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# DRY GREEK

# DRAINAGE STUDY

for

COLORADO SPRINGS COLORADO



R. KEITH HOOK & ASSOCIATES, INC. ENGINEERS - PLANNERS - CONSULTANTS 2545 E. PLATTE AVE. COLORADO SPRINGS, COLO.

# HYDROLOGIC ENGINEERING STUDY of the DRY CREEK DRAINAGE BASIN

for

THE DEPARTMENT OF PUBLIC WORKS COLORADO SPRINGS, COLORADO

November, 1966

R. Keith Hook & Associates, Inc. Engineers-Planners-Consultants Colorado Springs, Colorado

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Director of Public Works City Hall Colorado Springs, Colorado

Dear Sir:

Enclosed herewith is the engineering study of Dry Creek Drainage basin system.

This report describes precipitation run-off conditions as affected by existing terrain and as will affect proposed developed areas within the basin and methods of conveying subject run off.

Very truly yours,

R. Keith Hook & Associates, Inc.

Leonard C. Becker, P.E.



LOCATION MAP

#### I. DESCRIPTION

#### A. Scope and Purpose

This report establishes a drainage pattern criteria showing major and minor drainage systems that fall within the Dry Creek basin, and to its confluence with Monument Creek.

The subject drainage systems, as shown, and as described, will affect future land development with regard to proposed street systems, drainage structures and planned greenbelt systems, primarily within the Rockrimmon and Woodman Valley Subdivision areas.

It is the intent of this report to provide a guide to indicate areas of best suited roadway alignment; size and location of required drainage structures, roadways, reservoirs, or other drainage appurtenances.

Final subidivision of land may vary from guidelines, as established in this report; however, general requirements should be maintained.

#### B. Basin Description

The Dry Creek drainage basin covers approximately 3.9 square miles (2,494 Acres) lying within portions of Sections 32 and 33, Township 12 South, Range 67 West; Sections 1 through 5 and 10, 11, and 12, Township 13 South, Range 67 West and Sections 7 and 18, Township 13 South, Range 66 West. The area is located North and Northwesterly of Colorado Springs and bounds the the Woodmen Valley area and a portion of the Pikeview area.

Major surface run off flows from within the Pike National Forest boundary at the Westerly portion of the basin; thence Southeasterly into Monument Creek. Approximately 1.17 square miles is located within the Pike National Forest.

The topography of the basin is mountainous in the Western portion, gradually diminishing to a meadowland valley type terrain toward the central and Easterly areas. In the central and Easterly portion, the land widens into general gradual slopes and in the Central area meadowland terrain is predominate and in the Easterly portion it is more foothill type terrain. At Pikeview, the land is quite gently sloped.

Several minor drainage basins contribute to the Dry Creek basin, as shown on the drainage plan.

### I. (B.) continued.

All stream flow is intermittent throughout the basin.

The Westerly portion being mountainous creates a distinct channel system where surface flow is in narrow valleys creating small stream effect. Toward the central portion, no distinct channels exist, as this area of Woodman Valley is a wide basin and surface flow is contained in small roadside type ditches. Infiltration is high with low surface flow. In the Easterly portion, certain foothill terrain areas have distinct drainage channels, due to higher velocities in this area. Particular areas are as shown in the boundary of Rockrimmon Subdivision.

# C. Geological Formation and Soils

The Western portion of the Dry Creek basin consists of disintegrated Pikes Peak granite though found in both the solid and decomposed state.

Infiltration is relative high and surface run-off low.

The area is steep and channels have little distinction.

In the Central area, formation resulted from front range faults creating hogback appearance. This area has been covered by mesa gravels consisting of disintegrated gravel. Infiltration is high and run-off low, though some clayey sand is contained in the soil composition. Bedrock areas consists of Dawson Arkose, the Laramie formation and Pierre Shale in that order of increasing age. Bluff's in this area are formed from the Laramie and Foxhills Sand which is predominately sandstone, with minor clays.

In the Easterly portion of the basin, surface soils are overburden material, generally sandy. The range classification of the soil however, is from a clay size to gravel and in most cases, is immediately below the alluvium.

Basic soil in lower formation is Pierre Shale.

Infiltration in this area is high enough to result in comparable low run-off. Where Pierre Shale is exposed, run-off is high.

#### D. Rainfall

U. S. Weather Bureau records indicate approximately 14.5 inches per year rainfall is average, with major precipitation occuring in the months of April, May, July and August, with peaks up to 8.2 inches. Average high being in July, measuring 2.94 inches. Maximum high recorded in May.

The intense storms last approximately two (2) hours and longer storms up to six (6) hours.

It is evident in this basin, the longer storms produce a high volume of surface run-off, but do not create flooding.

The shorter, higher intense storms have created flooding conditions in lower sections, though not damaging to waterway systems.

It can be expected, from past records, the Dry Creek basin will experience storms of 2-inch intensity for one (1) hour periods at approximately 3 to 3.5-year periods. However, a 50-year frequency, 1-hour duration, 2-inch intensity has been designated by the City of Colorado Springs for design purposes and has been used in calculations for this study and report.

#### E. Surface Flow Criteria

Dry Creek basin has been divided into major and minor basin areas, as shown on the master drainage plan.

At the outfall point of each minor basin, peak run-off has been computed showing quantity of surface flow at the minor basin and major basin.

These flows will give the quantity of each minor basin the combined flow of the major basin, and finally the total flow of the entire basin.

From calculation tables and the drainage plan, surface flow can then be determined at any point in the basin.

All flows have been computed on a time element and the combined synthetic hydrographs were constructed for succeeding points as peak flow proceeds downstream. It will be shown that the peak time of the combined hydrograph increases as the crest flows downstream.

The hydrographs have been constructed in the absence of actual rainfall measurements and available data has been obtained from the Soil Conservation Service. When gaging has been instituted, adjustments to the hydrograph may be necessary.

#### I. (E.) continued

It is recommended a main gaging station be provided at the outfall of Dry Creek basin.

The hydrograph construction assumes the major portion of the Dry Creek basin will be developed into rural type residential units, excluding the National Forest area.

At the present time, a portion of this basin has been subdivided and future subdivisions are being planned.

#### F. Greenbelt System

The proposed routing of the greenbelt system within the Dry Creek drainage basin will basically follow the natural drainage course to allow the best use of the land as subdivisions are developed.

In the central portion of the basin, that area being developed as a part of the Woodman Valley Complex, the demarcation of surface run-off is not definite, due to the wide basin and meadowland terrain.

In the Rockrimmon area, drainage channels are well defined. This greenbelt strip will be used for parks and in open space, as playgrounds. It is the intent of the developer in this area to leave the channels in their natural appearance and configuration and provide slope treatment and maintenance that will up-grade the present channels.

The required widths of the greenbelts Right of Way, as shown on the drainage plan, will provide sufficient channel width to maintain approximately 2.5 to 4.5 feet of water depth during design rainfall and run-off. Sixteen feet access will also be included in Right of Way requirements.

In the area of this basin where gullies have been cut by run-off and subsequently eroded, it is recommended greenbelt channels be protected by providing erosion control and velocity control measures to be determined prior to subdivision development. Riprap shall be provided at all bends in the channel.

As this basin area is mountainous with some relative steep grades, a major portion of the greenbelt system would then require erosion protection, particularly in areas where a flooding condition may occur or where continued erosion may endanger future development. To provide logical protection without causing high cost construction, it must be determined

#### I. (F.) continued

in future planning and development the type of land subdivision contemplated.

During the preparation of this report, the various areas were analyzed with regard to future subdivision type development. In the Central portion, the area is a wide basin, open meadowland, where home sites will be clustered on acreage tracts. In this area, distinct shaping and construction of the greenbelt system is necessary with erosion protection required. In the East Central, more wooded and rustic type terrain exists, and future planning will provide for large undeveloped areas adjoining the greenbelt systems. Construction of homes will be hundreds of feet from the channel alignment. It is the intent, of course, to allow natural setting in this area.

Erosion is evident, and the greenbelt system will require some alignment changes and erosion protection. However, whether actual concrete line sections in this area are actually required and the extent of these sections, will have to be studied during development. It may be necessary in lower greenbelt areas (Easterly sections) to provide velocity control structures. In establishing drainage costs to the greenbelt systems, the major portion of the greenbelts were considered as requiring erosion protection by concrete lining or riprapping.

#### G. RESERVOIRS

Within the basin, thereis one (1) existing reservoir designed and constructed by the U. S. Soil Conservation District. This reservoir was provided to control erosion during high intensity storms. The dam is earthen fill and impounds 9.6 acrefect of water.

Subject reservoir is designated R-1 on the drainage plan. Under consideration of this drainage report and in compliance with the drainage board decision, this reservoir will not be maintained and a continuous channel will be indicated.

Existing lakes within this basin, as shown on the drainage plan, do not fall within the greenbelt channel and are therefore not considered in this report.

#### H. IMPROVEMENTS

The proposed improvements within the Dry Creek drainage basin consist of green-belt channel systems, concrete drainage culverts, drainage piping, drainage roadway outlets, bridges and modification as described. All drainage appurtenances are so located as to best suit proposed development.

It is the intent of the improvements to provide a roadway and drainage systems network that will not create problems during fifty-year design

#### I. (H.) continued

storms. Sufficient drainage outlets and ditches have been provided to relieve street and roadway from conveying excess water. Surface flow will not be contained in major thoroughfare roadway systems.

No specific catch basin, curb opening or drainage outlets have been designed in this report, as these structures will be applicable only to final developed conditions and should be designed to meet the specific need.

In the construction of ditches, means shall be provided to prevent erosion, particularly when velocities exceed 7 f.p.s.

Relative to the location and slope of ditches, concrete lining, sod, or native grass should be provided as a lining. Costs for ditch construction are based on all ditches being concrete lined or riprapped

With respect to the design of greenbelt systems, it is recommended in gulley regions, particularly in the Easterly portion, the channels be maintained in their present configuration. This is a somewhat narrower channel with approximate  $1\frac{1}{2}$ :1 slopes. Surface flow will be somewhat deeper than a more common greenbelt design but will better suit the surroundings.

It shall be noted in some cases roadway or street systems are not continuous. Where this occurs, the roadway or street system terminates at a cul de sac.

In the Rockrimmon boundary the roadway and drainage systems are designed to conform to the development pattern of the subdivision. At the Pikeview area, existing structures are to be removed and revised as shown.

In the Woodman Valley district West to Mt. St. Francis area, the development is in large tract type subdivision. The Woodman Valley Road is the only main access approach to the area; present and future development will not change the present alignment.

Where ditches or greenbelt systems are not lined, as shown on the drawings, velocities are such that erosion is not anticipated.

### CALCULATIONS

# Dry Creek Drainage Basin

Major Basin	Sub- Basin		ea Sq. Mi.	Bas L(ft)	in H(ft) Tc(Hr.)	Tp(Hr.)	Runoff Flow Q(in.)	Peak Flow (CFS) Qp
А	1 2 3	71.25 115.14 76.64	0.111 0.180 0.120	2200 6100 5700 Total,	1000 0.06 2080 0.15 1480 0.15	0.536 0.590 0.590	0.25 0.25 0.25	25.05 36.91 24.61
					Basin A			86.57*
В	1 2 3 4	62.96 54.00 70.01 62.30	0.098 0.085 0.109 0.097	2800 3300 5000 5000 Total,	1320 1/2 0.07 1180 7 7 0.09 970 //2 0.16 970 //2 0.16	0.542 0.554 0.596 0.596	0.25 0.25 0.25 0.25	21.88 18.56 22.13 18.69
					B <b>asi</b> n B			81.26*
C	1 2 3 4	85.07 47.63 56.89 67.39	0.133 0.074 0.089 0.105	3300 2900 2700 3600 Total,	1140 0.09 1080 0.08 1200 77 0.07 1000 0.10	0.554 0.548 0.542 0.560	0.25 0.25 0.25 0.25	29.05 16.41 19.87 22.69
				,	Basin C			88.02*
D	1 2 3	41.29 74.25 63.29	0.065 0.116 0.099	3000 3900 5000 Total,	400 / 1, 0.13 820 // 0.13 820,/// 0.17	0.578 0.578 0.60 <b>2</b>	0.35 0.35 0.35	19.00 34.10 27.10
					B <b>a</b> sin D			80.20*
E	1 2	106.58 108.14	0.167 0.169	6000 4300 Total,	470 % 0.26 230 - 0.23	0.656 0.638	0.35 0.35	42.90 <u>44.60</u>
				•	Basin E			87.50*
F	1 2 3 4	64.57 66.99 100.32 68.70	0.101 0.105 0.157 0.107	5700 3600 4200 3500 Total,	230	0.698 0.608 0.620 0.614	0.45 0.35 0.30 0.40	31.51 29.24 36.76 33.75
				•	Basin F			131.26*

Major Basin	Sub- B <b>asi</b> n	Ar Acres	ea Sq. Mi.	Ba L(ft)	asin H(ft)	Tc(Hrs)	Tp(Hr.)	Runoff Flow Q(in.)	Peak Flow (CFS) Qp
G	1 2 3	94.19 72.38 78.82	0.147 0.113 0.123	4400 3500 5500 Total,	410	0.27 0.22 0.24	0.662 0.632 0.644	0.45 0.35 0.30	48.52 30.28 27.73
					B <b>a</b> sin G	+			106.53*
H	1 2 3 4	21.03 60.00 99.65 22.17	0.033 0.094 0.156 0.035	2300 4400 3700 2200 Total,	220 310 230 240	0.12 0.21 0.20 0.11	0.572 0.626 0.620 0.566	0.30 0.30 0.30 0.30	8.38 21.81 36.53 8.98
				,	asin H				75.70*
J	1 2 3	87.44 36.90 85.02	0.137 0.058 0.133	5100 2200 4600 Total,	140 150 140	0.33 0.13 0.30	0.698 0.578 0.680	0.70 1.00 1.00	66.49 48.56 94.66
					asin J				209.71*
K	1 2 3 4 5	24.77 32.05 21.34 20.79 54.75	0.039 0.050 0.033 0.032 0.086	2100 3100 1100 1200 2600 Total,	110 150 40 100 170	0.14 0.19 0.10 0.075 0.15	0.584 0.614 0.560 0.543 0.590	1.40 1.40 1.40 1.40 1.40	45.26 55.17 39.93 39.79 98.50
					Basin K				278.65*
L	1 2 3 4 5 6	63.93 20.37 24.59 19.92 51.26 38.95	0.100 0.032 0.038 0.031 0.080 0.061	5000 1500 1000 2700 2600 1800 Total,	150 170 50 100 100 40	0.32 0.08 0.085 0.19 0.185 0.175	0.692 0.548 0.551 0.614 0.611 0.605	1.40 1.40 1.40 1.50 1.40	97.92 39.57 46.73 36.64 88.72 73.20
					B <b>a</b> sin L				38 <b>2.</b> 78*
Qp =	484 AQ	_	Q = <u>(</u>	P2S) <sup>2</sup>	! •	D = 0.5	Тр	= <u>D</u> 0.	6 Те

Tp Q (inches run-off)

D Time excess rainfall

Tp Peak time of hydrograph

F+.8s  $\frac{1}{2}$ 

 $<sup>\</sup>overline{2}$ 

A Area in Sq. Miles

To Concentration Time in Hours

Calculations - Sheet No. 3

Line	Base Qp	Base Tp	Ditch L(ft)	S%	Time(Hr)	Point Tp(Hr)	Qp
1-3	167.83	0.590	2700	13.4	0.093	0.683	263.49
2-3	88.02	0.554	2000	10.0	0.050	0.604	115.23`
3-14	378,72	0.578	4900	4.9	0.090	0.668	641.38
4-5	641.38	0 <b>.6</b> 68	7000	2.6	0.183	0.843	978.46
5 <b>-</b> 6	978.46	0.843	4900	2.0	0.143	0.986	1133.31
6-7	1133.31	0.986	3500	2.9	0.067	1.053	1244.97
8-9	39.79	0.543	400	7.5	0.006	0.549	47.20
10-11	98.50	0.590	1000	3.0	0.018	0.608	104.77
12-13	39 <b>.</b> 5 <b>7</b>	0.548	500	6.0	0.006	0.554	62.57
14-15	134.56	0.692	1000	4.0	0.015	0.707	157.56
16-17	88.72	0.611	550	1.5	0.015	0.626	88.72
18-19	73.20	0.605	800	5.1	0.011	0.616	73.20

# ${\tt C} \ {\tt A} \ {\tt L} \ {\tt C} \ {\tt U} \ {\tt L} \ {\tt A} \ {\tt T} \ {\tt I} \ {\tt O} \ {\tt N} \ {\tt S}$

Dry Creek Drainage Basin

# Greenbelt System

Ditch Configuration

			ncrete	rigurati Rip		Unlined	V(Ripra		ର
<u>Line</u>	<u>5%</u>	W(ft)	) d(ft)	W(ft)	d(ft)	Velocities Ft/Sec	$\underline{ t Ft/Sec}$	Cap.CFS	Actual CFS
1-3	13.4	3	3	6	3	10	30	630	263.49
2-3	10.0	3	3	6	3	8	30	540	115.23
3-4	4.9	3	4	8	3	18	27	800	641.38
4-5	2.6	3	5	10	3	18	23	1000	678.46
5-6	2.0	3	5.5	12	3	25	22	1150	1133.31
6-7	2.9	3	5.5	12	3	30	30	1400	1264.97
8-9	7.5	3	3	6	3	8	30	500	47.20
10-11	3.0	3	3	6	3	3	18	290	104.77
12-13	6.0	3	3	6	3	5	28	500	62.57
14-15	4.0	3	3	6	3	5	20	360	157.56
16-17	1.5	3	14	8	3	3	15	1500	88.72
18-19	5.1	3	3	6	3	5	24	430	73.20

\*Side slope for ditch is assumed to be 1.5:1.

Ditch Systems	<u>5%</u>	<u>M</u> €	t) <u>D(ft</u> )	Unlined Velocity Ft/Sec	Q Cap.CFS	Q Actual CFS
1	14	4	3	10	120	88.00
2	8	3	1.5	10	35	28.00
3	5	j÷	3	12	11+0	68.00
4	3	3	1.5	14	20	10.00
5	8	3	1.5	9	35	15.00
6	7	3	1.5	8	32	15.00

\*Ditch Systems, continued.

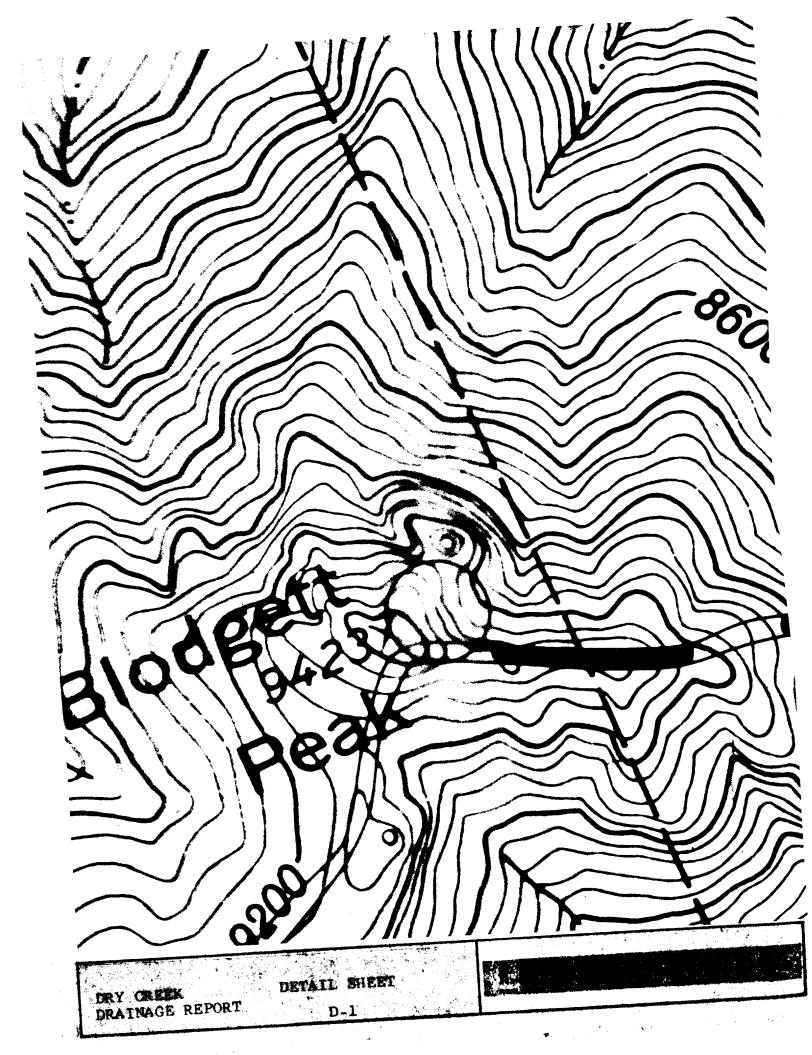
\*Ditch Systems, continued.

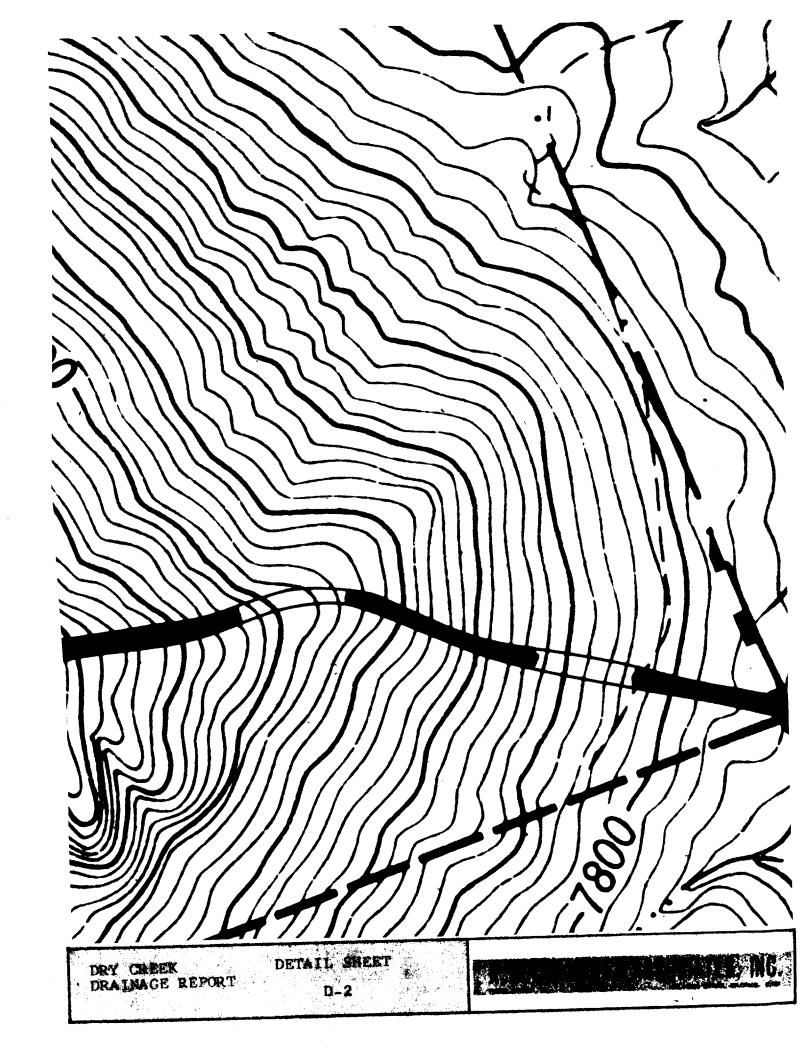
nel 1 Guertona	S. 0/2	W	D	Unlined Velocity Ft/Sec	Q Cap.CFS	Q Actual CFS
Ditch Systems 7	<u>s%</u> 5	$\frac{W}{3}$	$\frac{D}{1.5}$	6	28	20.00
8	6	3	1.5	7	30	22.00
9	6	3	2	8	50	35.00
10	6	3	2	8	50	35.00
11	<u>1</u> ;	3	1.5	5	25	12.00
12	6	3	1.5	7	30	15.00
13	8	3	1.5	9	35	13.00
14	10	3	1.5	1.1	38	14.00
	5	3	1.5	6	28	18.00
15	6	3	1.5	7	30	14.00
16	4	3	1.5	5	25	16.00
17					25	20.00
18	<del>) †</del>	3	1.5	5		
19	14.	3	1.5	5	25	21.00

<sup>\*</sup>Side slope for ditch is assumed to be 1.5:1.

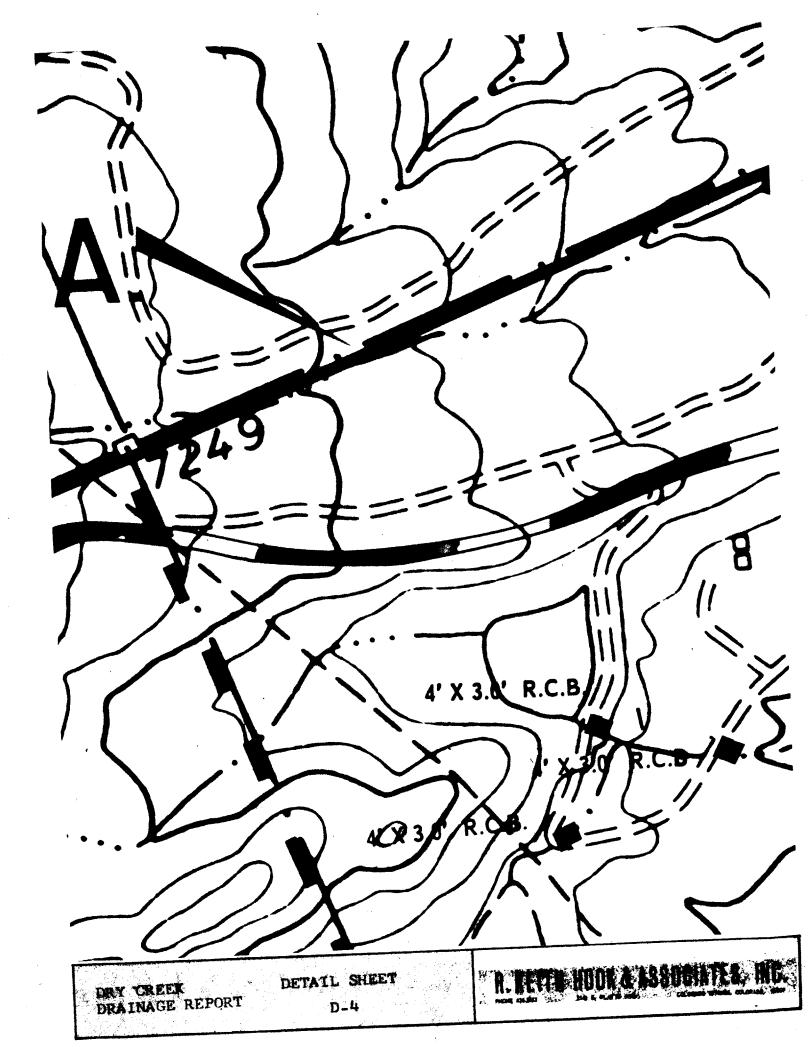
# LEGEND

SUB-BASING MINOR B	BOUNDARY ASINS OLLECTION ROADWAY BRIDGE CULVERT	POINT	
GREENBELT  RIPRAP  PROPOSED  PROPOSED  PROPOSED  SPECIAL	ORAINAGE DRAINAGE	STREET STRUCTURES IER & DRAINAGE OI DITCHES DESIGN	JTLET

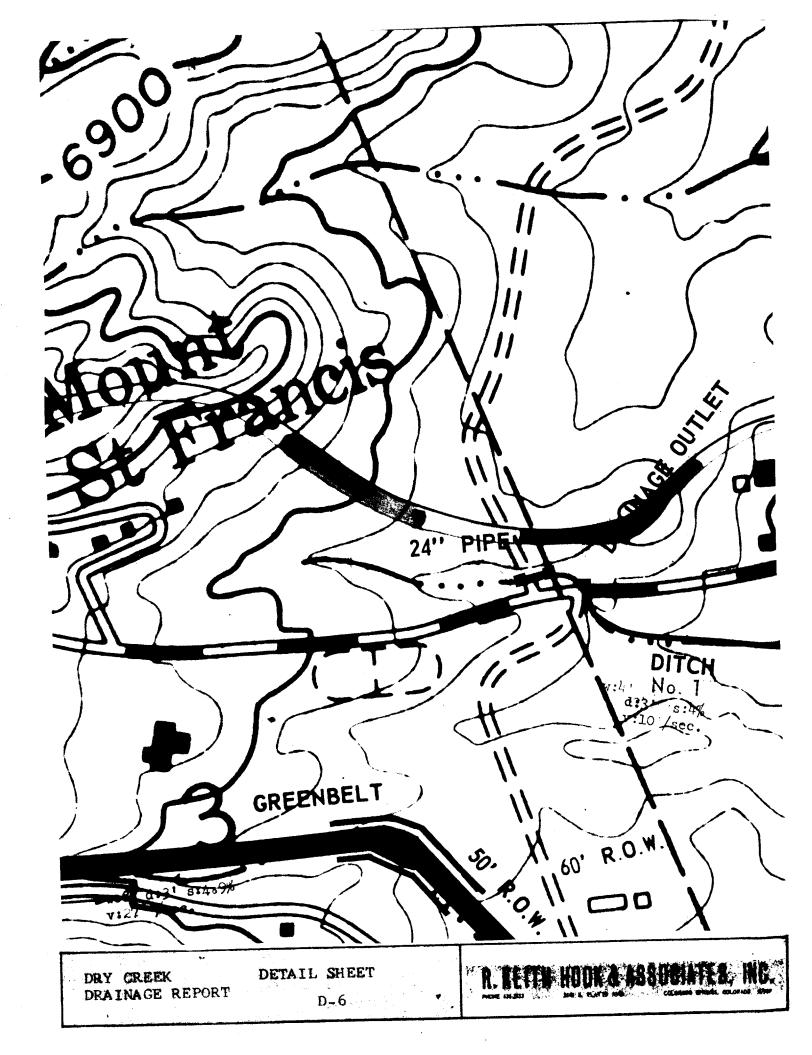


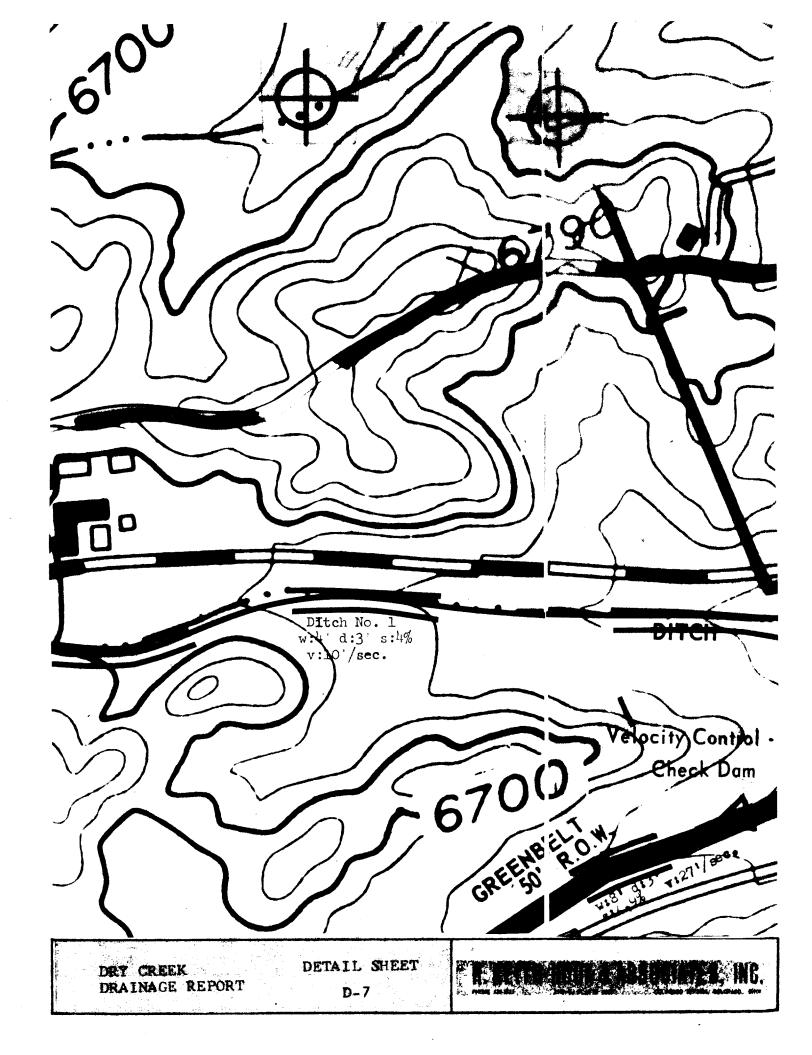


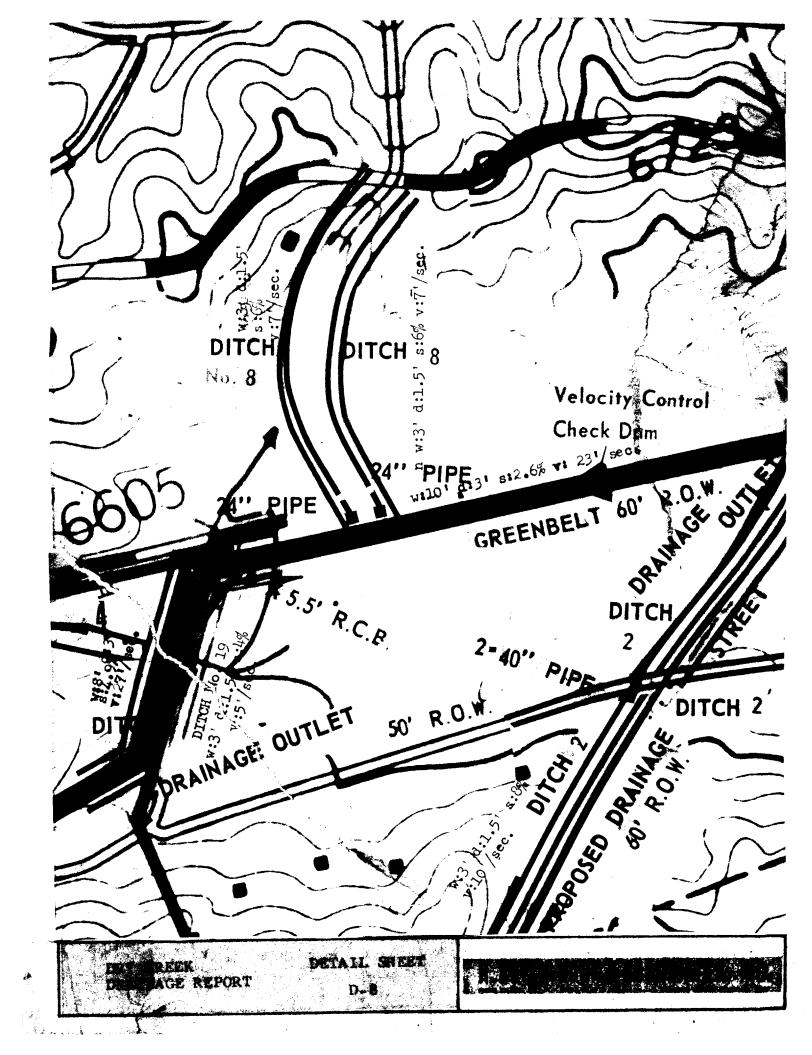


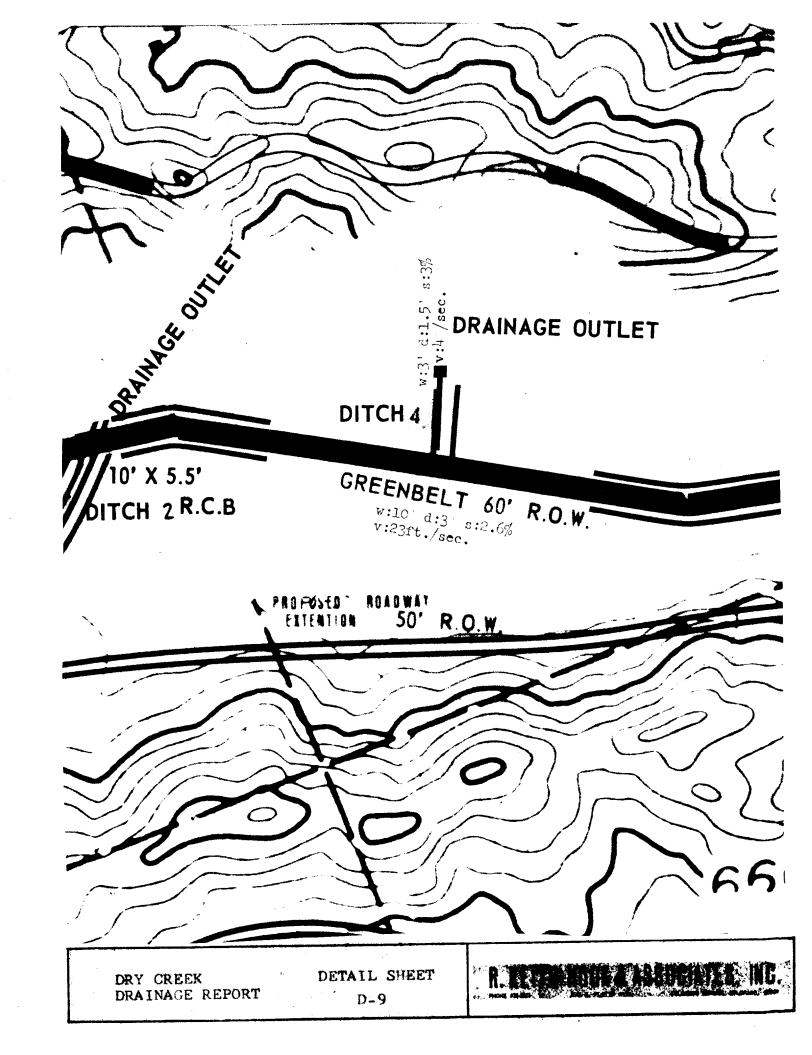


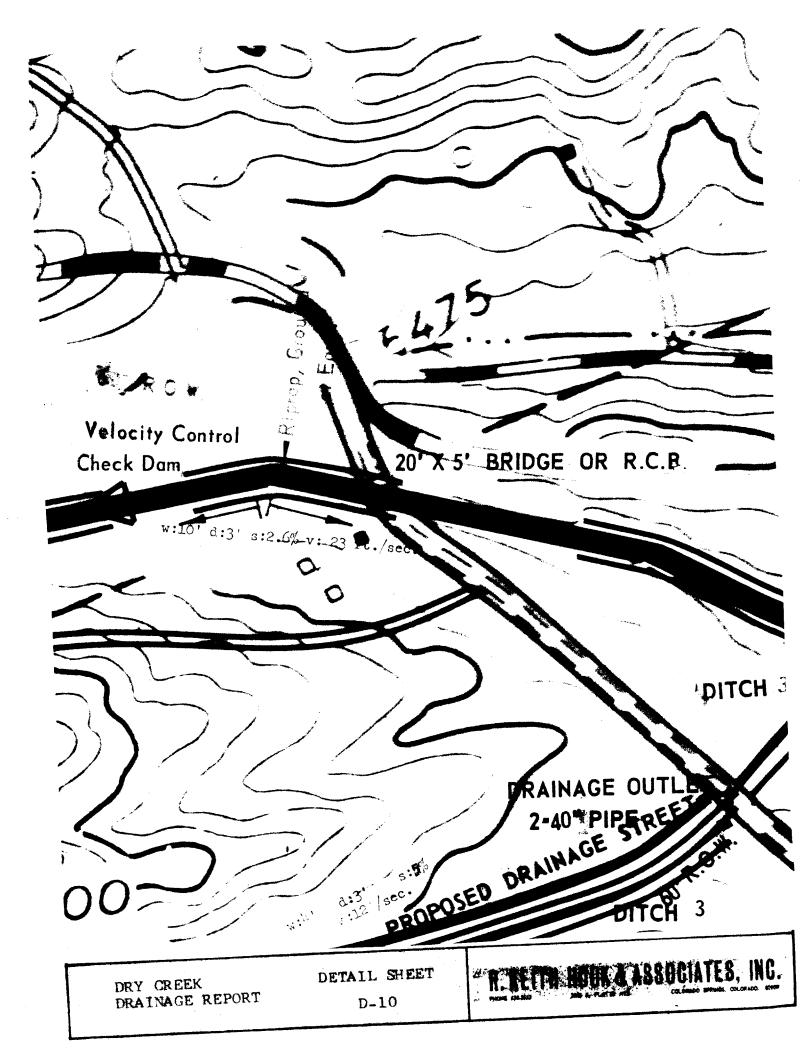


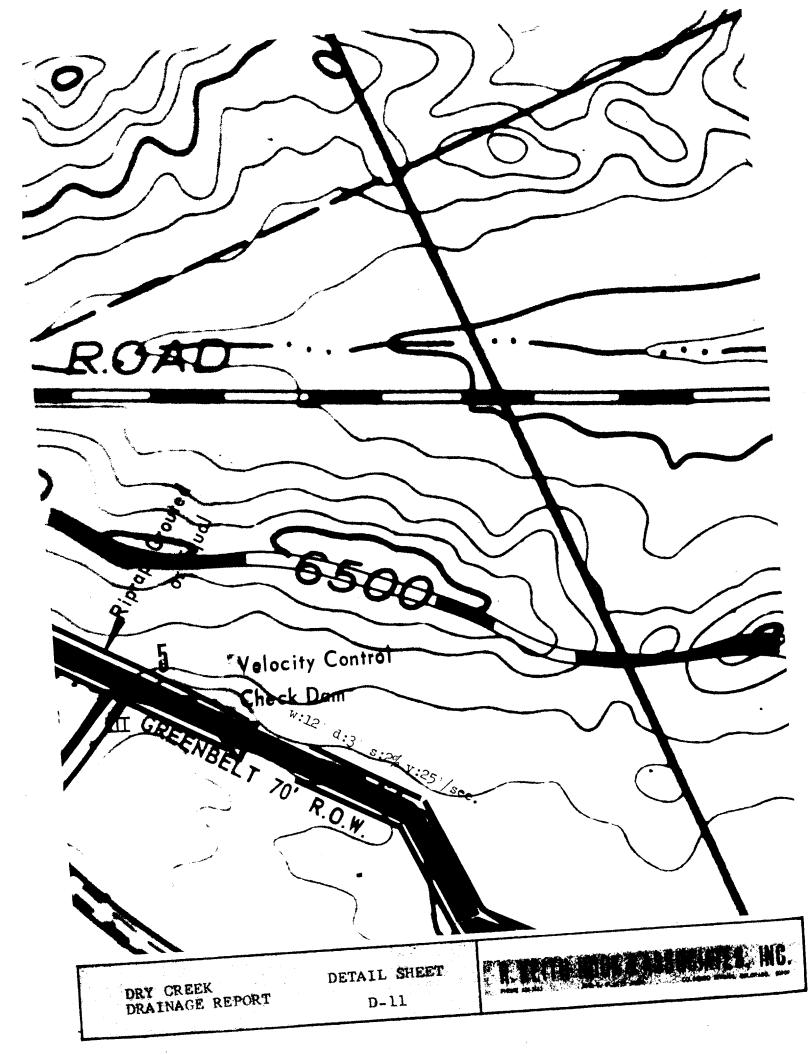


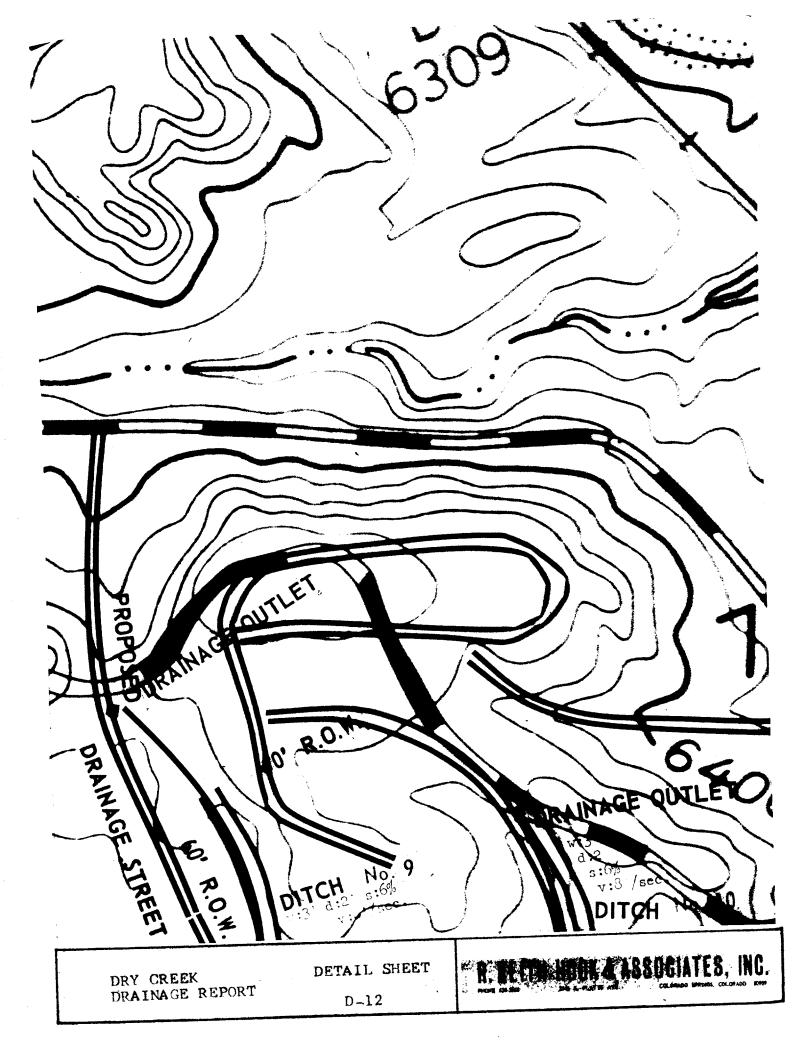


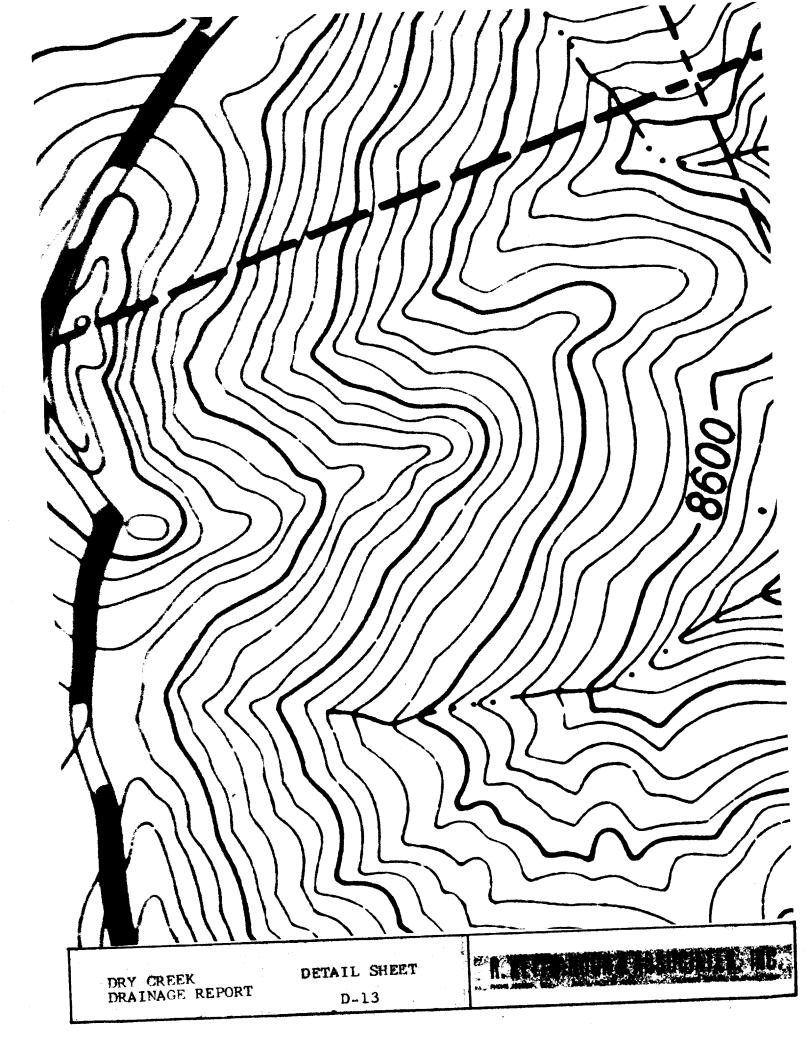


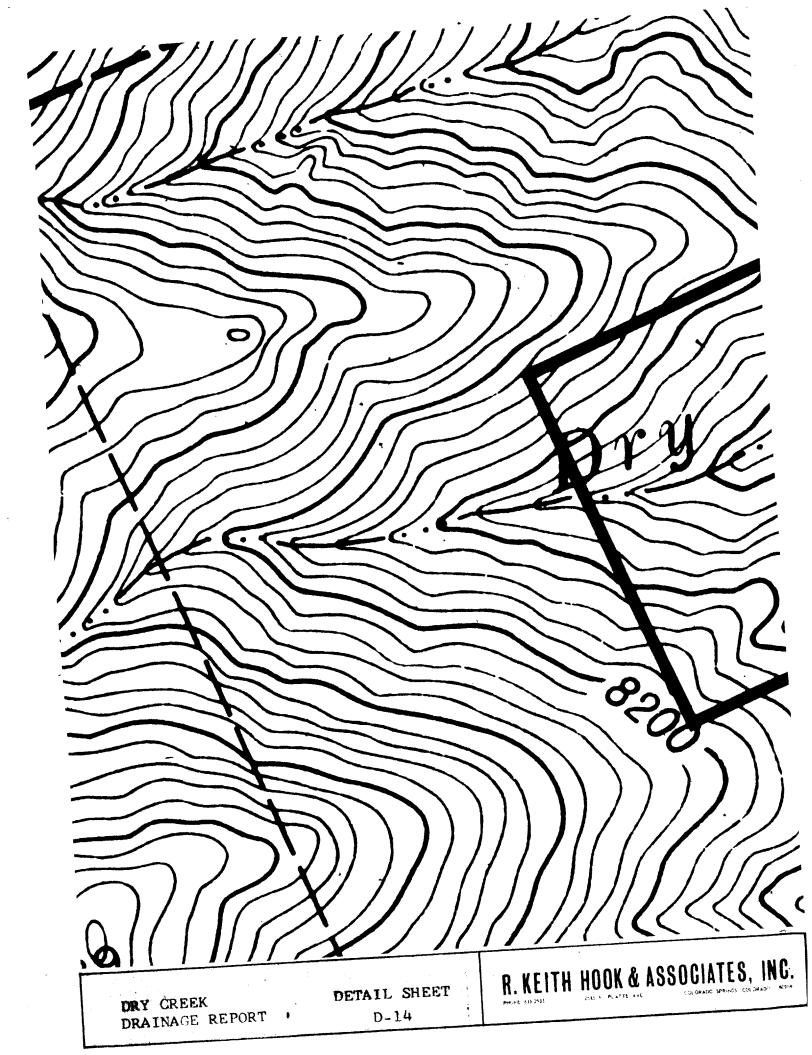


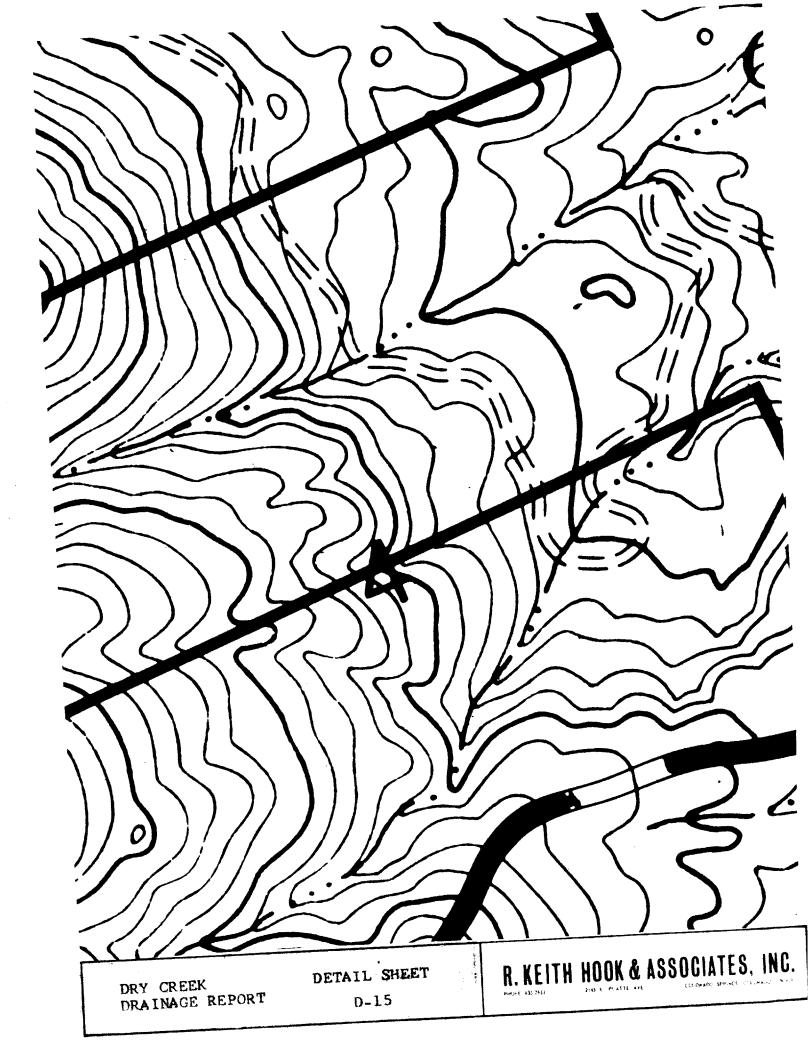


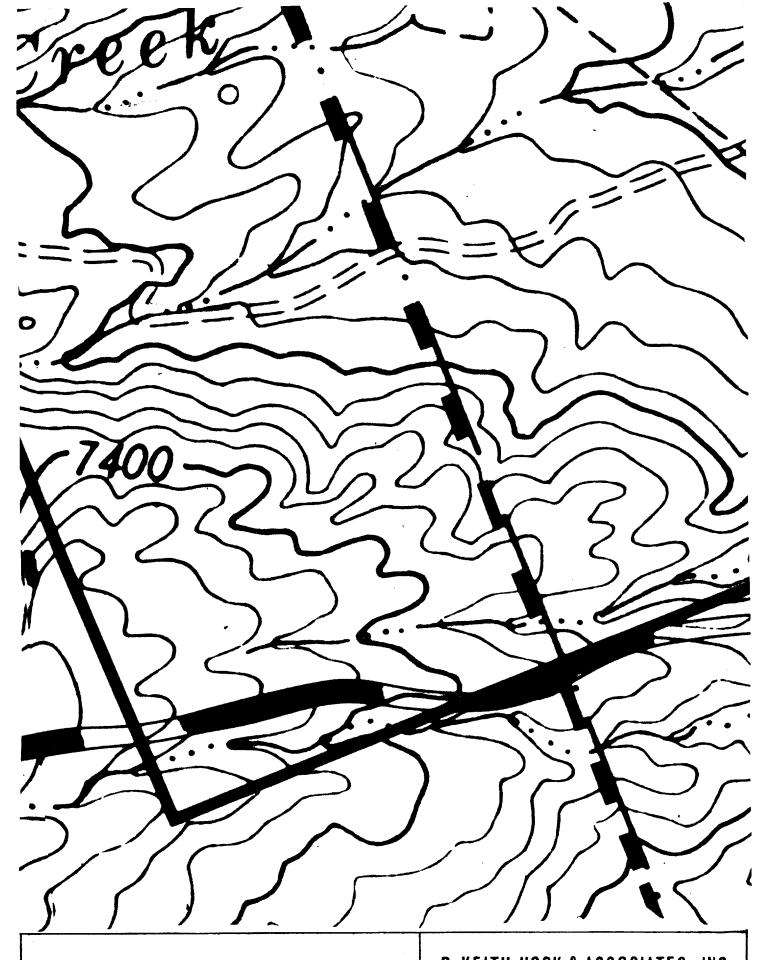








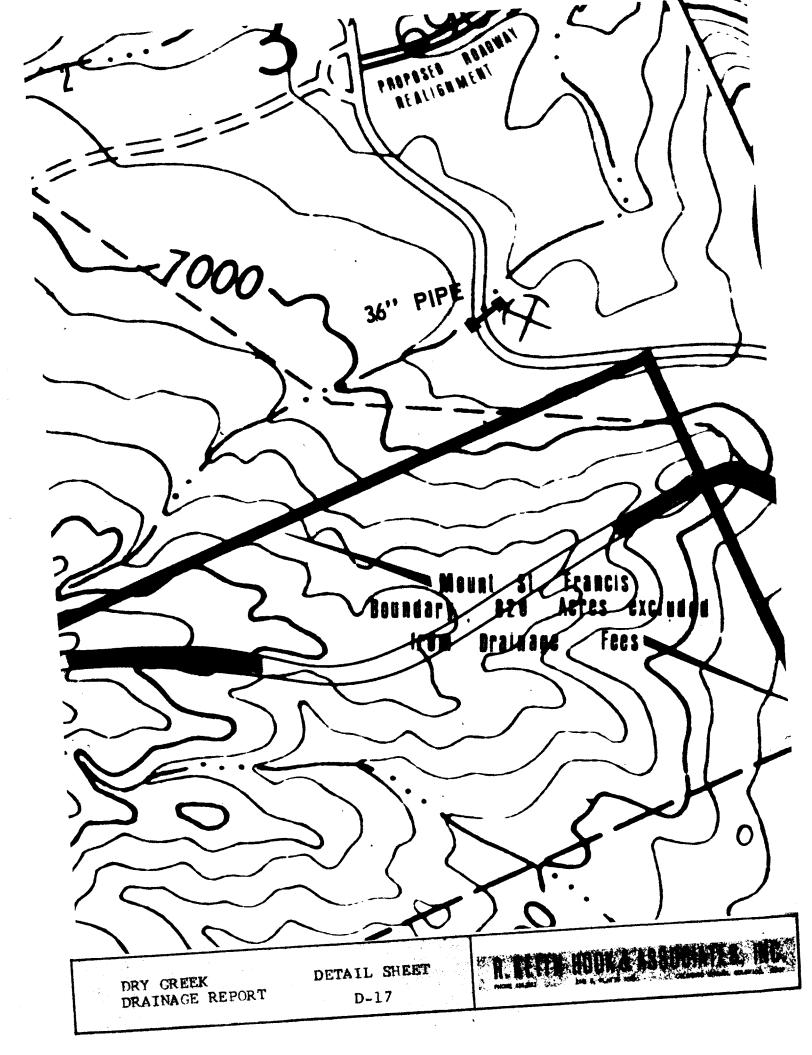


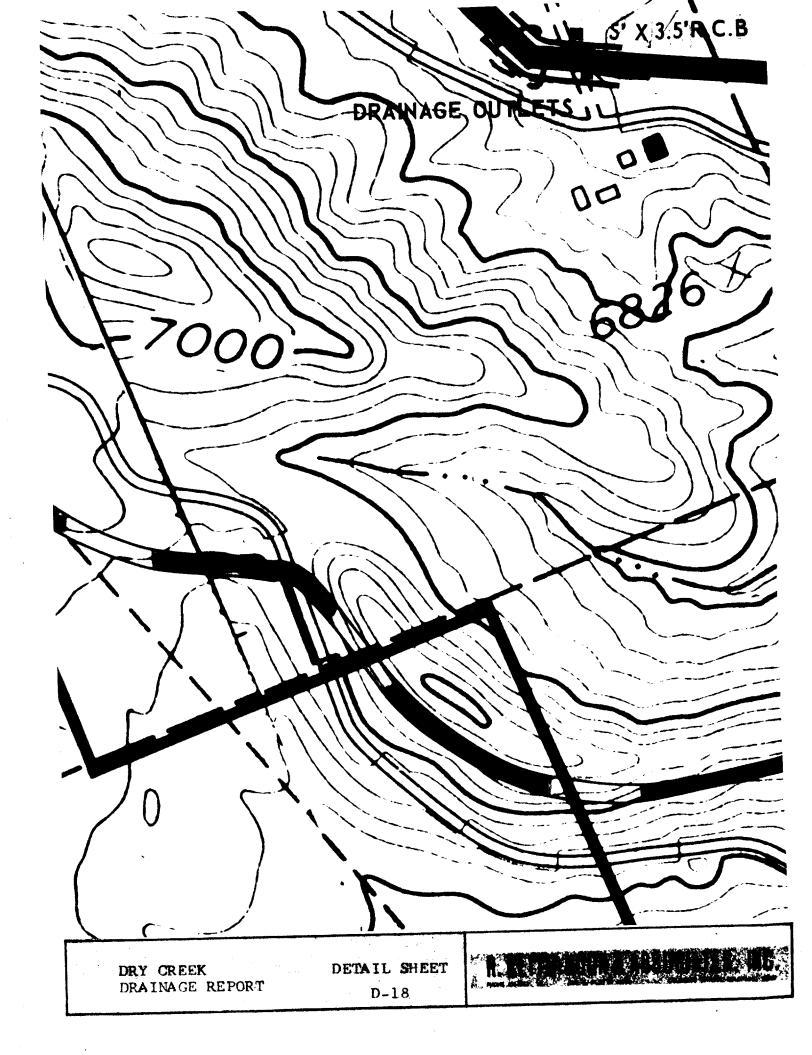


DRY CREEK
DRAINAGE REPORT

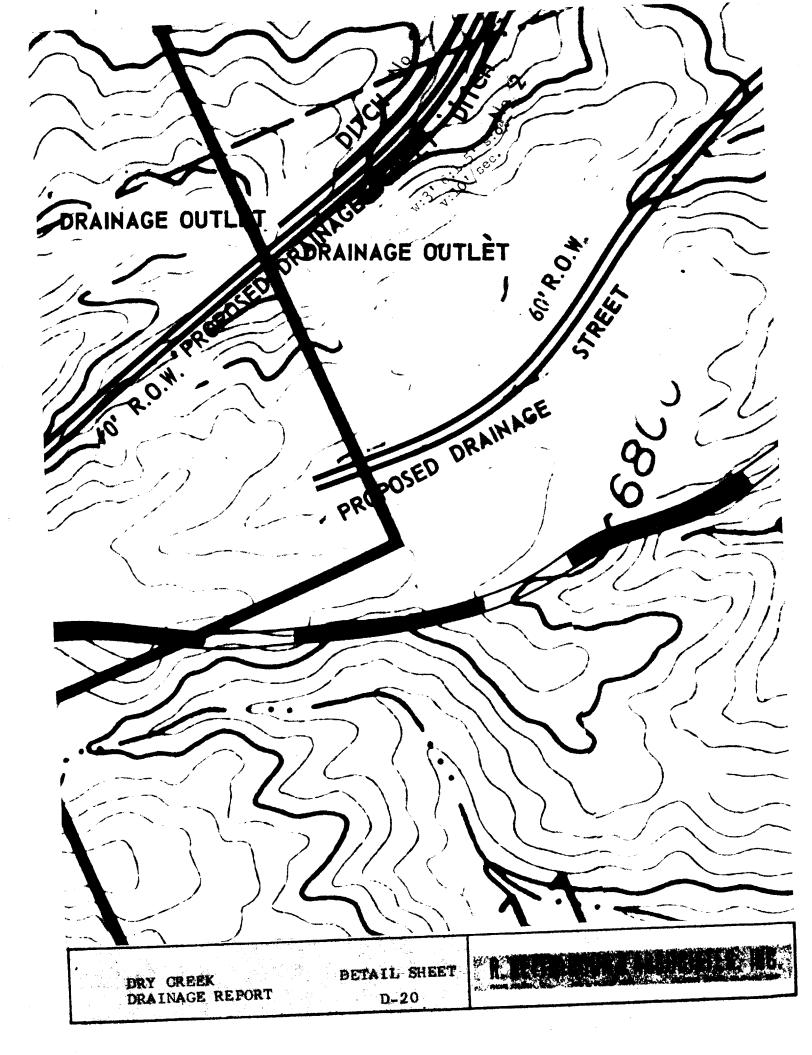
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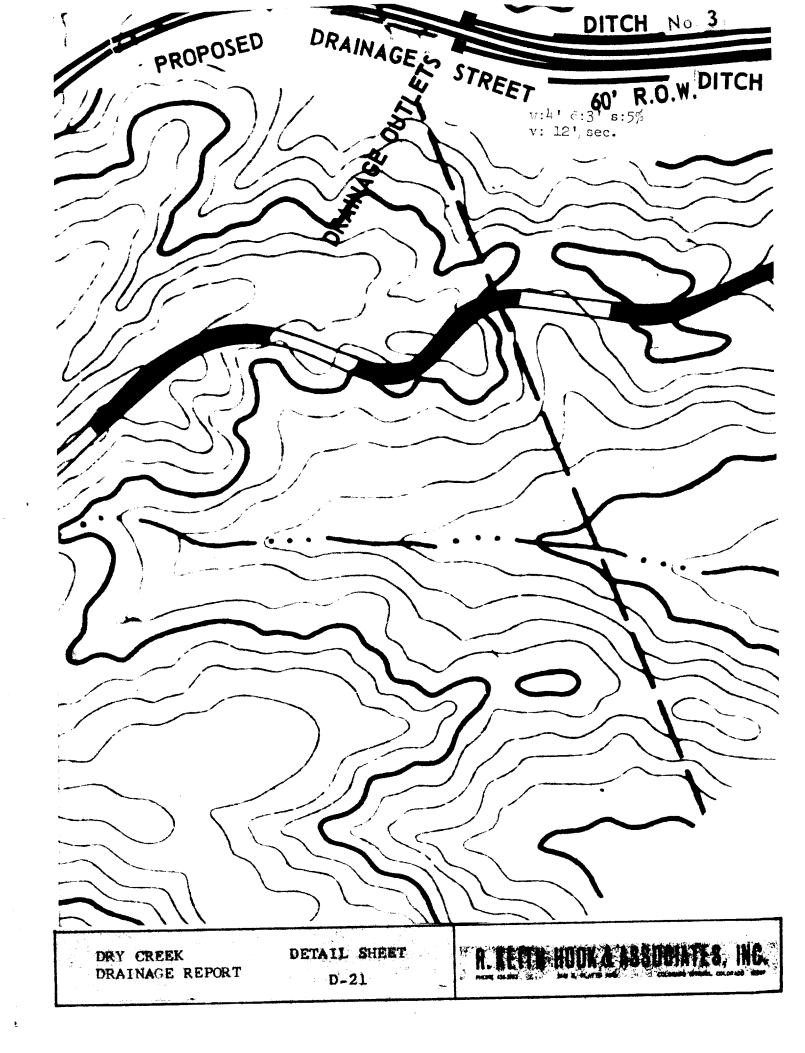
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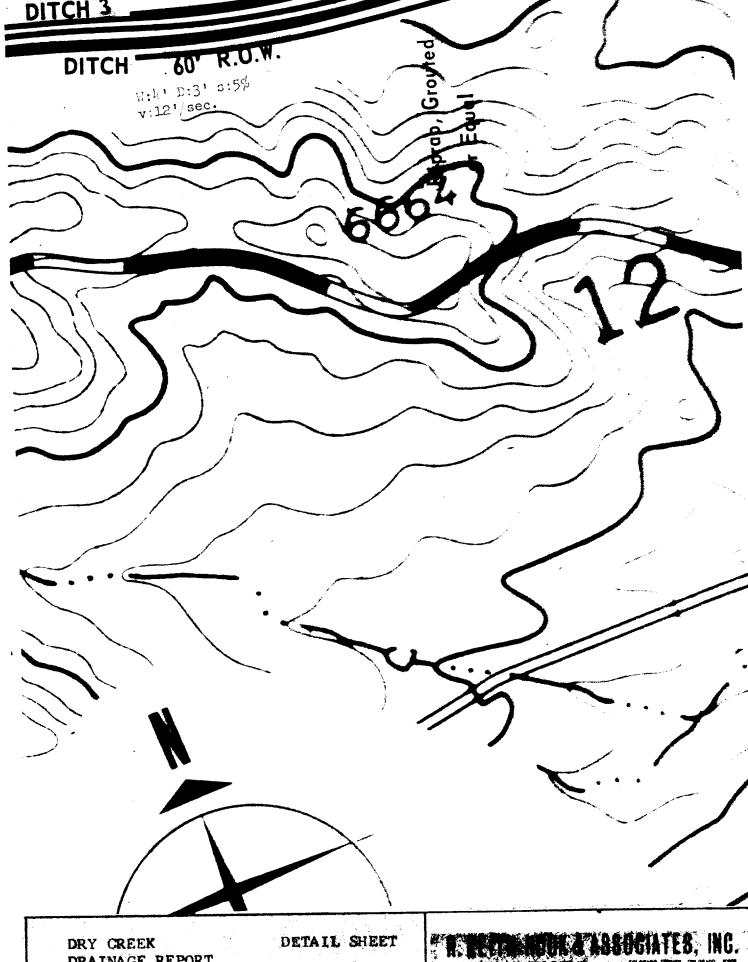






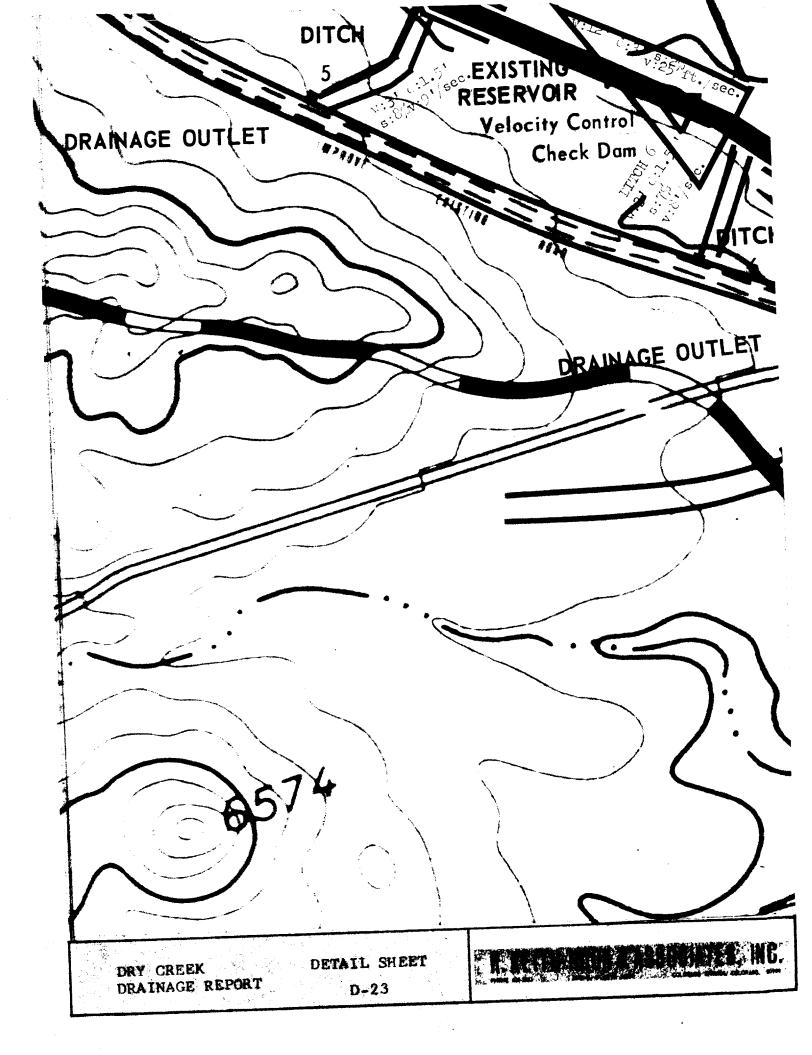


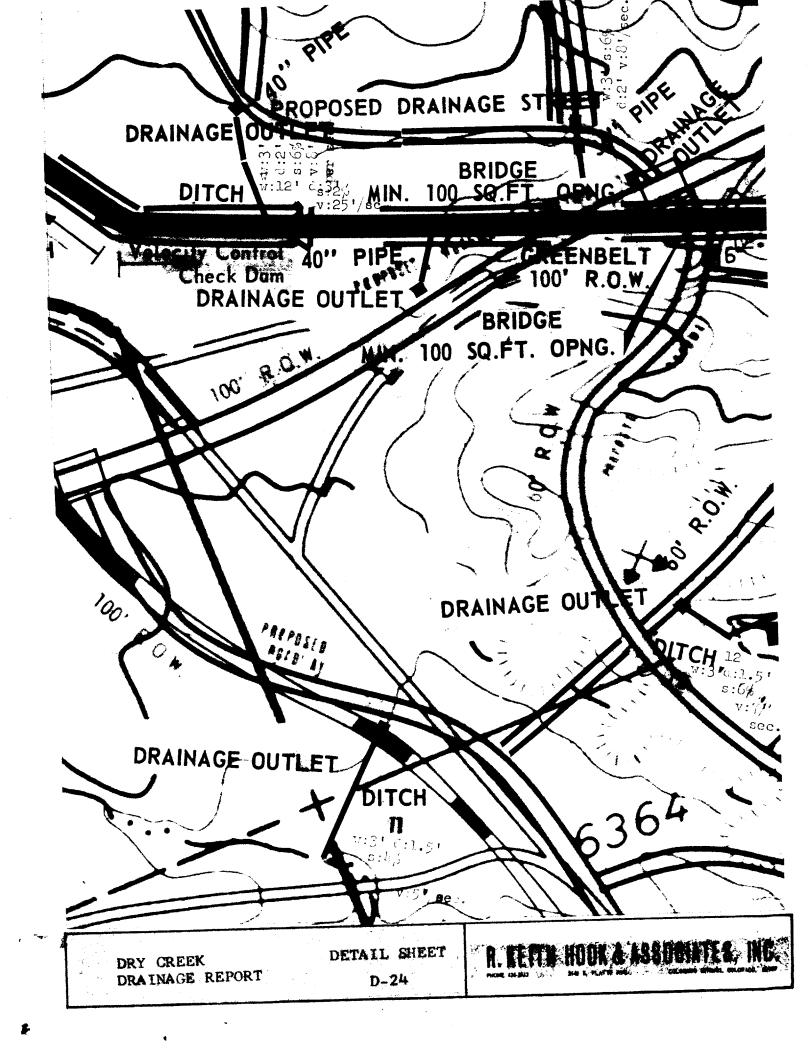


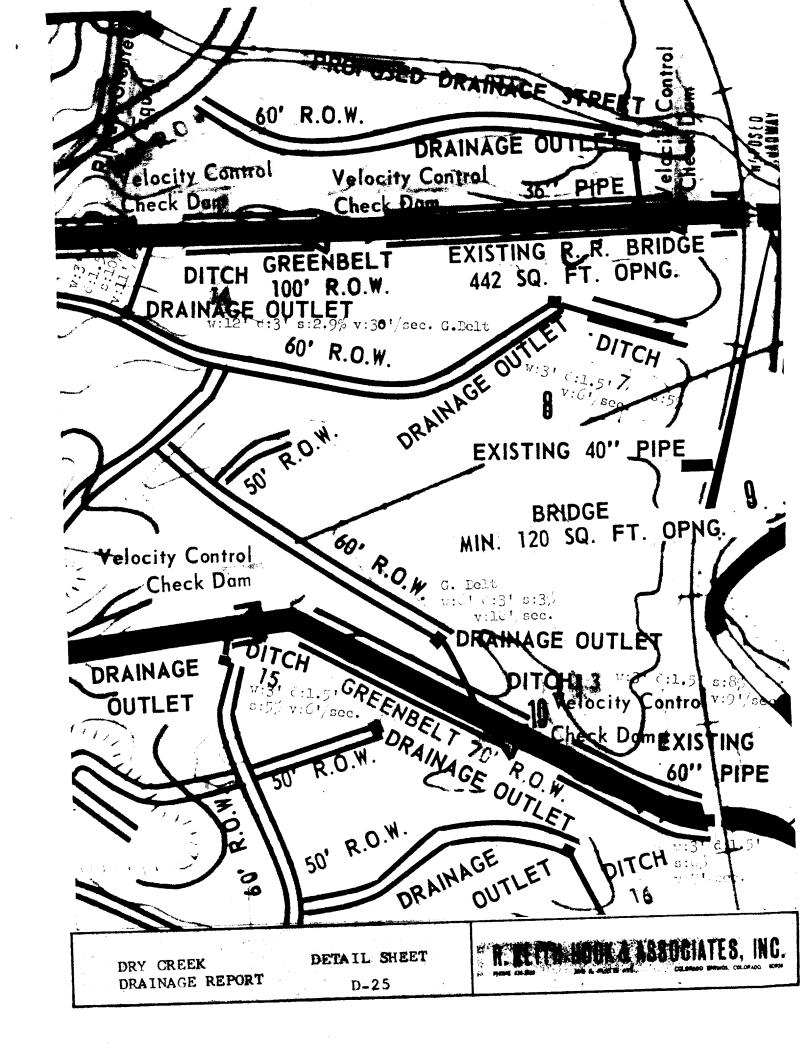


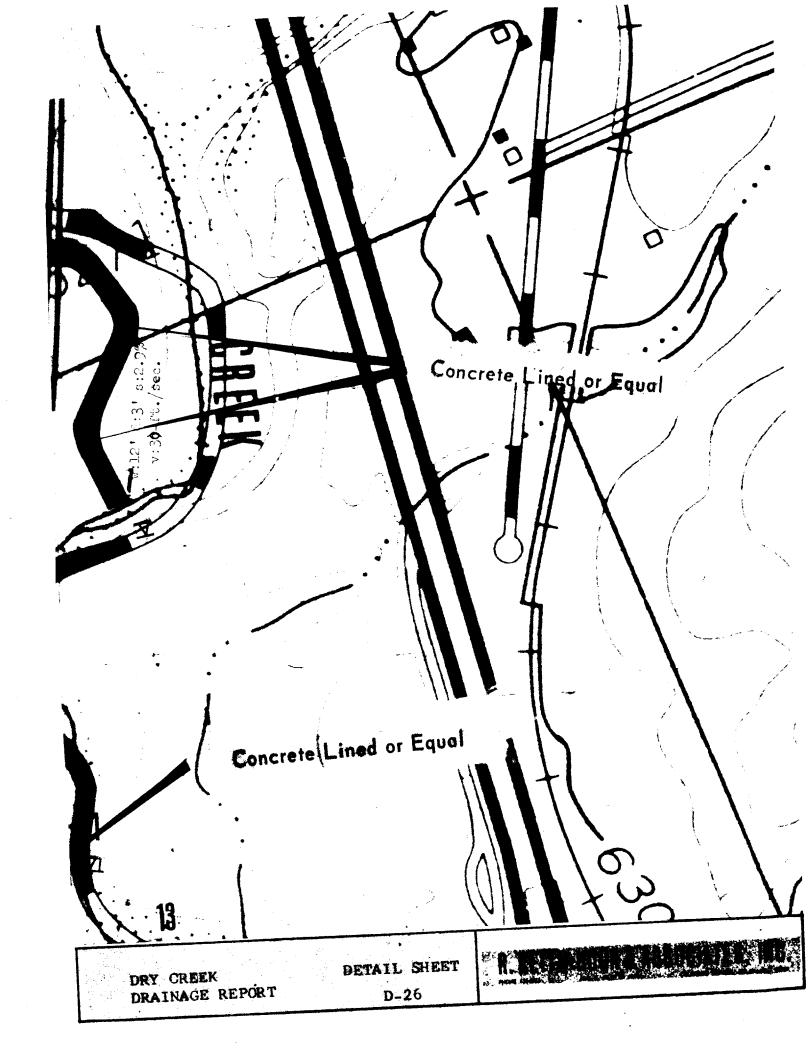
DRAINAGE REPORT

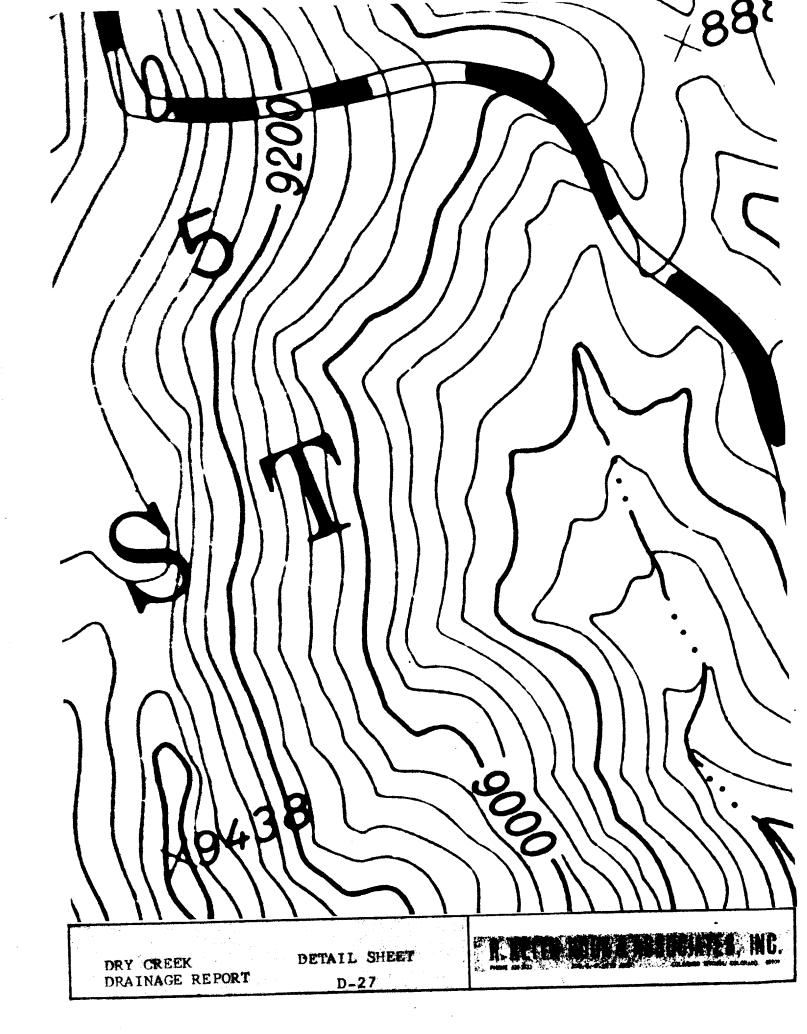
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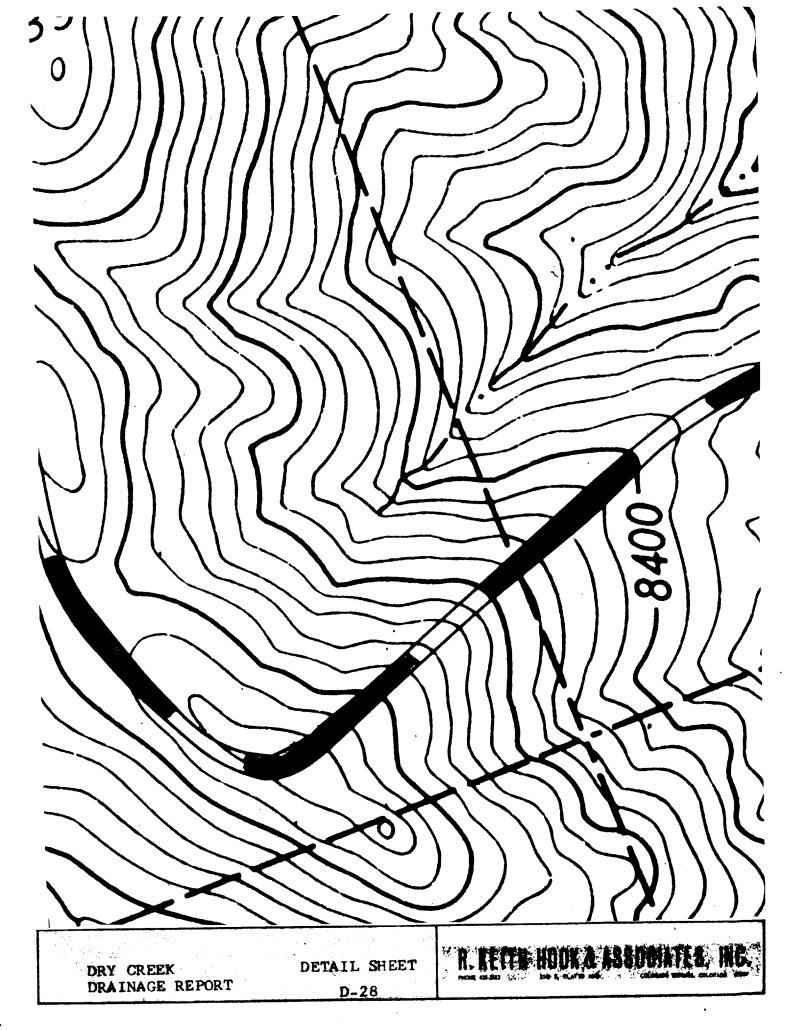


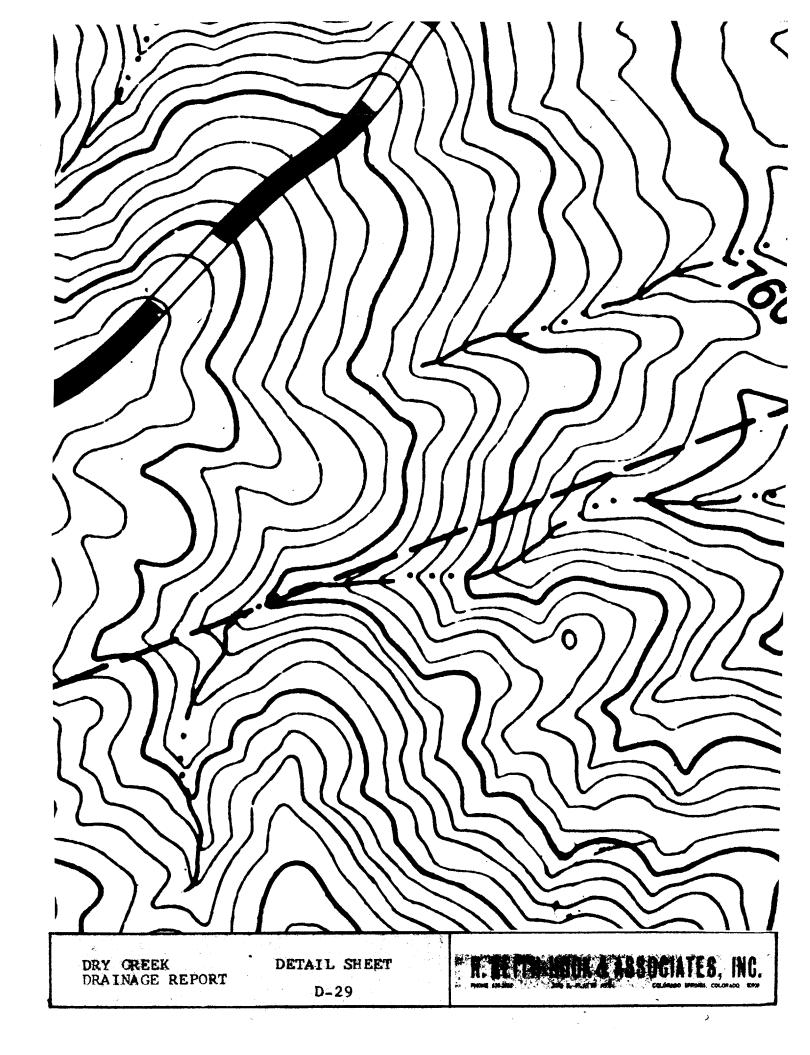




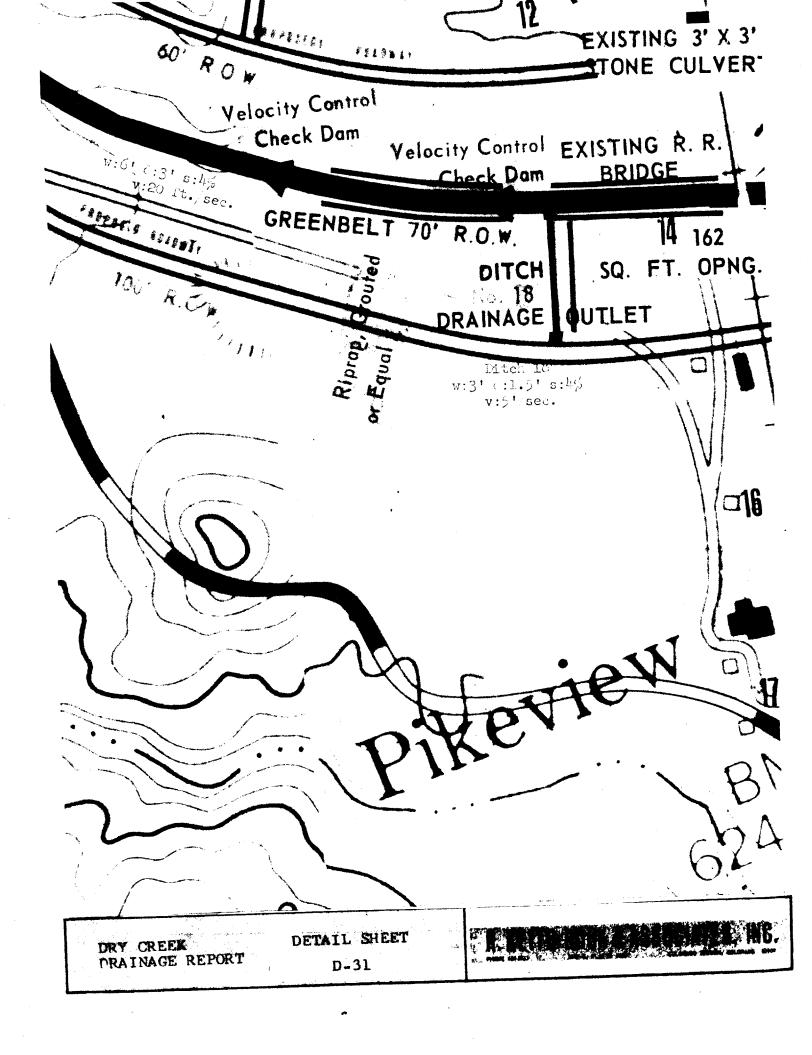


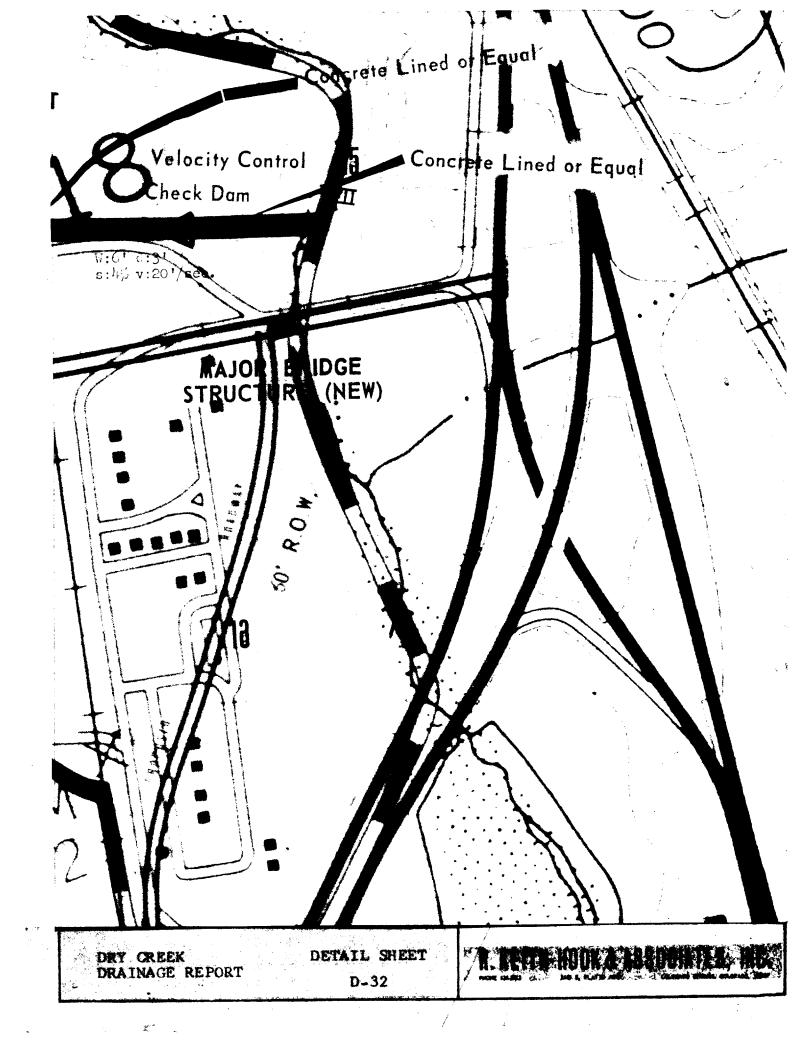


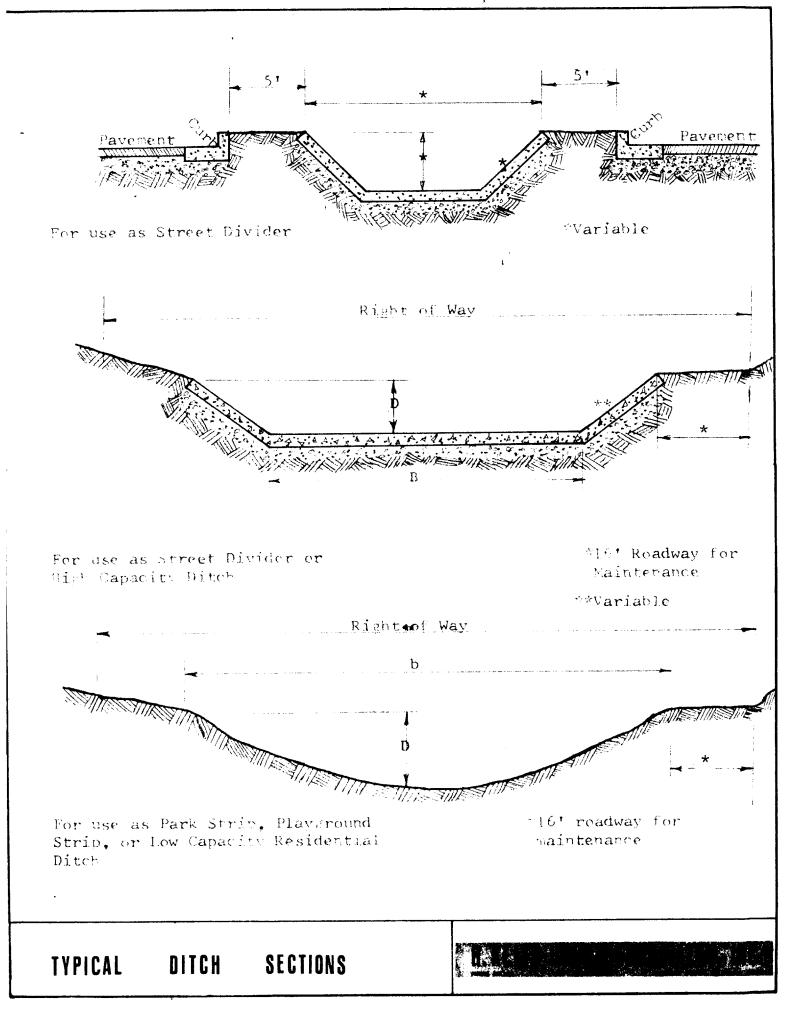


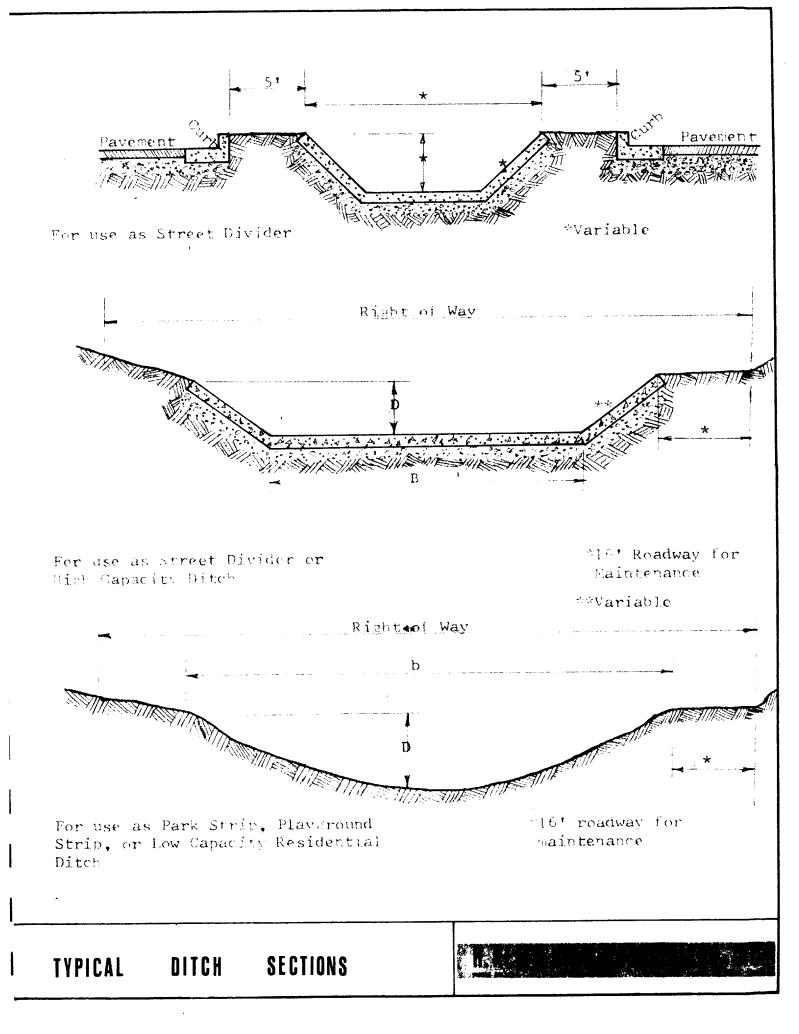


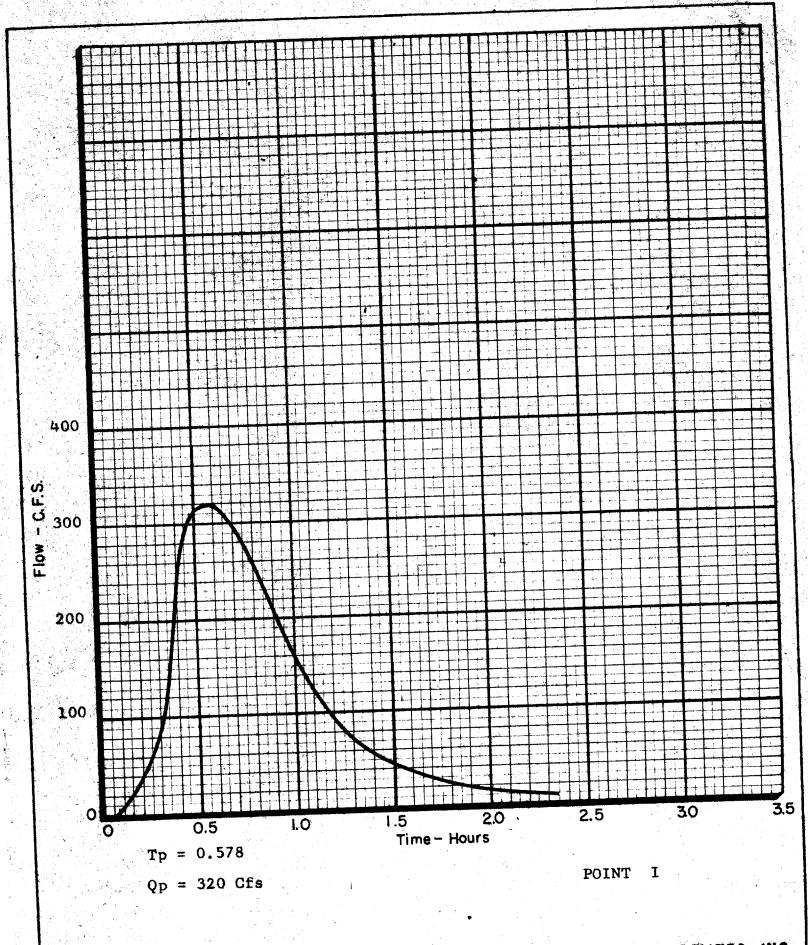


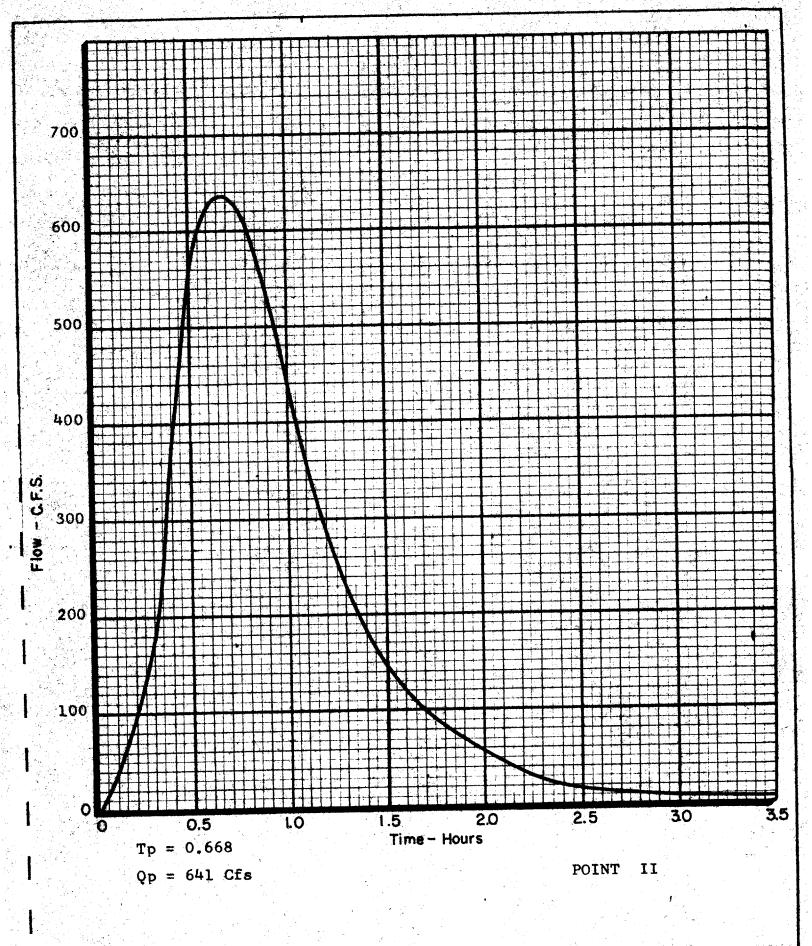


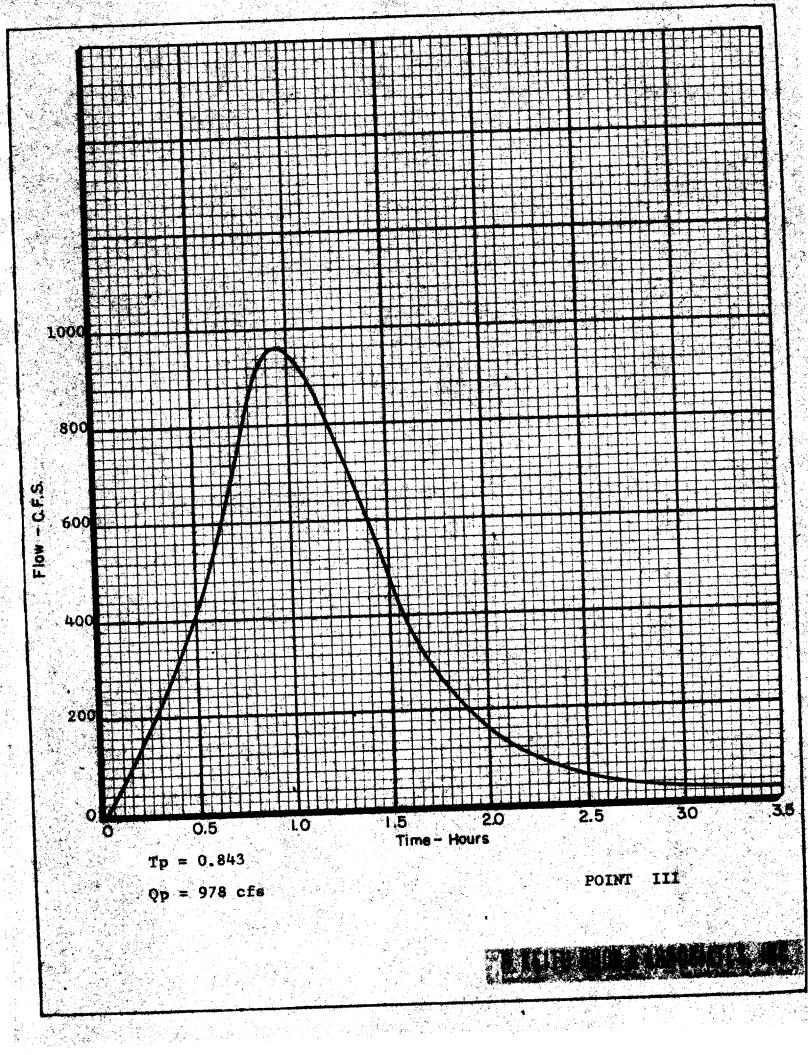


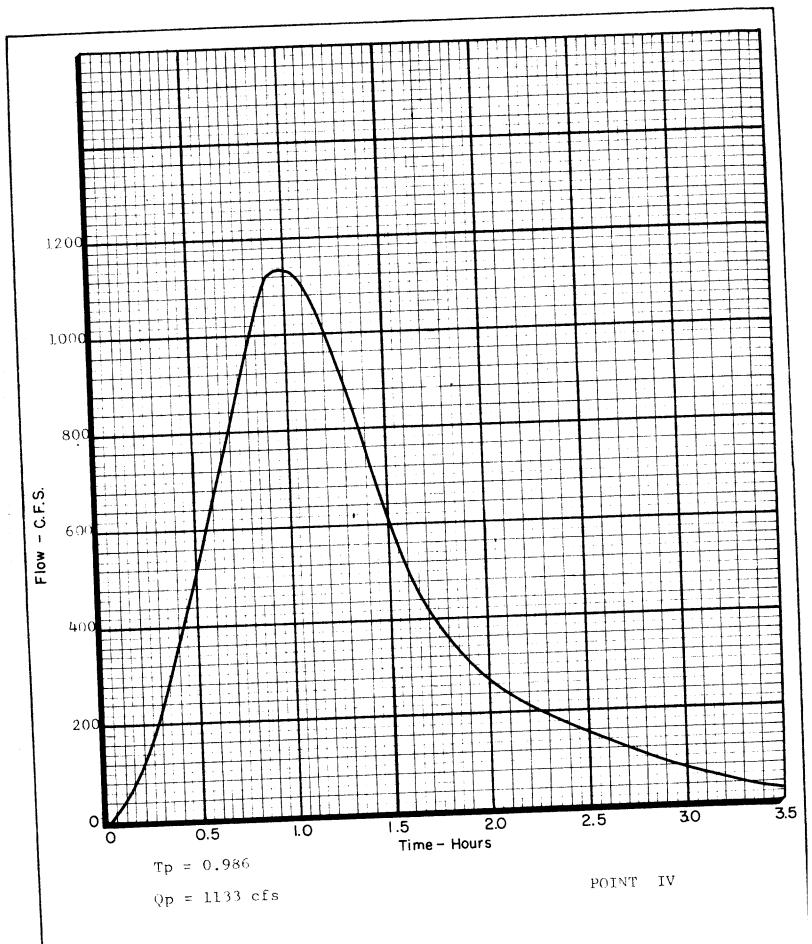


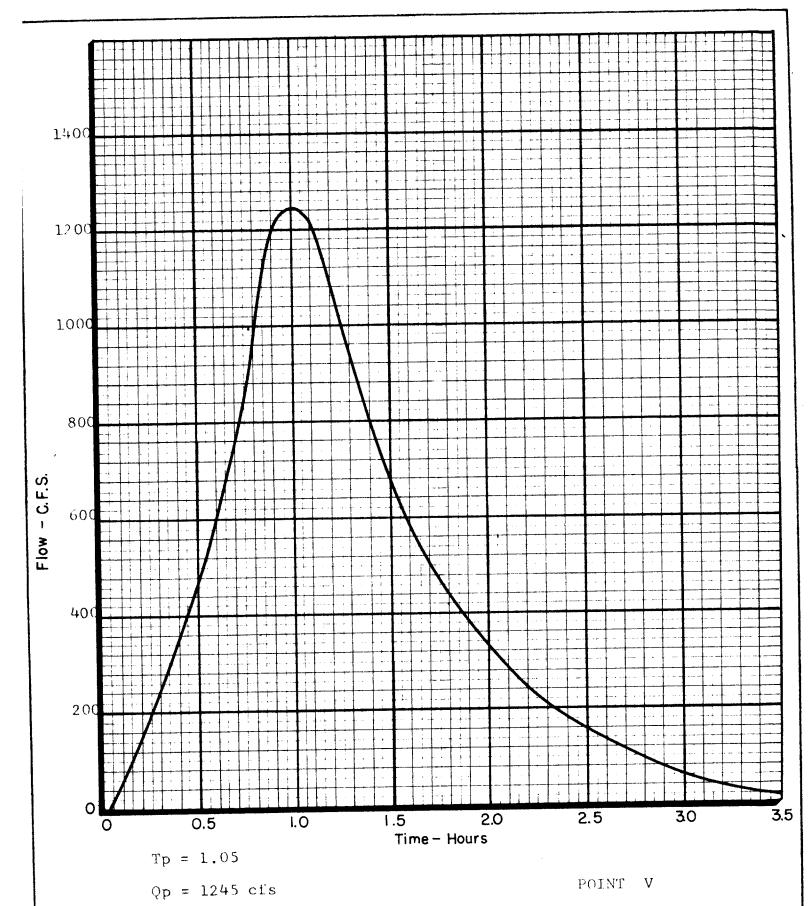


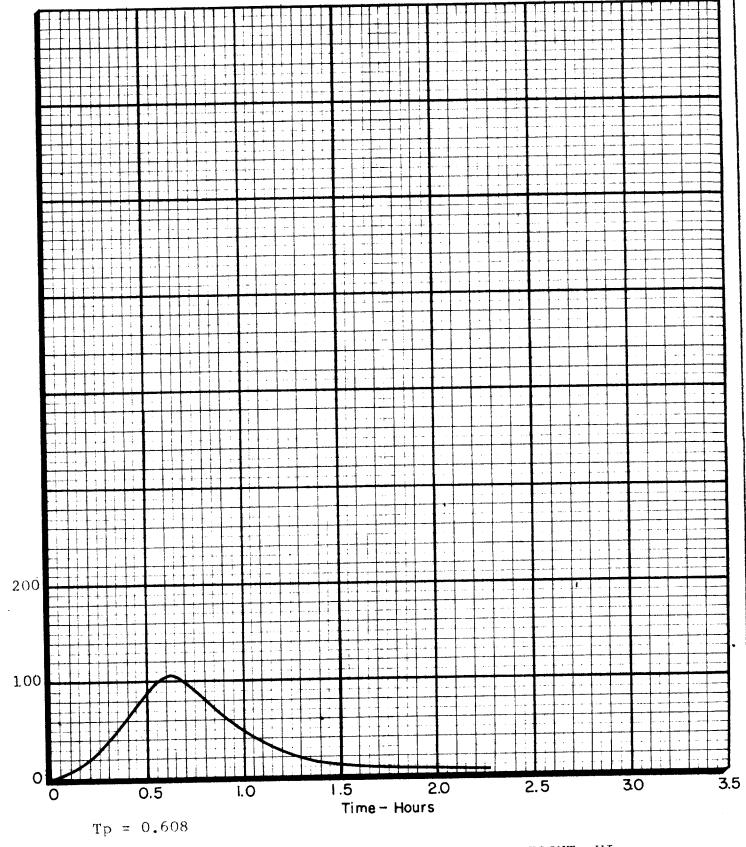






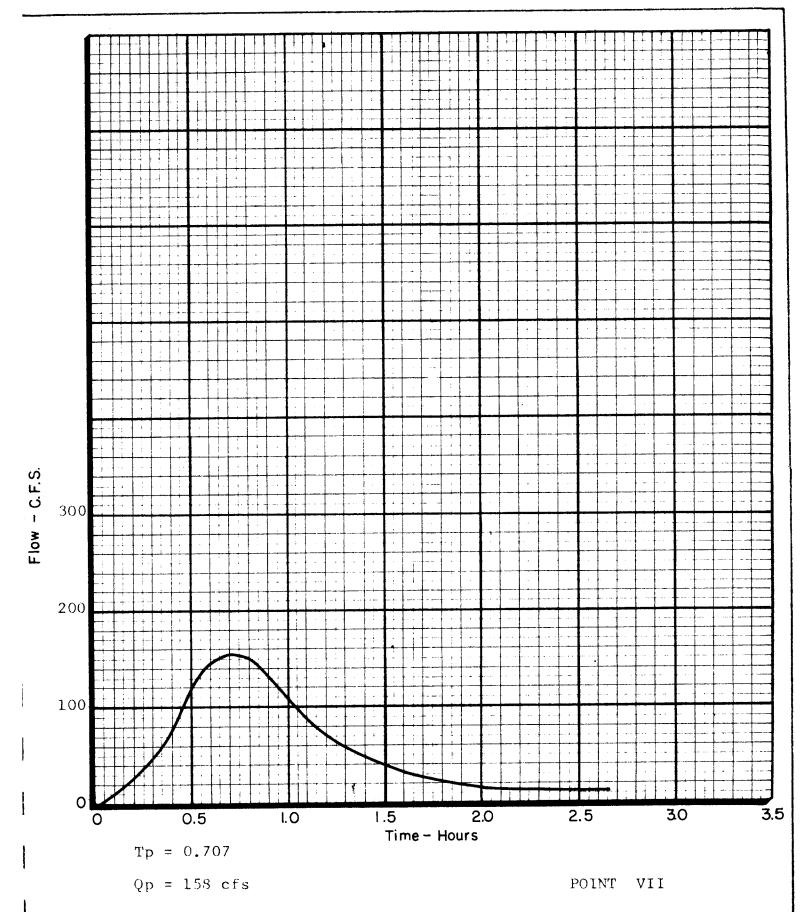






Qp = 105 cfs

VI POINT



## ESTIMATE OF COST

FOR THE

## DRY CREEK

## DRAINAGE BASIN (Cost in Place)

ITEM	DESCRIPTION	QUANTITY	UNIT	UNIT COST	AMOUNT
I.	STORM SEWER SYSTEM  (a) 24 "Plain concrete pipe (b) 36 "Plain Concrete Pipe (c) 40 "Plain Concrete Pipe (d) Headwall, Concrete  (Mesh Reinforced)  Total,	250	LF LF LF CY	10.00 17.00 22.00 40.00	800.00 4,250.00 7,920.00 960.00 \$13,930.00
II.	DRAINAGE DITCHES (Collector System) *1. DITCH NO. 1 W=4; D=3	: S=1.5:1			
	a. Shaping	3300	LF	0.30	990.00
	b. Erosion Control:  l. Riprap (grouted)  2. Concrete lined  3. Velocity Control  Check dam or ec		SY	5.00	5,000.00
	2. <u>DITCH NO. 2</u> W=3; D=3				0
	<ul><li>a. Shaping</li><li>b. Erosion Control:</li></ul>	5400	LF	0.15	810.00
	1. Riprap (grouted) 2. Concrete lined 3. Velocity Control Check dam or ec		SY	5.00	5,000.00
	3. <u>DITCH NO. 3</u> W=4; D=3 a. Shaping	3; S=1.5:1 6600	${ m LF}$	0.15	990.00
	b. Erosion Control: l. Riprap (grouted) 2. Concrete lined 3. Velocity Control		SY	5.00	7,500.00
	Check dam or ec	-			

4.	DITCH NO. 4 W=3; D=1.5; S=1	1 5.1			
4.	a. Shaping b. Erosion control:	200	LF	0.15	30.00
	1. Riprap (grouted) 2. Concrete lined 3. Velocity Control,	110	SY	5.00	550.00
	check dam or equal				
5.	DITCH NO. 5 W= 3; D=1.5; Sa. Shaping b. Erosion control:	=1.5:1 450	$\mathbf{LF}$	0.15	67.50
	1. Riprap (grouted) 2. Concrete lined 3. Velocity Control, check dam or equal	250 	SY	5.00	1,250.00
6.	DITCH NO. 6 W=3; D=1.5; S=1	1 5.1			
0.	a. Shaping b. Erosion Control:	450	LF	0.15	67.50
	1. Riprap (grouted) 2. Concrete lined 3. Velocity Control, check dam or equal	<b>2</b> 50 	SY	5.00	1,250.00
7.	DITCH NO. 7 W=3; D=1.5; S=	1.5:1 400	LF	0.15	60.00
	<ul><li>a. Shaping</li><li>b. Erosion Control:</li></ul>	400	TIL	0.17	00.00
	<ul><li>l. Riprap (grouted)</li><li>2. Concrete lined</li><li>3. Velocity Control,</li><li>check dam or equal</li></ul>	220	SY	5.00	1,100.00
8.	DITCH NO. 8 W=3; D=1.5; S=	1.5:1			
·	a. Shaping b. Erosion Control:	2400	LF	0.15	360.00
	<ol> <li>Riprap (grouted)</li> <li>Concrete lined</li> <li>Velocity Control, check dam or equal</li> </ol>	840	SY	5.00	4,200.00
	-				
9.	DITCH NO. 9 W=3; D=2; S=1. a. Shaping	5:1 1500	LF	0.20	300.00
	<ul><li>b. Erosion Control:</li><li>l. Riprap (grouted)</li><li>2. Concrete lined</li><li>3. Velocity Control,</li></ul>	400	SY	5.00	2,000.00
	check dam or equal				

10.	DITCH NO. 10 W=3; D=2; S=1.5:3 a. Shaping 1100	0.20	220.00
	b. Erosion Control: 1. Riprap (grouted) 400 2. Concrete lined 3. Velocity control, check dam or equal	5.00	2,000.00
11.	DITCH NO. 11 W=3; D=1.5; S=1.5  a. Shaping 400  b. Erosion Control:  1. Riprap (grouted)  2. Concrete lined  3. Velocity Control,  check dam or equal	0.15	60.00
12.	DTICH NO. 12 W=3; D=1.5; S=1.5  a. Shaping 200  b. Erosion Control:     1. Riprap (grouted)     2. Concrete lined     3. Velocity Control,     check dam or equal	0.15	30.00
13.	DITCH NO. 13 W=3; D=1.5; S=1.5  a. Shaping 250  b. Erosion Control:     1. Riprap (grouted)     2. Concrete lined     3. Velocity Control,     check dam or equal	0.15	37.50
14.	DITCH NO. 14 W=3; D=1.5; S=1.5  a. Shaping 250  b. Erosion Control:  1. Riprap (grouted)  2. Concrete lined  3. Velocity Control,  check dam or equal	0.15	37.50
15.	DITCH NO. 15 W=3; D=1.5; S=1.5  a. Shaping 80  b. Erosion Control:  1. Riprap (grouted)  2. Concrete lined  3. Velocity Control,  check dam'or equal	0.15	12.00

16. DITCH NO. 16 War a. Shaping b. Erosion Cont. 1. Riprap (g. 2. Concrete 3. Velocity	rol: routed) lined Control,	1.5:1	LF	0.15	45.00
17. DITCH NO. 17  a. Shaping  b. Erosion Cont.  l. Riprap (g. 2. Concrete  3. Velocity	rol: routed) lined	.5:1 280 	LF	0.15	42.00
18. DITCH NO. 18 W  a. Shaping  b. Erosion Com  1. Riprap (  2. Concrete  3. Velocity	trol: grouted) lined Control,	300 160 	LF SY	0.15 5.00	45.00 800.00
19. DITCH NO. 19 W  a. Shaping  b. Erosion Con  1. Riprap (  2. Concrete  3. Velocity	trol: grouted) lined	1.5:1 600	LF	0.15	90.00
check d	am or equal  Total, ITEM ch No. 1 not				<b>\$2</b> 8,954.00*
III. <u>DRAINAGE STRUCTURES</u>					
A. Box Culverts 10	ft.x 5.5 ft.	2	Ea. 40	00.00	8,000.00
B. Drainage Outlet		<b>2</b> 5	Ea. 2	00.00	5,000.00
C. Special intersect Design curb outl		3	Ea. 3	00.00	900.00
	Total, ITEM	NO. III.		• • • • •	\$13,900.00

IV.		ENBELT CONSTRUCTION				
	Α.	Earthwork and Re-alignme:		CV	0.30	3 000 00
		1. 60'ROW (4800 LF) 2. 70' ROW (10,000 LF)	10,000 35,000	CY	0.30 0.30	3,000.00 10,500.00
		3.100' ROW (5,000 LF)	20,000	CY	0.30	6,000.00
			•		_	·
	В.	± ± ` ,	0.000	O11	F 00	11 000 00
		1. 60 ROW (1600 LF) 2. 70' ROW (3,000 LF)	2,200 4,100	SY SY	5.00 5.00	11,000.00
		3.100' ROW (3,100 LF)	4,240	SY	5.00	21,200.00
			,		•	,
	C.	Concrete Lined or Equal	050	OT 7	(0.00	35 000 00
		1. 70' ROW (1,100 LF) 2. 100' ROW (1,000 LF)	<b>25</b> 0 🕍 <b>22</b> 0	CY CY	60.00 60.00	15,000.00 13,200.00
		2. 100 NOW (1,000 III)	220	O1	00.00	13,200.00
	D.	Velocity Control Check da	am 13	Ea.	L,000.00	13,000.00
		Total,	ITEM NO. IV.	• • • • •		\$113,400.00
٧.	BRI	DGES				
V.	$\frac{BRI}{A}$ .	100 sq.ft. opening,				
v.			3	<b>Ea.</b> (8	3,000.00	24,000.00
V.	Ā.	100 sq.ft. opening, L=80 ft. 2-(5'x5')	3	Ea. 8	3,000.00	24,000.00
V.		100 sq.ft. opening, L=80 ft. 2-(5'x5')	3 1		3,000.00	24,000.00 12,000.00
٧.	А. В.	100 sq.ft. opening, L=80 ft. 2-(5'x5') 162 sq.ft. opening, L=40 ft. 2-(6' x 5')	ep en Jahn jage ;		,	ŕ
V.	А. В.	100 sq.ft. opening, L=80 ft. 2-(5'x5') 162 sq.ft. opening, L=40 ft. 2-(6' x 5') Major Bridge,	1		,	ŕ
٧.	А. В.	100 sq.ft. opening, L=80 ft. 2-(5'x5')  162 sq.ft. opening, L=40 ft. 2-(6' x 5')  Major Bridge, Construction crossing Mon	l	Ea. 12	2,000.00	12,000.00
٧.	А. В.	100 sq.ft. opening, L=80 ft. 2-(5'x5') 162 sq.ft. opening, L=40 ft. 2-(6' x 5') Major Bridge,	1	Ea. 12	,	ŕ
V.	А. В.	100 sq.ft. opening, L=80 ft. 2-(5'x5')  162 sq.ft. opening, L=40 ft. 2-(6' x 5')  Major Bridge, Construction crossing Mon	l	Ea. 12	2,000.00	12,000.00
٧.	А. В.	100 sq.ft. opening, L=80 ft. 2-(5'x5')  162 sq.ft. opening, L=40 ft. 2-(6' x 5')  Major Bridge, Construction crossing Mon	1 nument 1	Ea. 12	2,000.00	12,000.00
V.	А. В.	100 sq.ft. opening, L=80 ft. 2-(5'x5')  162 sq.ft. opening, L=40 ft. 2-(6' x 5')  Major Bridge, Construction crossing Mor Creek  Total,	1 nument 1	Ea. 12	2,000.00	12,000.00

TOTAL LAND AREA - 2,494 Acres
Less National Forest
Area -747 Acres

\*\*Less Mt. Francis
Property -820 Acres

NET ACREAGE SUBJECT TO DRAINAGE COST 927 Acres \$406,184.00 - \$438.17 per Acre

