

Smith Creek Drainage Basin Planning Study

Job Number 8896.90

June 22, 2001



J-R ENGINEERING

A Subsidiary of Westrian

PRUDENT LINE CALCULATOR for DESIGN POINT No. 111

Storm	Q _p cfs	d hr.	Vol _i =6Q _p d cubic feet	Y _i =0.25Vol _i	Y _m	Y _m x 1.67 cubic feet	Long Term Potential Lateral Migration		Short Term Potential Lateral Migration
							PLM _{LT} feet	PLM _{LT} *30 feet	PLM _{ST} feet
100	463	2.50	6945	1736	257	429	0	9	2
50	335	2.50	5025	1256					
25	241	2.50	3615	904					
10	157	2.25	2120	530					
5	98	2.25	1323	331					
2	30	3.75	675	169					

3' assumed bank height for channel erosion

$$Y_m = 0.015Y_{100} + 0.015Y_{50} + 0.04Y_{25} + 0.08Y_{10} + 0.2Y_5 + 0.4Y_2$$

$$PLM_{LT} = Y_m \times 1.67 \times \text{bank height} / 500$$

$$PLM_{ST} = Y_m \times 1.67 \times \text{bank height} / 150$$

d=hydrograph duration (hrs)

The prudent line for sand channels is based on an enveloping curve considering the greater of (1) the 100 year flood plain, (2) the calculated setback based long term (30 year) erosion, (3) the calculated setback based short term (100-year flood) erosion, or (4) the setback based on the low flow channel top of bank (or the 10-year water surface when a low flow channel is not apparent) plus 50 feet.

Long term potential lateral migration is based on a 500' length.

Short term potential lateral migration is based on a 150' length.

The lateral migration numbers are estimates.

Setback from the low flow channel top of bank (or the 10-year water surface when a low flow channel is not apparent):

- (1) 100'
- (2) 9'
- (3) 2'
- (4) 50'

Therefore, the prudent line setback at this design point is 50 feet.

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June 22, 2001



J-R ENGINEERING

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PRUDENT LINE CALCULATOR for DESIGN POINT No. 109

Storm	Q _p cfs	d hr.	Vol _i =6Q _p d cubic feet	Y _i =0.25Vol _i	Y _m	Y _m x 1.67 cubic feet	Long Term Potential Lateral Migration		Short Term
							PLM _{LT} feet	PLM _{LT} *30 feet	Potential Lateral Migration PLM _{ST} feet
100	382	2.50	5730	1433	203	340	0	11	3
50	268	2.50	4020	1005					
25	184	2.50	2760	690					
10	123	2.25	1661	415					
5	77	2.25	1040	260					
2	24	3.75	540	135					

2' assumed bank height for channel erosion

$$Y_m = 0.015Y_{100} + 0.015Y_{50} + 0.04Y_{25} + 0.08Y_{10} + 0.2Y_5 + 0.4Y_2$$

$$PLM_{LT} = Y_m \times 1.67 \times \text{bank height}/500$$

$$PLM_{ST} = Y_m \times 1.67 \times \text{bank height}/150$$

d=hydrograph duration (hrs)

The prudent line for sand channels is based on an enveloping curve considering the greater of (1) the 100 year flood plain, (2) the calculated setback based long term (30 year) erosion, (3) the calculated setback based short term (100-year flood) erosion, or (4) the setback based on the low flow channel top of bank (or the 10-year water surface when a low flow channel is not apparent) plus 50 feet.

Long term potential lateral migration is based on a 500' length.

Short term potential lateral migration is based on a 150' length.

The lateral migration numbers are estimates.

Setback from the low flow channel top of bank (or the 10-year water surface when a low flow channel is not apparent):

- (1) 195'
- (2) 11'
- (3) 3'
- (4) 50'

Therefore, the prudent line setback at this design point is 195 feet.

Smith Creek Drainage Basin Planning Study

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June 22, 2001



J-R ENGINEERING

A Subsidiary of Westrian

PRUDENT LINE CALCULATOR for DESIGN POINT No. 107B

Storm	Q _p cfs	d hr.	Vol _i =6Q _p d cubic feet	Y _i =0.25Vol _i	Y _m	Y _m x 1.67 cubic feet	Long Term Potential Lateral Migration		Short Term
							PLM _{LT} feet	PLM _{LT} *30 feet	Potential Lateral Migration PLM _{ST} feet
100	281	2.50	4215	1054	156	261	0	6	2
50	197	2.50	2955	739					
25	140	2.50	2100	525					
10	94	2.25	1269	317					
5	59	2.25	797	199					
2	18	4.00	432	108					

3' assumed bank height for channel erosion

$$Y_m = 0.015Y_{100} + 0.015Y_{50} + 0.04Y_{25} + 0.08Y_{10} + 0.2Y_5 + 0.4Y_2$$

$$PLM_{LT} = Y_m \times 1.67 \times \text{bank height}/500$$

$$PLM_{ST} = Y_m \times 1.67 \times \text{bank height}/150$$

d=hydrograph duration (hrs)

The prudent line for sand channels is based on an enveloping curve considering the greater of (1) the 100 year flood plain, (2) the calculated setback based long term (30 year) erosion, (3) the calculated setback based short term (100-year flood) erosion, or (4) the setback based on the low flow channel top of bank (or the 10-year water surface when a low flow channel is not apparent) plus 50 feet.

Long term potential lateral migration is based on a 500' length.

Short term potential lateral migration is based on a 150' length.

The lateral migration numbers are estimates.

Setback from the low flow channel top of bank (or the 10-year water surface when a low flow channel is not apparent):

- (1) 140'
- (2) 6'
- (3) 2'
- (4) 50'

Therefore, the prudent line setback at this design point is 140 feet.

Smith Creek Drainage Basin Planning Study

Job Number 8896.90

June 22, 2001



J-R ENGINEERING

A Subsidiary of Westrian

PRUDENT LINE CALCULATOR for DESIGN POINT No. 107A

Storm	Q _p cfs	d hr.	Vol _i =6Q _p d cubic feet	Y _i =0.25Vol _i	Y _m	Y _m x 1.67 cubic feet	Long Term Potential Lateral Migration		Short Term
							PLM _{LT} feet	PLM _{LT} *30 feet	Potential Lateral Migration PLM _{ST} feet
100	263	2.75	4340	1085	148	247	0	2	1
50	184	2.75	3036	759					
25	132	2.50	1980	495					
10	90	2.25	1215	304					
5	56	2.25	756	189					
2	17	3.75	383	96					

8' assumed bank height for channel erosion

$$Y_m = 0.015Y_{100} + 0.015Y_{50} + 0.04Y_{25} + 0.08Y_{10} + 0.2Y_5 + 0.4Y_2$$

$$PLM_{LT} = Y_m \times 1.67 \times \text{bank height} / 500$$

$$PLM_{ST} = Y_m \times 1.67 \times \text{bank height} / 150$$

d=hydrograph duration (hrs)

The prudent line for sand channels is based on an enveloping curve considering the greater of (1) the 100 year flood plain, (2) the calculated setback based long term (30 year) erosion, (3) the calculated setback based short term (100-year flood) erosion, or (4) the setback based on the low flow channel top of bank (or the 10-year water surface when a low flow channel is not apparent) plus 50 feet.

Long term potential lateral migration is based on a 500' length.

Short term potential lateral migration is based on a 150' length.

The lateral migration numbers are estimates.

Setback from the low flow channel top of bank (or the 10-year water surface when a low flow channel is not apparent):

- (1) 33'
- (2) 2'
- (3) 1'
- (4) 50'

Therefore, the prudent line setback at this design point is 50 feet.

Smith Creek Drainage Basin Planning Study

Job Number 8896.90

June 22, 2001



J-R ENGINEERING

A Subsidiary of Westrian

PRUDENT LINE CALCULATOR for DESIGN POINT No. 105

Storm	Q _p cfs	d hr.	Vol _i =6Q _p d cubic feet	Y _i =0.25Vol _i	Y _m	Y _m x 1.67 cubic feet	Long Term Potential Lateral Migration		Short Term Potential Lateral Migration
							PLM _{LT} feet	PLM _{LT} *30 feet	PLM _{ST} feet
100	167	2.75	2756	689	101	169	0	3	1
50	114	2.75	1881	470					
25	87	2.75	1436	359					
10	61	2.50	915	229					
5	36	2.50	540	135					
2	10	4.00	240	60					

4' assumed bank height for channel erosion

$$Y_m = 0.015Y_{100} + 0.015Y_{50} + 0.04Y_{25} + 0.08Y_{10} + 0.2Y_5 + 0.4Y_2$$

$$PLM_{LT} = Y_m \times 1.67 \times \text{bank height}/500$$

$$PLM_{ST} = Y_m \times 1.67 \times \text{bank height}/150$$

d=hydrograph duration (hrs)

The prudent line for sand channels is based on an enveloping curve considering the greater of (1) the 100 year flood plain, (2) the calculated setback based long term (30 year) erosion, (3) the calculated setback based short term (100-year flood) erosion, or (4) the setback based on the low flow channel top of bank (or the 10-year water surface when a low flow channel is not apparent) plus 50 feet.

Long term potential lateral migration is based on a 500' length.

Short term potential lateral migration is based on a 150' length.

The lateral migration numbers are estimates.

Setback from the low flow channel top of bank (or the 10-year water surface when a low flow channel is not apparent):

- (1) 40'
- (2) 3'
- (3) 1'
- (4) 50'

Therefore, the prudent line setback at this design point is 50 feet.

HEC-1 COMPUTATIONS

HEC-1 COMPUTER FILES

EXISTING CONDITIONS

PATH: 889690/HYDRO/HEC-1/EXISTING/

FREQUENCY	RAINFALL	INPUT	OUTPUT	MODIFIED OUTPUT
2YR	2"	2EX.NET	2EX.OUT	2EX.TXT
5YR	2.6"	5EX.NET	5EX.OUT	5EX.TXT
10YR	3"	10EX.NET	10EX.OUT	10EX.TXT
50YR	4"	50EX.NET	50EX.OUT	50EX.TXT
100YR	4.6"	100EX.NET	100EX.OUT	100EX.TXT

FUTURE CONDITIONS- ALTERNATIVE 1

PATH: 889690/HYDRO/HEC-1/FUTURE/ALT1/

FREQUENCY	RAINFALL	INPUT	OUTPUT	MODIFIED OUTPUT
2YR	2"	2FUT1.NET	2FUT1.OUT	2FUT1.TXT
5YR	2.6"	5FUT1.NET	5FUT1.OUT	5FUT1.TXT
10YR	3"	10FUT1.NET	10FUT1.OUT	10FUT1.TXT
50YR	4"	50FUT1.NET	50FUT1.OUT	50FUT1.TXT
100YR	4.6"	100FUT1.NET	100FUT1.OUT	100FUT1.TXT

FUTURE CONDITIONS- ALTERNATIVE 2

PATH: 889690/HYDRO/HEC-1/FUTURE/ALT2/

FREQUENCY	RAINFALL	INPUT	OUTPUT	MODIFIED OUTPUT
2YR	2"	2FUT2.NET	2FUT2.OUT	2FUT2.TXT
5YR	2.6"	5FUT2.NET	5FUT2.OUT	5FUT2.TXT
10YR	3"	10FUT2.NET	10FUT2.OUT	10FUT2.TXT
50YR	4"	50FUT2.NET	50FUT2.OUT	50FUT2.TXT
100YR	4.6"	100FUT2.NET	100FUT2.OUT	100FUT2.TXT

FUTURE CONDITIONS- ALTERNATIVE 3

PATH: 889690/HYDRO/HEC-1/FUTURE/ALT3/

FREQUENCY	RAINFALL	INPUT	OUTPUT	MODIFIED OUTPUT
2YR	2"	2FUT3.NET	2FUT3.OUT	2FUT3.TXT
5YR	2.6"	5FUT3.NET	5FUT3.OUT	5FUT3.TXT
10YR	3"	10FUT3.NET	10FUT3.OUT	10FUT3.TXT
50YR	4"	50FUT3.NET	50FUT3.OUT	50FUT3.TXT
100YR	4.6"	100FUT3.NET	100FUT3.OUT	100FUT3.TXT

FUTURE CONDITIONS- ALTERNATIVE 3 HYDROGRAPH PLOTS

PATH: 889690/HYDRO/HEC-1/FUTURE/ALT3/

FREQUENCY	RAINFALL	INPUT	OUTPUT
2YR	2"	2FUT3.NET	2FUT3H.OUT
5YR	2.6"	5FUT3.NET	5FUT3H.OUT
10YR	3"	10FUT3.NET	10FUT3H.OUT
25YR	3.5"	25FUT3.NET	25FUT3H.OUT
50YR	4"	50FUT3.NET	50FUT3H.OUT
100YR	4.6"	100FUT3.NET	100FUT3H.OUT

<u>BASIN</u>	<u>SQ. MI</u>
101	0.0920
103	0.1670
105A	0.0693
105B	0.0686
107A	0.1367
107B	0.0408
109	0.1637
111	0.1894
201	0.1216
203	0.1113
205	0.0970
207	0.1200
209	0.1351
211	0.0799
213	0.1243
215	0.0589
217	0.0547
219	0.1298
301	0.1196
303	0.1300
305	0.0629
307	0.1081
309	0.1240
311	0.1064
313	0.1520
315	0.0886
401	0.1524
403	0.1007
405	0.0677
407	0.1685
501	0.1219
503	0.1193
505	0.1923
507	0.0958
509	0.1514
511	0.0907
601	0.0633
603	0.2514
605	0.1283
607	0.0840
609	0.1389
611	0.1095
613	0.1233
615A	0.0567
615B	0.0313
617A	0.0701
617B	0.0215
701	0.0722
703	0.1305
705	0.0869

	TOTAL:	5.48 SQ. MI.
DP603	TRIB A:	0.31 SQ. MI.
DP111	TRIB B:	0.93 SQ. MI.
DP505	PLIER RD.	0.43 SQ. MI.
DP315	TRIB C:	0.89 SQ. MI.
DP217	TRIB D:	0.29 SQ. MI.

Future Basin Changes

From Basin 617A:

618	0.0070 SQ. MI.
617A	0.0149 SQ. MI.
617C	0.0482 SQ. MI.

From Basin 605:

605A	0.0505 SQ. MI.
605B	0.0778 SQ. MI.

Client: _____ Job No: 8896.90

Project: _____ By: _____ Chk. By: _____ Date: 6-1-01

Subject: _____ Sheet No: 1 of 9



J-R ENGINEERING
A Subsidiary of Westrian

EXISTING Pond

Pond 106

Location: The Ridge at Fox Run, Tric No. 3
N. of Baptist Road, E. of Fox Run Lane, Longmeadow
Lane intersection

OUTLET - TWO 36" RCP CULVERTS

SIZE	7320	2. VOL	CFS
	22	1.4	50 } ESTIMATES
	24	2.6	80 }
	26	4.0	100 }
	28	5.8 ac-ft	190 cfs (172 cfs) existing

Maintained by The Ridge at Fox Run HOA

Peak runoff into pond 60, 75.2 cfs
Dip 200, 200 cfs

Client: _____ Job No: _____

Project: _____ By: _____ Chk. By: _____ Date: _____

Subject: _____ Sheet No: 2 of 9



J-R ENGINEERING
A Subsidiary of Westrian

Existing Pond

Pond 108

PER COSTM Engineering's FDR FOR THE
Ridge at Foxcroft Fil. No. 1 Rev Jan 7, 1996

Volume	Elevation	Discharge
0.0	7340	0
0.20	7342	20
0.68	7344	48
1.35	7346	220
2.32	7348	822

Client: _____ Job No: _____

Project: _____ By: _____ Chk. By: _____ Date: _____

Subject: _____ Sheet No: 3 of 9



J-R ENGINEERING
A Subsidiary of Westrian

EXISTING POND

Pond 610

Area	ELEV	Discharge
2.2 AL	6822	0
2.7	6823	11
3.3	6824	701
3.8	6825	2361
4.4	6826	4843
5.1	6827	10331
5.8	6828	16010

Pond 612

Area	ELEV	Discharge
1.82 AL	6762	0
2.77	6763	150
3.72	6764	510
4.5	6765	1160
5.28	6766	2120
5.78	6766.5	2680

Client: _____ Job No: 8810-70

Project: _____ By: _____ Chk. By: _____ Date: 5-23-01

Subject: _____ Sheet No: 4 of 9



J-R ENGINEERING
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EXISTING Condition Detention Ponds

Pond 614

Location: Ridge Point Apartments
N. of Northgate Road, east of structure

Outlet 24" RCP @ 2.56% w/ 7 3/4" Dia. orifice plate
10 yr

Size 6720 2 volume Discharge 9 cfs

6724 0.067 ac-ft

6726 0.32 6

6728 0.67 10

Ann. 1500 6730 1.16 ac-ft 13.3 (20)

Release Rate 13.3 cfs (100 yr) + 2.0 cfs un. restricted
3.99 (10 yr) + 1.0 cfs (10 yr)

7.22' deep max 100 yr ponding

Tributary Area 13.3 acres onsite trib to pond
2.4 acres un. restricted

Client: _____ Job No: _____

Project: _____ By: _____ Chk. By: _____ Date: _____

Subject: _____ Sheet No: 5 of 9



J-R ENGINEERING
A Subsidiary of Westrian

EXISTING POND

Pond 013

Location: West of Northwest Highlands
Northwest Northwest Road

	Area	Elevation	Discharge
0.12	5142	6794	4.67
0.96	41980	6796	7.44
1.09	47369	6798	9.43
1.21	52795	6800	22.99
1.34	58414	6802	29.35
1.47 ac	64325	6804	34.42

Client: _____ Job No: _____

Project: _____ By: _____ Chk. By: _____ Date: _____

Subject: _____ Sheet No: 6 of 9



J-R ENGINEERING
A Subsidiary of Westrian

Future Pond

Pond 605

Elevation	Storage	Discharge
6818	0	0
19	0.099	5.18
20	0.218	19.37
21	0.36	40.40
22	0.526	65.78
23	0.718	92.88
24	0.937	119.73
25	1.185	143.30
26	1.463	162.05
27	1.773	176.71
28	2.117	190.53
29	2.496	202.99
30	2.912 ac-ft	214.91

Pond 615

Elevation	Storage	Discharge
6766	0	0
6728	1	5
6730	2	10
6732	2.5 ac-ft	16.7

Pond 617

Elevation	Storage	Discharge
6740	0	0
6743	0.5	30
6748	1.0	40
6750	1.5 ac-ft	63

Pond 618

Elevation	Storage	Discharge
6768	0 ac-ft	0
6770	0.5 ac-ft	3
6772	1.0 ac-ft	6

Pond 604

Elevation	Storage	Discharge
6990	0	0
92	0.041	400
94	0.15	600
96	0.40	800
98	0.8	1000
100	1.2	1200
102	1.6	1400
104	2.0	1600
106	2.4	1800
108	2.8	2000

Client: Piccola, Inc

Job No: 8896.90

Project: Smith Creek DIPS LOR

By: _____

Date: 6-12-01

Subject: _____

Sheet No: 7 of 9



J-R ENGINEERING
A Subsidiary of Westrian

Proposed Elevation	Regional Discharge	Pond No. 1 Release
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6990	0	0
6992	0.44	10
6994	1.49	25
6996	2.93	50
6998	4.75	75
7000	6.91	150
7002	9.41	300
7004	12.27	1000
7006	15.50	1900

7005.96 AC @ HWL
 SA = 1.70 AC @ HWL

Locate at existing driveway in back of lot
 w/ 36" RCP culvert

407A	407B
407A - Pond	Pond - 506
665'	340'
0.0210	0.0210

SMITH CREEK DBPS POND CALCULATIONS

Pond 407

ELEVATIONS	SF	CF	AF	SUM
6990	0			
		18949.00	0.44	
6992	18949			0.44
		46055.00	1.06	
6994	27106			1.49
		62782.00	1.44	
6996	35676			2.93
		79075.00	1.82	
6998	43399			4.75
		93993.00	2.16	
7000	50594			6.91
		109064.00	2.50	
7002	58470			9.41
		124705.00	2.86	
7004	66235			12.27
		140482.00	3.23	
7006	74247			15.50
TOTAL		675105.00	15.50	

Client: _____ Job No: 8896.90

Project: _____ By: _____ Chk. By: _____ Date: 6-12-01

Subject: _____ Sheet No: 8 of 9



J-R ENGINEERING
A Subsidiary of Westrian

Proposed Regional Pond No. 2 Res 316

Elevation	S Storage	Release
7164	0.00 ac-ft	0.00
7166	0.72 ac-ft	10
7168	2.42 ac-ft	75
7170	4.57 ac-ft	90
7172	7.19 ac-ft	300
7174	10.29 ac-ft	1225

7173.99 AHWL 1219 cfs

SA = 1.66 AC @ HWL

locate at confluence of Trib C and Smith
Creek

SMITH CREEK DBPS POND CALCULATIONS

Pond 316

ELEVATIONS	SF	CF	AF	SUM
7164	0			
		31411.00	0.72	
7166	31411			0.72
		73877.00	1.70	
7168	42466			2.42
		93868.00	2.15	
7170	51402			4.57
		114019.00	2.62	
7172	62617			7.19
		135004.00	3.10	
7174	72387			10.29
TOTAL		448179.00	10.29	

Client: L. J. ...
Project: ... By: W.E. Chk. By: ...
Subject: ...

Job No: 8896.90
Date: 6-12-01
Sheet No: 9 of 9



JR ENGINEERING
A Subsidiary of Westrian

Proposed Regional Pond No. 3 Res Col 19

Elevation	Storage	Retention
6712	0	0
6714	2 ac-ft	800
6716	4 ac-ft	1200
6718	6 ac-ft	1500
6720	8 ac-ft	1600
6722 3.06 ac	11 ac-ft	1800
6724	13 ac-ft	1970
6723.88 M WL	1966 ac-ft	

NOT USED

locate and existing conduit at Northgate Road + Smith Street

2 year existing
HEC1 S/N 1343001909 HMVersion: 6.33 Data File: C:\WINNT\TEMP\~vbh2660 TMP

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*  
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *  
* U. S. ARMY CORPS OF ENGINEERS *  
* MAY 1991 *  
* HYDROLOGIC ENGINEERING CENTER *  
* VERSION 4.0.1E *  
* 609 SECOND STREET *  
* *  
* DAVIS, CALIFORNIA 95616 *  
* RUN DATE 06/19/2001 TIME 16:44:04 *  
* (916) 756-1104 *  
* *  
*****
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  X   X  XXXXXXXX  XXXXX      X  
  X   X  X        X   X      XX  
  X   X  X        X           X  
  XXXXXXXX  XXXX  X           XXXXX  X  
  X   X  X        X           X  
  X   X  X        X   X      X  
  X   X  XXXXXXXX  XXXXX      XXX
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.....  
.....  
: Full Microcomputer Implementation :  
: by :  
: Haestad Methods, Inc. :  
: :  
.....  
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37 Brookside Road * Waterbury, Connecticut 06708 * (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION.

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE*, *SINGLE EVENT DAMAGE CALCULATION, DSS: WRITE STAGE FREQUENCY,

DSS: READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE: GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	1	2	3	4	5	6	7	8	9	10	
	1	ID	Type	IIA storm							
	2	IT	15	0	0	288					
	3	ID	5								
	4	KK	SC205								
	5	KM	Smith Creek 205 Runoff								
	6	KD					22				
	7	BA	0.0970								
	8	PB	2								
	9	IN	15								
0.0165	10	PC	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143
0.0600	11	PC	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
0.8000	12	PC	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
0.8600	13	PC	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
0.8975	14	PC	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
0.9300	15	PC	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270
0.9550	16	PC	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
0.9800	17	PC	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
0.9925	18	PC	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
	19	PC	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
	20	LS	0	64							
	21	UD	0.257								
	22	KK	RT205								
	23	KM	Smith Creek Route 205 to 213								
	24	KD					22				
	25	RK	1530	0.0431	0.055		TRAP		2		
	26	KK	SC207								
	27	KM	Smith Creek 207 Runoff								
	28	KD					22				
	29	BA	0.120								
	30	PB	2								
	31	LS	0	65							
	32	UD	0.367								
	33	KK	SC213								
	34	KM	Smith Creek 213 Runoff								
	35	KD					22				
	36	BA	0.1243								
	37	PB	2								
	38	LS	0	66							
	39	UD	0.382								
	40	KK	DP213								
	41	KM	Combine RT205 SC207 and SC213								
	42	KD					22				
	43	HC	3								
	44	KK	RT213								
	45	KM	Smith Creek Route 213 to 215								
	46	KD					22				
	47	RK	1360	0.0493	0.055		TRAP		2		

LINE	ID	1	2	3	4	5	6	7	8	9	10
48	KK										
49	KM										
50	KD									22	
51	BA			0.1351							
52	PB			2							
53	LS			0	61						
54	UD			0.336							
55	KK										
56	KM										
57	KD									22	
58	BA			0.0799							
59	PB			2							
60	LS			0	62						
61	UD			0.418							
62	KK										
63	KM										
64	KD									22	
65	BA			0.0589							
66	PB			2							
67	LS			0	62						
68	UD			0.227							
69	KK										
70	KM										
71	KD									22	
72	HC				4						
73	KK										
74	KM										
75	KD									22	
76	RK			2110	0.0446	0.0745				TRAP	2
77	KK										
78	KM										
79	KD									22	
80	BA			0.1298							
81	PB			2							
82	LS			0	61						
83	UD			0.362							
84	KK										
85	KM										
86	KD									22	
87	HC				2						
88	KK										
89	KM										
90	KD									22	
91	BA			0.1216							
92	PB			2							
93	LS			0	62						
94	UD			0.340							

LINE	1	2	3	4	5	6	7	8	9	10
ID										
184	KK	SC311								
185	KM	Smith Creek 311 Runoff								
186	KD							22		
187	BA	0.1064								
188	PB	2								
189	LS	0	64							
190	UD	0.295								
191	KK	DP311								
192	KM	Combine RT305 SC307 SC309 and SC311								
193	KD							22		
194	HC	4								
195	KK	RT311								
196	KM	Tributary Route 311 to 315								
197	KD							22		
198	RK	2860	0.0448	0.0888				TRAP		2
199	KK	SC313								
200	KM	Smith Creek 313 Runoff								
201	KD							22		
202	BA	0.1520								
203	PB	2								
204	LS	0	64							
205	UD	0.373								
206	KK	SC315								
207	KM	Smith Creek 315 Runoff								
208	KD							22		
209	BA	0.0886								
210	PB	2								
211	LS	0	64							
212	UD	0.350								
213	KK	DP315								
214	KM	Combine RT311 SC313 and SC315								
215	KD							22		
216	HC	3								
217	KK	DP316								
218	KM	Combine RT220 and DP315								
219	KD							22		
220	HC	2								
221	KK	RT316								
222	KM	Smith Creek Route 316 to 401								
223	KD							22		
224	RK	2575	0.0361	0.120				TRAP	1	2

ID.	LINE	1	2	3	4	5	6	7	8	9	10
	225			KK	SC401						
	226			KM	Smith Creek 401 Runoff						
	227			KD					22		
	228			BA	0.1524						
	229			PB	2						
	230			LS	0	65					
	231			UD	0.437						
	232			KK	DP401						
	233			KM	Combine RT316 and SC401						
	234			KD					22		
	235			HC	2						
	236			KK	RT401						
	237			KM	Smith Creek Route 401 to 405						
	238			KD					22		
	239			RK	660	0.0548	0.120		TRAP	1	2
	240			KK	SC403						
	241			KM	Smith Creek 403 Runoff						
	242			KD					22		
	243			BA	0.1007						
	244			PB	2						
	245			LS	0	66					
	246			UD	0.333						
	247			KK	SC405						
	248			KM	Smith Creek 405 Runoff						
	249			KD					22		
	250			BA	0.0677						
	251			PB	2						
	252			LS	0	64					
	253			UD	0.356						
	254			KK	DP405						
	255			KM	Combine RT401 SC403 and SC405						
	256			KD					22		
	257			HC	3						
	258			KK	RT405						
	259			KM	Smith Creek Route 405 to 407						
	260			KD					22		
	261			RK	1500	0.0210	0.120		TRAP	1	2
	262			KK	SC101						
	263			KM	Smith Creek 101 Runoff						
	264			KD					22		
	265			BA	0.0920						
	266			PB	2						
	267			LS	0	64					
	268			UD	0.353						

LINE	ID	1	2	3	4	5	6	7	8	9	10
314	KK	RT105A									
315	KM	Tributary Route 105 to 107A									
316	KD								22		
317	RK	1000	0.0395	0.0727					TRAP		2
318	KK	SC107A									
319	KM	Smith Creek 107A Runoff									
320	KD								22		
321	BA	0.1367									
322	PB	2									
323	LS	0	68								
324	UD	0.287									
325	KK	RES108									
326	KM	EXISTING DETENTION POND 108									
327	KD								22		
328	RS	1	STOR	-1							
329	SV	0	0.20	0.68	1.35	2.32					
330	SE	7340	7342	7344	7346	7348					
331	SQ	0	20	48	220	822					
332	SE	7340	7342	7344	7346	7348					
333	KK	DP107A									
334	KM	Combine RES108 and RT105A									
335	KD								22		
336	HC	2									
337	KK	RT105B									
338	KM	TRIBUTARY ROUTE 107A TO 107B									
339	KD								22		
340	RK	1000	0.0395	0.0727					TRAP		2
341	KK	SC107B									
342	KM	SMITH CREEK 107B RUNOFF									
343	KD								22		
344	BA	0.0408									
345	PB	2									
346	LS	0	68								
347	UD	0.287									
348	KK	DP107B									
349	KM	COMBTINE RT105B AND SC107B									
350	KD								22		
351	HC	2									
352	KK	RT107									
353	KM	Tributary Route 107B to 109									
354	KD								22		
355	RK	1420	0.0359	0.120					TRAP		2

LINE	ID	1	2	3	4	5	6	7	8	9	10
356	KK	SC109									
357	KM	Smith Creek 109 Runoff									
358	KD								22		
359	BA	0.1637									
360	PB	2									
361	LS	0	68								
362	UD	0.398									
363	KK	DP109									
364	KM	Combine RT107 and SC109									
365	KD								22		
366	HC	2									
367	KK	RT109									
368	KM	Tributary Route 109 to 111									
369	KD								22		
370	RK	3840	0.0453	0.120					TRAP		2
371	KK	SC111									
372	KM	Smith Creek 111 Runoff									
373	KD								22		
374	BA	0.1894									
375	PB	2									
376	LS	0	69								
377	UD	0.382									
378	KK	DP111									
379	KM	Combine RT109 and SC111									
380	KD								22		
381	HC	2									
382	KK	SC407									
383	KM	Smith Creek 407 Runoff									
384	KD								22		
385	BA	0.1685									
386	PB	2									
387	LS	0	65								
388	UD	0.455									
389	KK	DP407									
390	KM	Combine DP111 RT405 and SC407									
391	KD								22		
392	HC	3									
393	KK	RT407									
394	KM	SMITH CREEK ROUTE 407 TO 506									
395	KD								22		
396	RK	1105	0.0210	0.120					TRAP	1	2

LINE	1	2	3	4	5	6	7	8	9	10
482			KK	RT601						
483			KM	Tributary Route 601 to 603						
484			KD					22		
485			RK	1170	0.0359	0.090		TRAP		2
486			KK	SC603						
487			KM	Smith Creek 603 Runoff						
488			KD					22		
489			BA	0.2514						
490			PB	2						
491			LS	0	68					
492			UD	0.325						
493			KK	DP603						
494			KM	Combine RT601 and SC603						
495			KD					22		
496			HC	2						
497			KK	DP604						
498			KM	Combine RT511 and DP603						
499			KD					22		
500			HC	2						
501			KK	RT604						
502			KM	Smith Creek Route 604 to 609						
503			KD					22		
504			RK	1380	0.0236	0.0928		TRAP	2	1
505			KK	SC605						
506			KM	Smith Creek 605 Runoff						
507			KD					22		
508			BA	0.1283						
509			PB	2						
510			LS	0	69					
511			UD	0.494						
512			KK	SC607						
513			KM	Smith Creek 607 Runoff						
514			KD					22		
515			BA	0.0840						
516			PB	2						
517			LS	0	69					
518			UD	0.270						
519			KK	SC609						
520			KM	Smith Creek 609 Runoff						
521			KD					22		
522			BA	0.1389						
523			PB	2						
524			LS	0	69					
525			UD	0.342						

HEC1 S/N: 1343001909

HMVersion: 6.33

Data File: C:\WINNT\TEMP\vbh2660.TMP

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

MAXIMUM STAGE	TIME OF OPERATION MAX STAGE	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA
					6-HOUR	24-HOUR	72-HOUR	
	HYDROGRAPH AT	SC205	2	6.00	1	0	0	0.10
	ROUTED TO	RT205	2	6.25	1	0	0	0.10
	HYDROGRAPH AT	SC207	3	6.00	1	0	0	0.12
	HYDROGRAPH AT	SC213	3	6.00	1	1	0	0.12
	3 COMBINED AT	DP213	7	6.25	3	1	0	0.34
	ROUTED TO	RT213	7	6.25	3	1	0	0.34
	HYDROGRAPH AT	SC209	1	6.50	0	0	0	0.14
	HYDROGRAPH AT	SC211	1	6.50	0	0	0	0.08
	HYDROGRAPH AT	SC215	1	6.25	0	0	0	0.06
	4 COMBINED AT	DP215	9	6.25	4	2	1	0.62
	ROUTED TO	RT215	9	6.50	4	2	1	0.62
	HYDROGRAPH AT	SC219	1	6.50	0	0	0	0.13
	2 COMBINED AT	DP219	9	6.50	4	2	1	0.75
	HYDROGRAPH AT	SC201	1	6.50	1	0	0	0.12
	ROUTED TO	RT201	1	6.50	1	0	0	0.12
	HYDROGRAPH AT	SC203	1	6.25	0	0	0	0.11
	2 COMBINED AT	DP203	2	6.50	1	1	0	0.23
	ROUTED TO	RT203	2	6.75	1	1	0	0.23
	HYDROGRAPH AT	SC217	0	6.25	0	0	0	0.05
	2 COMBINED AT	DP217	2	6.75	1	1	0	0.29
	2 COMBINED AT	DP220	11	6.50	6	3	1	1.03
	ROUTED TO	RT220	11	6.50	6	3	1	1.03
	HYDROGRAPH AT	SC301	2	6.00	1	0	0	0.12

HYDROGRAPH AT	SC303	2.	6.00	1.	0.	0.	0.13
2 COMBINED AT	DP303	4.	6.00	2.	1.	0.	0.25
ROUTED TO	RT303	4.	6.00	2.	1.	0.	0.25
HYDROGRAPH AT	SC305	1.	6.00	0.	0.	0.	0.06
2 COMBINED AT	DP305	5.	6.00	2.	1.	0.	0.31
ROUTED TO	RT305	5.	6.25	2.	1.	0.	0.31
HYDROGRAPH AT	SC307	2.	6.25	1.	0.	0.	0.11
HYDROGRAPH AT	SC309	2.	6.25	1.	0.	0.	0.12
HYDROGRAPH AT	SC311	2.	6.00	1.	0.	0.	0.11
4 COMBINED AT	DP311	10.	6.25	4.	2.	1.	0.65
ROUTED TO	RT311	10.	6.50	4.	2.	1.	0.65
HYDROGRAPH AT	SC313	2.	6.25	1.	0.	0.	0.15
HYDROGRAPH AT	SC315	1.	6.25	1.	0.	0.	0.09
3 COMBINED AT	DP315	13.	6.50	6.	3.	1.	0.89
2 COMBINED AT	DP316	25.	6.50	12.	6.	2.	1.92
ROUTED TO	RT316	24.	6.50	12.	6.	2.	1.92
HYDROGRAPH AT	SC401	3.	6.25	1.	1.	0.	0.15
2 COMBINED AT	DP401	27.	6.50	13.	6.	2.	2.08
ROUTED TO	RT401	26.	6.75	13.	6.	2.	2.08
HYDROGRAPH AT	SC403	3.	6.00	1.	0.	0.	0.10
HYDROGRAPH AT	SC405	1.	6.25	0.	0.	0.	0.07
3 COMBINED AT	DP405	29.	6.50	14.	7.	2.	2.25
ROUTED TO	RT405	29.	6.75	14.	7.	2.	2.25
HYDROGRAPH AT	SC101	1.	6.25	1.	0.	0.	0.09
ROUTED TO	RT101	1.	6.25	1.	0.	0.	0.09
HYDROGRAPH AT	SC103	4.	6.00	1.	1.	0.	0.17
HYDROGRAPH AT							

		SC105A	4	6 00	1	0	0	0.07
	3 COMBINED AT	DP103	9	6.00	3	1	0	0.33
	ROUTED TO	RES106	7	6.50	3	1	0	0.33
7320.29	6.50							
	ROUTED TO	RT103	7	6.50	3	1	0	0.33
	HYDROGRAPH AT	SC105B	4	6.00	1	0	0	0.07
	2 COMBINED AT	DP105	10	6.25	4	2	1	0.40
	ROUTED TO	RT105A	10	6.50	4	2	1	0.40
	HYDROGRAPH AT	SC107A	7	6.00	2	1	0	0.14
	ROUTED TO	RES108	6	6.25	2	1	0	0.14
7340.59	6.25							
	2 COMBINED AT	DP107A	15	6.25	6	2	1	0.53
	ROUTED TO	RT105B	15	6.25	6	2	1	0.53
	HYDROGRAPH AT	SC107B	2	6.00	1	0	0	0.04
	2 COMBINED AT	DP107B	16	6.25	6	3	1	0.57
	ROUTED TO	RT107	16	6.50	6	3	1	0.57
	HYDROGRAPH AT	SC109	7	6.00	2	1	0	0.16
	2 COMBINED AT	DP109	22	6.25	8	3	1	0.74
	ROUTED TO	RT109	21	6.50	8	3	1	0.74
	HYDROGRAPH AT	SC111	10	6.00	3	1	0	0.19
	2 COMBINED AT	DP111	28	6.50	11	5	2	0.93
	HYDROGRAPH AT	SC407	3	6.25	1	1	0	0.17
	3 COMBINED AT	DP407	56	6.50	26	12	4	3.34
	ROUTED TO	RT407	56	6.75	26	12	4	3.34
	HYDROGRAPH AT	SC501	3	6.00	1	0	0	0.12
	HYDROGRAPH AT	SC503	2	6.25	1	0	0	0.12
	HYDROGRAPH AT	SC505	4	6.25	2	1	0	0.19
	3 COMBINED AT	DP505	8	6.00	3	2	1	0.43

2 COMBINED AT	DP506	62.	6.75	29.	13.	4.	3.77
ROUTED TO	RT506	62.	6.75	29.	13.	4.	3.77
HYDROGRAPH AT	SC507	5.	6.00	1.	1.	0.	0.10
2 COMBINED AT	DP507	63.	6.75	30.	14.	5.	3.87
ROUTED TO	RT507	62.	6.75	30.	14.	5.	3.87
HYDROGRAPH AT	SC509	7.	6.00	2.	1.	0.	0.15
2 COMBINED AT	DP509	66.	6.75	32.	15.	5.	4.02
ROUTED TO	RT509	65.	7.00	32.	15.	5.	4.02
HYDROGRAPH AT	SC511	5.	6.00	1.	0.	0.	0.09
2 COMBINED AT	DP511	67.	7.00	33.	15.	5.	4.11
ROUTED TO	RT511	66.	7.00	33.	15.	5.	4.11
HYDROGRAPH AT	SC601	4.	6.00	1.	0.	0.	0.06
ROUTED TO	RT601	3.	6.00	1.	0.	0.	0.06
HYDROGRAPH AT	SC603	12.	6.00	3.	1.	0.	0.25
2 COMBINED AT	DP603	16.	6.00	4.	2.	1.	0.31
2 COMBINED AT	DP604	72.	7.00	37.	17.	6.	4.43
ROUTED TO	RT604	71.	7.00	37.	17.	6.	4.43
HYDROGRAPH AT	SC605	6.	6.25	2.	1.	0.	0.13
HYDROGRAPH AT	SC607	5.	6.00	1.	0.	0.	0.08
HYDROGRAPH AT	SC609	8.	6.00	2.	1.	0.	0.14
4 COMBINED AT	DP609	79.	7.00	41.	19.	6.	4.78
ROUTED TO	RES610	95.	6.75	39.	19.	6.	4.78
6823 12	6.75						
ROUTED TO	RT610	82.	7.00	38.	19.	6.	4.78
HYDROGRAPH AT	SC611	7.	6.00	2.	1.	0.	0.11
2 COMBINED AT	DP611	84.	7.00	39.	19.	7.	4.89
ROUTED TO	RES612	76.	7.25	39.	19.	7.	4.89

6762.50	7.25							
	ROUTED TO	RT612	75.	7.50	39.	19	7.	4.89
	HYDROGRAPH AT	SC613	8.	6.00	2	1	0	0.12
	ROUTED TO	RT613	7.	6.00	2.	1	0.	0.12
	HYDROGRAPH AT	SC615B	9.	5.75	1.	0.	0.	0.03
	ROUTED TO	RES614	4	6.00	1	0.	0.	0.03
6724.48	6.00							
	HYDROGRAPH AT	SC617A	4.	6.00	1.	0.	0.	0.07
	HYDROGRAPH AT	SC615A	4	5.75	1.	0	0.	0.06
	5 COMBINED AT	DP613	80.	7.50	41.	21.	7.	5.17
	ROUTED TO	RT614	79.	7.50	41.	21.	7.	5.17
	HYDROGRAPH AT	SC617B	1.	6.00	0.	0.	0.	0.02
	2 COMBINED AT	DP617	79.	7.50	42.	21.	7.	5.19
	ROUTED TO	RT617	78.	7.75	42.	21.	7.	5.19
	HYDROGRAPH AT	SC701	46.	6.00	8.	2.	1.	0.07
	HYDROGRAPH AT	SC703	40.	5.75	5.	2.	1.	0.13
	3 COMBINED AT	DP703	85.	7.75	52.	25.	9.	5.39
	ROUTED TO	RT703	84.	7.75	51.	25.	9.	5.39
	HYDROGRAPH AT	SC705	5.	6.00	1.	1.	0.	0.09
	2 COMBINED AT	DP705	85.	7.75	53.	26.	9.	5.48

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

VOLUME (IN)	ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO COMPUTATION INTERVAL	
								PEAK (CFS)	TIME TO PEAK (MIN)
0.12	RT205	MANE	2.71	1.76	366.57	0.12	15.00	1.60	375.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6094E+00 EXCESS=0.0000E+00 OUTFLOW=0.6091E+00 BASIN STORAGE= 0.5891E-09 PERCENT ERROR= 0.0									
0.14	RT213	MANE	1.75	7.39	376.62	0.14	15.00	7.38	375.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2491E+01 EXCESS=0.0000E+00 OUTFLOW=0.2491E+01 BASIN STORAGE= 0.2187E-08 PERCENT ERROR= 0.0									
0.11	RT215	MANE	3.16	9.15	380.60	0.11	15.00	8.68	390.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3666E+01 EXCESS=0.0000E+00 OUTFLOW=0.3664E+01 BASIN STORAGE= 0.1627E-07 PERCENT ERROR= 0.1									
0.09	RT201	MANE	3.28	1.02	394.87	0.09	15.00	1.01	390.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5631E+00 EXCESS=0.0000E+00 OUTFLOW=0.5629E+00 BASIN STORAGE= 0.8940E-09 PERCENT ERROR= 0.0									
0.08	RT203	MANE	3.96	1.70	397.89	0.08	15.00	1.67	405.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.9964E+00 EXCESS=0.0000E+00 OUTFLOW=0.9961E+00 BASIN STORAGE= 0.8250E-08 PERCENT ERROR= 0.0									
0.10	RT220	MANE	1.13	11.42	391.55	0.10	15.00	11.38	390.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5375E+01 EXCESS=0.0000E+00 OUTFLOW=0.5376E+01 BASIN STORAGE= 0.2047E-07 PERCENT ERROR= 0.0									
0.12	RT303	MANE	1.43	4.33	363.74	0.12	15.00	4.00	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1568E+01 EXCESS=0.0000E+00 OUTFLOW=0.1568E+01 BASIN STORAGE= 0.1453E-09 PERCENT ERROR= 0.0									
0.12	RT305	MANE	3.08	5.02	368.21	0.12	15.00	4.98	375.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1967E+01 EXCESS=0.0000E+00 OUTFLOW=0.1966E+01 BASIN STORAGE= 0.3429E-08 PERCENT ERROR= 0.0									
0.12	RT311	MANE	4.64	10.10	382.99	0.12	15.00	9.87	390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4089E+01 EXCESS=0.0000E+00 OUTFLOW=0.4088E+01 BASIN STORAGE=
0.7901E-07 PERCENT ERROR= 0.0

0.11 RT316 MANE 4.62 24.38 396.26 0.11 15.00 23.93 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1098E+02 EXCESS=0.0000E+00 OUTFLOW=0.1097E+02 BASIN STORAGE=
0.5349E-06 PERCENT ERROR= 0.1

0.11 RT401 MANE 1.15 26.57 393.23 0.11 15.00 26.11 405.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1206E+02 EXCESS=0.0000E+00 OUTFLOW=0.1206E+02 BASIN STORAGE=
0.1769E-06 PERCENT ERROR= 0.0

0.11 RT405 MANE 3.16 28.62 398.25 0.11 15.00 28.59 405.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1332E+02 EXCESS=0.0000E+00 OUTFLOW=0.1331E+02 BASIN STORAGE=
0.8449E-06 PERCENT ERROR= 0.0

0.12 RT101 MANE 3.92 1.45 381.61 0.12 15.00 1.44 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5779E+00 EXCESS=0.0000E+00 OUTFLOW=0.5776E+00 BASIN STORAGE=
0.2828E-08 PERCENT ERROR= 0.1

0.15 RT103 MANE 1.40 7.23 392.78 0.15 15.00 7.23 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2581E+01 EXCESS=0.0000E+00 OUTFLOW=0.2581E+01 BASIN STORAGE=
0.4253E-08 PERCENT ERROR= 0.0

0.16 RT105A MANE 1.56 9.80 379.28 0.16 15.00 9.55 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3378E+01 EXCESS=0.0000E+00 OUTFLOW=0.3378E+01 BASIN STORAGE=
0.8132E-08 PERCENT ERROR= 0.0

0.17 RT105B MANE 1.43 15.29 378.21 0.17 15.00 14.85 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4801E+01 EXCESS=0.0000E+00 OUTFLOW=0.4801E+01 BASIN STORAGE=
0.1447E-07 PERCENT ERROR= 0.0

0.17 RT107 MANE 2.75 16.13 379.80 0.17 15.00 15.53 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5234E+01 EXCESS=0.0000E+00 OUTFLOW=0.5231E+01 BASIN STORAGE=
0.6475E-07 PERCENT ERROR= 0.0

0.18 RT109 MANE 6.35 21.54 388.84 0.18 15.00 21.45 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6924E+01 EXCESS=0.0000E+00 OUTFLOW=0.6918E+01 BASIN STORAGE=
0.8610E-06 PERCENT ERROR= 0.1

0.13 RT407 MANE 1.93 56.12 394.22 0.13 15.00 56.10 405.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2364E+02 EXCESS=0.0000E+00 OUTFLOW=0.2364E+02 BASIN STORAGE=
0.1329E-05 PERCENT ERROR= 0.0

0.13 RT506 MANE 1.60 61.99 408.09 0.13 15.00 61.51 405.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2666E+02 EXCESS=0.0000E+00 OUTFLOW=0.2666E+02 BASIN STORAGE=
0.1715E-05 PERCENT ERROR= 0.0

0.13 RT507 MANE 2.53 63.11 410.94 0.13 15.00 61.77 405.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2767E+02 EXCESS=0.0000E+00 OUTFLOW=0.2766E+02 BASIN STORAGE=
0.3425E-05 PERCENT ERROR= 0.0

0.14 RT509 MANE 4.02 65.78 413.58 0.14 15.00 64.98 420.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2941E+02 EXCESS=0.0000E+00 OUTFLOW=0.2939E+02 BASIN STORAGE=
0.9226E-05 PERCENT ERROR= 0.0

0.14 RT511 MANE 0.72 66.50 421.37 0.14 15.00 66.24 420.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3032E+02 EXCESS=0.0000E+00 OUTFLOW=0.3032E+02 BASIN STORAGE=
0.2158E-05 PERCENT ERROR= 0.0

0.22 RT601 MANE 2.70 3.81 366.32 0.22 15.00 3.31 360.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7321E+00 EXCESS=0.0000E+00 OUTFLOW=0.7316E+00 BASIN STORAGE=
0.1146E-08 PERCENT ERROR= 0.1

0.14 RT604 MANE 1.79 71.70 422.58 0.14 15.00 71.35 420.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3367E+02 EXCESS=0.0000E+00 OUTFLOW=0.3367E+02 BASIN STORAGE=
0.5933E-05 PERCENT ERROR= 0.0

0.15 RT610 MANE 3.53 94.42 412.39 0.15 15.00 82.25 420.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3774E+02 EXCESS=0.0000E+00 OUTFLOW=0.3773E+02 BASIN STORAGE=
0.2207E-04 PERCENT ERROR= 0.0

0.15 RT612 MANE 2.63 75.61 442.59 0.15 15.00 75.44 450.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3891E+02 EXCESS=0.0000E+00 OUTFLOW=0.3891E+02 BASIN STORAGE=
0.2231E-04 PERCENT ERROR= 0.0

0.22 RT613 MANE 2.09 7.48 364.64 0.22 15.00 6.79 360.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1426E+01 EXCESS=0.0000E+00 OUTFLOW=0.1426E+01 BASIN STORAGE=
0.1212E-08 PERCENT ERROR= 0.0

0.15 RT614 MANE 0.87 79.64 451.83 0.15 15.00 79.12 450.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4262E+02 EXCESS=0.0000E+00 OUTFLOW=0.4262E+02 BASIN STORAGE=
0.7101E-05 PERCENT ERROR= 0.0

0.15 RT617 MANE 2.69 79.20 456.80 0.15 15.00 78.09 465.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4289E+02 EXCESS=0.0000E+00 OUTFLOW=0.4288E+02 BASIN STORAGE=
0.3317E-04 PERCENT ERROR= 0.0

0.18 RT703 MANE 2.52 84.43 470.22 0.18 15.00 84.25 465.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5075E+02 EXCESS=0.0000E+00 OUTFLOW=0.5073E+02 BASIN STORAGE=
0.4694E-04 PERCENT ERROR= 0.0

*** NORMAL END OF HEC-1 ***

5 year existing
HEC1 S/N: 1343001909 HMVersion 6.33 Data File: C:\WINNT\TEMP\vbh0800.TMP

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*****  
*****  
*  
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *  
* U. S. ARMY CORPS OF ENGINEERS *  
*                    MAY 1991 *  
* HYDROLOGIC ENGINEERING CENTER *  
*                    VERSION 4.0.1E *  
* 609 SECOND STREET *  
* *  
* DAVIS, CALIFORNIA 95616 *  
* RUN DATE 06/19/2001 TIME 16:43:37 *  
* (916) 756-1104 *  
* *  
*****  
*****
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  X    X  XXXXXXX  XXXXX        X  
  X    X  X        X    X        XX  
  X    X  X        X            X  
XXXXXXX  XXXX    X            XXXXX  X  
  X    X  X        X            X  
  X    X  X        X        X        X  
  X    X  XXXXXXX  XXXXX        XXX
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.....  
::: Full Microcomputer Implementation :::  
:::                    by                :::  
:::                    Haestad Methods, Inc        :::  
.....  
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37 Brookside Road * Waterbury, Connecticut 06708 * (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION.

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

ID	LINE	1	2	3	4	5	6	7	8	9	10
	1	ID	Type	IIA storm							
	2	IT	15	0	0	288					
	3	ID	5								
	4	KK	SC205								
	5	KM	Smith Creek 205 Runoff								
	6	KD						22			
	7	BA	0.0970								
	8	PB	2.6								
	9	IN	15								
0.0165	10	PC	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143
0.0600	11	PC	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
0.8000	12	PC	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
0.8600	13	PC	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
0.8975	14	PC	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
0.9300	15	PC	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270
0.9550	16	PC	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
0.9800	17	PC	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
0.9925	18	PC	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
	19	PC	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
	20	LS	0	64							
	21	UD	0.257								
	22	KK	RT205								
	23	KM	Smith Creek Route 205 to 207								
	24	KD						22			
	25	RK	1530	0.0431	0.055			TRAP		2	
	26	KK	SC207								
	27	KM	Smith Creek 207 Runoff								
	28	KD						22			
	29	BA	0.12								
	30	PB	2.6								
	31	LS	0	65							
	32	UD	0.367								
	33	KK	SC213								
	34	KM	Smith Creek 213 Runoff								
	35	KD						22			
	36	BA	0.1243								
	37	PB	2.6								
	38	LS	0	66							
	39	UD	0.382								
	40	KK	DP213								
	41	KM	Combine RT205 SC207 and SC213								
	42	KD						22			
	43	HC	3								
	44	KK	RT213								
	45	KM	Smith Creek Route 213 to 215								
	46	KD						22			
	47	RK	1360	0.0493	0.055			TRAP		2	

LINE	1	2	3	4	5	6	7	8	9	10
ID.										
48			KK	SC209						
49			KM	Smith Creek 209 Runoff						
50			KD					22		
51			BA	0.1351						
52			PB	2.6						
53			LS	0	61					
54			UD	0.336						
55			KK	SC211						
56			KM	Smith Creek 211 Runoff						
57			KD					22		
58			BA	0.0799						
59			PB	2.6						
60			LS	0	62					
61			UD	0.418						
62			KK	SC215						
63			KM	Smith Creek 215 Runoff						
64			KD					22		
65			BA	0.0589						
66			PB	2.6						
67			LS	0	62					
68			UD	0.227						
69			KK	DP215						
70			KM	Combine RT213 SC209 SC211 and SC215						
71			KD					22		
72			HC	4						
73			KK	RT215						
74			KM	Smith Creek Route 215 to 219						
75			KD					22		
76			RK	2110 0.0446 0.0745				TRAP		2
77			KK	SC219						
78			KM	Smith Creek 219 Runoff						
79			KD					22		
80			BA	0.1298						
81			PB	2.6						
82			LS	0	61					
83			UD	0.362						
84			KK	DP219						
85			KM	Combine RT215 and SC219						
86			KD					22		
87			HC	2						
88			KK	SC201						
89			KM	Smith Creek 201 Runoff						
90			KD					22		
91			BA	0.1216						
92			PB	2.6						
93			LS	0	62					
94			UD	0.340						

LINE	ID	1	2	3	4	5	6	7	8	9	10
184											
185											
186									22		
187											
188											
189											
190											
191											
192											
193									22		
194											
195											
196											
197									22		
198									TRAP		2
199											
200											
201									22		
202											
203											
204											
205											
206											
207											
208									22		
209											
210											
211											
212											
213											
214											
215									22		
216											
217											
218											
219									22		
220											
221											
222											
223									22		
224									TRAP	1	2

ID	LINE	1	2	3	4	5	6	7	8	9	10
	225			KK	SC401						
	226			KM	Smith Creek 401 Runoff						
	227			KD					22		
	228			BA	0.1524						
	229			PB	2.6						
	230			LS	0	65					
	231			UD	0.437						
	232			KK	DP401						
	233			KM	Combine RT316 and SC401						
	234			KD					22		
	235			HC	2						
	236			KK	RT401						
	237			KM	Smith Creek Route 401 to 405						
	238			KD					22		
	239			RK	840	0.0548	0.120		TRAP	1	2
	240			KK	SC403						
	241			KM	Smith Creek 403 Runoff						
	242			KD					22		
	243			BA	0.1007						
	244			PB	2.6						
	245			LS	0	66					
	246			UD	0.333						
	247			KK	SC405						
	248			KM	Smith Creek 405 Runoff						
	249			KD					22		
	250			BA	0.0677						
	251			PB	2.6						
	252			LS	0	64					
	253			UD	0.356						
	254			KK	DP405						
	255			KM	Combine RT401 SC403 and SC405						
	256			KD					22		
	257			HC	3						
	258			KK	RT405						
	259			KM	Smith Creek Route 405 to 407						
	260			KD					22		
	261			RK	1500	0.0210	0.120		TRAP	1	2
	262			KK	SC101						
	263			KM	Smith Creek 101 Runoff						
	264			KD					22		
	265			BA	0.0920						
	266			PB	2.6						
	267			LS	0	64					
	268			UD	0.353						

LINE	1	2	3	4	5	6	7	8	9	10
314										
315										
316									22	
317									TRAP	2
318										
319										
320									22	
321										
322										
323										
324										
325										
326										
327									22	
328										
329										
330										
331										
332										
333										
334										
335									22	
336										
337										
338										
339									22	
340									TRAP	2
341										
342										
343									22	
344										
345										
346										
347										
348										
349										
350									22	
351										
352										
353										
354									22	
355									TRAP	2

LINE	1	2	3	4	5	6	7	8	9	10
356										
357										
358									22	
359										
360										
361										
362										
363										
364										
365									22	
366										
367										
368										
369									22	
370									TRAP	2
371										
372										
373									22	
374										
375										
376										
377										
378										
379										
380									22	
381										
382										
383										
384									22	
385										
386										
387										
388										
389										
390										
391									22	
392										
393										
394										
395									22	
396									TRAP	1 2

LINE	1	2	3	4	5	6	7	8	9	10
ID	1	2	3	4	5	6	7	8	9	10
482			KK	RT601						
483			KM	Tributary Route 601 to 603						
484			KD					22		
485			RK	1170	0.0359	0.090		TRAP		2
486			KK	SC603						
487			KM	Smith Creek 603 Runoff						
488			KD					22		
489			BA	0.2514						
490			PB	2.6						
491			LS	0	68					
492			UD	0.325						
493			KK	DP603						
494			KM	Combine RT601 and SC603						
495			KD					22		
496			HC	2						
497			KK	DP604						
498			KM	Combine RT511 and DP603						
499			KD					22		
500			HC	2						
501			KK	RT604						
502			KM	Smith Creek Route 604 to 609						
503			KD					22		
504			RK	1380	0.0236	0.0928		TRAP	2	1
505			KK	SC605						
506			KM	Smith Creek 605 Runoff						
507			KD					22		
508			BA	0.1283						
509			PB	2.6						
510			LS	0	69					
511			UD	0.494						
512			KK	SC607						
513			KM	Smith Creek 607 Runoff						
514			KD					22		
515			BA	0.0840						
516			PB	2.6						
517			LS	0	69					
518			UD	0.270						
519			KK	SC609						
520			KM	Smith Creek 609 Runoff						
521			KD					22		
522			BA	0.1389						
523			PB	2.6						
524			LS	0	69					
525			UD	0.342						

LINE	1	2	3	4	5	6	7	8	9	10
ID										
570	KK	RT613								
571	KM	SMITH CREEK ROUTE 613 TO DP 613								
572	KD							22		
573	RK	2000	0.0360	0.030				TRAP	2	4
574	KK	SC615B								
575	KM	Smith Creek 615B Runoff								
576	KD							22		
577	BA	0.0313								
578	PB	2.6								
579	LS	0	78							
580	UD	0.160								
581	KK	RES614								
582	KM	EXISTING POND 614								
583	KD							22		
584	RS	1	STDR	-1						
585	SV	0	0.067	0.32	0.67	1.16	1.5			
586	SE	6722	6724	6726	6728	6730	6732			
587	SQ	0	4	6	10	13.3	20			
588	SE	6722	6724	6726	6728	6730	6732			
589	KK	SC617A								
590	KM									
591	KD							22		
592	BA	0.0701								
593	PB	2.6								
594	LS	0	69							
595	UD	0.258								
596	KK	SC615A								
597	KM	SMITH CREEK 615A								
598	KD							22		
599	BA	0.0567								
600	PB	2.6								
601	LS	0	69							
602	UD	0.180								
603	KK	DP613								
604	KM	COMBINE RT612 SC615A SC617A RT613 RES614								
605	KD							22		
606	HC	5								
607	KK	RT614								
608	KM	SMITH CREEK ROUTE 613 TO 617								
609	KD							22		
610	RK	1200	0.022	0.030				TRAP	2	4
611	KK	SC617B								
612	KM	Smith Creek 617B Runoff								
613	KD							22		
614	BA	0.0215								
615	PB	2.6								
616	LS	0	69							

HEC1 S/N: 1343001909

HMVersion 6.33

Data File: C:\WINNT\TEMP\vbh0800.TMP

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS. AREA IN SQUARE MILES

MAXIMUM STAGE	TIME OF OPERATION MAX STAGE	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA
					6-HOUR	24-HOUR	72-HOUR	
	HYDROGRAPH AT	SC205	9.	6.00	2.	1.	0.	0.10
	ROUTED TO	RT205	9.	6.00	2.	1.	0.	0.10
	HYDROGRAPH AT	SC207	12.	6.00	3.	1.	0.	0.12
	HYDROGRAPH AT	SC213	13.	6.00	3.	1.	0.	0.12
	3 COMBINED AT	DP213	34.	6.00	8.	3.	1.	0.34
	ROUTED TO	RT213	31.	6.00	8.	3.	1.	0.34
	HYDROGRAPH AT	SC209	7.	6.00	2.	1.	0.	0.14
	HYDROGRAPH AT	SC211	4.	6.25	1.	1.	0.	0.08
	HYDROGRAPH AT	SC215	4.	6.00	1.	0.	0.	0.06
	4 COMBINED AT	DP215	46.	6.00	13.	5.	2.	0.62
	ROUTED TO	RT215	42.	6.25	12.	5.	2.	0.62
	HYDROGRAPH AT	SC219	6.	6.00	2.	1.	0.	0.13
	2 COMBINED AT	DP219	48.	6.25	14.	6.	2.	0.75
	HYDROGRAPH AT	SC201	7.	6.00	2.	1.	0.	0.12
	ROUTED TO	RT201	6.	6.00	2.	1.	0.	0.12
	HYDROGRAPH AT	SC203	6.	6.00	2.	1.	0.	0.11
	2 COMBINED AT	DP203	12.	6.00	4.	2.	1.	0.23
	ROUTED TO	RT203	11.	6.25	4.	2.	1.	0.23
	HYDROGRAPH AT	SC217	3.	6.00	1.	0.	0.	0.05
	2 COMBINED AT	DP217	14.	6.00	4.	2.	1.	0.29
	2 COMBINED AT	DP220	61.	6.25	19.	8.	3.	1.03
	ROUTED TO	RT220	61.	6.25	19.	8.	3.	1.03
	HYDROGRAPH AT	SC301	11.	6.00	3.	1.	0.	0.12

HYDROGRAPH AT	SC303	12	6.00	3	1	0	0.13
2 COMBINED AT	DP303	23	6.00	5	2	1	0.25
ROUTED TO	RT303	22	6.00	5	2	1	0.25
HYDROGRAPH AT	SC305	6	6.00	1	1	0	0.06
2 COMBINED AT	DP305	28	6.00	7	3	1	0.31
ROUTED TO	RT305	24	6.00	7	3	1	0.31
HYDROGRAPH AT	SC307	8	6.25	2	1	0	0.11
HYDROGRAPH AT	SC309	10	6.00	3	1	0	0.12
HYDROGRAPH AT	SC311	10	6.00	2	1	0	0.11
4 COMBINED AT	DP311	51	6.00	14	5	2	0.65
ROUTED TO	RT311	48	6.25	14	5	2	0.65
HYDROGRAPH AT	SC313	12	6.00	3	1	0	0.15
HYDROGRAPH AT	SC315	8	6.00	2	1	0	0.09
3 COMBINED AT	DP315	65	6.25	19	7	2	0.89
2 COMBINED AT	DP316	125	6.25	38	15	5	1.92
ROUTED TO	RT316	121	6.25	37	15	5	1.92
HYDROGRAPH AT	SC401	13	6.25	4	1	0	0.15
2 COMBINED AT	DP401	133	6.25	41	16	5	2.08
ROUTED TO	RT401	128	6.25	41	16	5	2.08
HYDROGRAPH AT	SC403	12	6.00	3	1	0	0.10
HYDROGRAPH AT	SC405	6	6.00	1	1	0	0.07
3 COMBINED AT	DP405	142	6.25	45	18	6	2.25
ROUTED TO	RT405	133	6.50	45	18	6	2.25
HYDROGRAPH AT	SC101	8	6.00	2	1	0	0.09
ROUTED TO	RT101	7	6.25	2	1	0	0.09
HYDROGRAPH AT	SC103	17	6.00	4	2	1	0.17
HYDROGRAPH AT							

		SC105A	12.	6.00	2	1	0	0.07
	3 COMBINED AT	DP103	35.	6.00	8	3	1	0.33
	ROUTED TO	RES106	28	6.25	8	3	1	0.33
7321.12	6.25							
	ROUTED TO	RT103	27.	6.25	8.	3	1.	0.33
	HYDROGRAPH AT	SC105B	12.	6.00	2	1.	0.	0.07
	2 COMBINED AT	DP105	35.	6.25	11	4.	1.	0.40
	ROUTED TO	RT105A	34.	6.25	11.	4.	1.	0.40
	HYDROGRAPH AT	SC107A	22.	6.00	4	2.	1.	0.14
	ROUTED TO	RES108	19.	6.00	4.	2.	1.	0.14
7341.89	6.00							
	2 COMBINED AT	DP107A	52.	6.25	15.	6.	2.	0.53
	ROUTED TO	RT105B	51.	6.25	15.	6.	2.	0.53
	HYDROGRAPH AT	SC107B	7.	6.00	1.	0.	0.	0.04
	2 COMBINED AT	DP107B	55.	6.25	16.	6.	2.	0.57
	ROUTED TO	RT107	53.	6.25	16.	6.	2.	0.57
	HYDROGRAPH AT	SC109	22.	6.00	5.	2.	1.	0.16
	2 COMBINED AT	DP109	73.	6.25	21.	8.	3.	0.74
	ROUTED TO	RT109	69.	6.50	21.	8.	3.	0.74
	HYDROGRAPH AT	SC111	30.	6.00	7.	2.	1.	0.19
	2 COMBINED AT	DP111	91.	6.25	28.	10.	3.	0.93
	HYDROGRAPH AT	SC407	14.	6.25	4.	2.	1.	0.17
	3 COMBINED AT	DP407	233	6.25	76	30.	10.	3.34
	ROUTED TO	RT407	229.	6.50	76.	30.	10.	3.34
	HYDROGRAPH AT	SC501	13.	6.00	3	1.	0.	0.12
	HYDROGRAPH AT	SC503	9	6.00	3	1.	0	0.12
	HYDROGRAPH AT	SC505	18.	6.00	5	2.	1.	0.19
	3 COMBINED AT	DP505	40.	6.00	10	4	1	0.43

2 COMBINED AT	DP506	252	6 50	86.	34	11.	3. 77
ROUTED TO	RT506	252.	6 50	86.	34.	11.	3. 77
HYDROGRAPH AT	SC507	16	6 00	3.	1	0.	0. 10
2 COMBINED AT	DP507	257.	6 50	89.	35	12	3. 87
ROUTED TO	RT507	254	6 50	89.	35.	12.	3. 87
HYDROGRAPH AT	SC509	22.	6. 00	5.	2	1.	0. 15
2 COMBINED AT	DP509	268.	6. 50	94.	37.	12.	4. 02
ROUTED TO	RT509	258.	6. 50	93.	37	12.	4. 02
HYDROGRAPH AT	SC511	15.	6. 00	3.	1.	0.	0. 09
2 COMBINED AT	DP511	264.	6. 50	96.	38	13.	4. 11
ROUTED TO	RT511	261.	6. 50	96.	38.	13.	4. 11
HYDROGRAPH AT	SC601	11.	6. 00	2.	1	0.	0. 06
ROUTED TO	RT601	10.	6. 00	2.	1.	0.	0. 06
HYDROGRAPH AT	SC603	40.	6. 00	8.	3	1.	0. 25
2 COMBINED AT	DP603	50.	6. 00	10.	4.	1.	0. 31
2 COMBINED AT	DP604	284.	6. 50	106.	41.	14.	4. 43
ROUTED TO	RT604	277.	6. 50	106.	42	14.	4. 43
HYDROGRAPH AT	SC605	17.	6. 25	4.	2.	1.	0. 13
HYDROGRAPH AT	SC607	16.	6. 00	3.	1.	0.	0. 08
HYDROGRAPH AT	SC609	24.	6. 00	5.	2.	1.	0. 14
4 COMBINED AT	DP609	306.	6. 50	117.	46.	15.	4. 78
ROUTED TO	RES610	307.	6. 75	114.	46.	15.	4. 78
6823. 43	6 75						
ROUTED TO	RT610	298	6 75	114.	46	15.	4. 78
HYDROGRAPH AT	SC611	20.	6. 00	4.	1	0.	0. 11
2 COMBINED AT	DP611	303.	6. 75	116.	47	16	4. 89
ROUTED TO	RES612	302	6. 75	116.	47	16.	4. 89

6763.42 6.75

ROUTED TO	RT612	293	7.00	115.	47	16.	4.89
HYDROGRAPH AT	SC613	22.	6.00	4.	2.	1.	0.12
ROUTED TO	RT613	21.	6.00	4.	2.	1.	0.12
HYDROGRAPH AT	SC615B	18.	5.75	2.	1.	0.	0.03
ROUTED TO	RES614	6.	6.25	2.	1.	0.	0.03

6726.20 6.25

HYDROGRAPH AT	SC617A	13.	6.00	2.	1.	0.	0.07
HYDROGRAPH AT	SC615A	13.	5.75	2.	1.	0.	0.06
5 COMBINED AT	DP613	307.	7.00	124.	51.	17.	5.17
ROUTED TO	RT614	307.	7.00	124.	51.	17.	5.17
HYDROGRAPH AT	SC617B	4.	6.00	1.	0.	0.	0.02
2 COMBINED AT	DP617	308.	7.00	125.	51.	17.	5.19
ROUTED TO	RT617	305.	7.00	125.	51.	17.	5.19
HYDROGRAPH AT	SC701	68.	6.00	12.	3.	1.	0.07
HYDROGRAPH AT	SC703	79.	5.75	9.	3.	1.	0.13
3 COMBINED AT	DP703	320.	7.00	142.	57.	19.	5.39
ROUTED TO	R1703	315.	7.00	141.	57.	19.	5.39
HYDROGRAPH AT	SC705	15.	6.00	3.	1.	0.	0.09
2 COMBINED AT	DP705	319.	7.00	144.	58.	20.	5.48

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

VOLUME (IN)	IATAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO COMPUTATION INTERVAL	
								PEAK (CFS)	TIME TO PEAK (MIN)
0.31	RT205	MANE	1.84	9.09	362.92	0.31	15.00	8.67	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1585E+01 EXCESS=0.0000E+00 OUTFLOW=0.1585E+01 BASIN STORAGE= 0.9607E-09 PERCENT ERROR= 0.0									
0.34	RT213	MANE	1.21	33.35	362.23	0.34	15.00	31.00	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6175E+01 EXCESS=0.0000E+00 OUTFLOW=0.6175E+01 BASIN STORAGE= 0.2334E-08 PERCENT ERROR= 0.0									
0.30	RT215	MANE	2.18	45.48	364.86	0.30	15.00	42.31	375.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.9692E+01 EXCESS=0.0000E+00 OUTFLOW=0.9689E+01 BASIN STORAGE= 0.1776E-07 PERCENT ERROR= 0.0									
0.25	RT201	MANE	1.93	7.37	364.44	0.25	15.00	6.42	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1632E+01 EXCESS=0.0000E+00 OUTFLOW=0.1632E+01 BASIN STORAGE= 0.6762E-09 PERCENT ERROR= 0.0									
0.24	RT203	MANE	2.47	12.33	365.62	0.24	15.00	11.04	375.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2980E+01 EXCESS=0.0000E+00 OUTFLOW=0.2979E+01 BASIN STORAGE= 0.6994E-08 PERCENT ERROR= 0.0									
0.27	RT220	MANE	0.87	60.68	375.70	0.27	15.00	60.61	375.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1492E+02 EXCESS=0.0000E+00 OUTFLOW=0.1492E+02 BASIN STORAGE= 0.1850E-07 PERCENT ERROR= 0.0									
0.31	RT303	MANE	0.98	22.89	362.26	0.31	15.00	22.04	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4079E+01 EXCESS=0.0000E+00 OUTFLOW=0.4079E+01 BASIN STORAGE= 0.1669E-09 PERCENT ERROR= 0.0									
0.31	RT305	MANE	2.06	27.25	364.73	0.31	15.00	24.39	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5123E+01 EXCESS=0.0000E+00 OUTFLOW=0.5121E+01 BASIN STORAGE= 0.3647E-08 PERCENT ERROR= 0.0									
0.31	RT311	MANE	3.18	51.18	366.43	0.31	15.00	48.01	375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1067E+02 EXCESS=0.0000E+00 OUTFLOW=0.1067E+02 BASIN STORAGE=
0.7116E-07 PERCENT ERROR= 0.1

0.29 RT316 MANE 3.13 124.26 380.07 0.29 15.00 120.66 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2951E+02 EXCESS=0.0000E+00 OUTFLOW=0.2948E+02 BASIN STORAGE=
0.5156E-06 PERCENT ERROR= 0.1

0.29 RT401 MANE 0.87 133.21 376.79 0.29 15.00 128.32 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3215E+02 EXCESS=0.0000E+00 OUTFLOW=0.3215E+02 BASIN STORAGE=
0.2247E-06 PERCENT ERROR= 0.0

0.29 RT405 MANE 2.17 141.15 379.21 0.29 15.00 133.02 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3529E+02 EXCESS=0.0000E+00 OUTFLOW=0.3529E+02 BASIN STORAGE=
0.9137E-06 PERCENT ERROR= 0.0

0.31 RT101 MANE 2.50 7.74 365.60 0.31 15.00 6.83 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1504E+01 EXCESS=0.0000E+00 OUTFLOW=0.1503E+01 BASIN STORAGE=
0.2943E-08 PERCENT ERROR= 0.1

0.36 RT103 MANE 1.08 27.89 377.31 0.36 15.00 26.82 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6220E+01 EXCESS=0.0000E+00 OUTFLOW=0.6220E+01 BASIN STORAGE=
0.4515E-08 PERCENT ERROR= 0.0

0.38 RT105A MANE 1.09 35.22 377.44 0.38 15.00 34.43 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7943E+01 EXCESS=0.0000E+00 OUTFLOW=0.7943E+01 BASIN STORAGE=
0.9605E-08 PERCENT ERROR= 0.0

0.39 RT105B MANE 1.00 52.17 376.77 0.39 15.00 51.38 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1111E+02 EXCESS=0.0000E+00 OUTFLOW=0.1111E+02 BASIN STORAGE=
0.1345E-07 PERCENT ERROR= 0.0

0.39 RT107 MANE 2.15 55.01 379.70 0.39 15.00 53.34 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1208E+02 EXCESS=0.0000E+00 OUTFLOW=0.1208E+02 BASIN STORAGE=
0.7878E-07 PERCENT ERROR= 0.0

0.40 RT109 MANE 4.69 73.22 384.37 0.40 15.00 69.03 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1587E+02 EXCESS=0.0000E+00 OUTFLOW=0.1586E+02 BASIN STORAGE=
0.6500E-06 PERCENT ERROR= 0.0

0.33 RT407 MANE 1.35 233.08 378.44 0.33 15.00 229.22 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5887E+02 EXCESS=0.0000E+00 OUTFLOW=0.5886E+02 BASIN STORAGE=
0.1321E-05 PERCENT ERROR= 0.0

0.33 RT506 MANE 1.18 251.70 390.88 0.33 15.00 251.52 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6656E+02 EXCESS=0.0000E+00 OUTFLOW=0.6655E+02 BASIN STORAGE=
0.1764E-05 PERCENT ERROR= 0.0

0.33 RT507 MANE 1.78 256.90 393.50 0.33 15.00 254.21 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6889E+02 EXCESS=0.0000E+00 OUTFLOW=0.6888E+02 BASIN STORAGE=
0.3587E-05 PERCENT ERROR= 0.0

0.34 RT509 MANE 2.84 266.33 395.17 0.34 15.00 258.27 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7275E+02 EXCESS=0.0000E+00 OUTFLOW=0.7272E+02 BASIN STORAGE=
0.9400E-05 PERCENT ERROR= 0.0

0.34 RTS11 MANE 0.63 263.95 391.69 0.34 15.00 260.89 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7478E+02 EXCESS=0.0000E+00 OUTFLOW=0.7478E+02 BASIN STORAGE=
0.2261E-05 PERCENT ERROR= 0.0

0.47 RT601 MANE 2.03 11.36 363.59 0.47 15.00 10.33 360.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1578E+01 EXCESS=0.0000E+00 OUTFLOW=0.1578E+01 BASIN STORAGE=
0.1279E-08 PERCENT ERROR= 0.0

0.35 RT604 MANE 1.21 283.67 392.45 0.35 15.00 276.80 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.8223E+02 EXCESS=0.0000E+00 OUTFLOW=0.8223E+02 BASIN STORAGE=
0.5834E-05 PERCENT ERROR= 0.0

0.36 RT610 MANE 2.65 304.15 408.54 0.36 15.00 298.31 405.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.9110E+02 EXCESS=0.0000E+00 OUTFLOW=0.9105E+02 BASIN STORAGE=
0.2469E-04 PERCENT ERROR= 0.1

0.36 RT612 MANE 1.85 301.86 408.86 0.36 15.00 293.15 420.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.9385E+02 EXCESS=0.0000E+00 OUTFLOW=0.9384E+02 BASIN STORAGE=
0.2385E-04 PERCENT ERROR= 0.0

0.47 RT613 MANE 1.64 22.20 363.36 0.47 15.00 20.81 360.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3073E+01 EXCESS=0.0000E+00 OUTFLOW=0.3073E+01 BASIN STORAGE=
0.1642E-08 PERCENT ERROR= 0.0

0.37 RT614 MANE 0.55 307.11 420.80 0.37 15.00 306.95 420.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1016E+03 EXCESS=0.0000E+00 OUTFLOW=0.1016E+03 BASIN STORAGE=
0.7237E-05 PERCENT ERROR= 0.0

0.37 RT617 MANE 1.96 306.96 423.06 0.37 15.00 305.49 420.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1022E+03 EXCESS=0.0000E+00 OUTFLOW=0.1022E+03 BASIN STORAGE=
0.3398E-04 PERCENT ERROR= 0.0

0.40 RT703 MANE 1.80 319.96 423.58 0.40 15.00 315.36 420.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1147E+03 EXCESS=0.0000E+00 OUTFLOW=0.1147E+03 BASIN STORAGE=
0.5277E-04 PERCENT ERROR= 0.0

*** NORMAL END OF HEC-1 ***

10 year existing
HEC1 S/N: 1343001909 HMVersion: 6.33 Data File: C:\WINNT\TEMP\~vbh2A2B TMP

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*****  
*  
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *  
* U. S. ARMY CORPS OF ENGINEERS *  
* MAY 1991 *  
* HYDROLOGIC ENGINEERING CENTER *  
* VERSION 4.0 1E *  
* 609 SECOND STREET *  
* DAVIS, CALIFORNIA 95616 *  
* RUN DATE 06/19/2001 TIME 16:43:07 *  
* (916) 756-1104 *  
*  
*****
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  X   X  XXXXXXXX  XXXXX      X  
  X   X  X        X   X      XX  
  X   X  X        X           X  
  XXXXXX XXXX   X           XXXX  X  
  X   X  X        X           X  
  X   X  X        X   X      X  
  X   X  XXXXXXXX  XXXXX      XXX
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.....  
: :  
: : Full Microcomputer Implementation : :  
: : by : :  
: : Haestad Methods, Inc. : :  
: : : :  
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37 Brookside Road * Waterbury, Connecticut 06708 * (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS: WRITE STAGE FREQUENCY,

DSS: READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE: GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Type	IIA	storn							
2	IT	15		0		0	288				
3	ID	5									
4	KK	SC205									
5	KM	Smith Creek 205 Runoff									
6	KD								22		
7	BA	0.0970									
8	PB	3									
9	IN	15									
10	PC	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143	
0.0165											
11	PC	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530	
0.0600											
12	PC	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900	
0.8000											
13	PC	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550	
0.8600											
14	PC	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938	
0.8975											
15	PC	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270	
0.9300											
16	PC	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525	
0.9550											
17	PC	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775	
0.9800											
18	PC	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913	
0.9925											
19	PC	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000				
20	LS	0	64								
21	UD	0	257								
22	KK	RT205									
23	KM	Smith Creek Route 205 to 213									
24	KD								22		
25	RK	1530	0.0431	0.055			TRAP			2	
26	KK	SC207									
27	KM	Smith Creek 207 Runoff									
28	KD								22		
29	BA	0.120									
30	PB	3									
31	LS	0	65								
32	UD	0.367									
33	KK	SC213									
34	KM	Smith Creek 213 Runoff									
35	KD								22		
36	BA	0.1243									
37	PB	3									
38	LS	0	66								
39	UD	0.382									
40	KK	DP213									
41	KM	Combine RT205 SC207 and SC213									
42	KD								22		
43	HC	3									
44	KK	RT213									
45	KM	Smith Creek Route 213 to 215									
46	KD								22		
47	RK	1360	0.0493	0.055			TRAP			2	

ID	LINE	1	2	3	4	5	6	7	8	9	10
184	KK	SC311									
185	KM	Smith Creek 311 Runoff									
186	KD								22		
187	BA	0 1064									
188	PB	3									
189	LS	0	64								
190	UD	0.295									
191	KK	DP311									
192	KM	Combine RT305 SC307 SC309 and SC311									
193	KD								22		
194	HC	4									
195	KK	RT311									
196	KM	Tributary Route 311 to 315									
197	KD								22		
198	RK	2860 0.0448 0.0888							TRAP		2
199	KK	SC313									
200	KM	Smith Creek 313 Runoff									
201	KD								22		
202	BA	0.1520									
203	PB	3									
204	LS	0	64								
205	UD	0.373									
206	KK	SC315									
207	KM	Smith Creek 315 Runoff									
208	KD								22		
209	BA	0.0886									
210	PB	3									
211	LS	0	64								
212	UD	0.350									
213	KK	DP315									
214	KM	Combine RT311 SC313 and SC315									
215	KD								22		
216	HC	3									
217	KK	DP316									
218	KM	Combine RT220 and DP315									
219	KD								22		
220	HC	2									
221	KK	RT316									
222	KM	Smith Creek Route 316 to 401									
223	KD								22		
224	RK	2575 0.0361 0.120							TRAP	1	2

ID	LINE	1	2	3	4	5	6	7	8	9	10
314	KK	RT105A									
315	KM	Tributary Route 105 to 107A									
316	KD								22		
317	RK	1000	0.0395	0.0727					TRAP		2
318	KK	SC107A									
319	KM	Smith Creek 107A Runoff									
320	KD								22		
321	BA	0.1367									
322	PB	3									
323	LS	0	68								
324	UD	0.287									
325	KK	RES108									
326	KM	EXISTING DETENTION POND 108									
327	KD								22		
328	RS	1	STOR	-1							
329	SV	0	0.2	0.68	1.35	2.32					
330	SE	7340	7342	7344	7346	7348					
331	SQ	0	20	48	220	822					
332	SE	7340	7342	7344	7346	7348					
333	KK	DP107A									
334	KM	Combine RT105A and RES108									
335	KD								22		
336	HC	2									
337	KK	RT105B									
338	KM	TRIBUTARY ROUTE 107A TO 107B									
339	KD								22		
340	RK	1000	0.0395	0.0727					TRAP		2
341	KK	SC107B									
342	KM	SMITH CREEK 107B RUNOFF									
343	KD								22		
344	BA	0.0408									
345	PB	3									
346	LS	0	68								
347	UD	0.287									
348	KK	DP107B									
349	KM	COMBINE RT105B AND SC107B									
350	KD								22		
351	HC	2									
352	KK	RT107									
353	KM	Tributary Route 107B to 109									
354	KD								22		
355	RK	1420	0.0359	0.120					TRAP		2

ID	LINE	1	2	3	4	5	6	7	8	9	10
356	KK	SC109									
357	KM	Smith Creek 109 Runoff									
358	KD								22		
359	BA	0.1637									
360	PB	3									
361	LS	0	68								
362	UD	0.398									
363	KK	DP109									
364	KM	Combine RT107 and SC109									
365	KD								22		
366	HC	2									
367	KK	RT109									
368	KM	Tributary Route 109 to 111									
369	KD								22		
370	RK	3840	0.0453	0.120					TRAP	2	
371	KK	SC111									
372	KM	Smith Creek 111 Runoff									
373	KD								22		
374	BA	0.1894									
375	PB	3									
376	LS	0	69								
377	UD	0.382									
378	KK	DP111									
379	KM	Combine RT109 and SC111									
380	KD								22		
381	HC	2									
382	KK	SC407									
383	KM	Smith Creek 407 Runoff									
384	KD								22		
385	BA	0.1685									
386	PB	3									
387	LS	0	65								
388	UD	0.455									
389	KK	DP407									
390	KM	Combine RT111 RT405 and SC407									
391	KD								22		
392	HC	3									
393	KK	RT407									
394	KM	SMITH CREEK ROUTE 407 TO 506									
395	KD								22		
396	RK	1105	0.0210	0.120					TRAP	1	2

HEC1 S/N: 1343001909

HMVersion: 6.33

Data File: C:\WINNT\TEMP\~vbh2A2B.TMP

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

MAXIMUM STAGE	TIME OF OPERATION MAX STAGE	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA
					6-HOUR	24-HOUR	72-HOUR	
	HYDROGRAPH AT	SC205	17	6.00	3.	1.	0.	0.10
	ROUTED TO	RT205	16.	6.00	3.	1.	0.	0.10
	HYDROGRAPH AT	SC207	21.	6.00	5.	2.	1.	0.12
	HYDROGRAPH AT	SC213	23.	6.00	5.	2.	1.	0.12
	3 COMBINED AT	DP213	60.	6.00	13.	5.	2.	0.34
	ROUTED TO	RT213	56.	6.00	13.	5.	2.	0.34
	HYDROGRAPH AT	SC209	15	6.00	3.	1.	0.	0.14
	HYDROGRAPH AT	SC211	8.	6.00	2.	1.	0.	0.08
	HYDROGRAPH AT	SC215	8.	6.00	2.	1.	0.	0.06
	4 COMBINED AT	DP215	86.	6.00	20.	8.	3.	0.62
	ROUTED TO	RT215	76.	6.00	20.	8.	3.	0.62
	HYDROGRAPH AT	SC219	13.	6.00	3.	1.	0.	0.13
	2 COMBINED AT	DP219	89.	6.00	24.	9.	3.	0.75
	HYDROGRAPH AT	SC201	15.	6.00	3.	1.	0.	0.12
	ROUTED TO	RT201	13.	6.00	3.	1.	0.	0.12
	HYDROGRAPH AT	SC203	13.	6.00	3.	1.	0.	0.11
	2 COMBINED AT	DP203	26.	6.00	6.	2.	1.	0.23
	ROUTED TO	RT203	24.	6.00	6.	2.	1.	0.23
	HYDROGRAPH AT	SC217	6.	5.75	1.	1.	0.	0.05
	2 COMBINED AT	DP217	30.	6.00	8.	3.	1.	0.29
	2 COMBINED AT	DP220	119.	6.00	31.	12.	4.	1.03
	ROUTED TO	RT220	113.	6.00	31.	12.	4.	1.03
	HYDROGRAPH AT	SC301	21.	6.00	4.	2.	1.	0.12

HYDROGRAPH AT	SC303	22	6.00	4.	2.	1.	0.13
2 COMBINED AT	DP303	42	6.00	9.	3.	1.	0.25
ROUTED TO	RT303	41	6.00	9.	3.	1.	0.25
HYDROGRAPH AT	SC305	10	6.00	2.	1.	0.	0.06
2 COMBINED AT	DP305	51	6.00	11.	4.	1.	0.31
ROUTED TO	RT305	46.	6.00	11.	4.	1.	0.31
HYDROGRAPH AT	SC307	14.	6.25	4.	1.	0.	0.11
HYDROGRAPH AT	SC309	18.	6.00	4.	2.	1	0.12
HYDROGRAPH AT	SC311	18	6.00	4.	1.	0.	0.11
4 COMBINED AT	DP311	96.	6.00	22.	8.	3.	0.65
ROUTED TO	RT311	86	6.25	22.	8.	3.	0.65
HYDROGRAPH AT	SC313	23.	6.00	5.	2.	1.	0.15
HYDROGRAPH AT	SC315	14.	6.00	3.	1.	0.	0.09
3 COMBINED AT	DP315	115.	6.25	30.	11.	4.	0.89
2 COMBINED AT	DP316	228.	6.00	62.	23.	8.	1.92
ROUTED TO	RT316	227.	6.25	61.	23.	8.	1.92
HYDROGRAPH AT	SC401	22.	6.00	6.	2.	1.	0.15
2 COMBINED AT	DP401	249.	6.25	67.	25.	8.	2.08
ROUTED TO	RT401	244.	6.25	67.	25.	8.	2.08
HYDROGRAPH AT	SC403	21.	6.00	4.	1	0.	0.10
HYDROGRAPH AT	SC405	11	6.00	2.	1.	0.	0.07
3 COMBINED AT	DP405	267.	6.25	73.	27	9.	2.25
ROUTED TO	RT405	253	6.25	73.	28.	9.	2.25
HYDROGRAPH AT	SC101	14.	6.00	3.	1	0.	0.09
ROUTED TO	RT101	12	6.00	3.	1	0.	0.09
HYDROGRAPH AT	SC103	30	6.00	6.	2	1	0.17
HYDROGRAPH AT							

		SC105A	19.	6.00	4	1.	0.	0.07
	3 COMBINED AT	DP103	61	6.00	13.	5.	2.	0.33
	ROUTED TO	RES106	48.	6.25	13	5.	2	0.33
7321.92	6.25							
	ROUTED TO	RT103	46.	6.25	13	5.	2	0.33
	HYDROGRAPH AT	SC105B	18.	6.00	4	1.	0.	0.07
	2 COMBINED AT	DP105	59.	6.25	16.	6.	2.	0.40
	ROUTED TO	RT105A	58.	6.25	16.	6.	2.	0.40
	HYDROGRAPH AT	SC107A	36.	6.00	7.	2.	1.	0.14
	ROUTED TO	RES108	28	6.25	7.	2.	1.	0.14
7342.58	6.25							
	2 COMBINED AT	DP107A	86.	6.25	23.	8	3.	0.53
	ROUTED TO	RT105B	85.	6.25	23.	8.	3.	0.53
	HYDROGRAPH AT	SC107B	11.	6.00	2.	1.	0.	0.04
	2 COMBINED AT	DP107B	91.	6.25	25.	9	3.	0.57
	ROUTED TO	RT107	88.	6.25	25.	9.	3.	0.57
	HYDROGRAPH AT	SC109	36.	6.00	8.	3.	1.	0.16
	2 COMBINED AT	DP109	119.	6.25	33	12.	4.	0.74
	ROUTED TO	RT109	111.	6.50	32.	12.	4.	0.74
	HYDROGRAPH AT	SC111	47.	6.00	10.	3.	1.	0.19
	2 COMBINED AT	DP111	149.	6.25	42	15.	5.	0.93
	HYDROGRAPH AT	SC407	24	6.25	6	2.	1.	0.17
	3 COMBINED AT	DP407	426	6.25	121	45.	15.	3.34
	ROUTED TO	RT407	406	6.25	121.	45	15.	3.34
	HYDROGRAPH AT	SC501	23.	6.00	5.	2.	1.	0.12
	HYDROGRAPH AT	SC503	18	6.00	4	2	1.	0.12
	HYDROGRAPH AT	SC505	32	6.00	7.	3	1.	0.19
	3 COMBINED AT	BP505	73.	6.00	16.	6	2.	0.43

2 COMBINED AT	DP506	463	6.25	137.	51.	17.	3.77
ROUTED TO	RT506	446.	6.25	137	51.	17.	3.77
HYDROGRAPH AT	SC507	25.	6.00	5.	2.	1.	0.10
2 COMBINED AT	DP507	460.	6.25	141.	53.	18.	3.87
ROUTED TO	RT507	444	6.50	142.	53.	18.	3.87
HYDROGRAPH AT	SC509	36.	6.00	8.	3.	1.	0.15
2 COMBINED AT	DP509	464.	6.50	149.	55.	19.	4.02
ROUTED TO	RT509	464.	6.50	149.	55.	19.	4.02
HYDROGRAPH AT	SC511	23.	6.00	4.	2.	1.	0.09
2 COMBINED AT	DP511	473.	6.50	153.	57.	19.	4.11
ROUTED TO	RT511	470.	6.50	153.	57.	19.	4.11
HYDROGRAPH AT	SC601	18.	6.00	3.	1.	0.	0.06
ROUTED TO	RT601	16	6.00	3.	1.	0.	0.06
HYDROGRAPH AT	SC603	64.	6.00	12.	4.	1.	0.25
2 COMBINED AT	DP603	80.	6.00	15	5.	2.	0.31
2 COMBINED AT	DP604	504.	6.50	167.	62.	21.	4.43
ROUTED TO	RT604	499.	6.50	168.	62.	21.	4.43
HYDROGRAPH AT	SC605	27.	6.25	7.	2.	1.	0.13
HYDROGRAPH AT	SC607	24.	6.00	4.	2.	1.	0.08
HYDROGRAPH AT	SC609	38.	6.00	7.	3.	1.	0.14
4 COMBINED AT	DP609	543.	6.50	185.	69.	23.	4.78
ROUTED TO	RES610	533.	6.50	182.	68.	23.	4.78
6823.76			6.50				
ROUTED TO	RT610	527.	6.50	180.	68.	23.	4.78
HYDROGRAPH AT	SC611	30.	6.00	6	2.	1.	0.11
2 COMBINED AT	DP611	536.	6.50	185.	70.	24.	4.89
ROUTED TO	RES612	533.	6.75	185	70.	24.	4.89

6764 03 6.75

ROUTED TO	RT612	526.	6.75	185.	70.	24	4.89
HYDROGRAPH AT	SC613	35.	6.00	6.	2.	1.	0.12
ROUTED TO	RT613	33.	6.00	6.	2.	1	0.12
HYDROGRAPH AT	SC615B	24.	5.75	3.	1.	0.	0.03
ROUTED TO	RES614	8	6.25	3.	1.	0.	0.03

6727.18 6.25

HYDROGRAPH AT	SC617A	20.	6.00	4	1.	0.	0.07
HYDROGRAPH AT	SC615A	21.	5.75	3.	1.	0.	0.06
5 COMBINED AT	DP613	550.	6.75	198.	76.	26.	5.17
ROUTED TO	RT614	546.	6.75	198.	76.	26.	5.17
HYDROGRAPH AT	SC617B	6.	5.75	1.	0.	0	0.02
2 COMBINED AT	DP617	547.	6.75	199.	76.	26.	5.19
ROUTED TO	RT617	532.	6.75	199.	76.	26.	5.19
HYDROGRAPH AT	SC701	83	6.00	14.	4.	1.	0.07
HYDROGRAPH AT	SC703	108.	5.75	12.	4.	1.	0.13
3 COMBINED AT	DP703	559.	6.75	221.	84.	28.	5.39
ROUTED TO	RT703	541.	6.75	221.	84.	28.	5.39
HYDROGRAPH AT	SC705	24.	6.00	5.	2.	1.	0.09
2 COMBINED AT	DP705	548.	6.75	225.	86.	29.	5.48

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

VOLUME	INSTAQ	ELEMENT	DT	PEAK	TIME TO	VOLUME	DT	INTERPOLATED TO	
								COMPUTATION INTERVAL	PEAK
(IN)			(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)
0.47	RT205	MANE	1.64	16.63	362.72	0.47	15.00	16.05	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2425E+01 EXCESS=0.0000E+00 OUTFLOW=0.2425E+01 BASIN STORAGE=0.5913E-09 PERCENT ERROR= 0.0									
0.51	RT213	MANE	1.04	59.02	362.59	0.51	15.00	55.83	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.9293E+01 EXCESS=0.0000E+00 OUTFLOW=0.9293E+01 BASIN STORAGE=0.2106E-08 PERCENT ERROR= 0.0									
0.46	RT215	MANE	1.76	85.88	363.96	0.45	15.00	75.92	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1491E+02 EXCESS=0.0000E+00 OUTFLOW=0.1491E+02 BASIN STORAGE=0.1986E-07 PERCENT ERROR= 0.0									
0.40	RT201	MANE	1.62	15.02	363.27	0.40	15.00	13.38	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2583E+01 EXCESS=0.0000E+00 OUTFLOW=0.2583E+01 BASIN STORAGE=0.6813E-09 PERCENT ERROR= 0.0									
0.39	RT203	MANE	2.06	25.80	364.34	0.38	15.00	23.66	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4763E+01 EXCESS=0.0000E+00 OUTFLOW=0.4762E+01 BASIN STORAGE=0.8281E-08 PERCENT ERROR= 0.0									
0.42	RT220	MANE	0.65	118.58	361.24	0.42	15.00	113.48	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2335E+02 EXCESS=0.0000E+00 OUTFLOW=0.2335E+02 BASIN STORAGE=0.1972E-07 PERCENT ERROR= 0.0									
0.47	RT303	MANE	-0.88	41.97	361.36	0.47	15.00	40.80	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6240E+01 EXCESS=0.0000E+00 OUTFLOW=0.6241E+01 BASIN STORAGE=0.1044E-09 PERCENT ERROR= 0.0									
0.47	RT305	MANE	1.67	50.57	363.87	0.47	15.00	46.23	360.00
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7837E+01 EXCESS=0.0000E+00 OUTFLOW=0.7836E+01 BASIN STORAGE=0.4208E-08 PERCENT ERROR= 0.0									
0.47	PT311	MANE	2.61	94.90	366.16	0.47	15.00	85.77	375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1634E+02 EXCESS=0.0000E+00 OUTFLOW=0.1634E+02 BASIN STORAGE=
0.6761E-07 PERCENT ERROR= 0.0

0.44 RT316 MANE 2.72 227.58 367.68 0.45 15.00 227.30 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4573E+02 EXCESS=0.0000E+00 OUTFLOW=0.4570E+02 BASIN STORAGE=
0.4493E-06 PERCENT ERROR= 0.1

0.45 RT401 MANE 0.84 248.01 376.49 0.45 15.00 244.16 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4974E+02 EXCESS=0.0000E+00 OUTFLOW=0.4974E+02 BASIN STORAGE=
0.2308E-06 PERCENT ERROR= 0.0

0.46 RT405 MANE 1.89 263.69 378.04 0.45 15.00 253.31 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5446E+02 EXCESS=0.0000E+00 OUTFLOW=0.5446E+02 BASIN STORAGE=
0.8243E-06 PERCENT ERROR= 0.0

0.47 RT101 MANE 2.15 14.22 363.91 0.47 15.00 12.19 360.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2300E+01 EXCESS=0.0000E+00 OUTFLOW=0.2300E+01 BASIN STORAGE=
0.1952E-08 PERCENT ERROR= 0.0

0.53 RT103 MANE 0.92 47.87 376.95 0.53 15.00 46.42 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.9288E+01 EXCESS=0.0000E+00 OUTFLOW=0.9288E+01 BASIN STORAGE=
0.3917E-08 PERCENT ERROR= 0.0

0.56 RT105A MANE 0.93 59.33 376.84 0.56 15.00 58.16 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1176E+02 EXCESS=0.0000E+00 OUTFLOW=0.1176E+02 BASIN STORAGE=
0.9075E-08 PERCENT ERROR= 0.0

0.58 RT105B MANE 0.99 85.80 376.56 0.57 15.00 84.80 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1635E+02 EXCESS=0.0000E+00 OUTFLOW=0.1635E+02 BASIN STORAGE=
0.1615E-07 PERCENT ERROR= 0.0

0.58 RT107 MANE 1.85 90.34 378.00 0.58 15.00 88.08 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1775E+02 EXCESS=0.0000E+00 OUTFLOW=0.1775E+02 BASIN STORAGE=
0.6437E-07 PERCENT ERROR= 0.0

0.59 RT109 MANE 4.15 117.90 382.12 0.59 15.00 110.68 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2327E+02 EXCESS=0.0000E+00 OUTFLOW=0.2325E+02 BASIN STORAGE=
0.6371E-06 PERCENT ERROR= 0.1

0.50 RT407 MANE 1.18 425.78 377.47 0.50 15.00 405.73 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.8907E+02 EXCESS=0.0000E+00 OUTFLOW=0.8908E+02 BASIN STORAGE=
0.1351E-05 PERCENT ERROR= 0.0

0.50 RT506 MANE 0.91 462.34 376.95 0.50 15.00 445.90 375.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1008E+03 EXCESS=0.0000E+00 OUTFLOW=0.1008E+03 BASIN STORAGE=
0.1757E-05 PERCENT ERROR= 0.0

0.51 RT507 MANE 1.53 459.25 378.15 0.50 15.00 444.18 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1042E+03 EXCESS=0.0000E+00 OUTFLOW=0.1042E+03 BASIN STORAGE=
0.3967E-05 PERCENT ERROR= 0.0

0.51 RT509 MANE 2.49 463.80 392.69 0.51 15.00 463.79 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1098E+03 EXCESS=0.0000E+00 OUTFLOW=0.1098E+03 BASIN STORAGE=
0.9444E-05 PERCENT ERROR= 0.0

0.52 RT511 MANE 0.58 471.82 390.83 0.51 15.00 470.18 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1128E+03 EXCESS=0.0000E+00 OUTFLOW=0.1128E+03 BASIN STORAGE=
0.2267E-05 PERCENT ERROR= 0.0

0.67 RT601 MANE 1.88 17.54 364.39 0.67 15.00 16.48 360.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2261E+01 EXCESS=0.0000E+00 OUTFLOW=0.2261E+01 BASIN STORAGE=
0.1358E-08 PERCENT ERROR= 0.0

0.52 RT604 MANE 1.13 502.55 391.79 0.52 15.00 499.34 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1236E+03 EXCESS=0.0000E+00 OUTFLOW=0.1236E+03 BASIN STORAGE=
0.6074E-05 PERCENT ERROR= 0.0

0.54 RT610 MANE 2.26 532.57 394.39 0.53 15.00 526.56 390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1364E+03 EXCESS=0.0000E+00 OUTFLOW=0.1363E+03 BASIN STORAGE=
0.2356E-04 PERCENT ERROR= 0.0

0.54 RT612 MANE 1.55 531.09 407.51 0.54 15.00 526.25 405.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1403E+03 EXCESS=0.0000E+00 OUTFLOW=0.1403E+03 BASIN STORAGE=
0.2299E-04 PERCENT ERROR= 0.0

0.67 RT613 MANE 1.36 34.35 361.93 0.67 15.00 32.94 360.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4404E+01 EXCESS=0.0000E+00 OUTFLOW=0.4404E+01 BASIN STORAGE=
0.1157E-08 PERCENT ERROR= 0.0

0.55 RT614 MANE 0.60 548.89 405.87 0.55 15.00 546.19 405.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1513E+03 EXCESS=0.0000E+00 OUTFLOW=0.1513E+03 BASIN STORAGE=
0.7474E-05 PERCENT ERROR= 0.0

0.55 RT617 MANE 1.59 547.34 408.23 0.55 15.00 532.30 405.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1522E+03 EXCESS=0.0000E+00 OUTFLOW=0.1522E+03 BASIN STORAGE=
0.3537E-04 PERCENT ERROR= 0.0

0.58 RT703 MANE 1.63 556.50 409.26 0.58 15.00 541.13 405.00

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1681E+03 EXCESS=0.0000E+00 OUTFLOW=0.1681E+03 BASIN STORAGE=
0.5148E-04 PERCENT ERROR= 0.0

*** NORMAL END OF HEC-1 ***

50 year existing
 HEC1 S/N: 1343001909 HMVersion: 6.33 Data File C:\WINNT\TEMP\vbh0C39.TMP

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*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* U. S. ARMY CORPS OF ENGINEERS *
* MAY 1991 *
* HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.0 1E *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* RUN DATE 06/19/2001 TIME 16:42:40 *
* (916) 756-1104 *
*
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*****

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X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXXX XXXXX XXX

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: : : : :
: :
: : Full Microcomputer Implementation : :
: : by : :
: : Haestad Methods, Inc. : :
: :
: : : : :
: : : : :

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37 Brookside Road * Waterbury, Connecticut 06708 * (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, BSS: WRITE STAGE FREQUENCY,
 BSS: READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE: GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Type IIA storm									
2	IT	15	0	0	0	288					
3	ID	5									
4	KK	SC205									
5	KM	Smith Creek 205 Runoff									
6	KD								22		
7	BA	0.0970									
8	PB	4									
9	IN	15									
0.0165	10	PC	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143
0.0600	11	PC	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
0.8000	12	PC	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
0.8600	13	PC	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
0.8975	14	PC	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
0.9300	15	PC	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270
0.9550	16	PC	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
0.9800	17	PC	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
0.9925	18	PC	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
	19	PC	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
	20	LS	0	64							
	21	UD	0.257								
	22	KK	RT205								
	23	KM	Smith Creek Route 205 to 213								
	24	KD							22		
	25	RK	1530	0.0431	0.055			TRAP		2	
	26	KK	SC207								
	27	KM	Smith Creek 207 Runoff								
	28	KD							22		
	29	BA	0.12								
	30	PB	4								
	31	LS	0	65							
	32	UD	0.367								
	33	KK	SC213								
	34	KM	Smith Creek 213 Runoff								
	35	KD							22		
	36	BA	0.1243								
	37	PB	4								
	38	LS	0	66							
	39	UD	0.382								
	40	KK	DP213								
	41	KM	Combine RT205 SC207 and SC213								
	42	KD							22		
	43	HC	3								
	44	KK	RT213								
	45	KM	Smith Creek Route 213 to 215								
	46	KD							22		
	47	RK	1360	0.0493	0.055			TRAP		2	

ID	LINE	1	2	3	4	5	6	7	8	9	10
184	KK	SC311									
185	KM	Smith Creek 311 Runoff									
186	KD								22		
187	BA	0.1064									
188	PB	4									
189	LS	0	64								
190	UD	0.295									
191	KK	DP311									
192	KM	Combine RT305 SC307 SC309 and SC311									
193	KD								22		
194	HC	4									
195	KK	RT311									
196	KM	Tributary Route 311 to 315									
197	KD								22		
198	RK	2860	0.0448	0.0888					TRAP		2
199	KK	SC313									
200	KM	Smith Creek 313 Runoff									
201	KD								22		
202	BA	0.1520									
203	PB	4									
204	LS	0	64								
205	UD	0.373									
206	KK	SC315									
207	KM	Smith Creek 315 Runoff									
208	KD								22		
209	BA	0.0866									
210	PB	4									
211	LS	0	64								
212	UD	0.350									
213	KK	DP315									
214	KM	Combine RT311 SC313 and SC315									
215	KD								22		
216	HC	3									
217	KK	DP316									
218	KM	Combine RT220 and DP315									
219	KU								22		
220	HC	2									
221	KK	RT316									
222	KM	Smith Creek Route 316 to 401									
223	KD								22		
224	RK	2575	0.0361	0.120					TRAP	1	2