

**AMENDMENT NO. 4
PINE CREEK DRAINAGE BASIN
PLANNING STUDY AND
MASTER DEVELOPMENT DRAINAGE PLAN
FOR PINE CREEK SUBDIVISION
(Retrofit of Pine Creek Regional Detention Facility “C”
Part of Briargate Parkway Plaza Filing No. 1 (Track A))**

In conjunction with:

**Powers Boulevard Bridges Project
Briargate, Union, Pine Creek**

February xx, 2012

Prepared for:

**Colorado Department of Transportation
Region 2, Colorado Springs Residency**

Prepared by:



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ENGINEERS STATEMENT:


The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability on my part in preparing this report.


George K. Cotton, Colorado
Colorado PE 19501
For and On Behalf of Tsiouvaras Simmons Holderness, Inc.



2/28/2012
Date

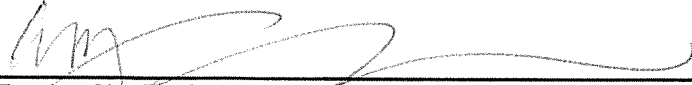
COLORADO DEPARTMENT OF TRANSPORTATION
REGION 2, COLORADO SPRINGS RESIDENCY


Resident Engineer

2/23/12
Date

CITY OF COLORADO SPRINGS:

Filed in accordance with Section 7-7-906 of the Code of the City of Colorado Springs, 2001, as amended


For the City Engineer

2/28/12
Date

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I. INTRODUCTION

CDOT is completing the segment of Powers Boulevard between Pine Creek and Briargate Parkway. The construction will complete the mainline bridges over Pine Creek, Union Boulevard and Briargate Parkway; and will pave the mainline. Within CDOT right-of-way limits, the stormwater runoff will be treated in accordance with CDOT and City of Colorado Springs MS4 permits. New permanent stormwater quality facilities (PSQF) will be constructed near Pine Creek and an existing PSQF will treat stormwater runoff for the segment of Powers Boulevard from Union Boulevard to Pine Creek.

Stormwater runoff from Powers Boulevard that is tributary to the Briargate Parkway drainage system currently has no PSQF. CDOT's project requirements allowed for retrofit of Regional Detention Facility "C" (RDF-C) in accordance with an agreement with the City of Colorado Springs. The other option permitted by CDOT design requirements was for construction of a PSQF within Powers Boulevard right-of-way. Because of the difficulty of siting a large volume PSQF within the project, the design-build team of Edward Kramer & Sons (build) and Tsiouvaras Simmons Holderness (design) chose the RDF-C retrofit approach.

This report presents the basis of the retrofit design of the primary outlet for RDF-C. The purpose of the retrofit is to provide regional treatment for all stormwater runoff that is tributary to the facility, which includes runoff from Powers Boulevard to the Briargate Parkway storm drainage system.

II. GENERAL LOCATION AND DESCRIPTION

Regional Detention Facility "C" is located in the northwest quadrant of the intersection of Union Boulevard and Briargate Parkway (see Exhibit 1). The primary outlet for the detention pond is located in the southwest corner. Geodetic coordinates for the outlet are approximately 38°57'59"N and 104°45'37"W.

RDF-C was constructed as a component of the Master Development Drainage Plan for the Pine Creek Subdivision. RDF-C is within the South Fork branch of Pine Creek and is one of four regional detention facilities constructed within that tributary. All of the inflows to RDF-C are conveyed to the basin via closed conduits. The largest inflows to the pond are from the Pine Creek South storm drainage system. This system has two large

inlets to RDF-C: one from Briargate that enters at the southeast corner into the pond forebay, and one from Union along the east side of the pond. There are also two inlets to the pond for local drainage systems that drain areas that are the north of the pond.

While no natural drainageways enter RDF-C, there is a jurisdictional wetland within the pond. When the pond was constructed, a constructed wetland was located along the south side of the pond as mitigation for wetland losses due to development. The wetland is fed by discharges from the pond forebay. Since construction of the pond, additional wetlands have established beyond the limits of the original mitigation area. Other wetlands that now exist in the pond include the area around the pond outlet. These wetlands are below elevation 6870.0, which is the berm height for the constructed wetland. Several wetlands have also formed on the perimeter of the pond where pond excavation intercepted groundwater seeps. Seeps can be observed on the north and east sides of the ponds. Groundwater seeps are not found in the vicinity of the pond outlet. It has been assumed that the entire work area near the pond outlet that is below elevation 6870.0 is jurisdictional wetland. The project has applied for a nationwide permit for work within wetland areas for project (see Appendix for a copy of the permit application).

III. DRAINAGE BASINS AND SUB-BASINS

RDF-C is a component of the drainage system for Pine Creek South Fork. The fully developed hydrology of this drainage basin is described in detail in the "Pine Creek Drainage Basin Planning Study" (JR Engineering, 1998). The watershed has 13 sub-basins of which 10 are tributary to RDF-C. The total drainage area to RDF-C is 1.04 square miles (664 acres) and has a weighted impervious area of 67.6%. The Powers Boulevard drainage basins that drain to Pine Creek South Fork have an area of 43.4 acres with an impervious percentage of 55%.

Sub-basin data is summarized in the appendix of this report (Hydrologic Input Calculations).

IV. DRAINAGE DESIGN CRITERIA

RDF-C is a non-jurisdictional detention dam that is currently privately owned by LP47, LLC and maintained and managed by the City of Colorado Springs. Design of the RDF-C water quality retrofit will conform to criteria of the City of Colorado Springs as stated in City of Colorado Springs “Drainage Criteria Manual” (DCM), Volumes 1, 2 and addenda. Specific sections of the DCM that are relevant to the detention facility retrofit design include Volume 1 Section 6.6 “Detention Storage Criteria” and Chapter 11 “Detention Storage”. Criteria for starting water surface elevations for extended detention basins are given in Volume 2 on page 4-22.

V. DRAINAGE FACILITY DESIGN

A. General Concept

The existing primary outlet for detention basin RDF-C will be modified to include a water quality outlet with a 40 hour drain time. The existing primary outlet consists of a 48-inch diameter reinforced concrete pipe that is supported by a standard headwall. To prevent debris from entering the pipe, the headwall has a sloping trash rack that is supported by the headwall and apron.

The new outlet design will raise the height of the headwall and wing-walls to a constant elevation. The elevation will be set to the stage in the RDF-C basin for the water quality capture volume (WQCV) plus 20% for accumulated sediment storage (i.e. design water quality volume).

The WQCV will be released through an orifice plate that is designed to drain that volume in 40 hours. The orifice plate will be placed on the front wall of the raised outlet headwall opposite the 48” outlet pipe. To prevent debris from clogging the orifice openings, a screen will be placed in front of the orifice plate. As a part of the screen design, a 2.5 foot deep micro-pool will be constructed to maintain a permanent pool of water in front of the screen, assuring that the lower portion of the screen will be free of floating debris. The micro-pool will be a square concrete sump that has side lengths equal to the existing headwall width of 8’-0”. An additional fence-like screen will be placed along the perimeter of the micro-

pool for the purposed of collecting larger debris and limiting access to the micro-pool except by authorized maintenance personnel.

During regular rainfall conditions, stormwater will pool against the headwall up to the elevation of the design water quality volume and gradually release. A water quality volume of 12.46 ac-ft is calculated for the total watershed area of 658.4 acres (1.03 sq. mi.) and 57.2% imperviousness. The design height of the raised headwalls will be 6'-5". From the base of the micro-pool, the structure will be 8'-11" high.

During storm rainfall conditions, stormwater will pool to the height of the headwall and begin spilling to the 48" outlet pipe. Initially, the headwall will act as a weir and will control the rate that water is released from the pond. However, once the flow increases, the release from the pond will be controlled by the outlet pipe.

Our analysis found that the outlet pipe runs in "inlet" control and that there is extra capacity in the Pine Creek South storm drain. We looked at the option of improving the headwall efficiency by adding a bevel around the outlet pipe (i.e. changing from an HDS Chart 1 outlet to an HDS Chart 3 outlet). This improvement would increase the outlet release from RDF-C by 12 to 14 percent and could partially make up for the initial period, when stormwater fills the WQCV and releases from the retrofit outlet are low. Analysis of this option however showed only minor overall improvement. Pond stage for the 100-year storm only decreased 0.1 foot and peak outflow by about 5.1 cfs (see Appendix, Hydrologic Model Output). This is well within the modeling error and so was not deemed to be a valid option.

To prevent debris from entering the outlet pipe, a sloping trash rack will be installed on top of the headwall. A prefabricated, tented rack was selected with raised sides and 60% open area that will be bolted to the outlet structure.

A new maintenance access road will be constructed from the existing access road near the forebay spillway along the toe slope (above the elevation of the wetland) to the micro-pool. The access road will be 10 feet wide on a level grade

The access road will be surfaced with a 6 inch depth of aggregate base course (CDOT Class 6 material) to stabilize the road.

It was found that even with improvements to the detention basin primary outlet that it will be necessary to increase the storage volume within the detention basin. The existing pond has a volume of 68.9 ac-ft at the spillway crest. Routing (using the HEC-HMS model) through the existing pond for the 100-year storm requires a volume of 72.8 ac-ft, which is equivalent to stage of 6882.1 (0.6 feet above the existing emergency spillway crest). [Note: The flood routing for Addendums No. 2 and No. 3 was accomplished using the older hydrologic analysis program, HEC-1 (USACE, 1990). In this computer program the routing time step is set manually. The hydrologic analysis for the current retrofit design used HEC-HMS, which has replaced HEC-1. In HEC-HMS, the computational time step is computed by the program to meet all tolerances. Addendum No. 2 used a 3.0 minute time step, while HEC-HMS finds this time step to be too long and computed a shorter time step of about 2.0 minutes. The shorter time step results in a more accurate routing computation and a larger volume of runoff stored in the pond. We estimate that continuity error in the original computation to be about 2.8% of the total inflow to the pond (209.3 ac-ft) based on the HEC-HMS analysis. This is a theoretical error and within the operational uncertainty of the detention pond.]

Routing of the 100-year storm with the primary outlet modified for water quality (with an initial stage corresponding to 0.5 WQCV) requires 81.3 ac-ft of flood storage. Raising the spillway approximately 1.5 feet provides 78.8 ac-ft of storage volume. The maximum 100-year stage is 6883.3 or 0.3 feet above the spillway elevation. In theory, this will result in a spill of 85 cfs over the spillway (similar to the estimated 84 cfs spill from the existing pond). The spill would be brief, lasting 36 minutes and releasing 3.3 ac-ft.

To accomplish the spillway raise, the existing concrete cutoff wall will be extended over a length of 190 feet by 1'-6". The existing riprap protection will be removed and approximately 380 cubic yards of embankment added to the spillway. The riprap protection will then be replaced to match the new elevation

of the cutoff wall. The raised spillway will be 3 feet below the elevation of the basin embankment. If the primary outlet were totally plugged, our analysis shows that the 100-year storm flow could pass over the spillway with 2 feet of freeboard.

B. Specific Details

Design exhibits for the RDF-C water quality retrofit are provided in the Appendix of this report. The design is presented on four plan sheets, which are part of the plan set for the Powers Boulevard Bridges Project. Sheet 181 shows the planned grading for the pond access road. The design shows regrading of the existing access road to the forebay with the new access road extending west along the south perimeter of the pond to the outlet. The detail for extending the existing emergency spillway cutoff wall is also shown on this sheet.

Sheet 182 shows the plan and elevation of the modified outlet. A work pad is provided at the outlet on the east side. To accommodate the embankment slope of the work pad at the micro-pool, the east wall of the micro-pool is extended and sloped to match the embankment slope of the pad. Other components of the outlet shown on this sheet include: the location of the orifice plate and water quality screen, the over flow trash rack, and a perimeter fence around the micro-pool. The perimeter of the micro-pool is fenced with a standard 6' high chain link fence. Access to the micro-pool is provided by a gate on the west side. A two foot concrete walkway around the perimeter of the micro-pool will provide a firm footing for removing debris from the perimeter fence.

Sheet 183 shows reinforcement and related structural details for the vault modifications and new micro-pool.

Sheet 184 shows fabrication details for the orifice plate and trash racks. The orifice plate will be mounted on the exterior of the outlet vault and surrounded by bar-grate trash rack. In accordance with UDFCD recommendations for a trash rack of this size, Amico-Klempt grade model 19-W-4 with 4" cross bar spacing is specified. The grate is configured to provide a vertical orientation of the bars, which facilitates cleaning. Access to the orifice plate is accomplished by

unbolting the bar grate from its vertical supports. A prefabricated overflow trash rack is specified. The Storm Rax structure is distributed by Contech and is manufactured with structural plastic (see product information in the Appendix).

C. Grading and Erosion Control

It is estimated that the retrofit construction will disturb 0.34 acres and require the placement of approximately 380 cubic yards of fill. Construction erosion control BMPs will be implemented at the site. A grading and erosion control permit will be obtained from the City of Colorado Springs for the retrofit.

D. Other Government Agency Requirements

The primary outlet for RDF-C is adjacent to a jurisdictional wetland. The area near the outlet will be disturbed in order to construct the retrofit. A Nationwide Permit No 43 Section 404 permit has been obtained for construction work in this wetland area from the U.S. Army Corps of Engineers (see Appendix: Letter from Van Truan to George Cotton, February 1, 2012).

VI. DRAINAGE FACILITY MAINTENANCE

CDOT and the City of Colorado Springs have agreed to jointly develop a maintenance plan for the outlet structure (see Appendix: Letter from Robin Kidder to Mark Andrew, February 11, 2011).

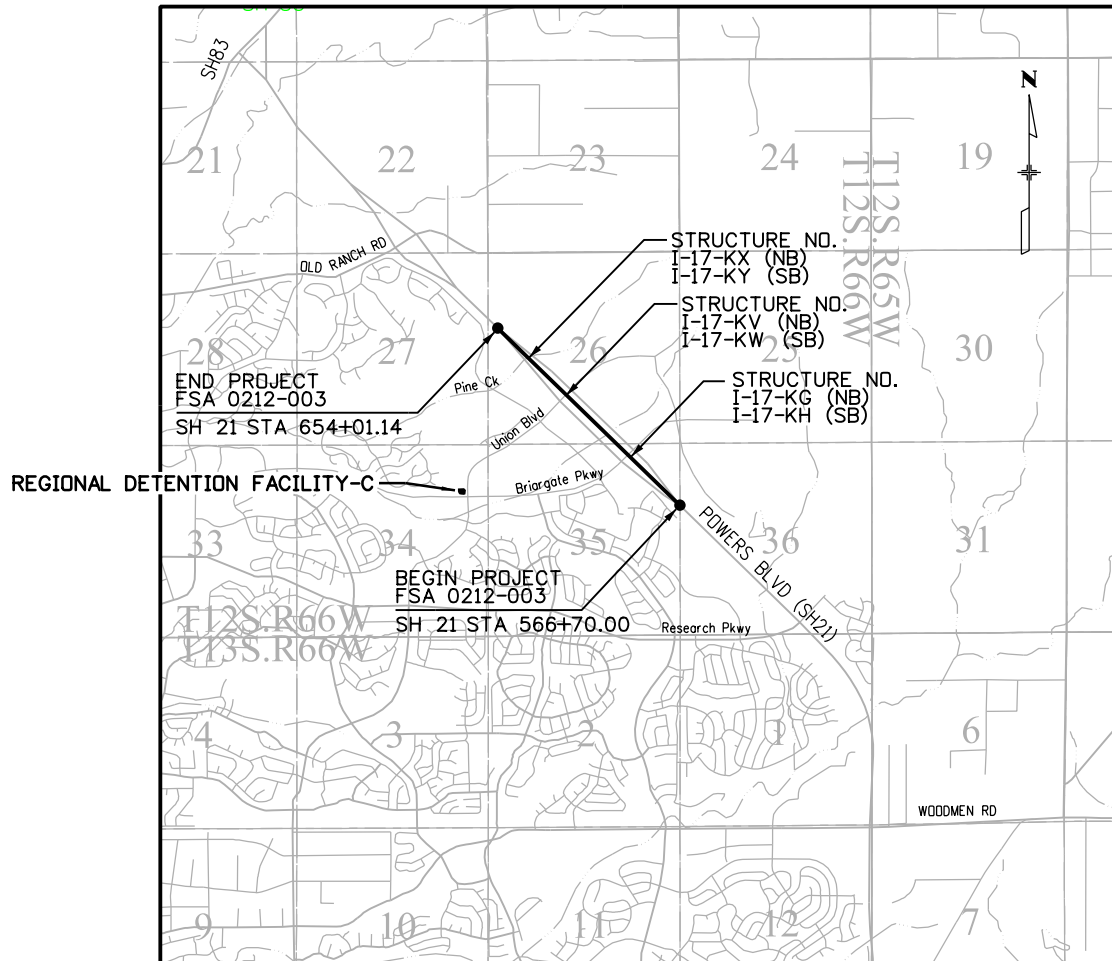
VII. REFERENCES

1. City of Colorado Springs / County of El Paso, 1991, "Drainage Criteria Manual"
2. JR Engineering, 1998, "Amendment No. 2 to Pine Creek Drainage Basin Planning Study and Master Development Drainage Plan for Pine Creek Subdivision (portion contributing to Pine Creek)", prepared for LP47, LLC
3. JR Engineering, 2002, "Amendment No. 3 to Pine Creek Drainage Basin Planning Study and Master Development Drainage Plan for Pine Creek Subdivision (portion contributing to Pine Creek)", prepared for LP47, LLC
4. Urban Drainage and Flood Control District, 2011, "Urban Storm Drainage Criteria Manual – Volume 3" Section T-5, Extended Detention Basin (EDB) and Section T-12, Outlet Structures
5. Urban Drainage and Flood Control District, 2011, "UD-BMP Workbook" version 3.01
6. USACE, Hydrologic Engineering Center, 2000, "Hydrologic Modeling System, HEC-HMS, Technical Reference Manual"
7. USACE, Hydrologic Engineering Center, 1990, "HEC-1, Flood Hydrographic Package User's Manual"

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PROJECT LOCATION MAP

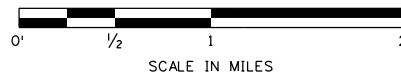




Photo 1. Looking west from main inlet culvert to RDF-C showing existing constructed wetland along south side of pond (left edge of pond bottom). Pond forebay is in foreground below culvert apron. Outlet is in the distance in the southwest corner (top left area of photo).



Photo2. Existing pond outlet with steel trash rack. Outlet consists of a 48" RCP with headwall and wingwalls. Constructed wetland is in the background and new wetland has established near the pond outlet.



	<p>POWERS BOULEVARD</p>	<p>EXHIBIT 2</p>
	<p>RDF-C SITE PHOTOS</p>	

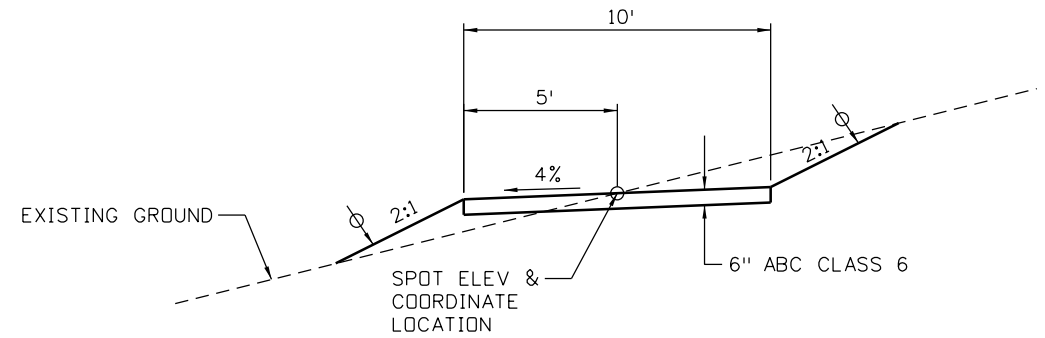


Photo 3. Looking east from RDF-C pond embankment showing existing constructed wetland along south side of pond (right half of pond bottom). Additional wetlands have established at other culvert inlets and groundwater seep points along the pond perimeter.

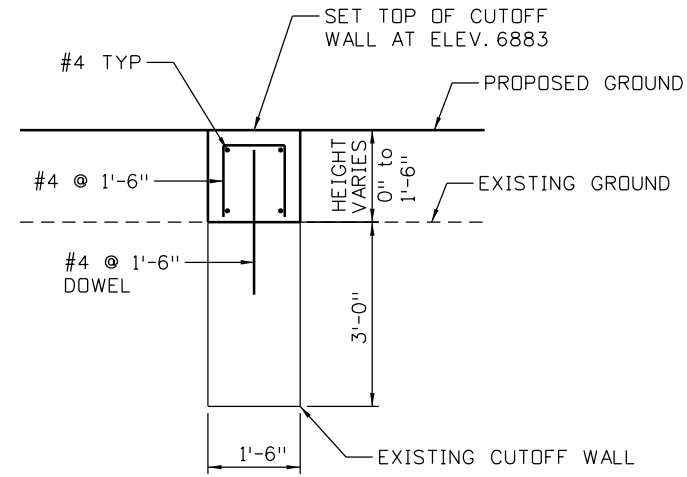


Photo 4. Looking south to pond outlet and spillway (highlighted in yellow) from RDF-C pond embankment.

	<p>POWERS BOULEVARD</p>	<p>EXHIBIT 2</p>
	<p>RDF-C SITE PHOTOS</p>	

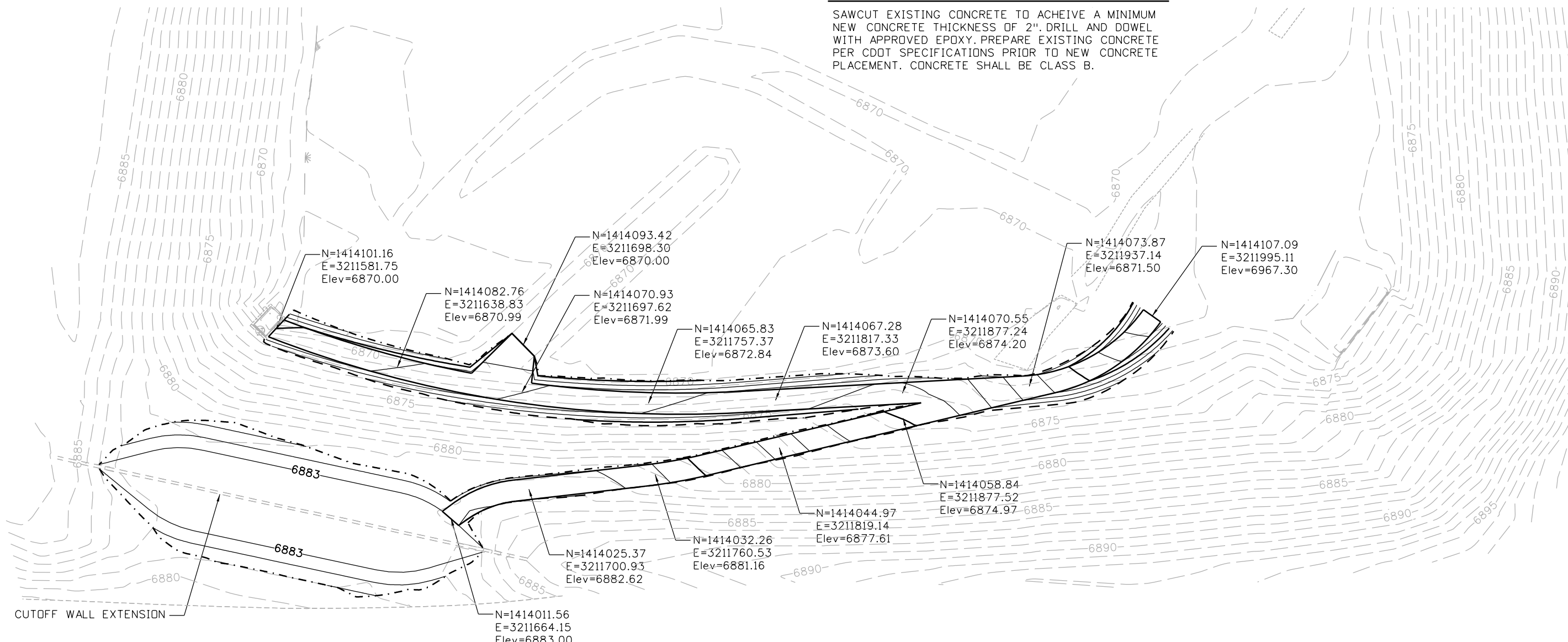


ACCESS ROAD TYPICAL SECTION



EXTENSION TO EXISTING CUTOFF WALL

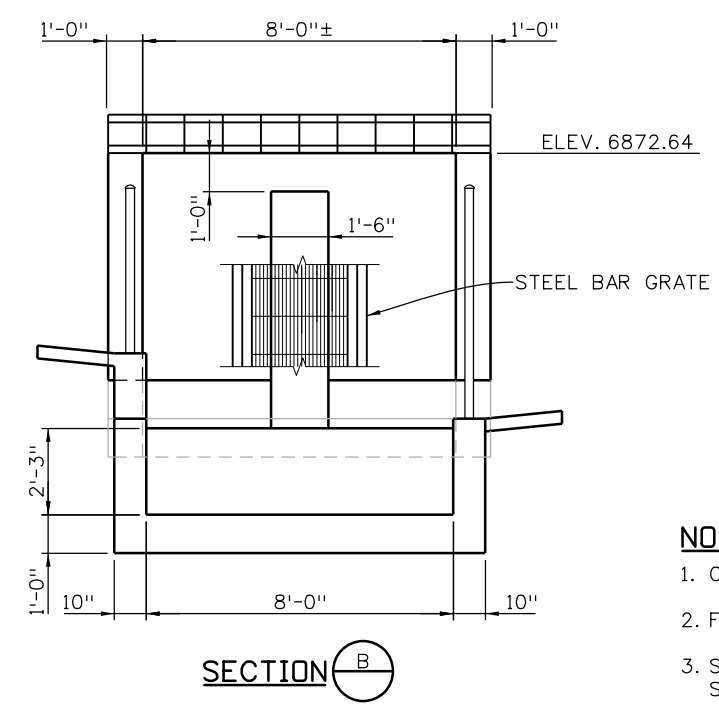
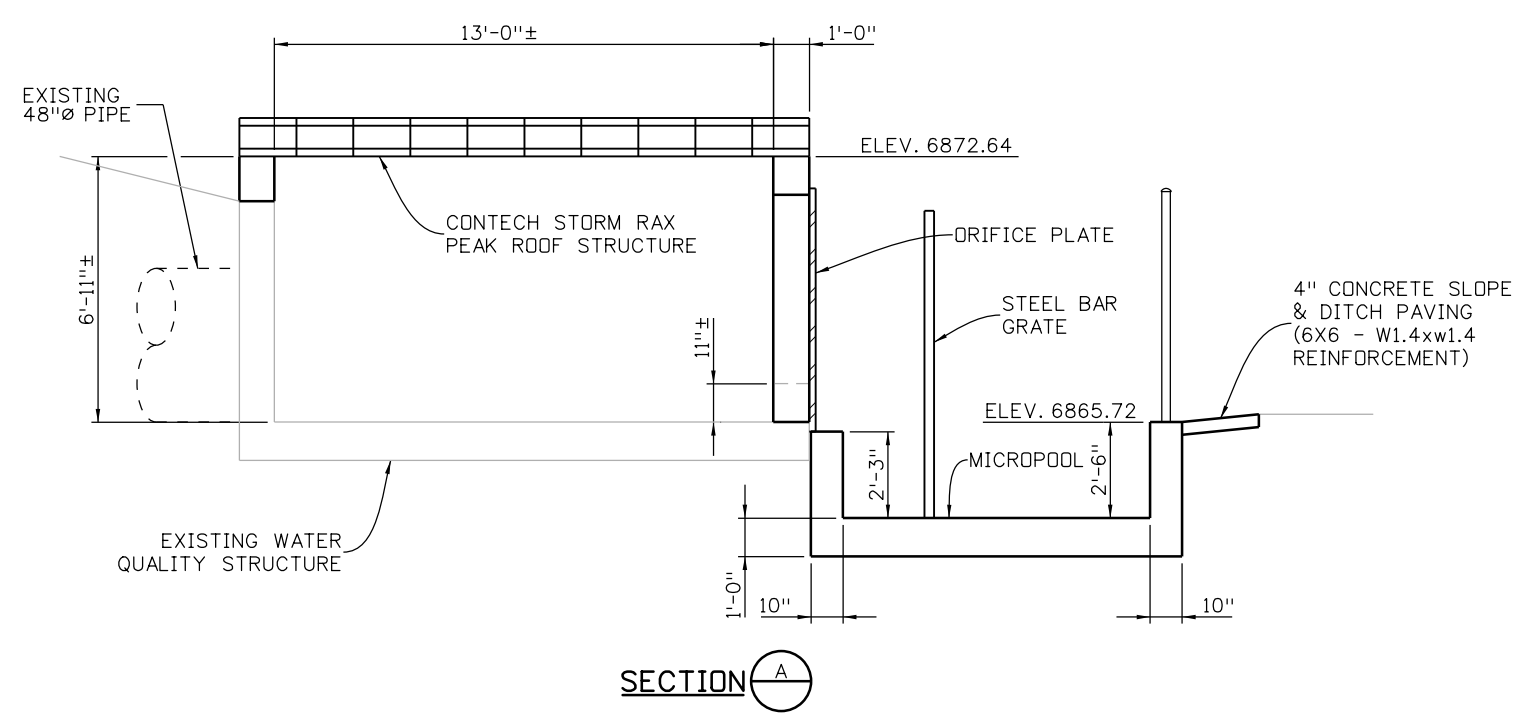
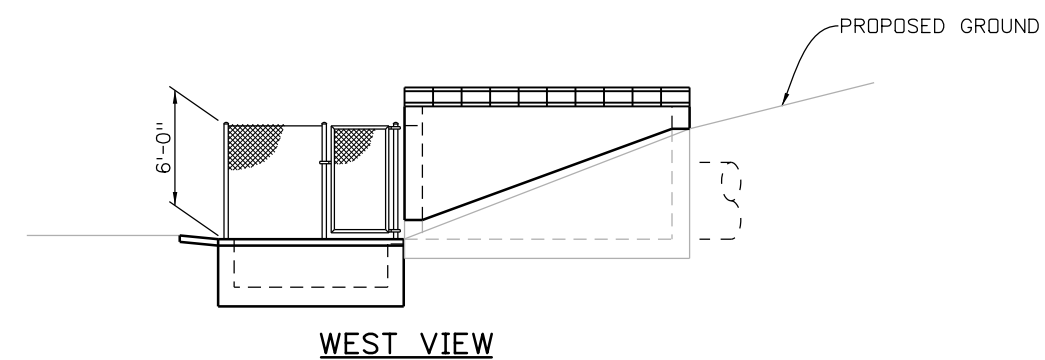
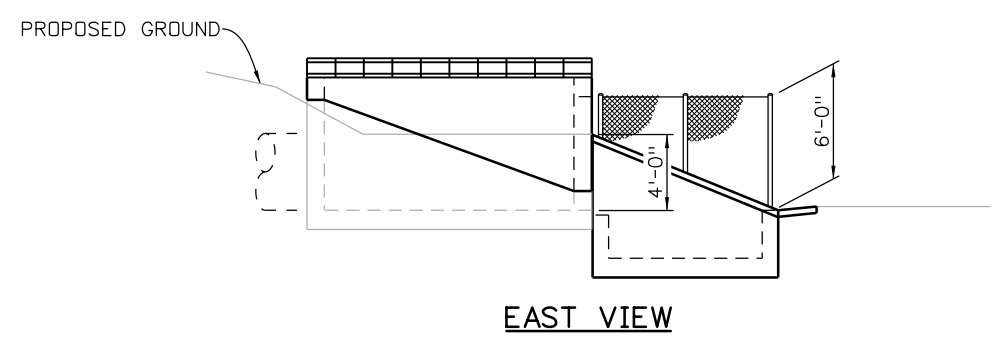
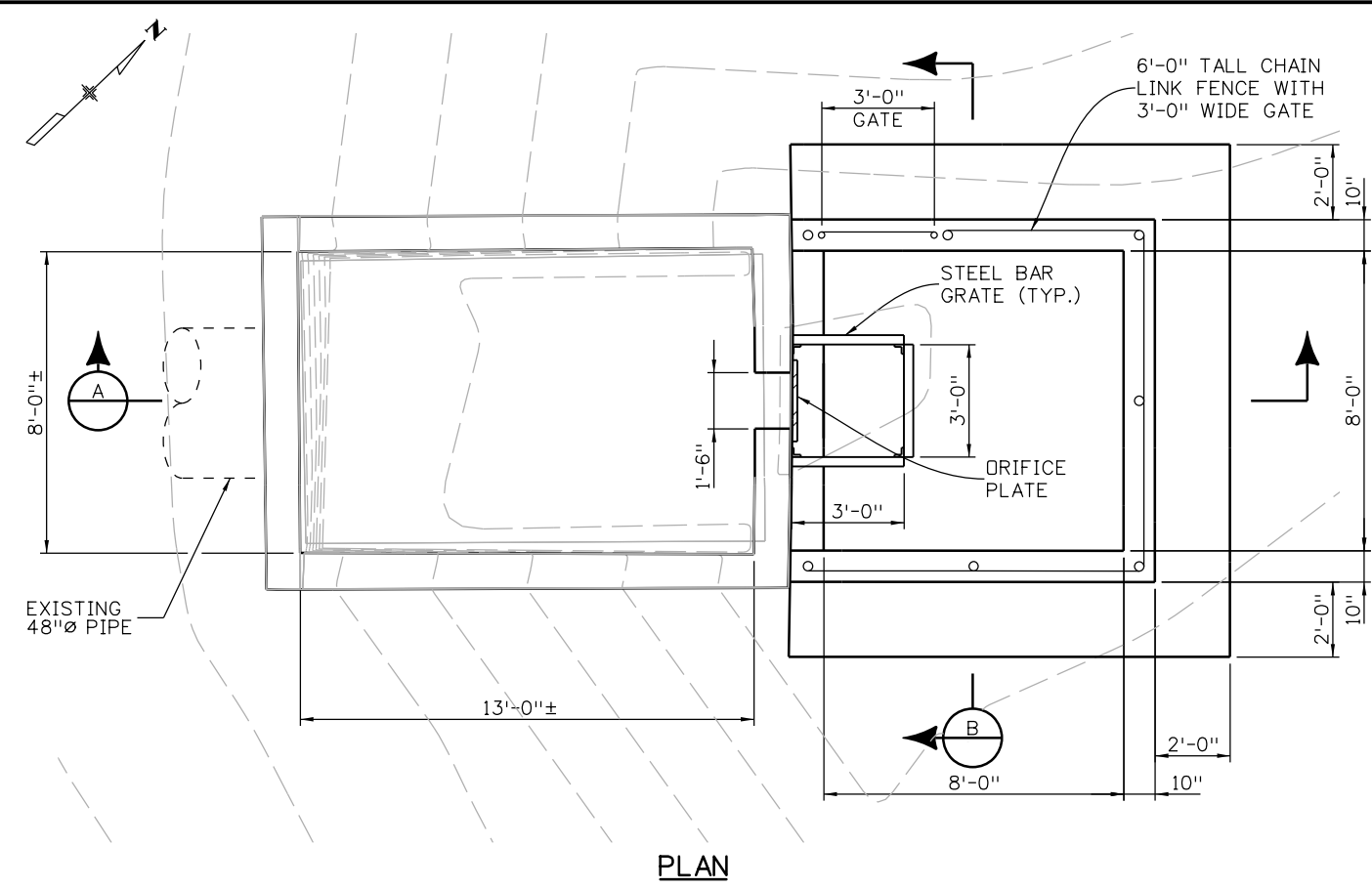
SAWCUT EXISTING CONCRETE TO ACHIEVE A MINIMUM NEW CONCRETE THICKNESS OF 2". DRILL AND DOWEL WITH APPROVED EPOXY. PREPARE EXISTING CONCRETE PER CDDT SPECIFICATIONS PRIOR TO NEW CONCRETE PLACEMENT. CONCRETE SHALL BE CLASS B.



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90% REVIEW JANUARY 2012



- NOTES:**
1. CONCRETE SHALL BE CLASS B.
 2. FENCE SHALL BE PER CDOT M-607-2.
 3. SEE NEXT RETROFIT 2 AND RETROFIT 3 SHEETS FOR REINFORCING AND DETAILS.

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Colorado Department of Transportation

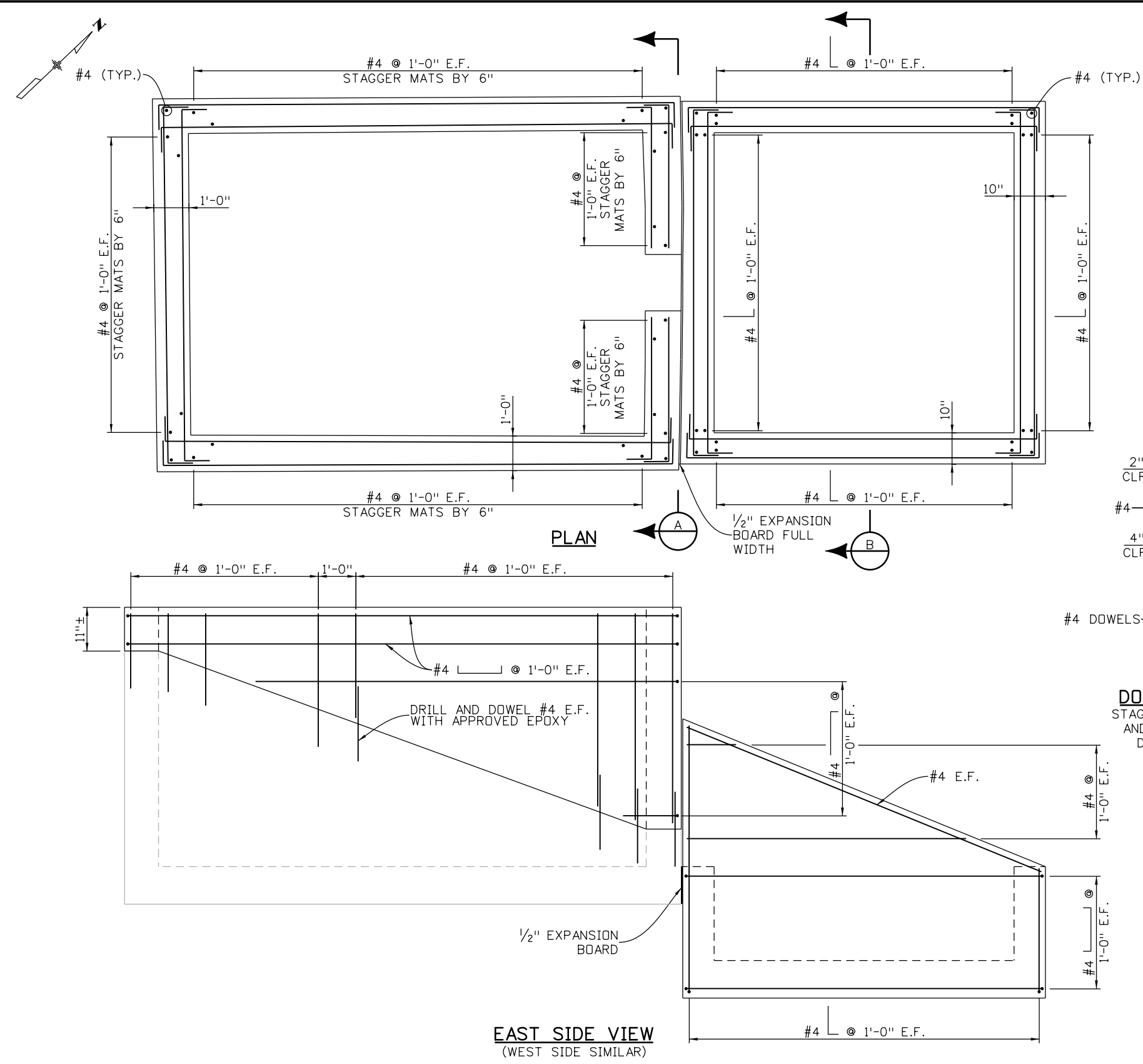
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Region 2 **MSA**

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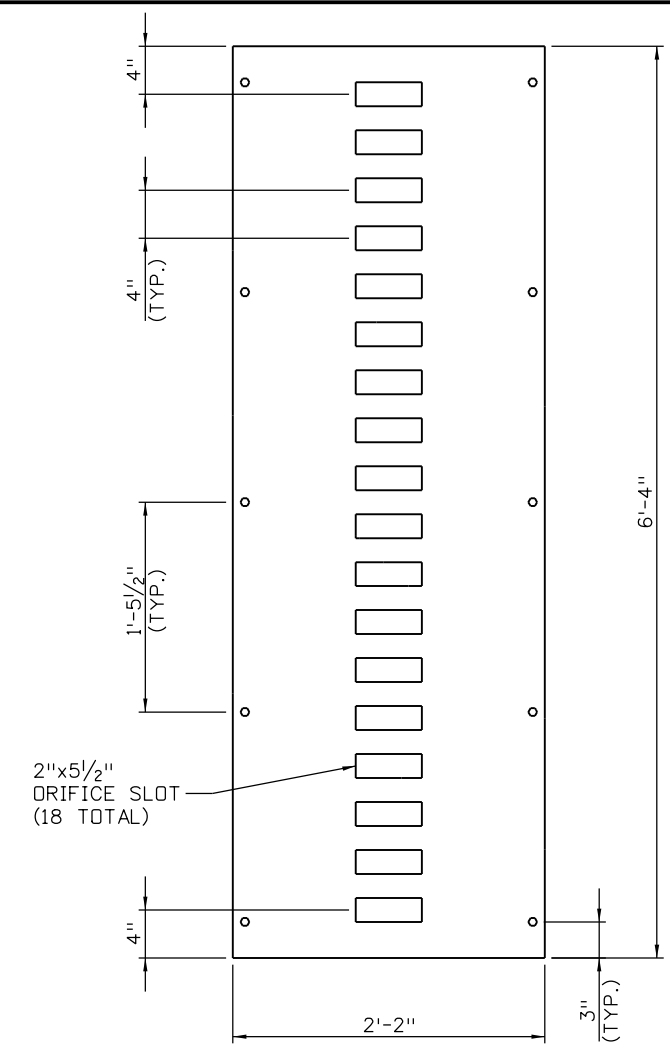


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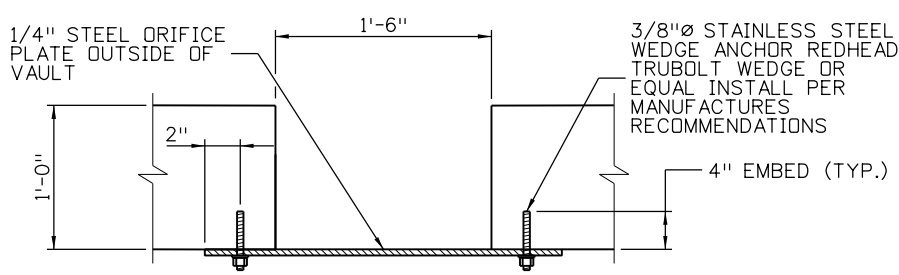
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2. PREPARE EXISTING CONCRETE PER CDOT SPECIFICATIONS PRIOR TO NEW CONCRETE PLACEMENT.
3. ALL REINFORCING TO BE GRADE 60.

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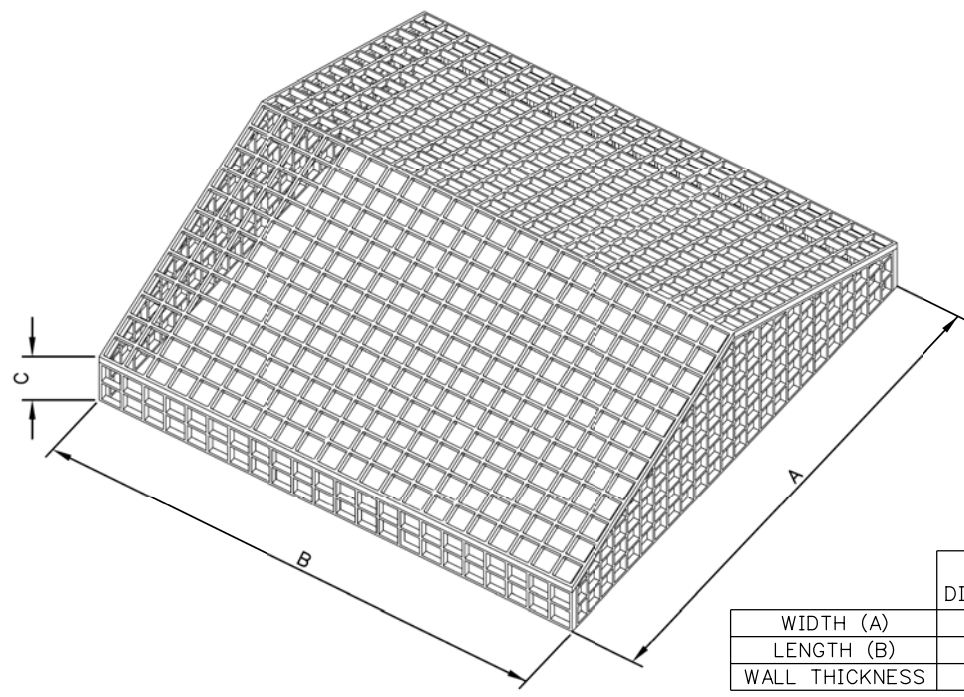
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ORIFICE PLATE DETAIL
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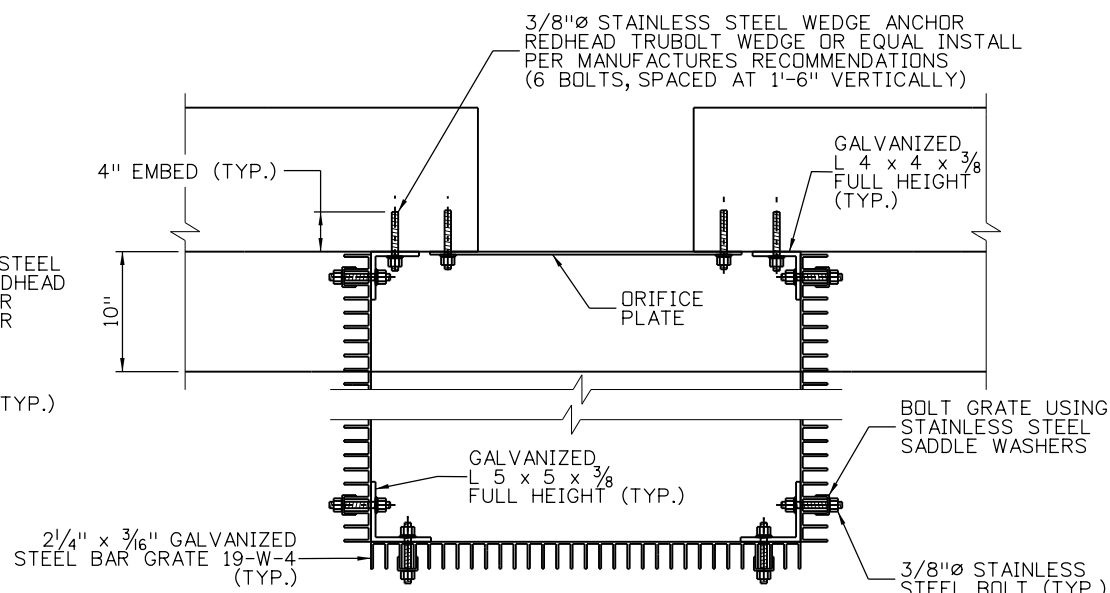


SECTION B ORIFICE PLATE DETAIL
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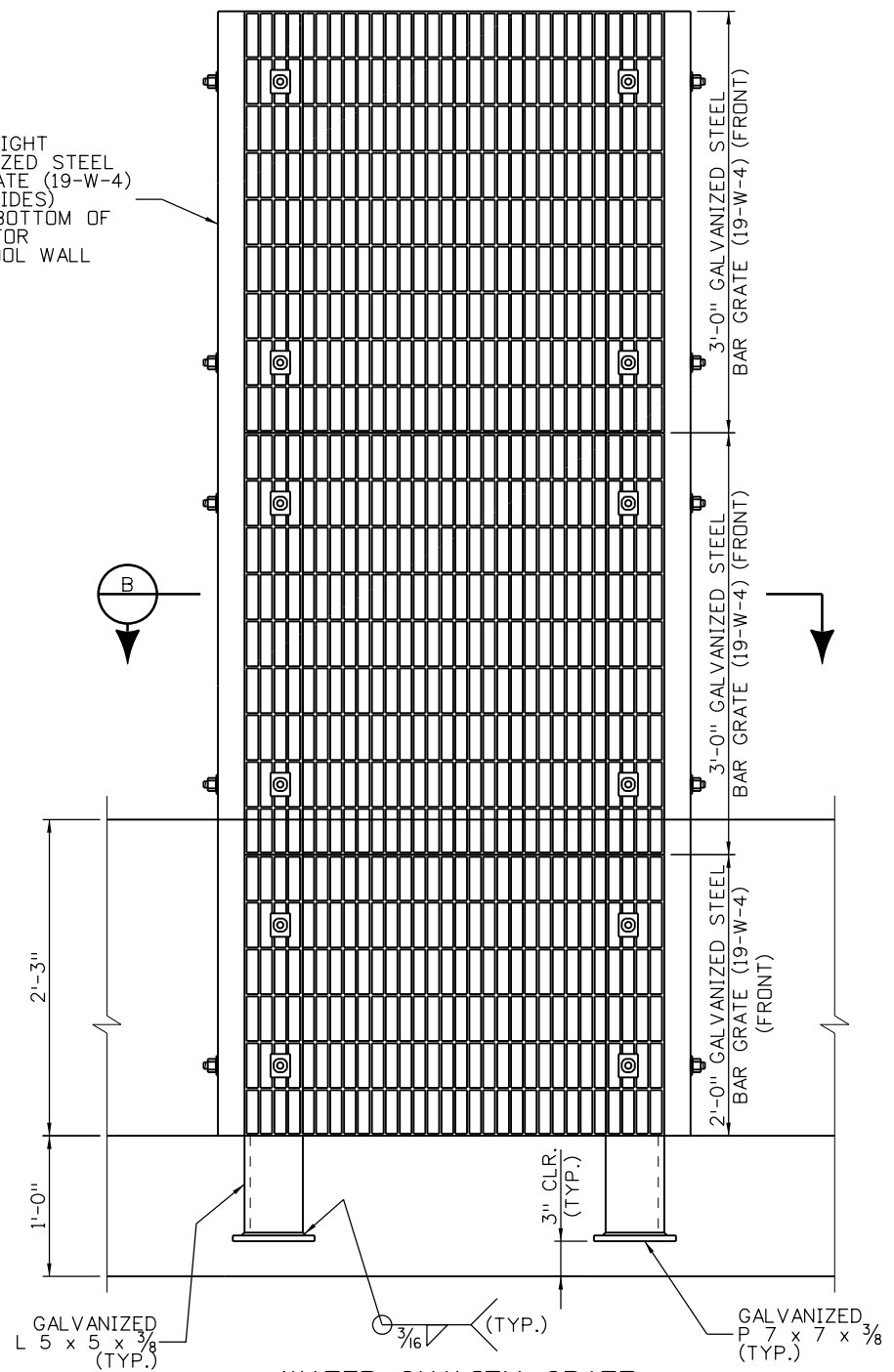
INSIDE DIMENSIONS	
WIDTH (A)	8 FT.
LENGTH (B)	13 FT.
WALL THICKNESS	12 IN.

STORM RAX PEAK ROOF STRUCTURE
NTS
(CONNECT TO OUTLET PER MANUFACTURER'S RECOMMENDATIONS)



SECTION B WATER QUALITY GRATE
NTS

FULL HEIGHT GALVANIZED STEEL BAR GRATE (19-W-4) (BOTH SIDES) NOTCH BOTTOM OF GRATE FOR MICROPOOL WALL



WATER QUALITY GRATE
NTS
(REBAR NOT SHOWN FOR CLARITY)

NOTES:

1. ALL STRUCTURAL STEEL SHALL BE GRADE 50 AASHTO M270 (AOTM A709).
2. ALL BOLTS SHALL BE HIGH STRENGTH BOLTS. BOLT, NUTS AND WASHERS SHALL CONFORM TO CDOT STANDARD SPEC. 509.08 HIGH STRENGTH BOLTS.
3. ALL STEEL ELEMENTS SHALL CONFORM TO CDOT SPECIFICATIONS, SECTION 509.
4. ALL STEEL SHALL BE GALVANIZED PER CDOT SPECIFICATIONS, SECTION 509.
5. ALL WELDING SHALL CONFORM TO CDOT SPECIFICATIONS, SECTION 509.

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						Sheet Subset: DRAIN		Subset Sheets: 20 of 20						

Structural HDPE Products for Water Screening



Key Advantages

Availability

CONTECH® Construction Products Inc. is pleased to introduce StormRax,™ its line of structural plastic trash racks and debris cages for stormwater management basins and pond structures from Plastic Solutions Inc. In addition to the full line of standard sizes, we can also customize to fit your specific requirements.

StormRax trash racks are available in numerous sizes and shapes to accommodate nearly every type of application.

Strength & Durability

Structural plastic has a cellular core surrounded by integral skins forming a totally integrated structure. Structural molded parts made from HDPE and fiberglass have a high strength-to-weight ratio and have 3 to 4 times greater rigidity than solid parts of the same material of equal weight.

Racks are designed to withstand the conditions of pond structures - rough handling, high/low temperatures and long term weather exposure. Structural plastic has replaced wood, concrete, solid plastics and metals in a variety of applications.

Quality Alternative

Structural plastic racks are a great alternative to painted and galvanized steel racks for use in stormwater management ponds and general water screening. They also provide a structurally sound product with a long lasting quality appearance.

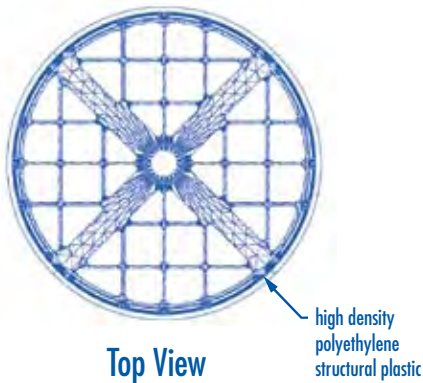
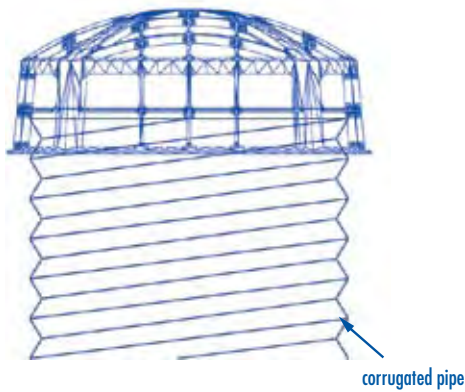


With structural plastic, you can take advantage of the many benefits such as:

- Lighter Weight
- Elimination of Corrosion
- Design Flexibility
- Greater Part Stiffness and Stability
- Chemical Resistance
- Installation Savings

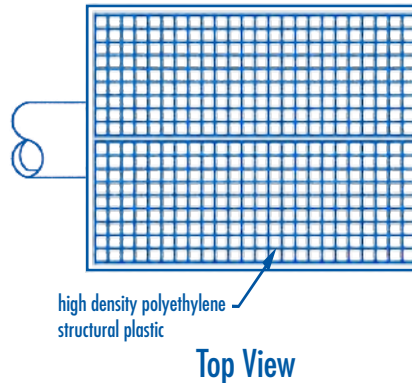
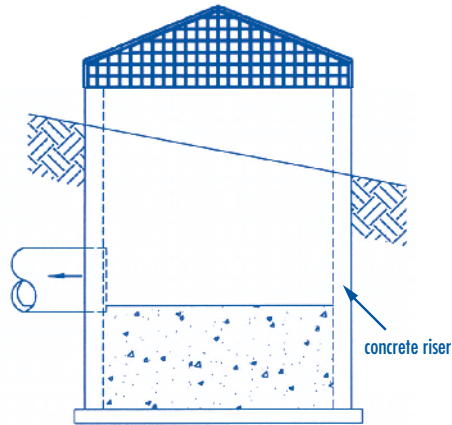
Applications and Options

Round Series



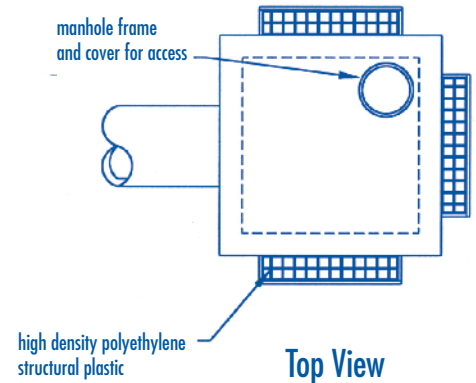
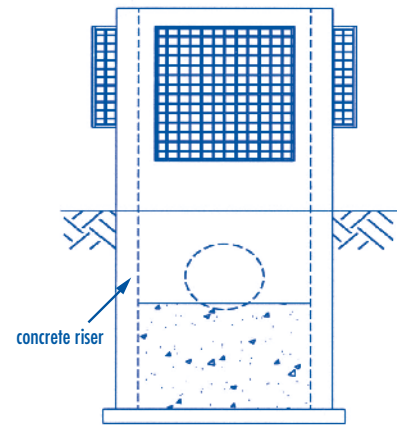
Top View

Peak Series



Top View

Flat Series



Top View

StormRax pyramid racks are available with an anti-vortex device and racks can be mounted on concrete structures, plastic and metal pipe.



New Modular Design - Improved 'Round Series'

Our newest trash rack evolution is constructed of Structural Foam Molded High Density Polyethylene, a strong and lightweight replacement for steel that has proven to be a durable and economical alternative.

CONTECH Construction Products Inc. provides site solutions for the civil engineering industry. CONTECH's portfolio includes bridges, drainage, retaining walls, sanitary sewer, stormwater, erosion control and soil stabilization products.

For more information about the products in this brochure, or to reach a sales representative in your region, call CONTECH's Corporate Office at 513-645-7000 or call toll free at 800-338-1122.

Visit our web site: www.contech-cpi.com

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Design Procedure Form: Extended Detention Basin (EDB)

Sheet 1 of 4

Designer: George Cotton
Company: TSH Engineering
Date: February 6, 2012
Project: Powers Blvd (SH 21) Bridges
Location: RDF "C" Pine Creek South Fork

1. Basin Storage Volume

- A) Effective Imperviousness of Tributary Area, I_a
- B) Tributary Area's Imperviousness Ratio ($i = I_a / 100$)
- C) Contributing Watershed Area
- D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm
- E) Design Concept
(Select EURV when also designing for flood control)
- F) Design Volume (1.2 WQCV) Based on 40-hour Drain Time
($V_{DESIGN} = (1.0 * (0.91 * i^2 - 1.19 * i^2 + 0.78 * i) / 12 * Area * 1.2)$)
- G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume
($V_{WQCV\ OTHER} = (d_6 * (V_{DESIGN} / 0.43))$)
- H) User Input of Water Quality Capture Volume (WQCV) Design Volume
(Only if a different WQCV Design Volume is desired)
- I) Predominant Watershed NRCS Soil Group
- J) Excess Urban Runoff Volume (EURV) Design Volume
 For HSG A: $EURVA = (0.1878i - 0.0104) * Area$
 For HSG B: $EURVB = (0.1178i - 0.0042) * Area$
 For HSG C/D: $EURV_{C/D} = (0.1043i - 0.0031) * Area$

$I_a = 57.2$ %

$i = 0.572$

Area = 658.400 ac

$d_6 = 0.43$ in

Choose One

- ☒ Water Quality Capture Volume (WQCV)
☐ Excess Urban Runoff Volume (EURV)

$V_{DESIGN} = 14.953$ ac-ft

$V_{DESIGN\ OTHER} = 14.953$ ac-ft

$V_{DESIGN\ USER} =$ ac-ft

Choose One

- ☐ A
☒ B
☐ C / D

EURV = ac-ft

2. Basin Shape: Length to Width Ratio

(A basin length to width ratio of at least 2:1 will improve TSS reduction.)

$L : W = 2.0 : 1$

3. Basin Side Slopes

- A) Basin Maximum Side Slopes
(Horizontal distance per unit vertical, 4:1 or flatter preferred)

$Z = 4.00$ ft / ft

4. Inlet

- A) Describe means of providing energy dissipation at concentrated inflow locations:

One main inlet with SAF energy dissipator
 Two other storm drain inlets with riprap aprons

Design Procedure Form: Extended Detention Basin (EDB)

Sheet 2 of 4

Designer: George Cotton
 Company: TSH Engineering
 Date: February 6, 2012
 Project: Powers Blvd (SH 21) Bridges
 Location: RDF "C" Pine Creek South Fork

5. Forebay

A) Minimum Forebay Volume
($V_{FMIN} = 3\%$ of the WQCV)

$V_{FMIN} = 0.374$ ac-ft

B) Actual Forebay Volume

$V_F = 0.510$ ac-ft

C) Forebay Depth
($D_F = 30$ inch maximum)

$D_F = 1.6$ in

D) Forebay Discharge

i) Undetained 100-year Peak Discharge

$Q_{100} = 1840.00$ cfs

ii) Forebay Discharge Design Flow
($Q_F = 0.02 * Q_{100}$)

$Q_F = 36.80$ cfs

E) Forebay Discharge Design

Choose One

- ☐ Berm With Pipe
☒ Wall with Rect. Notch
☐ Wall with V-Notch Weir

F) Discharge Pipe Size (minimum 8-inches)

Calculated $D_p =$ in

G) Rectangular Notch Width

Calculated $W_N = 2724.1$ in

6. Trickle Channel

A) Type of Trickle Channel

Choose One

- ☐ Concrete
☒ Soft Bottom

F) Slope of Trickle Channel

$S = 0.0063$ ft / ft

PROVIDE A CONSISTENT LONGITUDINAL
 SLOPE FROM FOREBAY TO MICROPOOL
 WITH NO MEANDERING. RIPRAP AND
 SOIL RIPRAP LINED CHANNELS ARE
 NOT RECOMMENDED.
 MINIMUM DEPTH OF 1.5 FEET

7. Micropool and Outlet Structure

A) Depth of Micropool (2.5-feet minimum)

$D_M = 2.5$ ft

B) Surface Area of Micropool (10 ft² minimum)

$A_M = 64$ sq ft

C) Outlet Type

Choose One

- ☒ Orifice Plate
☐ Other (Describe):

D) Depth of Design Volume (EURV or 1.2 WQCV) Based on the Design Concept Chosen Under 1.E.

$H = 6.25$ feet

E) Volume to Drain Over Prescribed Time

WQCV = 12.461 ac-ft

F) Drain Time
(Min T_D for WQCV= 40 hours; Max T_D for EURV= 72 hours)

$T_D = 40$ hours

G) Recommended Maximum Outlet Area per Row, (A_o)

$A_o = 9.55$ square inches

H) Orifice Dimensions:

- i) Circular Orifice Diameter or
 ii) Width of 2" High Rectangular Orifice

$D_{orifice} =$ inches

$W_{orifice} = 4.78$ inches

I) Number of Columns

$n_c = 1$ number

J) Actual Design Outlet Area per Row (A_o)

$A_o = 9.55$ square inches

K) Number of Rows (n_r)

$n_r = 18$ number

L) Total Outlet Area (A_{ot})

$A_{ot} = 179.3$ square inches

M) Depth of WQCV (H_{wqcv})
(Estimate using actual stage-area-volume relationship and V_{wqcv})

$H_{wqcv} =$ feet

N) Ensure Minimum 40 Hour Drain Time for WQCV

$T_{D wqcv} =$ hours

Design Procedure Form: Extended Detention Basin (EDB)

Sheet 3 of 4

Designer: George Cotton
 Company: TSH Engineering
 Date: February 6, 2012
 Project: Powers Blvd (SH 21) Bridges
 Location: RDF "C" Pine Creek South Fork

8. Initial Surge Volume

- A) Depth of Initial Surge Volume
 (Minimum recommended depth is 4 inches)
- B) Minimum Initial Surge Volume
 (Minimum volume of 0.3% of the WQCV)
- C) Initial Surge Provided Above Micropool

$D_{IS} = 12.0$ in

$V_{IS} = 1,628.4$ cu ft

$V_s = 64.0$ cu ft **INCREASE DEPTH OF INITIAL SURCHARGE
OR SURFACE AREA OF MICROPOOL**

9. Trash Rack

- A) Type of Water Quality Orifice Used

B) Water Quality Screen Open Area: $A_t = 38.5 \cdot (e^{-0.095D_s}) \cdot A_{ot}$

- C) For 2", or Smaller, Circular Opening (See Fact Sheet T-12):

- i) Width of Water Quality Screen and Concrete Opening ($W_{opening}$)
- ii) Height of Water Quality Screen (H_{TR})
- iii) Type of Screen, Describe if "Other"

Choose One

- ☐ Circular (up to 2" diameter)
☒ Rectangular (2" high)

$A_t = 5,707$ square inches

$W_{opening} =$ inches

$H_{TR} =$ inches

Choose One

- ☐ S.S. Well Screen with 60% Open Area*
☐ Other (Describe):

- D) For 2" High Rectangular Opening:

- i) Width of Rectangular Opening ($W_{orifice}$)
- ii) Width of Water Quality Screen Opening ($W_{opening}$)
- iii) Height of Water Quality Screen (H_{TR})
- iv) Type of Screen, Describe if "Other"

$W = 4.78$ inches

$W_{opening} = 6.0$ ft

$H_{TR} = 8.6$ ft

Choose One

- ☒ Aluminum Amico-Klemp SR Series (or equal)
☐ Other (Describe):

- v) Cross-bar Spacing

4.0 inches

- vi) Minimum Bearing Bar Size

$2\text{-}1/4$ inch x $3/16$ inch

Design Procedure Form: Extended Detention Basin (EDB)

Sheet 4 of 4

Designer: George Cotton
Company: TSH Engineering
Date: February 6, 2012
Project: Powers Blvd (SH 21) Bridges
Location: RDF "C" Pine Creek South Fork

10. Overflow Embankment

A) Describe embankment protection for 100-year and greater overtopping:

175 foot broad crested weir with riprap revetment

B) Slope of Overflow Embankment
 (Horizontal distance per unit vertical, 4:1 or flatter preferred)

$Z_E = 10.00$ ft / ft

11. Vegetation

Choose One

- ☐ Irrigated
☒ Not Irrigated

12. Access

A) Describe Sediment Removal Procedures

10' wide access road to micropool
 Access road to forebay currently exists.

Notes:

Comparison of Addendum No. 2 and No. 3 Hydrology

The planning for the Pine Creek Drainage has progressed through three phases. The original planning study was completed by Obering, Worth and Associates in 1988. This plan was updated in 1998 by JR Engineering and again in 2002. The design of Pine Creek Regional Detention Facility "C" was completed in 1998 and constructed in the same year. In 2003, the pond was retrofit to include a constructed wetland.

Addendum No. 2 identified ten (10) sub-basins that were tributary to Pond "C" with a total drainage area of 664.4 acres (1.038 sq. mi.). The weighted SCS curve number for the basin was 87.2 and the impervious fraction of the basin was 67.2%.

Addendum No. 3 refined the watershed and has 20 sub-basins that are tributary to Pond "C" with a total drainage area of 658.4 acres (1.029 sq. mi.). The weighted SCS curve number for the basin decreases slightly to 84.6 and the impervious fraction of the basin to 57.2%.

Despite the additional detail in hydrologic modeling, the inflow to Pond "C" is similar for the two Addendums. The Addendum No. 2 inflow peak was 1840 cfs, which is nearly identical to the Addendum No. 3 inflow peak of 1825 cfs. Peak outflows are essentially the same with Addendum No. 2 releasing at a peak rate of 227 cfs and Addendum No. 3 at 228 cfs. Peak stage and maximum storage volume are 77.4 feet and 69 ac-ft, respectively for Addendum No. 2, and 77.6 feet and 72 ac-ft, respectively for Addendum No. 3.

Given the similarity in hydrology of both models, it was decided that it was acceptable and slightly conservative to base the pond routing on the simpler Addendum No. 2 model. The design water quality volume, however was based on updated impervious data for the watershed provided in Addendum No. 3.

Sub-Basin Parameters / Fully Developed Conditions

from JR Engineering, 1998, "Amendment No. 2"

Appendix - Hydrologic Model Input Calculation

Sub-Basin Label	Total Area acres	Total Area s.m.	Weighted CN	Weighted Percent Impervious	Adjusted CN (1)	Total Lag (min)
PS1	96.2	0.150	78.1	44.9	78.4	12.30
PS2	98.3	0.154	87.4	68.4	85.2	11.29
PS3	103.6	0.162	85.9	68.9	84.8	12.30
PS4	34.8	0.054	92.3	83.6	93.2	8.06
PS5	42.0	0.066	95.6	93.7	98.0	8.11
PS6	48.0	0.075	82.8	59.0	86.5	7.36
PS7	57.0	0.089	93.3	86.8	96.3	7.16
PS8	78.3	0.122	81.6	58.4	86.0	7.63
PS9	81.8	0.128	92.9	85.7	94.5	7.81
PS10	24.4	0.038	72.9	20.5	72.9	9.59
PS11	35.7	0.056	79.1	48.6	80.3	10.35
PS12	98.0	0.153	70.1	10.0	68.5	14.00
PS13	41.9	0.065	73.9	25.0	76.1	8.93
At RDF-C	664.4	1.038		67.6%		

Notes: (1) CNs were adjusted by JRE to match
rational method calculations

Sub-Basin Parameters / Fully Developed Conditions

from JR Engineering, 2002, "Amendment No. 3"

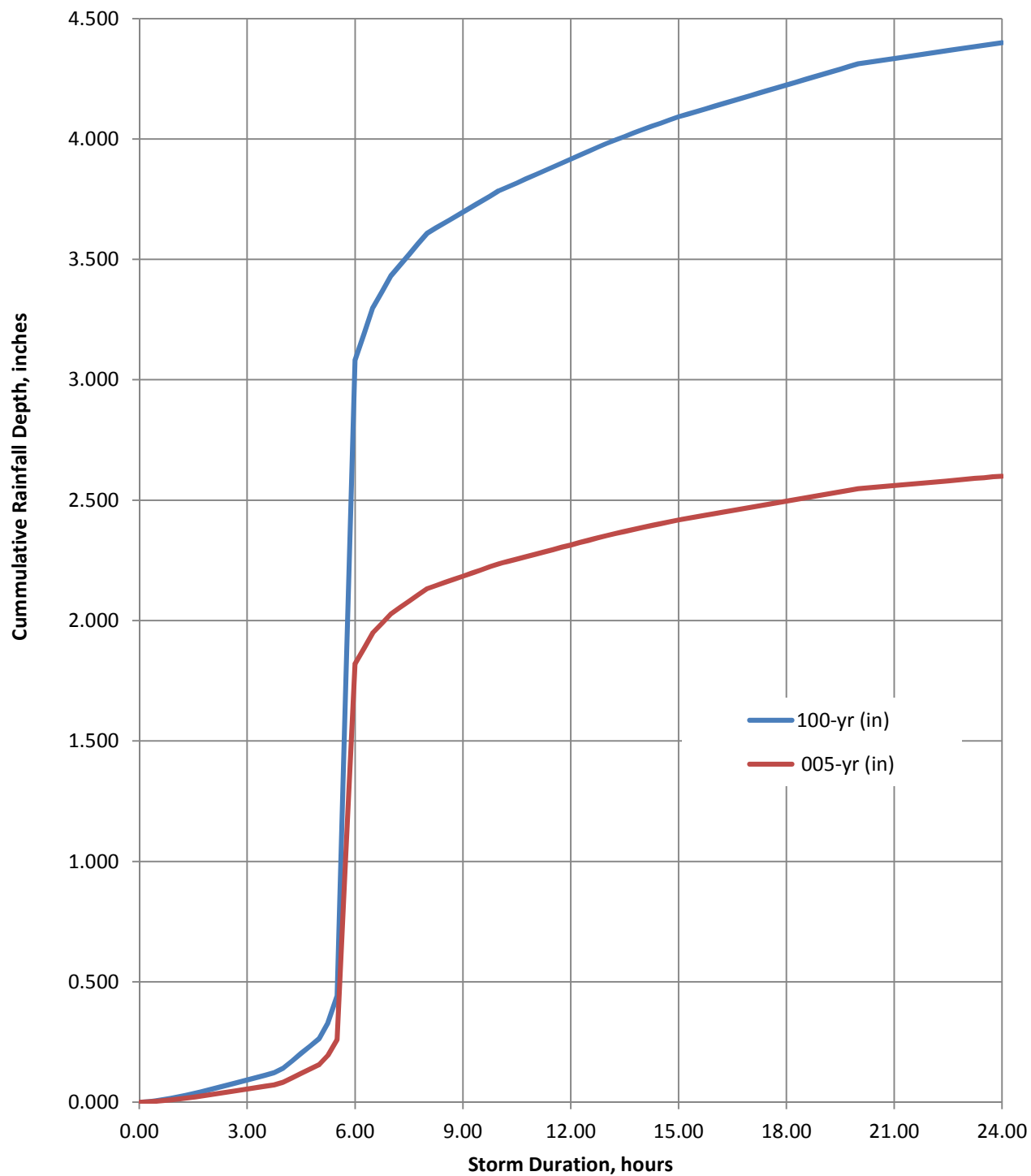
Map 1. Fully Developed Conditions

Sub-Basin Label	Total Area acres	Total Area s.m.	Weighted CN	Weighted Percent Impervious	Adjusted CN (1)	Total Lag (min)
PSE01	21.6	0.034	70.5	30.6	74.5	0.197
PSE02	18.3	0.029	74.9	36.3	77.0	0.169
PSE03	49.9	0.078	79.3	45.7	79.6	0.171
PSE04	47.7	0.075	71.9	32.2	75.6	0.192
PSE05	30.2	0.047	74.2	35.0	76.5	0.181
PSE06	34.6	0.054	78.4	42.1	78.4	0.189
PSE07	37.0	0.058	96.0	90.0	96.5	0.125
PSE08	37.3	0.058	78.8	46.5	80.0	0.165
PSE09	26.5	0.041	90.7	78.1	97.5	0.107
PSE10	22.8	0.036	83.7	60.1	83.2	0.175
PSE11	20.6	0.032	80.0	50.0	80.0	0.210
PS02	15.2	0.024	88.4	73.5	88.4	0.150
PS03	45.1	0.070	92.6	85.1	97.5	0.117
PS04	38.2	0.060	78.7	42.9	78.5	0.178
PS05	19.5	0.030	92.8	85.4	96.0	0.130
PS06	34.0	0.053	93.8	89.4	97.5	0.126
PS07	20.1	0.031	92.8	85.2	97.5	0.118
PS08	71.4	0.112	84.1	58.8	83.0	0.174
PS09	34.8	0.054	87.6	70.9	90.0	0.125
PS10	33.6	0.053	73.2	23.9	73.4	0.177
PS11	34.7	0.054	78.5	47.1	80.3	0.172
PS12	98.0	0.153	70.0	9.9	69.0	0.233
PS13	41.9	0.065	73.9	25.0	74.3	0.149
At RDF-C	658.4	1.029		57.2%		

Type IIA Storm Pattern (15 m interval)

Pine Creek Drainage Basin Colorado Springs, CO

Time (h)	Storm Distribution			Time (h)	Storm Distribution (cont.)		
	Type IIA Distri.	100-yr (in)	005-yr (in)		Type IIA Distri.	100-yr (in)	005-yr (in)
0.00	0.0000	0.000	0.000	12.00	0.89	3.92	2.31
0.25	0.0005	0.002	0.001	12.25	0.89	3.93	2.32
0.50	0.0015	0.007	0.004	12.50	0.90	3.95	2.33
0.75	0.0030	0.013	0.008	12.75	0.90	3.97	2.34
1.00	0.0045	0.020	0.012	13.00	0.91	3.98	2.35
1.25	0.0060	0.026	0.016	13.25	0.91	4.00	2.36
1.50	0.0080	0.035	0.021	13.50	0.91	4.01	2.37
1.75	0.0100	0.044	0.026	13.75	0.91	4.03	2.38
2.00	0.0120	0.053	0.031	14.00	0.92	4.04	2.39
2.25	0.0143	0.063	0.037	14.25	0.92	4.05	2.39
2.50	0.0165	0.073	0.043	14.50	0.92	4.07	2.40
2.75	0.0188	0.083	0.049	14.75	0.93	4.08	2.41
3.00	0.0210	0.092	0.055	15.00	0.93	4.09	2.42
3.25	0.0233	0.103	0.061	15.25	0.93	4.10	2.42
3.50	0.0255	0.112	0.066	15.50	0.94	4.11	2.43
3.75	0.0278	0.122	0.072	15.75	0.94	4.13	2.44
4.00	0.0320	0.141	0.083	16.00	0.94	4.14	2.44
4.25	0.0390	0.172	0.101	16.25	0.94	4.15	2.45
4.50	0.0460	0.202	0.120	16.50	0.95	4.16	2.46
4.75	0.0530	0.233	0.138	16.75	0.95	4.17	2.46
5.00	0.0600	0.264	0.156	17.00	0.95	4.18	2.47
5.25	0.0750	0.330	0.195	17.25	0.95	4.19	2.48
5.50	0.1000	0.440	0.260	17.50	0.96	4.20	2.48
5.75	0.4000	1.760	1.040	17.75	0.96	4.21	2.49
6.00	0.7000	3.080	1.820	18.00	0.96	4.22	2.50
6.25	0.7250	3.190	1.885	18.25	0.96	4.24	2.50
6.50	0.7500	3.300	1.950	18.50	0.97	4.25	2.51
6.75	0.7650	3.366	1.989	18.75	0.97	4.26	2.52
7.00	0.7800	3.432	2.028	19.00	0.97	4.27	2.52
7.25	0.7900	3.476	2.054	19.25	0.97	4.28	2.53
7.50	0.8000	3.520	2.080	19.50	0.98	4.29	2.54
7.75	0.8100	3.564	2.106	19.75	0.98	4.30	2.54
8.00	0.8200	3.608	2.132	20.00	0.98	4.31	2.55
8.25	0.8250	3.630	2.145	20.25	0.98	4.32	2.55
8.50	0.8300	3.652	2.158	20.50	0.98	4.32	2.55
8.75	0.8350	3.674	2.171	20.75	0.98	4.33	2.56
9.00	0.8400	3.696	2.184	21.00	0.99	4.33	2.56
9.25	0.8450	3.718	2.197	21.25	0.99	4.34	2.56
9.50	0.8500	3.740	2.210	21.50	0.99	4.35	2.57
9.75	0.8550	3.762	2.223	21.75	0.99	4.35	2.57
10.00	0.8600	3.784	2.236	22.00	0.99	4.36	2.57
10.25	0.8638	3.801	2.246	22.25	0.99	4.36	2.58
10.50	0.8675	3.817	2.256	22.50	0.99	4.37	2.58
10.75	0.8713	3.834	2.265	22.75	0.99	4.37	2.58
11.00	0.8750	3.850	2.275	23.00	1.00	4.38	2.59
11.25	0.8788	3.867	2.285	23.25	1.00	4.38	2.59
11.50	0.8825	3.883	2.295	23.50	1.00	4.39	2.59
11.75	0.8863	3.900	2.304	23.75	1.00	4.39	2.60
12.00	0.8900	3.916	2.314	24.00	1.00	4.40	2.60



Outlet Rating Curves - Retrofit Configuration #1 (Exst Outlet Pipe)

Project Survey (5)		Depth (ft)	Outlet Pipe Rating (cfs)		WQ Outlet (cfs)		Emergency Spillway (cfs)		Outlet Rating (cfs)		Comment
Elev (ft)	Storage (ac-ft)		HDS-5 Ch-1 Exst (1)	HDS-5 Ch-3 Bevel (2)	Weir (3) Retrofit	Orifice Plate (4)	Existing	Retrofit (6)	Existing	Retrofit	
6865.82	0.00	0.0	0.0	0.00	0.0	0.00	0.0	0.0	0.00	0.00	
6867.0	0.0043	1.2	3.7	1.4	0.0	0.80	0.0	0.0	3.70	0.8	
6868.0	0.47	2.2	31.5	32.5	0.0	1.83	0.0	0.0	31.50	1.83	
6869.0	2.27	3.2	56.7	60.9	0.0	3.12	0.0	0.0	56.70	3.12	
6870.0	5.51	4.2	79.5	86.6	0.0	4.62	0.0	0.0	79.50	4.62	
6870.17	6.23	4.35	83.3	91.6	0.0	4.84	0.0	0.0	83.30	4.84	Stage at 1/2 WQCV
6871.0	9.71	5.2	100.1	110.0	0.0	6.29	0.0	0.0	100.10	6.29	
6871.59	12.46	5.77	119.4	132.2	0.0	7.36	0.0	0.0	119.40	7.36	Stage at WQCV
6872.0	14.40	6.2	118.5	131.2	0.0	8.02	0.0	0.0	118.50	8.02	
6872.11	14.95	6.29	129.4	143.8	0.0	8.18	0.0	0.0	129.40	8.18	Stage at WQCV*1.2
6873.0	19.34	7.2	135.1	150.4	41.8	9.33	0.0	0.0	135.10	51.13	
6874.0	24.46	8.2	150.1	167.7	129.6	10.43	0.0	0.0	150.10	140.02	
6875.0	29.76	9.2	163.5	183.5	245.2	11.41	0.0	0.0	163.50	163.50	
6876.0	35.24	10.2	175.6	197.8	382.9	12.31	0.0	0.0	175.60	175.60	
6877.0	40.89	11.2	186.7	210.8	539.8	13.14	0.0	0.0	186.70	186.70	
6878.0	46.73	12.2	196.7	222.8	713.7	13.92	0.0	0.0	196.70	196.70	
6879.0	52.73	13.2	206.1	233.9	903.0	14.66	0.0	0.0	206.10	206.10	
6880.0	58.92	14.2	214.9	244.3	1106.6	15.36	0.0	0.0	214.90	214.90	
6881.0	65.30	15.2	223.3	254.3	1323.6	16.03	0.0	0.0	223.30	223.30	
6881.55	68.90	15.7	227.8	259.6	1448.3	16.39	0.0	0.0	227.80	227.80	Existing Spillway Crest
6882.0	71.92	16.2	231.5	263.9	1553.1	16.67	121.5	0.0	353.00	231.50	
6883.0	78.80	17.2	239.7	273.4	1794.6	17.30	702.8	0.0	942.48	239.70	Raised Spillway (6)
6883.5	82.34	17.7	244.9	279.5	1919.6	17.59	1096.0	142.3	1340.95	387.24	
6884.0	85.87	18.2	248.2	283.0	2047.4	17.89	1543.5	402.5	1791.73	650.70	
6885.0	93.12	19.2	257.0	292.9	2311.1	18.47	2579.3	1138.4	2836.26	1395.44	
6886.0	100.56	20.2	266.3	303.2	2585.2	19.02	3778.4	2091.5	4044.68	2357.75	Top of Dam Embankment

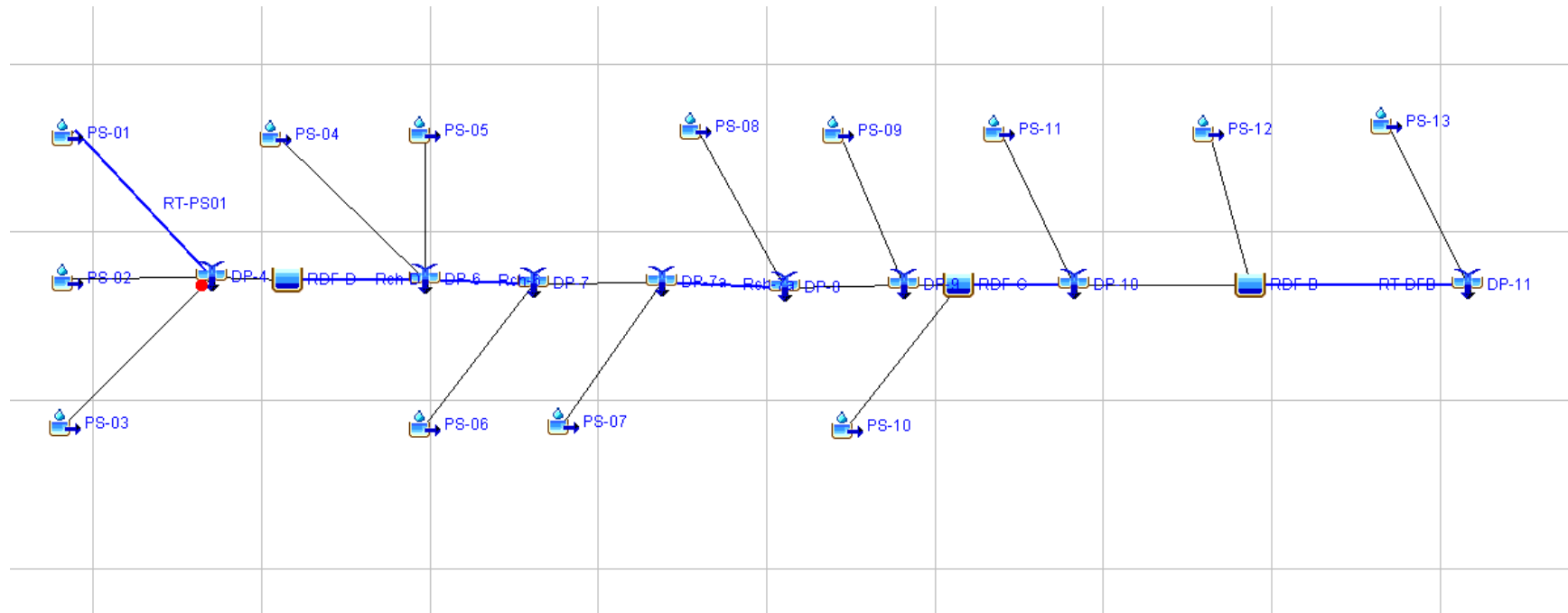
- Notes: (1) 4' RCP (Chart 1 / square edge with headwall) $S = 0.050$ '/'
(2) 4' RCP (Chart 3 / beveled-ring edge with headwall) $S = 0.050$ '/'
(3) Sharp crested weir, $L = 15$ ft (effective length)
(4) 15 rows 6.33"x2.0" orifices
(5) Assumes that Csprings datum is NGVD29 and project is NAVD88 (Project = CSprgs + 3.824')
(6) Raised spillway crest 1.5'

Outlet Rating Curves - Retrofit Configuration #2 (Beveled Headwall Outlet Pipe)

Project Survey (5)		Depth (ft)	Outlet Pipe Rating (cfs)		WQ Outlet (cfs)		Emergency Spillway (cfs)		Outlet Rating (cfs)		Comment
Elev (ft)	Storage (ac-ft)		HDS-5 Ch-1 Exst (1)	HDS-5 Ch-3 Bevel (2)	Weir (3) Retrofit	Orifice Plate (4)	Existing	Retrofit (6)	Existing	Retrofit	
6865.82	0.00	0.0	0.0	0.00	0.0	0.00	0.0	0.0	0.00	0.00	
6867.0	0.0043	1.2	3.7	1.4	0.0	0.80	0.0	0.0	3.70	0.8	
6868.0	0.47	2.2	31.5	32.5	0.0	1.83	0.0	0.0	31.50	1.83	
6869.0	2.27	3.2	56.7	60.9	0.0	3.12	0.0	0.0	56.70	3.12	
6870.0	5.51	4.2	79.5	86.6	0.0	4.62	0.0	0.0	79.50	4.62	
6870.17	6.23	4.35	83.3	91.6	0.0	4.84	0.0	0.0	83.30	4.84	Stage at 1/2 WQCV
6871.0	9.71	5.2	100.1	110.0	0.0	6.29	0.0	0.0	100.10	6.29	
6871.59	12.46	5.77	119.4	132.2	0.0	7.36	0.0	0.0	119.40	7.36	Stage at WQCV
6872.0	14.40	6.2	118.5	131.2	0.0	8.02	0.0	0.0	118.50	8.02	
6872.11	14.95	6.29	129.4	143.8	0.0	8.18	0.0	0.0	129.40	8.18	Stage at WQCV*1.2
6873.0	19.34	7.2	135.1	150.4	41.8	9.33	0.0	0.0	135.10	51.13	
6874.0	24.46	8.2	150.1	167.7	129.6	10.43	0.0	0.0	150.10	140.02	
6875.0	29.76	9.2	163.5	183.5	245.2	11.41	0.0	0.0	163.50	183.50	
6876.0	35.24	10.2	175.6	197.8	382.9	12.31	0.0	0.0	175.60	197.80	
6877.0	40.89	11.2	186.7	210.8	539.8	13.14	0.0	0.0	186.70	210.80	
6878.0	46.73	12.2	196.7	222.8	713.7	13.92	0.0	0.0	196.70	222.80	
6879.0	52.73	13.2	206.1	233.9	903.0	14.66	0.0	0.0	206.10	233.90	
6880.0	58.92	14.2	214.9	244.3	1106.6	15.36	0.0	0.0	214.90	244.30	
6881.0	65.30	15.2	223.3	254.3	1323.6	16.03	0.0	0.0	223.30	254.30	
6881.55	68.90	15.7	227.8	259.6	1448.3	16.39	0.0	0.0	227.80	259.60	Existing Spillway Crest
6882.0	71.92	16.2	231.5	263.9	1553.1	16.67	121.5	0.0	353.00	263.90	
6883.0	78.80	17.2	239.7	273.4	1794.6	17.30	702.8	0.0	942.48	273.40	Raised Spillway (6)
6883.5	82.34	17.7	244.9	279.5	1919.6	17.59	1096.0	142.3	1340.95	421.81	
6884.0	85.87	18.2	248.2	283.0	2047.4	17.89	1543.5	402.5	1791.73	685.50	
6885.0	93.12	19.2	257.0	292.9	2311.1	18.47	2579.3	1138.4	2836.26	1431.34	
6886.0	100.56	20.2	266.3	303.2	2585.2	19.02	3778.4	2091.5	4044.68	2394.65	Top of Dam Embankment

- Notes: (1) 4' RCP (Chart 1 / square edge with headwall) $S = 0.050$ '/'
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(5) Assumes that Csprings datum is NGVD29 and project is NAVD88 (Project = CSprgs + 3.824')
(6) Raised spillway crest 1.5'

Pine Creek HEC-HMS Schematic



Comparison of reservoir operations in Pine Creek South Fork

Description: Update survey of RDF-C reservoir area

Alternative 1: New water quality outlet w/ 1.45' raised spillway crest

Existing headwall conditions at pipe outlet

RDF	JR Report				Revised HMS (no spillway)				Pond		
	Inflow (cfs)	Outflow (cfs)	Max Stored (af)	Max Stage	Inflow (cfs)	Outflow (cfs)	Max Stored (af)	Max Stage	Min Elev (ft)	Pond Max Elev (ft)	Spillway Elev (ft)
D	1073	99	44	110.7	1265	115	55.8	112.9	100.0	114.0	81.55
C	1840	227	69	77.4	1865	233	72.8	82.1	65.8	86.0	
B	506	247	14	82.9	509	250	14.3	83.2	71.2	88.0	

	Revised HMS (with exst spillway)				RDF-C WQ Retrofit Alt 1 w/ spillway				
	Inflow	Outflow	Max		Inflow	Outflow	Max		Spillway
RDF	(cfs)	(cfs)	Stored (af)	Max Stage	(cfs)	(cfs)	Stored (af)	Max Stage	Elev (ft)
D	1265	115	55.8	112.9	1265	115	55.8	112.9	83.0 with initial 50% WQCV
C	1865	315*	71.0	81.9	1865	344.5*	81.3	83.3	
B	509	266	16.9	84.5	558	282	19.5	85.7	
*51 min / 84 cfs / 3.4 af				*36 min / 85 cfs / 3.3 af					

	RDF-C Clogged (with exst spillway)				RDF-C WQ Retrofit Alt 1 w/ Clogging				
RDF	Inflow (cfs)	Outflow (cfs)	Max Stored (af)	Max Stage	Inflow (cfs)	Outflow (cfs)	Max Stored (af)	Max Stage	Spillway Elev (ft)
D	1265	115	55.8	112.9	1265	115	55.8	112.9	83.0
C	1865	756	79.2	83.1	1865	439	86.2	84.0	
B	508	258	15.5	83.8	520	254	15.0	83.5	

with initial 50% WQCV



DEPARTMENT OF THE ARMY
ALBUQUERQUE DISTRICT, CORPS OF ENGINEERS
Southern Colorado Regulatory Office
200 S. Santa Fe Avenue, Suite 301
Pueblo, Colorado 81003

February 1, 2012

REPLY TO
ATTENTION OF

Regulatory Division

SUBJECT: Action No. SPA-2012-00051, Retrofit of Regional Detention Facility "C", El Paso County, Colorado

George Cotton
Tsiouvaras Simmons Holderness, Inc.
5690 DTC Blvd., Ste 345W
Greenwood Village, Colorado 80111

Mr. Cotton:

We received of your e-mail dated January 31, 2012 concerning Retrofit of Regional Detention Facility "C", El Paso County, Colorado. We have assigned Action No. SPA-2012-00051 to this activity. To avoid delay, please include this number in all future correspondence concerning this project.

We have reviewed this project in accordance with Section 404 of the Clean Water. Under Section 404, the Corps regulates the discharge of dredged and fill material into waters of the United States (U.S.), including wetlands. Based on your description of the proposed work, and other information available to us, we have determined that the proposed project will involve activities subject to Section 404. Therefore, a Department of the Army permit is required.

We have determined that this project is authorized by Nationwide Permit No. 43 for Stormwater Management Facilities. A summary of this permit and the regional conditions for Colorado is e available on our website at www.spa.usace.army.mil/reg/. You are only authorized to conduct the work described in your submittal

Our review of this project also addressed its effects on threatened and endangered species and historic properties in accordance with general conditions 17 and 18. Based on the information provided, we have determined that this project will not affect any species listed as threatened or endangered by the U.S. Fish and Wildlife Service within the permit area. We have also determined that this project will not affect historic properties listed, or eligible for listing, in

the National Register of Historic Places. However, please note that you are responsible for meeting the requirements of general condition 17 on endangered species and general condition 18 on historic properties.

This verification is valid until March 18, 2012, unless the nationwide permit is modified, suspended, revoked or reissued prior to that date. The Corps will issue a public notice when the nationwide permits are reissued. If you commence or are under contract to commence the authorized activity before the date that the relevant nationwide permit(s) is modified, reissued or revoked you will have twelve (12) months from the date of the modification, reissuance, or revocation of the nationwide permits to complete the activity under the present terms and conditions of the nationwide permits. Continued confirmation that an activity complies with the terms and conditions, and any changes to the nationwide permit, is the responsibility of the permittee.

You must allow representatives from this office to inspect the authorized activity at any time deemed necessary to ensure that it is being, or has been, accomplished in accordance with the terms and conditions of the nationwide permit.

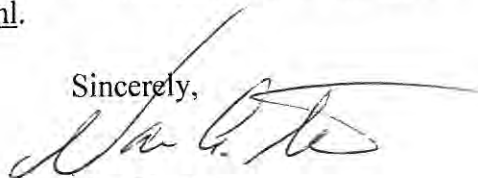
You must sign and submit to us the enclosed certification that the work, including any required mitigation, was completed in compliance with the nationwide permit. You should submit your certification within 30 days of the completion of work.

This permit is not an approval of the project design features, nor does it imply that the construction is adequate for its intended purpose. This permit does not authorize any injury to property or invasion of rights or any infringement of Federal, state or local laws or regulations. You must possess the authority, including property rights, to undertake the proposed work.

If you have any questions concerning our regulatory program, please contact Joshua Carpenter at 719-543-6914 or by e-mail at joshua.g.carpenter@usace.army.mil. At your

convenience, please complete a Customer Service Survey on-line available at <http://per2.nwp.usace.army.mil/survey.html>.

Sincerely,

A handwritten signature in black ink, appearing to read 'Van Truan', is written over a horizontal line.

Van Truan
Chief, Southern Colorado
Regulatory Office

**Certification of Compliance
with Department of the Army Nationwide Permit**

Action Number: SPA-2012-00051

Name of Permittee: Colorado Department of Transportation

Nationwide Permit: No. 43 for Stormwater Management Facilities

Upon completion of the activity authorized by this permit and any mitigation required by the permit, sign this certification and return it to the following address:

Van Truan
U.S. Army Corps of Engineers, Albuquerque District
Southern Colorado Regulatory Office
200 S. Santa Fe Avenue, Suite 301
Pueblo, Colorado 81003

Please note that your permitted activity is subject to a compliance inspection by an U.S. Army Corps of Engineers representative. If you fail to comply with this permit, you are subject to permit suspension, modification, or revocation.

Please enclose photographs showing the completed project (if available).

I hereby certify that the work authorized by the above referenced permit has been completed in accordance with the terms and conditions of the said permit, and required mitigation was completed in accordance with the permit conditions.

Date Work Started _____

Date Work Completed _____

Date

Signature of Permittee



ENGINEERING

February 11, 2011

Mark S. Andrew
CDOT Resident Engineer
1480 Quail Lake Loop Suite A
Colorado Springs, CO 80906

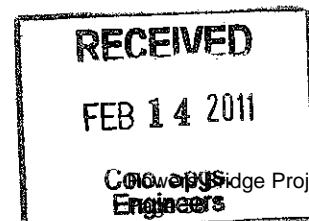
Re: Briargate and Union Detention Pond
Colorado Springs, CO

Dear Mark,

This is a follow up letter to the meeting on February 9, 2011, with City Engineering, City Streets Division and CDOT regarding CDOT's request to modify the outlet structure at the large detention pond at Union and Briargate. The City concurs with this request, which will allow CDOT to modify the outlet structure with the following commitments from CDOT:

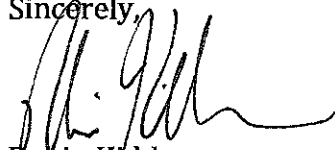
- During the design process, the City will be involved in the decision making to ensure the design meets current City specifications, as well as accepted industry practices for BMP design. The design will be reviewed and accepted by both the City and CDOT prior to construction.
- The outlet structure will require maintenance at recommended intervals. CDOT will commit to maintaining the outlet structure for every other maintenance cycle. The maintenance cycle will be determined based on the features of the final design of the outlet structure. CDOT will use best design practices to minimize maintenance for both the City and CDOT.
- CDOT will provide better access to the outlet structure to ensure that maintenance equipment can access the site.

30 S. Nevada Avenue, Ste 401, M/C 410, Colorado Springs, Colorado 80903
Tel 719-385-5907 Fax 719-385-5497



- CDOT will also honor all requirements to other regulatory parties such as US Fish and Wildlife Service, which may limit access to seasonal periods.
- CDOT to follow up with an Intergovernmental Agreement that will specify further details including maintenance commitments from CDOT once the final design is completed.

Sincerely,



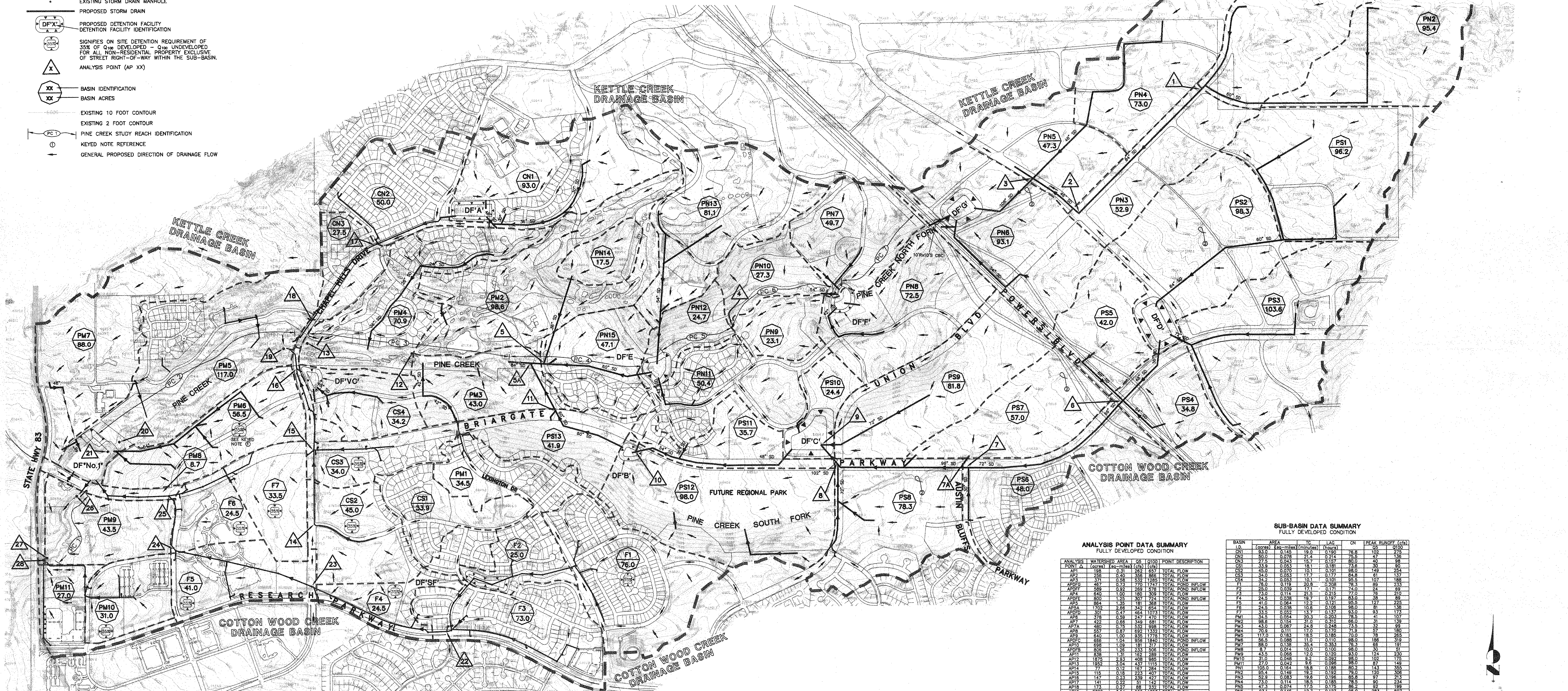
Robin Kidder
City Engineer

C: Tim Mitros, City of Colorado Springs
Bard Lower, City Streets Division
Dave Poling, CDOT R2 Program Engineer
Yun Han, CDOT Project Engineer

LEGEND

- CURRENT MAJOR DRAINAGE BASIN BOUNDARY
--- CURRENT SUB-BASIN BOUNDARY
--- PREVIOUS MAJOR DRAINAGE BASIN BOUNDARY (1988 DBPS)
--- LIMIT OF CURRENT STUDY
--- EXISTING STORM DRAIN
• EXISTING STORM DRAIN INLET
• EXISTING STORM DRAIN MANHOLE
--- PROPOSED STORM DRAIN
DF'X- PROPOSED DETENTION FACILITY
DETENTION FACILITY IDENTIFICATION
SIGNIFIES ON SITE DETENTION REQUIREMENT OF 35% OF Q₁₀₀ DEVELOPED - Q₁₀₀ UNDEVELOPED FOR ALL NON-RESIDENTIAL PROPERTY EXCLUSIVE OF STREET RIGHT-OF-WAY WITHIN THE SUB-BASIN.
X ANALYSIS POINT (AP XX)
XX BASIN IDENTIFICATION
XX BASIN ACRES
--- EXISTING 10 FOOT CONTOUR
--- EXISTING 2 FOOT CONTOUR
PC- PINE CREEK STUDY REACH IDENTIFICATION
○ KEYED NOTE REFERENCE
--- GENERAL PROPOSED DIRECTION OF DRAINAGE FLOW

AMENDMENT 2
TO
PINE CREEK DRAINAGE BASIN PLANNING STUDY
FULLY DEVELOPED CONDITION
BASIN MAP AND MASTER PLAN



GENERAL NOTES:

- FUTURE STORM DRAINS SHOWN ON THIS PLAN ARE ONLY INTENDED TO INDICATE GENERAL LOCATIONS AND APPROXIMATE SIZES OF FUTURE FACILITIES. ACTUAL STORM DRAIN SIZES AND LOCATIONS SHALL BE DETERMINED WITH MORE DETAILED ANALYSIS AT THE TIME OF DETAILED DESIGN OF THE FACILITIES. IT IS LIKELY THAT ADDITIONAL FACILITIES NOT SHOWN ON THIS PLAN WILL BE REQUIRED.
- PROPOSED DETENTION FACILITIES SHOWN ON THIS PLAN ARE ONLY INTENDED TO INDICATE GENERAL LOCATIONS AND LAND AREA REQUIRED FOR THESE FACILITIES. ACTUAL LOCATION AND LAND AREA REQUIRED SHALL BE DETERMINED AT THE TIME OF DETAILED DESIGN OF THE FACILITIES.
- EXCEPT AS OTHERWISE NOTED, THIS PLAN SHALL NOT MODIFY THE REQUIREMENTS OF PREVIOUSLY APPROVED MASTER DEVELOPMENT DRAINAGE PLANS AND FINAL DRAINAGE REPORTS.
- THE AREA ABOVE POWERS BOULEVARD SHOULD BE RE-EXAMINED AS MORE DETAIL ABOUT LAND PLANNING IS KNOWN. ADDITIONAL DETENTION FACILITIES LOCATED HIGHER IN THE WATERSHED SHOULD BE CONSIDERED.

KEYED NOTES:

- SUB-BASIN PM8 WAS ANALYZED ASSUMING FREE DISCHARGE FROM THE SUB-BASIN. FREE DISCHARGE FROM THE SUB-BASIN MAY BE ALLOWED PROVIDED THE OUTFALL SYSTEM TO PINE CREEK IS SIZED ACCORDINGLY.
- SECTION OF PINE CREEK TO BE ELIMINATED.

PROPOSED TREATMENT FOR PINE CREEK CHANNEL:

REACH ID	PROPOSED TREATMENT **
PC 1	LEAVE NATURAL WITH MINOR BANK AND BED STABILIZATION.
PC 2	LEAVE NATURAL.
PC 3	LEAVE NATURAL WITH MINOR BANK AND BED STABILIZATION.
PC 4	REGRADE TO PROVIDE WIDE DEPRESSED AREA TO SERVE AS EMERGENCY RELIEF CHANNEL. CONSTRUCT 54" STORM DRAIN TO CONVEY 100 YEAR DESIGN FLOW.
PC 5	LEAVE NATURAL WITH BED AND BANK STABILIZATION.
PC 6	LEAVE NATURAL WITH BED AND BANK STABILIZATION.
PC 7	LEAVE NATURAL WITH BED AND BANK STABILIZATION.

** ACTUAL TREATMENT REQUIREMENT TO BE DETERMINED WITH FUTURE DETAILED HYDRAULIC ANALYSIS.
- NATURAL CHANNEL WILL REQUIRE MONITORING TO VERIFY PERFORMANCE AFTER DEVELOPMENT OCCURS.
- EXCEPT FOR THE REACHES NOTED ABOVE, PINE CREEK CHANNEL WILL BE BY-PASSED WITH STORM DRAIN CONVEYANCES AND ELIMINATED WITHIN THE STUDY AREA.

REGIONAL DETENTION FACILITY
DATA SUMMARY
FULLY DEVELOPED CONDITION

DETENTION FACILITY ID	PEAK INFLOW (cfs)	PEAK OUTFLOW (cfs)	ESTIMATED PEAK STORAGE (cu-ft)
A	102	275	4
B	223	596	19
C	255	1840	163
D	164	1073	97
E	307	724	197
F	289	378	170
G	120	1747	166
No. 1	1297	2809	488

ANALYSIS POINT DATA SUMMARY
FULLY DEVELOPED CONDITION

ANALYSIS POINT A	WATERSHED AREA (acres)	Q5 (cfs)	Q100 (cfs)	POINT DESCRIPTION
AP1	156	65	882	TOTAL FLOW
AP2	255	0.40	556	TOTAL FLOW
AP3	421	0.58	532	TOTAL FLOW
AP4	427	0.73	770	TOTAL FLOW
AP5	589	0.52	289	TOTAL FLOW
AP6	640	1.20	180	TOTAL FLOW
AP7	800	1.25	307	TOTAL FLOW
AP8	866	1.35	181	TOTAL FLOW
AP9	1705	1.42	524	TOTAL FLOW
AP10	3501	0.47	484	TOTAL FLOW
AP11	450	0.75	532	TOTAL FLOW
AP12	458	0.75	532	TOTAL FLOW
AP13	458	0.75	532	TOTAL FLOW
AP14	422	0.68	549	TOTAL FLOW
AP15	450	0.75	532	TOTAL FLOW
AP16	458	0.75	532	TOTAL FLOW
AP17	458	0.75	532	TOTAL FLOW
AP18	458	0.75	532	TOTAL FLOW
AP19	458	0.75	532	TOTAL FLOW
AP20	458	0.75	532	TOTAL FLOW
AP21	458	0.75	532	TOTAL FLOW
AP22	458	0.75	532	TOTAL FLOW
AP23	458	0.75	532	TOTAL FLOW
AP24	458	0.75	532	TOTAL FLOW
AP25	458	0.75	532	TOTAL FLOW
AP26	458	0.75	532	TOTAL FLOW
AP27	458	0.75	532	TOTAL FLOW
AP28	458	0.75	532	TOTAL FLOW
AP29	458	0.75	532	TOTAL FLOW
AP30	458	0.75	532	TOTAL FLOW
AP31	458	0.75	532	TOTAL FLOW
AP32	458	0.75	532	TOTAL FLOW
AP33	458	0.75	532	TOTAL FLOW
AP34	458	0.75	532	TOTAL FLOW
AP35	458	0.75	532	TOTAL FLOW
AP36	458	0.75	532	TOTAL FLOW
AP37	458	0.75	532	TOTAL FLOW
AP38	458	0.75	532	TOTAL FLOW
AP39	458	0.75	532	TOTAL FLOW
AP40	458	0.75	532	TOTAL FLOW
AP41	458	0.75	532	TOTAL FLOW
AP42	458	0.75	532	TOTAL FLOW
AP43	458	0.75	532	TOTAL FLOW
AP44	458	0.75	532	TOTAL FLOW
AP45	458	0.75	532	TOTAL FLOW
AP46	458	0.75	532	TOTAL FLOW
AP47	458	0.75	532	TOTAL FLOW
AP48	458	0.75	532	TOTAL FLOW
AP49	458	0.75	532	TOTAL FLOW
AP50	458	0.75	532	TOTAL FLOW
AP51	458	0.75	532	TOTAL FLOW
AP52	458	0.75	532	TOTAL FLOW
AP53	458	0.75	532	TOTAL FLOW
AP54	458	0.75	532	TOTAL FLOW
AP55	458	0.75	532	TOTAL FLOW
AP56	458	0.75	532	TOTAL FLOW
AP57	458	0.75	532	TOTAL FLOW
AP58	458	0.75	532	TOTAL FLOW
AP59	458	0.75	532	TOTAL FLOW
AP60	458	0.75	532	TOTAL FLOW
AP61	458	0.75	532	TOTAL FLOW
AP62	458	0.75	532	TOTAL FLOW
AP63	458	0.75	532	TOTAL FLOW
AP64	458	0.75	532	TOTAL FLOW
AP65	458	0.75	532	TOTAL FLOW
AP66	458	0.75	532	TOTAL FLOW
AP67	458	0.75	532	TOTAL FLOW
AP68	458	0.75	532	TOTAL FLOW
AP69	458	0.75	532	TOTAL FLOW
AP70	458	0.75	532	TOTAL FLOW
AP71	458	0.75	532	TOTAL FLOW
AP72	458	0.75	532	TOTAL FLOW
AP73	458	0.75	532	TOTAL FLOW
AP74	458	0.75	532	TOTAL FLOW
AP75	458	0.75	532	TOTAL FLOW
AP76	458	0.75	532	TOTAL FLOW
AP77	458	0.75	532	TOTAL FLOW
AP78	458	0.75	532	TOTAL FLOW
AP79	458	0.75	532	TOTAL FLOW
AP80	458	0.75	532	TOTAL FLOW
AP81	458	0.75	532	TOTAL FLOW
AP82	458	0.75	532	TOTAL FLOW
AP83	458	0.75	532	TOTAL FLOW
AP84	458	0.75	532	TOTAL FLOW
AP85	458	0.75	532	TOTAL FLOW
AP86	458	0.75	532	TOTAL FLOW
AP87	458	0.75	532	TOTAL FLOW
AP88	458	0.75	532	TOTAL FLOW
AP89	458	0.75	532	TOTAL FLOW
AP90	458	0.75	532	TOTAL FLOW
AP91	458	0.75	532	TOTAL FLOW
AP92	458	0.75	532	TOTAL FLOW
AP93	458	0.75	532	TOTAL FLOW
AP94	458	0.75	532	TOTAL FLOW
AP95	458	0.75	532	TOTAL FLOW
AP96	458	0.75	532	TOTAL FLOW
AP97	458	0.75	532	TOTAL FLOW
AP98	458	0.75	532	TOTAL FLOW
AP99	458	0.75	532	TOTAL FLOW
AP100	458	0.75	532	TOTAL FLOW

ANALYSIS POINTS NOTE:
ANALYSIS POINTS CONTAINED IN THE HEC-1 MODEL AND IN THE ABOVE TABLE ARE SHOWN ON THE MAP WITHOUT THE PREFIX "AP."

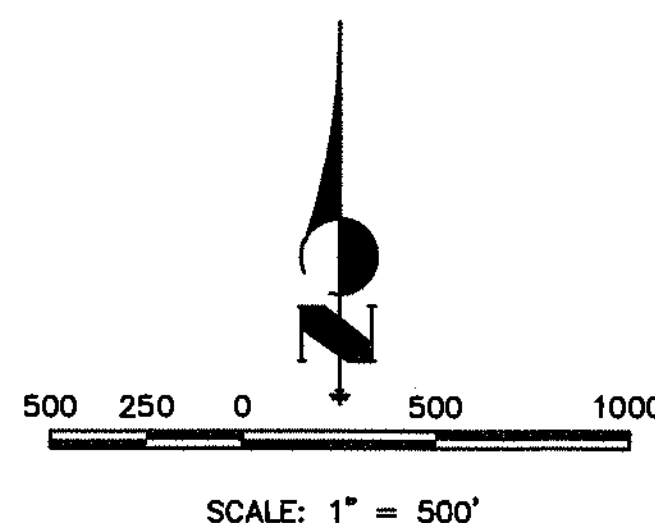
SUB-BASIN DATA SUMMARY
FULLY DEVELOPED CONDITION

BASIN	AREA (acres)	TC (min)	LAG (min)	ON (min)	PEAK RUNOFF (cfs)
PM1	83.0	0.15	13.0	0.100	65
PM2	50.0	0.078	21.4	0.214	40
PM3	45.0	0.043	13.1	0.141	40
PM4	33.9	0.053	18.1	0.181	30
PM5	34.0	0.053	19.1	0.191	40
PM6	45.0	0.100	12.1	0.121	40
PM7	25.0	0.039	17.1	0.171	24
PM8	33.0	0.114	21.5	0.215	30
PM9	24.5	0.038	19.7	0.197	30
PM10	41.0	0.084	12.6	0.126	40
PM11	24.5	0.038	19.7	0.197	30
PM12	33.5	0.052	13.7	0.137	30
PM13	34.5	0.054	20.3	0.203	40
PM14	88.8	0.154	31.0	0.310	31
PM15	30.0	0.051	24.6	0.246	30
PM16	56.5	0.088	11.0	0.110	88.0
PM17	88.0	0.138	35.4	0.353	68
PM18	8.7	0.014	10.0	0.100	10
PM19	43.5	0.058	12.0	0.120	30
PM20	31.0	0.048	9.2	0.092	102
PM21	27.0	0.042	8.8	0.088	67
PM22	45.0	0.053	19.1	0.191	40
PM23	105.0	0.184	18.8	0.188	80.2
PM24	19.4	0.016	12.4	0.124	19
PM25	52.9	0.083	19.6	0.196	55.8
PM26	73.0	0.114	18.5	0.185	78.5
PM27	17.3	0.014	12.4	0.124	17
PM28	228.6	0.146	12.7	0.127	283
PM29	48.7	0.016	18.5	0.185	48.7
PM30	24.38	0.011	7.7	0.077	24
PM31	102	0.16	110	0.288	102
PM32	173	0.27	161	0.317	173
PM33	198	0.31	194	0.331	198
PM34	NA	NA	NA	NA	NA
PM35	237	0.37	228	0.309	237
PM36	NA	NA	NA	NA	NA
PM37	284	0.46	281	0.386	284
PM38	2835	4.43	287	2829	2835
PM39	2835	4.43	287	2829	2835
PM40	2835	4.43	287	2829	2835
PM41	2835	4.43	287	2829	2835
PM42	2835	4.43	287	2829	2835
PM43	2835	4.43	287	2829	2835
PM44	2835	4.43	287	2829	2835
PM45	2835	4.43	287	2829	2835
PM46	2835	4.43	287	2829	2835
PM47	2835	4.43	287	2829	2835
PM48	2835	4.43	287	2829	2835
PM49	2835	4.43	287	2829	2835
PM50	2835	4.43	287	2829	2835
PM51	2835	4.43	287	2829	2835
PM52	2835	4.43	287	2829	2835
PM53	2835	4.43	287	2829	2835
PM54	2835	4.43	287	2829	2835
PM55	2835	4.43	287	2829	2835
PM56	2835	4.43	287	2829	2835
PM57	2835	4.43	287	2829	2835
PM58	2835	4.43	287	2829	2835
PM59	2835	4.43	287	2829	2835
PM60	2835	4.43	287	2829	2835
PM61	2835	4.43	287	2829	2835
PM62	2835	4.43	287	2829	2835
PM63	2835	4.43	287	2829	2835
PM64	2835	4.43	287	2829	2835
PM65	2835	4.43	287	2829	2835
PM66	2835	4.43	287	2829	2835
PM67	2835	4.43	287	2829	2835
PM68	2835	4.43	287	2829	2835
PM69	2835	4.43	287	2829	2835
PM70	2835	4.43	287	2829	2835
PM71	2835	4.43	287	2829	2835
PM72	2835	4.43	287	2829	2835
PM73	2835	4.43	287	2829	2835
PM74	2835	4.43	287	2829	2835
PM75	2835	4.43	287	2829	2835
PM76	2835	4.43	287	2829	2835
PM77	2835	4.43	287	2829	2835
PM78	2835	4.43	287	2829	2835
PM79	2835	4.43	287	2829	2835
PM80	2835	4.43	287	2829	2835
PM81	2835	4.43	287	2829	2835
PM82	2835	4.43	287	2829	2835
PM83	2835	4.43	287	2829	2835
PM84	2835	4.43	287	2829	2835
PM85	2835	4.43	287	2829	2835
PM86	2835	4.43	287	2829	2835
PM87	2835	4.43	287	2829	2835
PM88	2835	4.43	287	2829	2835
PM89	2835	4.43	287	2829	2835
PM90	2835	4.43	287	2829	2835
PM91	2835	4.43	287	2829	2835
PM92	2835	4.43	287	2829	2835
PM93	2835	4.43	287	2829	2835
PM94	2835	4.43	287	2829	2835
PM95	2835	4.43	287	2829	2835
PM96	2835	4.43	287	2829	2835
PM97	2835	4.43	287	2829	2835
PM98	2835	4.43	287	2829	2835
PM99	2835	4.43	287	2829	2835
PM100	2835	4.43	287	2829	2835

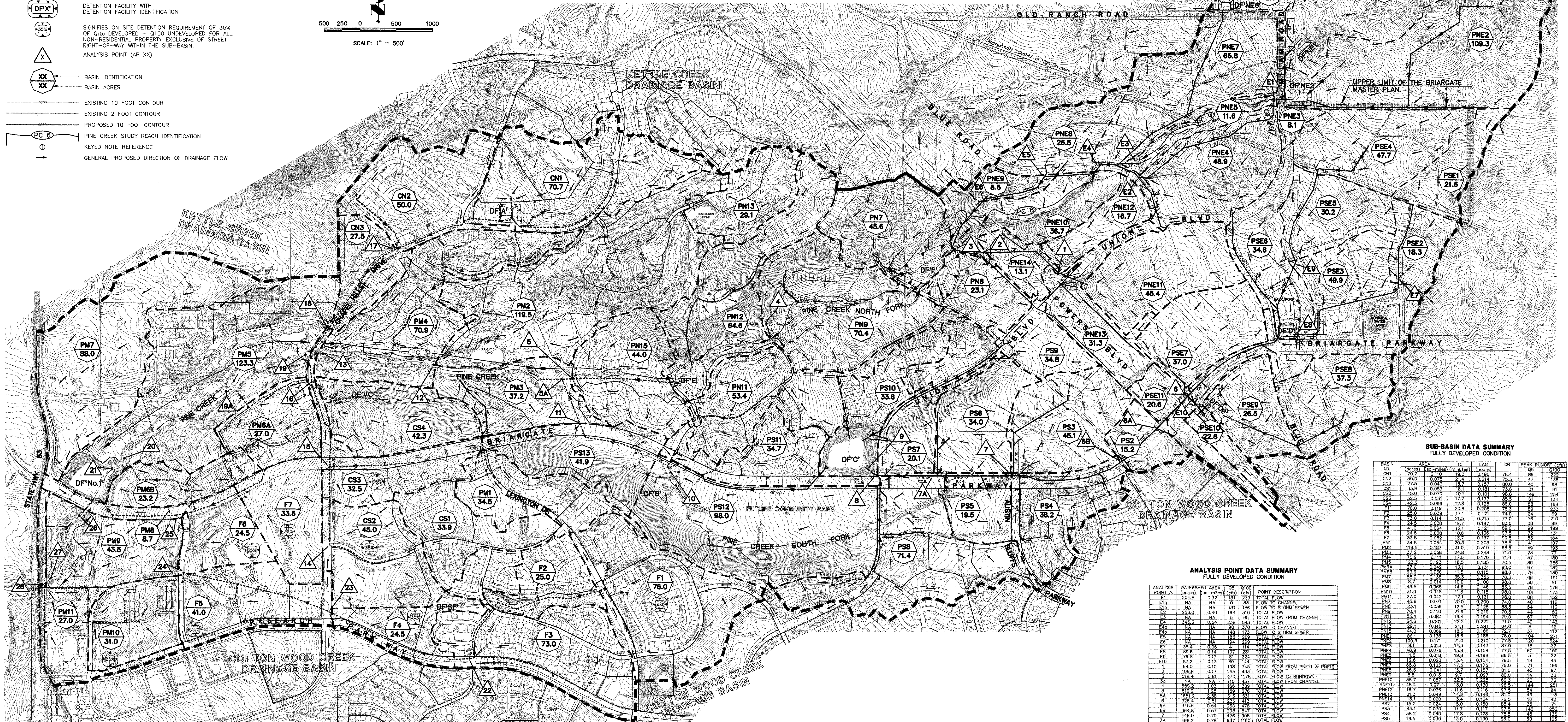
SCALE: 1" = 500'
PINE CREEK DRAINAGE BASIN
FULLY DEVELOPED CONDITION BASIN MAP
& MASTER PLAN 10/12/98

LEGEND

- CURRENT MAJOR DRAINAGE BASIN BOUNDARY
- CURRENT SUB-BASIN BOUNDARY
- PREVIOUS MAJOR DRAINAGE BASIN BOUNDARY (AMENDMENT 2)
- LIMIT OF CURRENT STUDY
- UPPER LIMIT BRIARGATE MASTER PLAN
- EXISTING STORM DRAIN
- PROPOSED STORM DRAIN
- DF'X' DETENTION FACILITY WITH DETENTION FACILITY IDENTIFICATION
- DF'X' SIGNIFIES ON SITE DETENTION REQUIREMENT OF 35% OF Q100 DEVELOPED - Q100 UNDEVELOPED FOR ALL NON-RESIDENTIAL PROPERTY EXCLUSIVE OF STREET RIGHT-OF-WAY WITHIN THE SUB-BASIN.
- XX BASIN IDENTIFICATION
- XX BASIN ACRES
- EXISTING 10 FOOT CONTOUR
- EXISTING 2 FOOT CONTOUR
- PROPOSED 10 FOOT CONTOUR
- PC 6 PINE CREEK STUDY REACH IDENTIFICATION
- KEYED NOTE REFERENCE
- GENERAL PROPOSED DIRECTION OF DRAINAGE FLOW



AMENDMENT 3 TO PINE CREEK BASIN PLANNING STUDY FULLY DEVELOPED CONDITION BASIN MAP AND MASTER PLAN



SUB-BASIN DATA SUMMARY
FULLY DEVELOPED CONDITION

BASIN ID	AREA (acres)	AREA (sq-miles)	TC (minutes)	LAG (hours)	Q100 (cfs)	PEAK RUNOFF (cfs)
1	1.0	0.02	1.0	0.00	1.0	1.0
2	1.0	0.02	1.0	0.00	1.0	1.0
3	1.0	0.02	1.0	0.00	1.0	1.0
4	1.0	0.02	1.0	0.00	1.0	1.0
5	1.0	0.02	1.0	0.00	1.0	1.0
6	1.0	0.02	1.0	0.00	1.0	1.0
7	1.0	0.02	1.0	0.00	1.0	1.0
8	1.0	0.02	1.0	0.00	1.0	1.0
9	1.0	0.02	1.0	0.00	1.0	1.0
10	1.0	0.02	1.0	0.00	1.0	1.0
11	1.0	0.02	1.0	0.00	1.0	1.0
12	1.0	0.02	1.0	0.00	1.0	1.0
13	1.0	0.02	1.0	0.00	1.0	1.0
14	1.0	0.02	1.0	0.00	1.0	1.0
15	1.0	0.02	1.0	0.00	1.0	1.0
16	1.0	0.02	1.0	0.00	1.0	1.0
17	1.0	0.02	1.0	0.00	1.0	1.0
18	1.0	0.02	1.0	0.00	1.0	1.0
19	1.0	0.02	1.0	0.00	1.0	1.0
20	1.0	0.02	1.0	0.00	1.0	1.0
21	1.0	0.02	1.0	0.00	1.0	1.0
22	1.0	0.02	1.0	0.00	1.0	1.0
23	1.0	0.02	1.0	0.00	1.0	1.0
24	1.0	0.02	1.0	0.00	1.0	1.0
25	1.0	0.02	1.0	0.00	1.0	1.0
26	1.0	0.02	1.0	0.00	1.0	1.0
27	1.0	0.02	1.0	0.00	1.0	1.0
28	1.0	0.02	1.0	0.00	1.0	1.0
29	1.0	0.02	1.0	0.00	1.0	1.0
30	1.0	0.02	1.0	0.00	1.0	1.0
31	1.0	0.02	1.0	0.00	1.0	1.0
32	1.0	0.02	1.0	0.00	1.0	1.0
33	1.0	0.02	1.0	0.00	1.0	1.0
34	1.0	0.02	1.0	0.00	1.0	1.0
35	1.0	0.02	1.0	0.00	1.0	1.0
36	1.0	0.02	1.0	0.00	1.0	1.0
37	1.0	0.02	1.0	0.00	1.0	1.0
38	1.0	0.02	1.0	0.00	1.0	1.0
39	1.0	0.02	1.0	0.00	1.0	1.0
40	1.0	0.02	1.0	0.00	1.0	1.0
41	1.0	0.02	1.0	0.00	1.0	1.0
42	1.0	0.02	1.0	0.00	1.0	1.0
43	1.0	0.02	1.0	0.00	1.0	1.0
44	1.0	0.02	1.0	0.00	1.0	1.0
45	1.0	0.02	1.0	0.00	1.0	1.0
46	1.0	0.02	1.0	0.00	1.0	1.0
47	1.0	0.02	1.0	0.00	1.0	1.0
48	1.0	0.02	1.0	0.00	1.0	1.0
49	1.0	0.02	1.0	0.00	1.0	1.0
50	1.0	0.02	1.0	0.00	1.0	1.0
51	1.0	0.02	1.0	0.00	1.0	1.0
52	1.0	0.02	1.0	0.00	1.0	1.0
53	1.0	0.02	1.0	0.00	1.0	1.0
54	1.0	0.02	1.0	0.00	1.0	1.0
55	1.0	0.02	1.0	0.00	1.0	1.0
56	1.0	0.02	1.0	0.00	1.0	1.0
57	1.0	0.02	1.0	0.00	1.0	1.0
58	1.0	0.02	1.0	0.00	1.0	1.0
59	1.0	0.02	1.0	0.00	1.0	1.0
60	1.0	0.02	1.0	0.00	1.0	1.0
61	1.0	0.02	1.0	0.00	1.0	1.0
62	1.0	0.02	1.0	0.00	1.0	1.0
63	1.0	0.02	1.0	0.00	1.0	1.0
64	1.0	0.02	1.0	0.00	1.0	1.0
65	1.0	0.02	1.0	0.00	1.0	1.0
66	1.0	0.02	1.0	0.00	1.0	1.0
67	1.0	0.02	1.0	0.00	1.0	1.0
68	1.0	0.02	1.0	0.00	1.0	1.0
69	1.0	0.02	1.0	0.00	1.0	1.0
70	1.0	0.02	1.0	0.00	1.0	1.0
71	1.0	0.02	1.0	0.00	1.0	1.0
72	1.0	0.02	1.0	0.00	1.0	1.0
73	1.0	0.02	1.0	0.00	1.0	1.0
74	1.0	0.02	1.0	0.00	1.0	1.0
75	1.0	0.02	1.0	0.00	1.0	1.0
76	1.0	0.02	1.0	0.00	1.0	1.0
77	1.0	0.02	1.0	0.00	1.0	1.0
78	1.0	0.02	1.0	0.00	1.0	1.0
79	1.0	0.02	1.0	0.00	1.0	1.0
80	1.0	0.02	1.0	0.00	1.0	1.0
81	1.0	0.02	1.0	0.00	1.0	1.0
82	1.0	0.02	1.0	0.00	1.0	1.0
83	1.0	0.02	1.0	0.00	1.0	1.0
84	1.0	0.02	1.0	0.00	1.0	1.0
85	1.0	0.02	1.0	0.00	1.0	1.0
86	1.0	0.02	1.0	0.00	1.0	1.0
87	1.0	0.02	1.0	0.00	1.0	1.0
88	1.0	0.02	1.0	0.00	1.0	1.0
89	1.0	0.02	1.0	0.00	1.0	1.0
90	1.0	0.02	1.0	0.00	1.0	1.0
91	1.0	0.02	1.0	0.00	1.0	1.0
92	1.0	0.02	1.0	0.00	1.0	1.0
93	1.0	0.02	1.0	0.00	1.0	1.0
94	1.0	0.02	1.0	0.00	1.0	1.0
95	1.0	0.02	1.0	0.00	1.0	1.0
96	1.0	0.02	1.0	0.00	1.0	1.0
97	1.0	0.02	1.0	0.00	1.0	1.0
98	1.0	0.02	1.0	0.00	1.0	1.0
99	1.0	0.02	1.0	0.00	1.0	1.0
100	1.0	0.02	1.0	0.00	1.0	1.0

ANALYSIS POINT DATA SUMMARY
FULLY DEVELOPED CONDITION

ANALYSIS POINT A	WATERSHED AREA (acres)	Q5 (cfs)	Q100 (cfs)	POINT DESCRIPTION
1	1.0	1.0	1.0	TOTAL FLOW
2	1.0	1.0	1.0	TOTAL FLOW
3	1.0	1.0	1.0	TOTAL FLOW
4	1.0	1.0	1.0	TOTAL FLOW
5	1.0	1.0	1.0	TOTAL FLOW
6	1.0	1.0	1.0	TOTAL FLOW
7	1.0	1.0	1.0	TOTAL FLOW
8	1.0	1.0	1.0	TOTAL FLOW
9	1.0	1.0	1.0	TOTAL FLOW
10	1.0	1.0	1.0	TOTAL FLOW
11	1.0	1.0	1.0	TOTAL FLOW
12	1.0	1.0	1.0	TOTAL FLOW
13	1.0	1.0	1.0	TOTAL FLOW
14	1.0	1.0	1.0	TOTAL FLOW
15	1.0	1.0	1.0	TOTAL FLOW
16	1.0	1.0	1.0	TOTAL FLOW
17	1.0	1.0	1.0	TOTAL FLOW
18	1.0	1.0	1.0	TOTAL FLOW
19	1.0	1.0	1.0	TOTAL FLOW
20	1.0	1.0	1.0	TOTAL FLOW
21	1.0	1.0	1.0	TOTAL FLOW
22	1.0	1.0	1.0	TOTAL FLOW
23	1.0	1.0	1.0	TOTAL FLOW
24	1.0	1.0	1.0	TOTAL FLOW
25	1.0	1.0	1.0	TOTAL FLOW
26	1.0	1.0	1.0	TOTAL FLOW
27	1.0	1.0	1.0	TOTAL FLOW
28	1.0	1.0	1.0	TOTAL FLOW
29	1.0	1.0	1.0	TOTAL FLOW
30	1.0	1.0	1.0	TOTAL FLOW
31	1.0	1.0	1.0	TOTAL FLOW
32	1.0	1.0	1.0	TOTAL FLOW
33	1.0	1.0	1.0	TOTAL FLOW
34	1.0	1.0	1.0	TOTAL FLOW
35	1.0	1.0	1.0	TOTAL FLOW
36	1.0	1.0	1.0	TOTAL FLOW
37	1.0	1.0	1.0	TOTAL FLOW
38	1.0	1.0	1.0	TOTAL FLOW
39	1.0	1.0	1.0	TOTAL FLOW
40	1.0	1.0	1.0	TOTAL FLOW
41	1.0	1.0	1.0	TOTAL FLOW
42	1.0	1.0	1.0	TOTAL FLOW
43	1.0	1.0	1.0	TOTAL FLOW
44	1.0	1.0	1.0	TOTAL FLOW
45	1.0	1.0	1.0	TOTAL FLOW
46	1.0	1.0	1.0	TOTAL FLOW
47	1.0	1.0	1.0	TOTAL FLOW
48	1.0	1.0	1.0	TOTAL FLOW
49	1.0	1.0	1.0	TOTAL FLOW
50	1.0	1.0	1.0	TOTAL FLOW
51	1.0	1.0	1.0	TOTAL FLOW
52	1.0	1.0	1.0	TOTAL FLOW
53	1.0	1.0	1.0	TOTAL FLOW
54	1.0	1.0	1.0	TOTAL FLOW
55	1.0	1.0	1.0	TOTAL FLOW
56	1.0	1.0	1.0	TOTAL FLOW
57	1.0	1.0	1.0	TOTAL FLOW
58	1.0	1.0	1.0	TOTAL FLOW
59	1.0	1.0	1.0	TOTAL FLOW
60	1.0	1.0	1.0	TOTAL FLOW
61	1.0	1.0	1.0	TOTAL FLOW
62	1.0	1.0	1.0	TOTAL FLOW
63	1.0	1.0	1.0	TOTAL FLOW
64	1.0	1.0	1.0	TOTAL FLOW
65	1.0	1.0	1.0	TOTAL FLOW
66	1.0	1.0	1.0	TOTAL FLOW
67	1.0	1.0	1.0	TOTAL FLOW
68	1.0	1.0	1.0	TOTAL FLOW
69	1.0	1.0	1.0	TOTAL FLOW
70	1.0	1.0	1.0	TOTAL FLOW
71	1.0	1.0	1.0	TOTAL FLOW
72	1.0	1.0	1.0	TOTAL FLOW
73	1.0	1.0	1.0	TOTAL FLOW
74	1.0	1.0	1.0	TOTAL FLOW
75	1.0	1.0	1.0	TOTAL FLOW
76	1.0	1.0	1.0	TOTAL FLOW
77	1.0	1.0	1.0	TOTAL FLOW
78	1.0	1.0	1.0	TOTAL FLOW
79	1.0	1.0	1.0	TOTAL FLOW
80	1.0	1.0	1.0	TOTAL FLOW
81	1.0	1.0	1.0	TOTAL FLOW
82	1.0	1.0	1.0	TOTAL FLOW
83	1.0	1.0	1.0	TOTAL FLOW
84	1.0	1.0	1.0	TOTAL FLOW
85	1.0	1.0	1.0	TOTAL FLOW
86	1.0	1.0	1.0	TOTAL FLOW
87	1.0	1.0	1.0	TOTAL FLOW
88	1.0	1.0	1.0	TOTAL FLOW
89	1.0	1.0	1.0	TOTAL FLOW
90	1.0	1.0	1.0	TOTAL FLOW
91	1.0	1.0	1.0	TOTAL FLOW
92	1.0	1.0	1.0	TOTAL FLOW
93	1.0	1.0	1.0	TOTAL FLOW
94	1.0	1.0	1.0	TOTAL FLOW
95	1.0	1.0	1.0	TOTAL FLOW
96	1.0	1.0	1.0	TOTAL FLOW
97	1.0	1.0	1.0	TOTAL FLOW
98	1.0	1.0	1.0	TOTAL FLOW
99	1.0	1.0	1.0	TOTAL FLOW
100	1.0	1.0	1.0	TOTAL FLOW

GENERAL NOTES:

- FUTURE STORM SEWERS SHOWN ON THIS PLAN ARE ONLY INTENDED TO INDICATE GENERAL LOCATIONS AND APPROXIMATE SIZES OF FUTURE FACILITIES. ACTUAL STORM SEWERS SIZES AND LOCATIONS SHALL BE DETERMINED WITH MORE DETAILED ANALYSIS AT THE TIME OF DETAILED DESIGN OF THE FACILITIES. IT IS LIKELY THAT ADDITIONAL FACILITIES NOT SHOWN ON THIS PLAN WILL BE REQUIRED.
- PROPOSED DETENTION FACILITIES SHOWN ON THIS PLAN ARE ONLY INTENDED TO INDICATE GENERAL LOCATIONS AND LAND AREA REQUIRED FOR THESE FACILITIES. ACTUAL LOCATION AND LAND AREA REQUIRED SHALL BE DETERMINED AT THE TIME OF DETAILED DESIGN OF THE FACILITIES.
- EXCEPT AS OTHERWISE NOTED, THIS PLAN SHALL NOT MODIFY THE REQUIREMENTS OF PREVIOUSLY APPROVED MASTER DEVELOPMENT DRAINAGE PLANS AND FINAL DRAINAGE REPORTS.

KEYED NOTES:

- SECTION OF PINE CREEK TO BE ELIMINATED.
- FLOW IS TO BE DIVERTED TO A STORM SEWER IN FREQUENT EVENTS AND IS TO BE DIVIDED BETWEEN THE STORM SEWER AND NATURAL CHANNEL IN LARGER EVENTS.
- AN EMERGENCY OVERFLOW/RELIEF ROUTE SHOULD BE PLANNED ACROSS THIS SITE FROM THE LOW POINT OF TELSTAR DRIVE TO PINE CREEK.

PROPOSED TREATMENT FOR PINE CREEK CHANNEL:

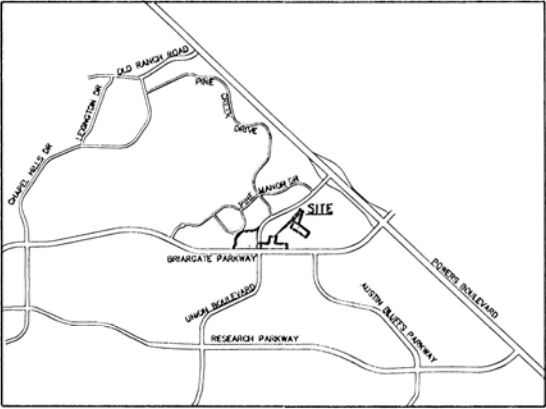
REACH ID	PROPOSED TREATMENT **
PC 1	LEAVE NATURAL WITH ONE DROP/CONTROL STRUCTURE. (COMPLETE)
PC 2	LEAVE NATURAL WITH MINOR BED STABILIZATION AND MODIFICATIONS TO DF No. 1 RUNDOWN CHANNEL.
PC 3	LEAVE NATURAL WITH GRADE CONTROL STRUCTURES.
PC 4	REGRADE TO PROVIDE WIDE DEPRESSED AREA TO SERVE AS EMERGENCY RELIEF CHANNEL. CONSTRUCT 54" STORM DRAIN TO CONVEY 100 YEAR DESIGN FLOW. (COMPLETE)
PC 5	LEAVE NATURAL WITH GRADE CONTROL STRUCTURES.
PC 6	LEAVE NATURAL WITH GRADE CONTROL STRUCTURES.
PC 7	LEAVE NATURAL WITH FREQUENT FLOWS CONVEYED IN BY-PASS STORM SEWER.
PC 8	LEAVE NATURAL. FREQUENT FLOWS CONVEYED IN BY-PASS STORM SEWER.
PC 9	LEAVE NATURAL WITH SOME RESHAPING. FREQUENT FLOWS CONVEYED IN BY-PASS STORM SEWER.

PINE CREEK DETENTION FACILITY "C"
CITY OF COLORADO SPRINGS, COUNTY OF EL PASO, STATE OF COLORADO
GRADING AND EROSION CONTROL PLANS
JULY 1998

GENERAL NOTES:

- IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY THE EXISTENCE AND LOCATION OF ALL UNDERGROUND UTILITIES ON AND ADJACENT TO THE SITE. THE OMISSION FROM OR THE INCLUSION OF UTILITY LOCATIONS ON THE PLANS SHALL NOT TO BE CONSTRUED AS THE NON-EXISTENCE OF OR A DEFINITE LOCATION OF EXISTING UNDERGROUND UTILITIES.
- THE CONTRACTOR WILL TAKE THE NECESSARY PRECAUTIONS TO PROTECT EXISTING UTILITIES, BUILDINGS, FENCES, AND ROADWAYS FROM DAMAGE DUE TO THIS OPERATION. ANY DAMAGE TO THE ABOVE WILL BE REPAIRED AT THE CONTRACTOR'S EXPENSE, AND ANY SERVICE DISRUPTION WILL BE SETTLED BY THE CONTRACTOR.
- OVERLOT GRADING SHALL BE COMPLETED TO A SUBGRADE TOLERANCE OF PLUS OR MINUS 0.2'.
- CONTRACTOR SHALL OBTAIN COPIES OF THE SOILS REPORT FROM THE GEOTECHNICAL ENGINEER AND KEPT ONSITE DURING ALL EARTHWORK OPERATIONS.
- THE SITE SHALL BE STRIPPED A MINIMUM OF 0.5' BELOW EXISTING GRADE AND THE TOPSOIL STOCKPILED ON OR OFFSITE FOR REUSE.
- MAXIMUM CUT/FILL SLOPES SHALL NOT EXCEED 3:1, UNLESS OTHERWISE NOTED.
- THE PRIMARY FUNCTION OF THIS FACILITY IS STORMWATER DETENTION. AS SUCH IT WILL BE EXPECTED TO ACT AS A DAM FOR PERIOD DURING AND FOLLOWING ANY MAJOR STORM. ANY USE OR ACTIVITY THAT WOULD COMPROMISE THIS FUNCTION SHOULD BE CAREFULLY CONTROLLED, I.E. USES THAT ENTAIL OBJECTS THAT COULD CLOG THE SPILLWAY OR COMPROMISE THE BERM OR OUTLET SPILLWAY AREA.
- BENCHMARKS:

- 92' CUT SQUARE ON TOP OF CURB ON BRIARGATE PARKWAY APPROXIMATELY 300±' EAST OF THE INTERSECTION OF BRIARGATE PARKWAY AND LEXINGTON DRIVE.
E.L. = 6798.71
- THE SOUTH 1/4 CORNER OF SECTION 27 BEING A 3-1/4" ALUMINUM CAP STAMPED L.S. 10958 APPROXIMATELY 2540' EAST OF THE EXISTING END OF CURB ON BRIARGATE PARKWAY AND APPROXIMATELY 660' NORTH OF THE SAME.
E.L. = 6823.58

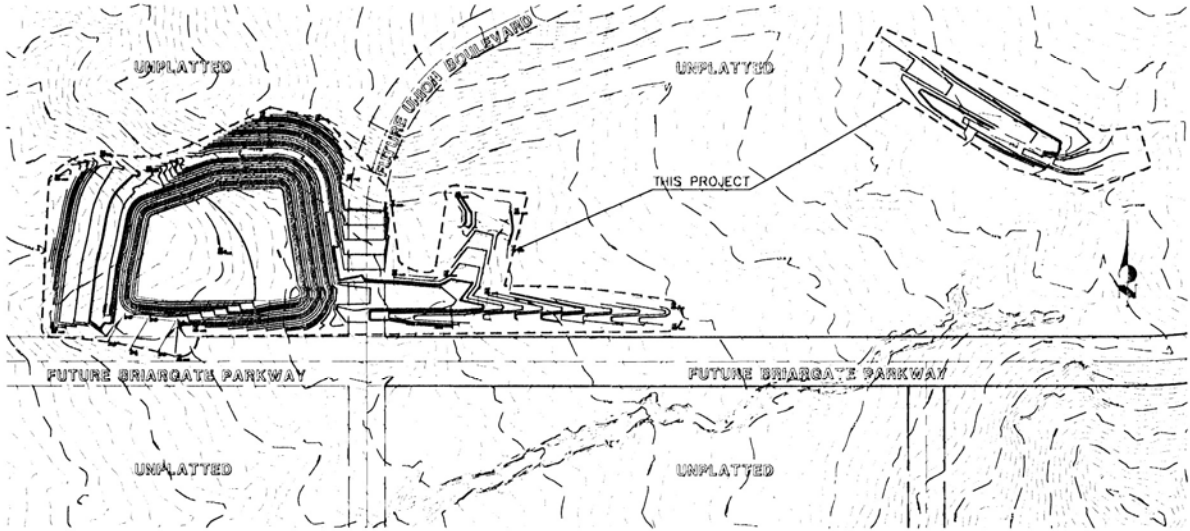


VICINITY MAP
NTS

EROSION CONTROL CRITERIA:

EROSION AND SEDIMENT CONTROL SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR. EROSION CONTROL MEASURES SHALL BE IMPLEMENTED IN A MANNER THAT WILL PROTECT PROPERTIES AND PUBLIC FACILITIES FROM ADVERSE EFFECTS OF EROSION AND SEDIMENTATION AS A RESULT OF CONSTRUCTION AND EARTH ACTIVITIES WITHIN THE PROJECT SITE.

- INSTALL ALL EROSION CONTROL MEASURES INDICATED ON THE EROSION CONTROL EROSION PLAN PRIOR TO ANY EARTHWORK DISTURBANCE. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ADDITIONAL EROSION CONTROL MEASURES INCIDENTAL TO THE WORK.
- THE CONTRACTOR SHALL CHECK ALL EROSION CONTROL MEASURES AFTER EVERY RAINFALL. ALL NECESSARY REPAIRS OR REPLACEMENT SHALL BE DONE IMMEDIATELY.
- SEDIMENT TRAPPED BY CHECKDAMS, SEDIMENT BASINS AND SILT FENCES SHALL BE PERIODICALLY REMOVED AS NECESSARY TO ENSURE PROPER FUNCTION PROPER FUNCTION OF THESE MEASURES.
- ALL NECESSARY EROSION AND SEDIMENT CONTROL MEASURES SHALL REMAIN IN PLACE AND MAINTAINED UNTIL SUCH TIME AS THE EROSION AND SEDIMENTATION POTENTIAL IS MITIGATED AND THE SITE DEEMED STABLE BY REVIEW AUTHORITIES. AT SUCH TIME THE CONTRACTOR SHALL REMOVE ALL EROSION CONTROL DEVICES, COLLECTED DEBRIS AND SEDIMENT FROM THE SITE AND AND DISPOSE OF ALL SUCH MATERIALS IN AN ACCEPTABLE MANNER.



INDEX MAP
SCALE 1" = 300'

EROSION CONTROL COST OPINION:

1. 9 EACH - STRAW BALE FOR CHECK DAMS @ \$4.00/BALE	\$ 108
3. 1440 LF SILT FENCE @ \$1.00/LF	\$ 1440
4. 25% MAINTENANCE AND REPLACEMENT	\$ 387
5. 22.0 AC. OF RESEEDING @ \$500.00/AC.	\$ 11000
TOTAL	\$ 12935

JR ENGINEERING, LTD. CANNOT AND DOES NOT GUARANTEE THAT THE CONSTRUCTION COSTS WILL NOT VARY FROM THESE OPINIONS OR PROBABLE CONSTRUCTION COSTS. THESE OPINIONS REPRESENT OUR BEST JUDGEMENT AS A DESIGN PROFESSIONAL FAMILIAR WITH THE CONSTRUCTION INDUSTRY AND IN THIS DEVELOPMENT.

AGENCIES:

DEVELOPER: L.P. 47, LLC dba
LA PLATA INVESTMENTS
7150 CAMPUS DRIVE, SUITE 365
COLORADO SPRINGS, COLORADO 80920
MR. BOB INGELS (719) 260-7477

CIVIL ENGINEER: JR ENGINEERING, LTD.
4935 NORTH 30TH STREET
COLORADO SPRINGS, COLORADO 80918
MR. FRANK TRIPI (719) 593-2593

ENGINEERING DIVISION: CITY OF COLORADO SPRINGS
101 W. COSTILLA STREET
COLORADO SPRINGS, COLORADO 80903
MR. TIM MITROS (719) 385-5061

WATER RESOURCES: WASTEWATER:
CITY OF COLORADO SPRINGS
111 S. CASCADE AVENUE, SUITE 201
COLORADO SPRINGS, COLORADO 80903
MR. JERRY VALLE (719) 448-8252

GAS DEPT: CITY OF COLORADO SPRINGS
101 S. CONEJOS STREET
COLORADO SPRINGS, COLORADO 80903
MR. DAVE DEUTSCH (719) 668-3520

ELECTRIC DEPT: CITY OF COLORADO SPRINGS
7710 DURANT DRIVE
COLORADO SPRINGS, COLORADO 80920
MR. DAN GIECK (719) 668-4962

TELEPHONE COMPANY: U.S. WEST COMMUNICATIONS
(LOCATORS) (800) 922-1987
A.T. & T.
(LOCATORS) (719) 635-3674

APPROVALS:

IF SUCH WORK IS PERFORMED IN ACCORDANCE WITH THE GRADING AND EROSION CONTROL PLAN, THE WORK WILL NOT BECOME A HAZARD TO LIFE AND LIMB, ENDANGER PROPERTY, OR ADVERSELY AFFECT THE SAFETY, USE, OR STABILITY OF A PUBLIC WAY, DRAINAGE CHANNEL, OR OTHER PROPERTY.

PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF OF
JR ENGINEERING, LTD.

Kyle H. Campbell
KYLE H. CAMPBELL, COLORADO P.E. 29794

11/10/98
DATE

THE OWNER WILL COMPLY WITH THE REQUIREMENTS OF THIS GRADING AND EROSION CONTROL PLAN.

Bob Tripi
OWNER

11/12/98
DATE

THIS GRADING PLAN IS FILED IN ACCORDANCE WITH SECTION 15-3-1503 (ENACTED AS ORD. 82-56) OF THE CODE OF THE CITY OF COLORADO SPRINGS, 1980, AS AMENDED. EROSION CONTROL IS REVIEWED IN ACCORDANCE WITH SECTION 4.9 OF THE DRAINAGE CRITERIA MANUAL, OCTOBER 1991, LATEST REVISION.

Tim Mitros
CITY ENGINEER, CITY OF COLORADO SPRINGS

12/14/98
DATE

SHEET INDEX

TITLE SHEET
GRADING PLAN & EROSION CONTROL PLAN
DROP STRUCTURE

SHEET 1 OF 4
SHEET 2 & 3 OF 4
SHEET 4 OF 4

UNLESS SHOWN OTHERWISE, ALL DIMENSIONS ARE APPROVED BY THE APPROPRIATE REVIEWING AGENCIES, JR ENGINEERING, LTD. FOR THE PURPOSES DESIGNATED BY WRITTEN AUTHORIZATION.

48 HOURS BEFORE YOU DIG,
CALL UTILITY LOCATORS
1-800-922-1987
CITY OF COLORADO SPRINGS DEPT. OF UTILITIES
GAS, ELECTRIC, WATER AND WASTEWATER

JR Engineering, Ltd.
4855 North 30th Street
Colorado Springs, Colorado 80918
(719) 593-2593 • FAX (719) 528-6613

NO.	SCALE	DATE	DES. BY	CHK. BY	DWN. BY
1	NONE	7/9/98	TDS	JRB	JAC

PINE CREEK DETENTION FACILITY "C"	GRADING AND EROSION CONTROL PLANS	TITLE SHEET
SHEET 1 OF 4		

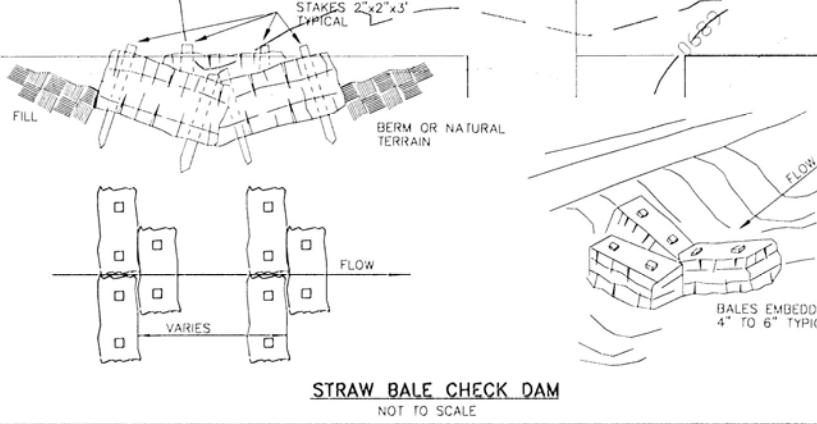
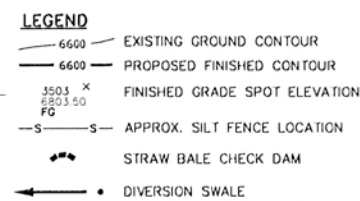
JOB NO.
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THE EMERGENCY SPILLWAY WILL PASS 1850 cfs AT A FLOW DEPTH OF 2.5 ft

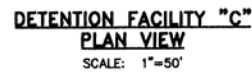
48 HOURS BEFORE YOU DIG,
CALL UTILITY LOCATORS
1-800-922-1987
CITY OF COLORADO SPRINGS DEPT. OF UTILITIES
GAS, ELECTRIC, WATER AND WASTEWATER

NO.	REVISION	BY	DATE
SCALE 1"=50'			
DATE 7/9/98			
DES. BY WF/TDS			
CHK. BY JRS			
DWN. BY JAC			

PINE CREEK DETENTION FACILITY "C"	
GRADING AND EROSION CONTROL PLANS	
SHEET 2 OF 4	
JOB NO.	8716.20



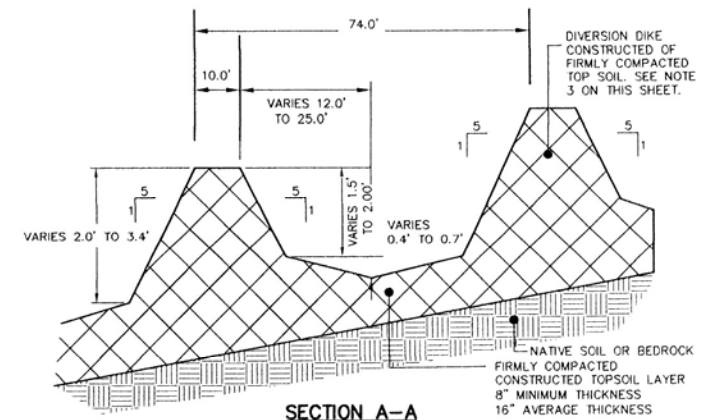
Kyle R. Campbell 11.11.98
KYLE R. CAMPBELL, COLORADO P. 11.11.98
Powers Bridge Project
Page 43



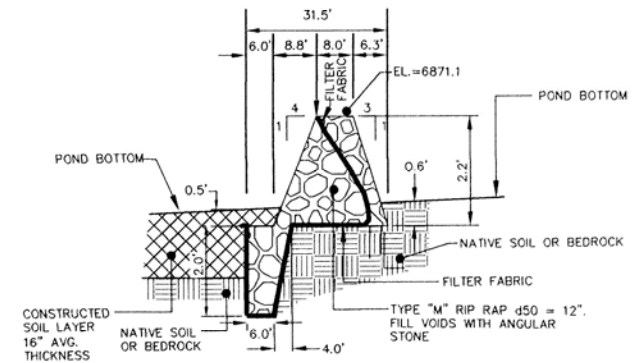
1. ALL MATERIALS AND INSTALLATION PROCEDURES SHALL BE IN COMPLIANCE WITH THE CITY OF COLORADO SPRINGS, ENGINEERING DIVISION SUBDIVISION POLICY MANUAL AND STANDARD SPECIFICATIONS.
2. MAJOR GRADING AND INLET AND OUTLET FACILITIES ARE TO BE CONSTRUCTED PER THE PLANS FOR "BRIARGATE PARKWAY STORM DRAIN" AS REVISED JULY 2003, BY J.R. ENGINEERING, THE PROPOSED WETLAND MITIGATION AREA SHALL BE GRADED PER THIS PLAN.
3. THE ENTIRE AREA SHOWN TO BE PLANTED WITH WETLAND FORBS OR WILLOWS SHALL BE OVER-EXCAVATED BY 15" AVERAGE, 8" MINIMUM DEPTH, WITH TOP SOIL. THE SITE SHALL CONTAIN SUFFICIENT ORGANIC MATTER TO SUPPORT THE PROPOSED PLANTS. THE SOIL SHALL BE COMPACTED FIRM ENOUGH TO RETAIN FORM AND RESIST EROSION BUT SHALL BE LOOSE ENOUGH TO ALLOW PLANT GROWTH.
4. PROPOSED CONTOURS ARE NOT SHOWN ON THE POND BOTTOM FOR CLARITY.
5. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY THE EXISTENCE AND LOCATION OF ALL ABOVE GROUND AND UNDERGROUND UTILITIES ALONG THE ROUTE AND THE WORK SHALL BE STOPPED FROM PROCEEDING IF THE UTILITY LOCATIONS ON THE PLANS IS NOT BE CONSIDERED AS THE NONEXISTENCE OF OR A DEFINITE LOCATION OF EXISTING ABOVE GROUND AND UNDERGROUND UTILITIES.
6. THE CONTRACTOR WILL TAKE THE NECESSARY PRECAUTIONS TO PROTECT EXISTING UTILITIES FROM DAMAGE DUE TO THIS OPERATION, ANY DAMAGE TO EXISTING UTILITIES SHALL BE REPAIRED AT THE CONTRACTORS EXPENSE, AND ANY SERVICE DISRUPTION WILL BE SETTLED BY THE CONTRACTOR.

QUESTIONS REGARDING PLANTING SHOULD BE DIRECTED
TO TRENT MILLER OF SWCA (303) 487-1183.

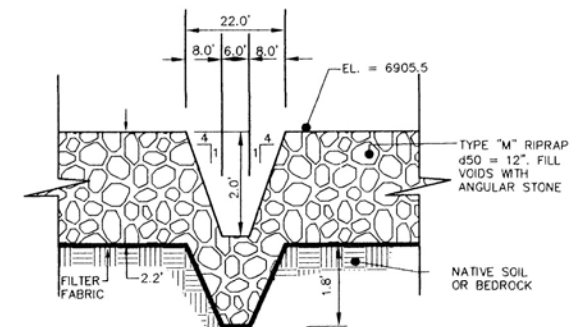
Received: Tim White 10/27/03



SECTION A-A
TYPICAL DIVERSION DIKE/SWALE
N.T.S.



SECTION B-B
RIP-RAP SEDIMENT TRAP BERM
N.T.S.



SECTION C-C
LOW-FLOW NOTCH THROUGH
SEDIMENT TRAP BERM
N.T.S.

Vancel Fossinger Powers Bridge Project
VANCEL S. FOSSINGER, COLORADO P.E. 131872 Page 45 DATE SHE

J·R ENGINEERING
Subsidiary of Westman



DESIGNED BY	VSF	DATE	09/29/03
DRAWN BY	KWS	V-SCALE	
CHECKED BY	<i>WJF</i>	V-VARIES	

PINE CREEK DETENTION FACILITY C

WEILAND GRADING AND PLANNING PLAN

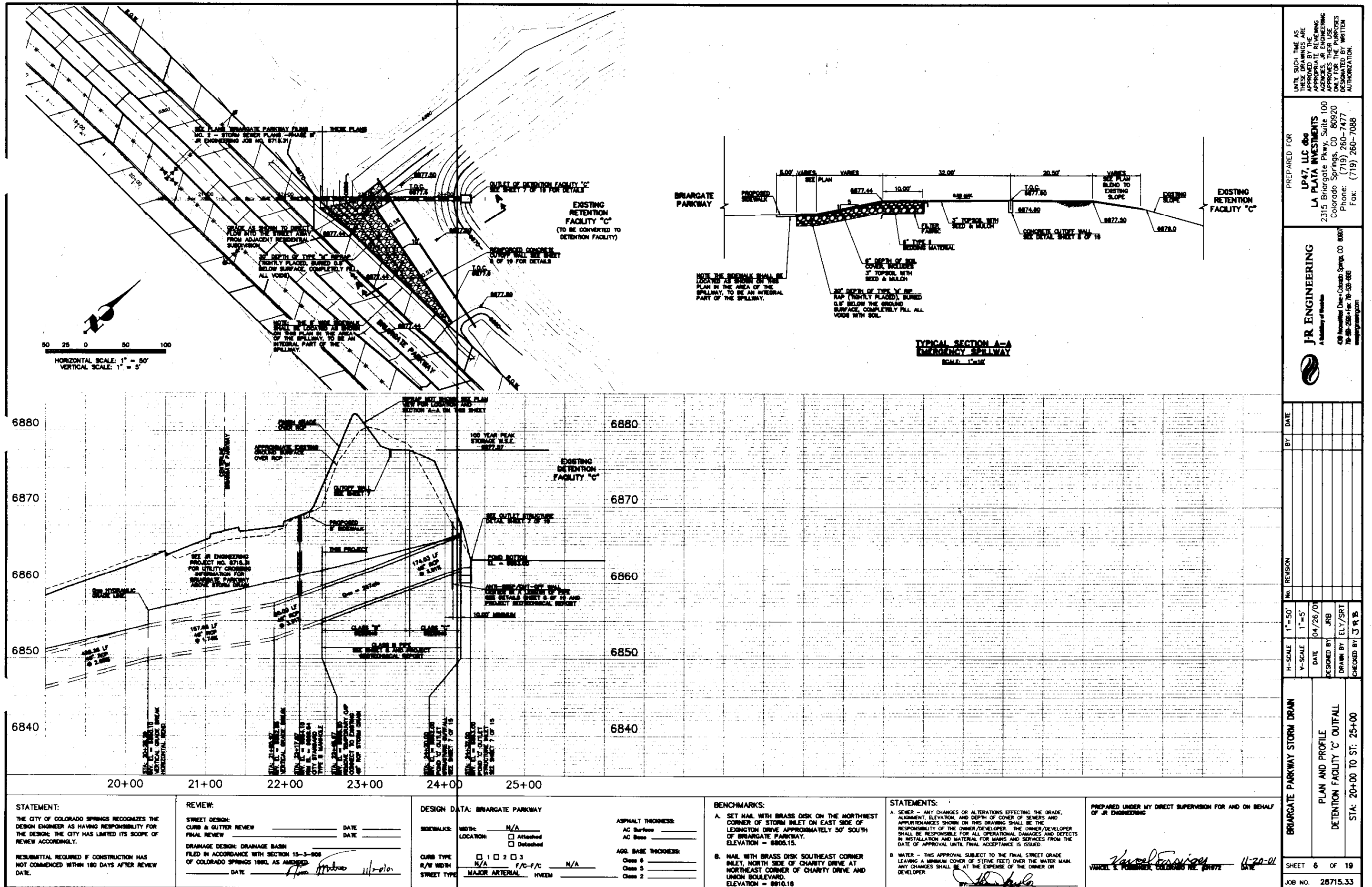
SHEET 1 OF 1

JOB NO. 28716.20

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Latitude: 38° 00' 00" N
Longitude: 104° 45' 00" W
Elevation: 6111.00
Sheet: 6

0111-06
Sheet 6 of 10
Project: D



PLAN & BARGRATE ASSEMBLY

PLAN - INLET

SECTION E-E

SCALE 1"=1'

PLAN- HORIZONTAL WALL
REINFORCING STEEL

ELEVATION- ADDITIONAL
REINF. AT PIPE PENETRATION

SECTION D-D
(GRATE & GRATE SUPPORTS NOT SHOWN)

SECTION C-C

STEEL FABRICATION NOTES:

1. FABRICATED STEEL STRUCTURES SHALL BE CONSTRUCTED IN ACCORDANCE WITH AISC AND AWS SPECIFICATIONS.
2. THE OUTLET STRUCTURE BARGARTE IS DESIGNED FOR A VERTICAL LOAD OF 300 LBS./SQ. FT.
3. ALL STRUCTURAL STEEL SHAPES TO INCLUDE: ANGLE, PLATE, AND BAR SHALL MEET ASTM A36 SPECIFICATIONS, FY= 36 KSI MINIMUM.
- STRUCTURAL TUBING SHALL MEET ASTM A500 GRADE B SPECIFICATIONS, FY= 46 KSI MINIMUM.
- STEEL PIPE SHALL BE STANDARD WEIGHT PIPE ASTM A53 GRADE B, FY= 35 KSI MINIMUM.
4. WELDS NOT INDICATED SHALL BE 1/8" MINIMUM FILLET OR GROOVE, CONTINUOUS 90 DEGREE JOINTS. CONSIDER VANDALISM LOADS, WELD ACCORDINGLY AT CRITICAL LOCATIONS.
5. PRIOR TO PAINTING REMOVE ALL OIL, SCALE, AND SLAG, GRIND OFF BURRS AND SHARP EDGES.
6. PAINT WITH ONE SHOP COAT OF ZINC RICH PRIMER AND TWO COATS OF ALUMINUMUM PAINT, AASHTO M-69

SCALE 3/8" = 1'

SEE CONCRETE SPECIFICATIONS SHEET 10 OF 15

PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF
OF JR ENGINEERING

Harold K. Davis 11-20-0

UNTIL SUCH TIME AS THESE DRAWINGS ARE APPROVED BY THE APPROPRIATE REVIEWING AGENCIES, JR ENGINEERING APPROVES THEIR USE ONLY FOR THE PURPOSES DESIGNATED BY WRITTEN AUTHORIZATION.

PREPARED FOR
LP47, LLC d/b/a
LA PLATA INVESTMENTS
 2315 Briargate Pkwy, Suite 200
 Colorado Springs, CO 80905
 Phone: (719) 260-7700
 Fax: (719) 260-7701

J·R ENGINEERING
A Subsidiary of Westcon
1300 Arapahoe Drive • Colorado Springs, CO
761-55-2333 • Fax 761-528-6863



H-SCALE		VARIES	No.	REVISION	BY	DATE
V-SCALE		VARIES				
DATE		04/26/01				
DESIGNED BY		JRB				
DRAWN BY		SRT/ELY				

BRIARGATE PARKWAY STORM DRAIN

DETENTION FACILITY "C"
OUTLET STRUCTURE DETAILS

SHEET 7 OF 1

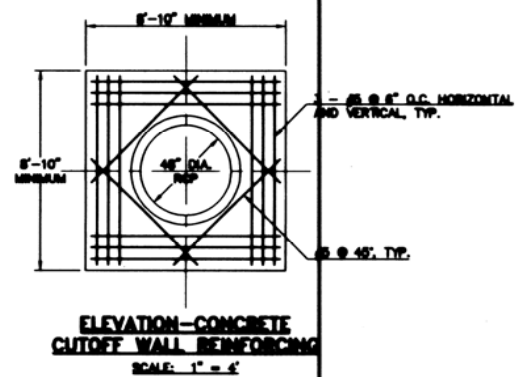
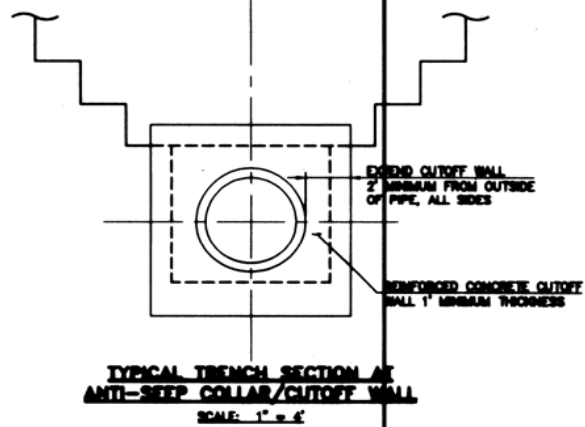
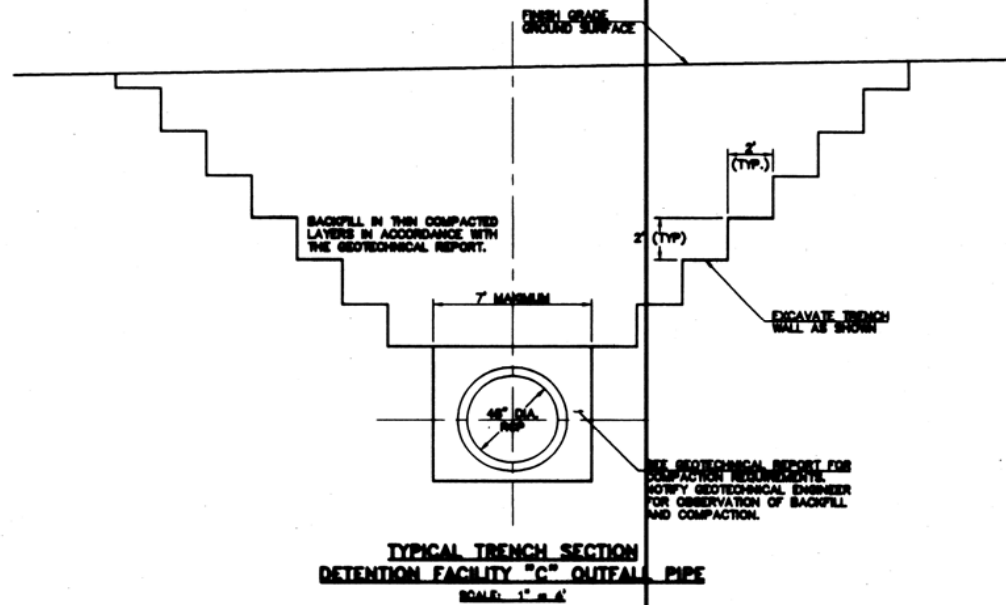
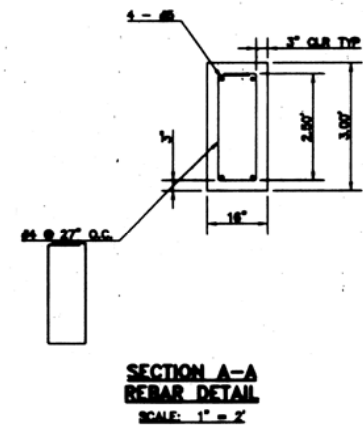
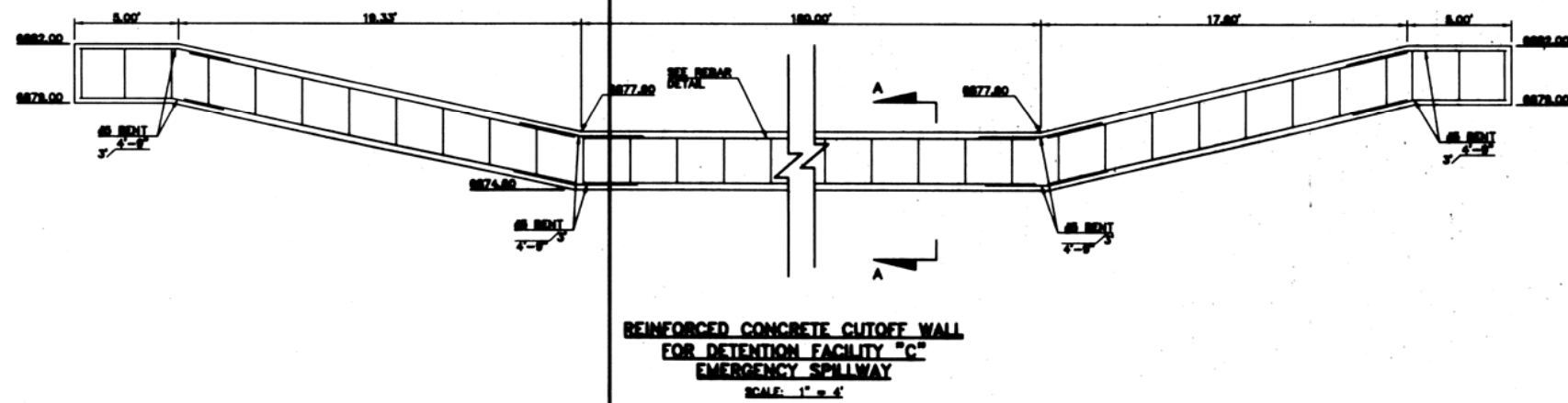
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0111-08
Sheets of 10

Preliminary Drainage Report
Regional Detention Facility "C" Water Quality Retrofit



PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF
OF J.R. ENGINEERING
James R. Frazier 11-20-01
JAMES R. FRAZIER, LICENSED PROFESSIONAL ENGINEER, NO. 00072 DATE

BY		DATE	REVISION		VARIES		H-SCALE		V-SCALE		DATE		DESIGNED BY		DRAWN BY		CHECKED BY	
			No.		VARIES	VARIES					04/26/01		JRB		SRT/ELY		JTR	
BRIARGATE PARKWAY STORM DRAIN																		
REINFORCED CONCRETE CUTOFF WALL																		
DETENTION FACILITY "C" EMERGENCY SPILLWAY																		
INCLUDING ANTI-SEEP COLLAR DETAILS																		
SHEET 8 OF 10																		
28715.33																		

UNTIL SUCH TIME AS
THESE DRAWINGS ARE
APPROVED BY THE
APPROPRIATE REVIEWING
AGENCIES, J.R. ENGINEERING
ONLY FOR THE PURPOSES
DESIGNATED BY WRITTEN
AUTHORIZATION.

PREPARED FOR
LP47, LLC dba
LA PLATA INVESTMENTS
2315 Briargate Pkwy, Suite 100
Colorado Springs, CO 80920
Phone: (719) 260-7477
Fax: (719) 260-7088

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A subsidiary of Woodward
438 Associated Drive • Colorado Springs, CO 80907
719-588-2888 • Fax 719-588-6800
www.jrengineering.com

0111-08-8