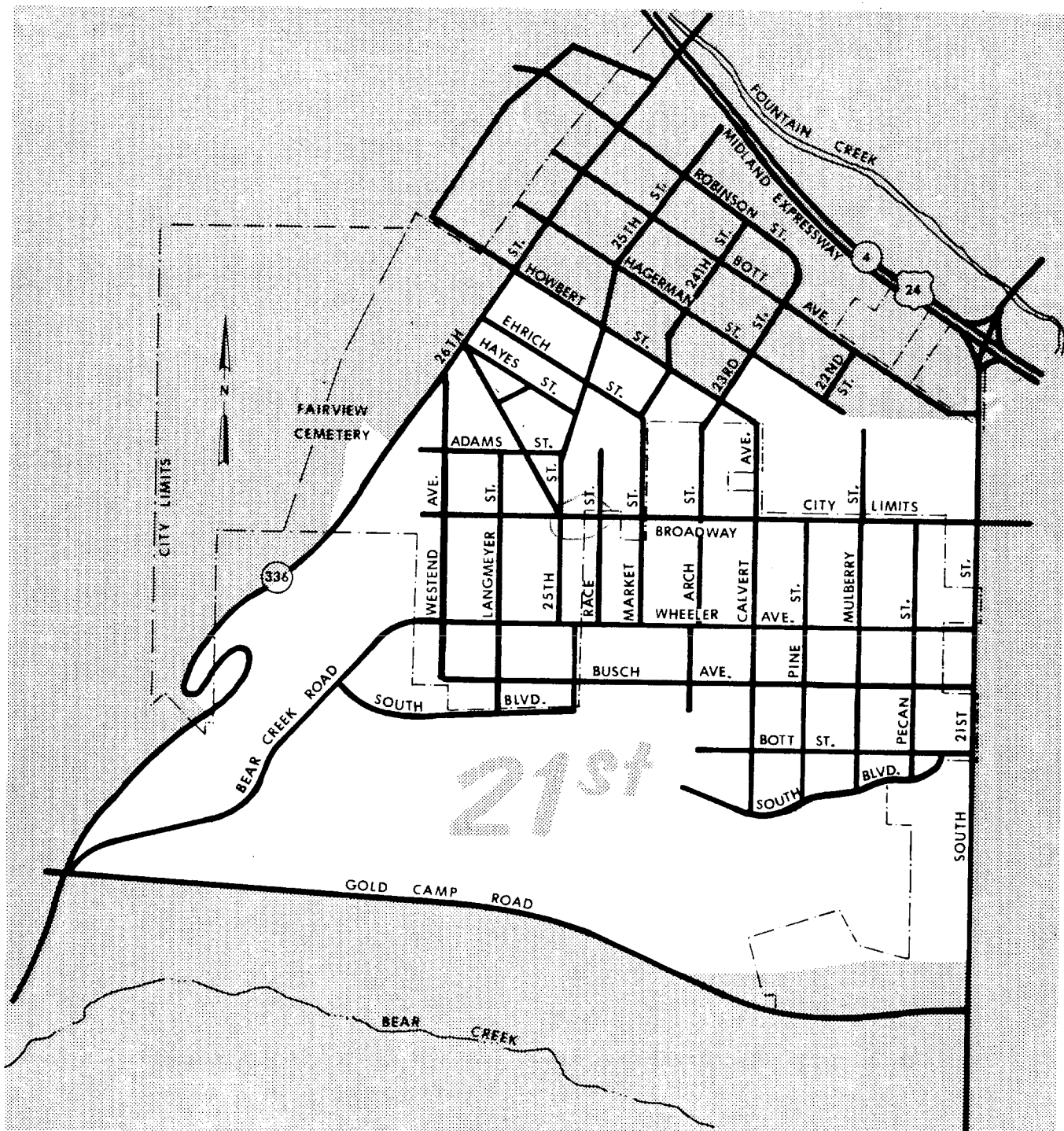


SOUTH 21st STREET Master Drainage Basin Study



ARCHITECTS
ENGINEERS
PLANNERS
SURVEYORS

r. keith hook & associates, inc.



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June 23, 1977

Mr. Dewitt Miller
Director of Public Works
P. O. Box 1575
Colorado Springs, CO 80901

Dear Sir:

Transmitted herewith is the engineering study of the South 21st Master Drainage Basin System.

This report has been prepared in conformance to those requirements as set forth in Contract No. 77-38, dated April 12, 1977, between the City of Colorado Springs and R. KEITH HOOK & ASSOCIATES, INC., Engineers and attached letter by the Engineer dated March 2, 1977.

Our technical data applied to this study is from latest drainage criteria prepared by the Department of Public Works.

As portions of this study extend beyond the present City limits, it is recommended joint meetings be held between the City and County Public Works Departments and the Drainage Board for review and comments prior to final approval.

Very truly,

R. KEITH HOOK & ASSOCIATES, INC.

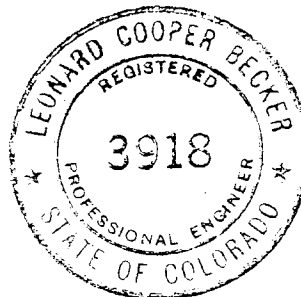


Leonard C. Becker, P.E.
Executive Vice President/Director
Engineering Department

LCB/jml

Enclosure

ARCHITECTS
ENGINEERS
PLANNERS
SURVEYORS



HYDROLOGIC ENGINEERING STUDY

of the

SOUTH 21st STREET

DRAINAGE BASIN

for

THE DEPARTMENT OF PUBLIC WORKS

COLORADO SPRINGS, COLORADO

JUNE, 1977

R. KEITH HOOK & ASSOCIATES, INC.
CONSULTING ENGINEERS
2545 East Platte Place
Colorado Springs, Colorado 80909

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I. DESCRIPTION

A. Scope and Purpose

This report has been prepared to establish the improvements necessary to provide proper storm runoff facilities and systems and to establish a drainage basin fee for the area within the boundary of the 21st drainage basin, as delineated in this report.

Storm flow run-off has been computed, using design criteria of 3.5 inch intensity, 100 year storm frequency and 6 hour duration.

It is the intent of this report to direct surface flows along those routes and systems, that will eliminate excess concentration of storm waters at any location, that will basically maintain dry street and roadway conditions, that will utilize greenbelt and piping systems, that will however consider economics of possible alternatives to keep improvement costs appropriate and that will maintain aesthetic qualities of the basin area.

All existing street systems that will logically be improved, though presently are only gravel surfaced, are considered to be surfaced with curb and gutter. In analyzing surface runoff quantities and direction of flow, these streets will therefore be considered as conveying allowable surface runoff.

Those present roadway systems that would not logically be improved with curb and gutter, will convey surface runoff in side ditch sections. The delineation of these roadway and street systems are shown on the drainage plan.

Approximately 100 Acres of undeveloped land in the Southerly portion of the basin does not reflect future street extensions in this report as this area has not been considered as being conducive to typical subdivision developed. It is possible a few large parcels may develop commercially or industrially in the future, with access roads paralleling the slope. Minimum grading of site preparation would be required to maintain natural drainage courses. The westerly portion of this area is being used as gravel extraction and if land use changes in the future a detailed drainage report should be prepared.

Nearly all this lies outside the City limits. Approximately 80 Acres of land lies between South 26th Street and Bear Creek Road. This area is sparsely populated and due to steep grades, from 9 percent to 10 percent, is considered as not conducive to typical subdivision development. This area also does not reflect proposed street extensions.

B. Basin Description

South 21st Drainage Basin is comprised of 417 Acres more or less. 168 Acres lie within the City limits of Colorado Springs and 249 Acres are in El Paso County.

The basin is bounded on the west by portions of: South 26th Street, on the North by Howbert Street, on the East by South 21st Street, and on the South by Gold Camp Road.

No major drainage channel intersects the basin and surface flow entering the basin from the westerly and southerly portions initially contained in relatively small ditches and channels along with surface sheet flow characteristics.

The majority of the platted streets are unimproved, consisting of gravel surfaced roadways. Surface runoff at several street intersections is presently intercepted into grated inlets and thence into drainage channels. Flows in ditch sections are contained in existing pipes or culverts crossing under streets.

All surface flow in the basin outfalls at one (1) point, contained in a 10' x 10' culvert crossing under 21st Street and thence into Fountain Creek via a large channel.

All existing drainage ditches, channels, piping and facilities are shown on the drainage plan on Figure A.

Due to the majority of unimproved streets surface run-off during a nominal storm creates erosion to the streets and ditches requiring immediate repair.

During the course of preparing this report, residents within the area have called the City advising damage to their properties as a result of excess water and velocities overflowing ditches.

Presently the Southerly portion of the Basin is undeveloped, consisting of scarred land in the Southwest portion, as a result of gravel extraction and rather steep grassed slopes in the Southeast portion. From these areas surface flows are not specifically directed, other than natural surface flow routes, creating excess flows at points intercepting streets parallel and perpendicular to the surface run-off.

Average grades in these areas are 10 percent, creating excess velocities of surface flow as this run-off enters developed areas. Particular high velocities of surface flow was noted on South 21st Street and resultant flooding and erosion as a result of 7 per cent grades.

Of the present areas unplatted, and in view of the zoning established, it would appear the land will eventually be developed into commercial and industrial sites.

C. Hydrologic Soil Description

The undeveloped areas of the basin lie principally in the Southeasterly and Southwesterly areas.

In the Southwesterly area, the soil consists of gravels and alluvium formed from westerly mountain gravels overlying the Pierre shale group. This type soil has a hydrologic classification of relative high infiltration SC5 (A) rate and a high rate of water transmission. At the present time this area is used for gravel extraction and the surface area is hard packed and as a result of this and due to the 9-10 per cent grades, a higher run-off factor has been applied to this area.

The Southeasterly portion consists of vegetation and native grasses. This also has a relative high infiltration SC5(A) rate and a high rate of water transmission. A higher run-off factor, however has been applied to this area as the grades are also 9 to 10 per cent.

The soil characteristics in the present developed areas and those areas of planned development fall within the soil classification of SC5 "C" and "D" categories, consisting of lean clayey materials and fat clays with moderate to slow water infiltration and high transmission rates.

D. Storm Runoff Criteria

The procedures used in this report to establish runoff calculations, rainfall intensities, duration and storm frequency were adopted from the following manuals:

1. Determination of Storm Runoff Criteria, Colorado Springs, Department of Public Works
2. USDA - SC5, including "procedures for Determining Peak Flows in Colorado"
3. Bureau of Reclamation Design of Small Dams (Book) complex Synthetic Hydrograph Procedures

Basic calculations utilized a 3.5 inch rainfall intensity, a 6 hour storm duration and a 100 year occurrence.

Formulas for hydraulic calculations are shown in Section VI.

E. Major Drainage Channel Systems

The greenbelt system extends from the west side of South 21st Street westerly to its northerly termination at the intersection of Enrich and Market Streets. From the intersection at Mulberry extended, the greenbelt system extends southerly to a point 450 feet south of Bott Street, thence westerly to a point 500 feet south of Langmeyer Street extended.

A branch of the major greenbelt system extends northerly along Mulberry Street to a point of intersection.

2700 feet of the system lies within the City limits.

4200 feet of the system lies in El Paso County.

Portions of the above described major greenbelt system, as shown on the drainage plan, are present drainage channels, conveying surface runoff from the south and west portions of the basin to an existing outfall structure in the northeast corner of the basin and thence crossing under South 21st to its confluence with Fountain Creek.

It is the intent to provide the southerly portion of the major greenbelt system as an interceptor of the surface runoff from the undeveloped land in the extreme southerly portion of the basin. As previously mentioned, the grades in this area average 10 per cent.

F. Improvements

The proposed improvements described in this report and shown on the drainage plan consist of the following:

- a - Greenbelt Channel System - Shaping and Lining
- b - Drainage Piping System
- c - Drainage Structures and Appurtenances
- d - Drainage channels
- e - Drainage Inlets and Catch Basins
- f - Velocity Control Structures
- g - Maintenance Access Roadways
- h - On-going maintenance Program.

The location of proposed drainage facilities, including greenbelt systems, drainage channels, piping systems, catch basins and appurtenances are shown as a guide and recommendations for drainage improvements and as a guide to establish drainage basin fees. It is the intent that drainage improvements basically conform to this report.

In addition to upgrading the existing major channel and supplementing this channel and developing new channels into greenbelt systems, several of the existing pipe culverts crossing under streets, and existing ditches will require improving in order to maintain minimum flow in the street systems, a network of drainage piping is required in the southerly and westerly portions of the basin draining surface flows into the piping system and thence into the greenbelt systems.

Within the ditch sections, velocities will exceed 5 fps in some sections requiring velocity control structures. In addition, shaping existing greenbelt channels and lining will also be required.

The existing drainage structures and piping crossing under street systems or as portions of the existing drainage channel system are described and shown on the drainage plan and identified by hydrograph point numbers. Required improvement to these structures and piping is described in facilities improvements, page 36 and 37.

An analysis of the existing drainage structures and piping in the main drainage channel show deficiency in conveying a 3.5 inch rainfall

at peak flow. The cross-section of the proposed major greenbelt indicates the rise in water level if these deficient structures are not improved, as recommended.

Recommended catch basins sizes and locations are shown on the drainage plan, variations from standard design are required at certain locations and are described and shown on the drainage plan in the report.

Easements will be required for the southerly greenbelt system and to provide for this improvement requirement a contingency cost has been included in the cost estimates included in this report.

(All costs in place and projected to 1979)

10

COST ESTIMATE - DEVELOPER FUNDS

(All costs in place and projected to 1979)

<u>ITEM</u>	<u>QUANTITY</u>	<u>UNIT</u>	<u>UNIT COST</u>	<u>AMOUNT</u>
Storm Drain Piping System				
RCP: 18"	1400	L.F.	\$ 9.06	\$ 12,681.90
24"	550	L.F.	12.99	7,144.50
30"	500	L.F.	19.45	9,725.00
36"	550	L.F.	35.49	19,519.50
48"	325	L.F.	48.93	15,902.25
				<u>\$ 64,973.15</u>
Catch Basins				
D10R: 4'	4	Ea.	\$ 608.85	\$ 2,435.40
6'	2	Ea.	839.03	1,678.06
8'	2	Ea.	977.13	1,954.26
12'	4	Ea.	1,470.15	5,880.60
Grated Inlet	1	Ea.	2,000.00	2,000.00
				<u>\$ 13,948.32</u>
Major Drainage Channel Systems:				
Shaping, Lining	5250	L.F.	\$ 40.00	\$210,000.00
Slope Treatment	5250	L.F.	10.00	52,500.00
				<u>\$262,500.00</u>
Manholes	7	Ea.	\$ 1,200.00	\$ 8,400.00
				<u>\$ 8,400.00</u>
GRAND TOTAL				\$349,821.47

Total Assessable Area = 324.4 Acres

Gross Cost Per Acre = $\frac{\$349,821.47}{324.4 \text{ Acres}}$ = \$1,078.36/Acre
(unadjusted)

COST ESTIMATE - BREAKDOWN AND SUMMARY

Total Basin Area = +/- 417 Acres

Total Platted Area = +/- 274 Acres

Platted Developed Area = 119.6 Acres

Platted Undeveloped Area = 154.4 Acres

Total Unplatted Area = +/- 170 Acres

Platted Undeveloped Area + Unplatted Area = 324.4 Acres
(Area available for Drainage fee Assessment)

Total Developer Costs = \$349,821.47

- Collected Drainage Fees = 14,194.43

= Adjusted Total Cost = 335,627.04

Cost Per Acre = $\frac{\$335,627.04}{324.4 \text{ Acres}}$ = \$1,034.61/Acre + 10% Eng. & Cont'n.
Cost Per Acre = \$1138.00

Total City Appropriated Funds Cost = \$578,906.64

Remodeling of Existing = \$10,727.96
Drainage Structures
(See Page 34)

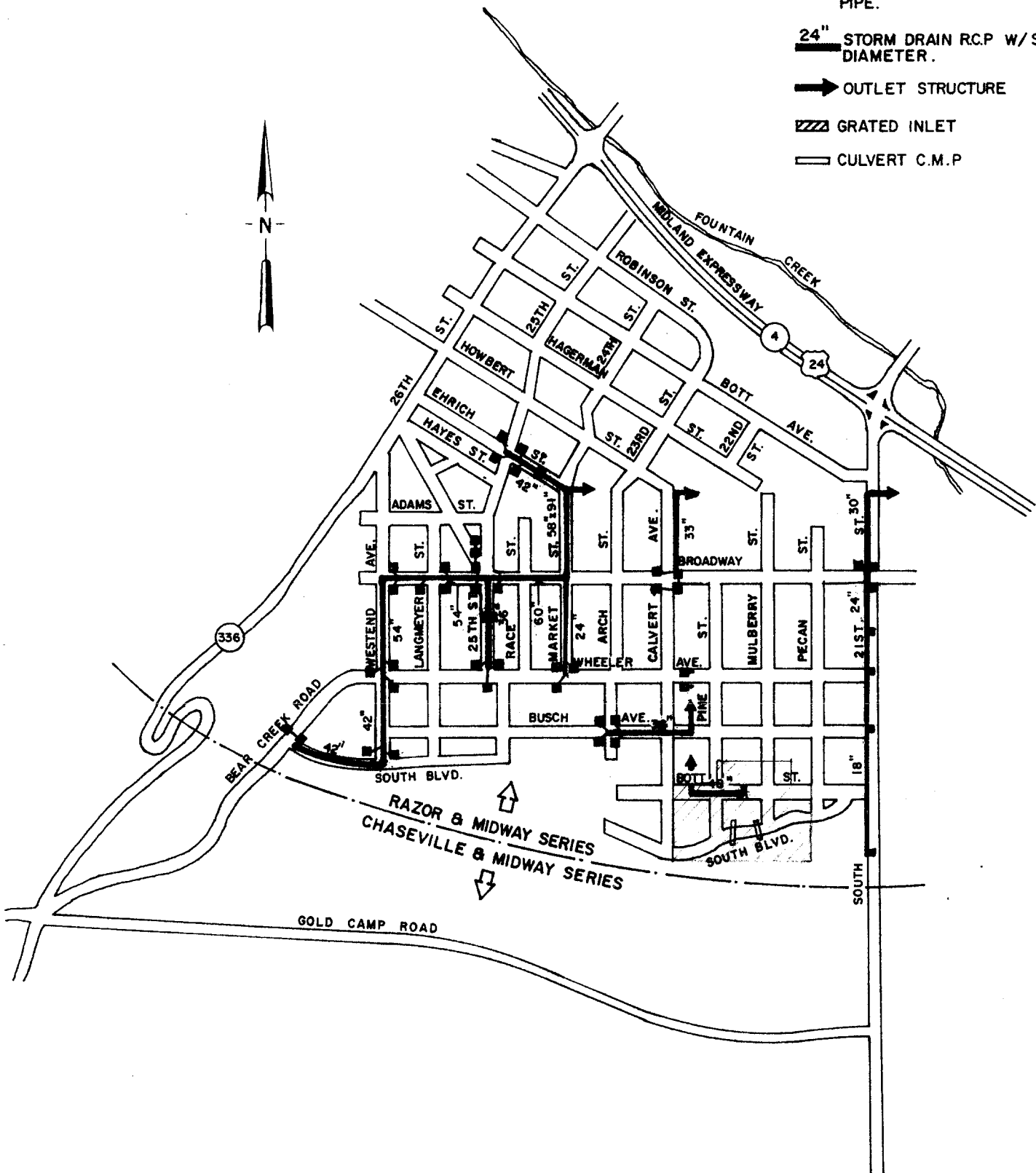
Total Project Cost = \$925,261.64

SUMMARY OF AREA IN BASIN

	<u>ACRES</u>	<u>SQ. MILES</u>	<u>PERCENTAGE</u>
In City Limits	167.8	0.262	40.2
In County Limits	249.9	0.390	59.8
TOTAL	417.7	0.652	100.0

LEGEND

- CATCH BASIN W/CONNECTOR PIPE.
- 24" STORM DRAIN R.C.P W/ SIZE DIAMETER.
- ➔ OUTLET STRUCTURE
- ▨ GRATED INLET
- ▭ CULVERT C.M.P



STORM DRAIN PIPING SYSTEM

SOUTH 21st BASIN

Hydraulic Calculations for Flow in Open Channels and Non-Pressurized Pipe

Form: Mannings Equation

$$V = \frac{C}{n} R^{2/3} S^{1/2}$$

Where:

V = Velocity in feet per second

C = Coefficient = 1.486

n = Mannings Coefficient

R = Hydraulic radius

S = Slope in feet per 100 feet

SUMMARY MANNING'S n VALUES

Concrete Lined	-	n	=	.013
Earth Bottom, Concrete Sides	-	n	=	.022
Earth or Rubble Bottom, Rubble Sides	-	n	=	.033-0.04
Natural Stream	-	n	=	.04
Natural Stream	-	n	=	.05
Concrete Pipe or Culvert Box	-	n	=	.013
CMP (3" x 1")	-	n	=	.027
Asphaltic Pavement	-	n	=	.019
Smooth Flow Pipes	-	n	=	.013

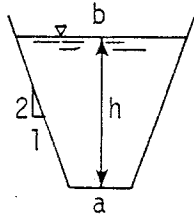
Example: Open Channel Calculations

Equation: Mannings

$$n = 0.013$$

$$Q = 180 \text{ cfs}$$

$$\text{Slope} = 2.00\% = 0.02$$



$$\text{Area} = \frac{1}{2} (a+b) h = \frac{(2a+h) h}{2}$$

$$\text{WP} = a + 2 \left(h^2 + \frac{h^2}{4} \right)^{1/2}$$

$$R = \frac{\text{Area}}{\text{WP}} = \frac{(2a+h)h}{2 \left(a + 2h \left(\frac{5}{4} \right)^{1/2} \right)}$$

$$V = \frac{1.486}{n} R^{2/3} S^{1/2}$$

$$Q = VA$$

Solution:

Size:

$$a = 3.0 \text{ ft}$$

$$h = 2.5 \text{ ft} + \text{F.S.}$$

$$V = 18.63 \text{ fps}$$

$$Q = 198 \text{ cfs}$$

Example: Pipe Flow Calculations
(Non-Pressurized)

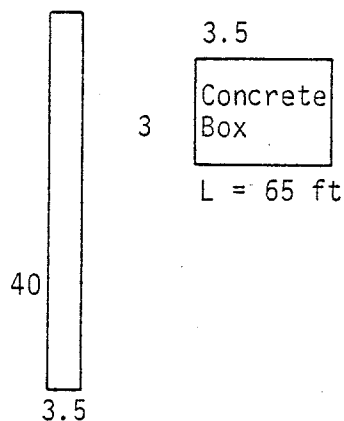
Equation = Mannings
n = .013
Q = 315 cfs
Slope = 6.77%

$$\text{Area} = \frac{\pi D^2}{4}$$
$$R = \frac{D}{4}$$
$$V = \frac{1.486}{n} R^{2/3} S^{1/2}$$
$$Q = VA$$

Solution: Size: D = 48"
V = 29.7 fps
Q = 373 cfs

HYDROGRAPH POINT #7

Existing Culvert on Broadway at Market



$$\text{Drop} = 1.0'$$

$$S = \frac{1}{65} = .0154$$

For Box

$$A = 10.5 \text{ ft}^2$$

$$WP = 13 \text{ ft}$$

$$R = \frac{10.5}{13} = .8077$$

$$V = \frac{1.486}{.013} (.8077)^{2/3} (.0154)^{1/2} = 12.30 \text{ fps}$$

$$Q = VA = (12.30)(10.5) = 129.18 \text{ cfs}$$

For grate

$$Q = CA\sqrt{2gh} = (.6) (40) (3.5) \sqrt{32.2}$$

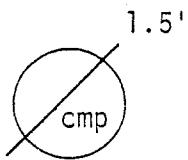
$$Q = 476.66 \text{ cfs}$$

$$Q \text{ clogged} = 317.7$$

$$\text{Max Flow Allowable} = \underline{\underline{129.2 \text{ cfs}}}$$

HYDROGRAPH POINTS #8 TO 9

Existing Culverts on Enrich



$$A = \pi (1.5)^2 = 1.767$$

$$R = \frac{D}{4} = \frac{1.5}{4} = .375$$

Slope = 2.34%

$$V = \frac{1.486}{.027} (.375)^{2/3} (.0234)^{1/2} = 4.378 \text{ fps}$$

$$\underline{Q = VA = 7.74 \text{ cfs @}}$$

HYDROGRAPH POINT #13

Existing Culvert on Busch between Colvert & Pine

35 LF



44"



70 LF CMP
60' Ø

$$\text{For Pipe: } A = \pi \frac{66^2}{12} = 23.76 \text{ ft}^2$$

$$R = \frac{D}{4} = \frac{66}{12} = 1.375$$

$$S = \frac{1.1}{70} = .0157$$

$$V = \frac{1.486}{.027} (1.375)^{2/3} (.0157)^{1/2}$$

$$V = 8.53 \text{ fps}$$

$$Q = VA = 202.69 \text{ cfs}$$

For Grating:

Assume 60% clear opening

Assume Max head to be curb heights = .5'

Seelye: $Q = CA \sqrt{2gh}$ $c = .6$

$$A = (35) \frac{44}{12} = 128.33$$

$$g = 32.2 \frac{\text{ft}}{\text{sec}^2}$$

$$h = .5'$$

$$Q = (.6)(12833)[2(32.2)(.5)]^{1/2}$$

$$Q = 436.93 \text{ cfs}$$

$$Q \text{ clogged} = 291.28$$

Max Flow in present conditions = 203 cfs

HYDRGRAPH POINT #14

Existing 3 side by side Culverts at Wheeler & Pine

Lowheads: 3' High = 36"
 4' Wide = 48" 44" Ø circulate
 53 lf
 Drop = .75'
 N = .027

$$A = \frac{D^2}{4} = \frac{\pi \left(\frac{44}{12}\right)^2}{4} = 10.56 \text{ ft}^2$$

$$WP = \pi D = \pi \left(\frac{44}{12}\right) = 11.52$$

$$R = \frac{A}{WP} = \frac{10.56}{11.52} = 0.917$$

$$S = \frac{.75}{53} = 0.0142$$

$$V = \frac{1.486}{.027} (.917)^{2/3} (.0142)^{1/2} = \underline{\underline{6.18 \text{ fps}}}$$

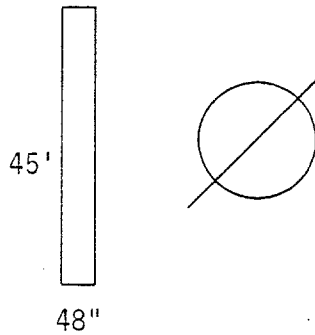
$$Q = VA (6.18)(10.56) = 65.24 \text{ cfs}$$

$$\underline{\underline{Qt = 3Q = 195.7 \text{ cfs}}}$$

HYDROGRAPH POINT #15

Existing Culvert on Wheeler at Mulberry

Lowhead equal D = 54" CMP



$$A = \pi \frac{\left(\frac{54}{12}\right)^2}{4} = 15.904 \text{ ft}^2$$

$$WP = \pi D = 14.137$$

$$R = \frac{D}{4} = \frac{54}{58} = 1.125$$

$$\text{Slope} = \frac{.43}{50} = .0086$$

$$V = \frac{1.486}{.027} (1.125)^{2/3} (.0086)^{1/2} = 5.52 \text{ fp}$$

$$Q = VA = (5.52)(15.904) = 87.80 \text{ cfs}$$

$$Q \text{ clogged} = 58.53$$

(Pipe Controls)

HYDROGRAPH POINT #16

Existing Culvert on Broadway at Mulberry
for through pipe

CMP



3.25 x 5.25

D = 54 "

A = 15.904

R = 1.125

Slope = $\frac{4.5'}{60}$ = .0750

$V = \frac{1.486}{.027} (1.125)^{2/3} (.075)^{1/2} = 16.304 \text{ fps}$

Q = VA = 259.3 cfs

For Gratings & Pipe

$Q = (.6) (2) (16) \sqrt{32} \quad (2/3)$

Q = 72.407 cfs

Max flow in other pipe = 72.4 cfs

HYDROGRAPH POINT #17

Existing Culvert at Calvert & Broadway

4' ID CMP
65 LF
4 ft Drop

$$N = 0.027$$

$$\text{Slope} = \frac{(.4)}{(65)} (100) = 0.62\% = .0062$$

$$\text{Area} = 12.57 \text{ ft}^2$$

$$V_o = 1.4860 \text{ fps}$$

$$Q_o = 18.67 \text{ cfs}$$

$$\sqrt{\frac{S}{N}} = \sqrt{\frac{.0062}{.027}} = 2.9054$$

$$V = (1.4860) (2.9054) = 4.32 \text{ fps}$$

$$Q = (18.67) (2.9054) = \underline{\underline{54.244 \text{ cfs}}}$$

Method II:

$$A = \frac{(\pi)(16)}{4} = 4 = 12.56 \text{ ft}^2$$

$$WP = \pi D = 12.57 \text{ ft}^2$$

$$R = 1$$

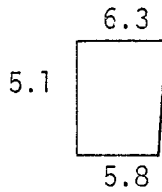
$$S = \frac{.4}{65} = .0062$$

$$V = 14.86 (1)^{2/3} (.0062)^{1/2} = 4.32 \text{ fps}$$

$$Q = VA = (4.32)(12.57) = 54.27 \text{ cfs} \quad \text{OK Check}$$

HYDROGRAPH POINT #18

Existing Box Culvert at end of Culvert



$$\begin{aligned} \text{Drop} &= 1.75' \\ L &= 35' \end{aligned}$$

$$A = \frac{(6.3 + 5.8)}{2} (5.1) = 30.855 \text{ ft}$$

$$WP = 6.3 = 5.8 + 10.2 = 22.3$$

$$R = \frac{A}{WP} = 1.394$$

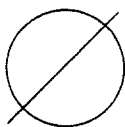
$$V = \frac{1.486}{.013} (1.394)^{2/3} \left(\frac{1.75}{35} \right)^{1/2} = 31.75 \text{ fps}$$

$$\underline{Q = VA = 980 \text{ cfs}}$$

BWTWEEN HYDROGRAPH POINTS #19 & 21

Existing Culverts above 21st Street

2 @



6'

60 LF CMP

$$\text{Slope} = \frac{.2}{60} = .0033$$

$$A = \frac{\pi (36)}{4} = 28.27$$

$$R = \frac{6}{4} = 1.5$$

$$V = \frac{1.486}{.027} (1.5)^{2/3} (.0033)^{1/2}$$

$$V = 4.164 \text{ fps}$$

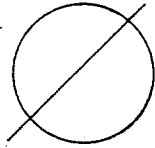
$$Q = VA = 117.7$$

$$\underline{\underline{Q_t = 2Q = 235.4 \text{ cfs}}}$$

HYDROGRAPH POINT #21

Existing culverts leading into 21st Street

2 @



7' CMP
160 LF

$$A = \frac{(\pi) (49)}{4} = 38.48$$

$$R = \frac{D}{4} = \frac{7}{4} = 1.75$$

$$\text{Slope} = \frac{4.5}{110} = .0409$$

$$V = \frac{1.486}{.027} (1.75)^{2/3} (.0490)^{1/2}$$

$$V = 16.165 \text{ fps}$$

$$Q = VA = 622.05 \text{ cfs}$$

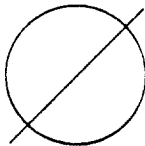
$$Q_t = 2Q = 1244 \text{ cfs}$$

Drain Above: 3' x 1.5' A = 4.5

$$Q = (.6)(4.5)(32)^{1/2} (2/3)$$

$$\underline{\underline{Q = 10.18 \text{ cfs}}}$$

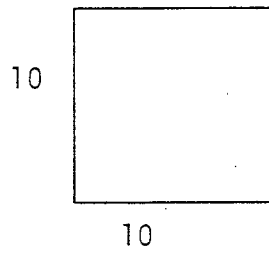
Connecting Pipe:



18" one in both culverts

HYDROGRAPH POINT #22

Existing Box Culvert Under 21st Street



$$A = 100 \text{ ft}^2$$

$$WP = 40 \text{ ft}$$

$$R = \frac{10}{4} = 2.5$$

$$\text{Slope} = .0409$$

$$V = \frac{1.486}{.013} (2.5)^{2/3} (.0409)^{1.2}$$

$$V = 42.58 \text{ fps}$$

$$\underline{Q = VA = 4258 \text{ cfs}}$$

Existing Culvert Across 26th Street

21" Concrete Pipe \emptyset

65 LF

N = .013

5.6' Drop

$$\text{Slope} = S = \frac{5.6}{65} = .086$$

$$\text{Area} = \pi \frac{D^2}{4} = \frac{(\pi) (21)^2}{4} = 2.405 \text{ ft}^2$$

$$\text{WP} = \pi D = \frac{(\pi) (21)}{12} = 5.498 \text{ ft}$$

$$R = \frac{A}{\text{WP}} = \frac{2.405}{5.498} = .437$$

$$V = \frac{1.486}{.013} (.437)^{2/3} (.086)^{1/2} = \underline{\underline{19.317 \text{ fps}}}$$

$$\underline{\underline{Q = VA = 416.458 \text{ cfs}}}$$

STREET SYSTEM DATA AND CALCULATIONS

STREET	FROM/TO	LENGTH (ft)	SLOPE (%)	WIDTH (ft.)	RIGHT OF WAY	ELEV. FR/TO	STREET CAPACITY (V/Q)
South	Westend/Langmeyer	380	3.95	32	60	228/213	11.4/81.3
South	Langmeyer/Race	500	1.40	32	60	213/206	6.8/48.3
Busch	Westend/Langmeyer	380	2.89	32	60	195/184	9.8/69.5
Busch	Langmeyer/Race	100/200/215	3.00/2.50/2.33	32	60	184/181	9.98/70.9/8.15/57.8/8.8/62.4
Busch	Race/Arch	810	3.70	32	60	181/151	11.1/78.6
Busch	Arch/Calvert	380	3.68	32	60	151/137	11.0/78.4
Busch	Calvert/Pine	200/180	3.50/+ .56	32	60	137/129	10.78/76.5/4.3/30.3
Busch	Pine/Mulberry	380	.53	32	60	129/127	4.2/29.6
Busch	Mulberry/Pecan	360	-1.67	32	60	127/133	7.43/52.7
Busch	Pecan/21st Street	380	-2.89	32	60	133/144	9.8/69.5
Wheeler	Westend/Langmeyer	380	4.74	32	60	181/163	12.5/89.1
Wheeler	Langmeyer/25th	380	4.21	32	60	163/147	11.8/83.9
Wheeler	25th/Race	240	-.42	32	60	147/148	-
Wheeler	Race/Market	40/330	-1.25/1.67	32	60	143/143	6.4/45.5/7.43/52.7
Wheeler	Market/Arch	80/280	-.63/2.68	32	60	143/136	4.5/320/9.4/66.9
Wheeler	Arch/Calvert	380	2.89	32	60	136/125	9.8/69.5
Wheeler	Calvert/Mulberry	730	2.47	32	60	125/107	9.1/64.3
Wheeler	Mulberry/Walnut/Pecan	380	-2.37	32	60	107/116	8.9/62.9
Wheeler	Walnut/21st	100/370	-1.5/1.22	32	60	116/114	7.06/50.1/6.3/44.9
Broadway	Westend/Langmeyer	380	4.21	50	100	163/147	11.8/83.9
Broadway	Langmeyer/25th	380	3.68	50	100	147/133	11.0/78.4
Broadway	25th/Race	230	3.91	50	100	133/124	11.4/80.8
Broadway	Race/Market	350	2.00	50	100	124/117	8.15/57.8
Broadway	Market/Arch	60/320	-.83/2.34	32	100	117/110	5.2/36 8.8/62.5
Broadway	Arch/Calvert	380	3.68	32	100	110/96	11.0/78.4
Broadway	Calvert/Mulberry	730	1.78	32	100	96/83	7.67/54.4
Broadway	Mulberry/Pecan	380	1.58	32	100	83/77	7.23/51.3
Broadway	Walnut/21st	350	3.14	32	100	77/66	10.2/72.5
Adams	Westend/Langmeyer	380	5.53	36	100	165/144	8.4/97.1
Adams	Langmeyer/Modes	150	2.67	36	100	144/140	5.9/67.5
Adams	Modes/25th	250	4.40	36	100	140/129	7.5/86.6
Bear Creek	South/Westend	920	6.41	32	60	6240/6181	9.1/104.5
Hayes	26th/25th	830	3.86	36	60	153/121	7.1/81.1
Enrich	26th/25th	770	4.03	36	60	145/114	7.2/82.9
Enrich	25th/Market	470	2.34	36	60	114/103	5.5/63.2
Howbert	26th/25th	670	3.73	36	60	136/111	6.9/79.7
Howbert	25th/Market	540	2.96	36	60	11/95	6.2/71.0
Howbert	Market/Arch	430	1.86	36	60	95/87	4.9/56.3
Westend	South/Busch	270	12.22	36	80	228/195	12.5/144.3
Westend	Busch/Wheeler	400	3.50	36	80	195/181	6.7/77.2
Westend	Wheeler/Broadway	700	2.57	36	80	181/163	5.8/66.2
Westend	Broadway/Adams	440	-0.50	36	80	163/165	2.5/29.2
Westend	Adams/26th	550	-.91	36	80	165/170	3.4/39.4
Langmeyer	South/Busch	200	14.5	36	60	213/184	13.7/157.2
Langmeyer	Busch/Wheeler	400	5.25	36	60	184/163	8.2/94.6
Langmeyer	Wheeler/Broadway	700	2.29	36	60	163/147	5.4/62.5

STREET SYSTEM DATA AND CALCULATIONS
(continued)

STREET	FROM/TO	LENGTH (ft)	SLOPE (%)	WIDTH (ft.)	RIGHT OF WAY	ELEV. FR/TO	STREET CAPACITY (V/Q)
Langmeyer	Broadway/Adams	430	.70	36	60	147/144	3.0/34.5
Race	South/Busch	200	12.50	36	60	206/181	12.7/146.0
Race	Busch/Wheeler	420	8.10	36	60	181/147	10.2/117.5
Race	Wheeler/Broadway	700	3.29	36	60	147/124	6.5/74.9
25th	Wheeler/Broadway	600	2.00	60	80	147/133	4.3/54.2
25th	Broadway/Adams	430	.93	60	80	133/129	3.0/37.0
Market	Wheeler/Broadway	700	3.71	36	60	143/117	6.9/79.5
Market	Broadway/Enrich	700	2.00	36	60	117/103	5.1/58.4
Arch	Busch/Wheeler	430	3.49	36	60	151/136	6.7/77.1
Arch	Wheeler/Broadway	700	3.71	36	60	136/110	6.9/79.5
Arch	Broadway/Howbert	800	2.89	36	60	110/87	6.1/70.2
23rd	Howbert/Hagerman	380	2.63	36	60	87/77	5.8/67.0
23rd	Hagerman/Bott	400	-	36	60	77/-	-
Calvert	Busch/Wheeler	420	2.86	60	100	137/125	5.2/64.8
Calvert	Wheeler/Broadway	700	4.14	60	100	125/96	6.2/78.0
Pine	Busch/Wheeler	420	4.29	32	60	129/111	11.9/84.7
21st	View La./ Bott Ave.	1300	5.85	36	80	246/170	8.7/99.9
21st	Bott Ave./Busch	400	6.50	36	80	170/144	9.2/105.3
21st	Busch/Wheeler	420	7.14	36	80	144/114	9.6/110.3
21st	Wheeler/Broadway	700	6.86	36	80	114/66	9.4/108.1
21st	Broadway/7-11	480	3.54	60	100	66/49	5.8/72.1
Market	Enrich/Howbert	340	2.35	36	40 & 60	103/95	5.5/63.3
24th	Howbert/Haggerman	400	4.00	36	60	95/79	7.2/82.6
24th	Haggerman/Bott	400	-	36	60	-	-
South	Bear Creek/Westend	680	1.76	32	60	240/228	7.6/54.1
Bott	Arch/Pine	750	2.33	32	60	165/147.5	8.8/62.4
Bott	Pine/Mulberry	220/130	.23/- .40	32	60	147.5/147.5	-/3.7/26.5
Bott	Mulberry/Pecan	350	-3.00	32	60	147.5/158	9.98/70.9
Bott	Pecan/21st	400	-.75	32	60	158/161	4.9/34.9
South	Arch/Calvert	250/150	3.60/-67	32	80	180/172	10.9/77.6/4.7/33.0
South	Calvert/Pine	200/100/100	1.50/-5.09/3.0	32	80	172/171	7.06/50.1/12.89/91.5/9.98/70.9
South	Pine/Mulberry	380	0.26	32	80	171/170	-
South	Mulberry/Pecan	400	-2.50	32	80	170/180	9.11/64.7
South	Pecan/Bott	300	4.67	32	80	180/166	12.4/88.4
Pine	Bott/Busch	400	4.63	32	60	147.5/129	12.4/88.0
Mulberry	Bott/Busch	400	5.13	32	60	147.5/127	13.1/92.6
Pecan	Bott/Busch	400	6.25	32	60	158/133	14.3/102.0
Pine	Wheeler/Broadway	700	3.43	32	60	11/87	10.7/75.7

HYDROGRAPH POINT DATA

HYDROGRAPH POINT	DROP (ft)	LENGTH (ft)	SLOPE (%)	ACCUM. BASIN AREA (sq.mi.)	Tc (hr)	CN	Q (in)	qp (csm/in)	q TOTAL (cfs)	Tp (hr)	Tb (hr)
1	216	2800	7.71	.0600	.157	91	2.55	1150	175	3.09	8.25
1A	200	2100	9.52	.0282	.116			1230	88	3.07	8.20
1B	200	2100	9.52	.0133	.116			1230	42	3.07	8.20
2	270	3200	8.44	.0936	.169			1120	265	3.10	8.28
3	285	3900	7.31	.1354	.207			1060	365	3.12	8.34
4	93	1100	8.50	.0267	.074			1280	35	3.04	8.13
5	316	4600	6.87	.1807	.241			1000	460	3.14	8.40
6	43	800	5.37	.0103	.069			1280	35	3.04	8.12
7	335	5200	6.44	.2108	.272			950	510	3.16	8.44
8	86	1500	5.73	.0439	.109			1280	145	3.06	8.18
9	350	5800	5.98	.2762	.306			910	640	3.18	8.50
10	190	2900	6.55	.0854	.172			1110	240	3.10	8.29
11	153	1500	10.20	.0492	.087			1280	160	3.05	8.15
12	150	1600	9.37	.0390	.095			1280	125	3.06	8.16
13	230	3700	6.22	.1736	.212			1050	465	3.13	8.35
14	248	4100	6.05	.1845	.232			1005	475	3.14	8.38
15	40	800	5.00	.0311	.071			1280	100	3.04	8.12
16	276	4900	5.63	.2389	.273			950	580	3.16	8.45
17	60	1200	5.00	.0166	.097			1280	55	3.06	8.16
18	365	6650	5.49	.3292	.349			860	720	3.21	8.57
19	380	7250	5.24	.3545	.380			830	750	3.23	8.62
	290	5500	5.27	.2389	.307			910	555	3.18	8.50
20	200	2800	7.14	.0245	.162			1140	70	3.10	8.27
21	400	7150	5.59	.6330	.367			850	1300	3.22	8.60
22	410	7200	5.69	.6330	.367			850	1370	3.22	8.60

CHANGES IN DEFICIENT EXISTING DRAINAGE STRUCTURES

<u>LOCATION</u>	<u>EXISTING</u>	<u>CHANGES REQUIRED</u>	<u>ESTIMATED COST</u>
Along Enrich	2 @ 18" CMP	Remove Culverts	\$ 45.00
At Broadway & Calvert	48" CMP	Remove Culvert	50.00
At Pine & Wheeler	3 @ 36"x48" CMP	Remove Culverts Replace with 2 @ 53 LF 54" RCP @ 2.00% grade	\$ 6,558.98
At Wheeler & Mulberry =	54" Ø Lowhead CMP	Remove Culvert Replace with 5 LF 42" RCP @ 2.00% grade	\$ 317.85
At Point #18	5'x6' Cinder Block Conduit	Remove Culvert Replace with 35 LF 66" RCP	\$ 3,306.13
At End of Pecan	2 @ 72" CMP	Remove and lay to 1.7% grade	\$ 175.00
At West end & Wheeler	Dikes	Remove Dikes	\$ 275.00
		TOTAL	\$10,727.96

DRAINAGE STRUCTURE INVENTORY

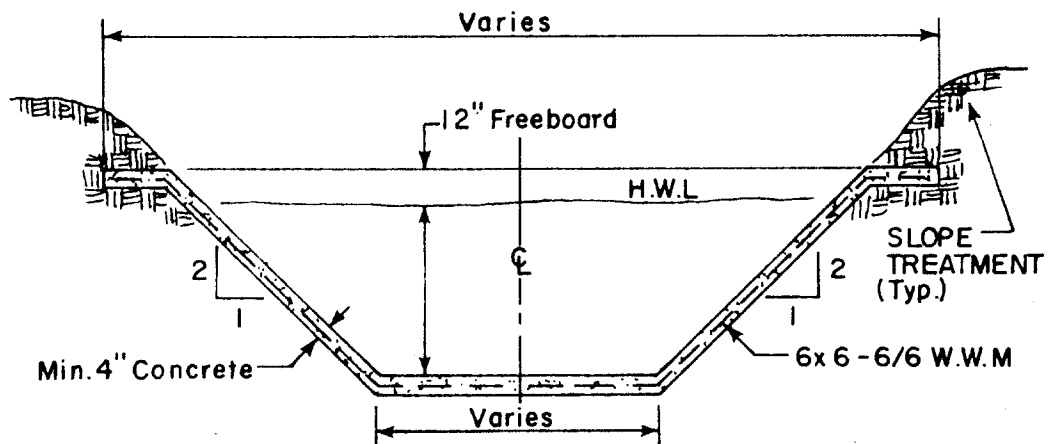
<u>LOCATION</u>	<u>EXISTING STRUCTURE</u>	<u>QP EXISTING (cfs)</u>	<u>QP REQUIRED (cfs)</u>	<u>REQUIRED STRUCTURE</u>
Along Bear Creek	-	-	130	2600 L.F. 1.5x2" Lined Channel
At Bear Creek & South	-	-	130	Flaired Intake
Along South: Bear Creek to Westend	-	-	130	Diversion Structures
At Westend & South	-	-	55	650 L.F. 42" RCP 2010' - D10R
Along Westend: South to Wheeler	-	-	175	650 L.F. 42" RCP
At Westend & Wheeler	Dikes	-	105	3012' - D10R
Along Westend: Wheeler to Broadway	-	-	265	700 L.F. 54" RCP
West of Westend (South)	-	-	95	700 L.F. 2'x2.5' Lined Channel
West of Westend (North)	-	-	85	500 L.F. 2'x2.5' Lined Channel
At Westend & Broadway	-	-	25	150 L.F. 2'x3' Lined Channel, Flaired
Along Broadway: Westend to 25th	-	-	365	20 6'-D10R Intake
At Broadway & Langmeyer	-	-	40	750 L.F. 54" RCP 30 6'-D10R
At Broadway & 25th	-	-	30	30 6'-D10R
At Modes and 25th	-	-	45	20 10'-D10R
At Wheeler & 25th	-	-	85	30 10'-D10R
Along 25th: Wheeler to Broadway	-	-	85	700 L.F. 36" RCP
Along Broadway: 25th to Market	-	-	465	600 L.F. 60" RCP
At Wheeler & Market	-	-	35	20 6'-D10R, 10 4'-D10R
Along Market: Wheeler to Broadway	-	-	35	700 L.F. 24" RCP
At Broadway & Market	3.5'x40' Grated Inlet	130	35	- - - - -
Along Market: Broadway to Enrich	-	-	510	650 L.F. 58"x91" RCP
At 25th & Enrich	-	-	145	40 16' - D10R
Along Enrich: 25th to Market	-	-	145	550 L.F. 42" RCP
At Arch & Busch	-	-	125	40 12' - D10R
Along Busch: Arch to Major Channel	44"x35' Grated Inlet	203	125	550 L.F. 36" RCP
On Bott St: Between Mulberry & Pine	-	-	160	10 4'x32' Grated Inlet
Along Bott St.	-	-	160	350 L.F. 48" RCP
At Pine & Wheeler	-	-	50	20 8' - D10R
At Broadway & Calvert	-	-	55	40 6' - D10R
At 21st & Broadway	104' D10R	10	40	20 6' - D10R
At 21st & Above Bott St.	-	-	30	10 10' - D10R
Along 21st, Wheeler to Broadway	-	-	75	700 L.F. 24" RCP
Along 21st, Between Wheeler & Broadway	-	-	Minimum	104' - D10R

DRAINAGE STRUCTURE INVENTORY (continued)

<u>LOCATION</u>	<u>EXISTING STRUCTURE</u>	<u>QP EXISTING (cfs)</u>	<u>QP REQUIRED (cfs)</u>	<u>REQUIRED STRUCTURE</u>
Along 21st, Above Bott St. to Wheeler	-	-	30-40	1350 L.F. 18" RCP
At 21st & Busch	-	-	Minimum	104' - D10R
At 21st & Wheeler	-	-	Minimum	104' - D10R
Along Mulberry: Wheeler to Broadway	-	-	100	600 L.F. 2'x3' Lined Channel
Along 21st: Broadway to Major Channel	-	-	70	500 L.F. 30" RCP
UPPER Major Channel to Point #10	-	-	0-240	2300 2'x2.5' - 3'x3.75' Lined Channel
Major Channel: #10 to #13	-	-	240 -350	700 L.F. 3'x3.75' Lined Channel
Major Channel: #13 to #14	-	-	465	400 L.F. 3'x4.5" Lined Channel
Major Channel: #14 to #16	-	-	475	850 L.F. 3.5'x4.75' Lined Channel
Major Channel: #16 to #19	-	-	580	500 L.F. 3.5'x5.5' Lined Channel
Major Channel: #9 to #18	-	-	640	750 L.F. 3.5'x5.5' Lined Channel
Major Channel: #18 to #19	-	-	720	800 L.F. 4'x5.75' Lined Channel
Major Channel: #19 to #21	-	-	1300	700 L.F. 5'x7' Lined Channel
Along Enrich	2 @ 18" CMP	Min.	-	Curb & Gutter
At Broadway & Calvert	48" CMP	54	55	Replace w/ 40 6' - D10R
Along Calvert: Broadway to Major Channel	-	-	55	650 L.F. 33" RCP
Along Busch: Between Calvert & Pine	44" x 35'	203	40	-
	Grated Inlet	-	-	-
Along South: Between Pine & Mulberry	-	-	100	20 80L.F. 21" RCP At Ground Grade
At Pine and Wheeler	3 @ 36"x48"	195	475	20 53 L.F. 54" RCP @ 2.00 %
	CMP	-	-	-
At Wheeler & Mulberry	4' x 45'	400	100	-
	Grated Inlet	-	-	-
At Wheeler & Mulberry	54" Lowhead	58	100	5 L.F. 42" RCR @ 2.00%
	CMP	-	-	-
At Broadway & Mulberry	2 @ 4'x4'	75	45	-
	Grated Inlet	-	-	-
At Broadway & Mulberry	2 @ 3.25' x 620	-	580	-
	5.25' Ellipse	-	-	-
At Point #18	5'x6' Cinder	980	720	35 L.F. 66" RCP
	Block Conduit	-	-	-
At End of Pecan	2 @ 72" CMP	235	1300	Increase Grade to 1.7%
On West side of 21st Street	2 @ 84" CMP	1244	1300	-
Under 21st Street	10'x10'	4250	1300	-
	Concrete	-	-	-
	Conduit	-	-	-

DRAINAGE BASIN IMPROVEMENTS INVENTORY SUMMARY

<u>ITEM</u>	<u>DIAMETER</u> (in)	<u>LENGTH</u> (ft)	<u>DIMENSIONS</u> (in)	<u>QUANTITY</u>
RCP	18"	1400	-	-
RCP	21"	160	-	-
RCP	24"	1400	-	-
RCP	27"	70	-	-
RCP	30"	500	-	-
RCP	33"	650	-	-
RCP	36"	1250	-	-
RCP	42"	1900	-	-
RCP	48"	325	-	-
RCP	54"	1400	-	-
RCP	60"	500	-	-
RCP	-	650	58"x91"	-
Catch Basins	-	-	4' D10R	5
Catch Basins	-	-	6' D10R	16
Catch Basins	-	-	8' D10R	2
Catch Basins	-	-	10' D10R	11
Catch Basins	-	-	12' D10R	7
Catch Basins	-	-	16' D10R	4
Grated Inlets	-	-	4'x32'	1
Lined Channels	-	2600	1.5'x2'	-
Lined Channels	-	1900	2'x2.5'	-
Lined Channels	-	750	2'x3'	-
Lined Channels	-	2300	3'x3.75'	-
Lined Channels	-	1300	3.5'x5.5'	-
Lined Channels	-	400	3'x4.5'	-
Lined Channels	-	800	3.5'x4.75'	-
Lined Channels	-	750	5'x7'	-
Flaired End	-	-	-	-
Sections	-	-	-	3
Manholes	-	-	-	21

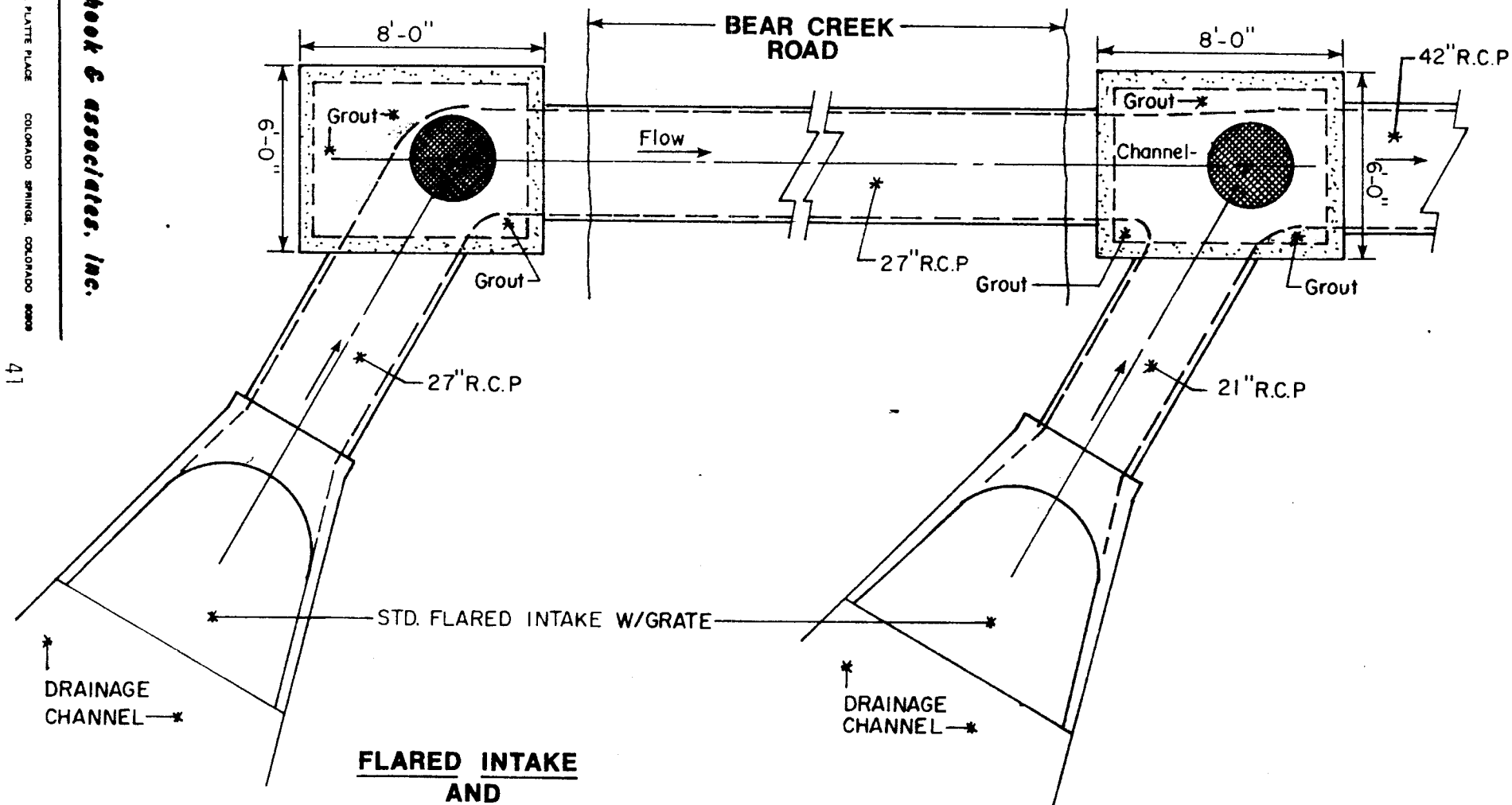


Drainage Channel

r. keith hook & associates, inc.

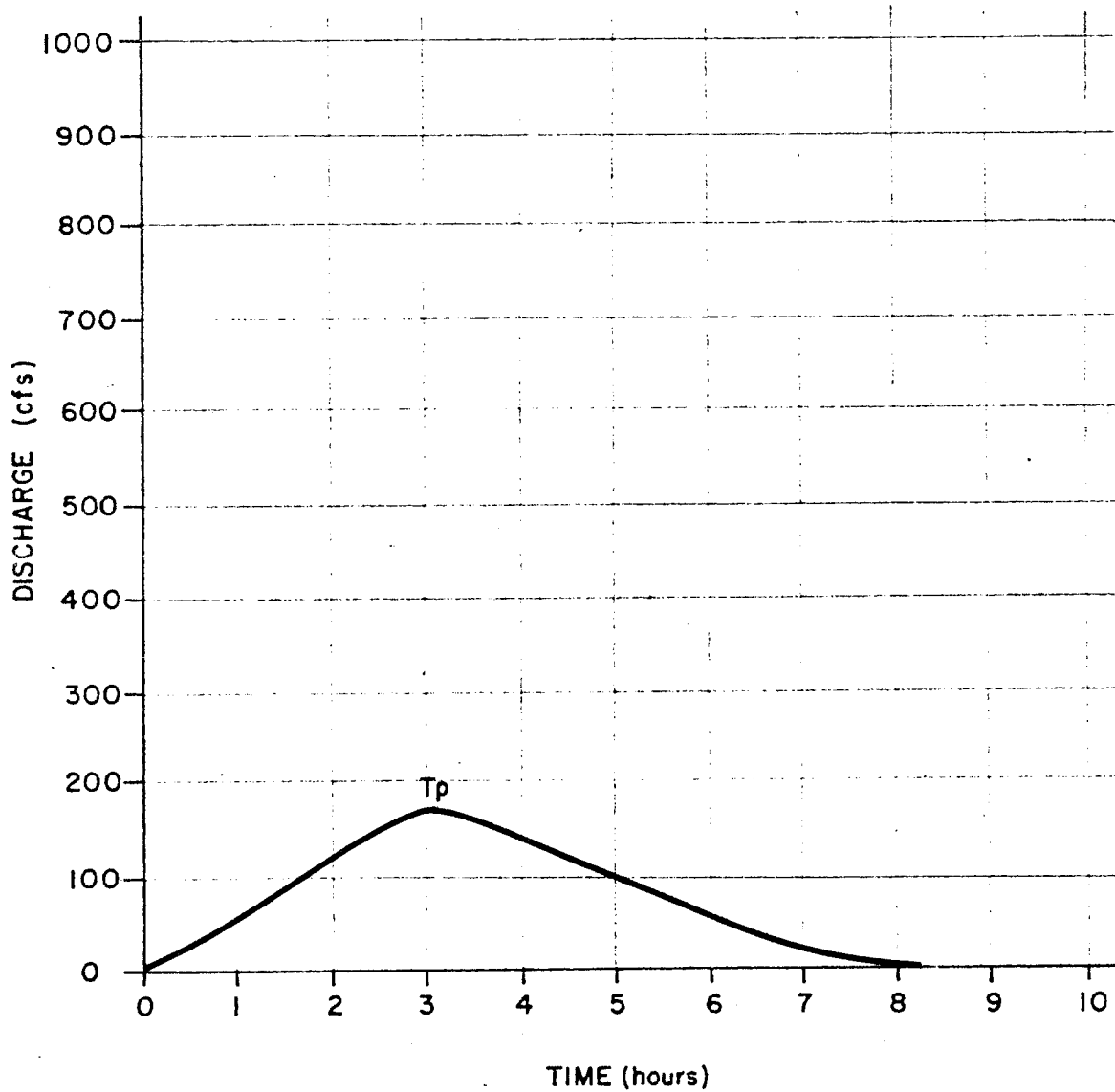
PHONE 473-5653 2646 E. PLATTE PLACE COLORADO SPRINGS, COLORADO 80909

FIGURE-2



**FLARED INTAKE
AND
DIVERSION STRUCTURE**
FIGURE-3

HYDROGRAPH POINT 1



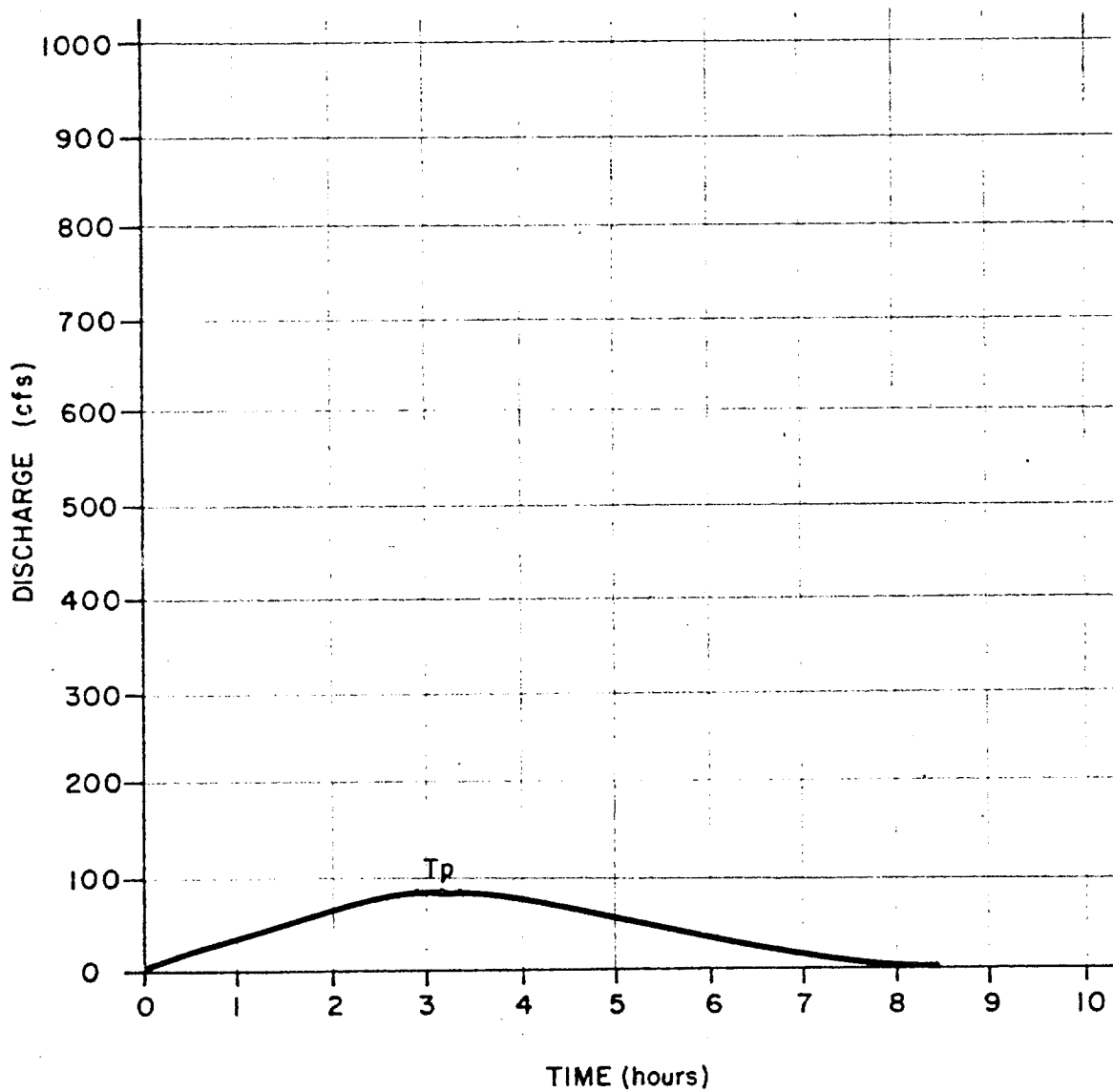
$T_p = 3.09$ hrs.

$T_b = 8.25$ hrs.

$Q_p = 175$ cfs

r. keith hook & associates, inc.

HYDROGRAPH POINT 1A



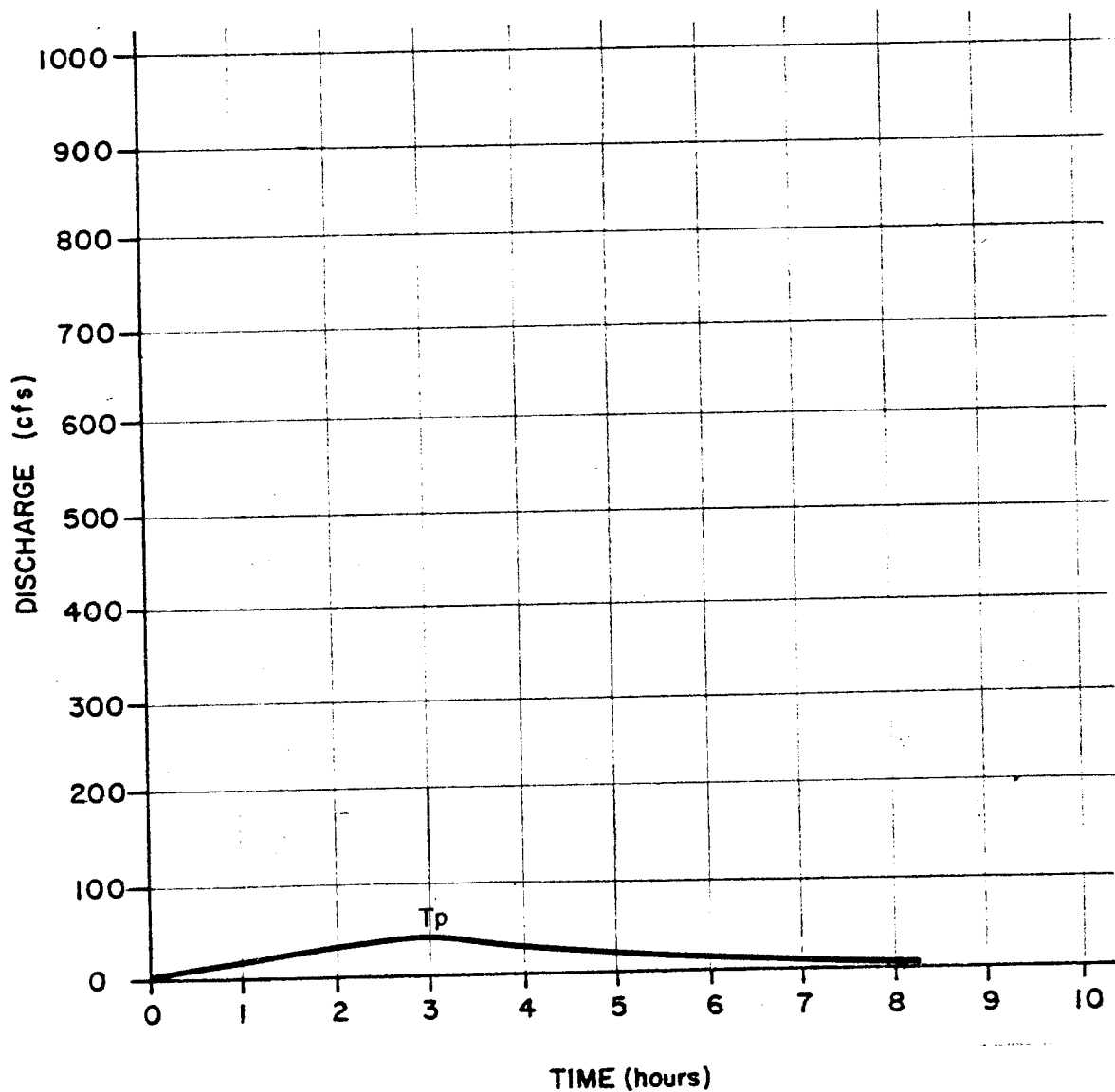
$T_p = 3.07$ hrs.

$T_b = 8.20$ hrs.

$Q_p = 88$ cfs

r. keith hook & associates, inc.

HYDROGRAPH POINT 1B



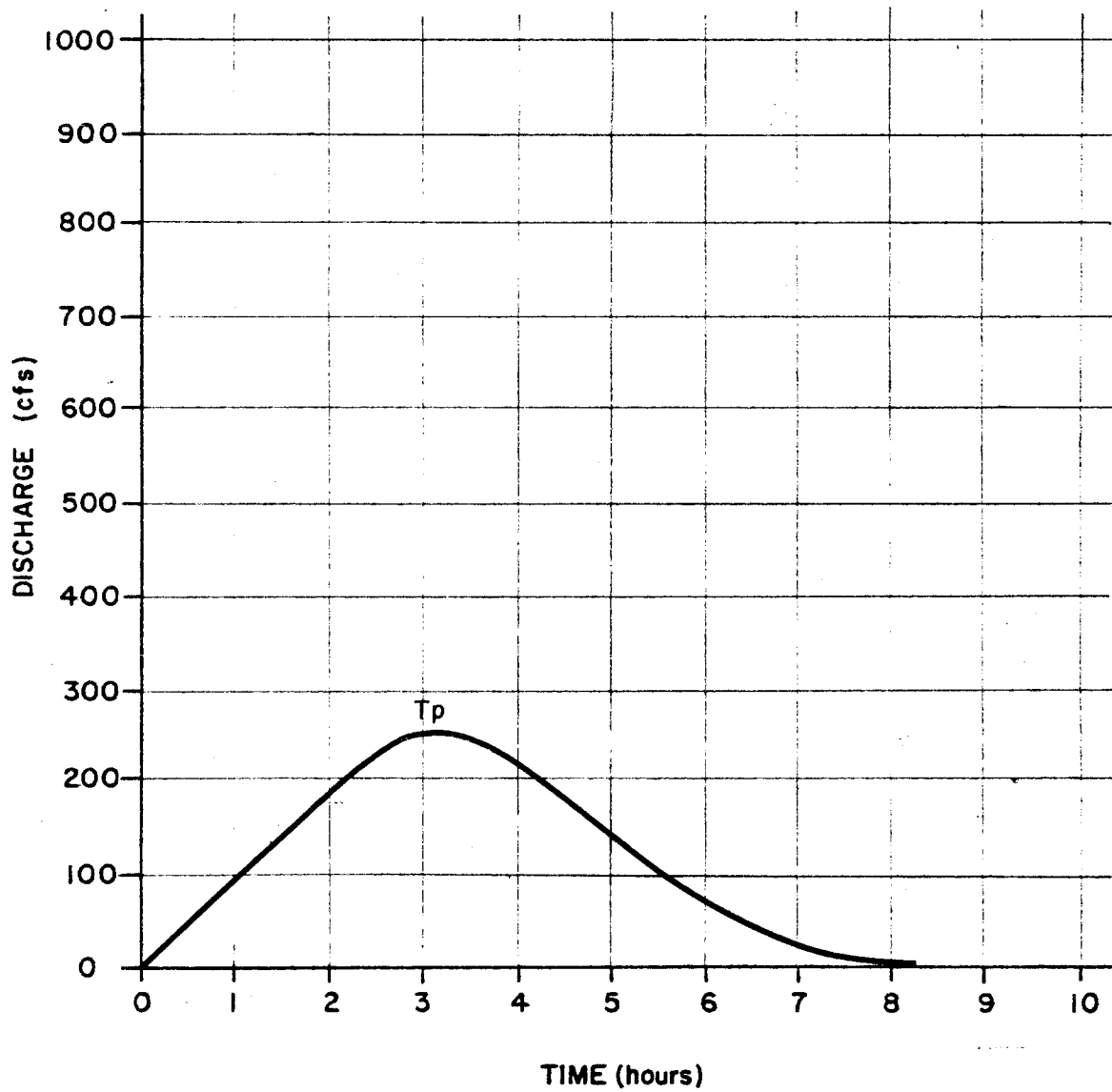
$T_p = 3.07$ hrs.

$T_b = 8.20$ hrs.

$Q_p = 42$ cfs

r. keith hook & associates, inc.

HYDROGRAPH POINT 2



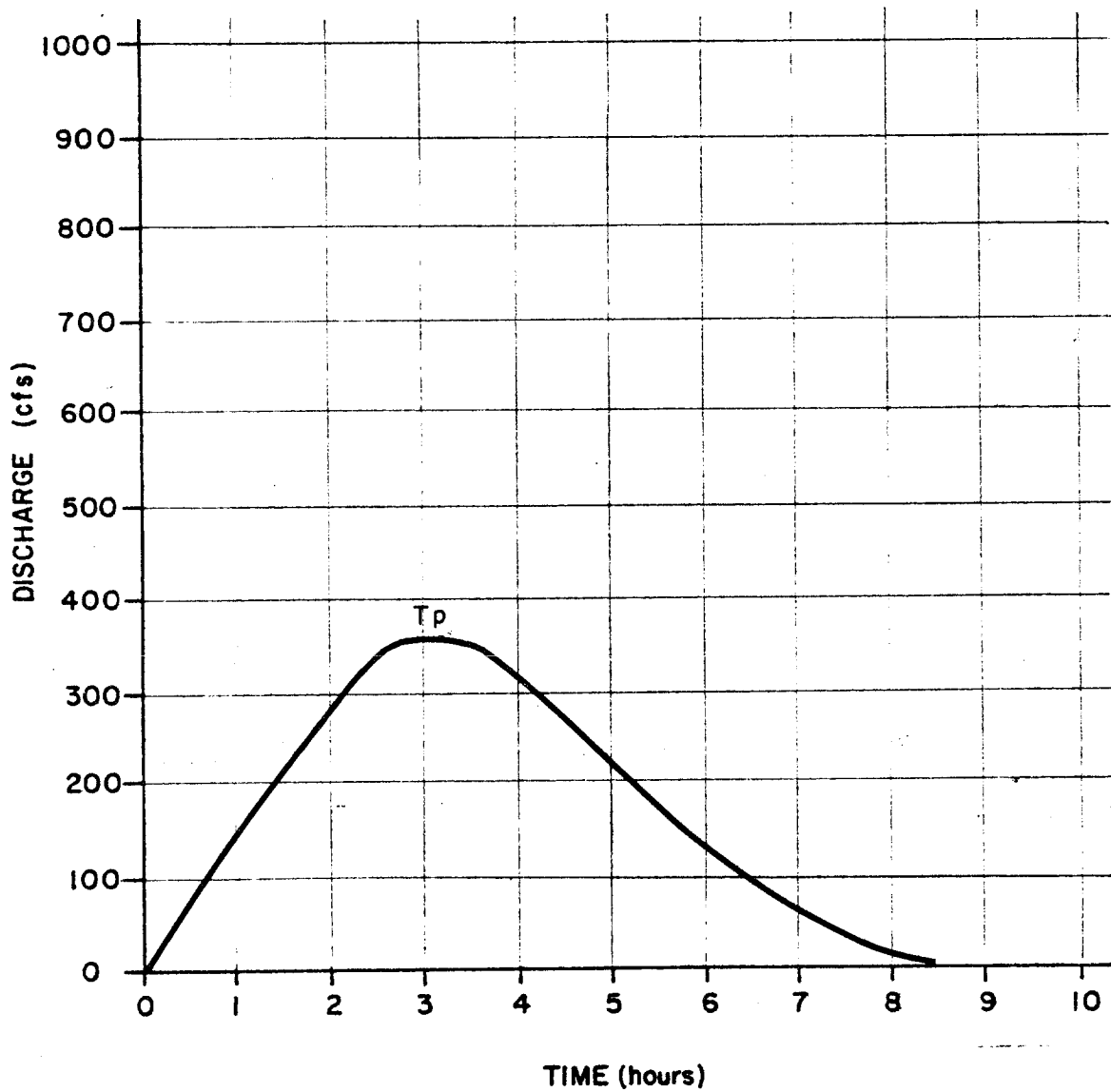
$T_p = 3.10$ hrs.

$T_b = 8.28$ hrs.

$Q_p = 265$ cfs

r. keith hook & associates, inc.

HYDROGRAPH POINT 3



$T_p = 3.12$ hrs.

$T_b = 8.34$ hrs.

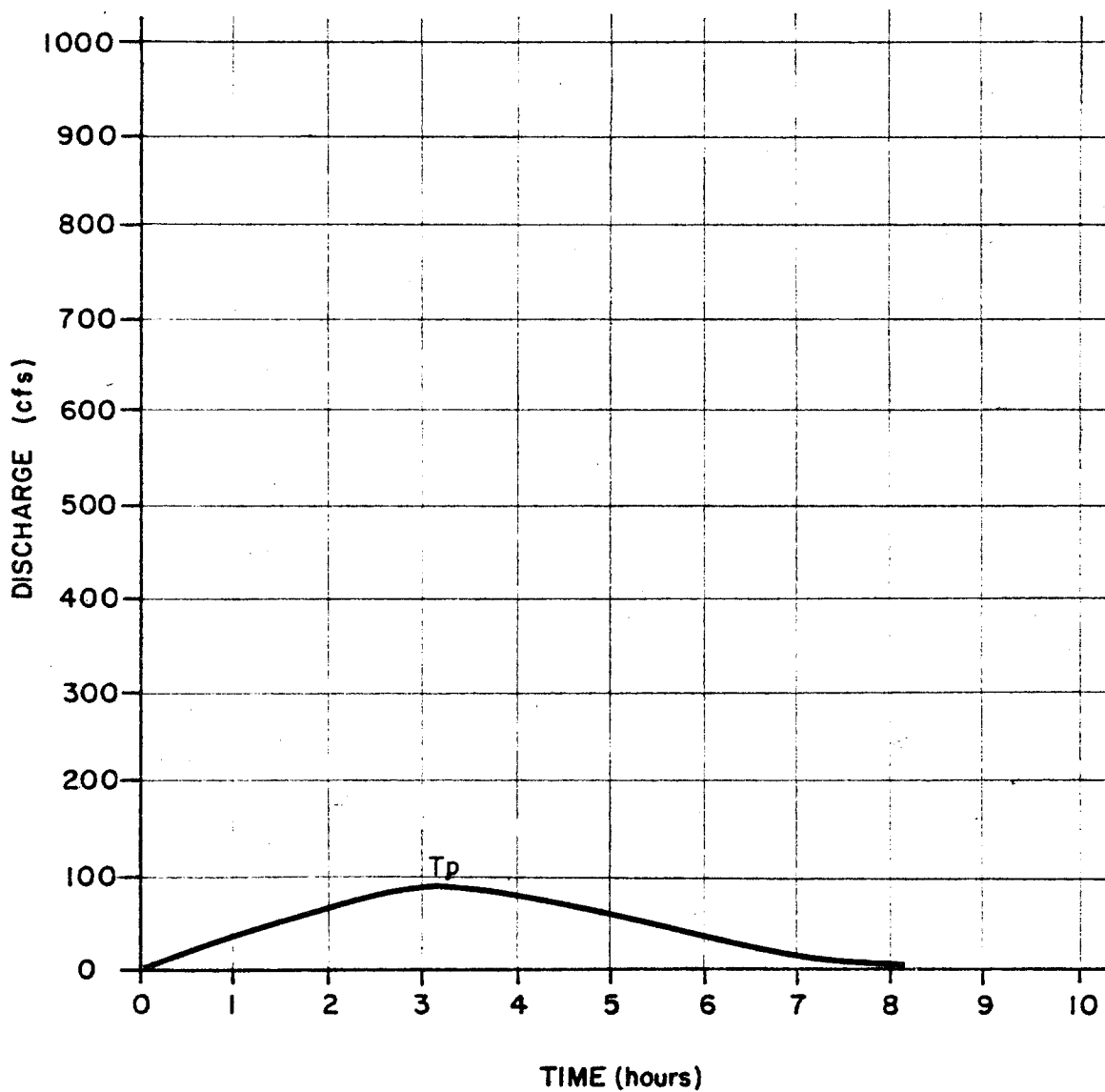
$Q_p = 365$ cfs

r. keith hook & associates, inc.



PHONE 473-8853 2545 E. PLATTE PLACE COLORADO SPRINGS, COLORADO 80909

HYDROGRAPH POINT 4



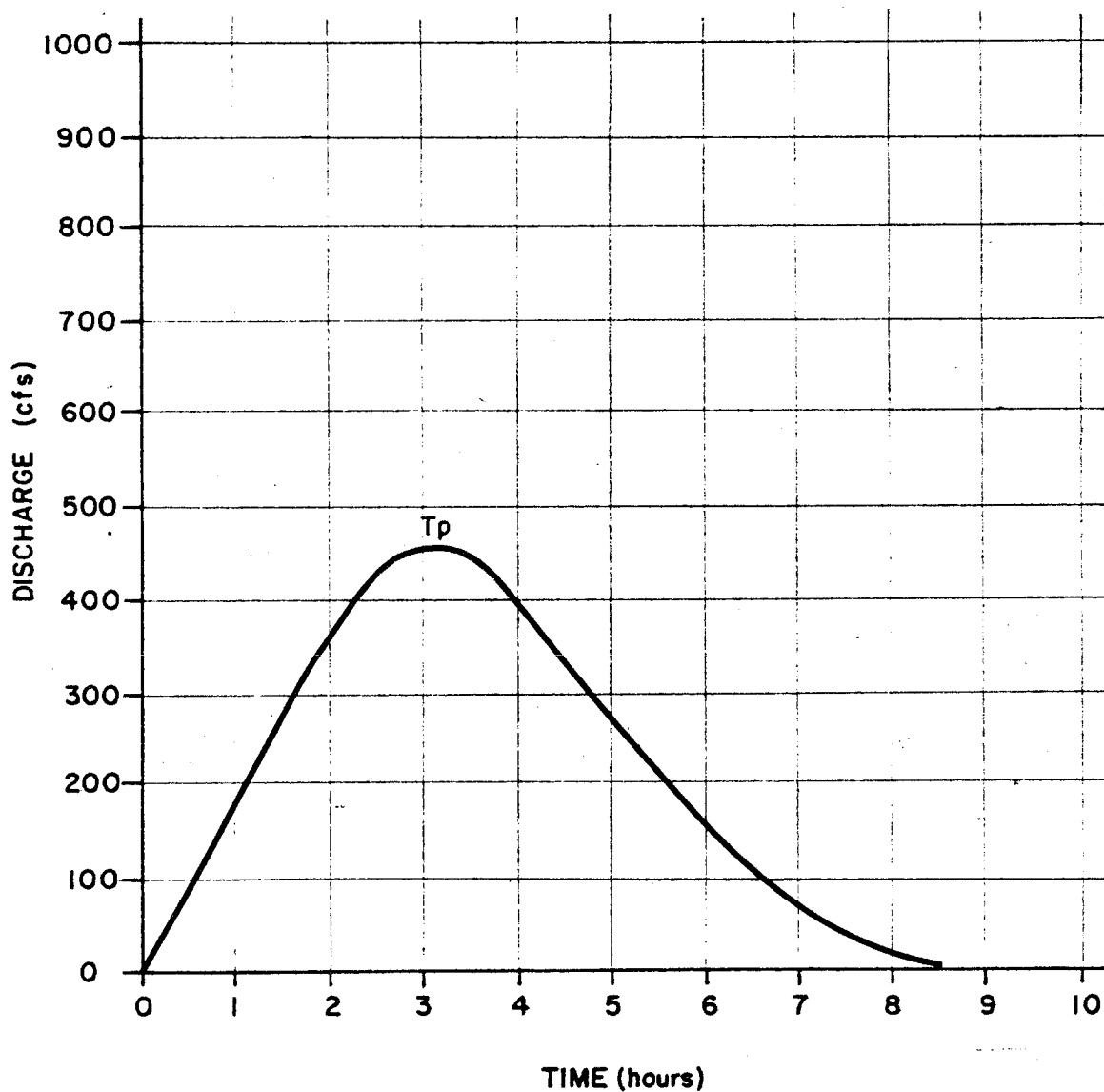
$T_p = 3.04$ hrs.

$T_b = 8.13$ hrs.

$Q_p = 85$ cfs

r. keith hook & associates, inc.

HYDROGRAPH POINT 5



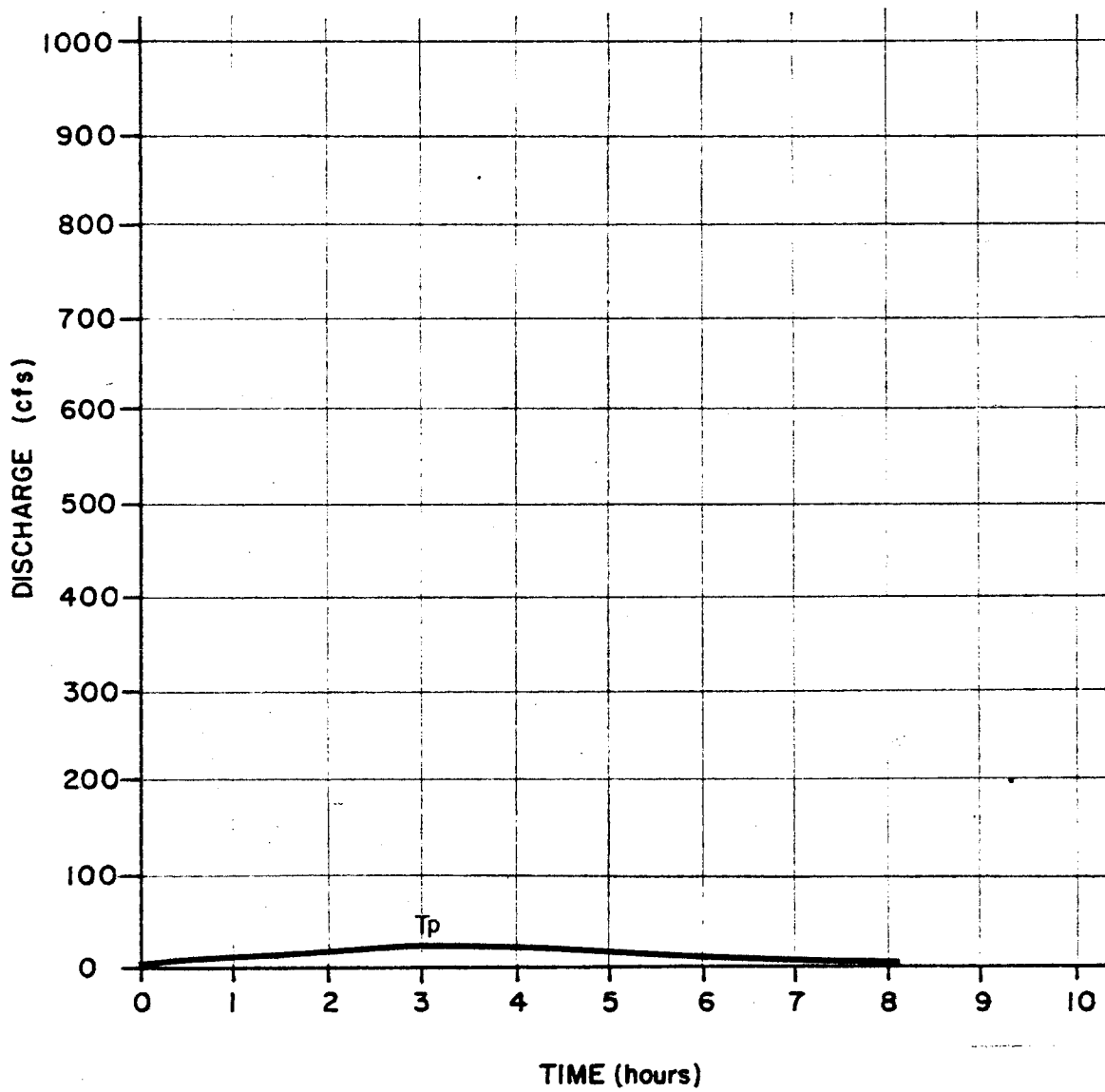
$T_p = 3.14$ hrs.

$T_b = 8.40$ hrs.

$Q_p = 460$ cfs

r. keith hook & associates, inc.

HYDROGRAPH POINT 6



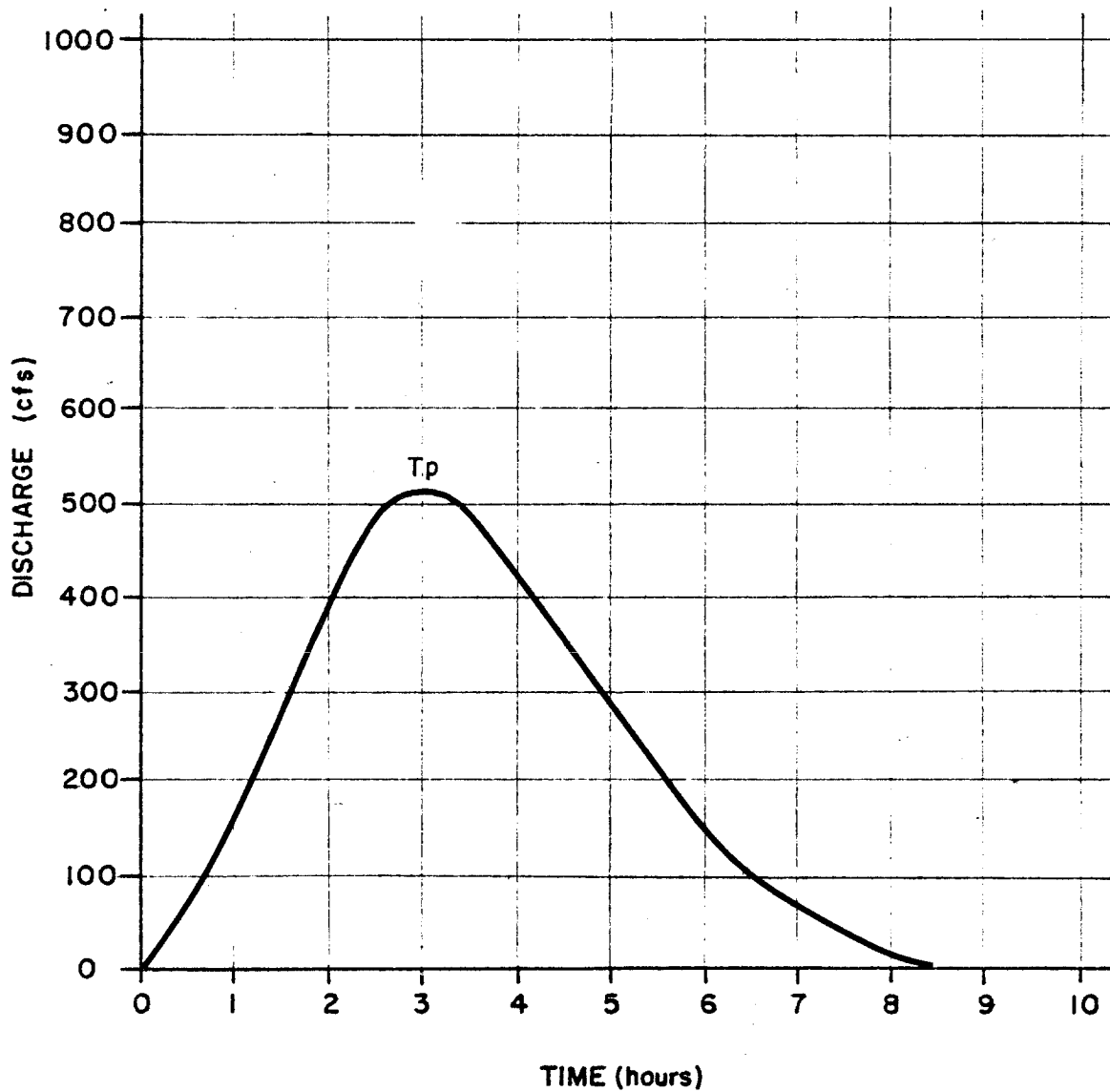
$T_p = 3.04$ hrs.

$T_b = 8.12$ hrs.

$Q_p = 35$ cfs

r. keith hook & associates, inc.

HYDROGRAPH POINT 7



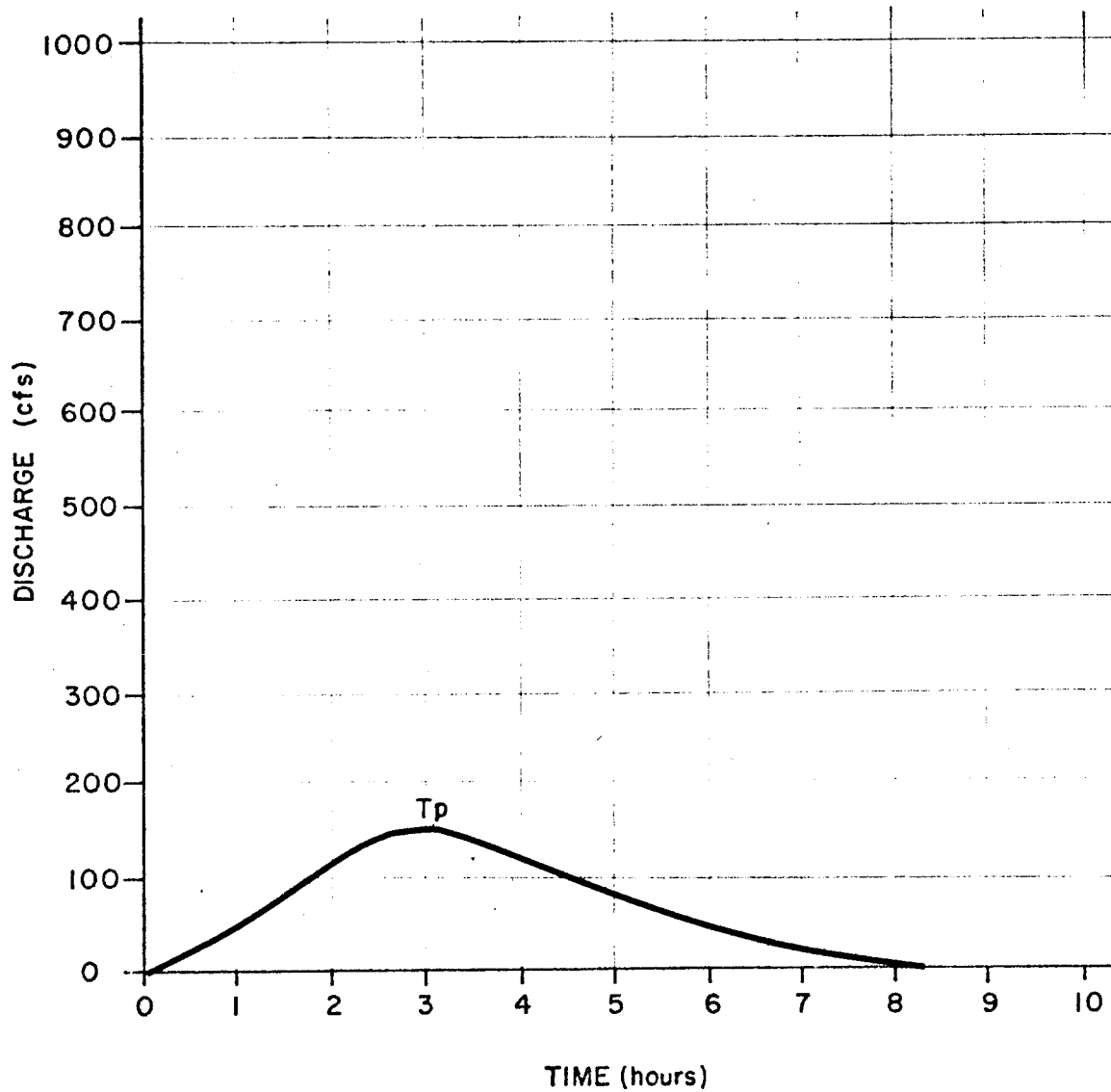
$T_p = 3.16$ hrs.

$T_b = 8.44$ hrs.

$Q_p = 510$ cfs

r. keith hook & associates, inc.

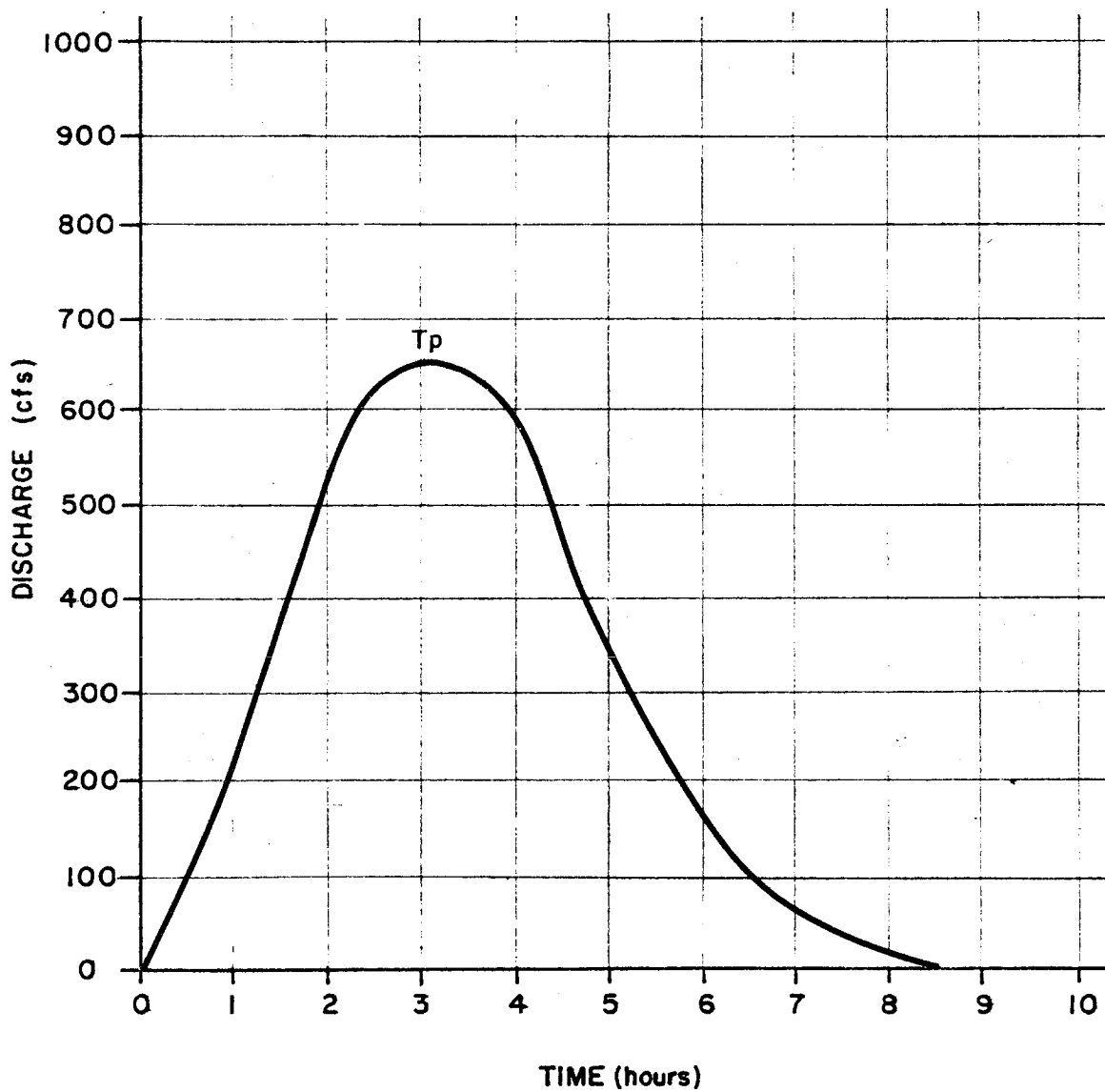
HYDROGRAPH POINT 8



$T_p = 3.06$ hrs.
 $T_b = 8.18$ hrs.
 $Q_p = 145$ cfs

n. Keith Beck & associates, Inc.

HYDROGRAPH POINT 9



$T_p = 3.18$ hrs.

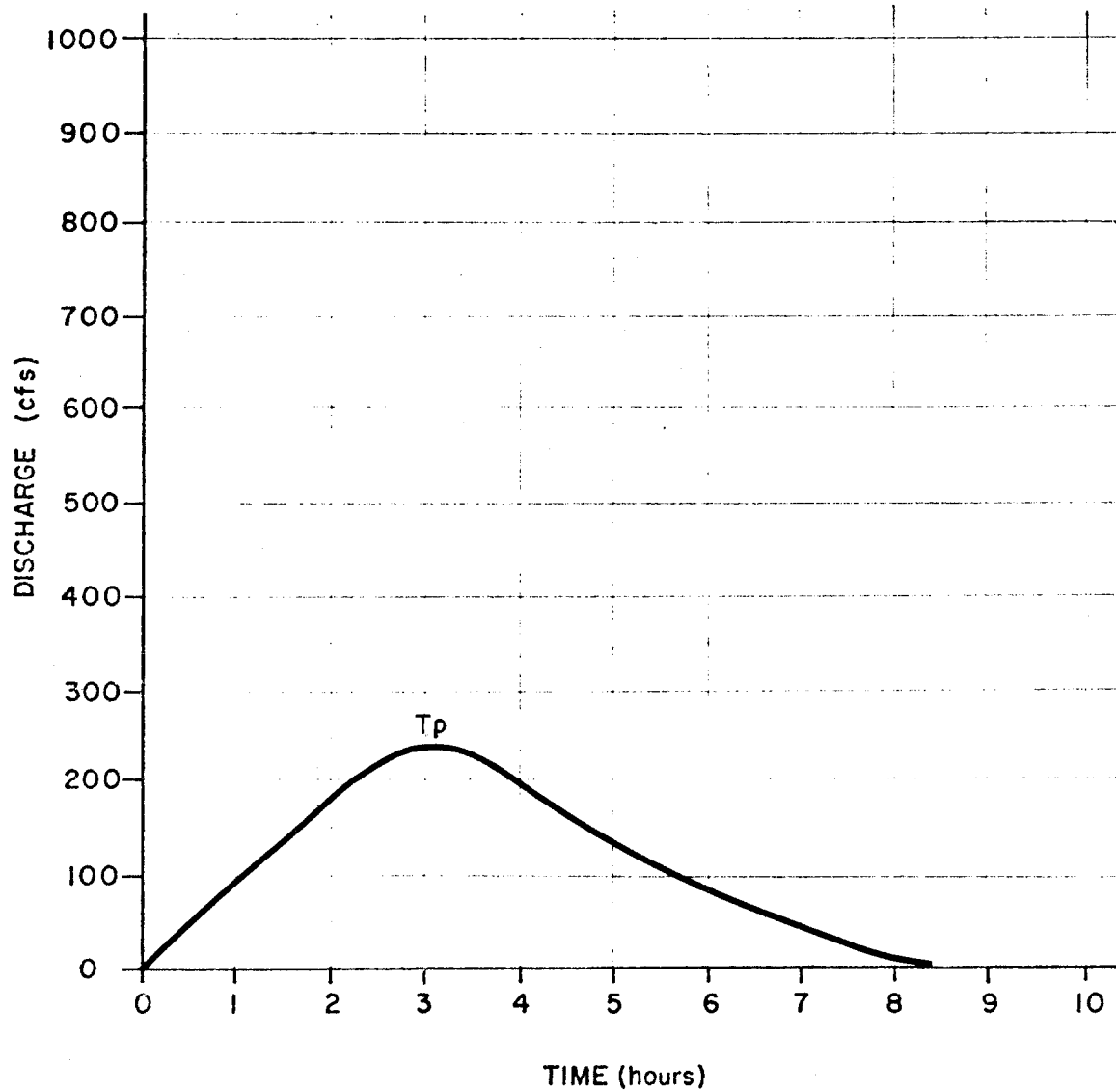
$T_b = 8.50$ hrs.

$Q_p = 640$ cfs

r. keith hook & associates, inc.

PHONE 473-6888 2846 E. PLATTE PLACE COLORADO SPRINGS, COLORADO 80909

HYDROGRAPH POINT 10



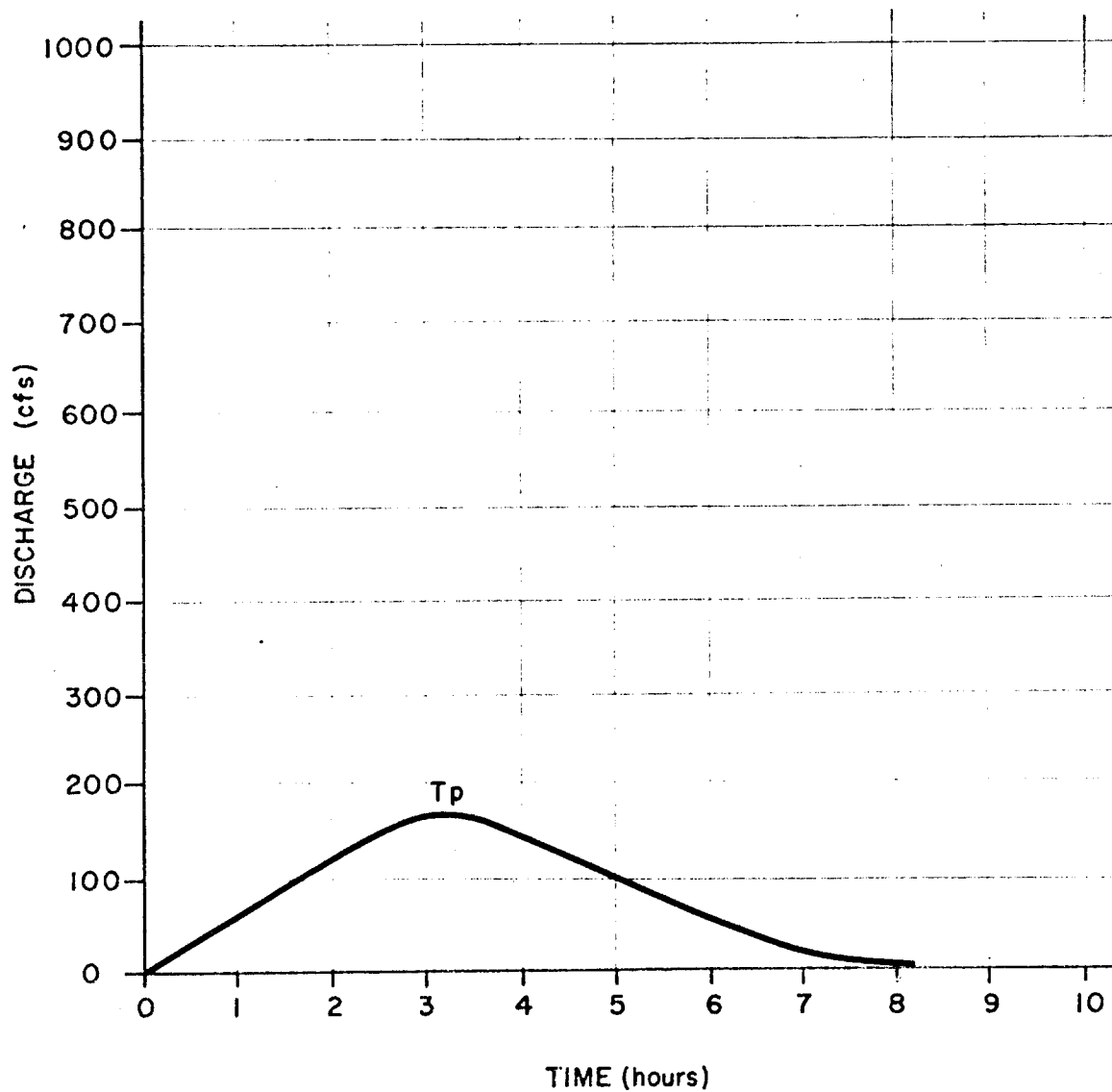
$T_p = 3.10$ hrs.

$T_b = 8.29$ hrs.

$Q_p = 240$ cfs

H. Leigh Cook & Associates, Inc.

HYDROGRAPH POINT 11



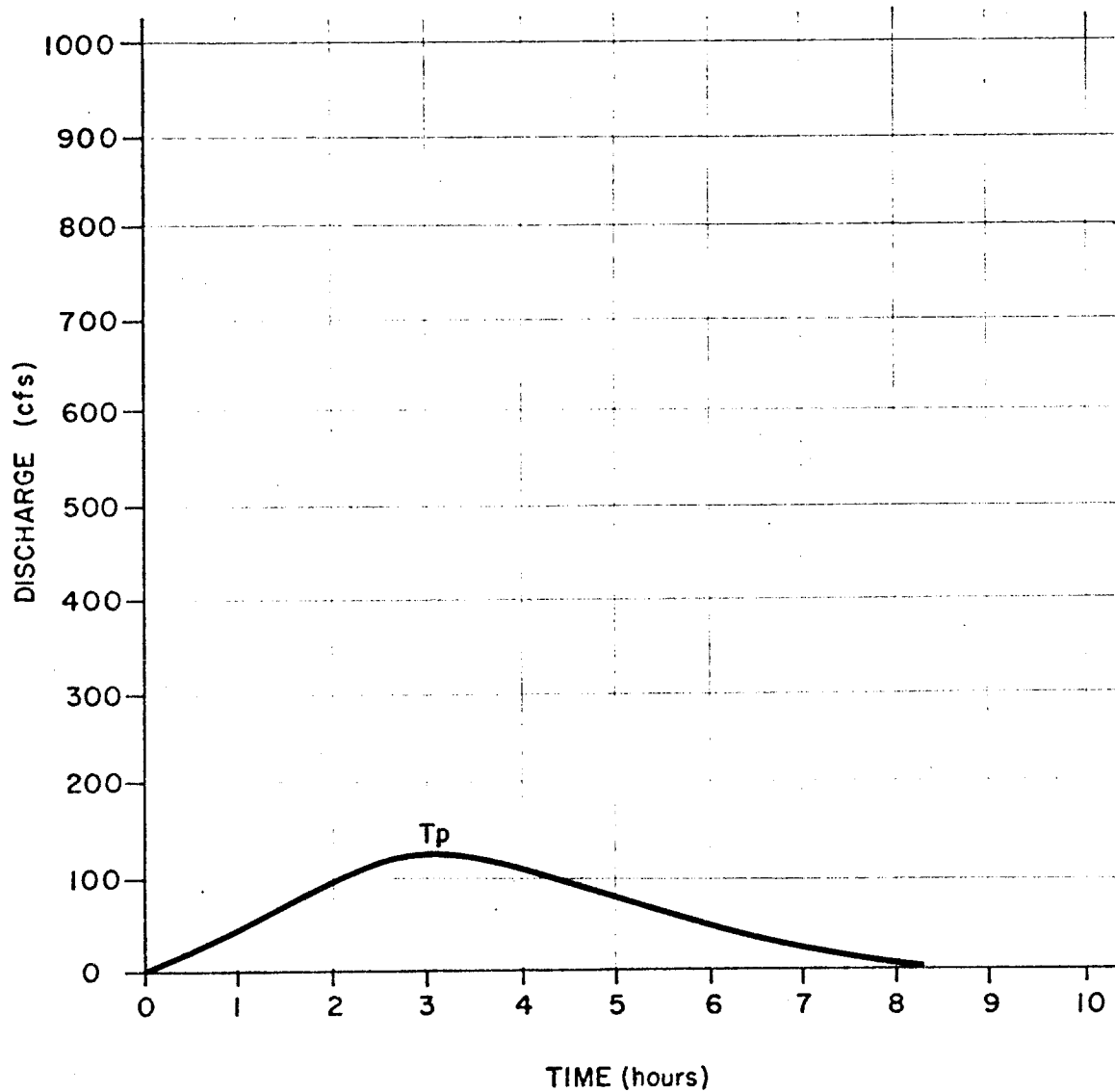
$T_p = 3.05$ hrs.

$T_b = 8.15$ hrs.

$Q_p = 160$ cfs

r. Keith Bush & Associates, Inc.

HYDROGRAPH POINT 12



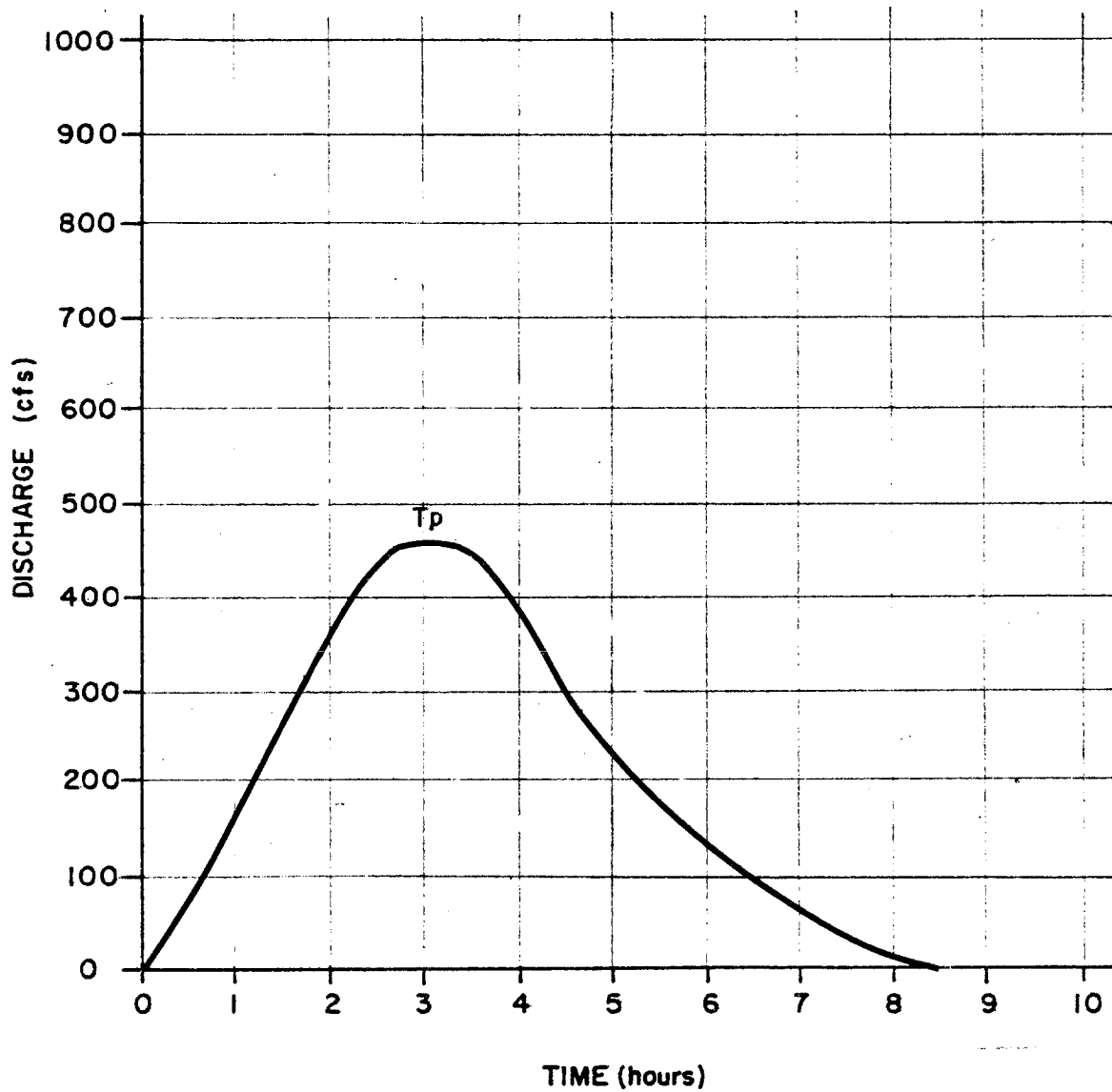
$T_p = 3.06$ hrs.

$T_b = 8.16$ hrs.

$Q_p = 125$ cfs

n. Keith Root & Associates, Inc.

HYDROGRAPH POINT 13



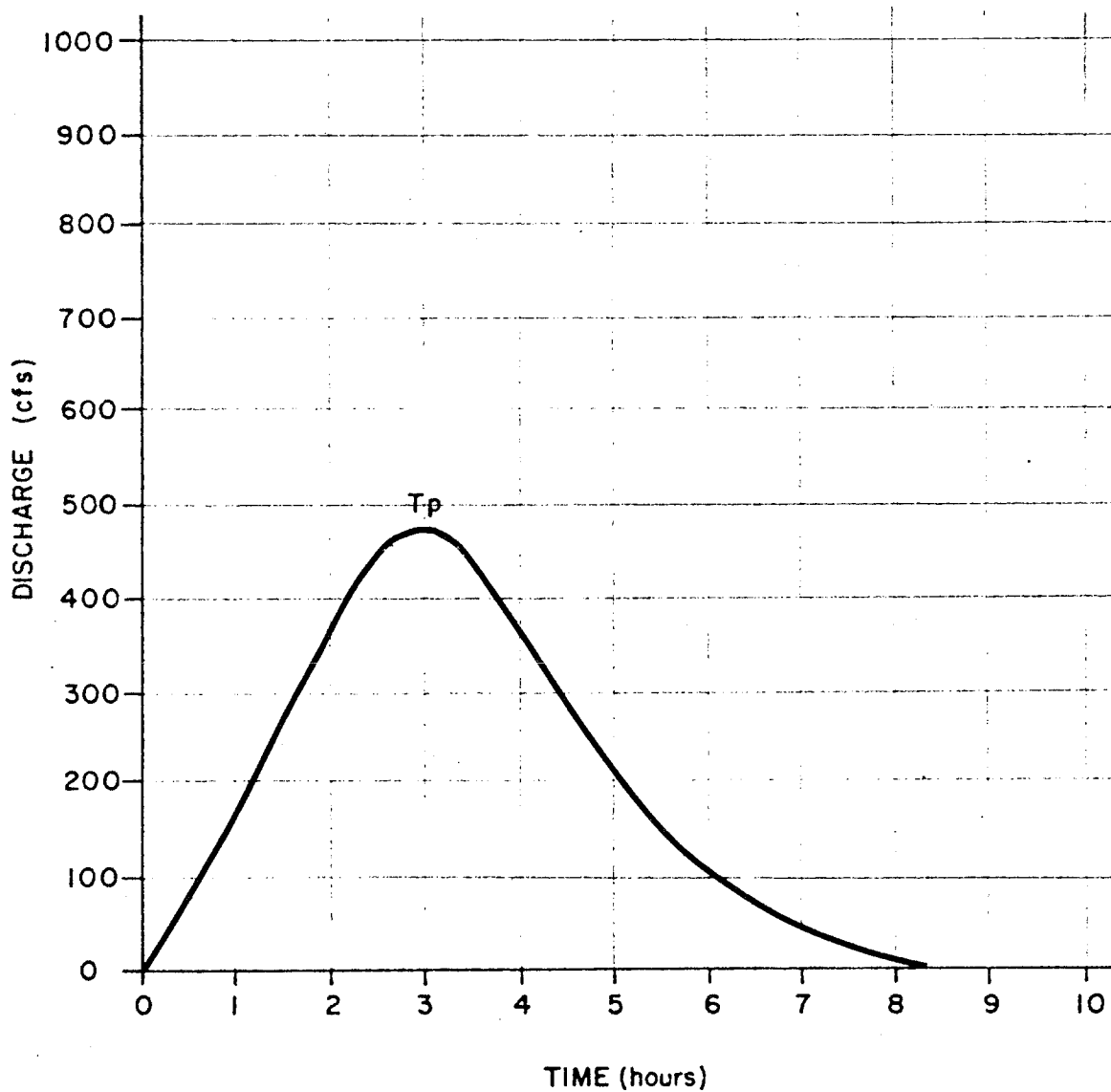
$T_p = 3.13$ hrs.

$T_b = 8.35$ hrs.

$Q_p = 465$ cfs

r. keith hook & associates, inc.

HYDROGRAPH POINT 14



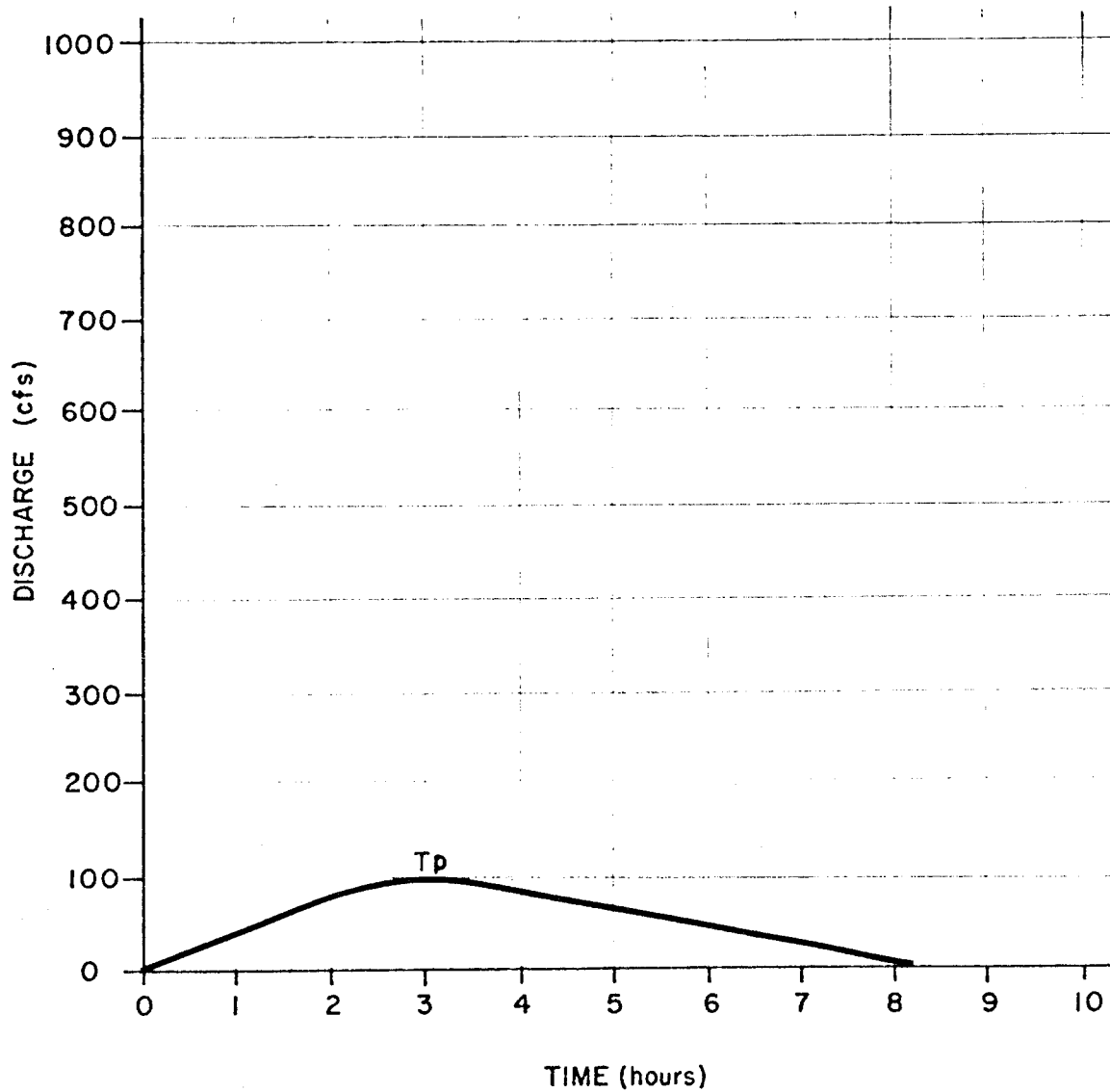
$T_p = 3.14$ hrs.

$T_b = 8.38$ hrs.

$Q_p = 475$ cfs

r. keith hook & associates, inc.

HYDROGRAPH POINT 15



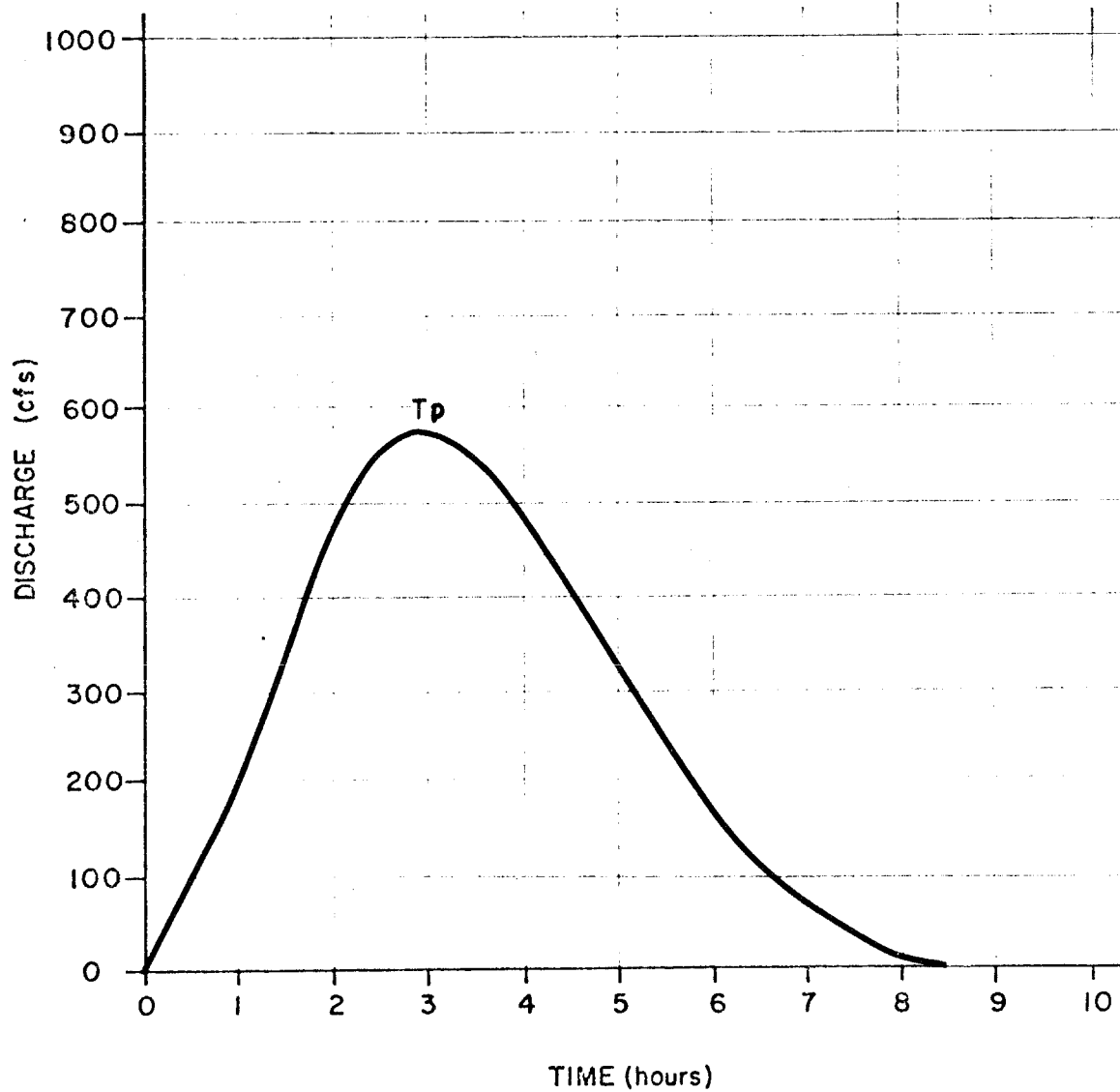
$T_p = 3.04$ hrs.

$T_b = 8.12$ hrs.

$Q_p = 100$ cfs

E. Keith Cook & Associates, Inc.

HYDROGRAPH POINT 16



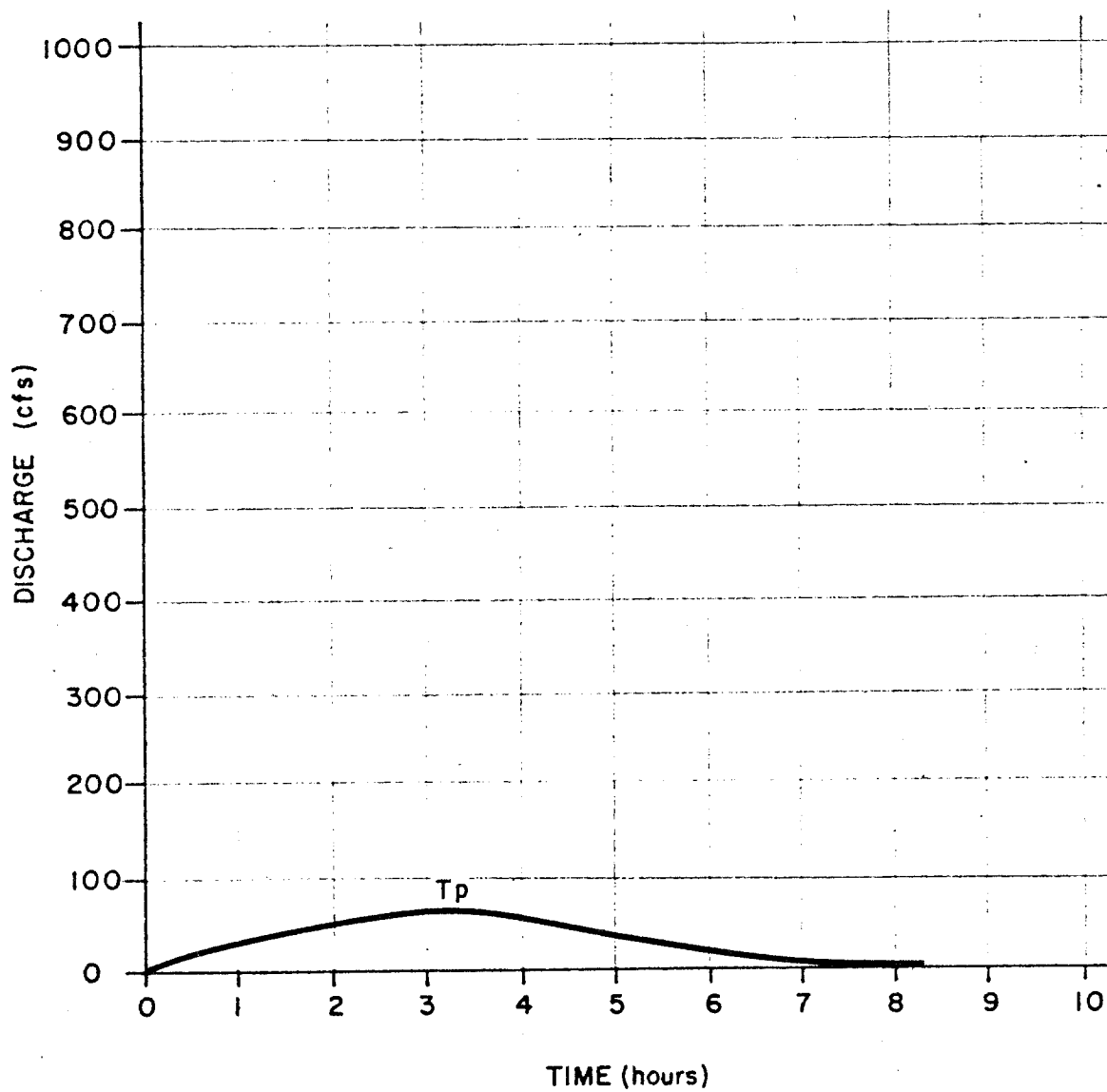
$T_p = 3.16$ hrs.

$T_b = 8.45$ hrs.

$Q_p = 580$ cfs

W. Keith Cook & Associates, Inc.

HYDROGRAPH POINT 17



$T_p = 3.06$ hrs.

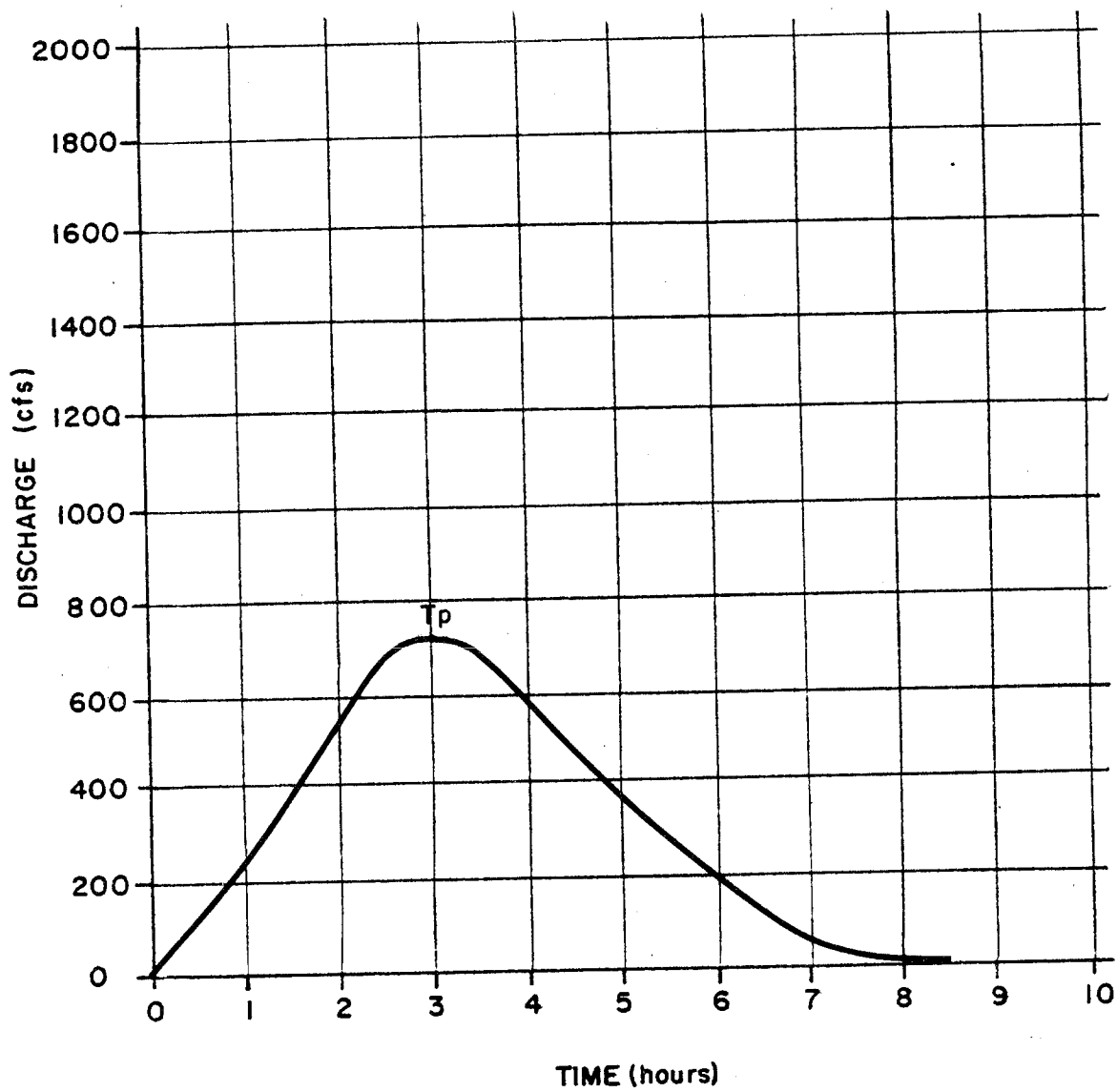
$T_b = 8.16$ hrs.

$Q_p = 55$ cfs

r. keith hook & associates, inc.



HYDROGRAPH POINT 18



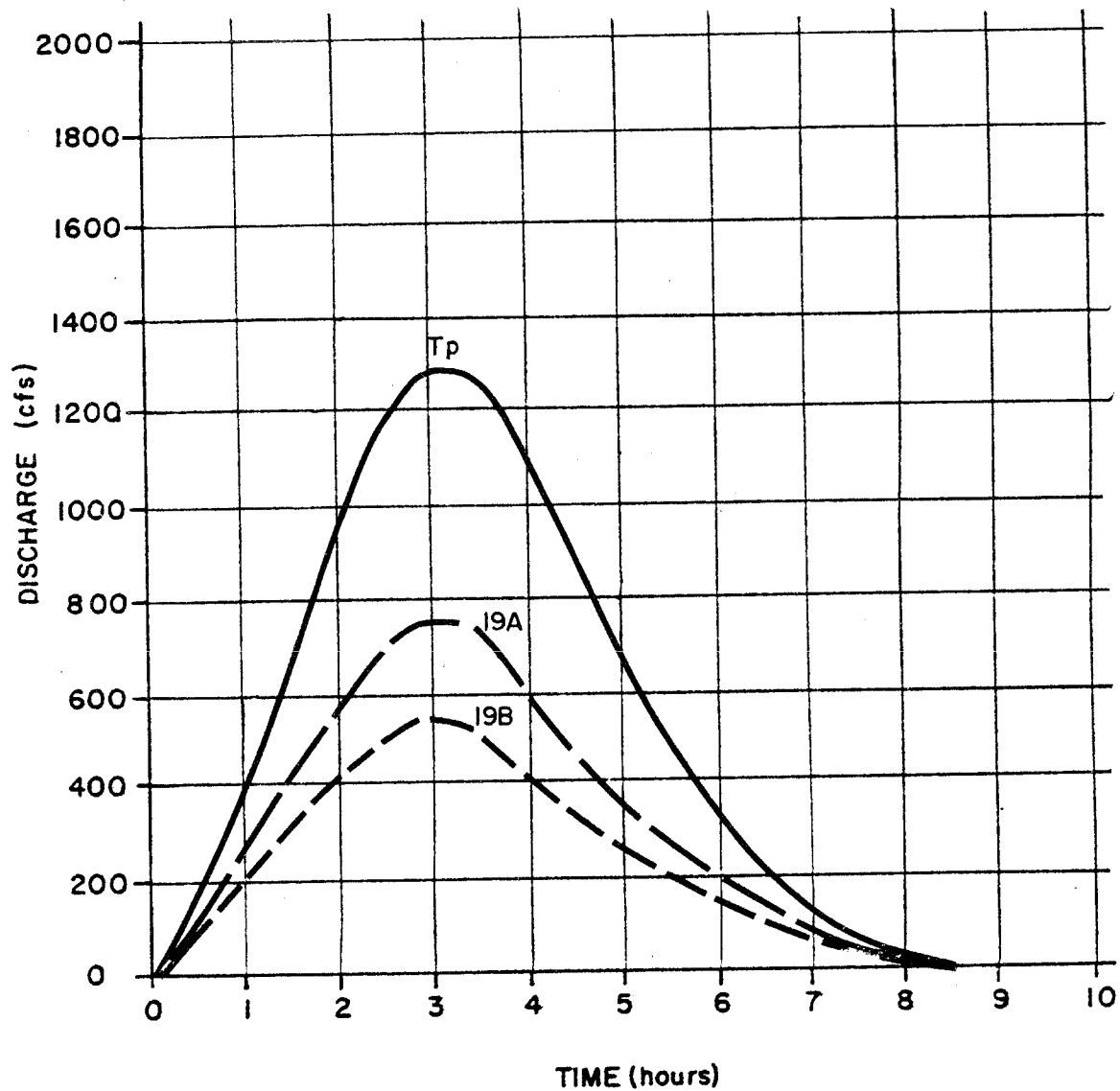
$T_p = 3.21$ hrs.

$T_b = 8.57$ hrs.

$Q_p = 720$ cfs

r. keith hook & associates, inc.

HYDROGRAPH POINT 19



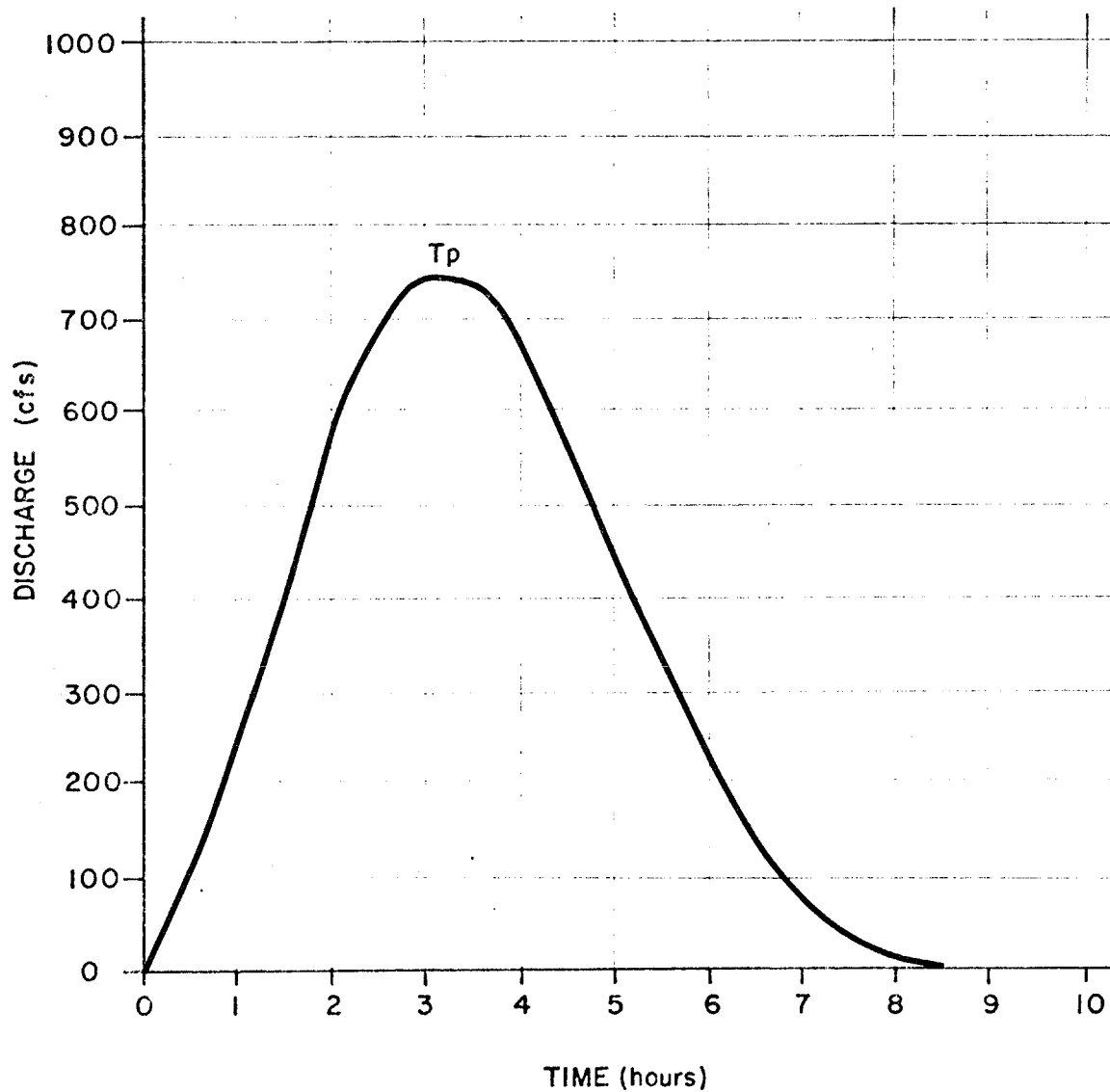
$T_p = 3.20$ hrs.

$T_b = 8.50$ hrs.

$Q_p = 1300$ cfs

r. keith hook & associates. inc.

HYDROGRAPH POINT 19A



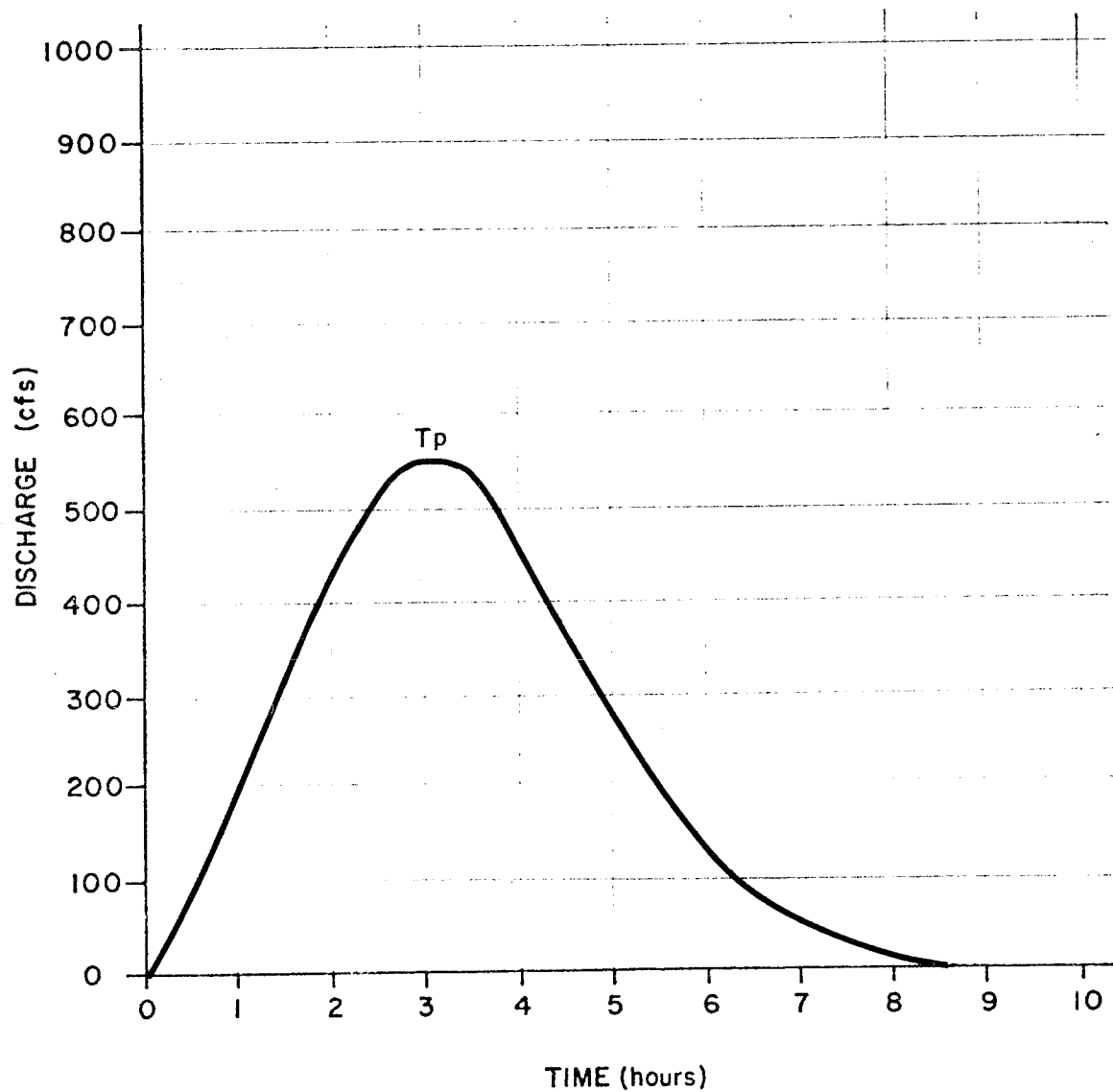
$T_p = 3.23$ hrs.

$T_b = 8.62$ hrs.

$Q_p = 750$ cfs

W. L. H. & Associates, Inc.

HYDROGRAPH POINT 19B



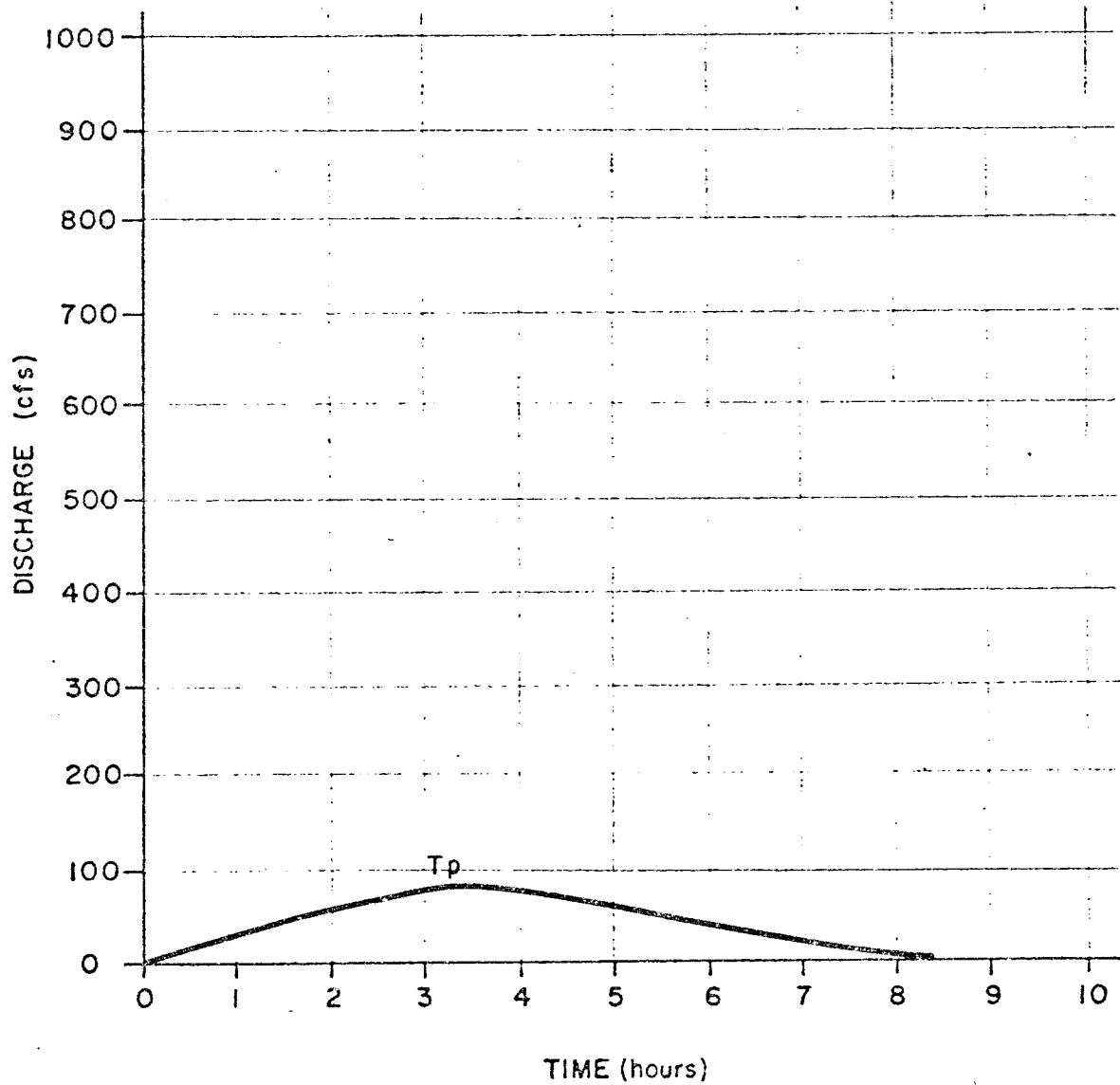
$T_p = 3.18$ hrs.

$T_b = 8.50$ hrs.

$Q_p = 555$ cfs

R. Keith Koch & Associates, Inc.

HYDROGRAPH POINT 20



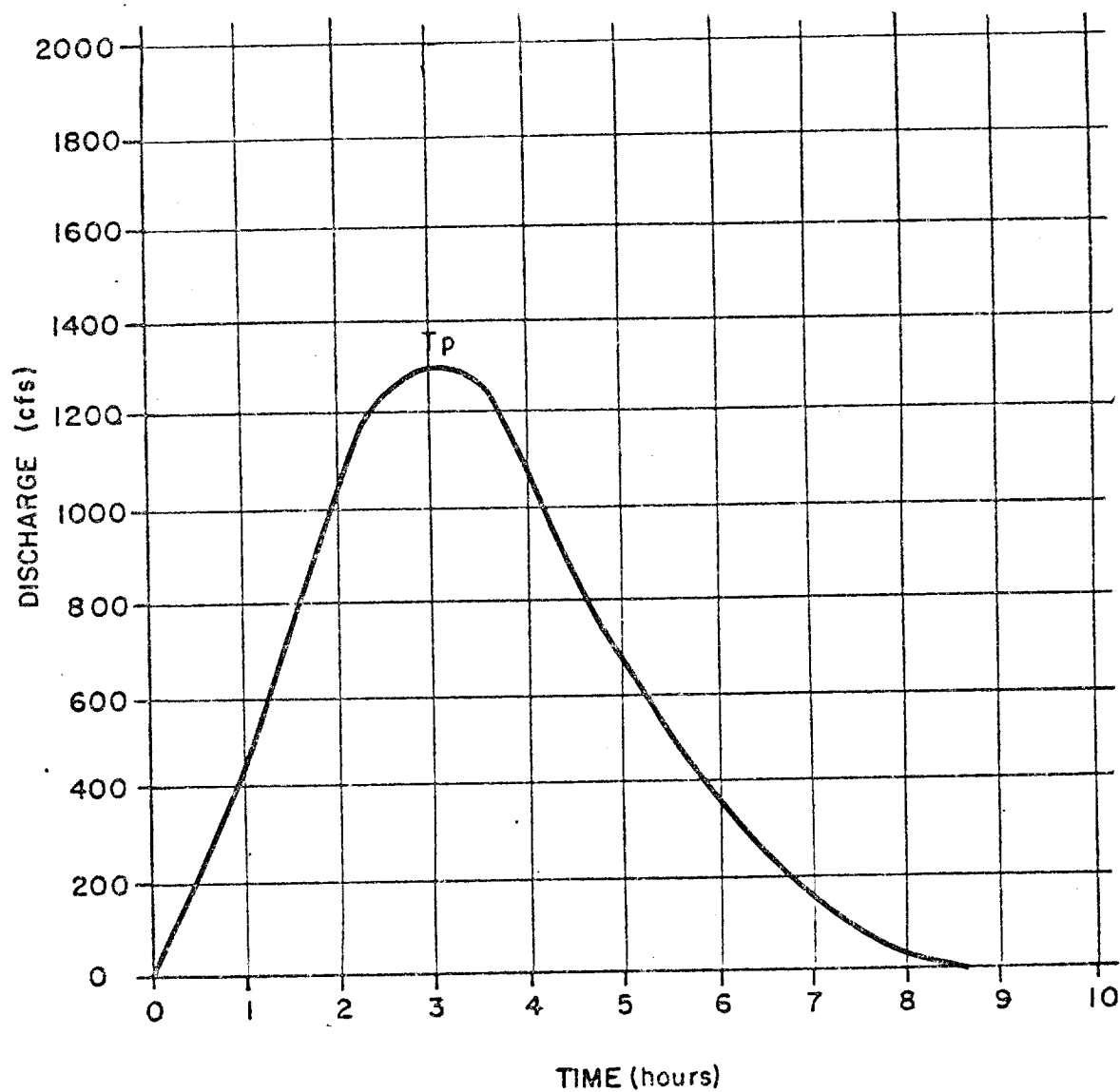
$T_p = 3.10$ hrs.

$T_b = 8.27$ hrs.

$Q_p = 70$ cfs

r. Keith hook & associates, inc.

HYDROGRAPH POINT 21



$T_p = 3.22$ hrs.

$T_b = 8.60$ hrs.

$Q_p = 1300$ cfs

r. keith hook & associates, inc.

RECOMMENDED FREEBOARD AND HEIGHT OF
BANK OF LINED CHANNELS (U.S. BUREAU
OF RECLAMATION) - FROM CHOW, V.T.
"OPEN CHANNEL HYDRAULICS", FIGURE 7-1

