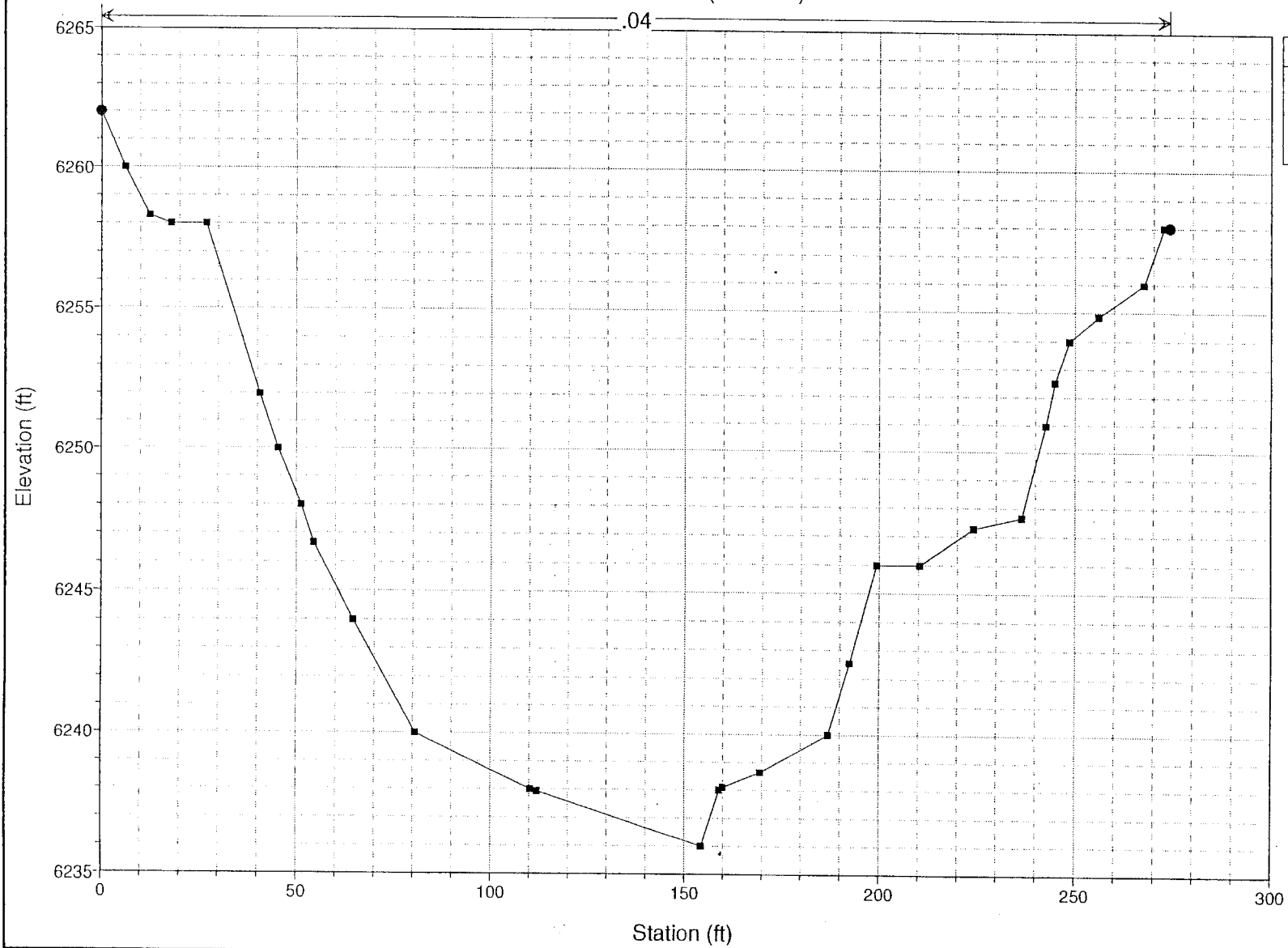
## Hydraulics

## Channel Cross Sections

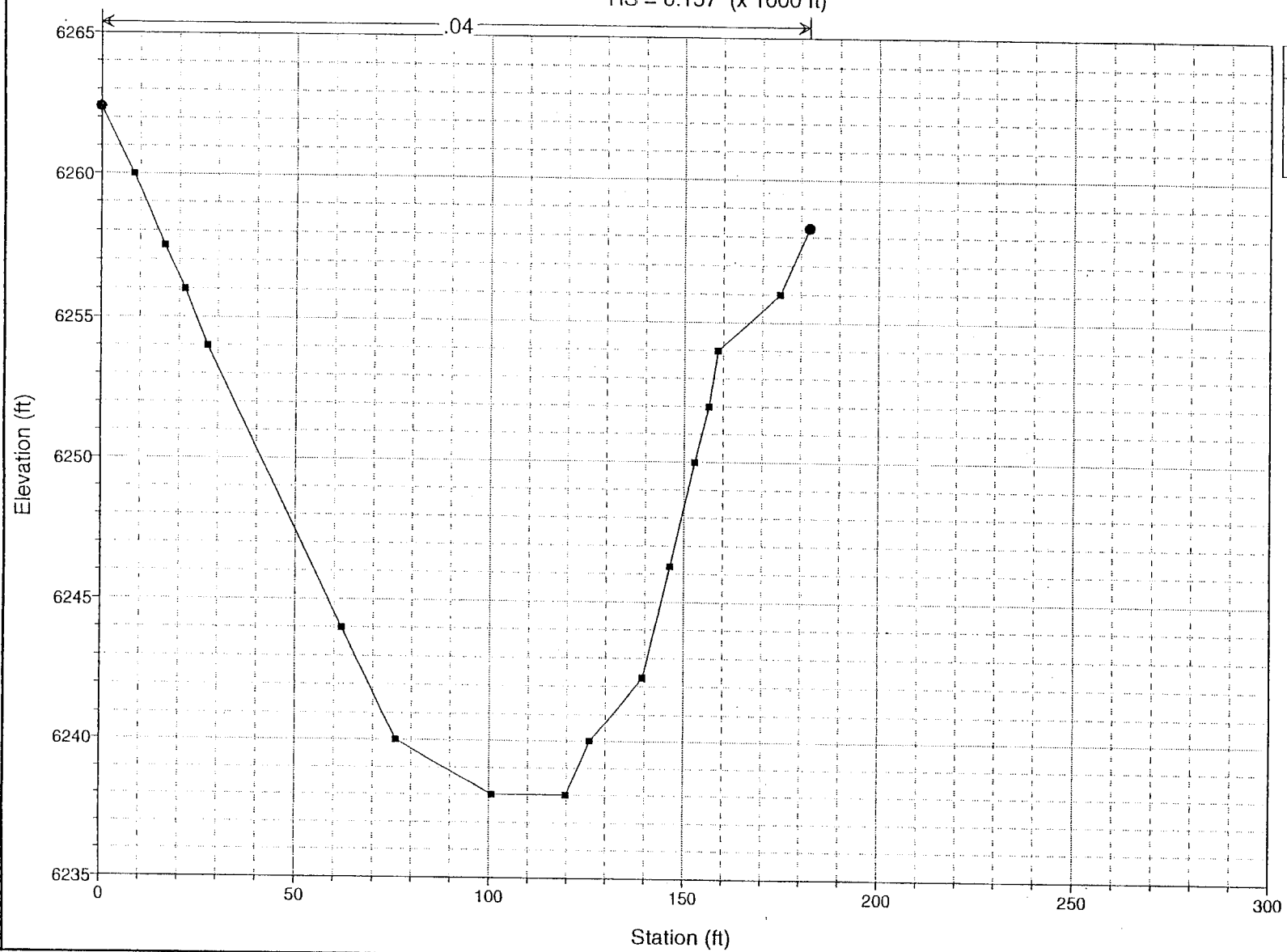
# Cottonwood Creek

RS = 0 (x 1000 ft)

.04

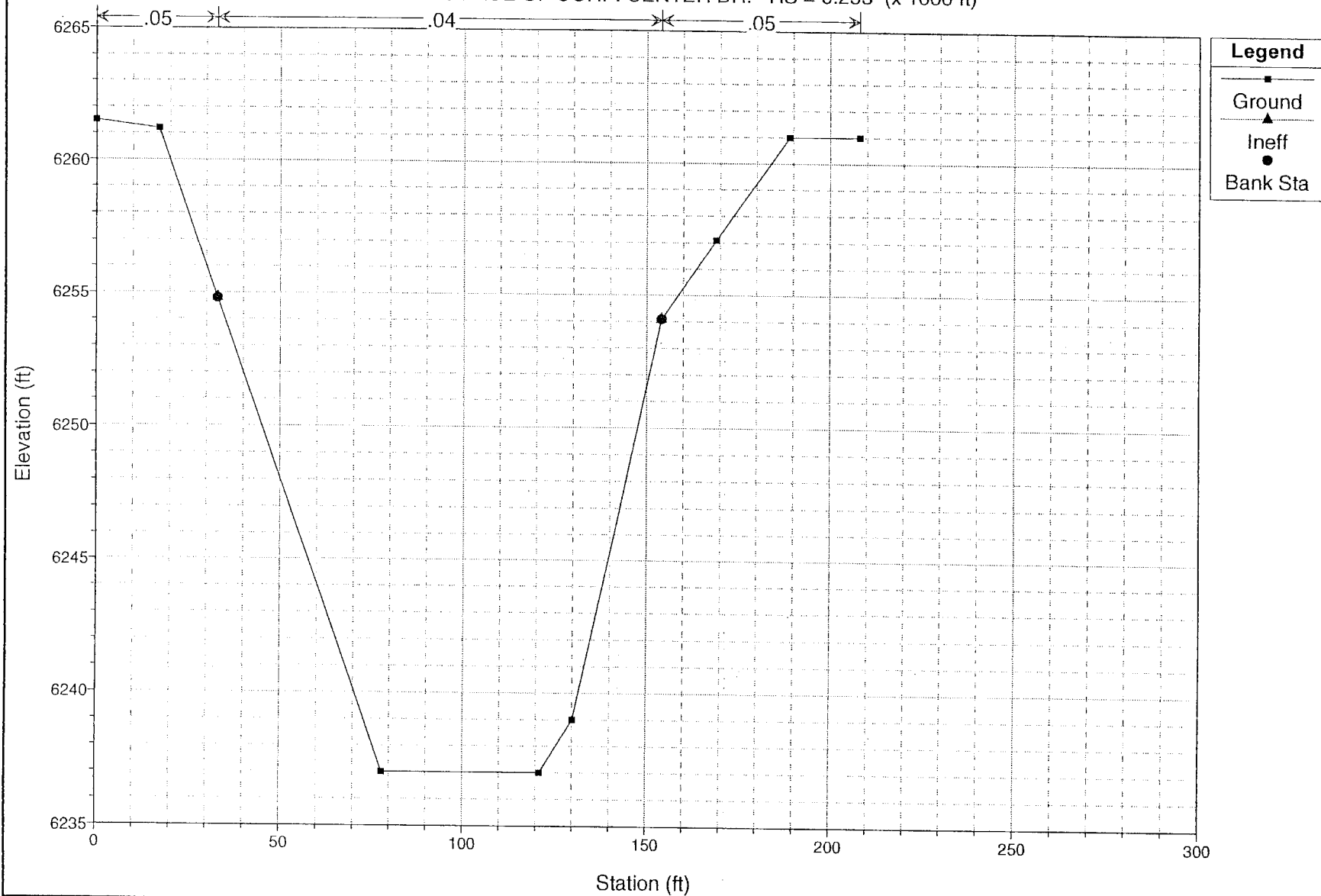


Cottonwood Creek  
RS = 0.157 (x 1000 ft)



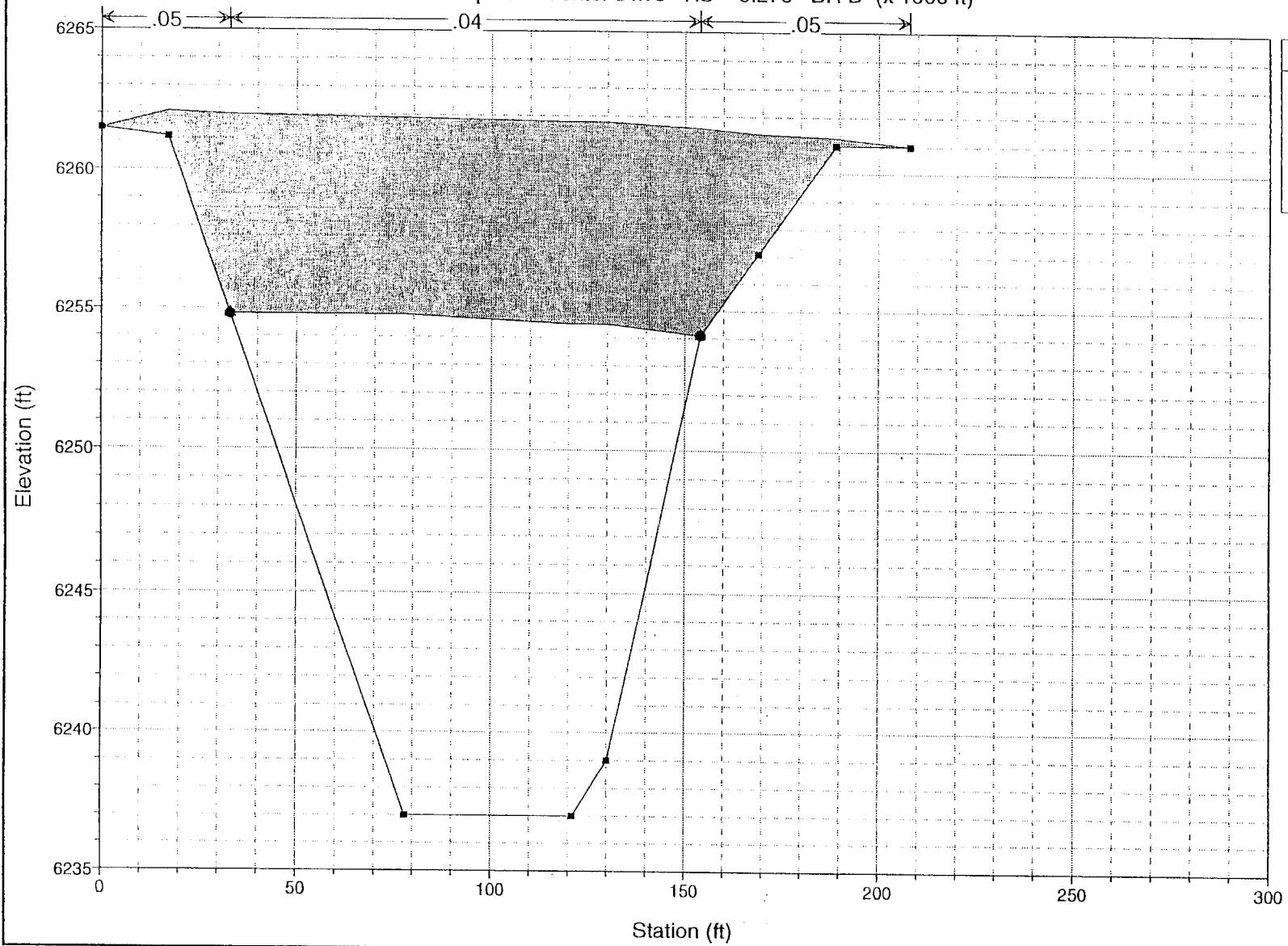
# Cottonwood Creek

XS @ D/S FACE OF CORP. CENTER DR. RS = 0.253 (x 1000 ft)



# Cottonwood Creek

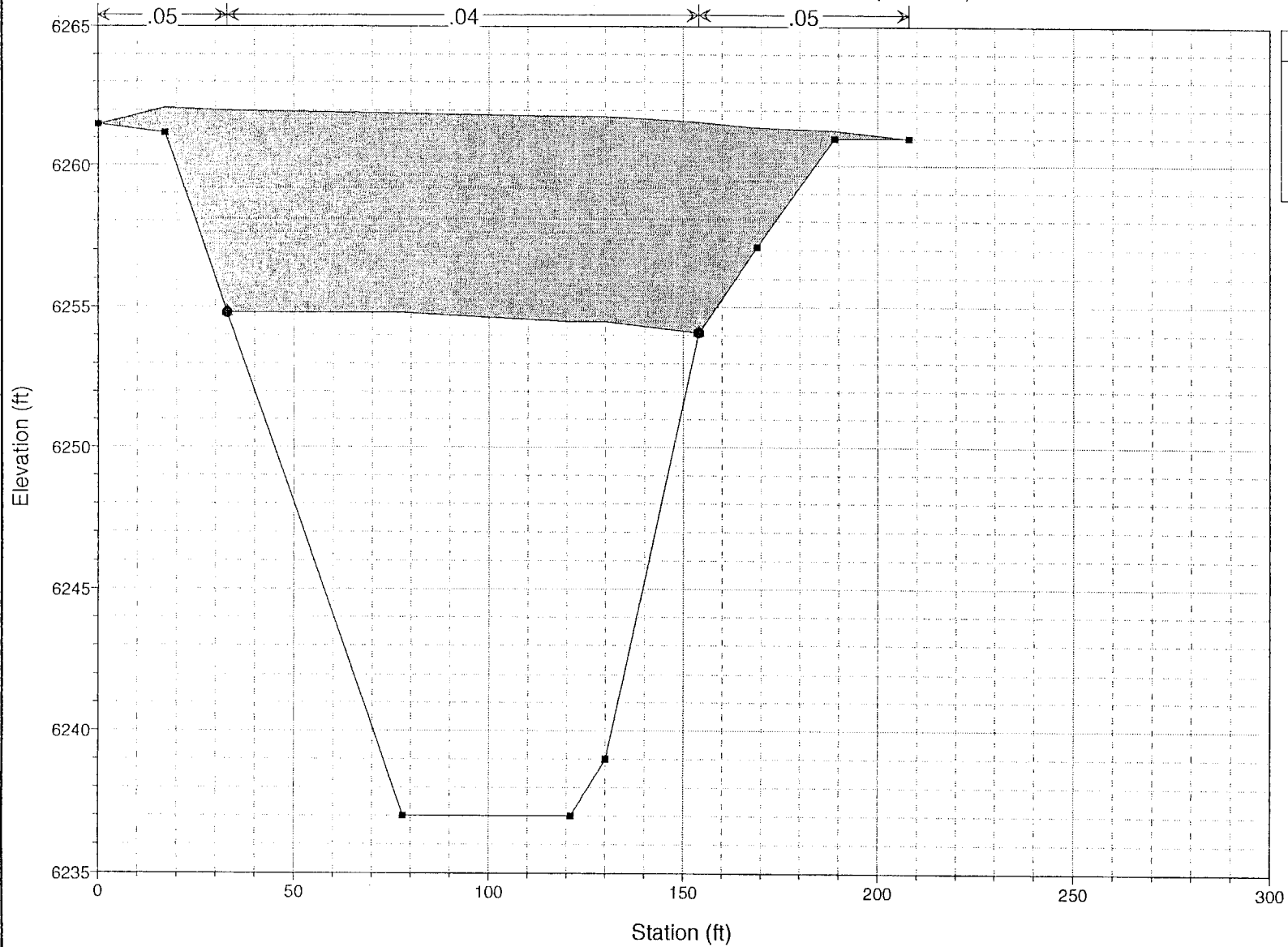
Corporate Center Drive RS = 0.276 BR D (x 1000 ft)



- Legend**
- Ground
  - Ineff
  - Bank Sta

# Cottonwood Creek

Corporate Center Drive RS = 0.276 BR U (x 1000 ft)



## Legend

Ground

Ineff

Bank Sta



# Cottonwood Creek

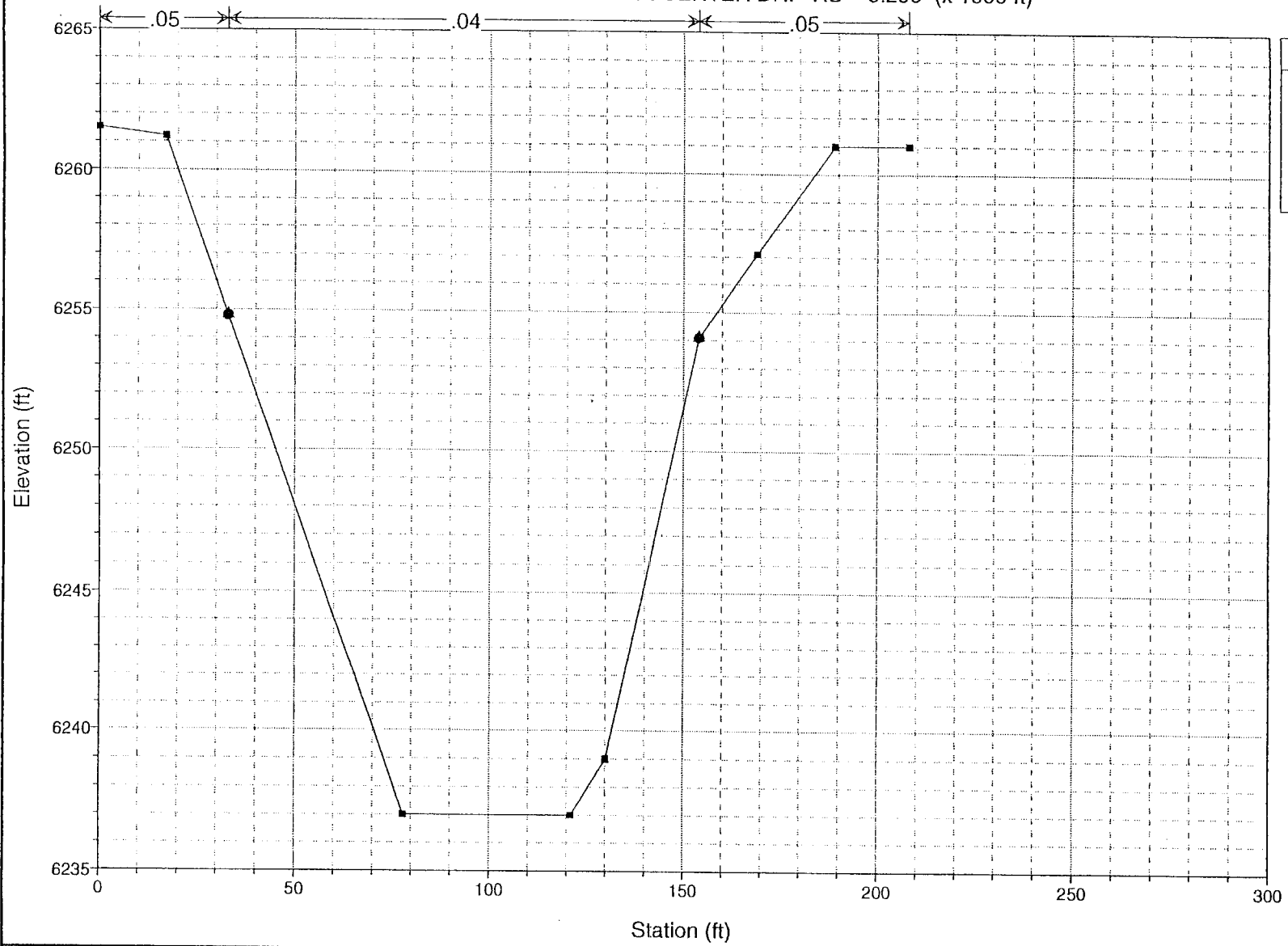
XS @ U/S FACE OF CORP. CENTER DR. RS = 0.299 (x 1000 ft)

## Legend

Ground

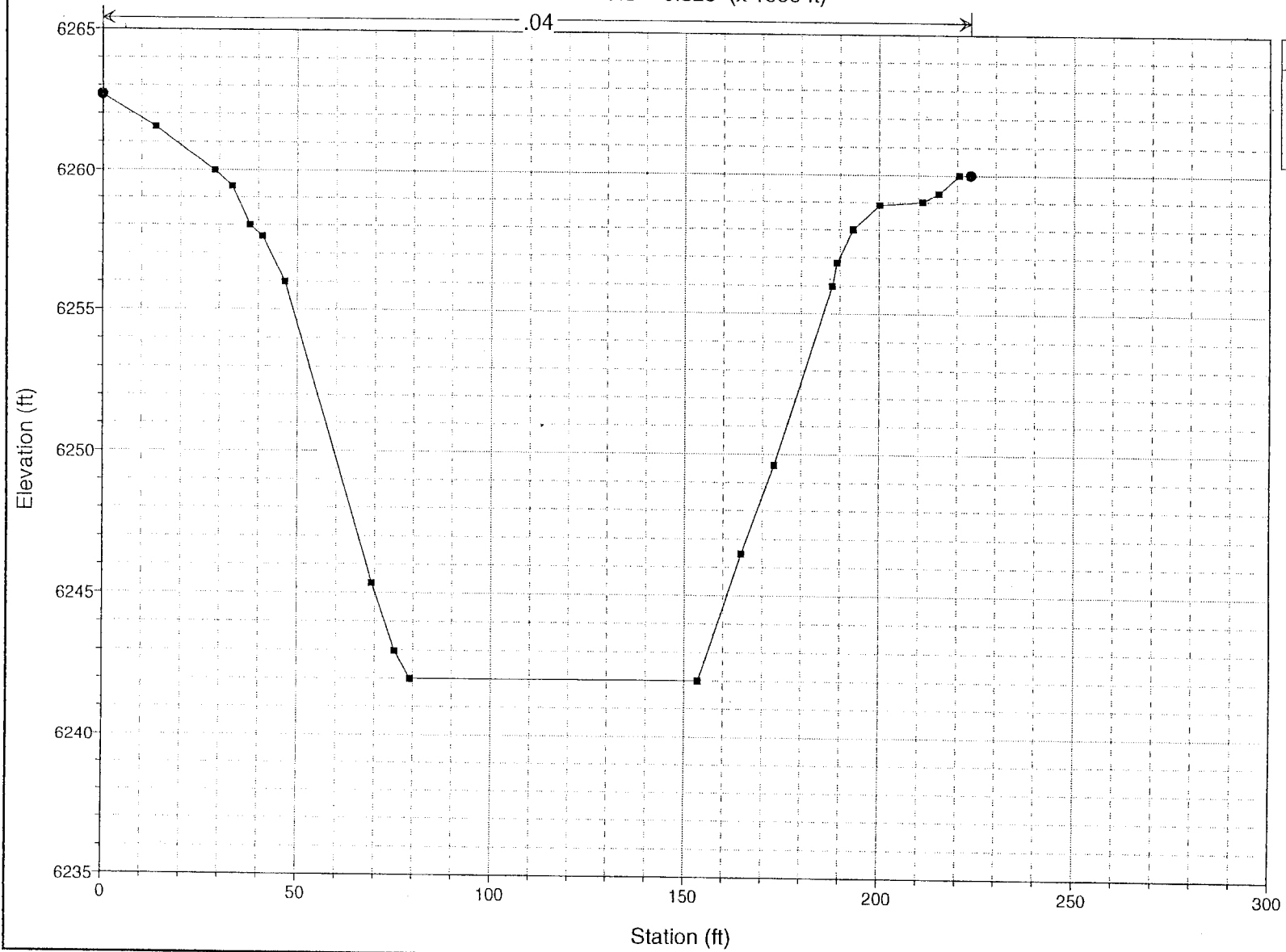
Ineff

Bank Sta



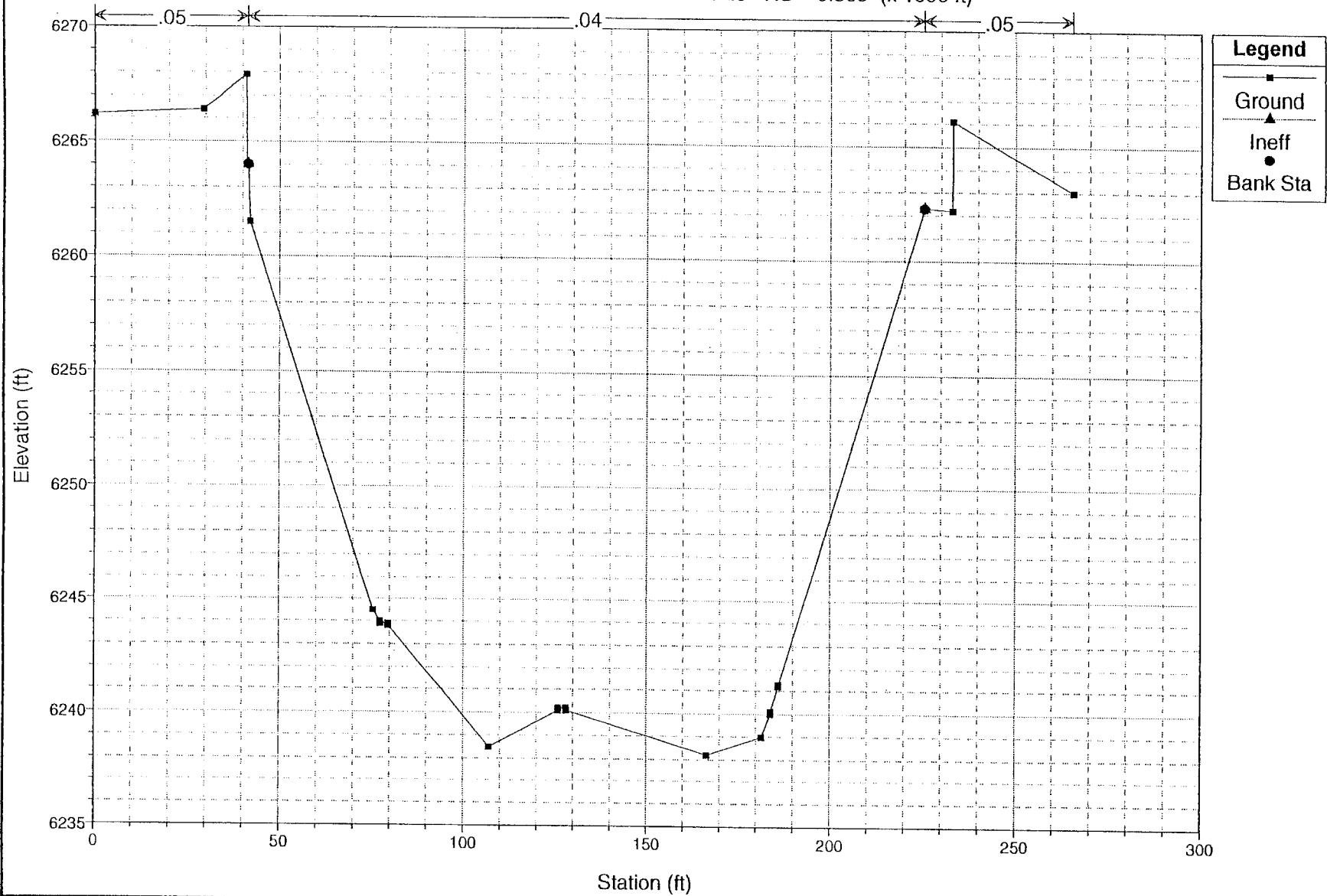


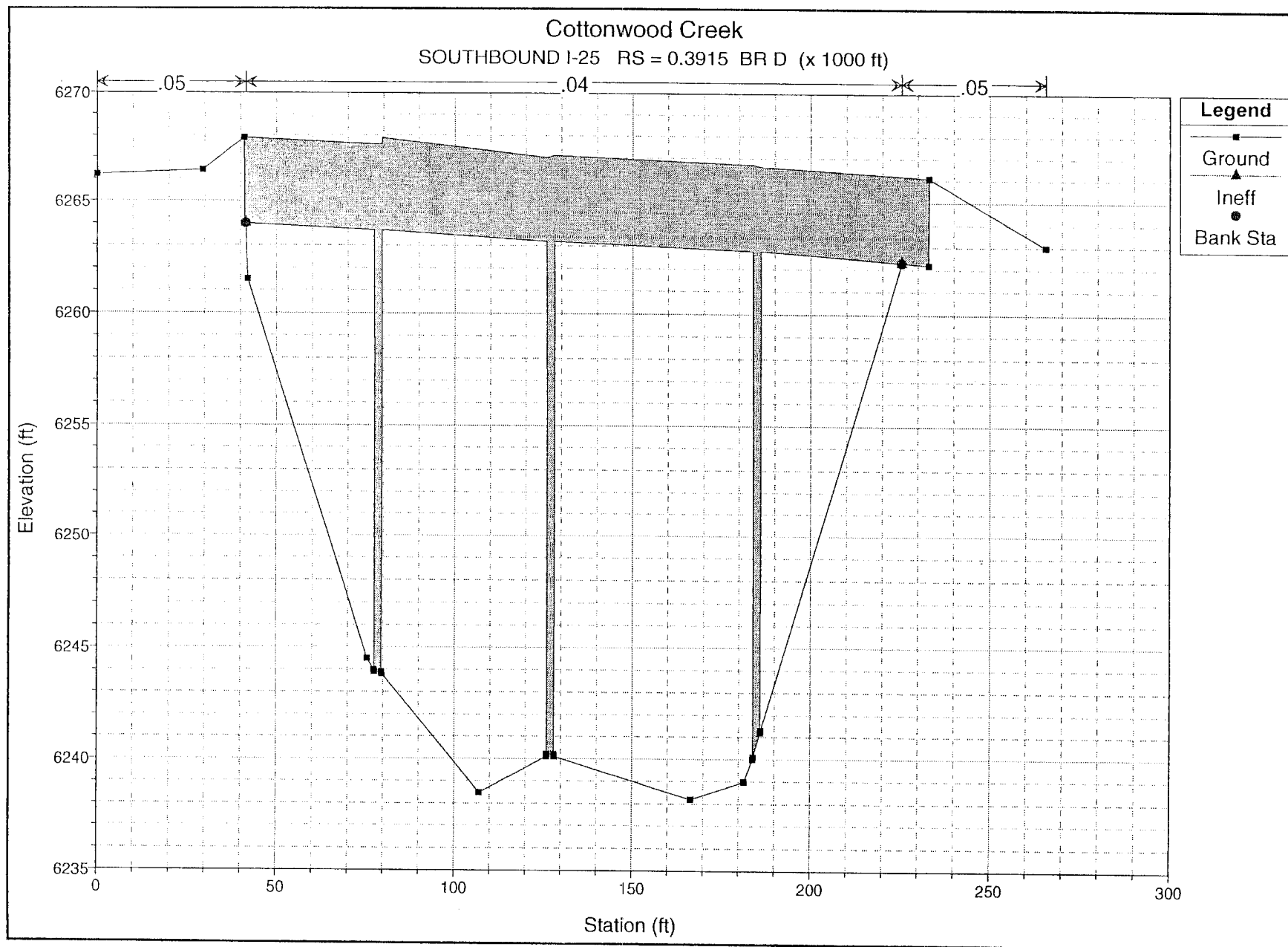
Cottonwood Creek  
RS = 0.329 (x 1000 ft)

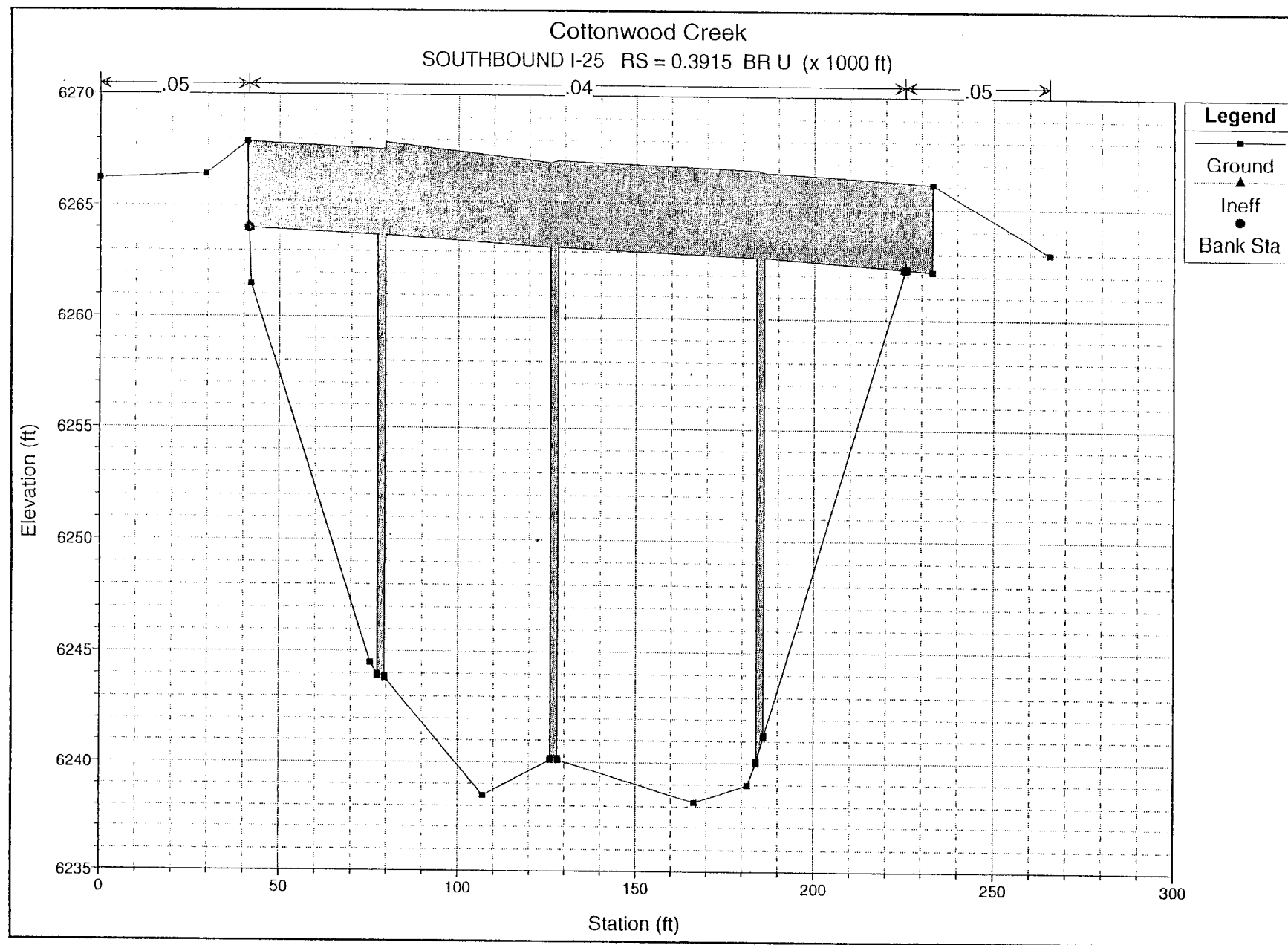


# Cottonwood Creek

XS @ D/S FACE OF SOUTHBOUND I-25 RS = 0.369 (x 1000 ft)

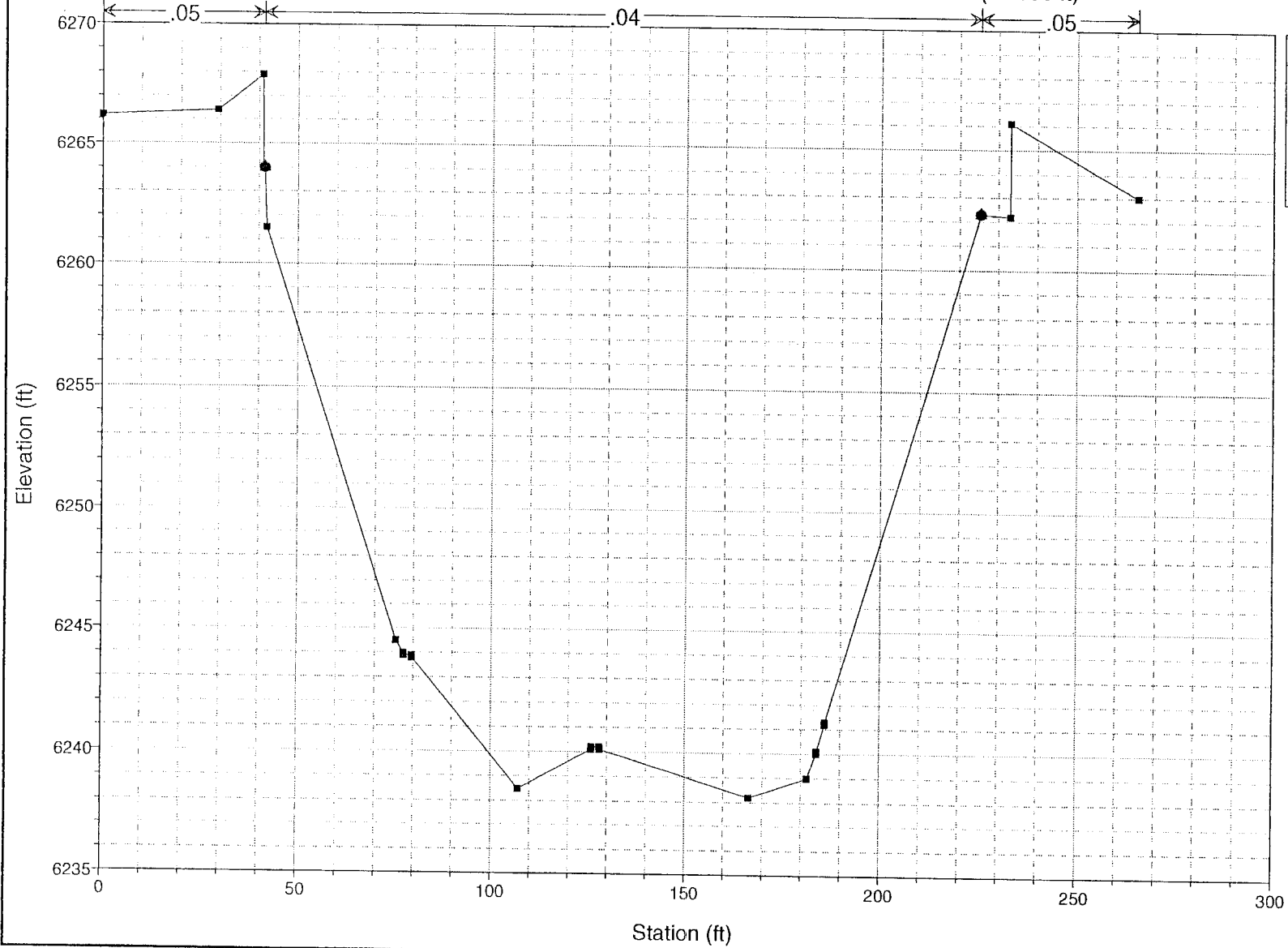






# Cottonwood Creek

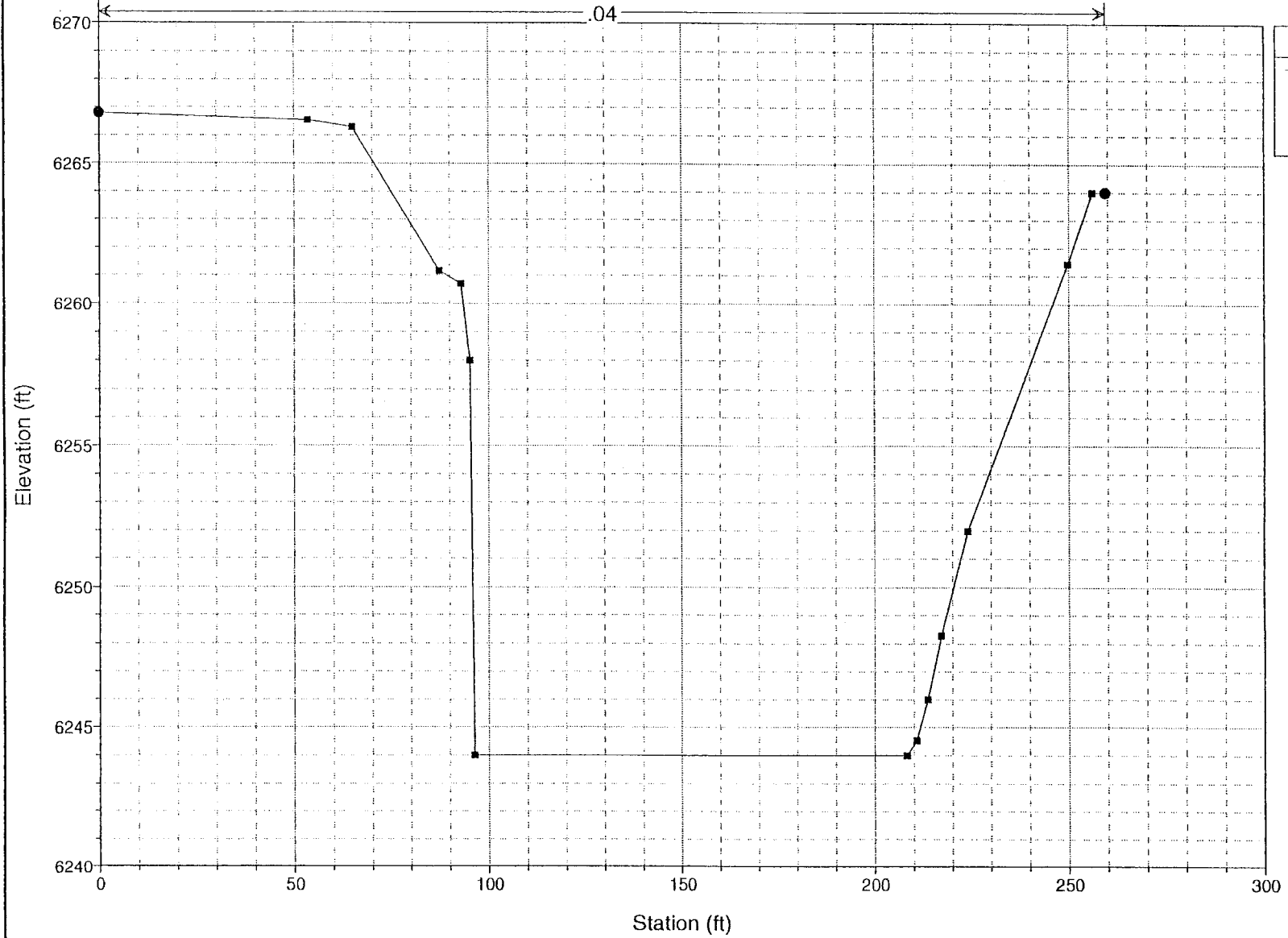
XS @ U/S FACE OF I-25 SOUTHBOUND BRIDGE RS = 0.414 (x 1000 ft)



## Legend

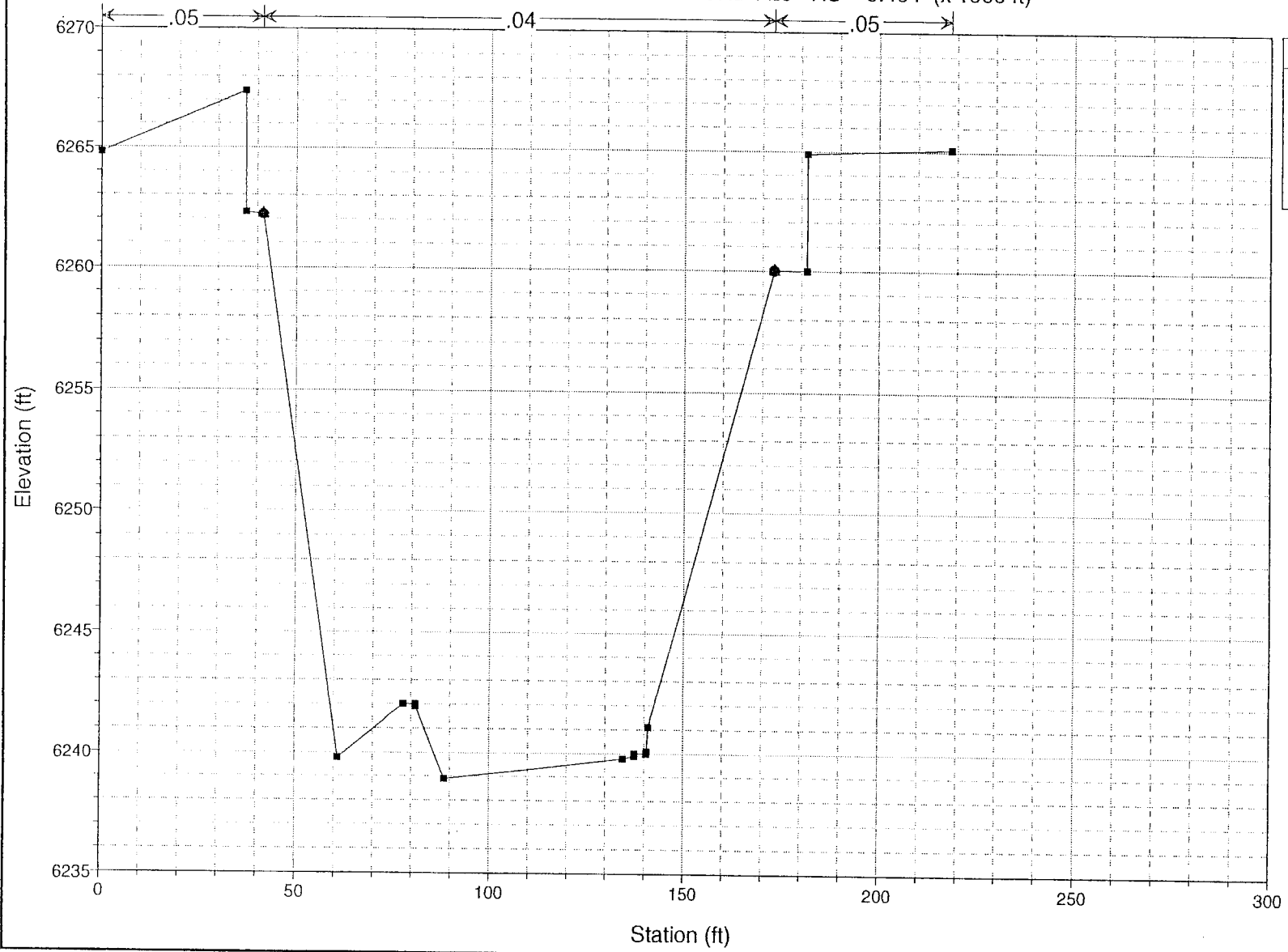
- Ground
- Ineff
- Bank Sta

Cottonwood Creek  
CROSS SECTION BETWEEN I-25 BRIDGES RS = 0.434 (x 1000 ft)



# Cottonwood Creek

XS @ D/S FACE OF NORTHBOUND I-25 RS = 0.464 (x 1000 ft)

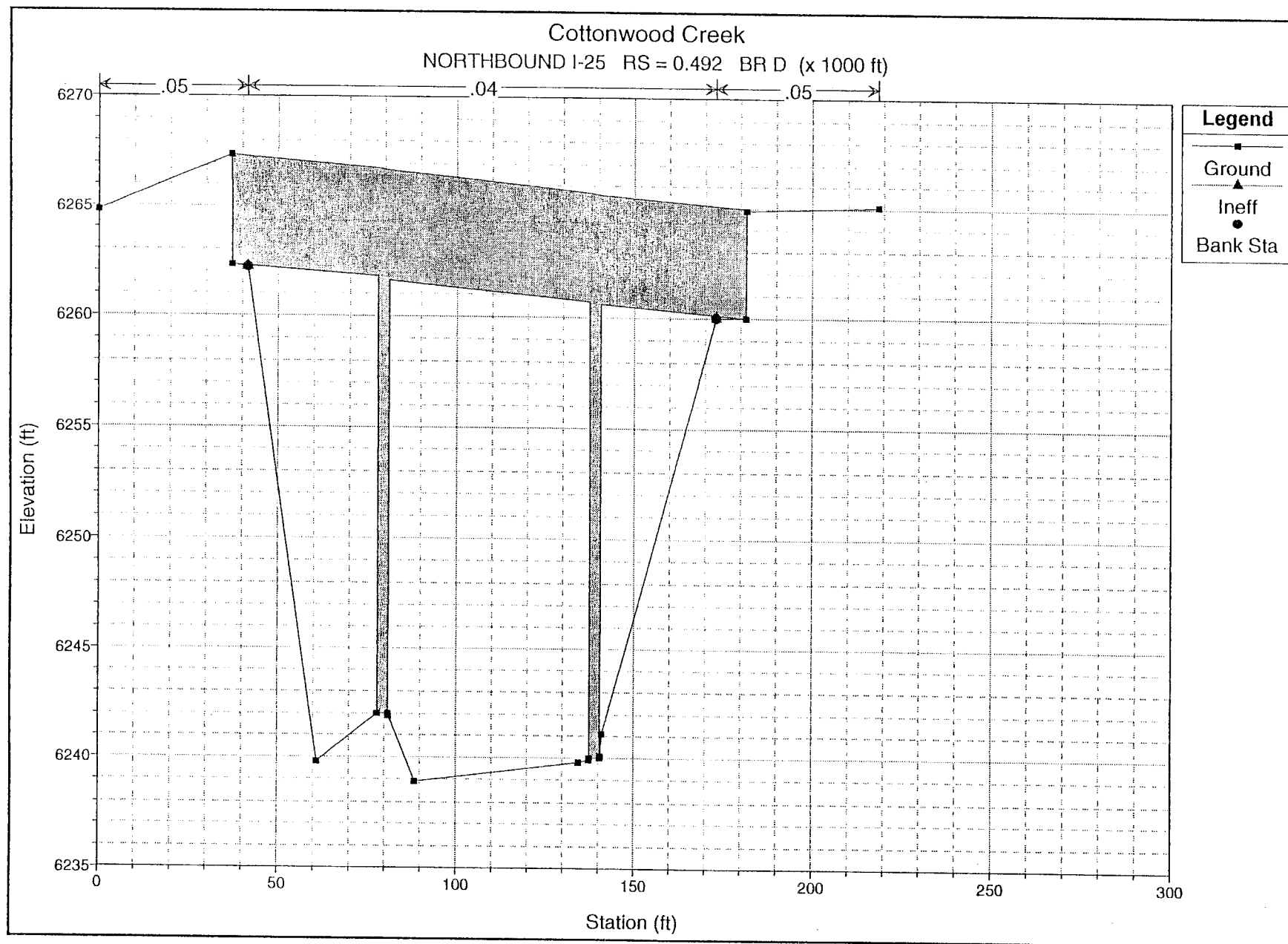


## Legend

Ground

Ineff

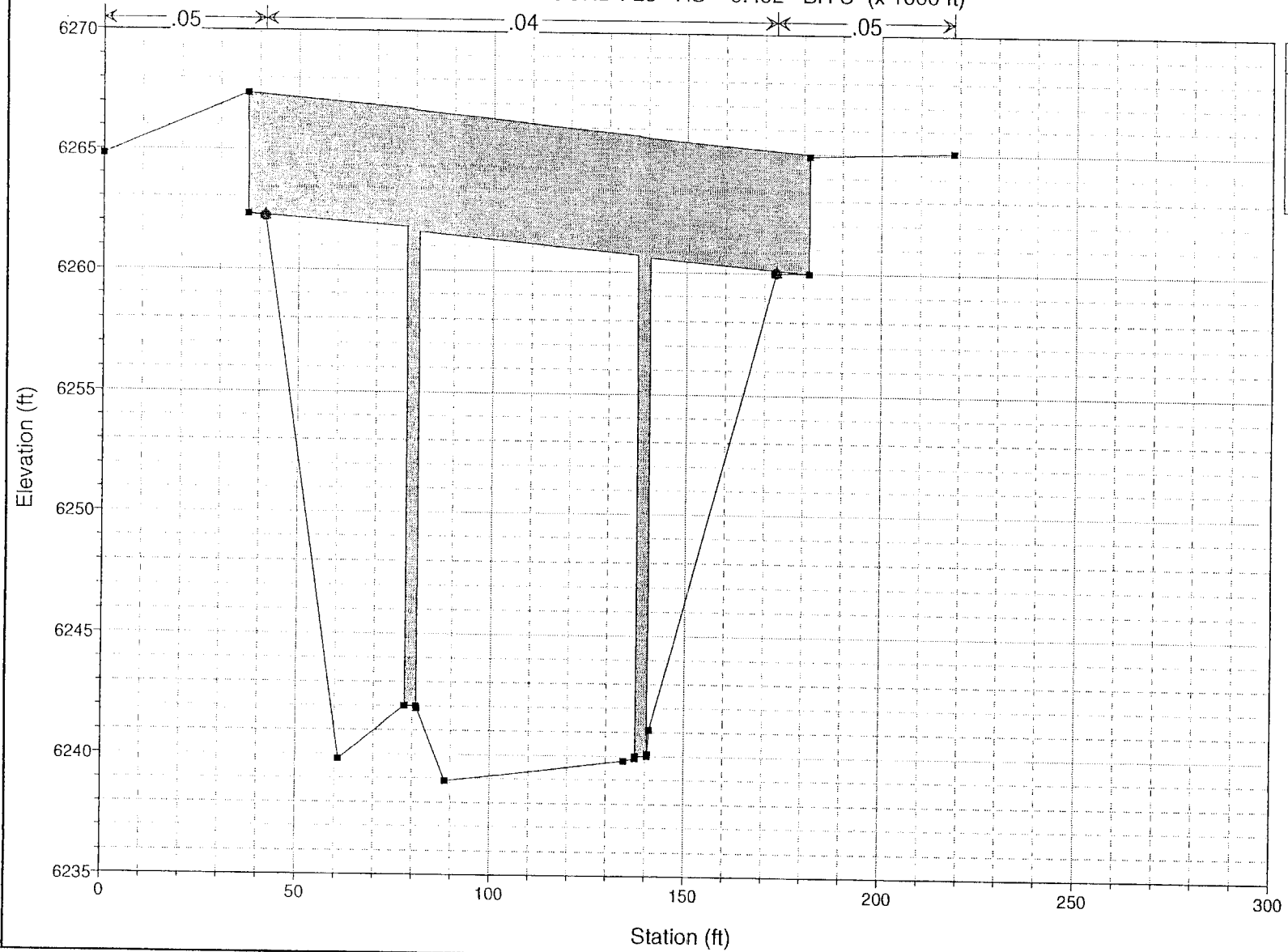
Bank Sta





# Cottonwood Creek

NORTHBOUND I-25 RS = 0.492 BR U (x 1000 ft)

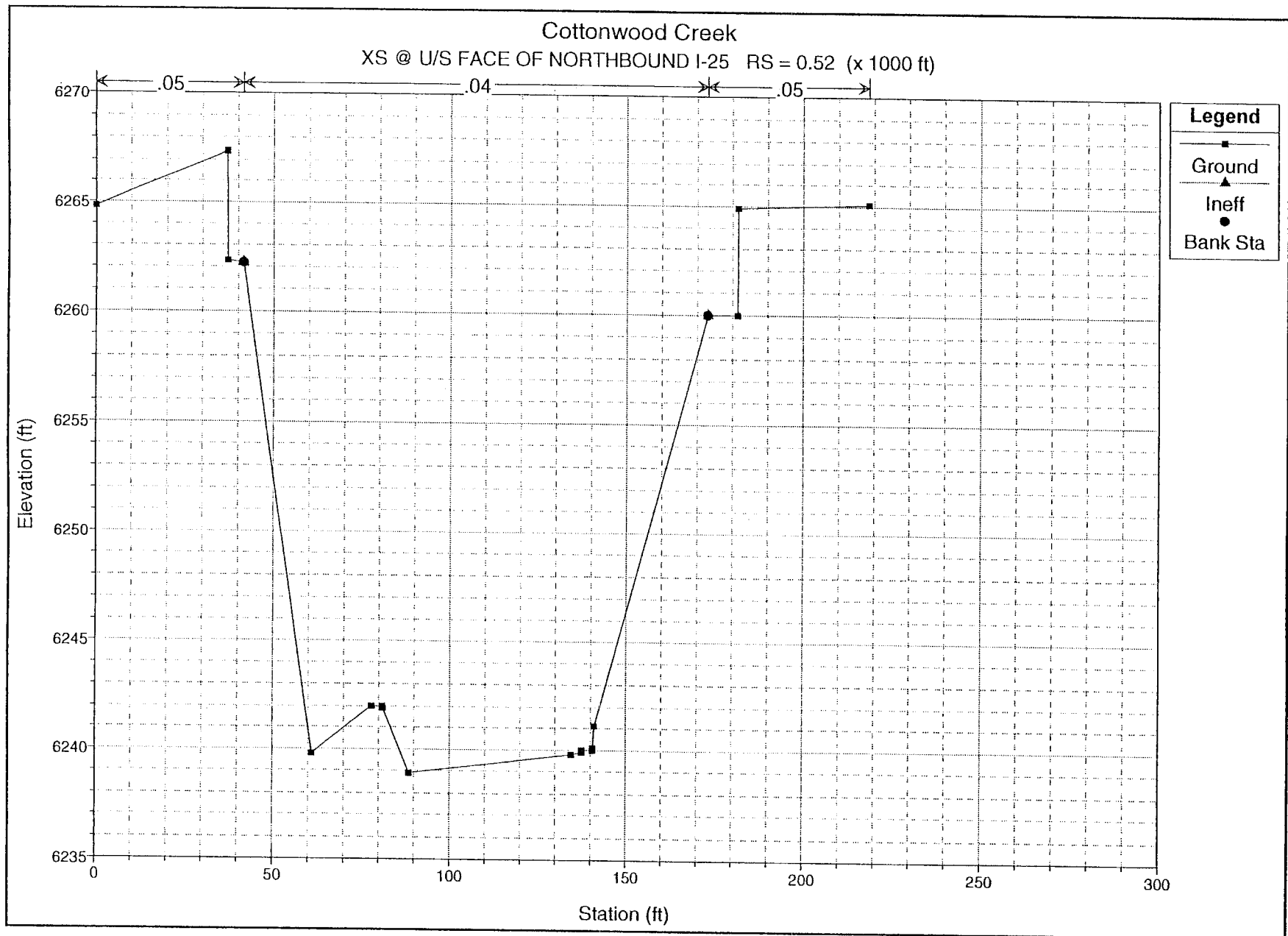


## Legend

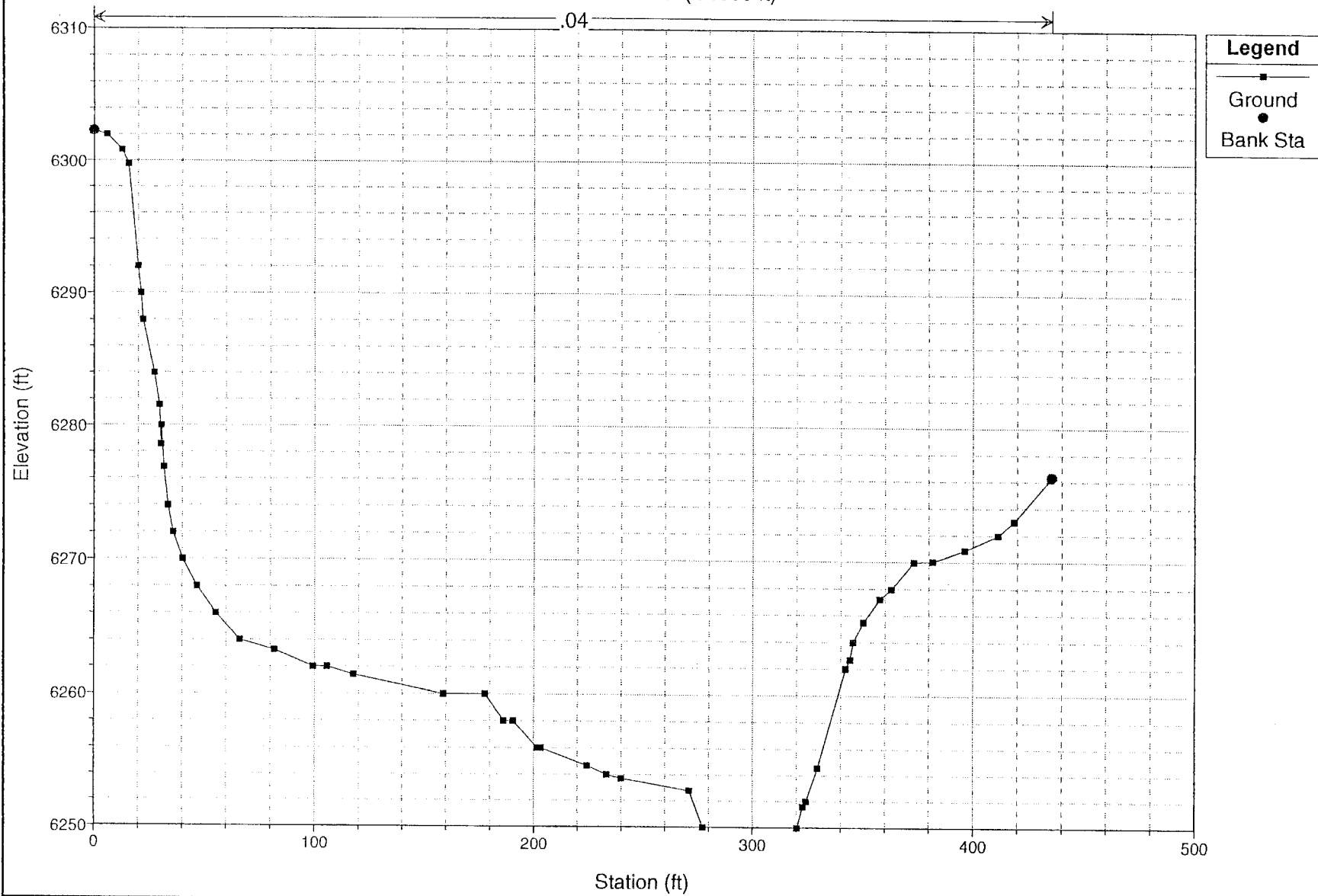
Ground

Ineff

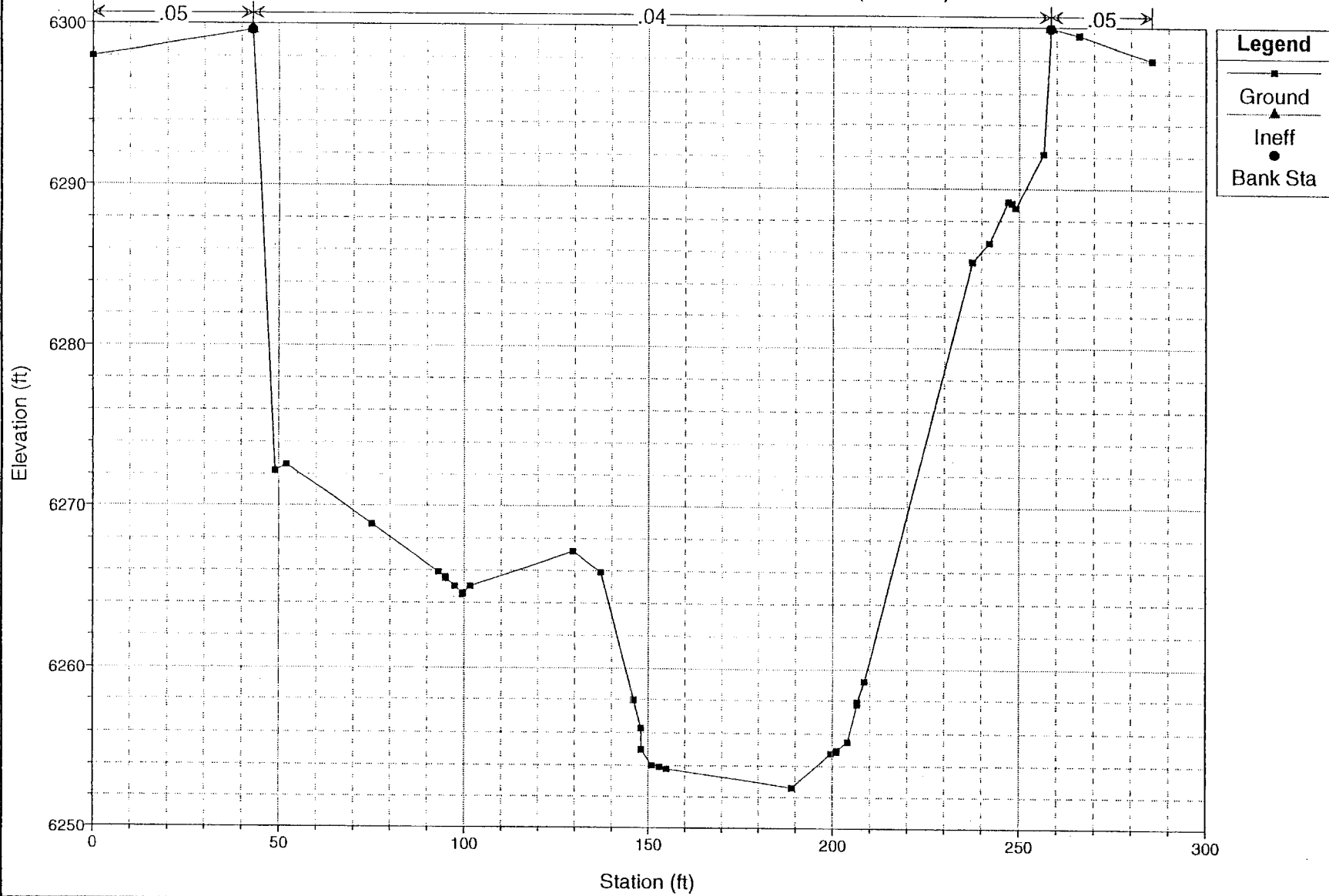
Bank Sta



Cottonwood Creek  
RS = 0.933 (x 1000 ft)

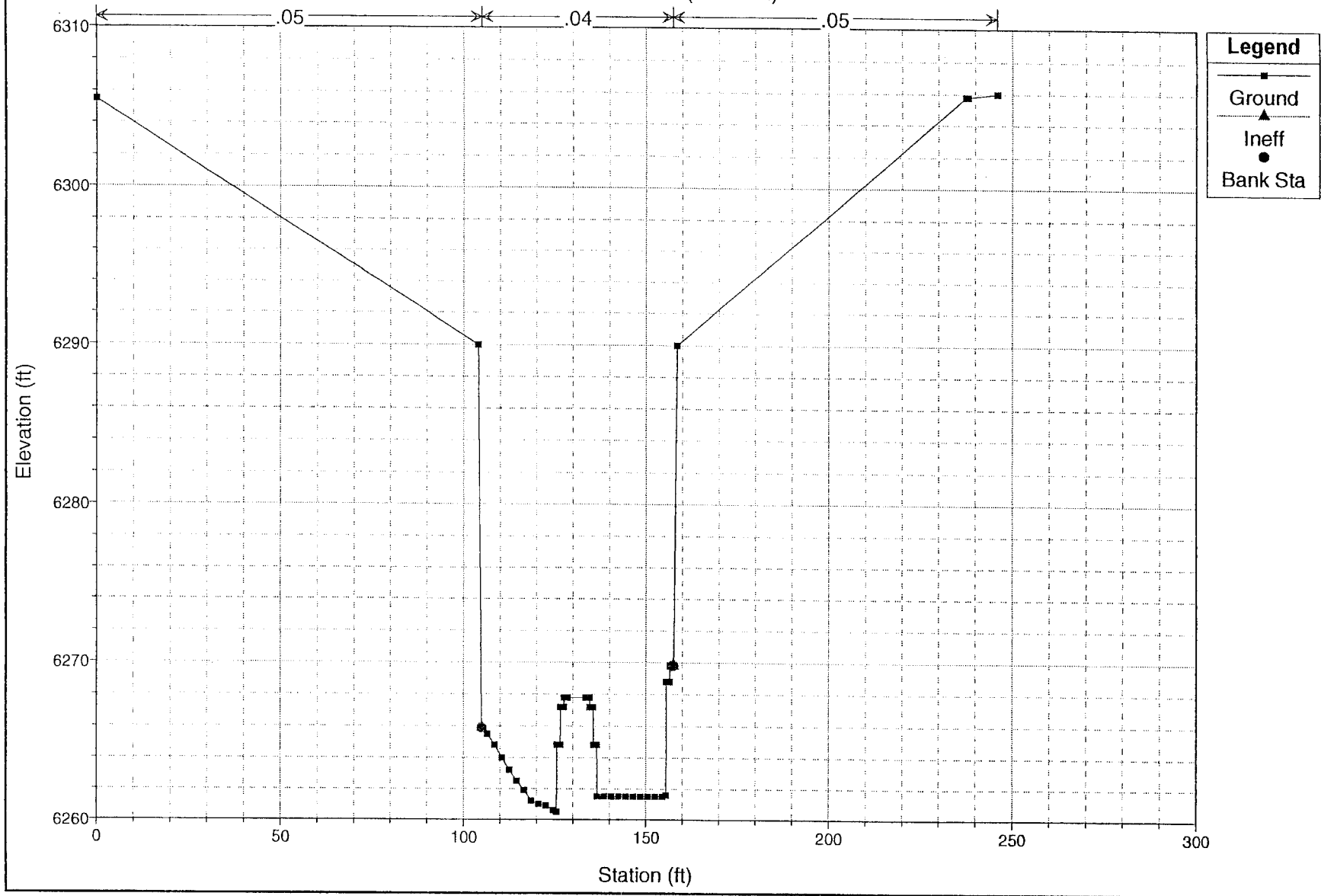


Cottonwood Creek  
XS @ D/S FACE OF VINCENT DRIVE RS = 1.4 (x 1000 ft)



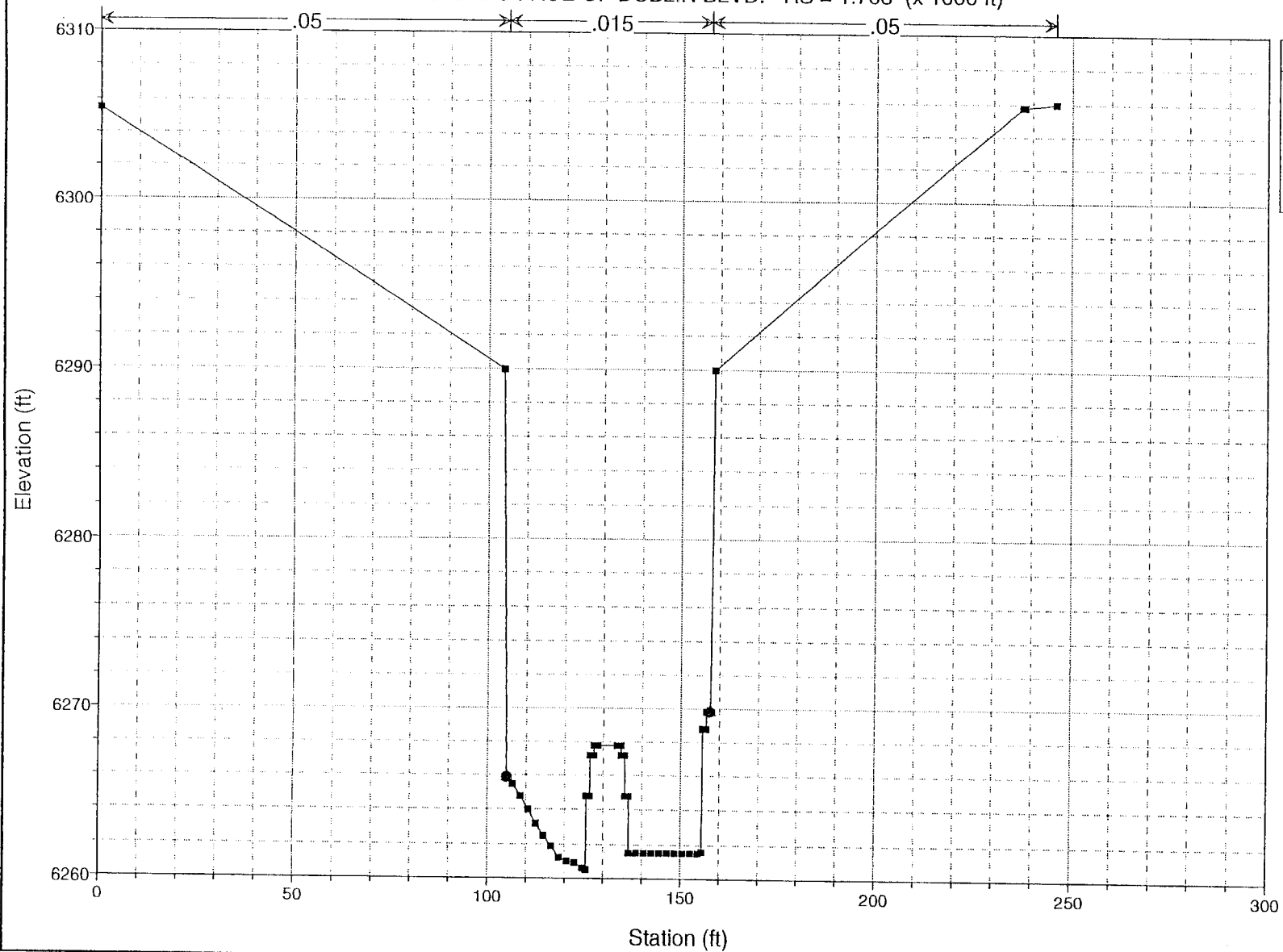
# Cottonwood Creek

RS = 1.709 (x 1000 ft)

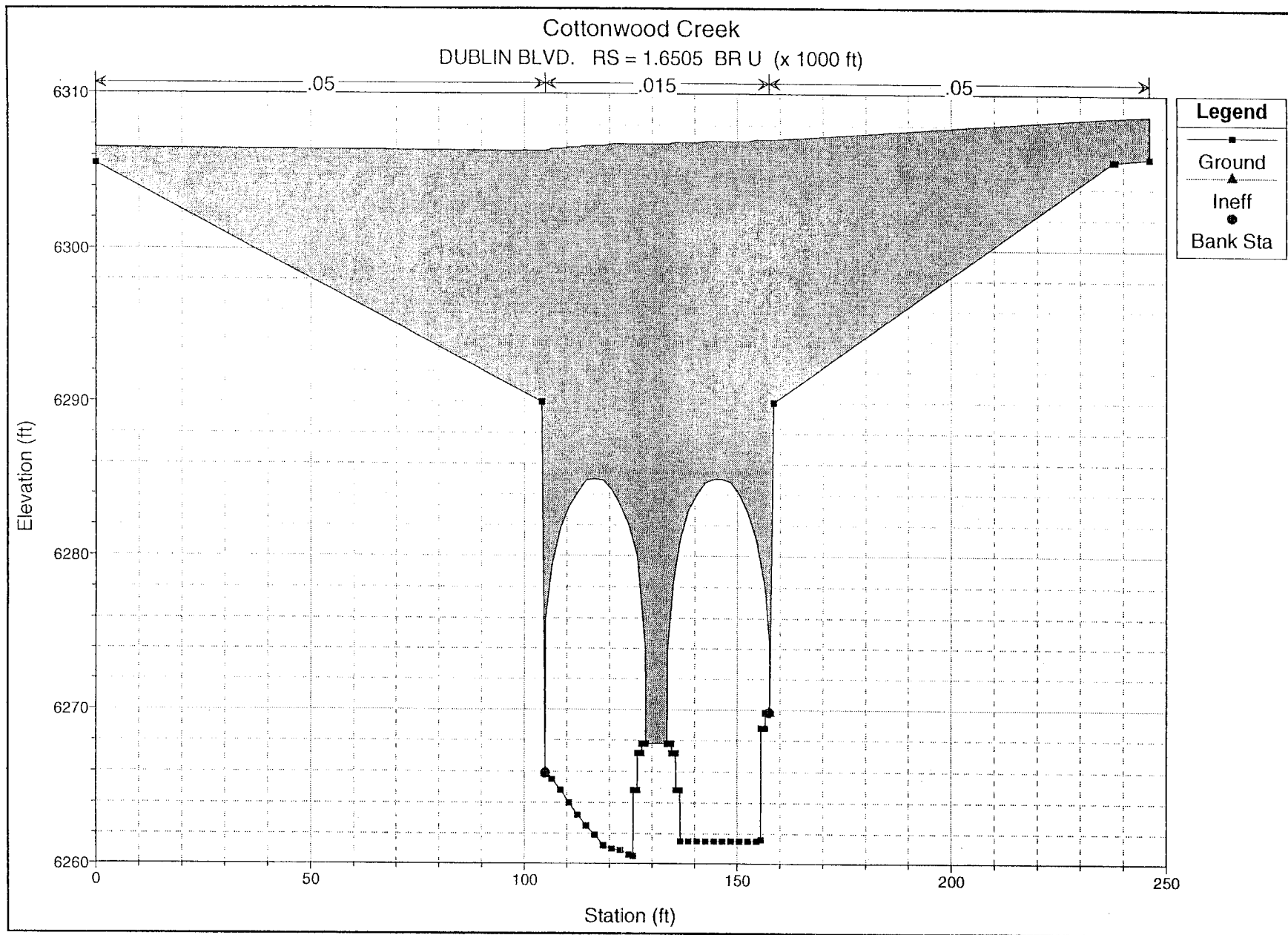


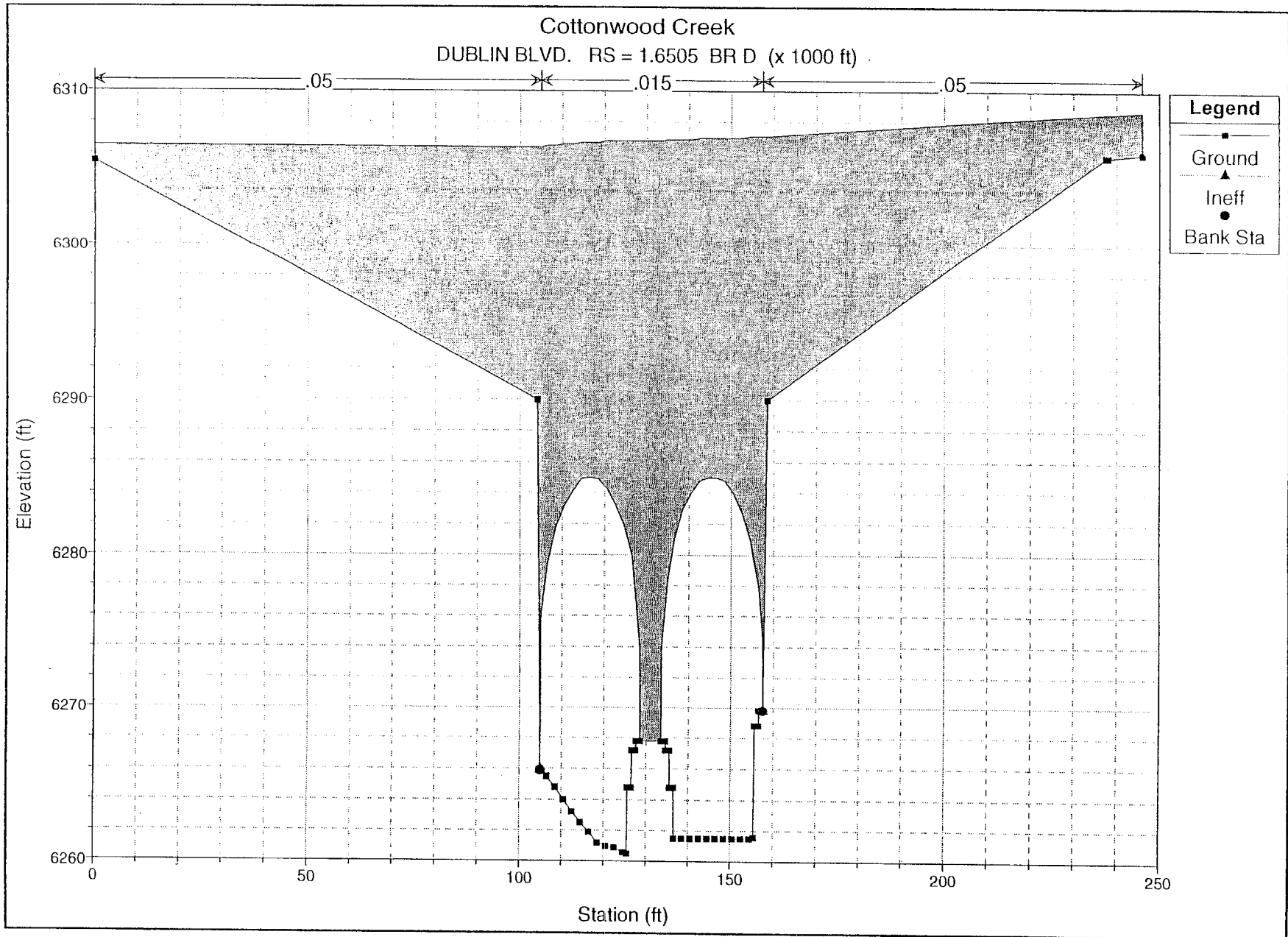
# Cottonwood Creek

XS @ U/S FACE OF DUBLIN BLVD. RS = 1.708 (x 1000 ft)



- Legend**
- Ground
  - Ineff
  - Bank Sta

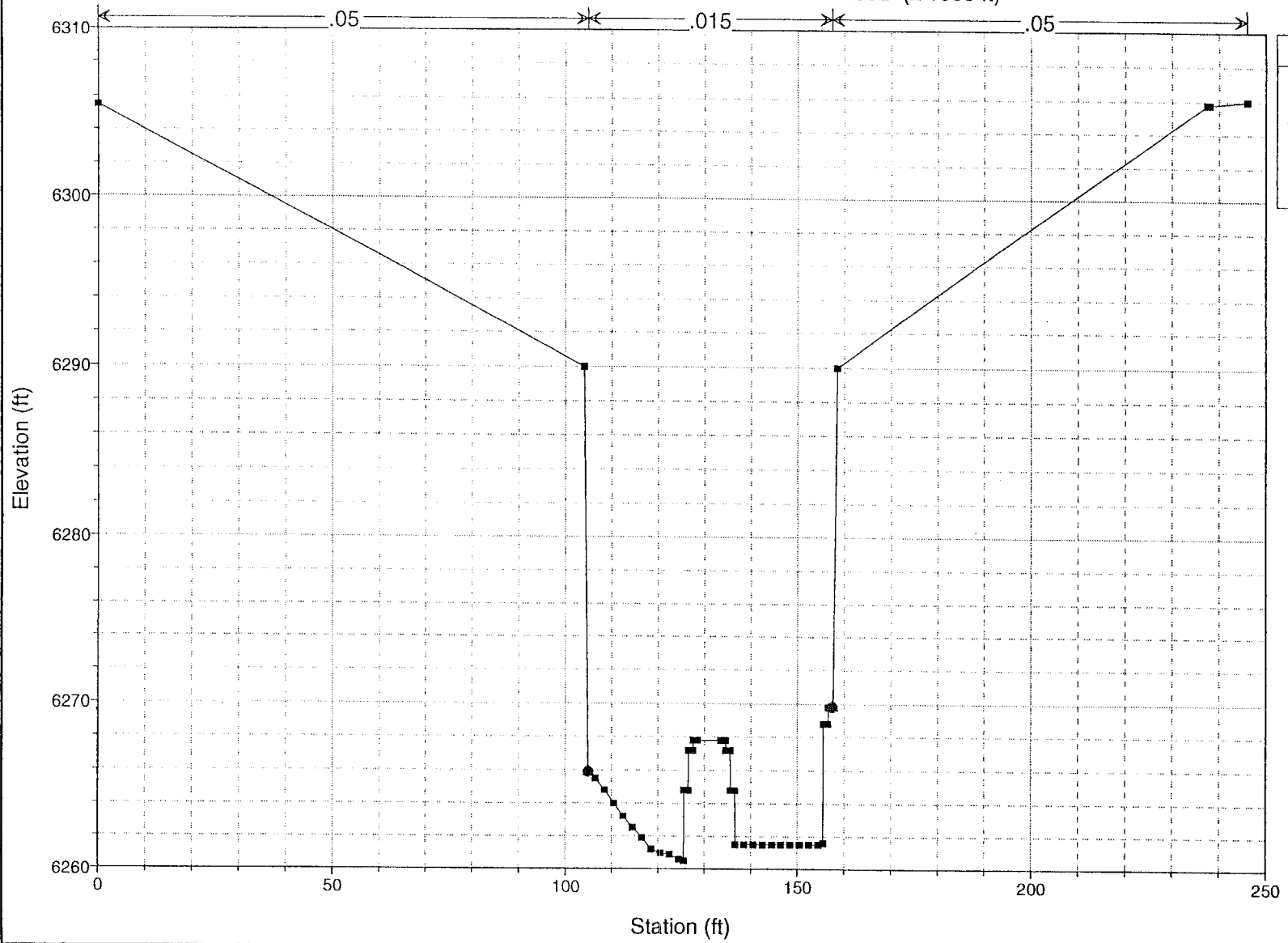






# Cottonwood Creek

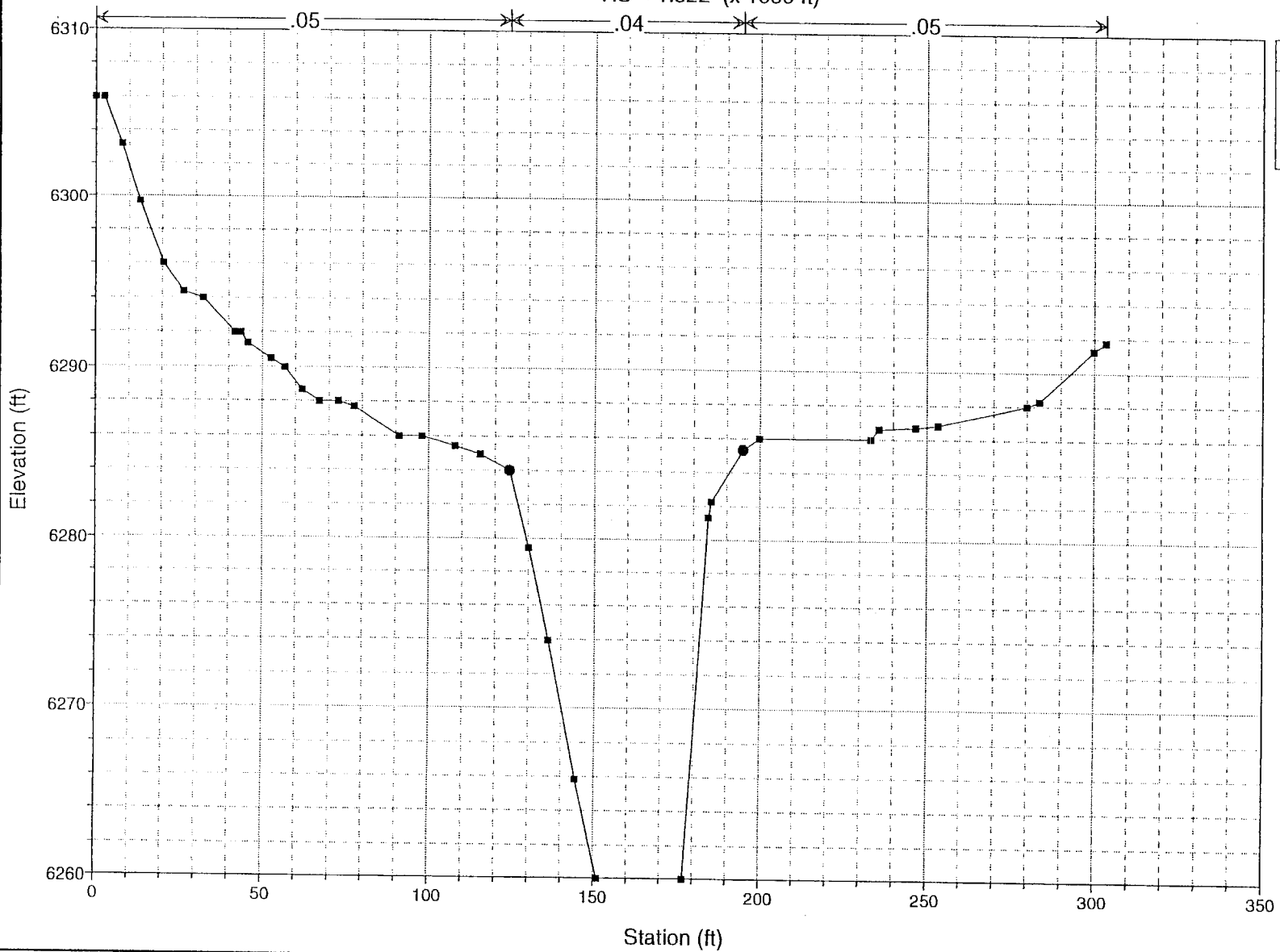
XS @ D/S FACE OF DUBLIN BLVD. RS = 1.592 (x 1000 ft)



- Legend**
- Ground
  - Ineff
  - Bank Sta

# Cottonwood Creek

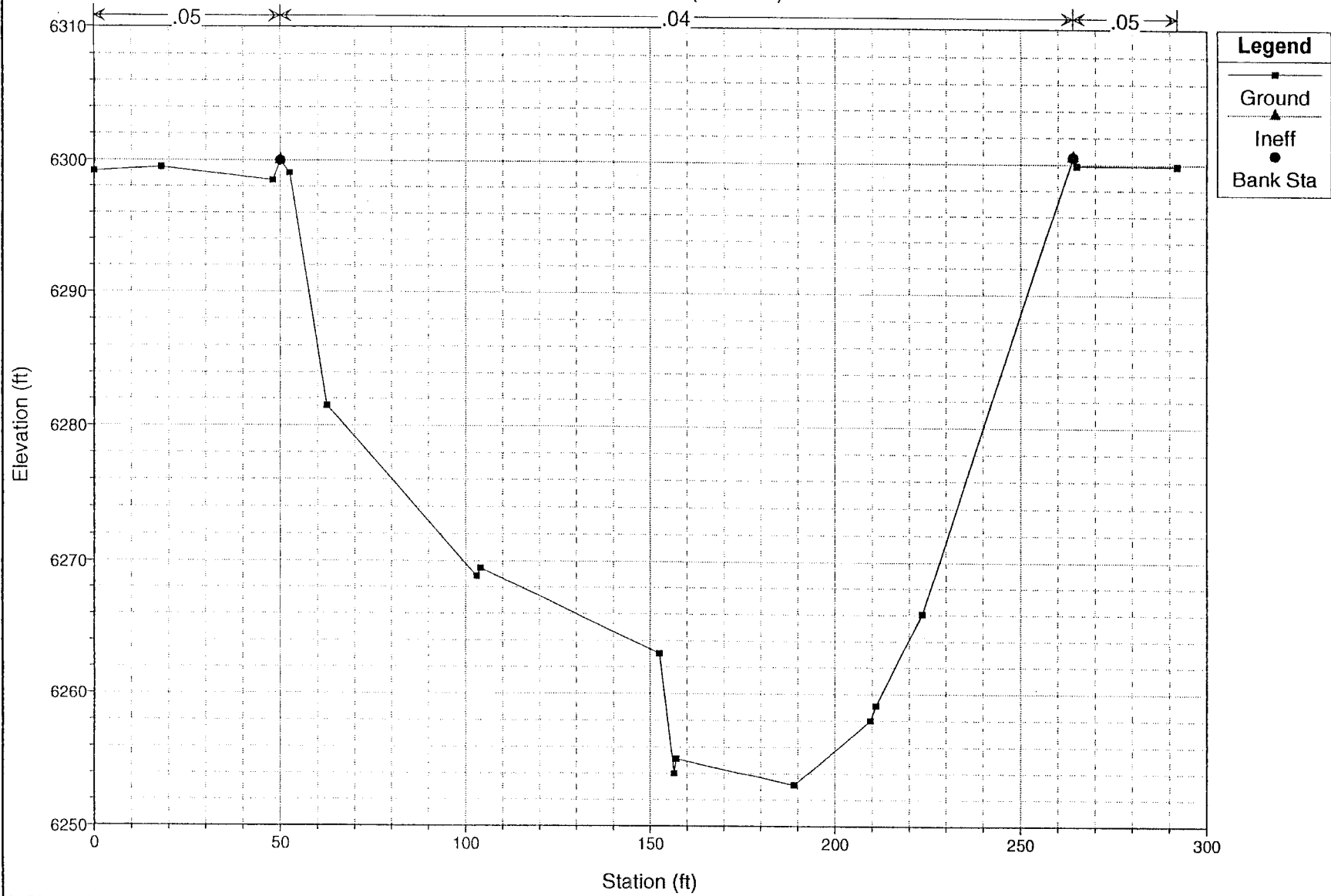
RS = 1.522 (x 1000 ft)



**Legend**

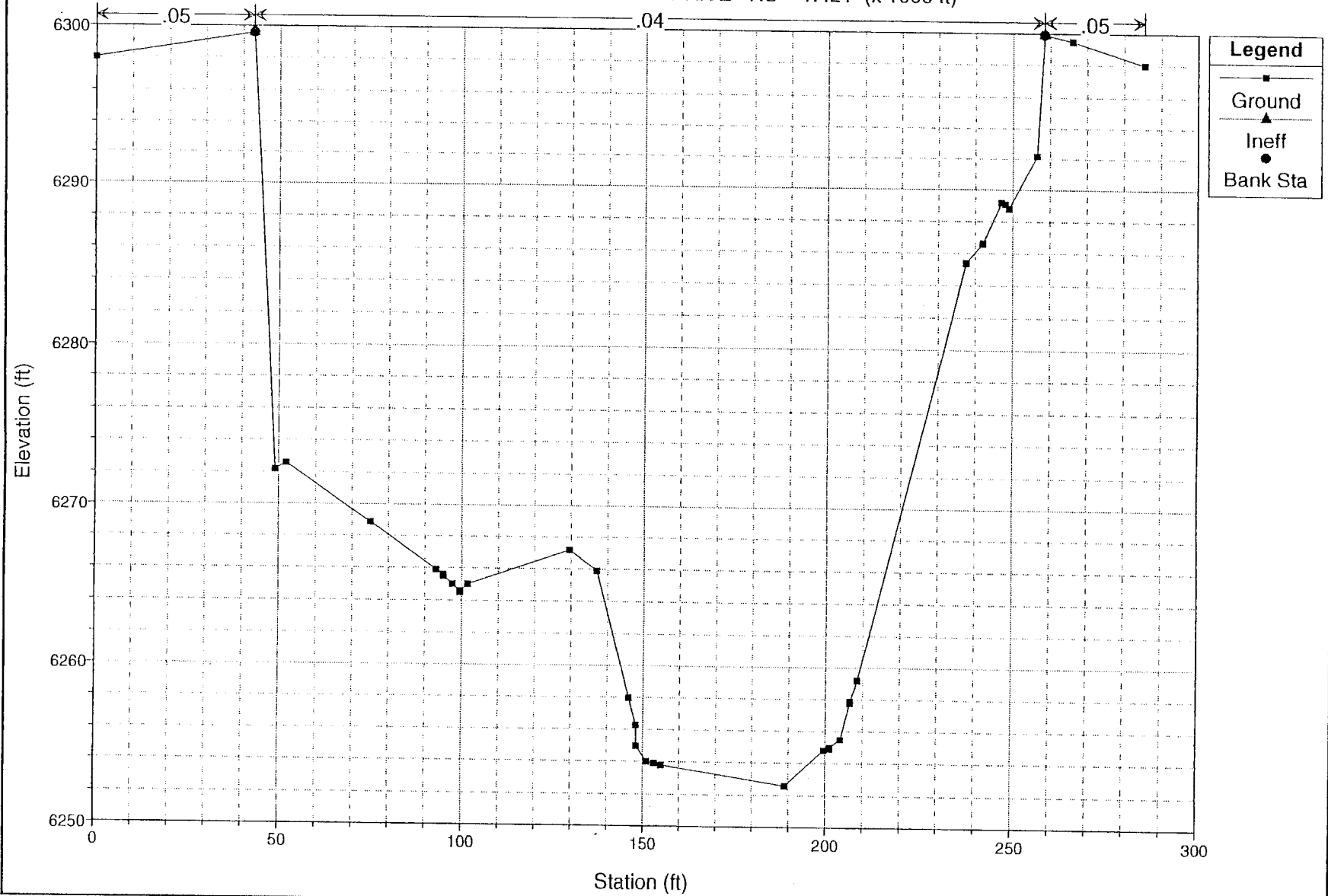
- Ground
- Bank Sta

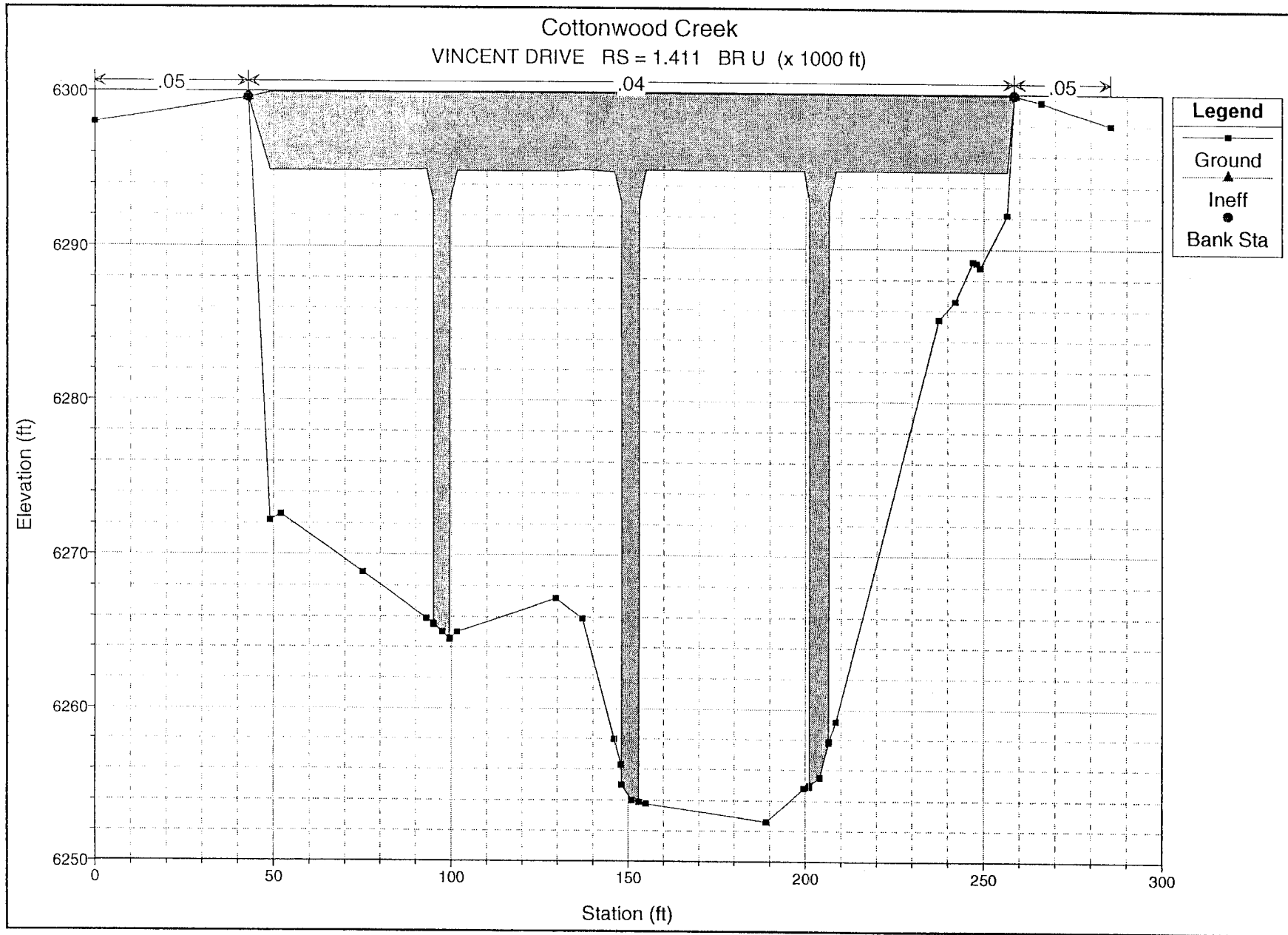
Cottonwood Creek  
RS = 1.422 (x 1000 ft)



# Cottonwood Creek

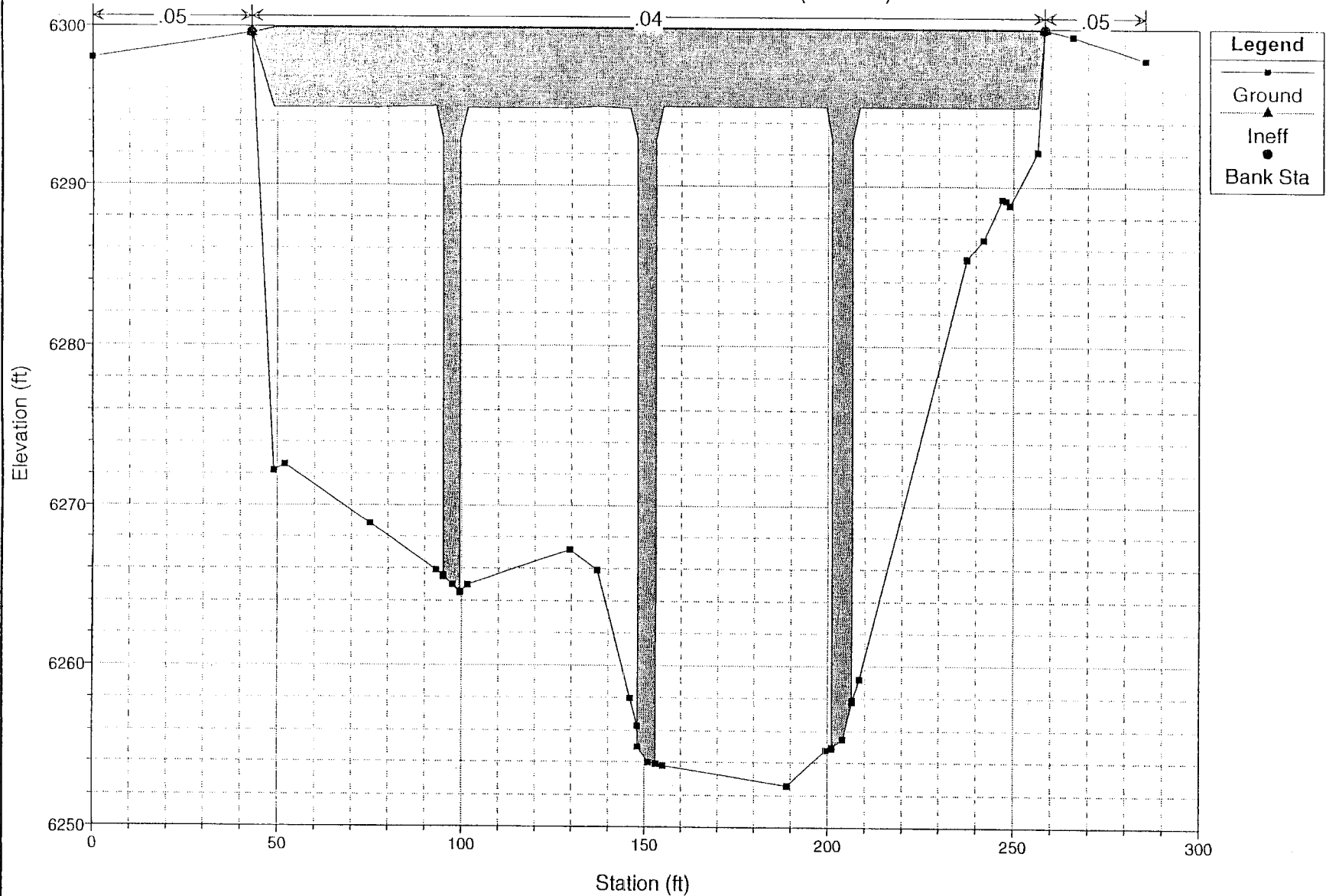
XS @ U/S FACE OF VINCENT DRIVE RS = 1.421 (x 1000 ft)



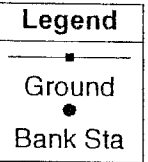
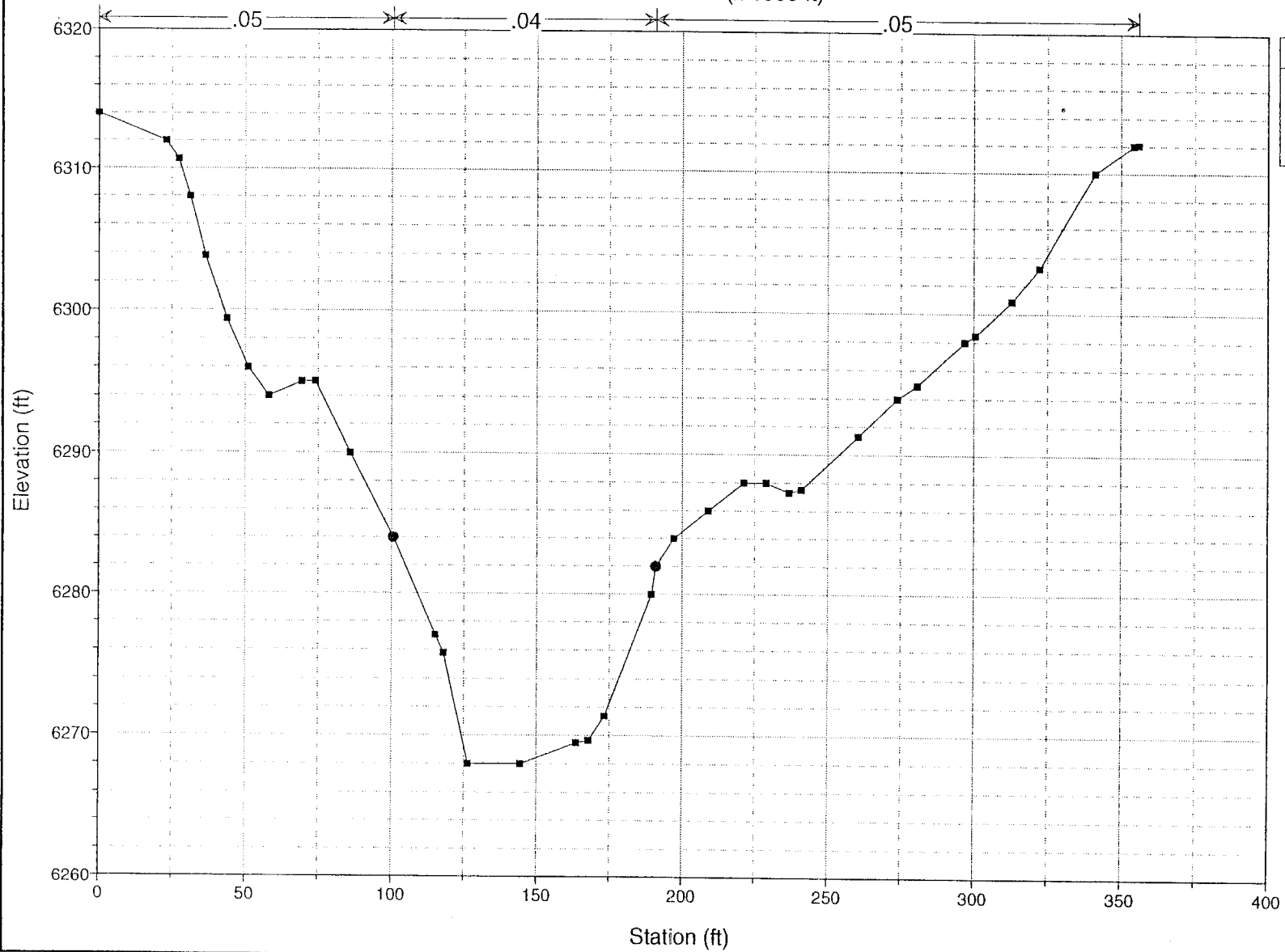


# Cottonwood Creek

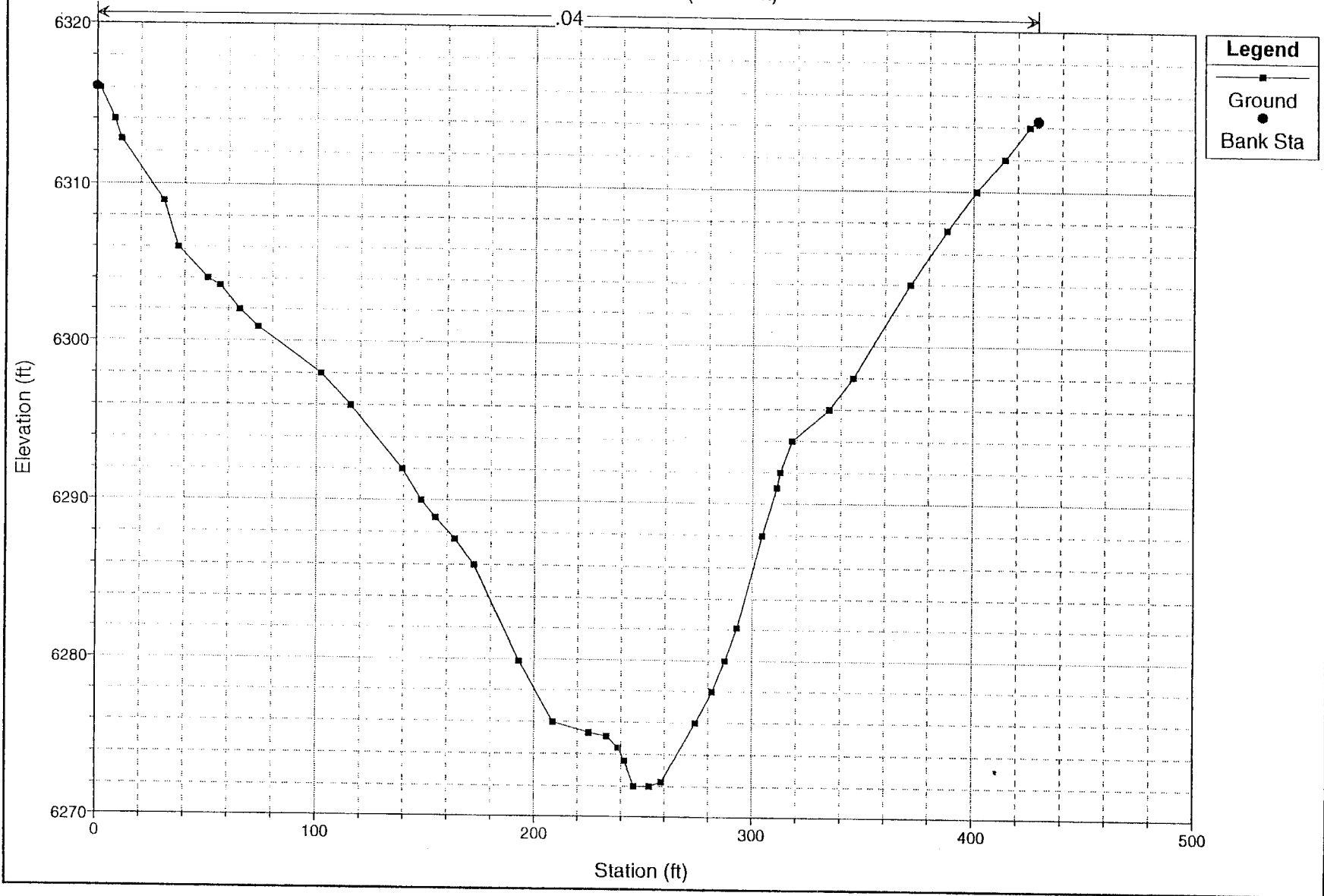
VINCENT DRIVE RS = 1.411 BR D (x 1000 ft)



Cottonwood Creek  
RS = 1.981 (x 1000 ft)



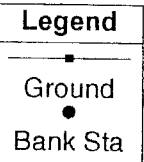
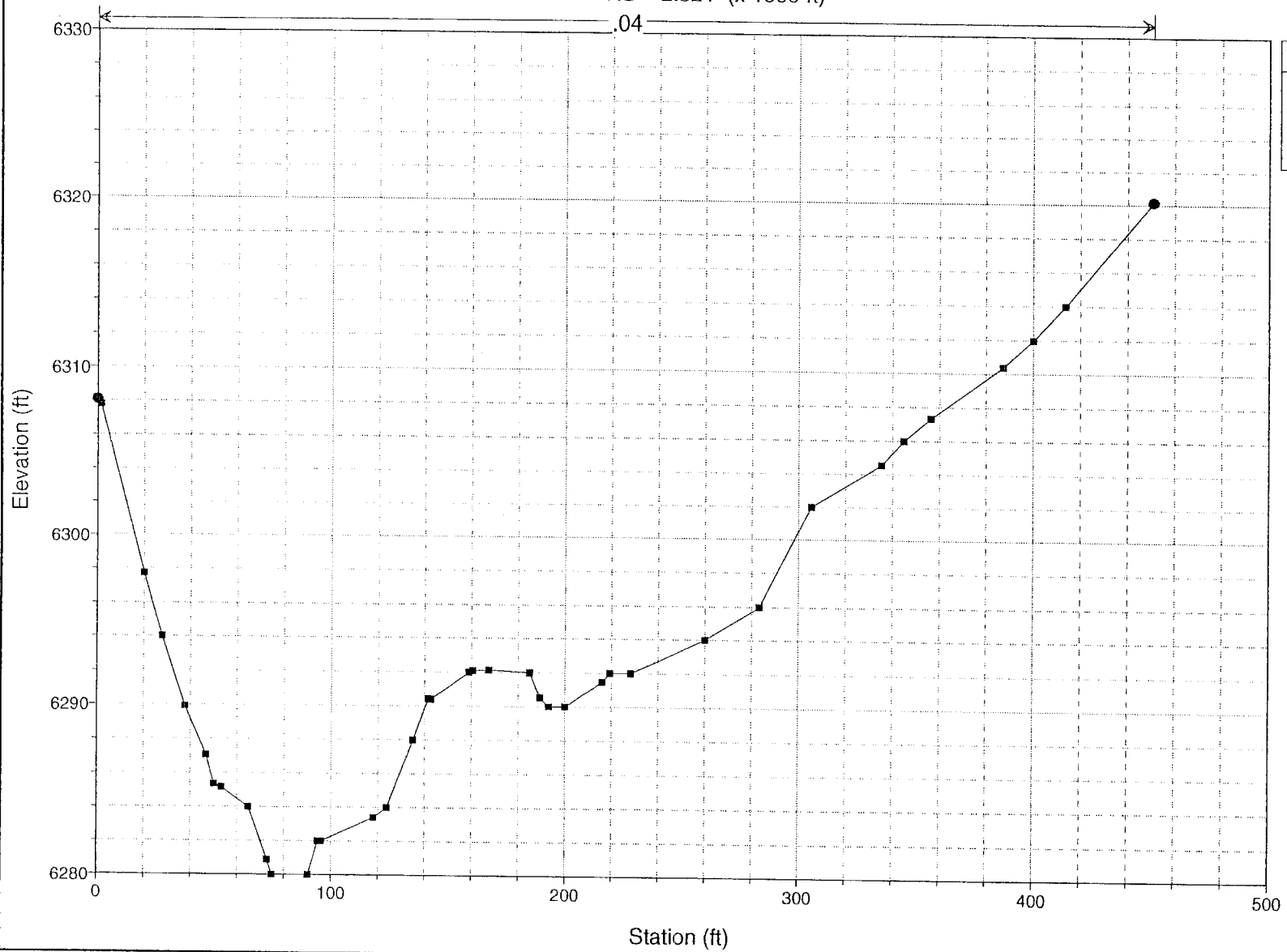
Cottonwood Creek  
RS = 2.217 (x 1000 ft)



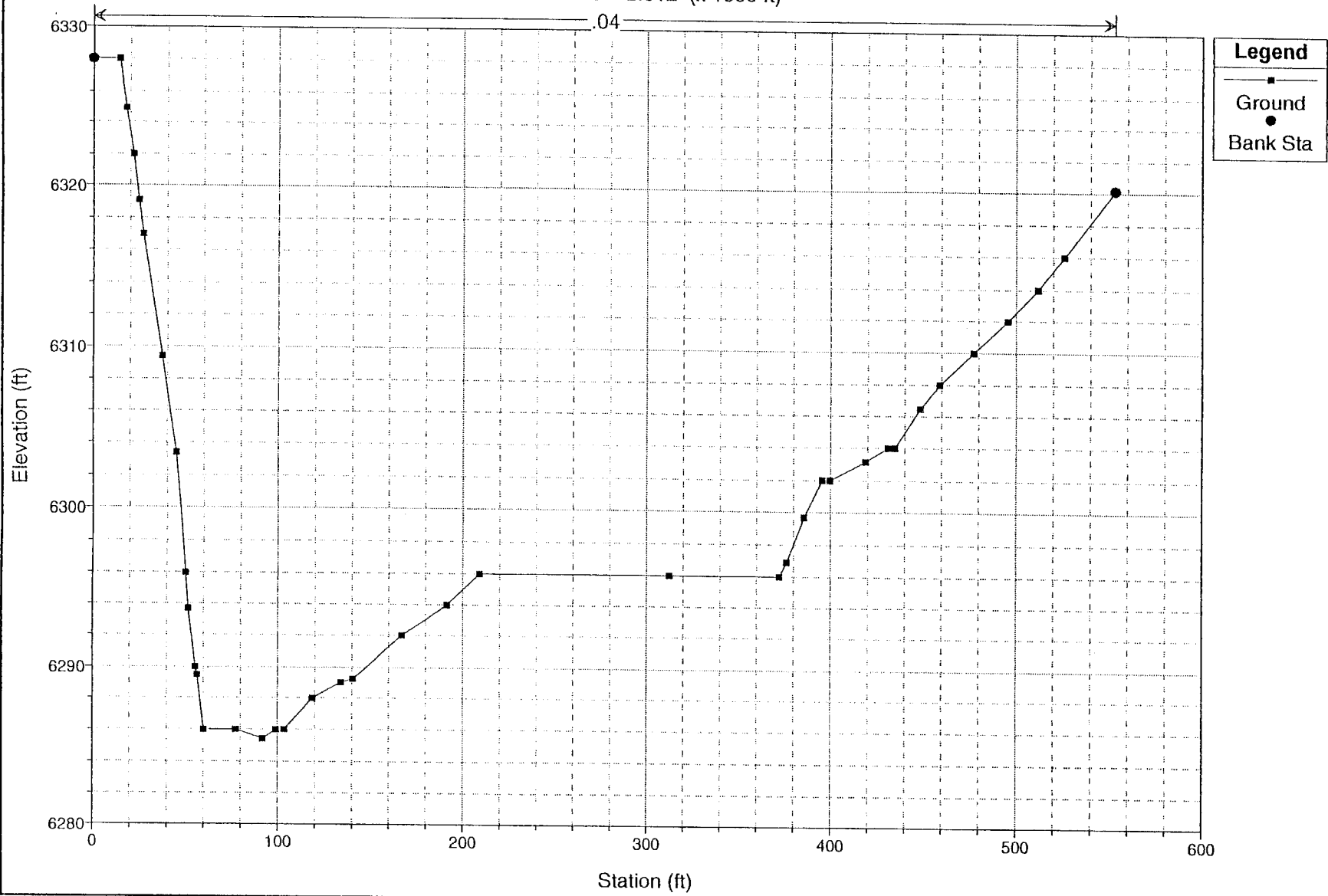


# Cottonwood Creek

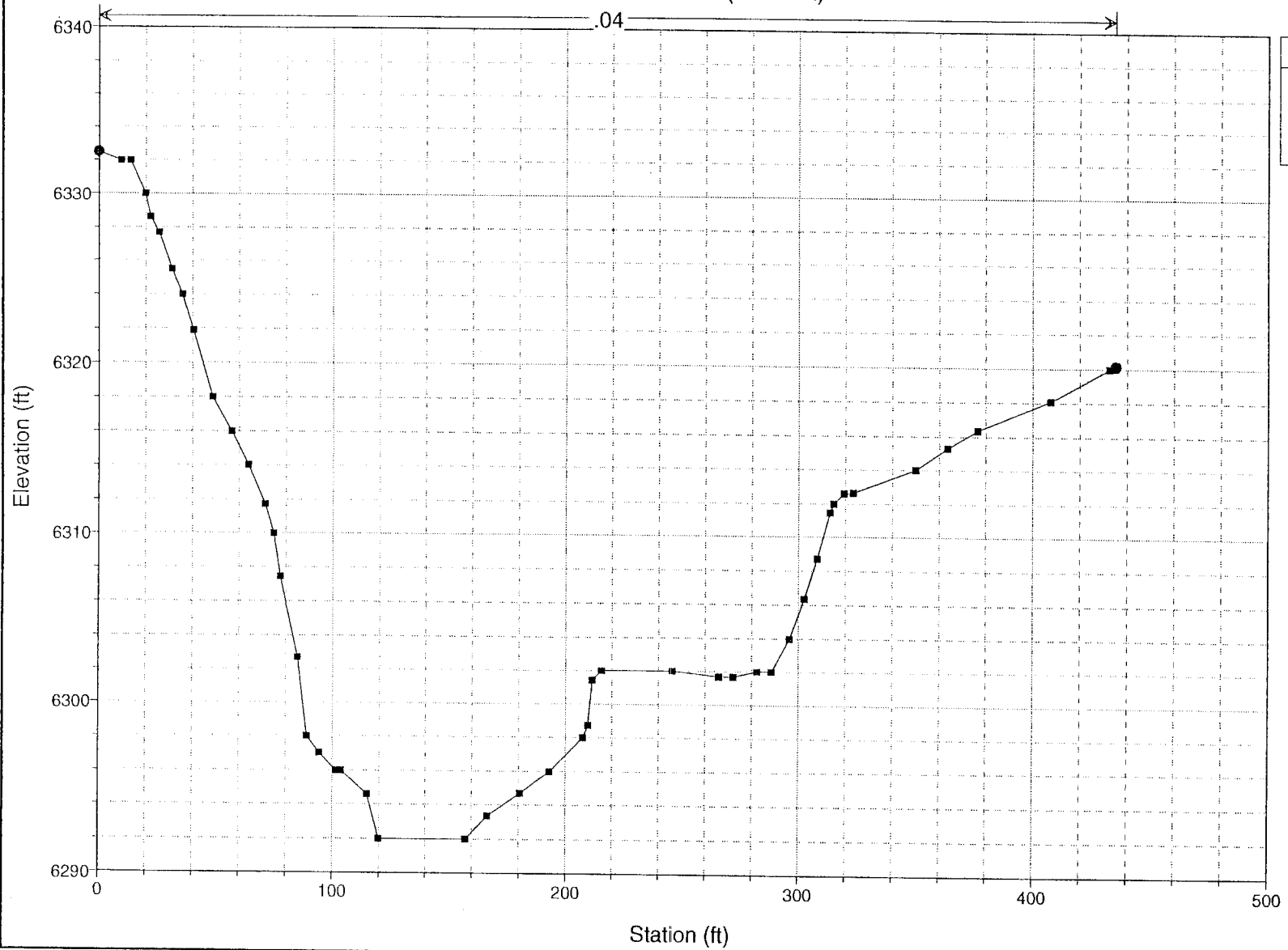
RS = 2.521 (x 1000 ft)



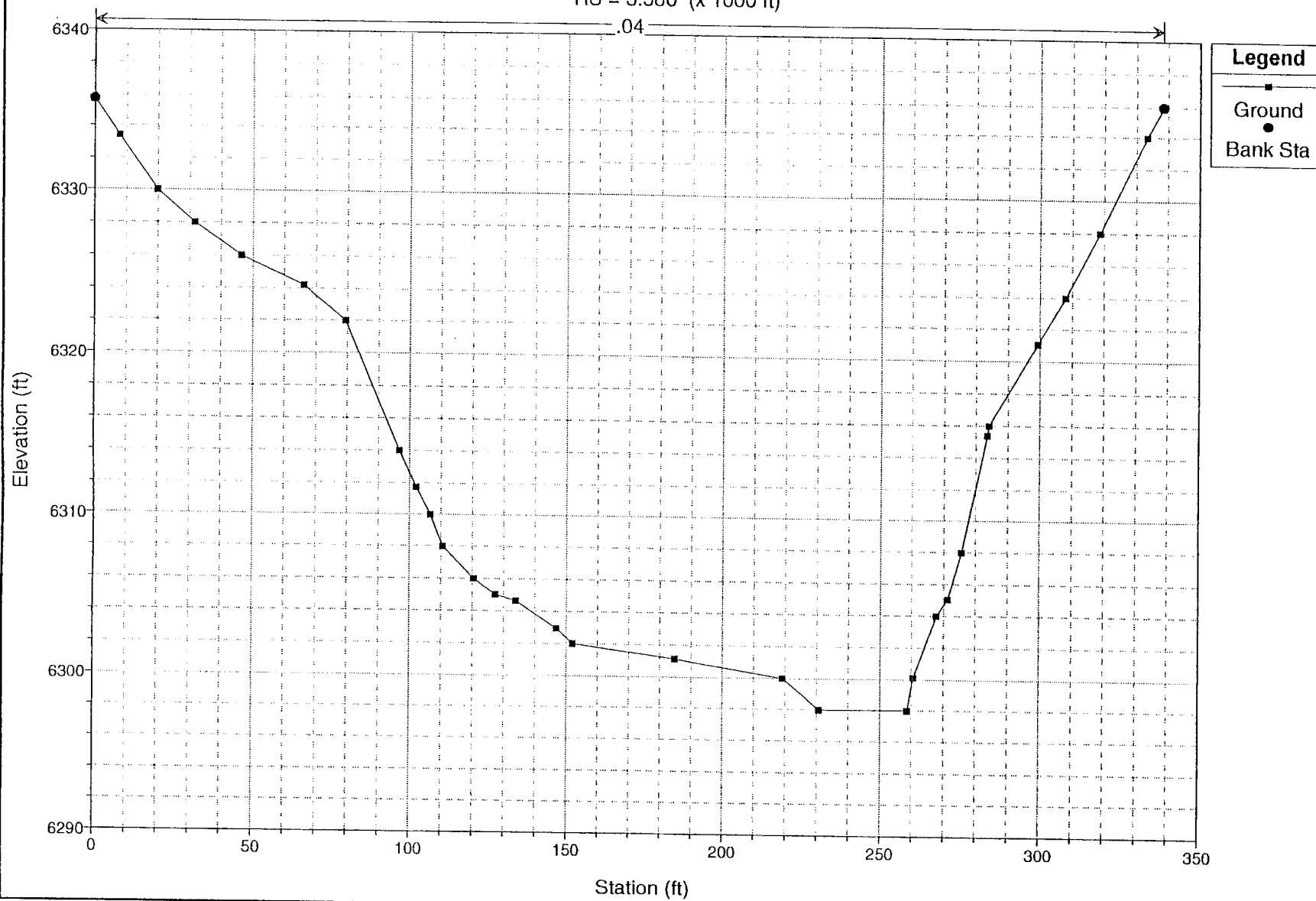
Cottonwood Creek  
RS = 2.812 (x 1000 ft)



Cottonwood Creek  
RS = 3.243 (x 1000 ft)



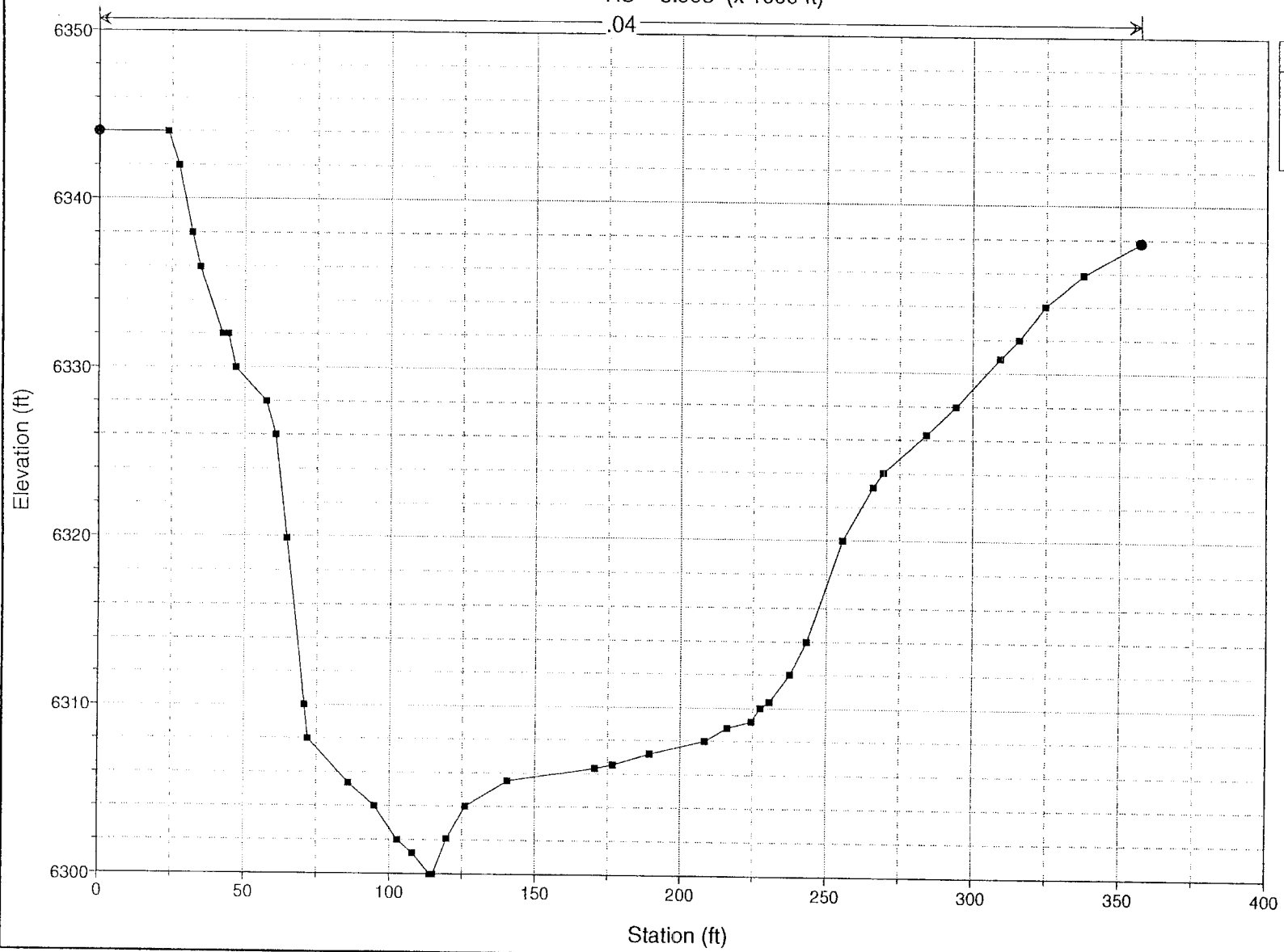
Cottonwood Creek  
RS = 3.586 (x 1000 ft)



# Cottonwood Creek

RS = 3.903 (x 1000 ft)

.04

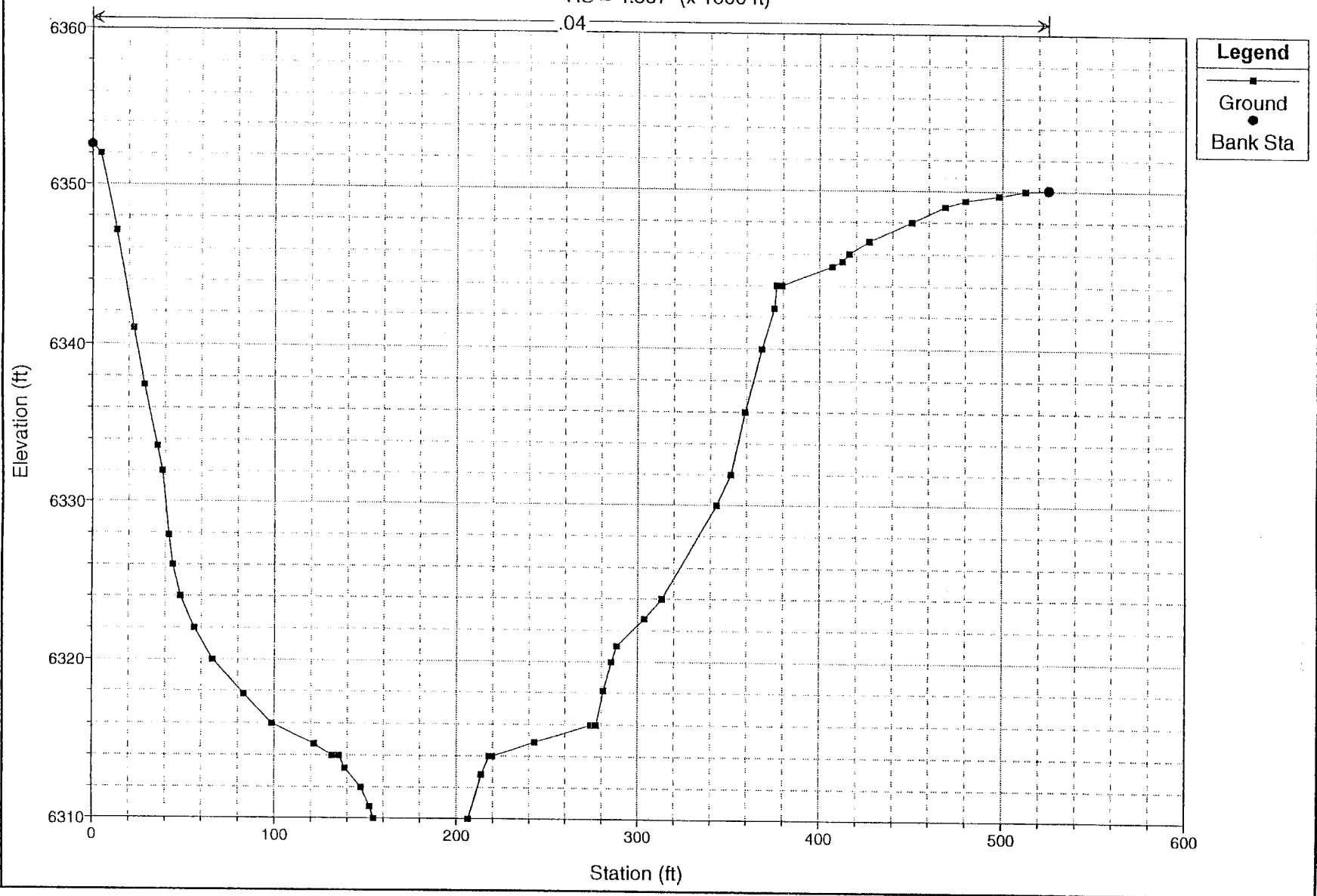


## Legend

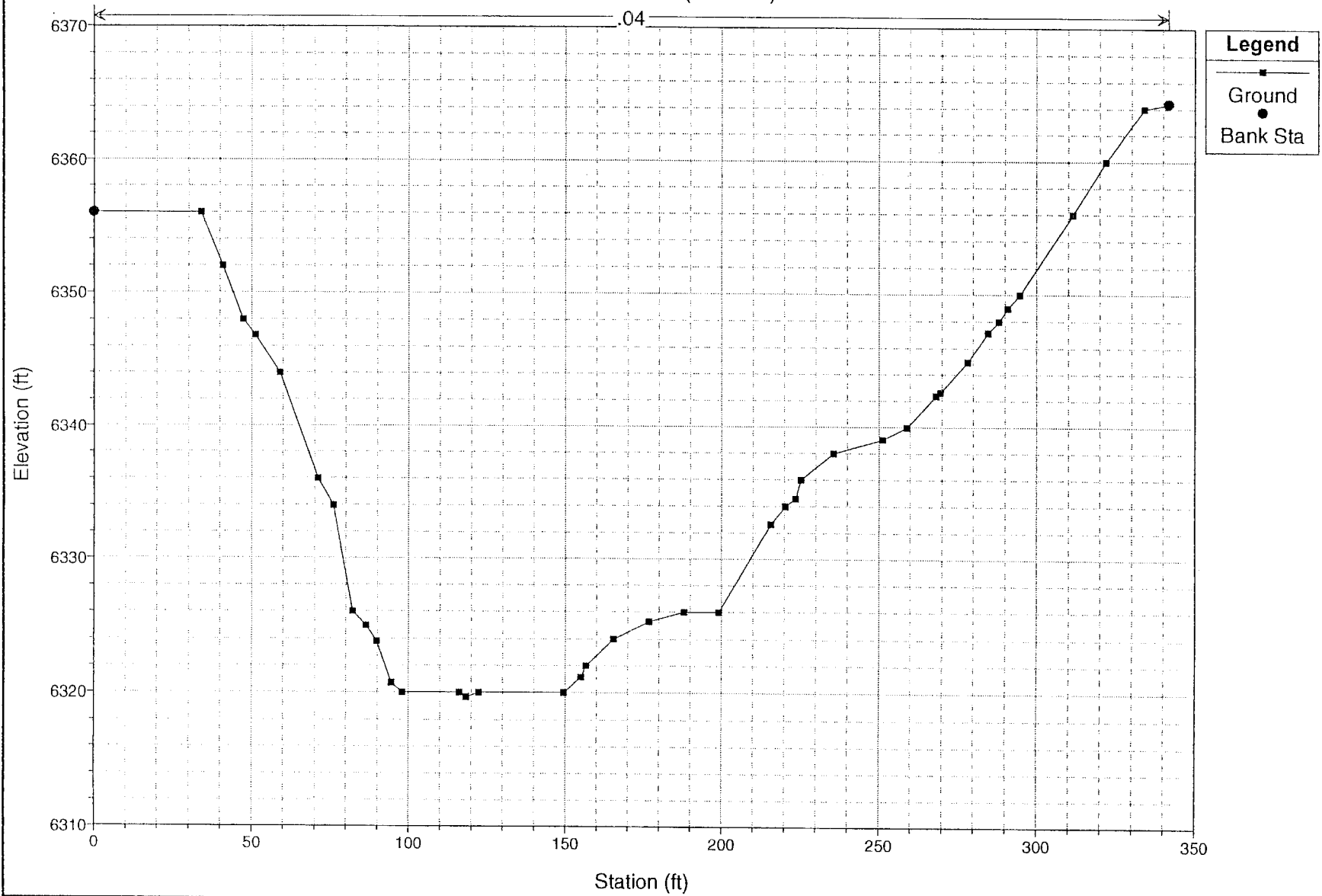
Ground

Bank Sta

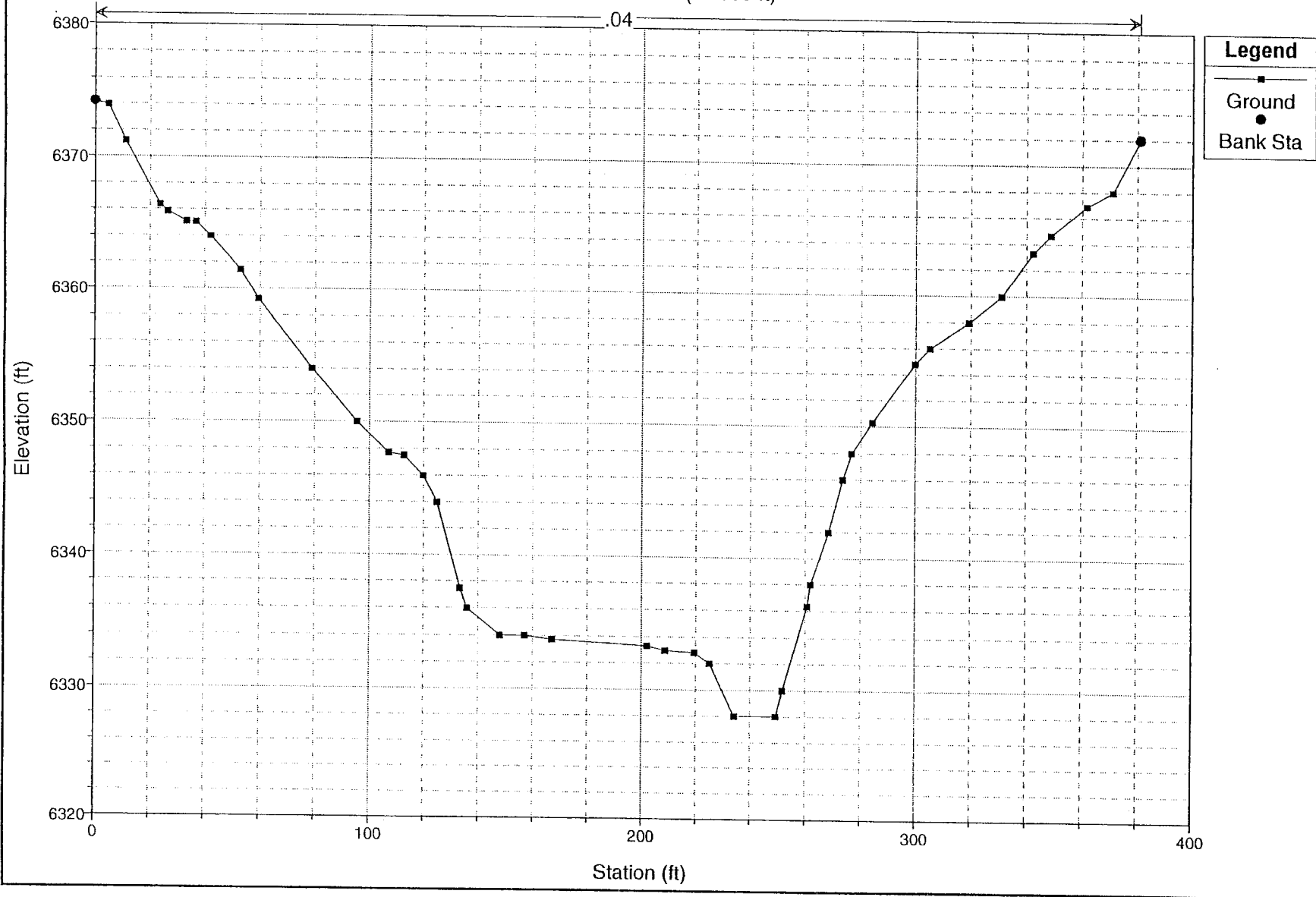
Cottonwood Creek  
RS = 4.367 (x 1000 ft)



Cottonwood Creek  
RS = 5.028 (x 1000 ft)

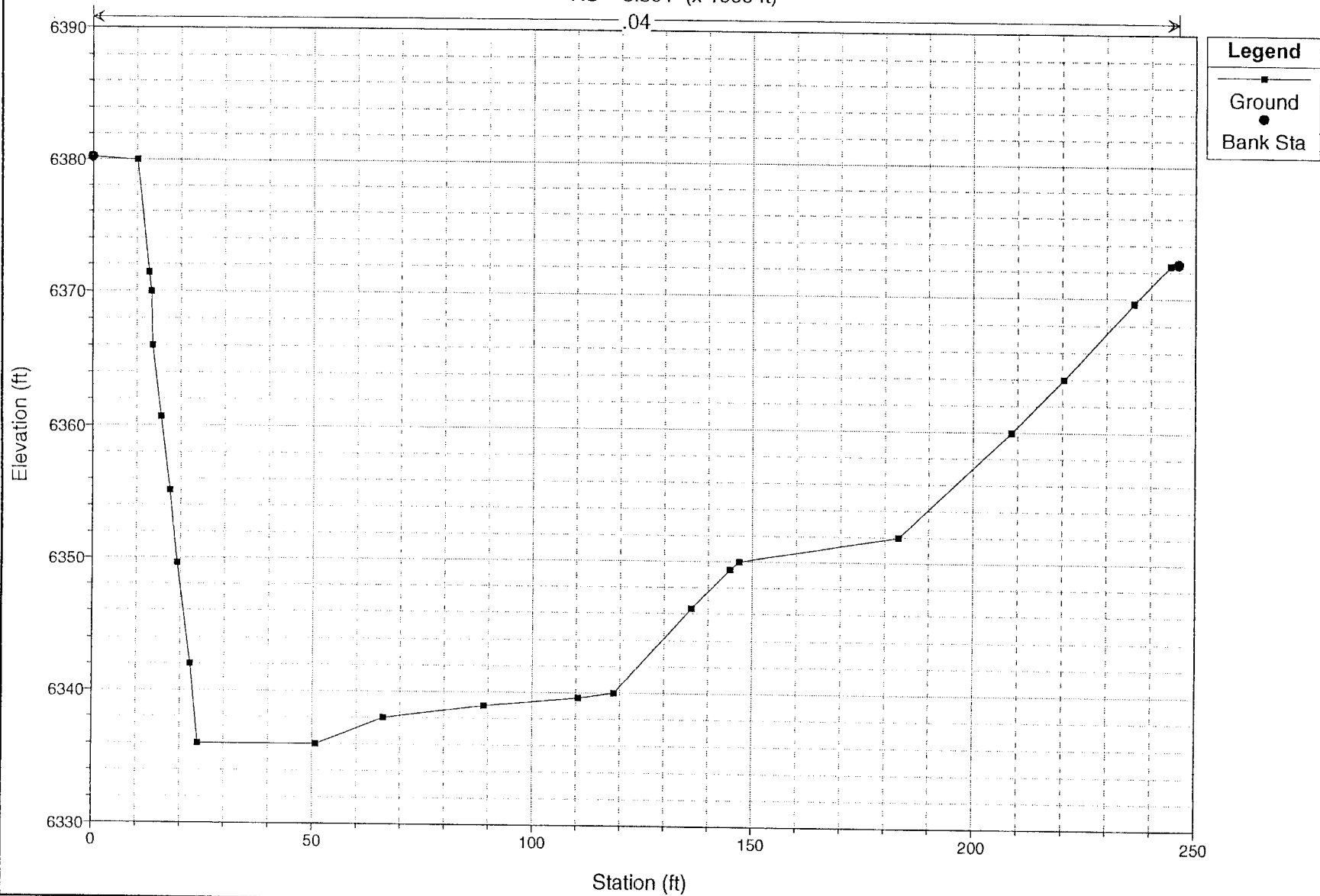


Cottonwood Creek  
RS = 5.468 (x 1000 ft)

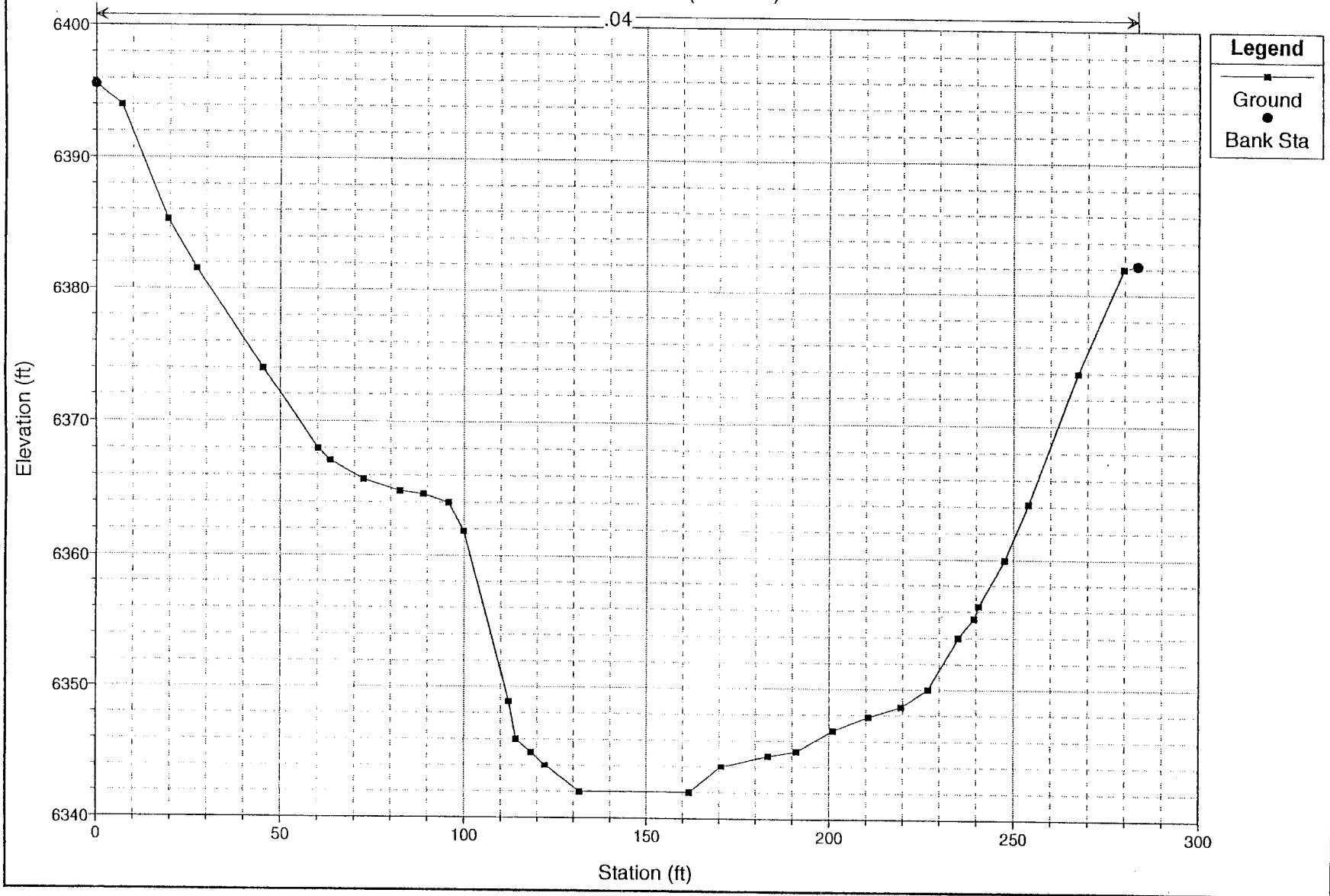




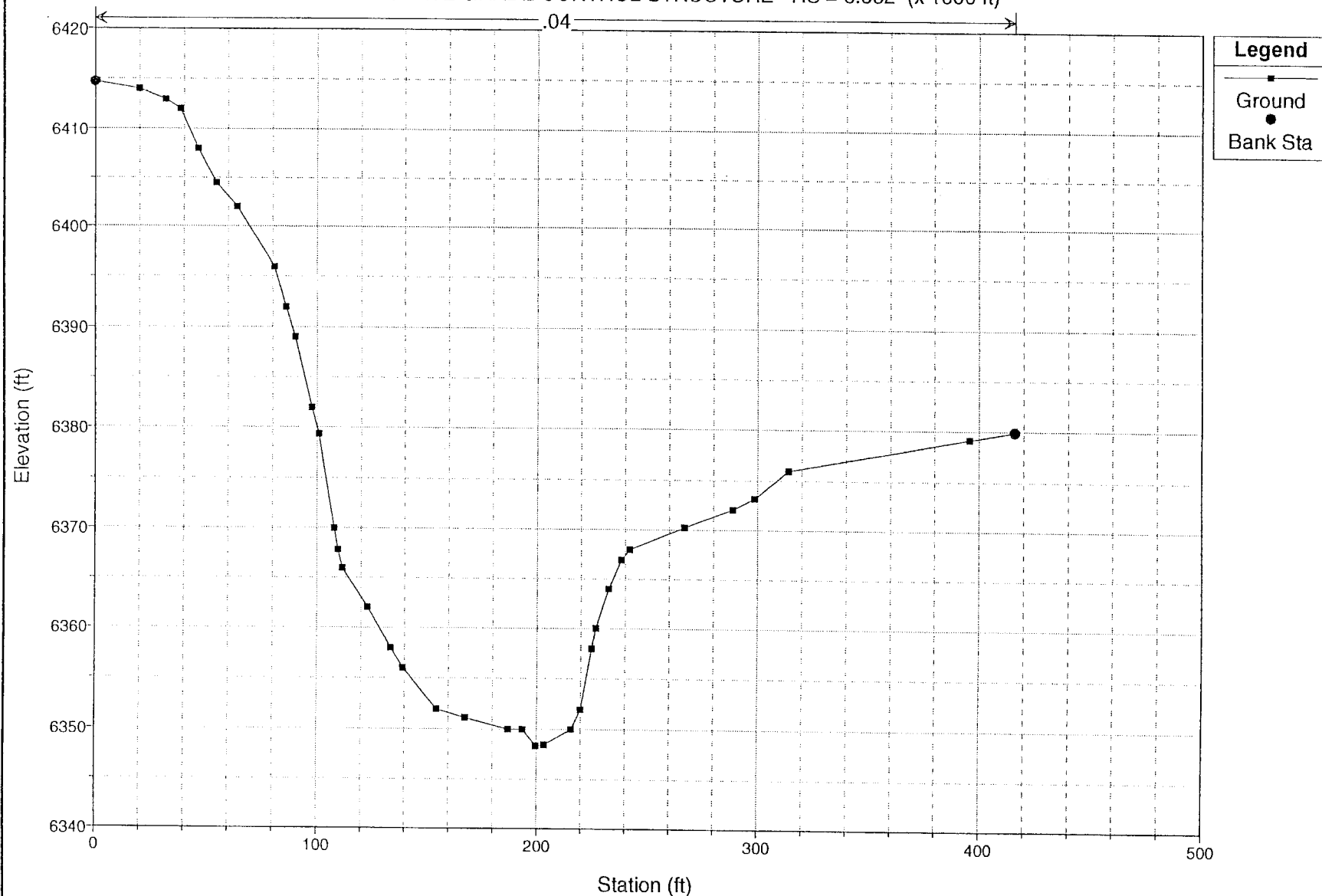
Cottonwood Creek  
RS = 5.801 (x 1000 ft)



Cottonwood Creek  
RS = 6.235 (x 1000 ft)

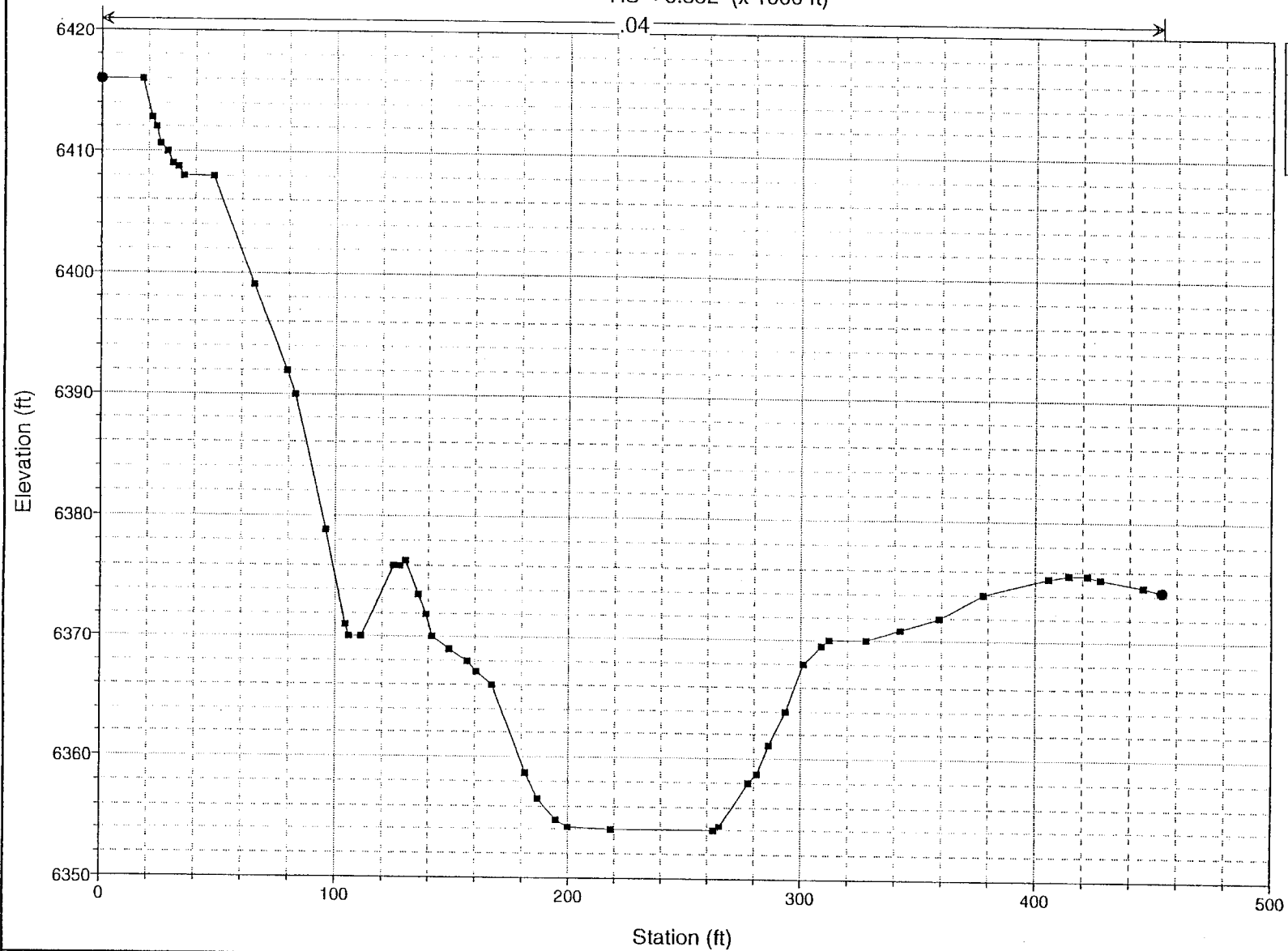


Cottonwood Creek  
CONCRETE GRADE CONTROL STRUCTURE RS = 6.652 (x 1000 ft)



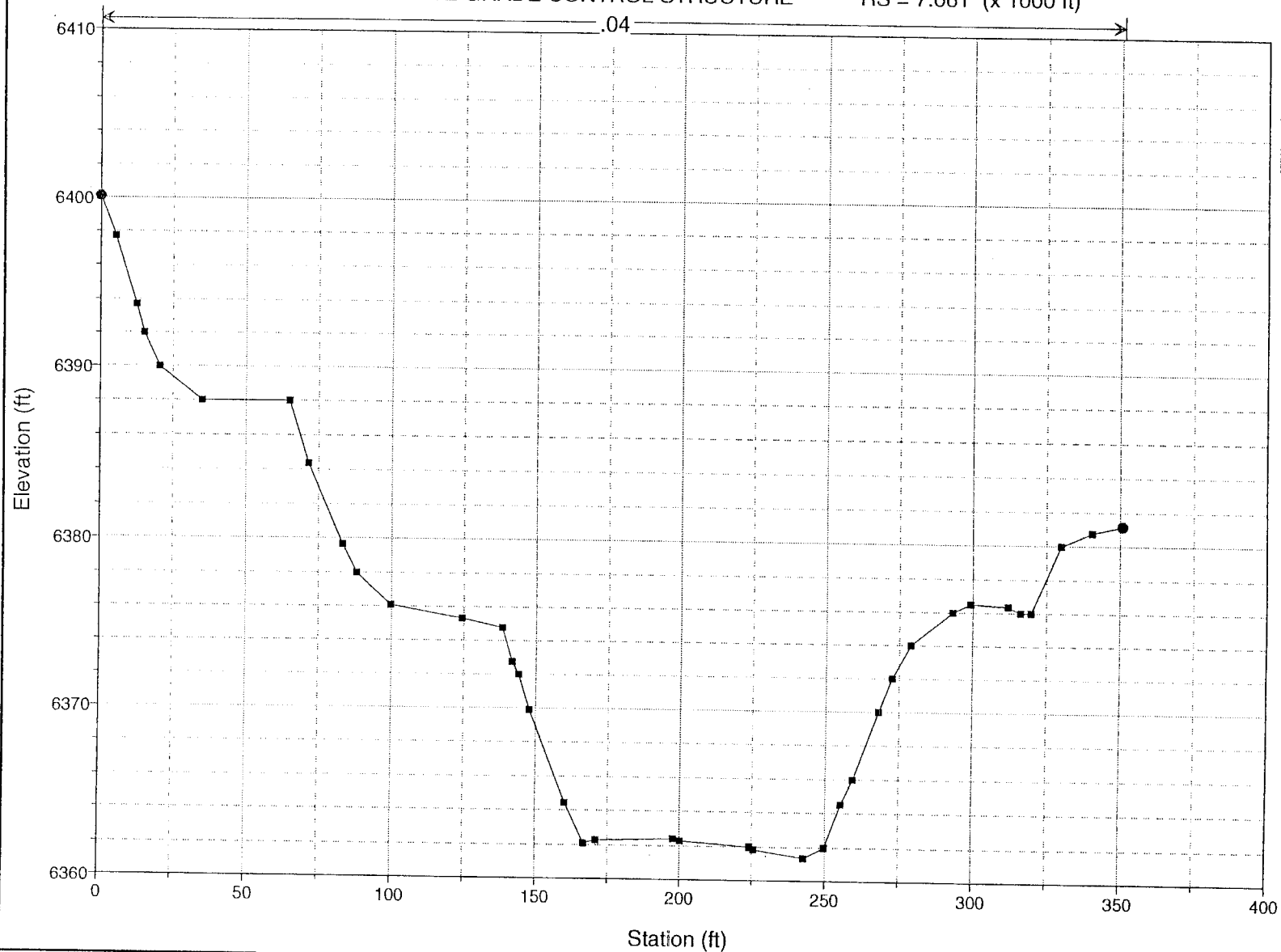
# Cottonwood Creek

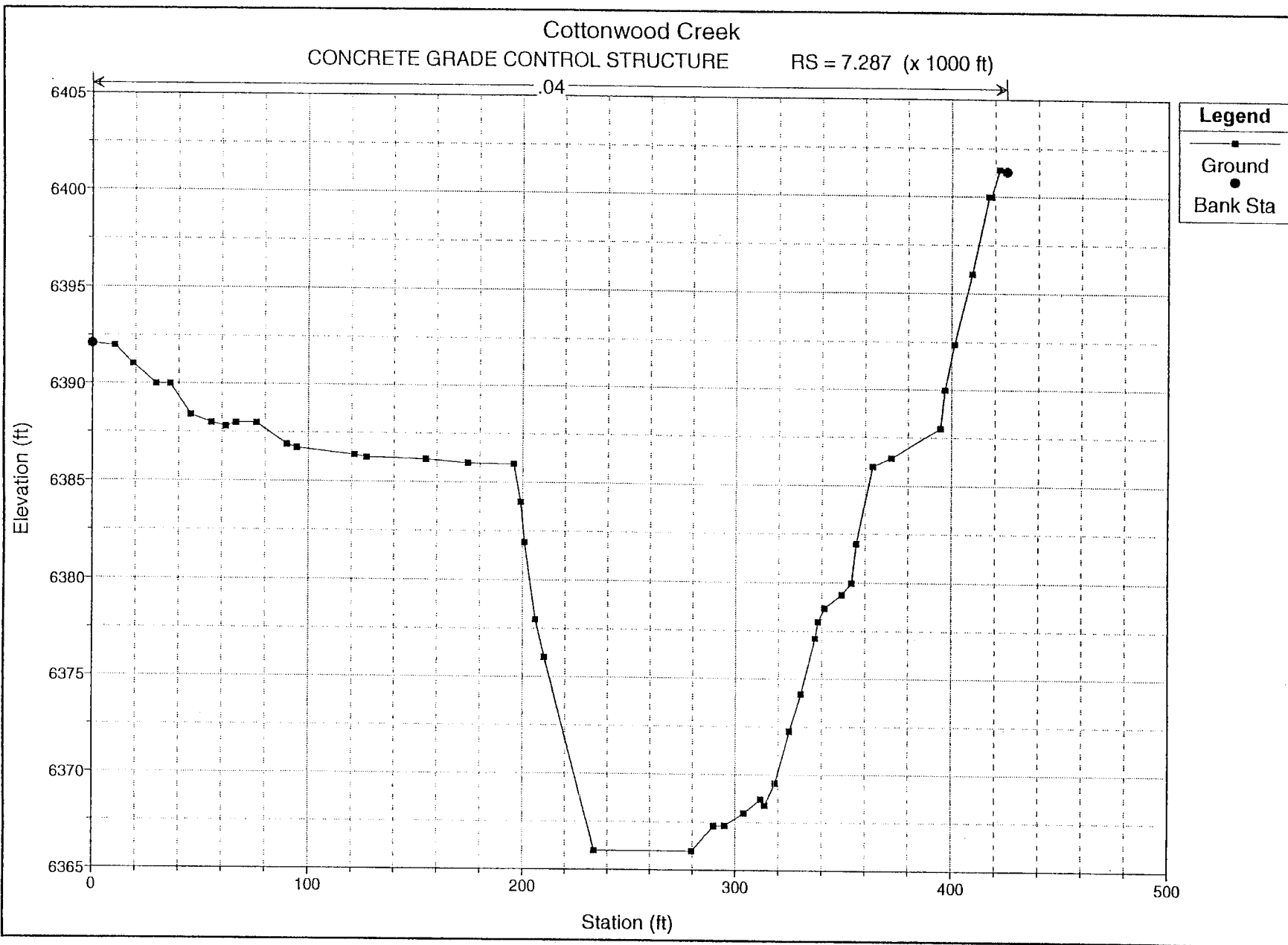
RS = 6.852 (x 1000 ft)



Cottonwood Creek  
CONCRETE GRADE CONTROL STRUCTURE

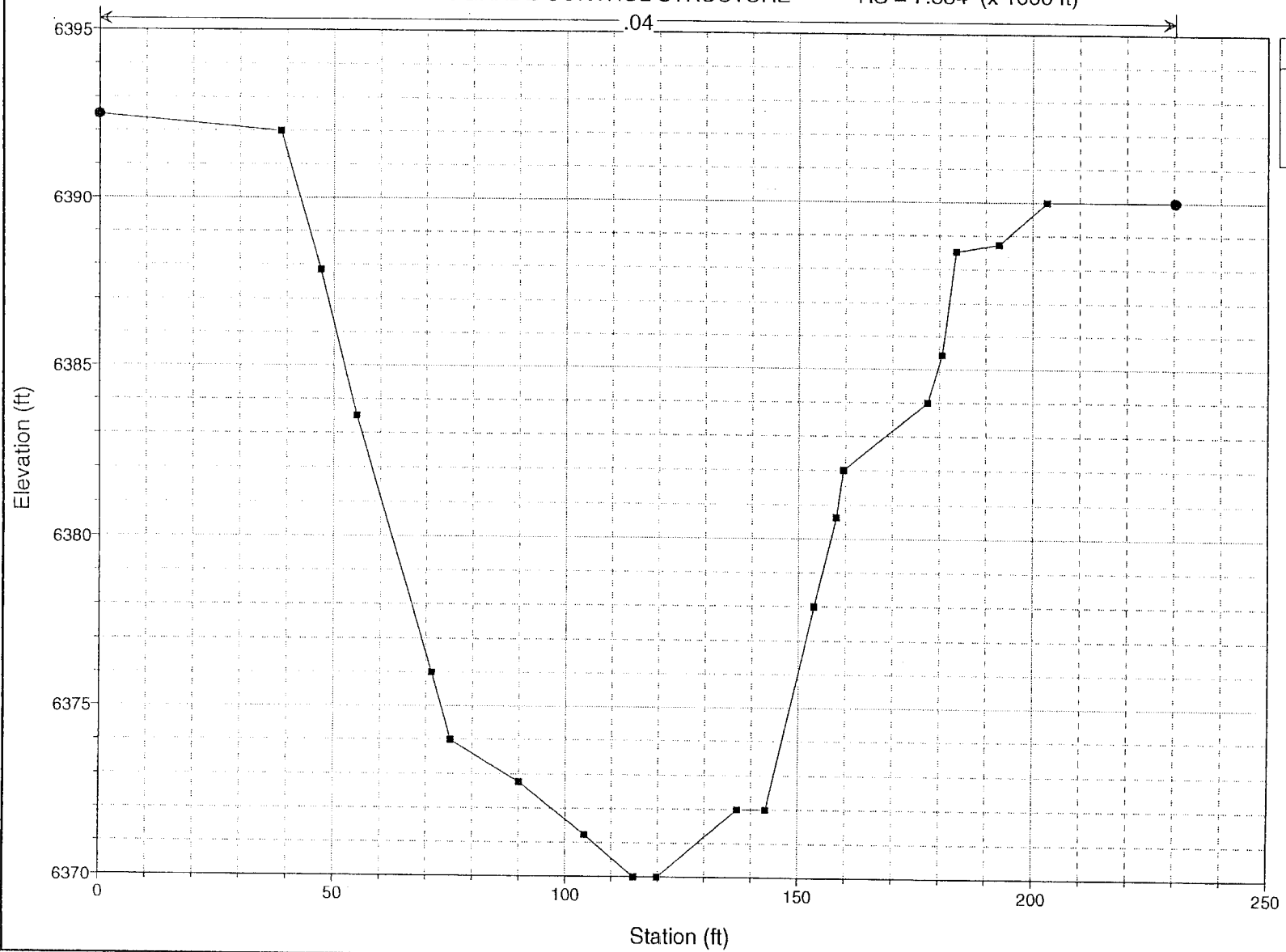
RS = 7.061 (x 1000 ft)





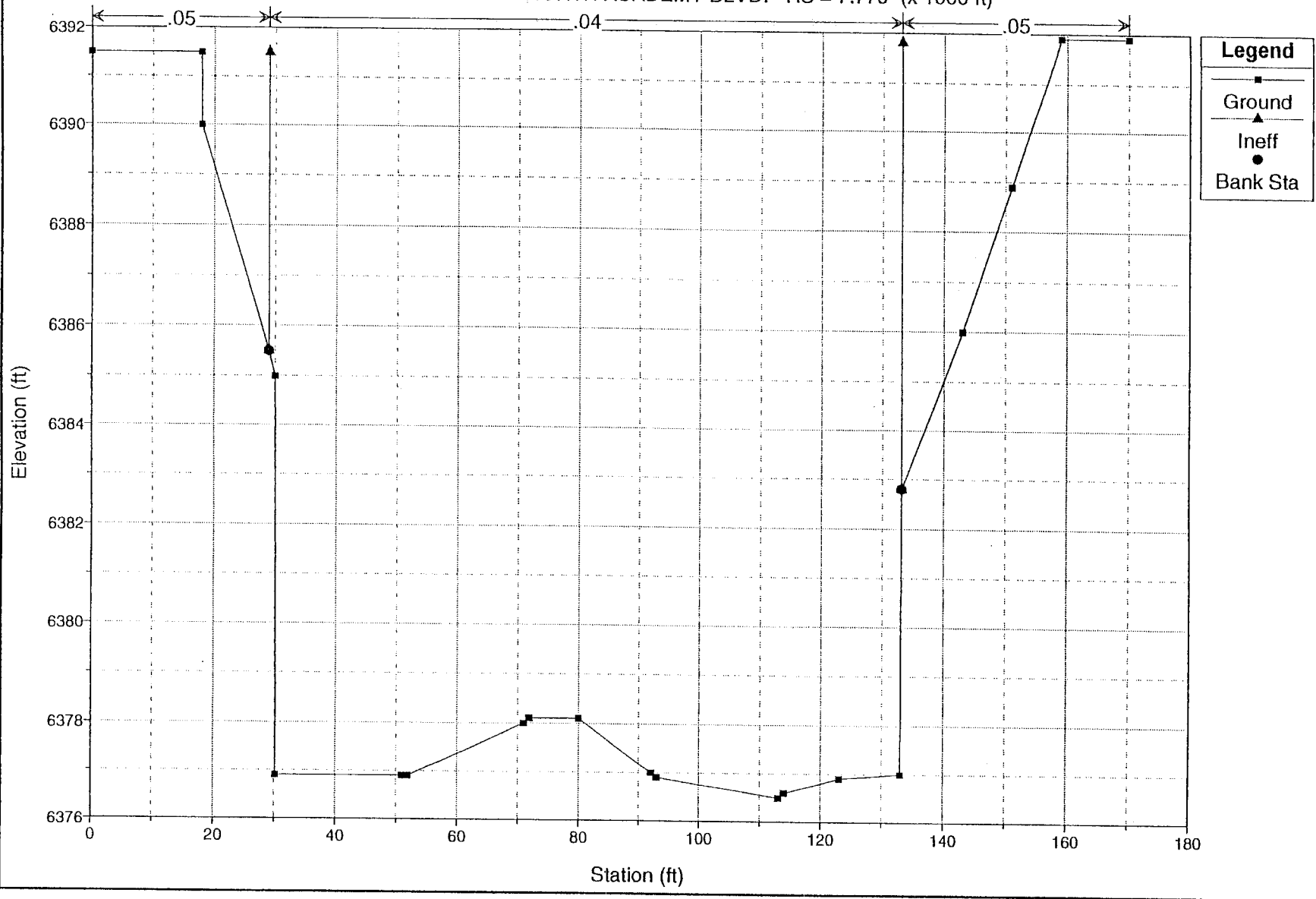
Cottonwood Creek  
CONCRETE GRADE CONTROL STRUCTURE

RS = 7.584 (x 1000 ft)

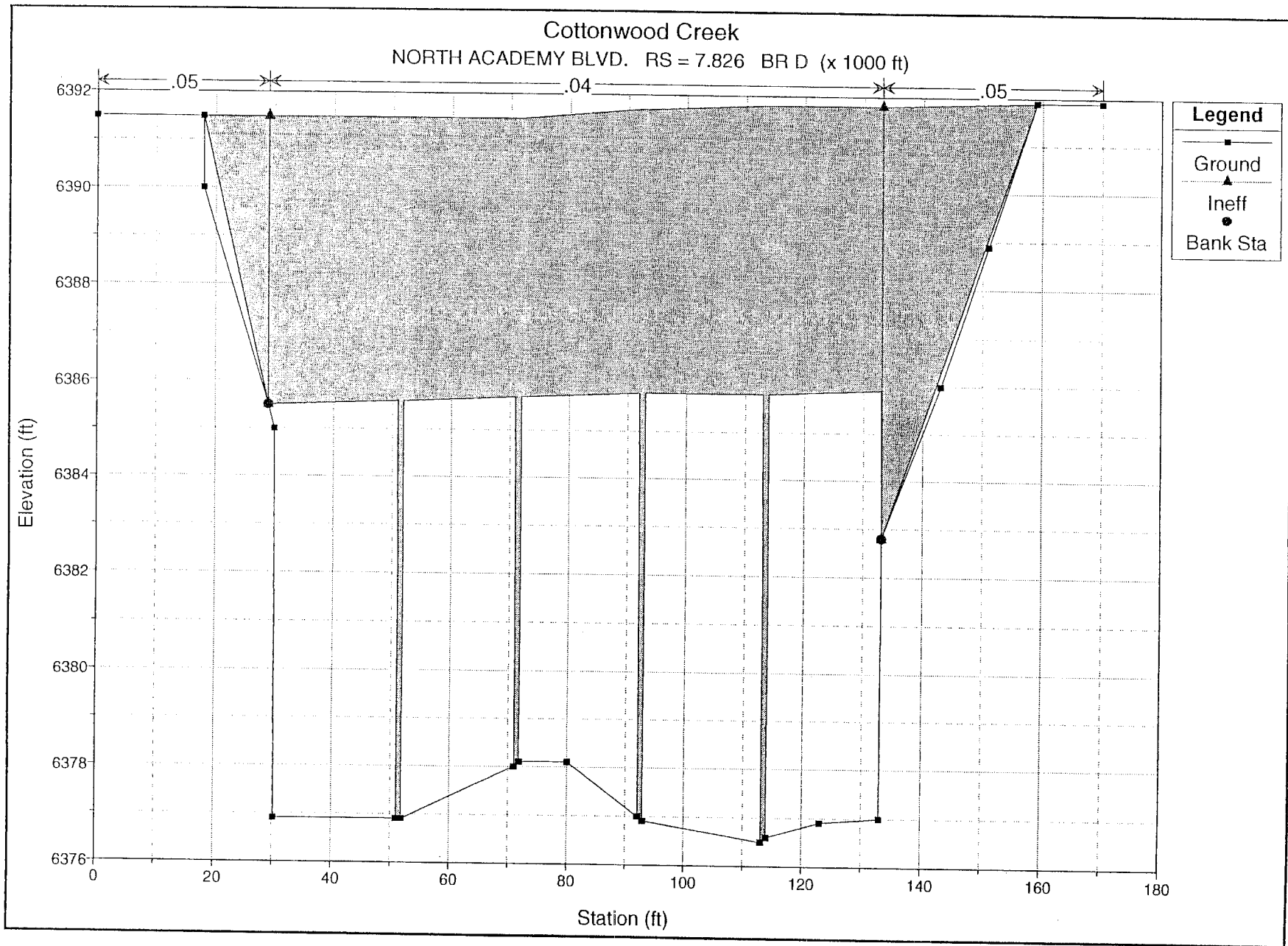


# Cottonwood Creek

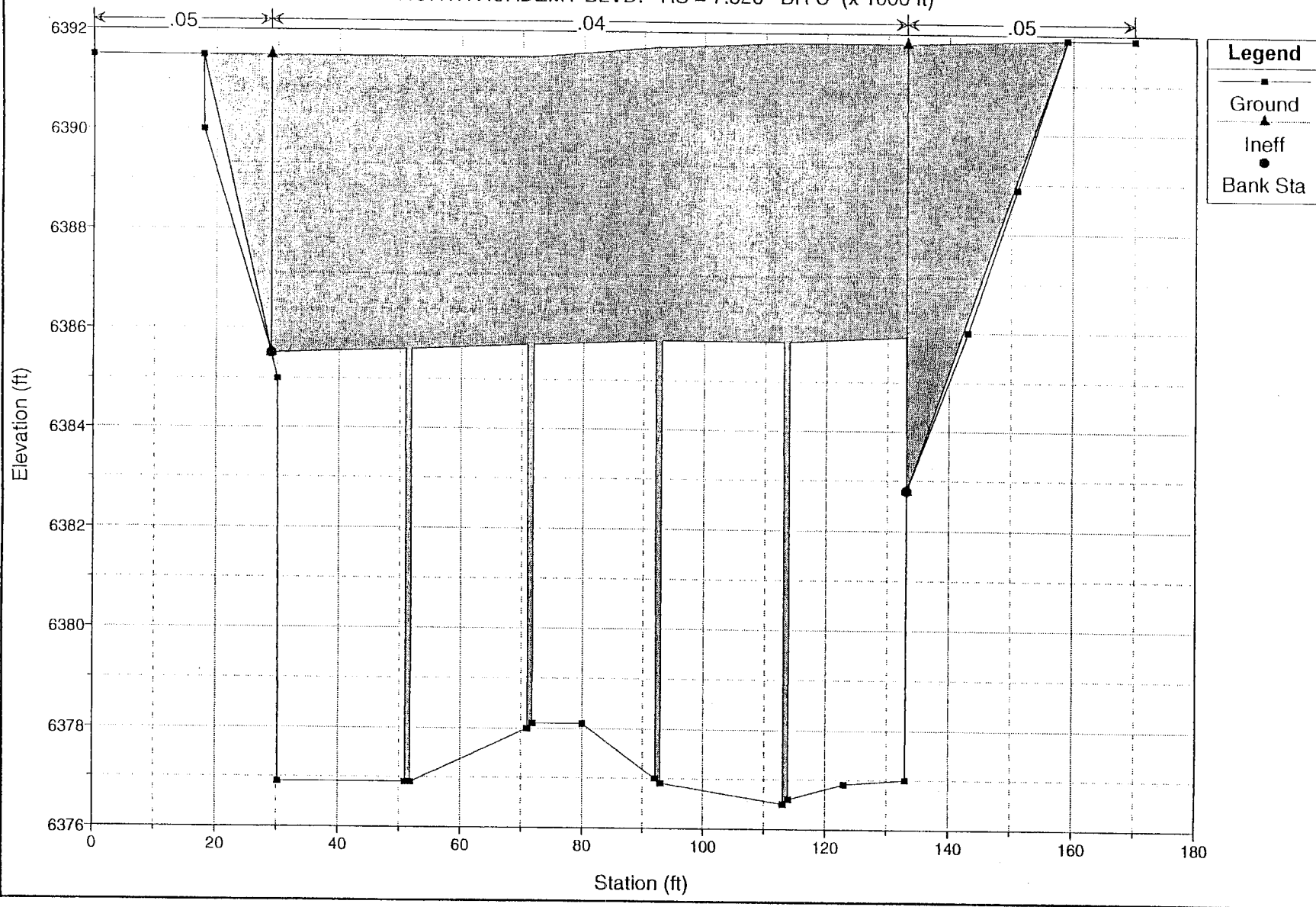
XS @ D/S FACE OF NORTH ACADEMY BLVD. RS = 7.779 (x 1000 ft)





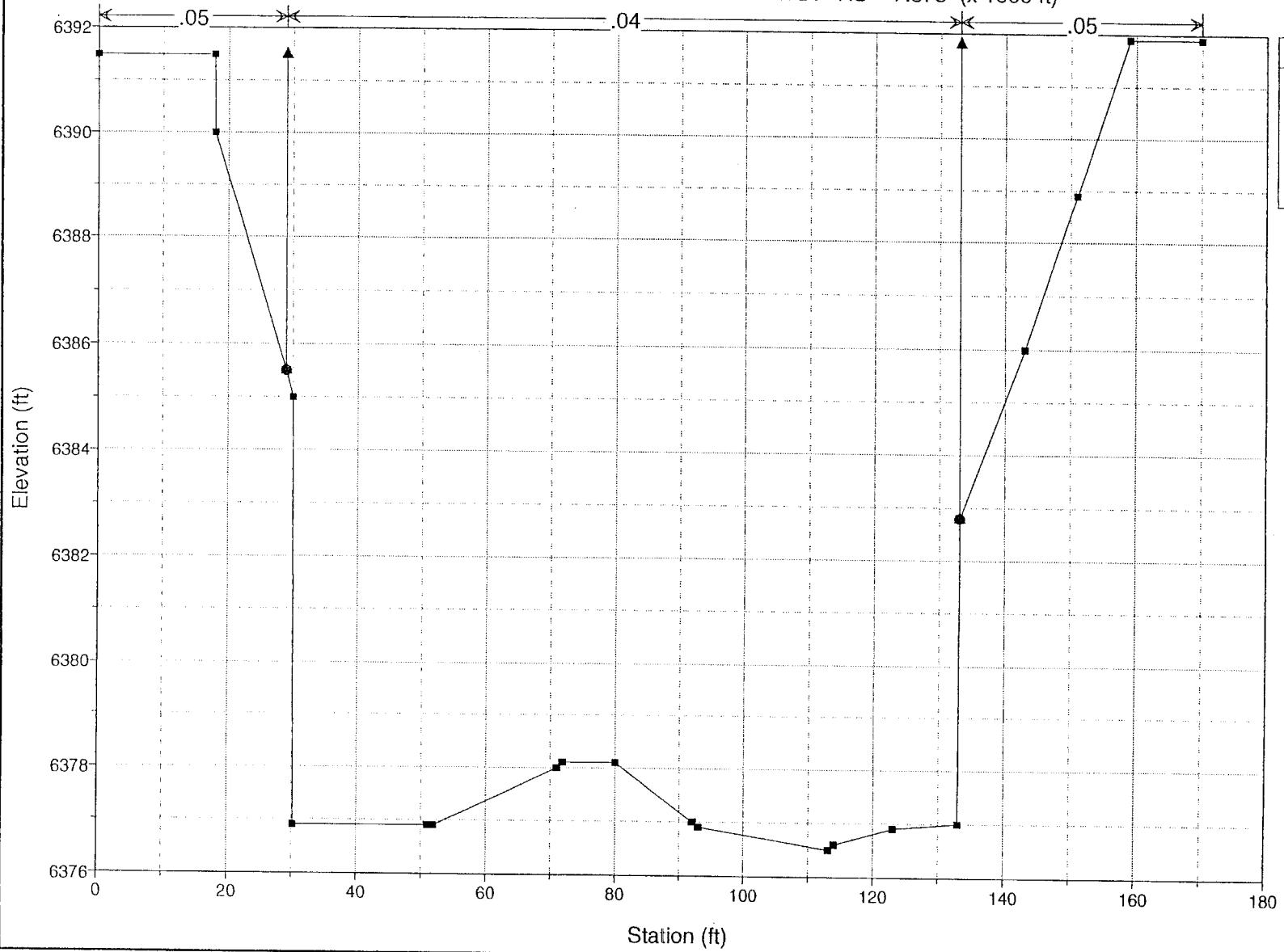


Cottonwood Creek  
NORTH ACADEMY BLVD. RS = 7.826 BR U (x 1000 ft)

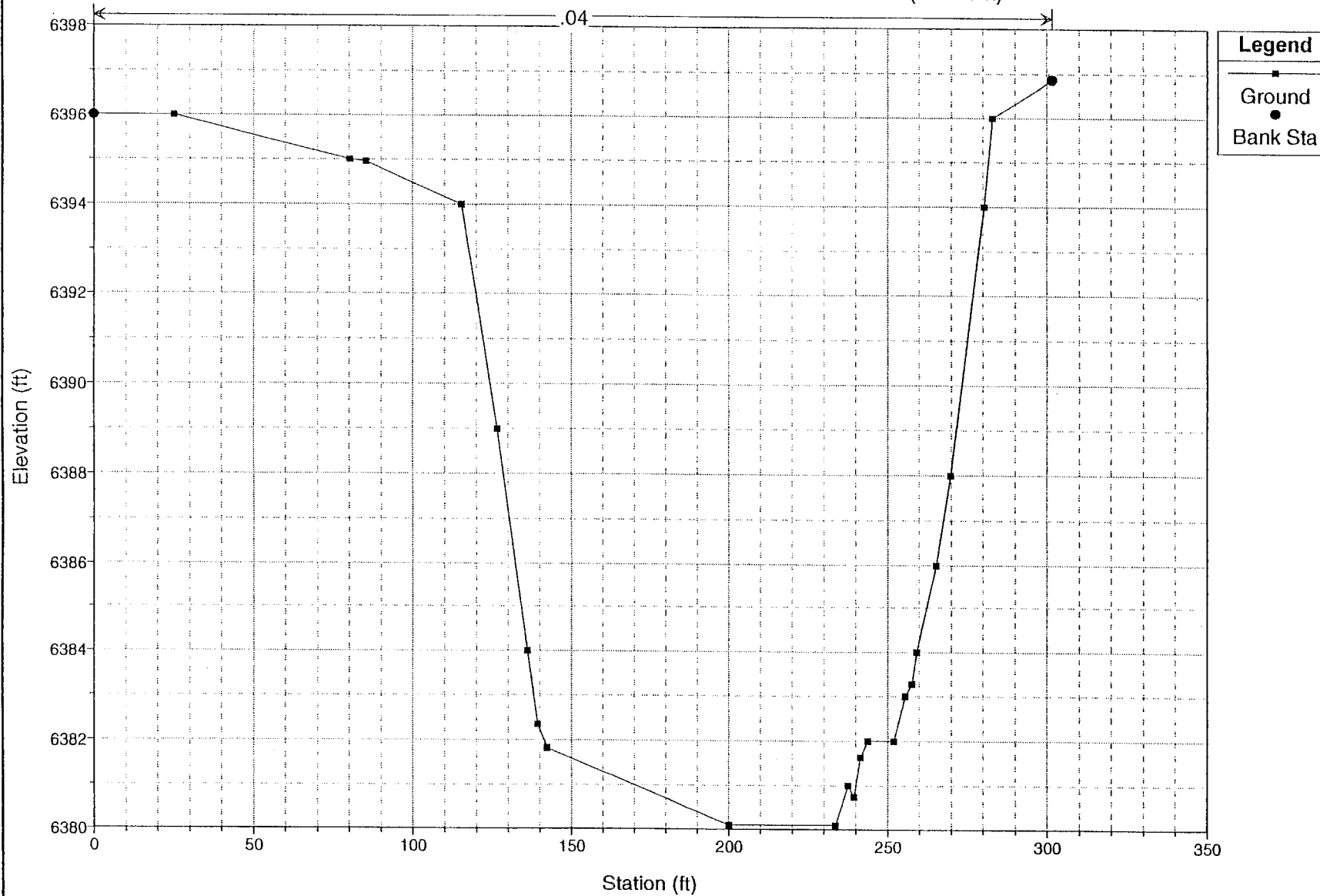


# Cottonwood Creek

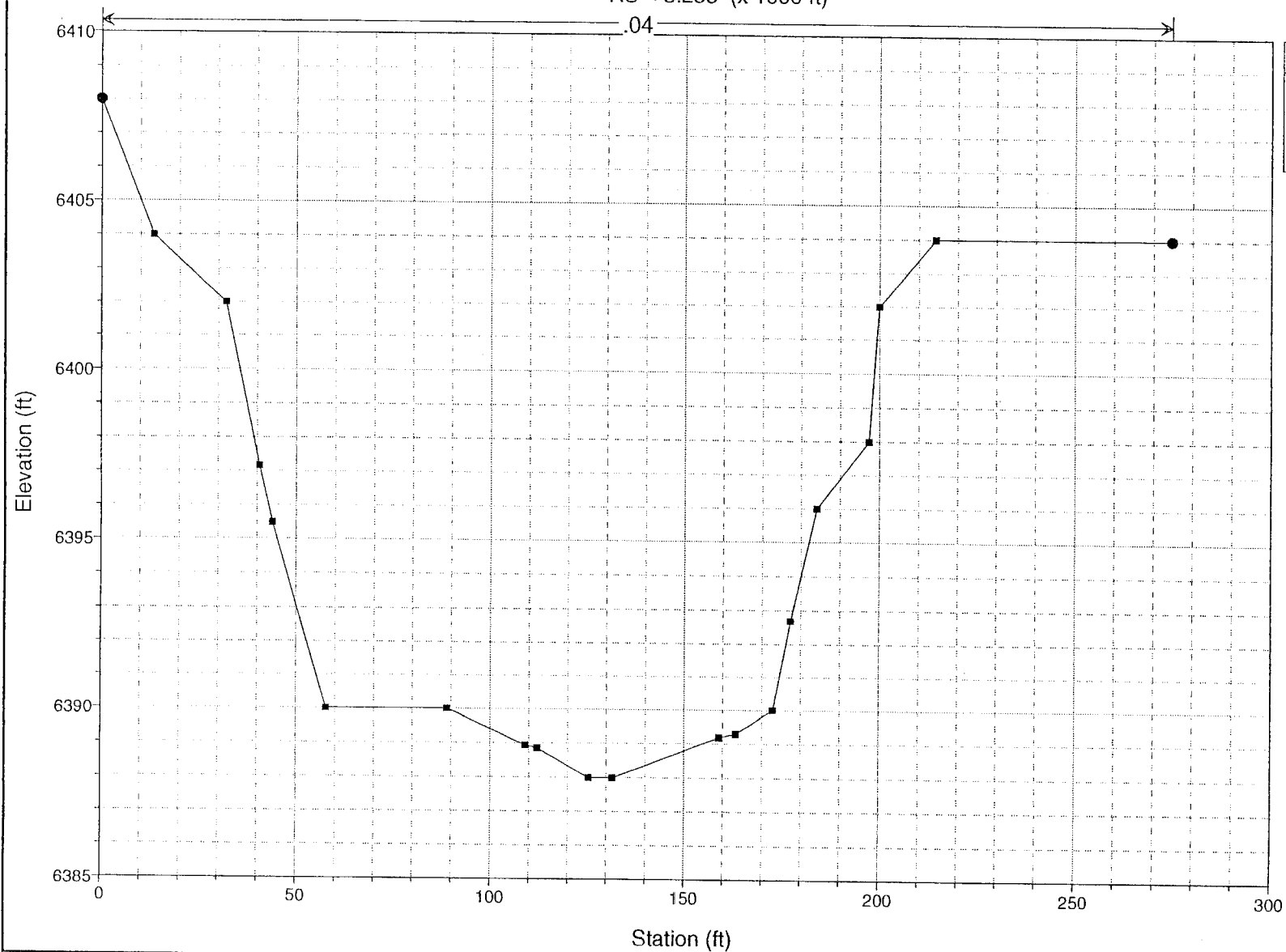
XS @ U/S FACE OF NORTH ACADEMY BLVD. RS = 7.873 (x 1000 ft)



Cottonwood Creek  
CONCRETE GRADE CONTROL STRUCTURE RS = 7.948 (x 1000 ft)



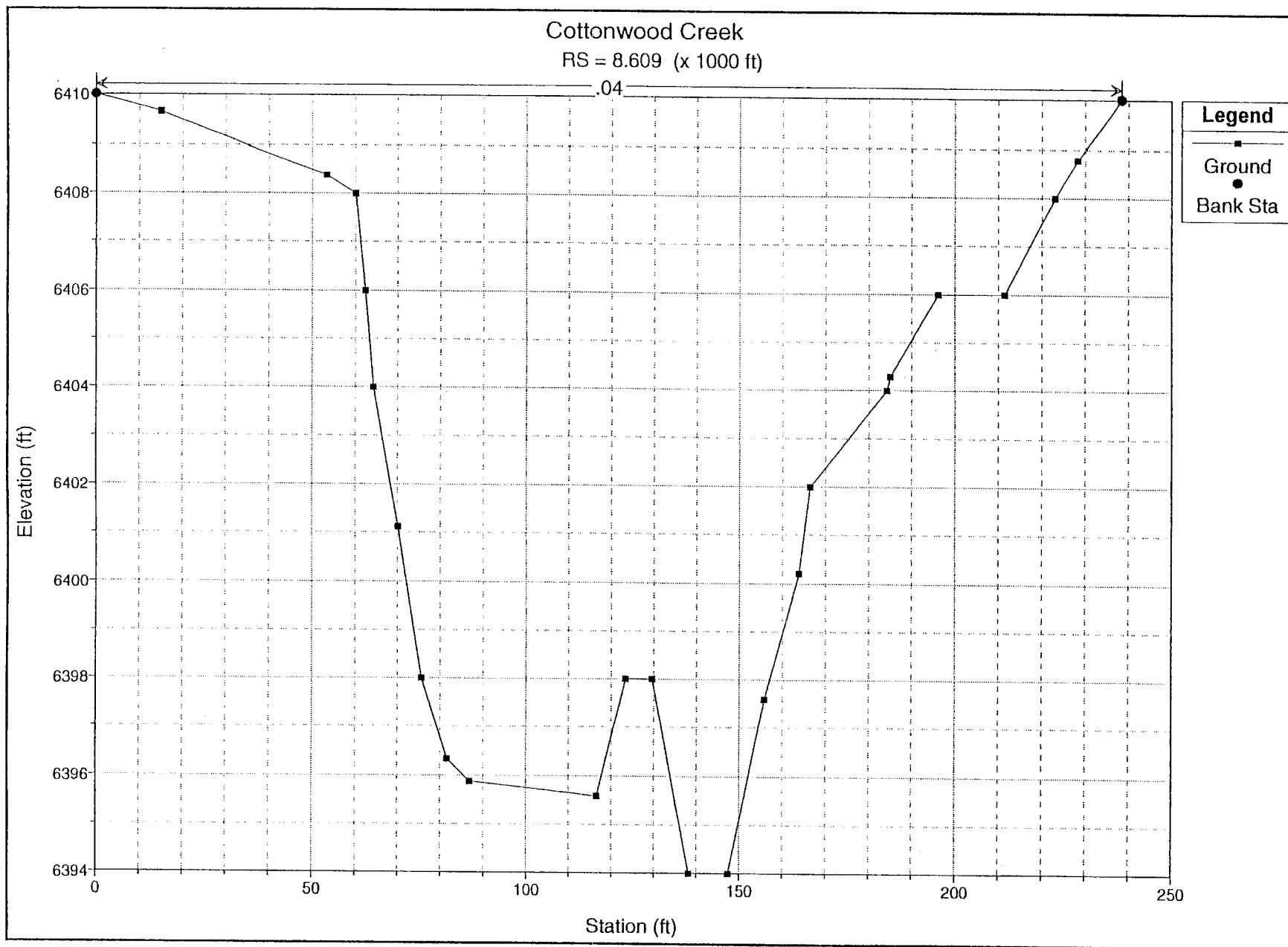
Cottonwood Creek  
RS = 8.253 (x 1000 ft)



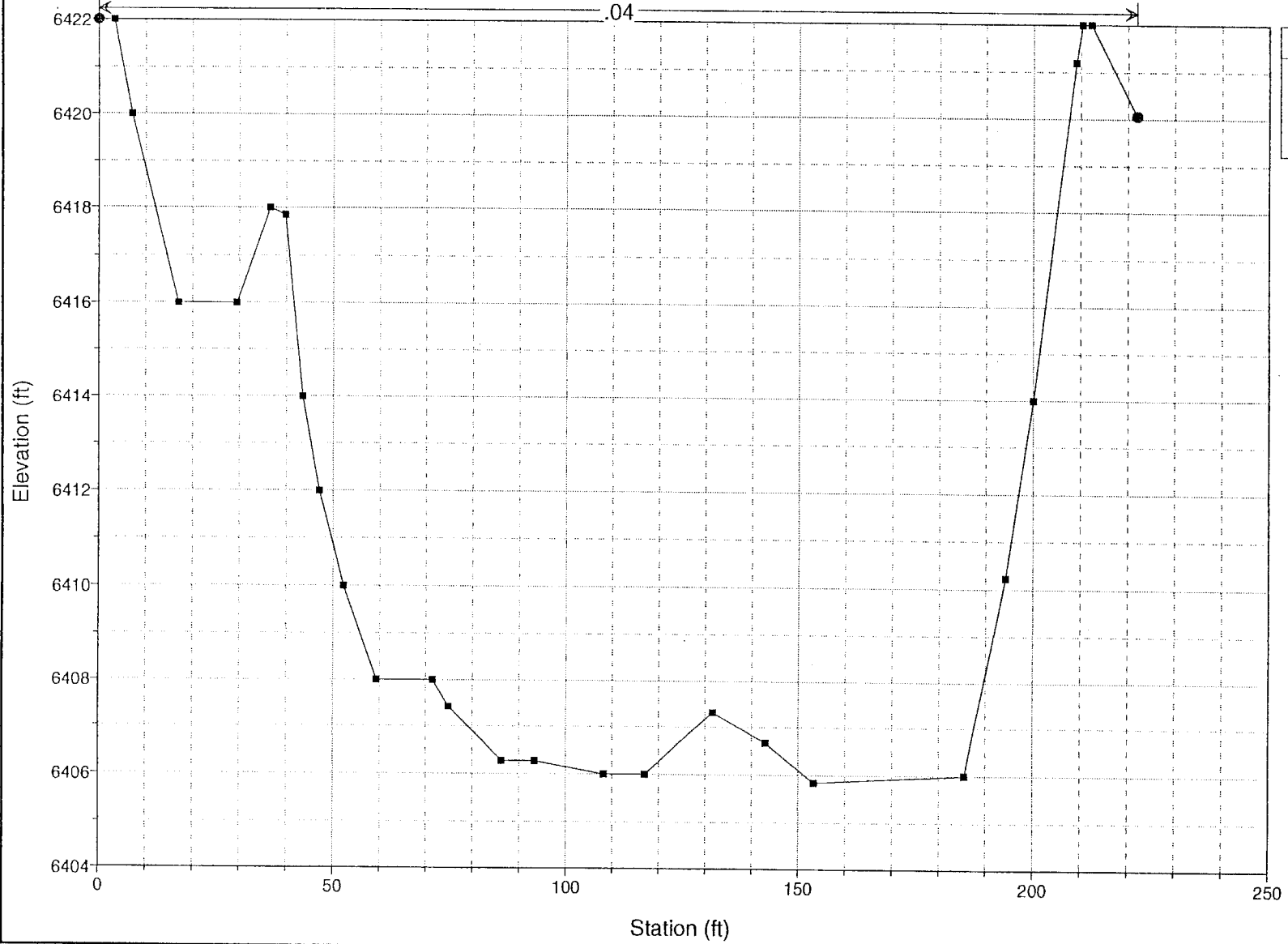
**Legend**

Ground

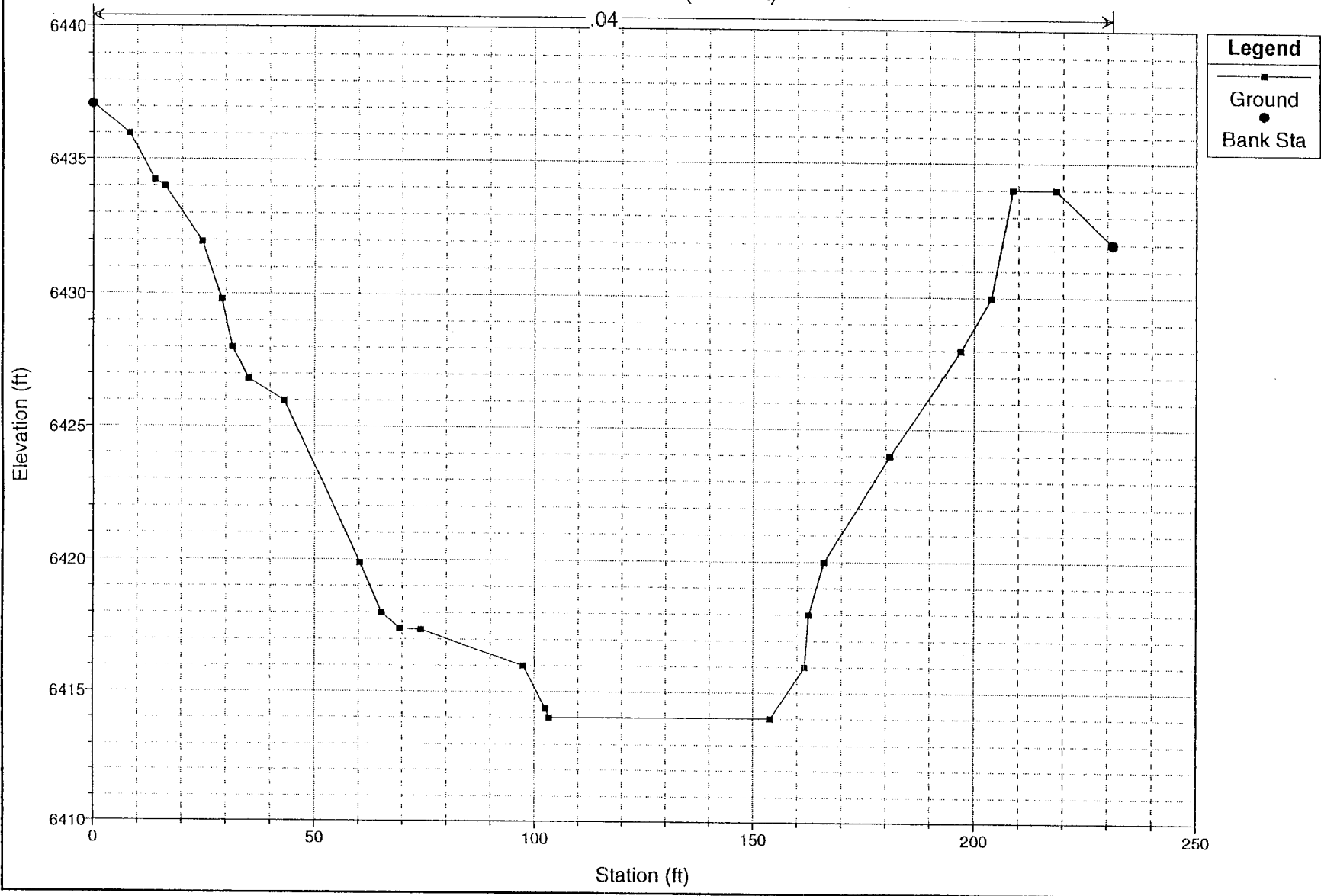
Bank Sta



Cottonwood Creek  
RS = 9.201 (x 1000 ft)



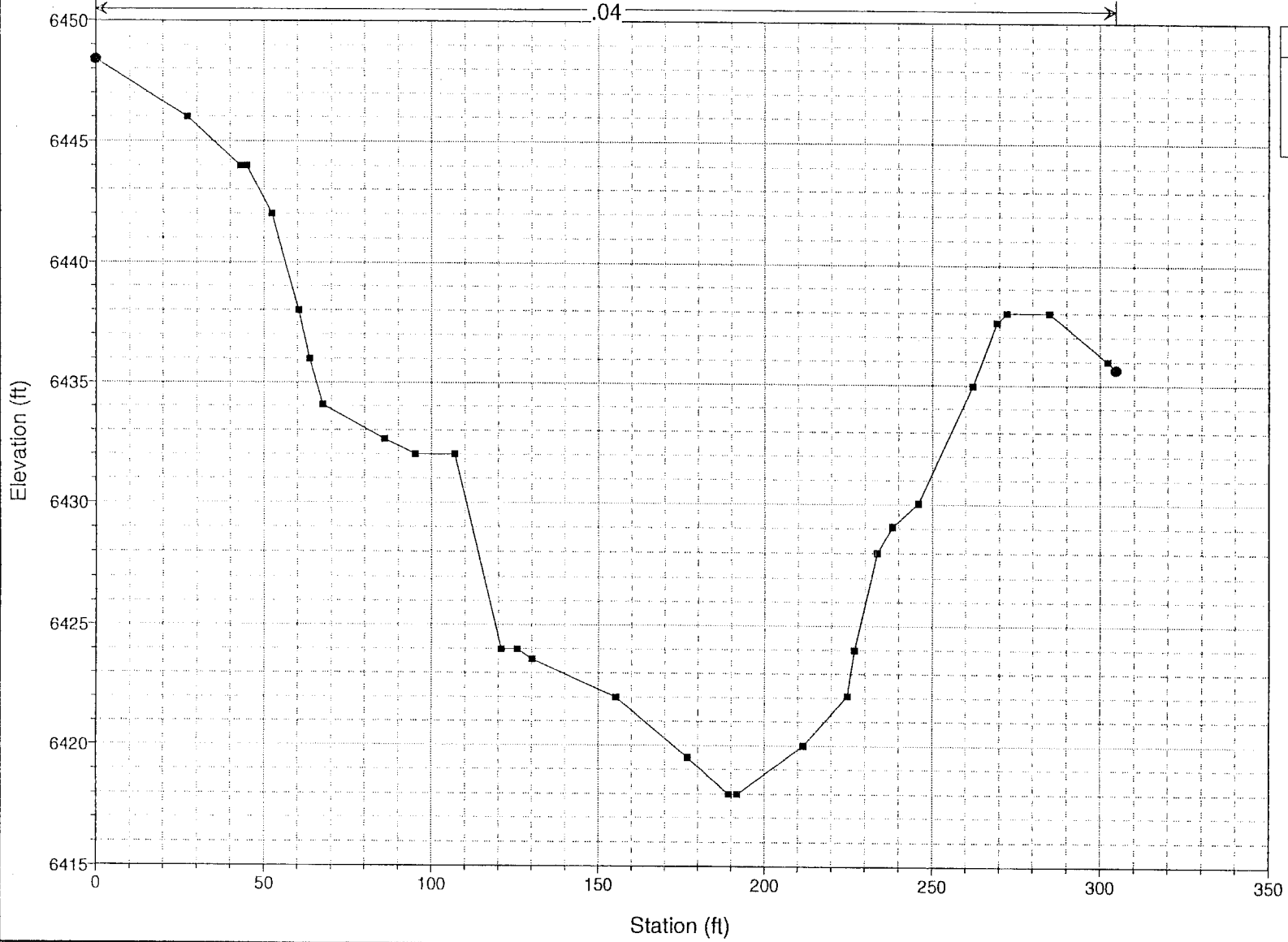
Cottonwood Creek  
RS = 9.714 (x 1000 ft)





Cottonwood Creek  
RS = 10.03 (x 1000 ft)

.04

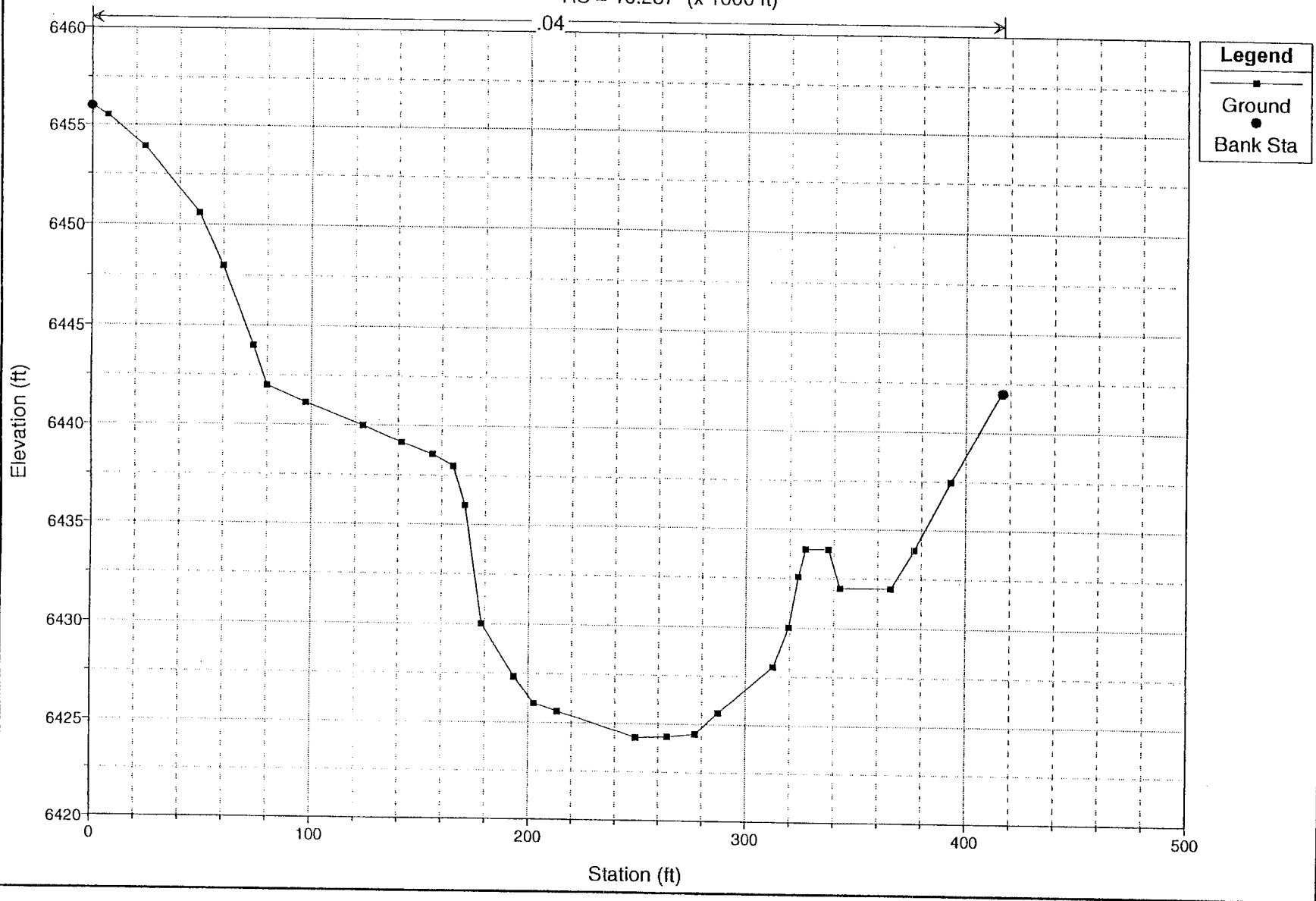


**Legend**

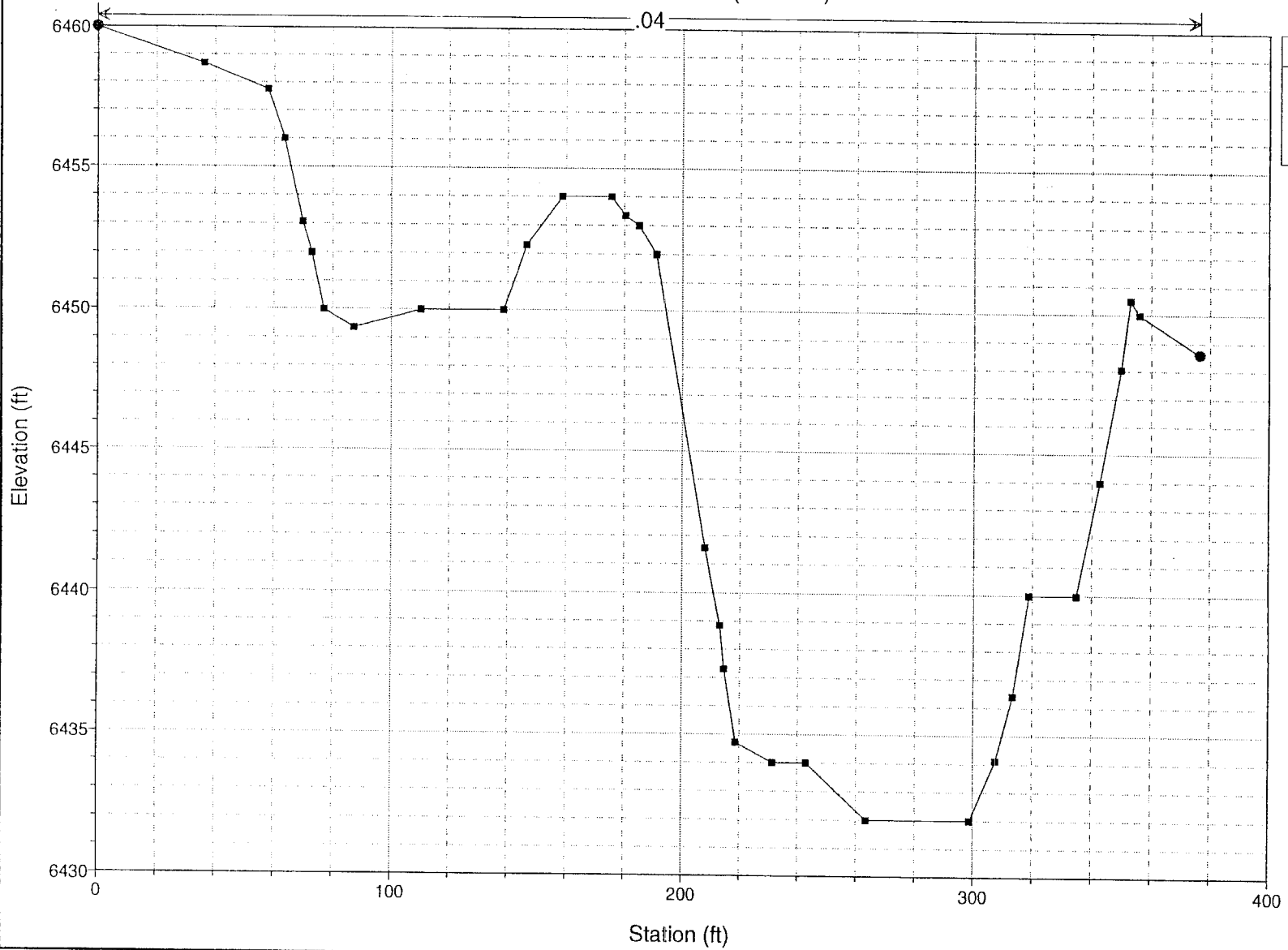
Ground

Bank Sta

Cottonwood Creek  
RS = 10.287 (x 1000 ft)



Cottonwood Creek  
RS = 10.803 (x 1000 ft)



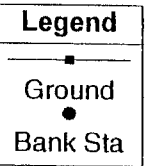
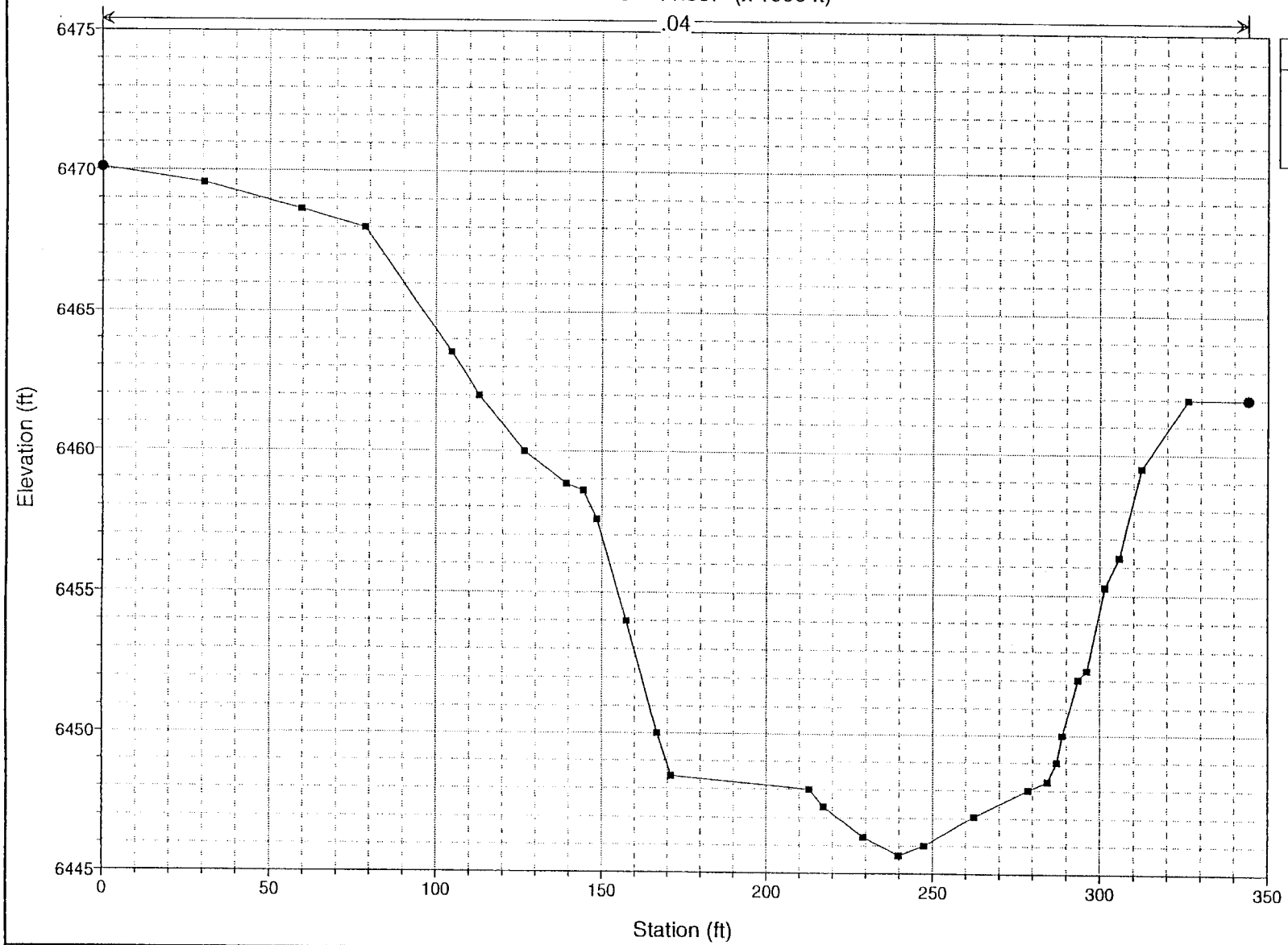
**Legend**

Ground

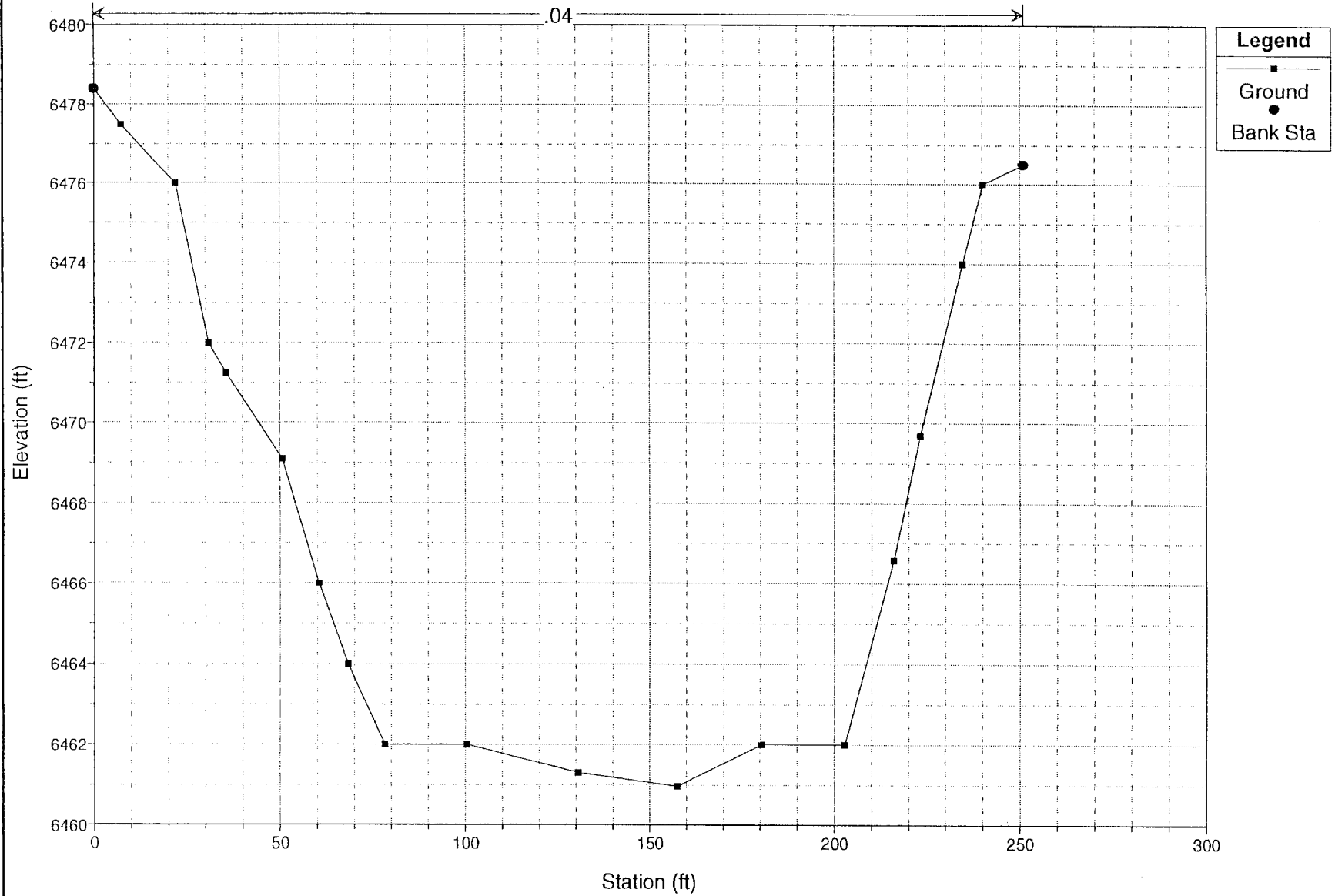
Bank Sta

# Cottonwood Creek

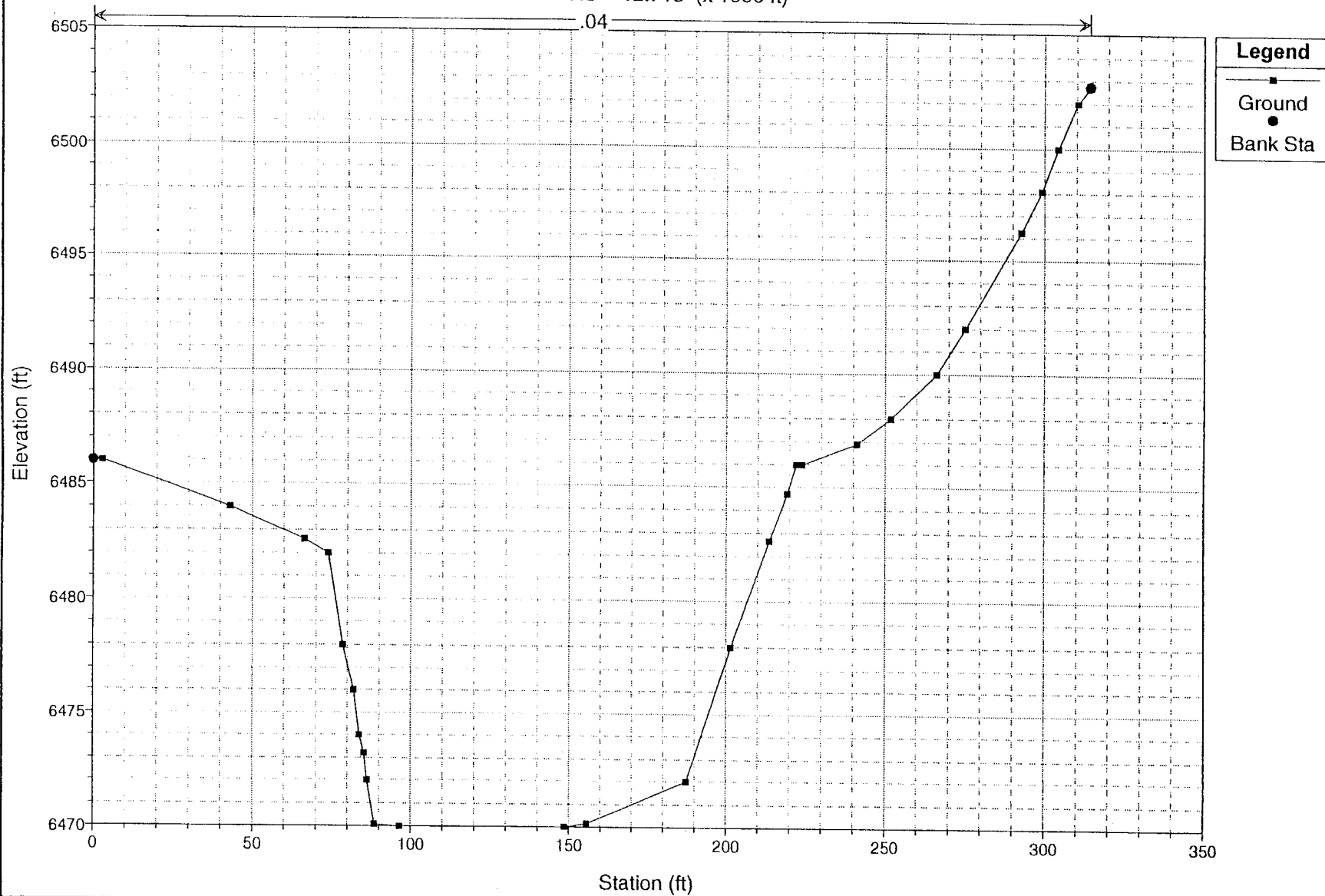
RS = 11.357 (x 1000 ft)



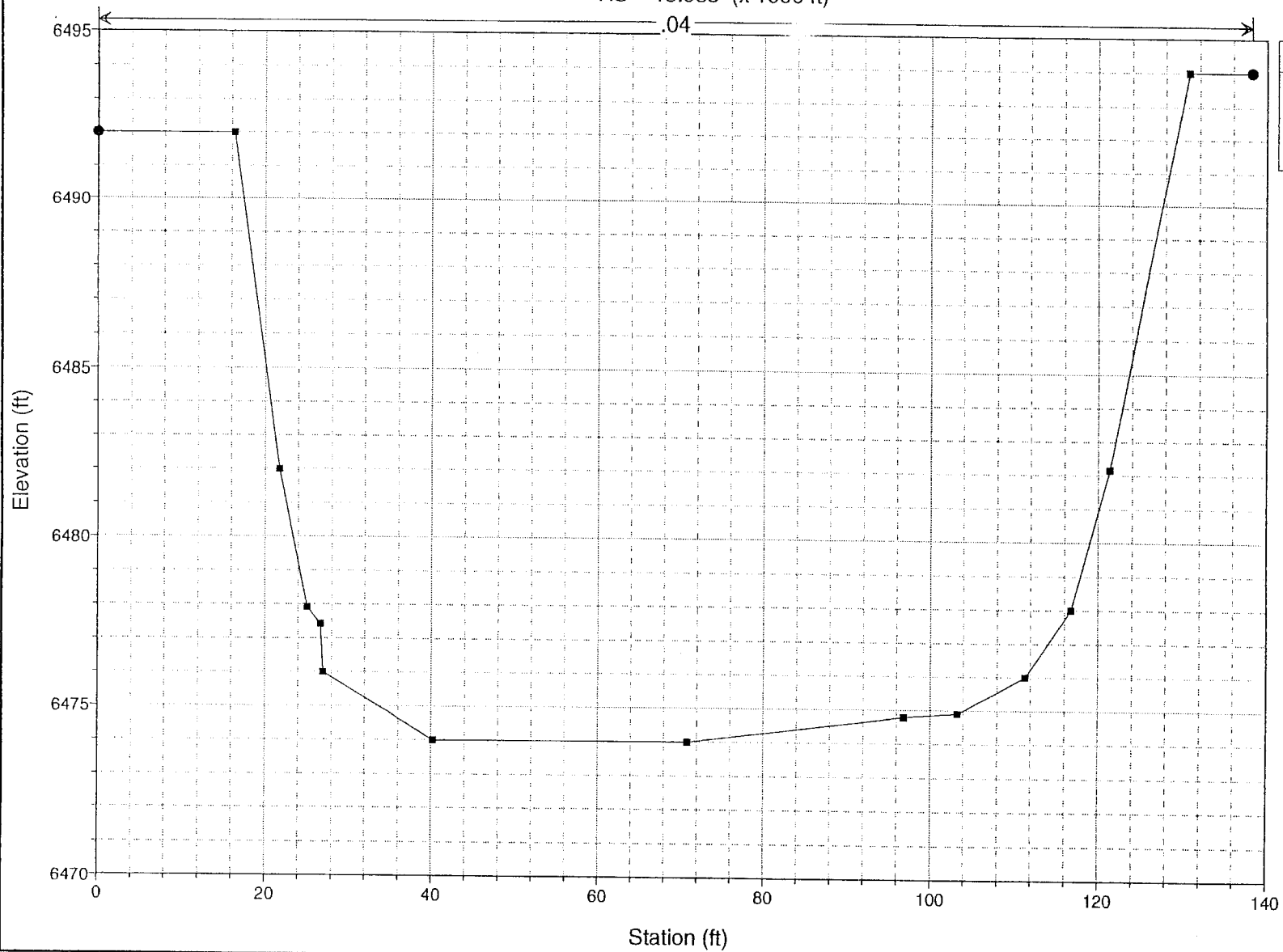
Cottonwood Creek  
RS = 12.03 (x 1000 ft)



Cottonwood Creek  
RS = 12.715 (x 1000 ft)

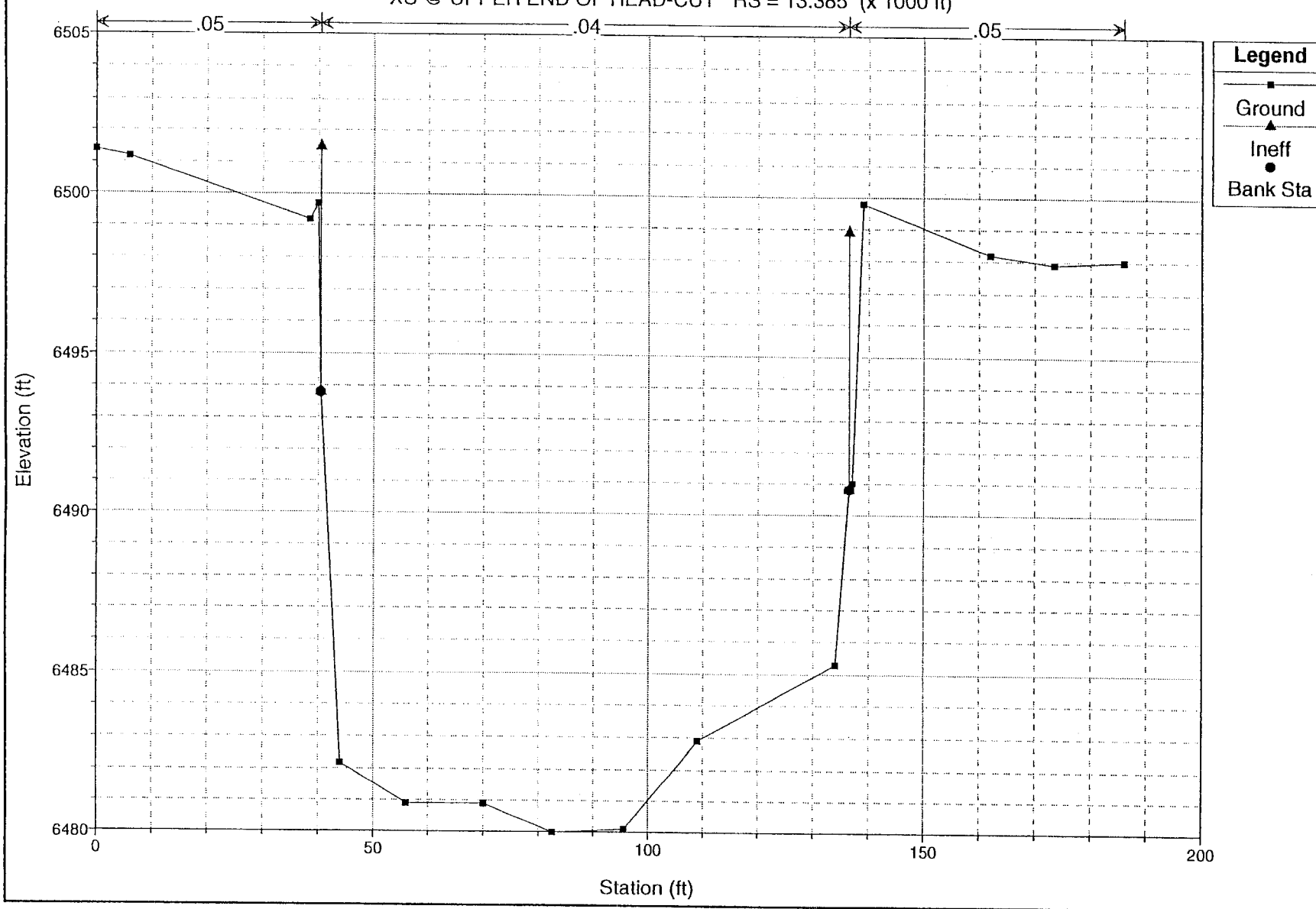


Cottonwood Creek  
RS = 13.085 (x 1000 ft)



- Legend
- Ground
  - Bank Sta

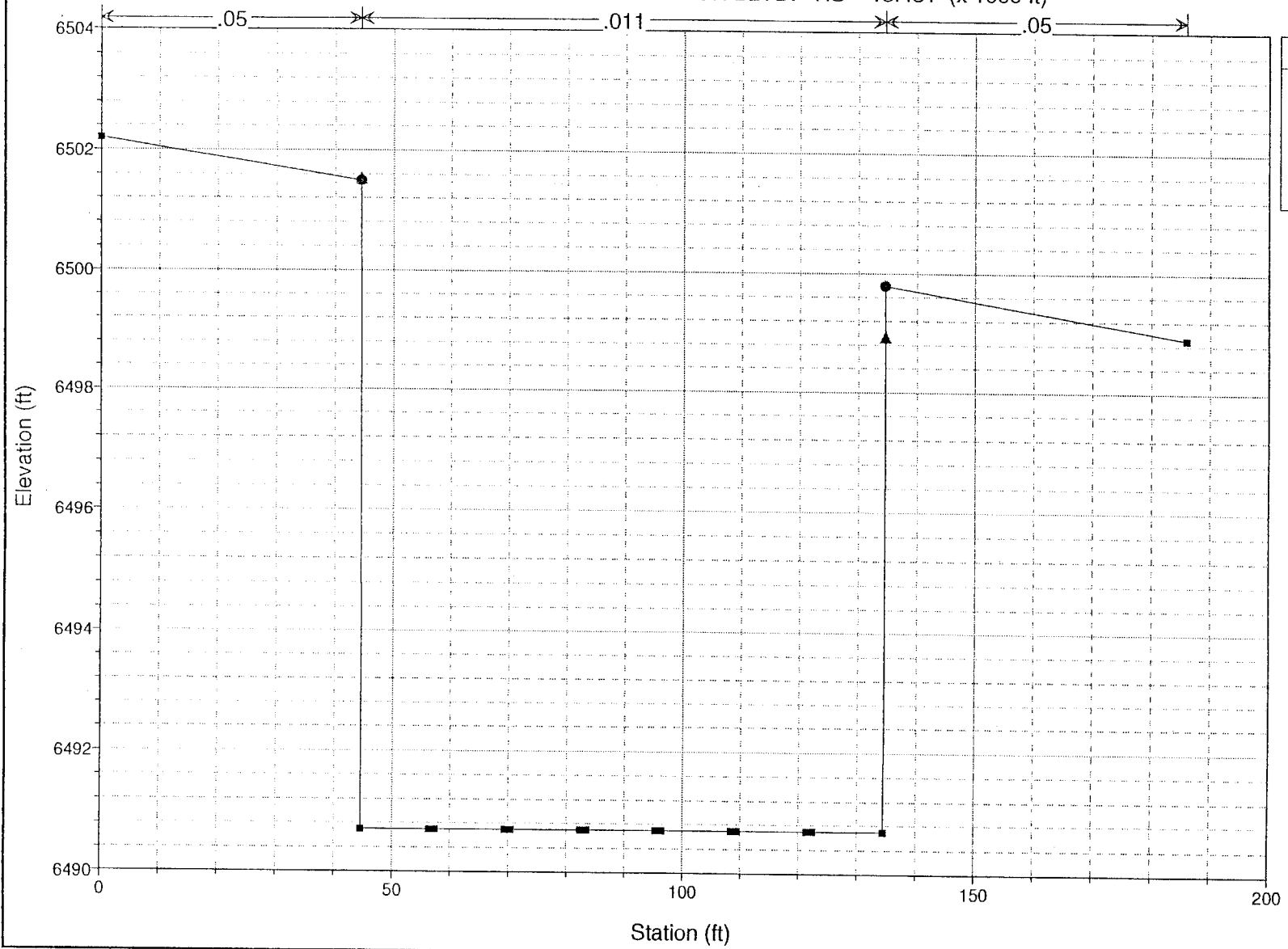
XS @ UPPER END OF HEAD-CUT RS = 13.385 (x 1000 ft)





# Cottonwood Creek

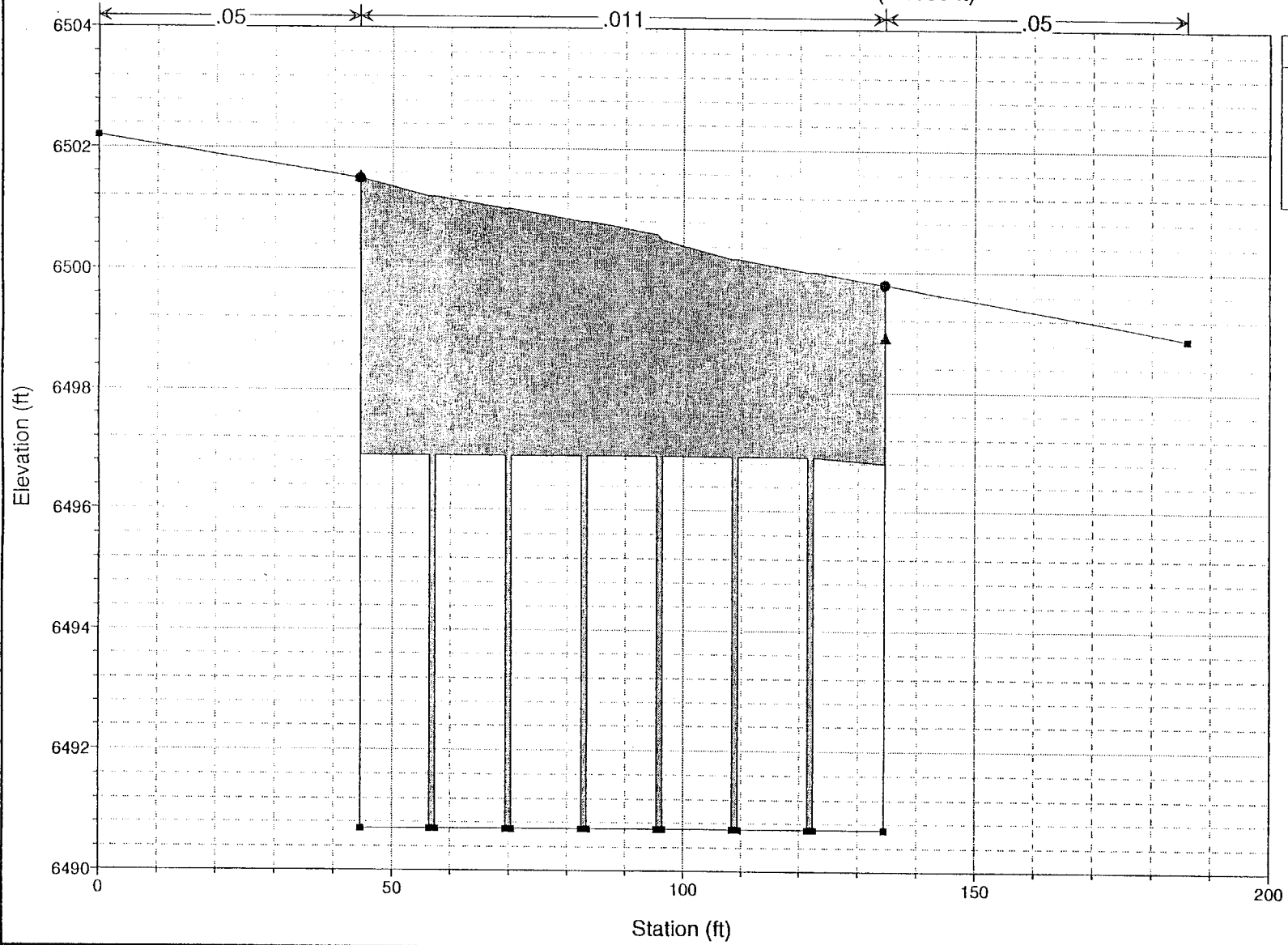
XS @ D/S FACE OF NORTH UNION BLVD. RS = 13.431 (x 1000 ft)

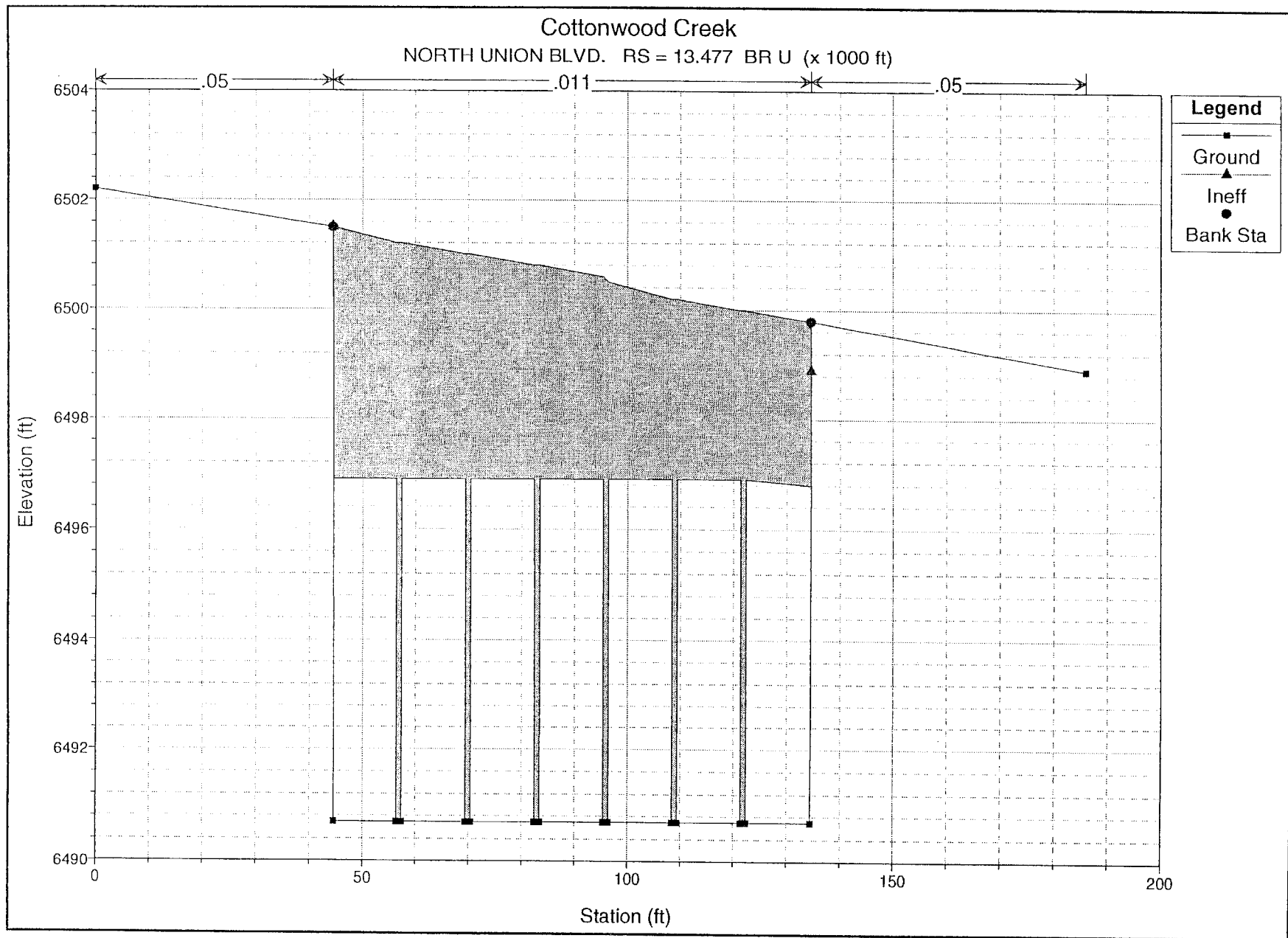


## Legend

- Ground
- Ineff
- Bank Sta

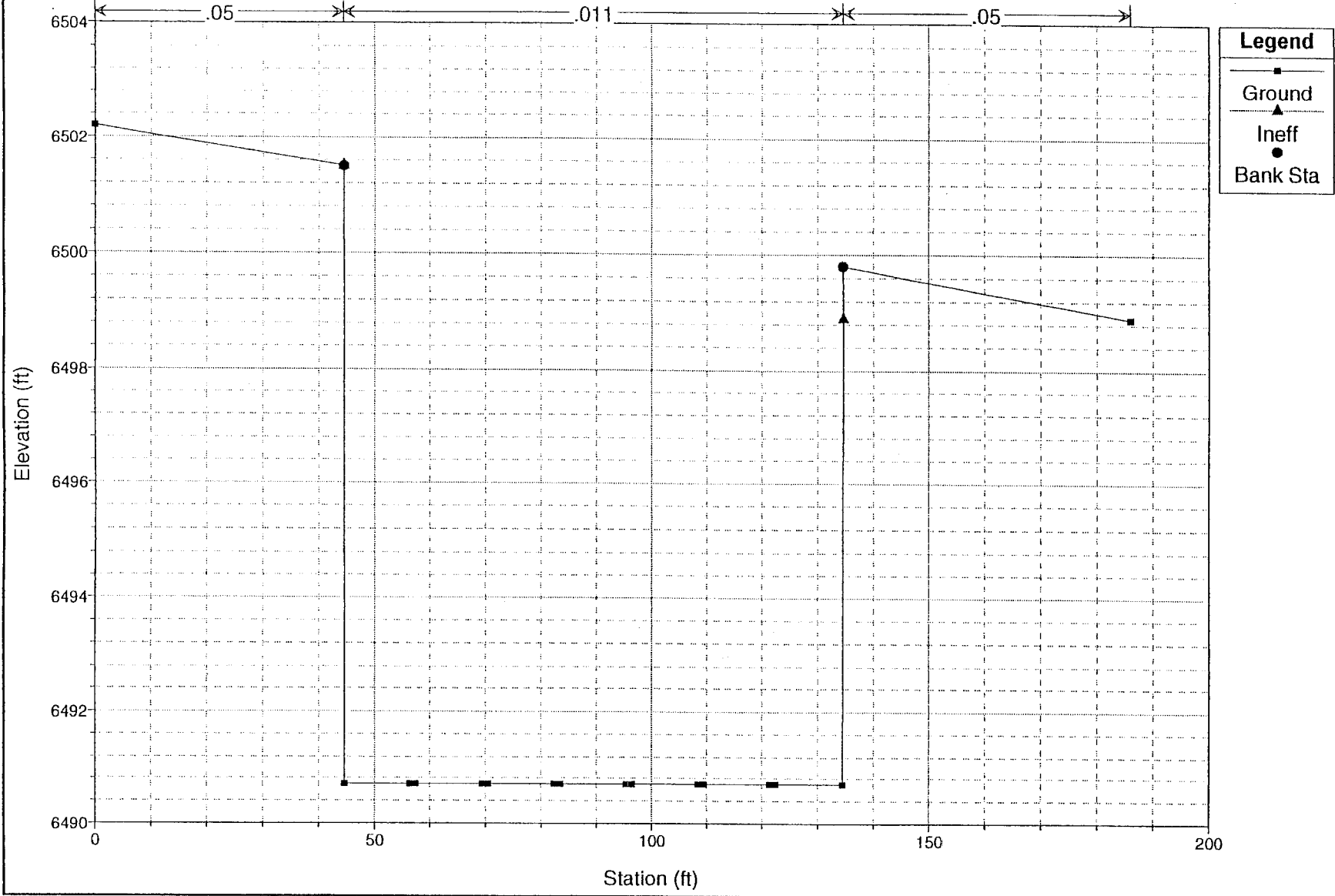
Cottonwood Creek  
NORTH UNION BLVD. RS = 13.477 BR D (x 1000 ft)

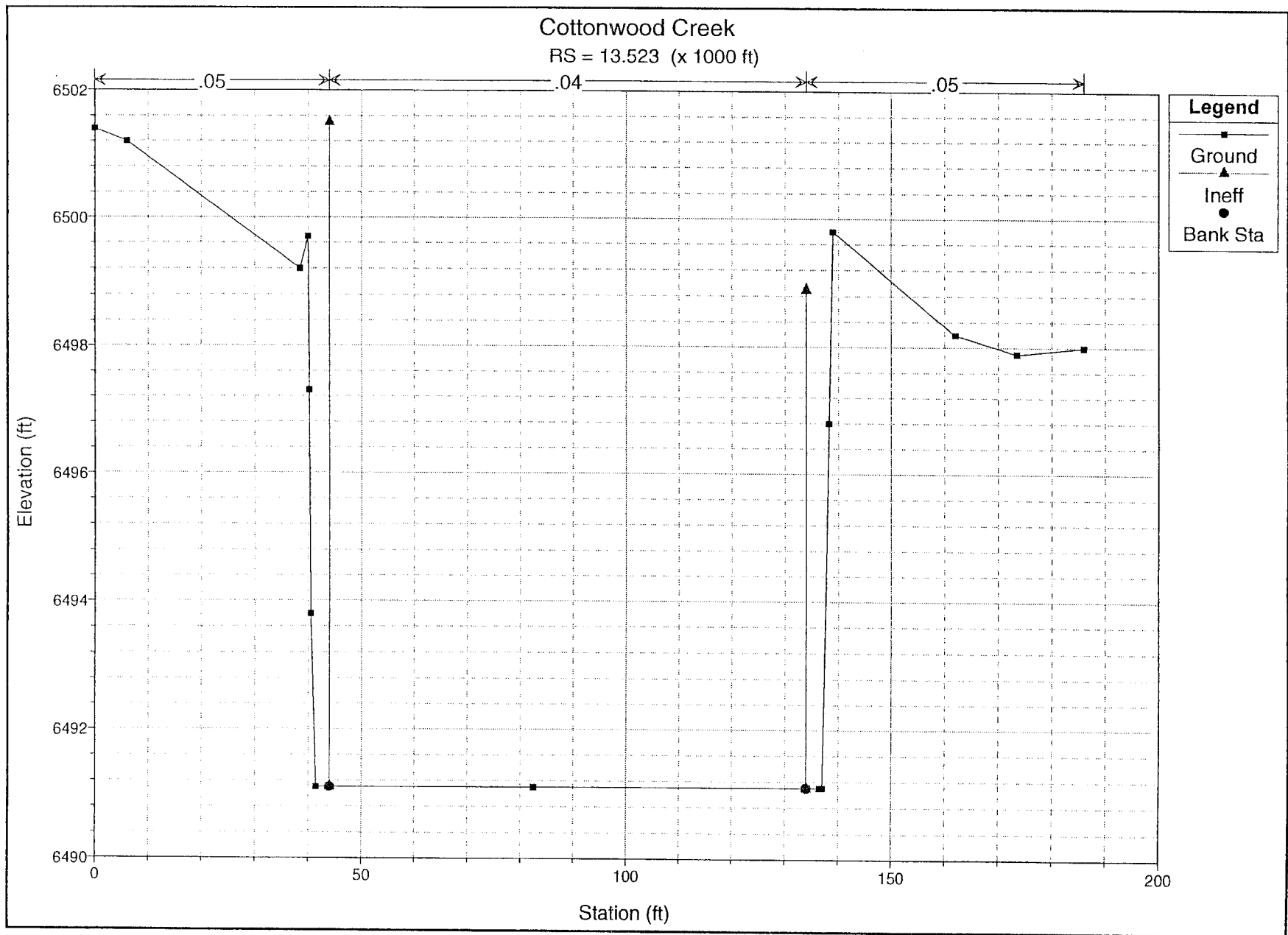




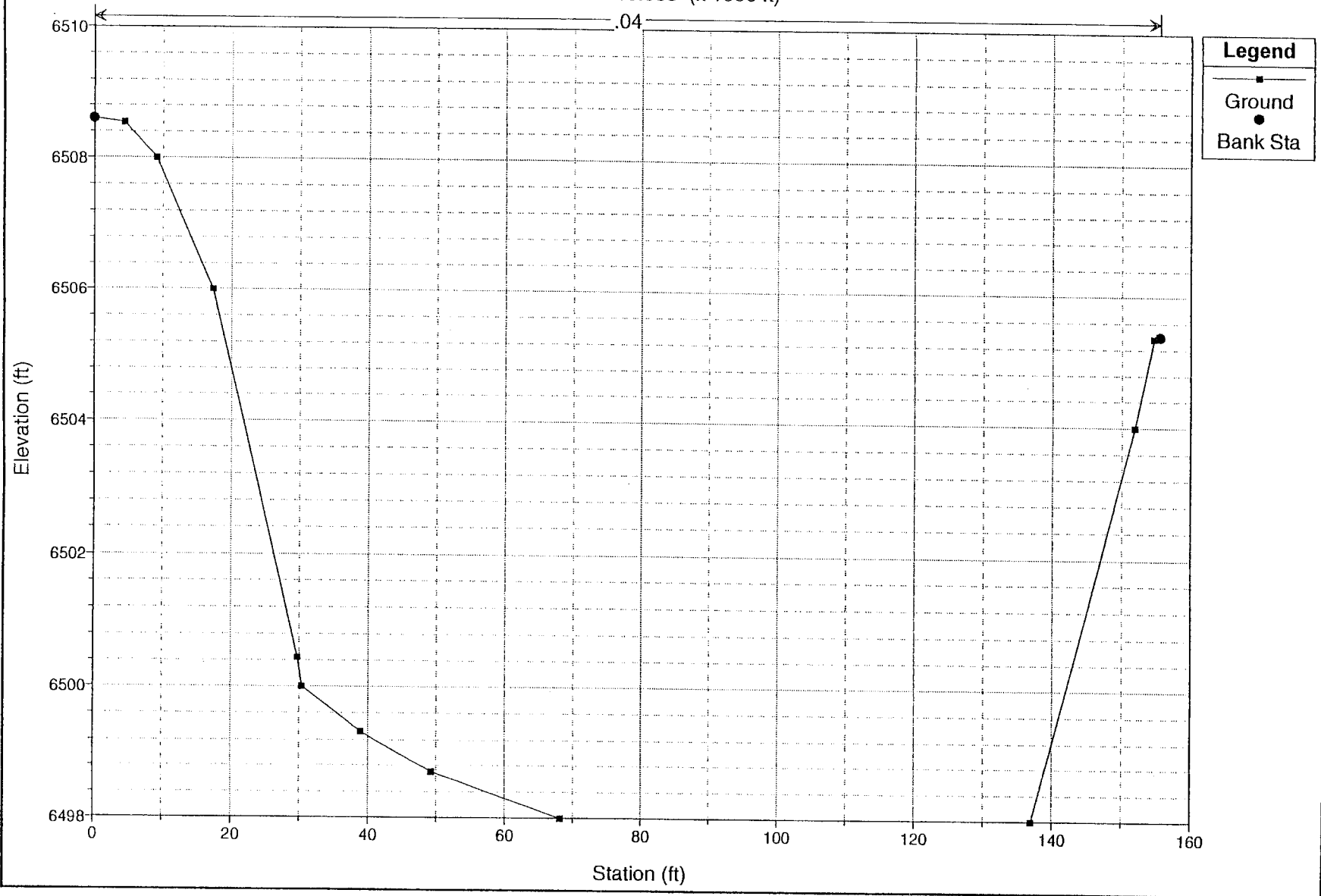
# Cottonwood Creek

XS @ U/S FACE OF NORTH UNION BLVD. RS = 13.522 (x 1000 ft)

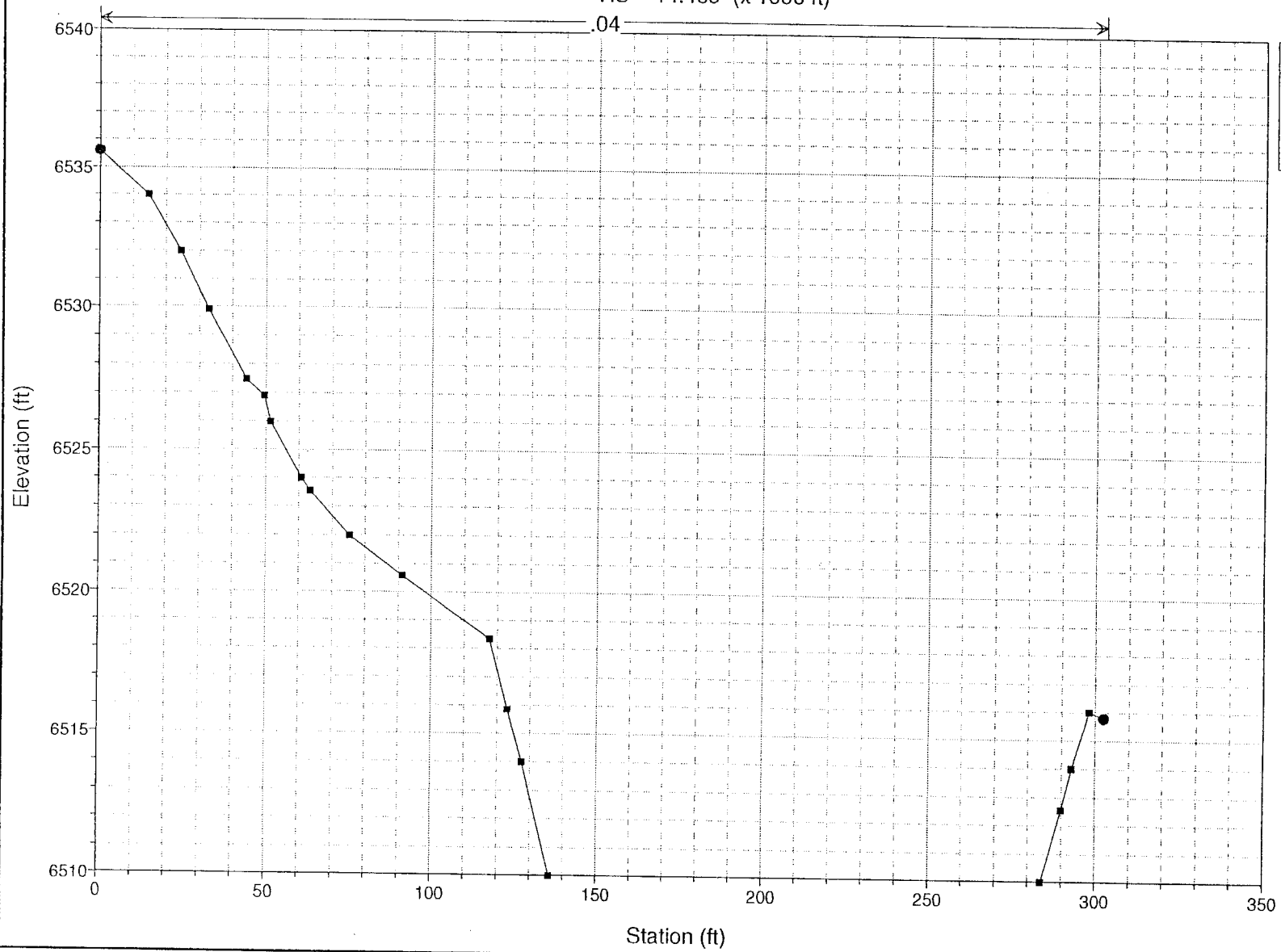




Cottonwood Creek  
RS = 13.633 (x 1000 ft)



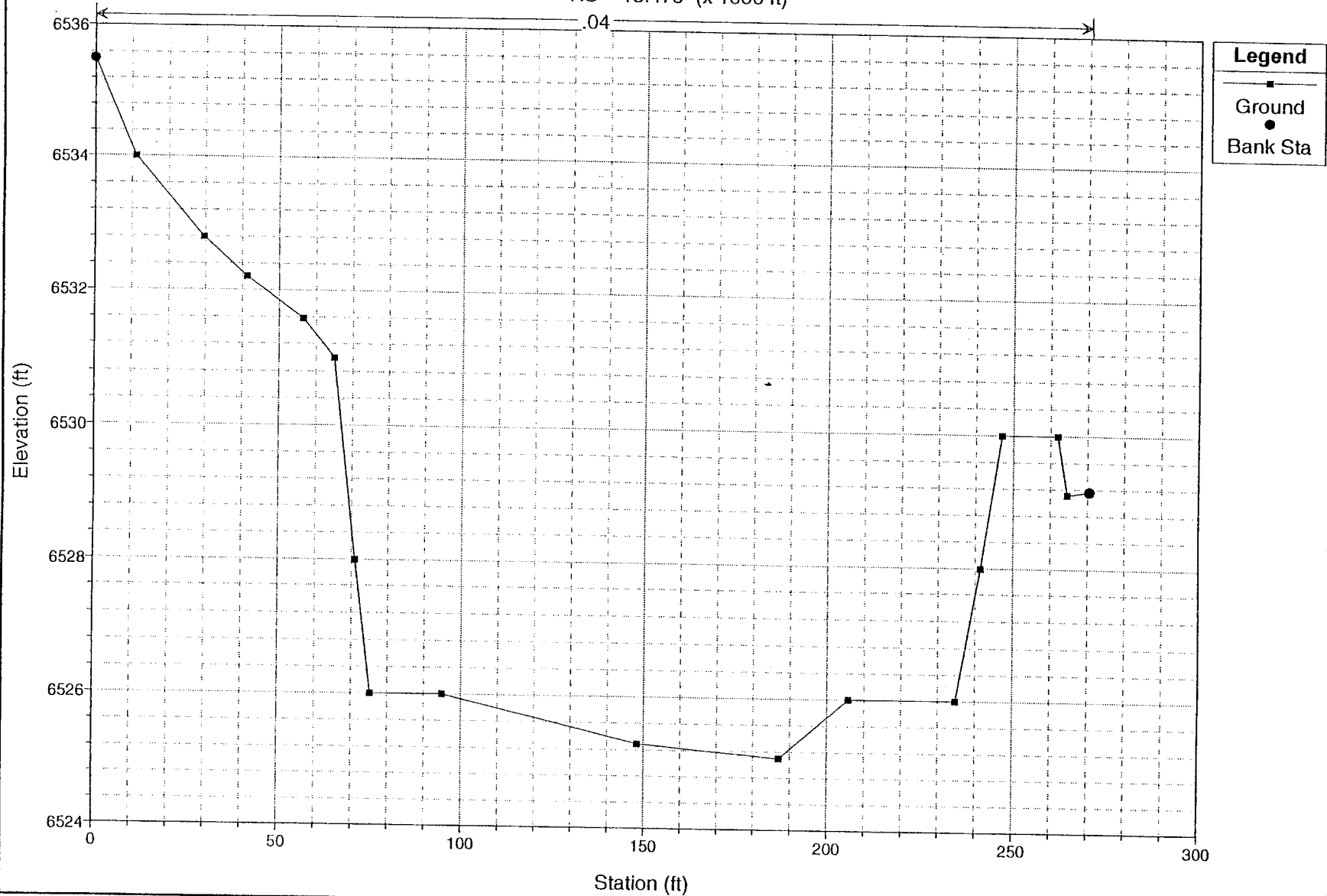
Cottonwood Creek  
RS = 14.469 (x 1000 ft)



**Legend**

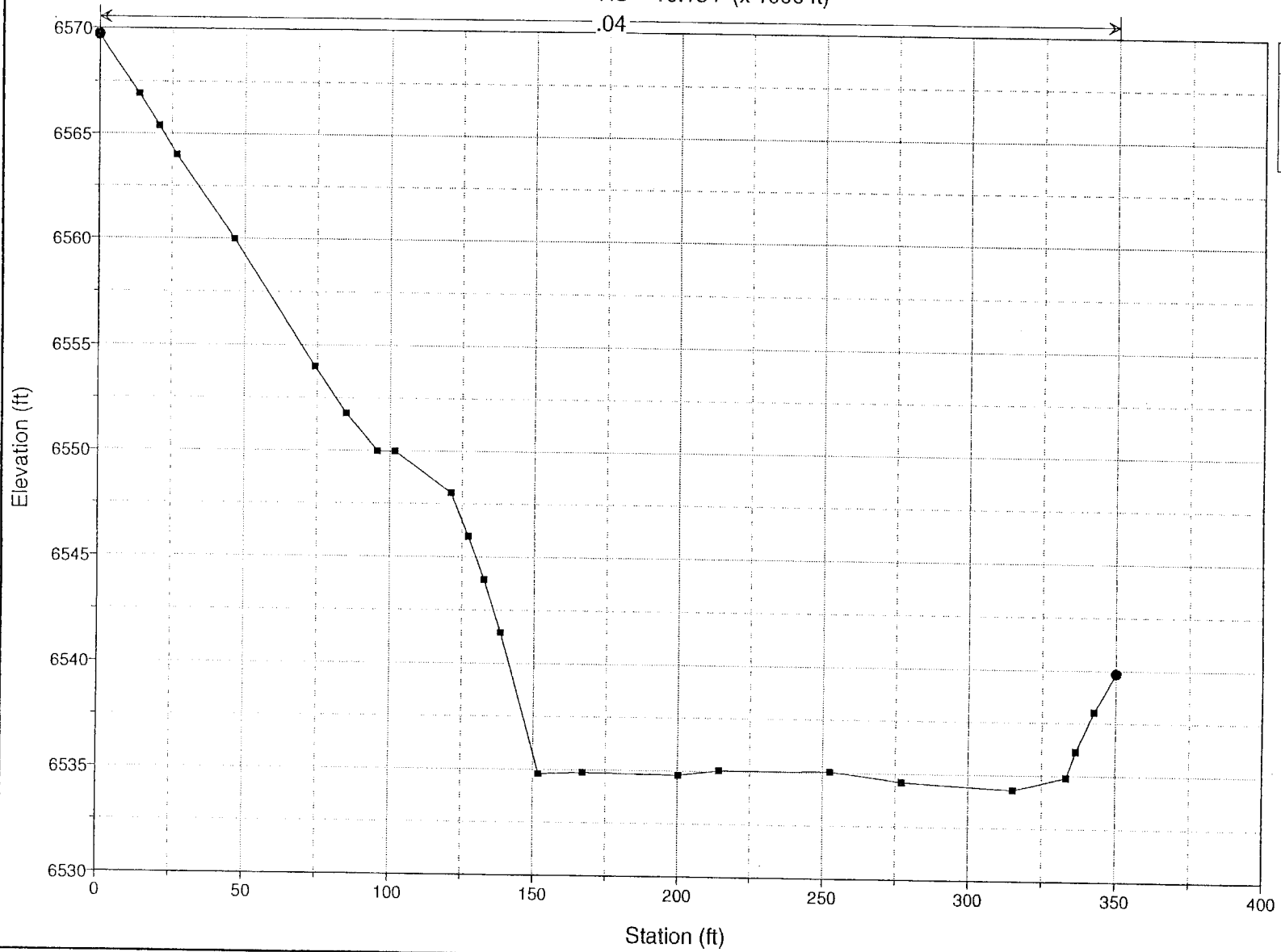
- Ground
- Bank Sta

Cottonwood Creek  
RS = 15.479 (x 1000 ft)





Cottonwood Creek  
RS = 16.134 (x 1000 ft)



Cottonwood Creek  
RS = 17.087 (x 1000 ft)

