

Peterson Air Force Base
Colorado Springs, Colorado

Type "A" Report
Basewide Storm Drainage Study
Peterson Project No. 91-1061E
for
1003 CES/DEED, Stop 37, Peterson AFB, Colorado 80914

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100% Submittal

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PART 1

GENERAL DESCRIPTION

1

1.1 Purpose:

The purpose of this report is to provide Type "A" services for Peterson AFB, Project 91-1061E, Basewide Storm Drainage Study. The existing storm drainage system was constructed in phases without the benefit of a comprehensive drainage plan. The result is an incohesive and inadequate system. This report will identify existing problem drainage areas and make recommendations for improving the major drainage system. Future development will also be anticipated. Drainage system improvements will comply with future flows and drainage patterns.

1.2 Project Description:

The study area includes all of Peterson AFB north and east of the existing runways except Peterson East. The area is approximately 1,000 acres of mostly developed land. The storm water runoff will be analyzed using the Army Corps of Engineers hydraulics computer program HEC-1. Hydrographs and rainfall rates are provided by the City of Colorado Springs. Future drainage requirements will be anticipated and incorporated into the proposed drainage plan.

1.3 Authorization:

This Type "A" report was authorized by 3 SSW/PKBAC Contract No. DACA21-90-00004, "Basewide Storm Drainage Study, No. 91-1061E".

1.4 Criteria Used:

1.4.1 City of Colorado Springs and El Paso County, Drainage Criteria Manual, 1987.

1.4.2 All applicable Air Force regulations.

PART 2

ANALYSIS CRITERIA AND METHODS

2

2.1 General:

The City of Colorado Springs and El Paso County have developed a Drainage Criteria Manual which presents analysis criteria and methods appropriate for use by Peterson Air Force Base. That manual is generally the basis of all storm water analysis presented in this report. The City of Colorado Springs will be supplied with copies of all phases of this report. Final review and approval of this report will not be made by the City, although it is technically in their jurisdiction. Air Force personnel are solely responsible for internal drainage issues. The City of Colorado Springs comments, suggestions, and guidance are always welcome.

2.2 Storm Water Runoff:

The general approach to determining the storm water runoff for Peterson AFB is first to identify drainage patterns, organize the site into drainage areas, determine the hydraulic properties of each drainage area, and develop computer models which describes the behavior of storm water. For this site the existing drainage areas are organized according to the underground storm sewer collector to which it contributes. The main exception to this rule is when a storm sewer diverts flow from the natural surface drainage pattern and it is known that the culvert will not receive or convey a significant percentage of the flow generated by that drainage area.

The hydraulic properties of the site are determined by first considering the type of soil on the site, the type and condition of vegetation covering the site, the percent of the site with impervious cover, the slope of the surface, and the storm water collection system. All of these variables are subject to some judgment and no two hydrologists will reach exactly the same conclusions.

Runoff can be modeled by two methods: the Rational Method or the Soil Conservation Service (SCS) Hydrograph Method. The rational method is appropriate for drainage areas of less than 100 acres and is easily performed by hand calculations. The hydrograph method is appropriate for large areas and requires computer analysis. It is determined that the hydrograph method should be used for this site due to the large basin sizes and the flexibility of computer analysis. The Drainage Criteria Manual has no preferences as to the computer program used to generate storm water runoff from the SCS Type IIA, 24-hour hydrograph. The Army Corps of Engineers HEC-1 program is acceptable and is used in this report. HEC-1 is powerful, flexible and is completely appropriate for this site.

Two storm reoccurrence frequencies are recommended by the Drainage Criteria Manual; the 10-year and 100-year intervals. The storm sewer system should be capable of conveying the 10-year rainfall. The 100-year runoff should be considered in the storm sewer system design; however, a system capable of conveying a 100-year storm would be expensive and generally not cost effective. A well designed system will adequately convey frequent storms without disrupting normal activities or resulting in damage. Low

reoccurrence frequency storms will result in some flooding, and minor damage should be tolerated.

2.3 Storm Sewers and Hydraulic Structures:

Storm sewers, drop structures and other structures are designed based on the criteria provided in the drainage manual. Storm sewers are intended to function at capacity for the 10-year storm. This means the culvert will be flowing full with maximum depth in the inlets and manholes. Rainfall exceeding the 10-year event will flow on the surface.

2.4 Roads and Inlets:

The size and spacing of inlets is to be determined using the Drainage Criteria Manual. The intent is to provide a system which allows normal traffic patterns during minor storms and allows access of emergency vehicles during major events. These criteria should apply to both new systems and improvements to existing storm sewers.

PART 3

EXISTING CONDITIONS

3

3.1 General:

The study area encompasses approximately 1,000 acres of mostly developed land. The slope of the site is generally to the south at approximately 1 1/2 percent. The natural soil type is SCS Type A, Blakeland Sandy Loam, which is highly porous. Vegetation cover is generally good. There are no natural drainage features on the site, although Sand Creek passes along the northwest corner. The area in the vicinity of the creek slopes to the west.

3.2 Existing Collector System:

The existing storm drain system can be divided into seven main collectors. They are:

- 3.2.1 Main line in Hamilton Avenue. This line ties most of the onsite storm sewers to a swale which discharges into the recreational pond at the southern most limits of the study area. The storm sewer is 72" from the discharge headwall to Peterson Boulevard. Between Peterson Boulevard and Otis Street the pipe diameter decreases in stages to a final diameter of 24". Either directly or indirectly drainage areas A, B, C, D, E, and F contribute to this storm sewer. (Refer to map in the Appendix).
- 3.2.2 A 36" collector runs up Mitchell Street from the 72" main line in Hamilton Avenue to Stewart Avenue. It continues north in Mitchell Street as a 21" line which collects storm water from the family housing area. A second 36" line branches west in Stewart Avenue and collects additional runoff from family housing to the north. Drainage area B is the main source of runoff for this storm sewer.
- 3.2.3 A major collector ties to the 72" main line in Hamilton Avenue and runs north along Peterson Boulevard to almost Paine Street. The line is tied to a secondary network of storm sewers and inlets which collect runoff from a large area west of Peterson Boulevard. The line diameter is 48" at Hamilton Avenue and decreases in stages to a final 18" diameter. Drainage Area E contributes to this storm sewer.
- 3.2.4 A 21" storm sewer extends north along Otis Street from Hamilton Avenue to approximately Ent Avenue. From there it branches into a system of minor roof and parking lot drains. Much of the flow in this storm sewer comes from drainage Area F. Some flow is diverted from drainage Area D.
- 3.2.5 Space Command Headquarters has a 48" storm sewer system which collects flow in the vicinity of the building and conveys it west to Sand Creek. Drainage Area H is the main contributor to this storm sewer.

- 3.2.6 A storm sewer system in the area near the west entrance to the base collects flow from a large area west of Peterson Boulevard and generally north of Paine Street. The system varies in size but discharges to Sand Creek as a 54" pipe. This storm sewer conveys storm water from Drainage Area G.
- 3.2.7 A 30" storm sewer extends west from the intersection of Hamilton Avenue and Paine Street. This line discharges into a swale which discharges into Sand Creek. Drainage Area F is the main source of storm water for this storm sewer.

Numerous minor culverts and storm sewers exist onsite which collect roof and surface runoff. Some are tied to the above mentioned storm sewer collectors while others daylight and surface flow to an inlet or other collection structure.

3.3 Major Drainage Areas:

The study area has been divided into nine existing major drainage areas: one for each of the seven main collectors and two which contribute directly to detention pond #3. The drainage areas are:

- 3.3.1 Drainage Area A consists mainly of the golf course located at the south end of the Base. A large pond in the center of the basin receives much of the runoff. A 36" pipe at Kincheloe Loop ties this basin to the 72" Hamilton Avenue Main Collector. The vegetation cover is good and very little impervious cover exists. Calculations indicate the runoff from this area to be 32 cfs and 87 cfs for the 10-year and 100-year events, respectively. These numbers ignore the detention affects of the existing pond and other depressions. Considering this the actual runoff from Drainage Area A is probably much less.
- 3.3.2 Drainage Area B is the largest of all the drainage areas encompassing almost all of the family housing area and a large area north of the Family Housing Area to State Highway 94. All this drainage flows into the Mitchell Street Collector. The storm water runoff from this 292 acre area is relatively modest at 73 cfs and 213 cfs for the 10-year and 100-year rainfalls respectively. This is mainly due to good vegetation cover, Type A soil north of the family housing area and low impervious cover. Planned development in the area north of family housing and south of State Highway 94 will significantly increase runoff.
- 3.3.3 Drainage Area C is small at 14 acres. Minor culverts tie the area to both the Mitchell Street and Hamilton Avenue Collectors. However, the majority of the 37 cfs/63 cfs runoff surface flows to a sump area south of Hamilton Avenue.
- 3.3.4 Drainage Area D consists of all areas which flow directly into the Hamilton Avenue Collector west of Mitchell Street. The basin encompasses 136 acres of mostly developed land. There is some overlap between these drainage areas and other collectors: however, their diversion is assumed minimal. The calculated runoff is 90 cfs and 207 cfs for the 10-year and 100-year events.
- 3.3.5 Drainage Area E contributes to the Peterson Boulevard Collector. This area is 80 acres of developed land with a high percentage of impervious cover. As a result, the runoff is high at 152 cfs and 277 cfs for the 10-year and 100-year

storms. The area is covered with a network of secondary storm sewers which collect roof and surface runoff.

- 3.3.6 Drainage Area F is unusual in that four different collectors intercept some flow from the basin, however, none to a degree which affects the general surface flow patterns. Field investigations indicate the majority of the flow enters the Hamilton Avenue Collector near Paine Street. The basin size is approximately 57 acres. Storm water runoff is calculated to be 63 cfs and 134 cfs for the 10-year and 100-year events. Significant development opportunities exist in this basin. Future development will significantly increase flows and should be anticipated with drainage improvements.
- 3.3.7 Drainage Area G consists of 197 acres mostly west of Peterson Boulevard and north of Paine Street. The basin flows into the 54" collector to Sand Creek. The area is generally not developed with a relatively low percent impervious cover. The calculated flows are 102 cfs and 257 cfs for the 10-year and 100-year events, respectively. Future development in this basin will increase flows significantly.
- 3.3.8 Drainage Area H encompasses Space Command Headquarters and flows into a 48" storm sewer to Sand Creek. This area is 51 acres with a modest percent impervious cover. Storm water runoff is 64 cfs and 133 cfs for the 10-year and 100-year events, respectively. No further development is anticipated in this drainage area.
- 3.3.9 Drainage Area I consists of the golf course, shooting range and an undeveloped area. Impervious cover is very low. This area surface flows to a sump inlet which discharges directly into City Detention Pond # 11. Calculated runoff is very low at 29 cfs and 90 cfs. Little future development is anticipated.

3.4 Locations of Special Concern

Throughout Peterson Air Force Base there are localized areas which exhibit frequent flooding. These areas are numerous with existing conditions; however, considerable relief of this flooding will be realized by the major drainage system improvements presented in this report.

3.5 Analysis of Existing Storm Sewer System:

In general, the storm sewer system is not capable of conveying the 10-year event. Flows were calculated based on existing conditions and compared with the capacity of the existing collectors. Those findings are presented in Table 1. No effort was made to confirm the adequacy of the existing inlets to divert surface flow to the collectors.

3.6 Analysis of Detention Ponds

City Detention Pond #11 is the only existing detention pond which is designed to accept flow from the study area. That pond has been analyzed in previous reports and found

to have adequate capacity. It is not analyzed in detail in this report; however, it is included in the computer model. The intent of doing this is to provide an approximate water surface elevation which will indicate if further detailed analysis is warranted.

Incorporating local detention ponds into the future drainage system was not considered, due to the high value of the limited remaining space available for development.

3.7 Offsite Drainage Areas

There are no offsite drainage areas which contribute significant flow to the study area. There is a small area on the north side of State Highway 94 which flows into existing Drainage Area B. Runoff from this area is minor and is due to a low percent impervious cover and high infiltration rate.

TABLE 1 EXISTING MAJOR DRAINAGE COLLECTOR			
COLLECTOR	EXISTING CAPACITY (CFS)	EXISTING FLOWS (CFS) 10-YEAR	EXISTING FLOWS (CFS) 100-YEAR
Hamilton Avenue - Peterson to Mitchell - Mitchell to Det. Pond #3	250 310	262 316	536 662
Mitchell Street	60	73	213
Peterson Boulevard	130	152	277
Space Command 48"	125	64	133
Sand Creek 54"	220	102	257
Sand Creek 30"	70	63	134

PART 4

FUTURE DEVELOPMENT

4

4.1 General:

The study area is generally developed; however, opportunities exist for further development. The major area for development is the open area east of Space Command Headquarters, between State Highway 94 and the Family Housing area. This area encompasses approximately 100 acres. This area is now in a relatively natural state and runoff is light. Major drainage improvements will be required to protect existing facilities from increased flows resulting from the development of this area.

Additional development is also planned for a 20 acre area west of Peterson Boulevard and north of Paine Street. This area will also require storm sewer improvements when developed.

Numerous smaller areas onsite will also be developed. Computer models used in the analysis of the future sites are adjusted for maximum buildout.

PART 5

PROPOSED DRAINAGE IMPROVEMENTS

5

5.1 Proposed Major Drainage Areas:

The proposed drainage areas are delineated by generally the same boundaries as the existing drainage area. The main difference between the existing and proposed areas is that additional basins were created where key flows were needed. These key flows were necessary to size diversions which convey flow from the existing storm sewer system or to confirm the capacity of the existing system. The proposed diversions are detailed in Section 5.2.

- 5.1.1 Drainage Area A consists of 47 acres of mainly golf course with little impervious cover. Vegetation cover is in good condition. A pond is located roughly in the center of the drainage area. The flow direction is to the southwest at 2 percent. Computer analysis indicates runoff from this area to be 15 cfs and 45 cfs for the 10-year and 100-year events respectively. These flows do not account for the detention provided by the pond and other depressions. The actual flows will probably be considerably less. No significant future development is anticipated in this area.
- 5.1.2 Drainage Area B is 40 acres of mostly open space. Included is a portion of the family housing area and part of the shooting range. Some building and road improvements are expected in the area. Flow is to the west at approximately 1 percent. The calculated flows from this basin are 12 cfs and 38 cfs for the 10-year and 100-year events respectively.
- 5.1.3 Drainage Area C encompasses 147 acres of mostly family housing. No further development is anticipated in this area. The surface flow is to the south at 1.2 percent. The calculated flows from this area are 145 cfs and 316 cfs for the 10-year and 100-year storms. Flow from this area will be collected in an improved Stewart Avenue storm sewer and diverted east to a new swale.
- 5.1.4 Drainage Area D is relatively small with 28 acres. Future land use indicates the area will be administrative, community commercial, community services, and housing. A high impervious cover is assumed. All flow from this basin enters the Mitchell Street Collector. The calculated flows will be 75 cfs and 126 cfs for the 10-year and 100-year storms.
- 5.1.5 Drainage Area E is very small at 14 acres of mostly administrative use. The open space in the basin is assumed to be fully developed. Impervious cover will be high. Flow is to the south at 1 1/2 percent.

This basin contributes to both the Mitchell Street and Hamilton Avenue Collector. The total calculated flow is 38 cfs and 63 cfs for the 10-year and 100-year events.

- 5.1.6 Drainage Area F covers 121 acres which will be fully developed. The land use categories included are administrative, industrial, community commercial, aircraft O&M, and outdoor recreation. The majority of storm water from this area flows south to the Hamilton Avenue Collector. The flows are 63 cfs and 184 cfs for the 10-year and 100-year storms.
- 5.1.7 Drainage Area G encompasses 34 acres of medical, community commercial, community services, and administrative land use. The area is now fully developed and no significant changes in cover are anticipated. The direction of flow is to the south at approximately 1 1/2 percent. All the runoff from this area goes into the Peterson Boulevard Collector system. The calculated flows are 91 cfs and 151 cfs for the 10-year and 100-year events.
- 5.1.8 Drainage Area H is 48 acres of fully developed land. Land use is administrative, community commercial, and community services. No additional development is anticipated. The entire drainage area now flows into the Peterson Boulevard collector. This drainage area was added to define the flow converging at Peterson Boulevard and Stewart Avenue. That intersection is a convenient location to construct a diversion storm sewer in Stewart Avenue which will convey flow from the overloaded Peterson Boulevard and Hamilton Avenue Collectors. The calculated flows are 124 cfs and 204 cfs for the 10-year and 100-year events.
- 5.1.9 Drainage Area I covers 52 acres of industrial, open space, administrative, community commercial and community services. The majority of flow from this area goes to the 30" storm sewer to Sand Creek however some flow is diverted to the Otis Street Collector and to Sand Creek in the 54" Collector. There are opportunities for development in this drainage area. It is considered fully developed in the flow rate calculations. The 10-year and 100-year flows are 136 cfs and 227 cfs.
- 5.1.10 Drainage Area J is large at 105 acres. Land use will be outdoor recreation, industrial, community services, and community commercial. All storm water runoff from this drainage area enters the 54" collector which flows directly to Sand Creek. Some future development will be made. The calculated flow rates are 161 cfs and 325 cfs for the 10-year and 100-year storms.
- 5.1.11 Drainage Area K encompasses 31 acres. The land use will be mostly special space missions with some community commercial. The drainage area was added because future development will require a storm sewer system to tie into. Diverting flow from this area to Sand Creek will help

reduce the load on down stream collectors. The calculated flow rates are 83 cfs and 138 cfs for the 10-year and 100-year events.

- 5.1.12 Drainage Area L is 53 acres of administrative land. No further development is anticipated. The impervious cover is moderate with considerable open space. All the storm water runoff from this area flows to a 48" collector to Sand Creek. No other drainage areas contribute significant flow to this culvert. The calculated flows are 74 cfs and 151 cfs for the 10-year and 100-year storms.
- 5.1.13 Drainage Area M encompasses 62 acres of land dedicated for administrative use. The area is open space at present so considerable development will occur. This basin slopes to the south at approximately 2 percent. At present this area sheet flows south across the north boundary of the existing family housing. The extensive development anticipated will require a storm sewer system. It is recommended a diversion storm sewer be constructed to convey flow from this area through family housing to a new swale. The flow rates are 160 cfs and 270 cfs for the 10-year and 100-year events.
- 5.1.14 Drainage Area N is a long thin drainage area along the east boundary of the study area. The area is now open space and is expected to remain so. Paine Street will ultimately be extended to the north end of this area. It is not known how much it will affect storm water runoff in the area. All the flow from this site will be collected into a swale which runs from the southeast corner of Drainage Area M to City Detention Pond # 11. The calculated flows are 21 cfs and 74 cfs for the 10-year and 100-year storms.
- 5.1.15 Drainage Area O is 117 acres of land reserved for outdoor recreation. Vegetation cover is good and very little impervious cover exists. The flow direction is to the south at an average slope of 2 percent. A sump inlet into City Detention Pond #11 receives the runoff. No further development is anticipated in this drainage area. The calculated flows are 34 cfs and 108 cfs for the 10-year and 100-year storms.
- 5.1.16 Drainage Area P is approximately 17 acres of land mostly dedicated for highway use with some commercial zoning. At present, most of this area flows into a detention area created by State Highway 94. When development occurs in this area it is assumed a culvert will be constructed under the highway which will allow flow to impact the site. It is recommended that a 48" storm sewer be constructed along the north Peterson property line to intercept this flow. Calculations indicate the flow rates to be 2 and 14 for the 5-year and 100-year events.
- 5.1.17 Drainage Area Q is a 100 acre offsite flow which combines with Drainage Area P at the north property line. At present, the area discharges very little flow; however, once development occurs the runoff will be significant, 216 cfs and 372 cfs. It is recommended that a 60" storm sewer be constructed to intercept this flow and divert it to the new

swale on the east side of family housing.

5.2 Major New Drainage Improvements:

The existing storm sewer system is undersized for existing conditions based on the 10-year storm. Future development will increase drainage problems on site. To help eliminate the need to perform expensive replacement of undersized existing collectors it is recommended that where possible storm water be diverted away from these collectors. The following new drainage systems are recommended:

- 5.2.1 The East Swale is a swale to be constructed from the northeast corner of the Family Housing Area to City Detention Pond # 11. The swale would collect and divert flow away from the existing undersized storm sewer system. The swale should be grass lined and designed with a slope gradual enough to prevent erosion during minor storm events. Drop structures consisting of a concrete runoff wall and extensive riprap will be required at intervals varying with the slope of the surface. Drainage areas C, H, M and N contribute to this swale.
- 5.2.2 The North 60" Storm Sewer is a 60" RCP to be constructed from the north side of the Family Housing Area to the East Swale. Temporary swales would be constructed along the north side of the family housing area to divert flow into the 60" pipe. The temporary swales could be replaced by culverts and inlets when the area is further developed. Drainage Area M contributes to this storm sewer.
- 5.2.3 The East 72" Storm Sewer is necessary to lessen the required improvements to the Mitchell Street Collector and Hamilton Avenue Collector. A 72" RCP should be constructed from Mitchell Street at Stewart Avenue east to the new swale east of the golf course. This line, in conjunction with the new north 60" storm sewer, would reduce the flow to the Mitchell Street Collector to its existing capacity. Drainage Areas H and C contribute to this storm sewer.
- 5.2.4 The Sand Creek 48" storm sewer should extend from Sand Creek at the west entrance east to Peterson Boulevard. Development west of Peterson Boulevard and north of Paine Street will be tied to this line. Drainage Area K contributes to this storm sewer.
- 5.2.5 The Stewart Avenue 54" storm sewer is required to relieve the undersized Peterson Boulevard Collector. Rather than replacing the existing Peterson Boulevard Collector it would be preferable to extend the new 72" culvert mentioned in paragraph 5.2.3 at Stewart Avenue and Mitchell Street along Stewart Avenue to Peterson Boulevard. This extension should be 54" diameter. The flow in the 42" storm sewer in Peterson Boulevard could then be diverted east relieving the load on the Peterson Boulevard and Hamilton Avenue Collectors. Drainage Area H contributes to this storm sewer.

5.2.6 Northeast 60" diversion is a 60" storm sewer which will collect offside flows entering the north property line east of Space Command Headquarters. This storm sewer should start approximately 1,500 feet east of Peterson Boulevard and extend east 1,200 feet to the existing fence line. At the fence it will run south approximately 3,000 feet where it will discharge into the proposed East Swale. Drainage Areas P and Q contributed to this culvert.

5.3 Major Existing Drainage Structure Improvements:

The proposed new storm sewers and swale will divert enough flow away from the existing system that no major reconstruction will be required for the existing system. Minor improvements such as inlet replacements will still be required. See Table 2 for a summary of the Flowrates after the Proposed Drainage Improvements.

**TABLE 2
FUTURE MAJOR DRAINAGE COLLECTORS**

COLLECTOR	CAPACITY (CFS)	FUTURE FLOWS 10-YEAR	FUTURE FLOWS 100-YEAR
Hamilton Avenue - Peterson to Mitchell - Mitchell to Det. Pond #3	250 310	154 290	335 602
Mitchell Street	60	86	161
Peterson Boulevard	130	91	151
Space Command	125	74	151
Sand Creek 54"	220	161	325
Sand Creek 30"	70	136	227
East Swale (15', 3:1, S=0.0025)	1,200	647	1,180
New North 60"	190	160	270
New East 72"	300	269	534
New Sand Creek 48"	110	83	138
New Stewart Avenue 54"	140	124	207
New Northeast 60"	190	218	387

PART 6

PHASING OF IMPROVEMENTS

1. Improve inlets in Peterson Boulevard.
2. Improve inlets in Mitchell Street.
3. Improve inlets and ditch along Hamilton Boulevard.
4. Construct East Swale from City Detention Pond #11 to the East 72".
5. Construct the East 72", Stewart Avenue 54" and Stewart Avenue 48" Storm Sewers. Improve inlets in Stewart. Tie the Stewart Avenue 48" to existing Peterson Boulevard 42" storm sewer.
6. Extend the East Swale from the East 72" to a point approximately 1,100 feet north of family housing. Much of this swale will be temporary and will be replaced by the Northeast 60" storm sewer.
7. Construct the 60" Family Housing storm sewer and the 60" Northeast storm sewer. Both of these lines will be constructed prior to development of Drainage Area M. However, prior to development, the temporary portion of the East Swale can divert much of the flow from Family Housing. Area development of the west portion of Drainage Area O north of State Highway 94 may require construction of the Northeast 60" prior to construction of the Family Housing 60" line.
8. Construction of the 48" Sand Creek Line should be coordinated with development west of Peterson Boulevard and north of Pain Street.

PART 7
SUMMARY

5

7.1 General:

The storm sewer system in the study area can be improved to adequately convey the 10-year storm by the construction of new storm sewers and swales to divert storm water runoff from existing undersized storm sewers. By diverting flows away from developed areas, removal and replacement of existing storm sewers can be minimized which will minimize cost and disruption of normal base operations.

PART 8

REFERENCES

7

- 1) Base Comprehensive Plan, Phase I, Peterson Air Force Base, Colorado Springs, Colorado, December, 1990
- 2) Drainage Criteria Manual, City of Colorado Springs / El Paso County, October, 1987
- 3) Peterson Field Drainage Basin Master Plan Update, City of Colorado Springs, Colorado, URS, August, 1984

APPENDIX

GENERAL INFORMATION

TABLE 5-7
 RUNOFF CURVE NUMBERS
 FOR HYDROLOGIC SOIL-COVER COMPLEXES
 URBAN AND SUBURBAN CONDITIONS 1/
 (For Antecedent Moisture Condition III)
 (From: U.S. Department of Agriculture,
 Soil Conservation Service, 1977)

**NOTE: THIS TABLE TO
 BE USED FOR 2-HOUR
 STORM ONLY.**

<u>Land Use</u>	<u>Hydrologic Soil Group</u>			
	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>
Open spaces, lawns, parks, golf courses, cemeteries, etc.				
Good condition: grass cover on 75% or more of the area	59*	78	88	91
Fair condition: grass cover on 50% to 75% of the area	69*	84	91	93
Commercial and business areas (85% impervious)	96*	97	98	98
Industrial districts (72% impervious)	92*	95	97	98
Residential: <u>2/</u>				
<u>Acres per Dwelling Unit</u>	<u>Average %</u>			
	<u>impervious</u> ^{3/}			
1/8 acre or less	65	89*	94	96
1/4 acre	38	78*	88	93
1/3 acre	30	75*	86	92
1/2 acre	25	73*	85	91
1 acre	20	70*	84	91
Paved parking lots, roofs, driveways, etc.	99	99	99	99
Streets and roads:				
paved with curbs and storm sewers	99	99	99	99
gravel	89*	94	96	97
dirt	86*	92	95	96

1/ For a more detailed description of agricultural land use curve numbers, refer to in the National Engineering Handbook (U.S. Dept. of Agriculture, Soil Conservation Service, 1972).

2/ Curve numbers are computed assuming the runoff from the house and driveway is directed towards the street with a minimum of roof water directed to lawns where additional infiltration could occur.

3/ The remaining pervious areas (lawn) are considered to be in good pasture condition for these curve numbers.

* Not to be used wherever overlot grading or filling is to occur.

TABLE 5-6
 RUNOFF CURVE NUMBERS FOR HYDROLOGIC
 SOIL-COVER COMPLEXES--RURAL CONDITIONS
 (Antecedent Moisture Condition III, and $I_a = 0.2 S$)
 (From: U.S. Dept. of Agriculture,
 Soil Conservation Service, 1977)

NOTE: THIS TABLE TO
 BE USED FOR 2-HOUR
 STORM ONLY.

Land Use	Cover Treatment or Practice	Hydrologic Condition	Runoff curve number by Hydrologic soil group			
			A	B	C	D
Fallow	Straight Row	----	89	94	97	98
Row crops	Straight Row	Poor	86	92	95	97
	Straight Row	Good	83	90	94	96
	Contoured	Poor	85	91	93	95
	Contoured	Good	82	88	92	94
	Cont. and terraced	Poor	82	88	91	92
	Cont. and terraced	Good	79	86	90	92
Small grain	Straight Row	Poor	82	89	93	95
		Good	80	88	93	95
	Contoured	Poor	80	88	92	94
		Good	78	87	92	93
	Cont. and terraced	Poor	78	86	91	92
		Good	77	85	90	92
Close-seeded legumes <u>1/</u> or rotation meadow	Straight Row	Poor	82	89	94	96
		Good	76	86	92	94
	Contoured	Poor	81	88	93	94
		Good	74	84	90	93
	Cont. and terraced	Poor	80	87	91	93
		Good	70	83	89	91
Pasture or range		Poor	84	91	94	96
		Fair	69	84	91	93
		Good	59	78	88	91
	Contoured	Poor	67	83	92	95
		Fair	64	77	88	93
		Good	15	55	85	91
Meadow		Good	50	76	86	90
Woods		Poor	65	82	89	93
		Fair	56	78	87	91
		Good	43	74	85	89
Farmsteads		----	77	88	92	94
Roads (dirt) <u>2/</u> (hard surface) <u>2/</u>		----	86	92	95	96
		----	88	93	96	97

1/ Close-drilled or broadcast

2/ Including right-of-way

TABLE 5-5
 RUNOFF CURVE NUMBERS
 FOR HYDROLOGIC SOIL-COVER COMPLEXES
 URBAN AND SUBURBAN CONDITIONS 1/
 (For Antecedent Moisture Condition II)
 (From: U.S. Department of Agriculture,
 Soil Conservation Service, 1977)

NOTE: THIS TABLE TO
 BE USED FOR 24-HOUR
 STORM ONLY.

<u>Land Use</u>	<u>Hydrologic Soil Group</u>			
	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>
Open spaces, lawns, parks, golf courses, cemeteries, etc.				
Good condition: grass cover on 75% or more of the area	39*	61	74	80
Fair condition: grass cover on 50% to 75% of the area	49*	69	79	84
Commercial and business areas (85% impervious)	89*	92	94	95
Industrial districts 72% impervious)	81*	88	91	93
Residential: <u>2/</u>				
<u>Acres per Dwelling Unit</u>		<u>Average % impervious</u> ^{3/}		
1/8 acre or less	65	77*	85	90
1/4 acre	38	61*	75	83
1/3 acre	30	57*	72	81
1/2 acre	25	54*	70	80
1 acre	20	51*	68	79
Paved parking lots, roofs, driveways, etc.	98	98	98	98
Streets and roads:				
paved with curbs and storm sewers	98	98	98	98
gravel	76*	85	89	91
dirt	72*	82	87	89

1/ For a more detailed description of agricultural land use curve numbers, refer to in the National Engineering Handbook (U.S. Dept. of Agriculture, Soil Conservation Service, 1972).

2/ Curve numbers are computed assuming the runoff from the house and driveway is directed towards the street with a minimum of roof water directed to lawns where additional infiltration could occur.

3/ The remaining pervious areas (lawn) are considered to be in good pasture condition for these curve numbers.

* Not to be used wherever overlot grading or filling is to occur.

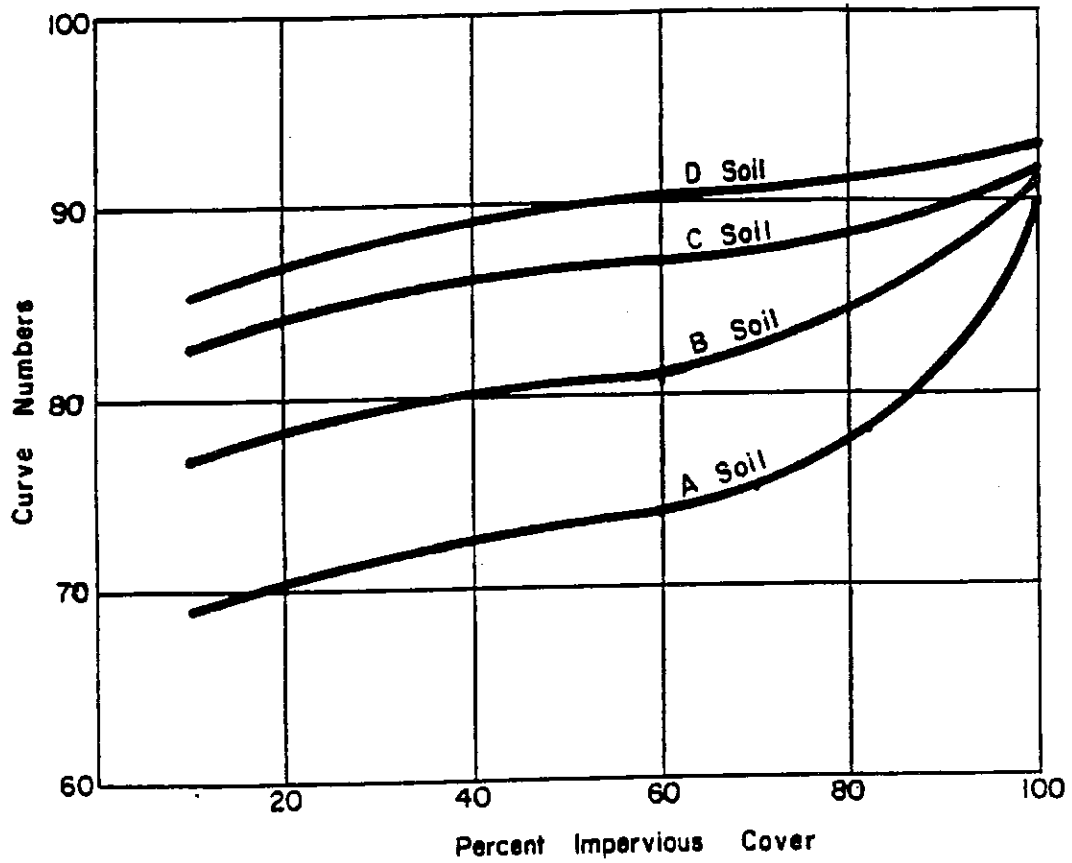
TABLE 5-4
 RUNOFF CURVE NUMBERS FOR HYDROLOGIC
 SOIL-COVER COMPLEXES--RURAL CONDITIONS
 (Antecedent Moisture Condition II, and $I_a = 0.2 S$)
 (From: U.S. Dept. of Agriculture,
 Soil Conservation Service, 1977)

NOTE: THIS TABLE TO
 BE USED FOR 24-HOUR
 STORM ONLY.

Land Use	Cover Treatment or Practice	Hydrologic Condition	Runoff curve number by Hydrologic soil group			
			A	B	C	D
Fallow	Straight Row	----	77	86	91	94
Row crops	Straight Row	Poor	72	81	88	91
	Straight Row	Good	67	78	85	89
	Contoured	Poor	70	79	84	88
	Contoured	Good	65	75	82	86
	Cont. and terraced	Poor	66	74	80	82
	Cont. and terraced	Good	62	71	78	81
Small grain	Straight Row	Poor	65	76	84	88
		Good	63	75	83	87
	Contoured	Poor	63	74	82	85
		Good	61	73	81	84
	Cont. and terraced	Poor	61	72	79	82
		Good	59	70	78	81
Close-seeded legumes <u>1/</u> or rotation meadow	Straight Row	Poor	66	77	85	89
		Good	58	72	81	85
	Contoured	Poor	64	75	83	85
		Good	55	69	78	83
	Cont. and terraced	Poor	63	73	80	83
		Good	51	67	76	80
Pasture or range		Poor	68	79	86	89
		Fair	49	69	79	84
		Good	39	61	74	80
	Contoured	Poor	47	67	81	88
		Fair	25	59	75	83
		Good	6	35	70	79
Meadow		Good	30	58	71	78
Woods		Poor	45	66	77	83
		Fair	36	60	73	79
		Good	25	55	70	77
Farmsteads		----	59	74	82	86
Roads (dirt) <u>2/</u> (hard surface) <u>2/</u>		----	72	82	87	89
		----	74	84	90	92

1/ Close-drilled or broadcast

2/ Including right-of-way



**URBAN HYDROLOGIC SOIL COVER COMPLEX
& ASSOCIATED CURVE NUMBERS**

REFERENCE : Pikes Peak Area Council of Governments Areawide Urban Runoff Control Manual



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Drainage Criteria Manual

Urban Hydrologic Soil Cover

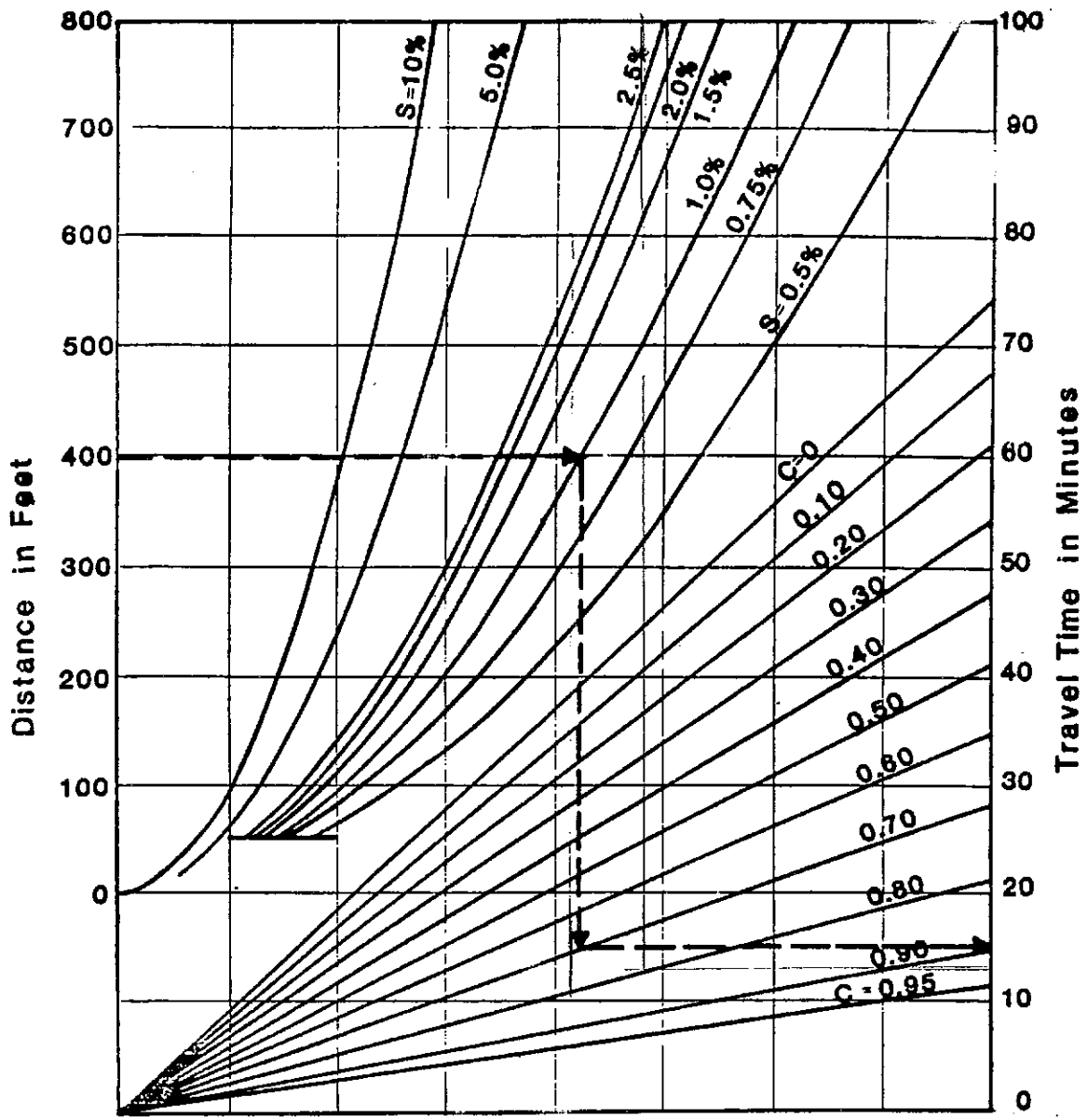
Complex and Associated Curve Numbers

Date

OCT. 1987

Figure

5-7



REFERENCE : Wright - McLaughlin Engineers, Urban Storm Drainage Criteria Manual, Vol. 1,
 Denver Regional Council of Governments, Denver, Co. 1977



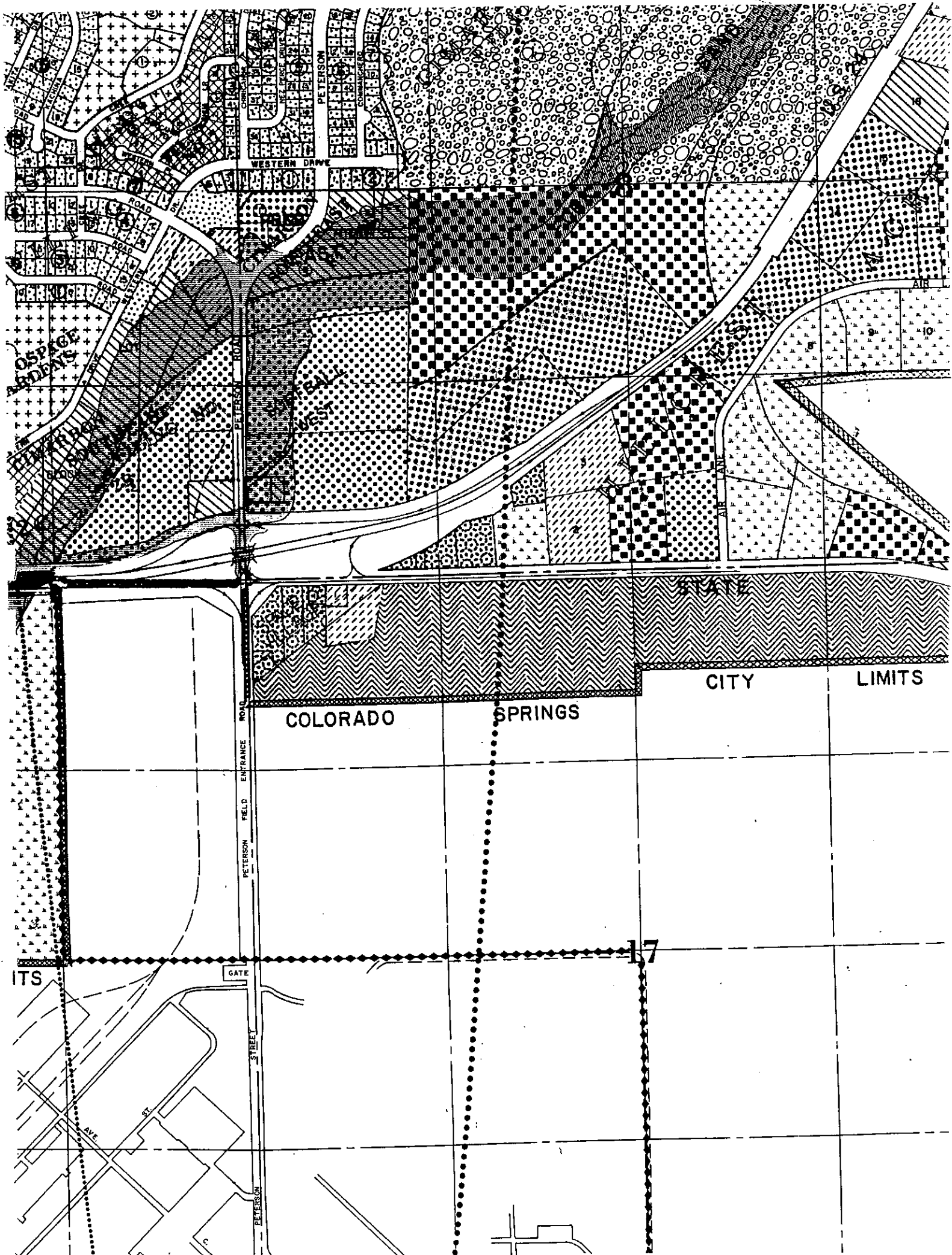
HDR Infrastructure, Inc.
 A Centerra Company

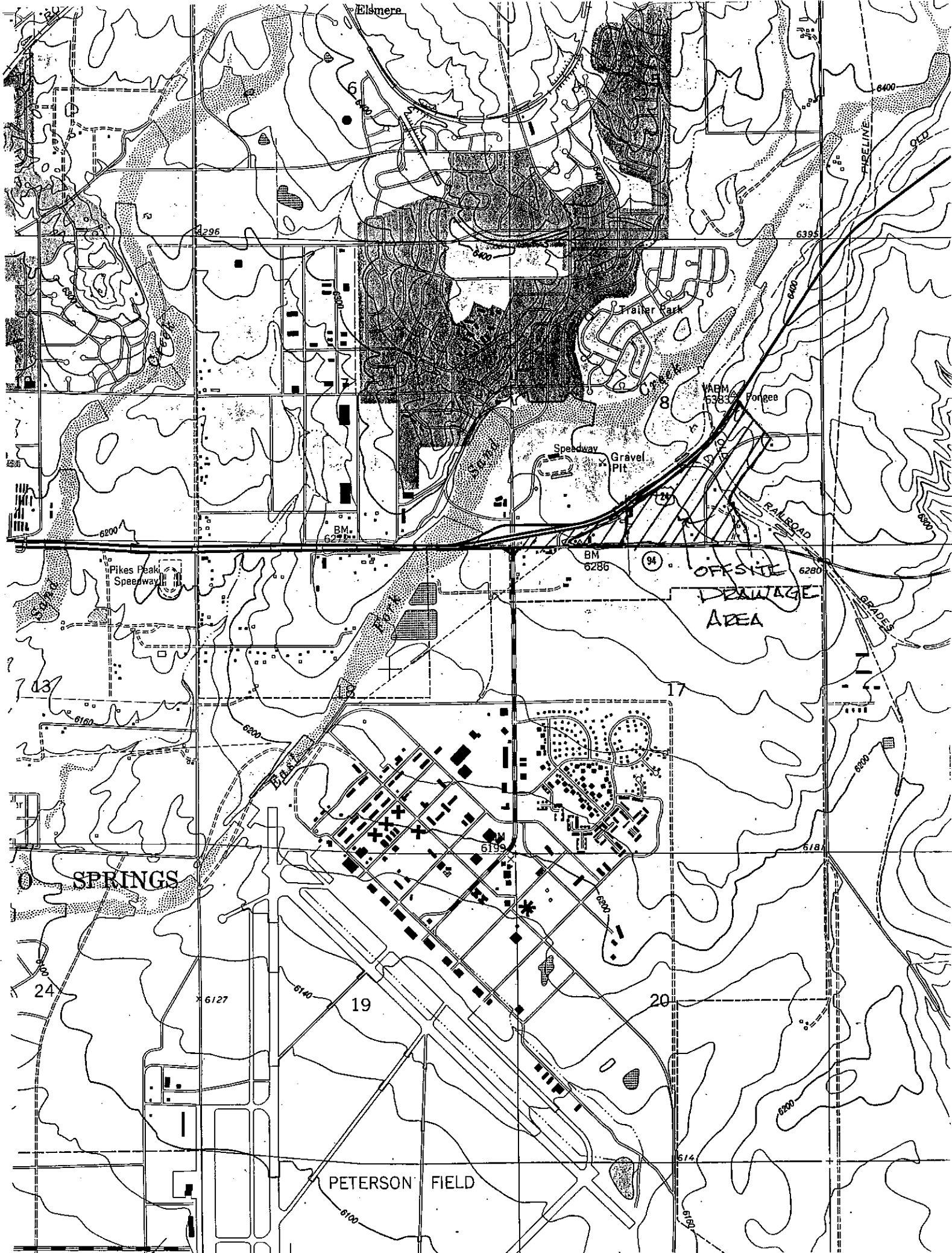
The City of Colorado Springs / El Paso County
 Drainage Criteria Manual

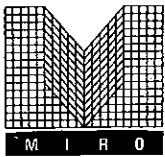
Overland Flow Curves

Date
OCT. 1987

Figure
5-2





Title PAFB DRAWAGE

Date _____

Job No. _____

RAINFALL INTENSITYBy RHS

Sheet _____

of _____

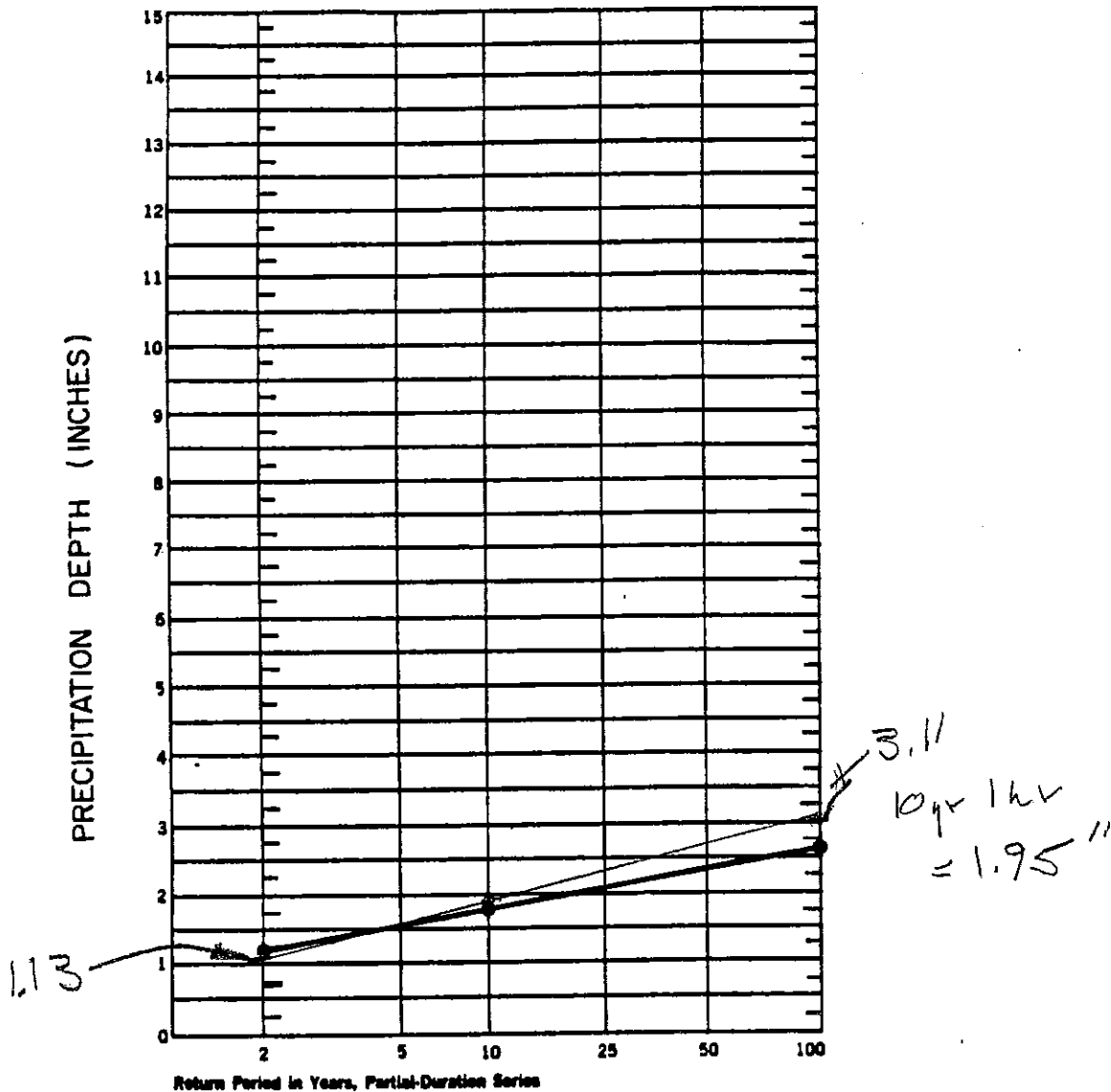
$$\begin{array}{lll} 1) & 2-4R & 6HR & X_1 = 1.6 \\ & 2-4R & 24HR & X_2 = 2.0 \\ & 100-4R & 6HR & X_3 = 3.6 \\ & 100HR & - 24HR & X_4 = 4.5 \end{array}$$

$$Z = 6.2$$

$$2) Y_2 = 0.218 + 0.709 [(1.6)(1.6/2.0)] = 1.13$$

v

$$\begin{aligned} 3) Y_{100} &= 1.897 + 0.439 [(3.6)(3.6/4.5)] \\ &\quad - 0.008 (6.2) = 3.11 \end{aligned}$$



EXAMPLE

2 yr. 1 hr rainfall (calculated) = 1.19"
 100 yr. 1 hr rainfall (calculated) = 2.64"
 10 yr. 1 hr rainfall (interpolated) = 1.78"

REFERENCE : NOAA Atlas 2, Volume 3 - Colorado

NOTE: This example is for Colorado Springs as indicated on the isopluvials.



HDR Infrastructure, Inc.
 A Centerra Company

The City of Colorado Springs / El Paso County
 Drainage Criteria Manual

RAINFALL DEPTH - DURATION RELATIONSHIP

Date	OCT. 1987
Figure	5 - 6

EXISTING CONDITION HEC-1 OUTPUT

*FIX
 DIAGRAM
 PETERSON AIR FORCE BASE, COLORADO SPRINGS, CO
 ID HEC1 INPUT FILE PAFBFIX.HC1
 ID 10 AND 100-YEAR EVENTS - 24 HOUR DURATION - TYPE IIA
 15 25JAN92 0 100
 4 1
 IN 15 25JAN92 0
 JR PREC .67 1.0

H SPACE COMMAND DRAINAGE AREA AT NORTH CENTER
 KO 21 60
 BA .0799
 LS 4.5
 UD 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120 0.0143
 PC0.0165 0.0188 0.0210 0.0233 0.0255 0.0278 0.0320 0.0390 0.0460 0.0530
 UD 0.0600 0.0750 0.1000 0.4000 0.7000 0.7250 0.7500 0.7650 0.7800 0.7900
 UD 0.8000 0.8100 0.8200 0.8250 0.8300 0.8350 0.8400 0.8450 0.8500 0.8550
 PC0.8600 0.8638 0.8675 0.8713 0.8750 0.8788 0.8825 0.8863 0.8900 0.8938
 PC0.8975 0.9013 0.9050 0.9083 0.9115 0.9148 0.9180 0.9210 0.9240 0.9270
 UD 0.9300 0.9325 0.9350 0.9375 0.9400 0.9425 0.9450 0.9475 0.9500 0.9525
 UD 0.9550 0.9575 0.9600 0.9625 0.9650 0.9675 0.9700 0.9725 0.9750 0.9775
 PC0.9800 0.9813 0.9825 0.9838 0.9850 0.9863 0.9875 0.9888 0.9900 0.9913
 PC0.9925 0.9938 0.9950 0.9963 0.9975 0.9988 1.0000
 UD 0 80
 UD 0.19

G DRAINAGE AREA AT NORTHWEST CORNER
 KO 21 60
 BA .3085
 LS 0 72
 UD 0.38

F CENTRAL DRAINAGE AREA TO WEST END OF HAMILTON
 KO 21 60
 BA .0889
 UD 0 80
 UD 0.22

E CENTRAL AREA TO PETERSON BLVD
 KO 21 60
 BA .1257
 UD 0 87
 UD 0.19

D AREA WHICH FLOWS DIRECTLY INTO HAMILTON
 KO 21 60
 BA .2121
 LS 0 76
 UD 0.41

DEF COMBINE AREAS D E AND F AT PETERSON AND HAMILTON
 HC 3

B-1 OFFSITE NORTH OF 94 AND SOUTH OF U.S. 24
 BA 0.125
 LS 0 30
 UD .33

B EAST AREA WHICH INCLUDES MOST OF FAMILY HOUSING AND AREAS TO THE NORTH
 KO 21 60
 BA .4568
 LS 0 68
 UD 0.65

B-TOT COMBINED OFFSITE AND ONSITE AT B

*FIX 003
 *DIAGRAM 002
 ID 036
 ID 036
 ID 036
 IT 040
 IO 039
 IN 038
 JR 043
 * 001
 KK 045
 KO 047
 BA 008
 PB 069
 PC 070
 PC 070
 PC 070
 PC 070
 PC 070
 PC 070
 PC 070
 PC 070
 PC 070
 PC 070
 PC 070
 PC 070
 PC 070
 PC 070
 PC 070
 PC 070
 LS 056
 UD 112
 * 001
 KK 045
 KO 047
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 KO 047
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 KO 047
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 KO 047
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 HC 030
 * 001
 KK 045
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 KO 047
 BA 008
 LS 056
 UD 112
 * 001
 KK 045

HC 2
 C SMALL AREA ON MITCHELL
 BA.02270
 LS 0 90
 0.08
 KK BC COMBINE DRAINAGE AREAS B AND C AT HAMILTON AND MICHELL
 HC 2
 BCDE COMBINE DRAINAGE AREAS BC AND DE AT HAMILTON AND MICHELL
 HC 2
 A WEST SIDE OF GOLF COURSE
 BA .0740
 LS 0 68
 0.11
 KK DEBCA COMBINE DRAINAGE AREAS DEBC AND A NEAR MICHELL
 HC 2
 I EAST SIDE OF GOLF COURSE AND SOME OFFSITE
 BA .2561
 LS 0 65
 0.72
 KKDEBCA1 COMBINE DRAINAGE AREAS DEBCA AND I AT DETENTION POND #2
 HC 2
 D1 DETENTION VOLUME REQUIRED
 21 60
 DETENTION BASIN #1

RS	1	ELEV	6110.5				
SA	.1	4.14	5.82	6.47	7.84	9.17	10.55
	6110.4	6111	6113	6115	6120	6125	6130
	1	4	20	30	34	36	40
SE	6110.4	6111	6113	6115	6120	6125	6130

 *
 Z

HC 030
 * 001
 KK 045
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 HC 030
 * 001
 KK 045
 HC 030
 * 001
 KK 045
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 HC 030
 * 001
 * 001
 KK 045
 KO 047
 KM 046
 RS 092
 SA 096
 SE 099
 SQ 104
 SE 099
 * 001
 ZZ 127


```
*****  
*  
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *  
* SEPTMBER 1990 *  
* VERSION 4.0 *  
*  
* RUN DATE 03/25/1992 TIME 14:32:08 *  
*  
*****
```

```
*****  
*  
* U.S. ARMY CORPS OF ENGINEERS *  
* HYDROLOGIC ENGINEERING CENTER *  
* 609 SECOND STREET *  
* DAVIS, CALIFORNIA 95616 *  
* (916) 756-1104 *  
*  
*****
```

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X X XXXXXXX XXXXX X  
X X X X X XX  
X X X X X  
XXXXXXX XXXX X XXXXX X  
X X X X X  
X X X X X  
X X XXXXXXX XXXXX XXX
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:::::  
:::::  
:::  
::: Full Microcomputer Implementation :::  
::: by :::  
::: Haestad Methods, Inc. :::  
:::  
:::::  
:::::
```

37 Brookside Road * Waterbury, Connecticut 06708 * (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, .
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*** FIX ***

*DIAGRAM

1 ID PETERSON AIR FORCE BASE, COLORADO SPRINGS, CO
 2 ID HEC1 INPUT FILE PAFBFIX.HC1
 3 ID 10 AND 100-YEAR EVENTS - 24 HOUR DURATION - TYPE IIA
 4 IT 15 25JAN92 0 100
 5 IO 4 1
 6 IN 15 25JAN92 0
 7 JR PREC .67 1.0

*

8 KK H SPACE COMMAND DRAINAGE AREA AT NORTH CENTER
 9 KO 21 60
 10 BA .0799
 11 PB 4.5
 12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120 0.0143
 13 PC 0.0165 0.0188 0.0210 0.0233 0.0255 0.0278 0.0320 0.0390 0.0460 0.0530
 14 PC 0.0600 0.0750 0.1000 0.4000 0.7000 0.7250 0.7500 0.7650 0.7800 0.7900
 15 PC 0.8000 0.8100 0.8200 0.8250 0.8300 0.8350 0.8400 0.8450 0.8500 0.8550
 16 PC 0.8600 0.8638 0.8675 0.8713 0.8750 0.8788 0.8825 0.8863 0.8900 0.8938
 17 PC 0.8975 0.9013 0.9050 0.9083 0.9115 0.9148 0.9180 0.9210 0.9240 0.9270
 18 PC 0.9300 0.9325 0.9350 0.9375 0.9400 0.9425 0.9450 0.9475 0.9500 0.9525
 19 PC 0.9550 0.9575 0.9600 0.9625 0.9650 0.9675 0.9700 0.9725 0.9750 0.9775
 20 PC 0.9800 0.9813 0.9825 0.9838 0.9850 0.9863 0.9875 0.9888 0.9900 0.9913
 21 PC 0.9925 0.9938 0.9950 0.9963 0.9975 0.9988 1.0000

22 LS 0 80
 23 UD 0.19

*

24 KK G DRAINAGE AREA AT NORTHWEST CORNER
 25 KO 21 60
 26 BA .3085
 27 LS 0 72
 28 UD 0.38

*

29 KK F CENTRAL DRAINAGE AREA TO WEST END OF HAMILTON
 30 KO 21 60
 31 BA .0889
 32 LS 0 80
 33 UD 0.22

*

34 KK E CENTRAL AREA TO PETERSON BLVD
 35 KO 21 60
 36 BA 0.1257
 37 LS 0 87
 38 UD 0.19

*

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

39 KK D AREA WHICH FLOWS DIRECTLY INTO HAMILTON
 40 KO 21 60
 41 BA 0.2121
 42 LS 0 76
 43 UD 0.41
 *

44 KK DEF COMBINE AREAS D E AND F AT PETERSON AND HAMILTON
 45 HC 3
 *

46 KK B-1 OFFSITE NORTH OF 94 AND SOUTH OF U.S. 24
 47 BA 0.14
 48 LS 0 30
 49 UD .023
 *

50 KK B EAST AREA WHICH INCLUDES MOST OF FAMILY HOUSING AND AREAS TO THE NORTH
 51 KO 21 60
 52 BA 0.4568
 53 LS 0 68
 54 UD 0.65
 *

55 KK B-TOT COMBINED OFFSITE AND ONSITE AT B
 56 HC 2
 *

57 KK C SMALL AREA ON MITCHELL
 58 BA .02270
 59 LS 0 90
 60 UD 0.08
 *

61 KK BC COMBINE DRAINAGE AREAS B AND C AT HAMILTON AND MICHELL
 62 HC 2
 *

63 KK BCDE COMBINE DRAINAGE AREAS BC AND DE AT HAMILTON AND MICHELL
 64 HC 2
 *

65 KK A WEST SIDE OF GOLF COURSE
 66 BA .0740
 67 LS 0 68
 68 UD 0.11
 *

69 KK DEBCA COMBINE DRAINAGE AREAS DEBC AND A NEAR MICHELL
 70 HC 2
 *

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

71 KK I EAST SIDE OF GOLF COURSE AND SOME OFFSITE
 72 BA .2561
 73 LS 0 65
 74 UD 0.72
 *

75 KK DEBCAI COMBINE DRAINAGE AREAS DEBCA AND I AT DETENTION POND #2
 76 HC 2
 *
 *

77 KK D1 DETENTION VOLUME REQUIRED
 78 KO 21 60
 79 KM DETETIION BASIN #1
 80 RS 1 ELEV 6110.5
 81 SA .1 4.14 5.82 6.47 7.84 9.17 10.55
 82 SE 6110.4 6111 6113 6115 6120 6125 6130
 83 SQ 1 4 20 30 34 36 40
 84 SE 6110.4 6111 6113 6115 6120 6125 6130
 *
 85 ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
8	H	
	.	
24	.	G
	.	.
29	.	F
	.	.
34	.	E
	.	.
39	.	D
	.	.
44	.	DEF.....
	.	.
46	.	B-1
	.	.
50	.	B
	.	.
55	.	B-TOT.....
	.	.
57	.	C
	.	.
61	.	BC.....
	.	.
63	.	BCDE.....
	.	.
65	.	A
	.	.
69	.	DEBCA.....
	.	.
71	.	I
	.	.
75	.	DEBCAI.....
	.	V
	.	V
77	.	D1

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
SEPTEMBER 1990
VERSION 4.0
*
* RUN DATE 03/25/1992 TIME 14:32:08
*

*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*

PETERSON AIR FORCE BASE, COLORADO SPRINGS, CO
HEC1 INPUT FILE PAFBFIX.HC1
10 AND 100-YEAR EVENTS - 24 HOUR DURATION - TYPE IIA

5 IO OUTPUT CONTROL VARIABLES
IPRNT 4 PRINT CONTROL
IPLOT 1 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 15 MINUTES IN COMPUTATION INTERVAL
IDATE 25JAN92 STARTING DATE
ITIME 0000 STARTING TIME
NQ 100 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 26JAN92 ENDING DATE
NDTIME 0045 ENDING TIME
ICENT 19 CENTURY MARK
COMPUTATION INTERVAL .25 HOURS
TOTAL TIME BASE 24.75 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
.67 1.00

*
8 KK * H * SPACE COMMAND DRAINAGE AREA AT NORTH CENTER
* *

9 KO OUTPUT CONTROL VARIABLES

```

IPRNT      4 PRINT CONTROL
IPLOT      1 PLOT CONTROL
QSCAL      0. HYDROGRAPH PLOT SCALE
IPNCH      0 PUNCH COMPUTED HYDROGRAPH
IOUT       21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1      1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2      60 LAST ORDINATE PUNCHED OR SAVED
TIMINT     .250 TIME INTERVAL IN HOURS

```

```

6 IN      TIME DATA FOR INPUT TIME SERIES
          JXMIN      15 TIME INTERVAL IN MINUTES
          JXDATE     25JAN92 STARTING DATE
          JXTIME     0 STARTING TIME

```

SUBBASIN RUNOFF DATA

```

10 BA     SUBBASIN CHARACTERISTICS
          TAREA      .08 SUBBASIN AREA

```

PRECIPITATION DATA

```

11 PB     STORM      4.50 BASIN TOTAL PRECIPITATION

```

```

12 PI     INCREMENTAL PRECIPITATION PATTERN
          .00      .00      .00      .00      .00      .00      .00      .00      .00      .00
          .00      .00      .00      .00      .00      .00      .01      .01      .01      .01
          .02      .02      .30      .30      .03      .02      .01      .01      .01      .01
          .01      .01      .00      .00      .00      .00      .01      .00      .00      .00
          .00      .00      .00      .00      .00      .00      .00      .00      .00      .00
          .00      .00      .00      .00      .00      .00      .00      .00      .00      .00
          .00      .00      .00      .00      .00      .00      .00      .00      .00      .00
          .00      .00      .00      .00      .00      .00      .00      .00      .00      .00
          .00      .00      .00      .00      .00      .00      .00      .00      .00      .00

```

```

22 LS     SCS LOSS RATE
          STRL      .50 INITIAL ABSTRACTION
          CRVNBR    80.00 CURVE NUMBER
          RTIMP     .00 PERCENT IMPERVIOUS AREA

```

```

23 UD     SCS DIMENSIONLESS UNITGRAPH
          TLAG      .19 LAG

```

UNIT HYDROGRAPH
6 END-OF-PERIOD ORDINATES

```

112.      70.      18.      5.      1.      0.

```

* *** **

```

*****
*          *
*          *
*          *
*****

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```

24 KK     *          G *      DRAINAGE AREA AT NORTHWEST CORNER
          *          *

```

```

25 KO     OUTPUT CONTROL VARIABLES
          IPRNT     4 PRINT CONTROL
          IPLOT     1 PLOT CONTROL
          QSCAL     0. HYDROGRAPH PLOT SCALE
          IPNCH     0 PUNCH COMPUTED HYDROGRAPH

```

IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 60 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .250 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

26 BA SUBBASIN CHARACTERISTICS
 TAREA .31 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

27 LS SCS LOSS RATE
 STRTL .78 INITIAL ABSTRACTION
 CRVNBR 72.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

28 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .38 LAG

UNIT HYDROGRAPH
 10 END-OF-PERIOD ORDINATES

137. 297. 206. 86. 39. 17. 8. 4. 2. 0.

* ** ** ** **

29 KK * *
 * F * CENTRAL DRAINAGE AREA TO WEST END OF HAMILTON
 * *

30 KO OUTPUT CONTROL VARIABLES

IPRNT 4 PRINT CONTROL
 IPLOT 1 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 60 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .250 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

31 BA SUBBASIN CHARACTERISTICS

TAREA .09 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

32 LS SCS LOSS RATE

STRTL .50 INITIAL ABSTRACTION
 CRVNR 80.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

33 UD SCS DIMENSIONLESS UNITGRAPH

TLAG .22 LAG

UNIT HYDROGRAPH
 6 END-OF-PERIOD ORDINATES

103. 89. 26. 8. 2. 1.

*** **

34 KK * E * CENTRAL AREA TO PETERSON BLVD

35 KO OUTPUT CONTROL VARIABLES

IPRNT 4 PRINT CONTROL
 IPLOT 1 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 60 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .250 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

36 BA SUBBASIN CHARACTERISTICS

TAREA .13 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.01	.01	.01	.01	.01

42 LS SCS LOSS RATE
STRTL .63 INITIAL ABSTRACTION
CRVNBR 76.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

43 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .41 LAG

UNIT HYDROGRAPH
10 END-OF-PERIOD ORDINATES

80. 191. 150. 67. 32. 15. 7. 3. 2. 1.

*** ** ** ** **

* *
44 KK * DEF * COMBINE AREAS D E AND F AT PETERSON AND HAMILTON
* *

45 HC HYDROGRAPH COMBINATION
ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

** ** ** **

* *
46 KK * B-1 * OFFSITE NORTH OF 94 AND SOUTH OF U.S. 24
* *

SUBBASIN RUNOFF DATA

47 BA SUBBASIN CHARACTERISTICS
TAREA .14 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

48 LS SCS LOSS RATE
STRTL 4.67 INITIAL ABSTRACTION
CRVNBR 30.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

49 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .02 LAG

UNIT HYDROGRAPH
5 END-OF-PERIOD ORDINATES

268. 75. 15. 3. 0.

*** **

* *
50 KK * B * EAST AREA WHICH INCLUDES MOST OF FAMILY HOUSING AND AREAS TO THE NORTH
* *

51 KO OUTPUT CONTROL VARIABLES

IPRNT 4 PRINT CONTROL
IPLOT 1 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 60 LAST ORDINATE PUNCHED OR SAVED
TIMINT .250 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

52 BA SUBBASIN CHARACTERISTICS

TAREA .46 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

53 LS SCS LOSS RATE

STRTL .94 INITIAL ABSTRACTION
CRVNBR 68.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

54 UD SCS DIMENSIONLESS UNITGRAPH

TLAG .65 LAG

UNIT HYDROGRAPH
15 END-OF-PERIOD ORDINATES

62. 209. 285. 248. 156. 89. 54. 32. 19. 11.

7. 4. 2. 1. 0.

*** **

55 KK * B-TOT * COMBINED OFFSITE AND ONSITE AT B

56 HC HYDROGRAPH COMBINATION ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

57 KK * C * SMALL AREA ON MITCHELL

SUBBASIN RUNOFF DATA

58 BA SUBBASIN CHARACTERISTICS TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

Table with 10 columns of precipitation data values ranging from .00 to .03.

59 LS SCS LOSS RATE STRTL .22 INITIAL ABSTRACTION CRVNBR 90.00 CURVE NUMBER RTIMP .00 PERCENT IMPERVIOUS AREA

50 UD SCS DIMENSIONLESS UNITGRAPH TLAG .08 LAG

UNIT HYDROGRAPH 5 END-OF-PERIOD ORDINATES

44. 12. 2. 0. 0.

*** **

61 KK * BC * COMBINE DRAINAGE AREAS B AND C AT HAMILTON AND MICHELL

52 HC HYDROGRAPH COMBINATION ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

53 KK * BCDE * COMBINE DRAINAGE AREAS BC AND DE AT HAMILTON AND MICHELL

54 HC HYDROGRAPH COMBINATION ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

55 KK * A * WEST SIDE OF GOLF COURSE

SUBBASIN RUNOFF DATA

56 BA SUBBASIN CHARACTERISTICS TAREA .07 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

Table with 10 columns of precipitation data values ranging from .00 to .03.

57 LS SCS LOSS RATE STRL .94 INITIAL ABSTRACTION CRVNBR 68.00 CURVE NUMBER RTIMP .00 PERCENT IMPERVIOUS AREA

68 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .11 LAG

UNIT HYDROGRAPH
5 END-OF-PERIOD ORDINATES

142. 40. 8. 2. 0.

*** **

59 KK * DEBCA * COMBINE DRAINAGE AREAS DEBC AND A NEAR MICHELL
* *

70 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

* **

71 KK * I * EAST SIDE OF GOLF COURSE AND SOME OFFSITE
* *

SUBBASIN RUNOFF DATA

72 BA SUBBASIN CHARACTERISTICS
TAREA .26 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

3 LS SCS LOSS RATE
STRTL 1.08 INITIAL ABSTRACTION
CRVNBR 65.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

4 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .72 LAG

UNIT HYDROGRAPH
16 END-OF-PERIOD ORDINATES

27. 94. 144. 137. 102. 60. 37. 23. 14. 9.
5. 3. 2. 1. 1. 0.

* *
75 KK * DEBCAI * COMBINE DRAINAGE AREAS DEBCA AND I AT DETENTION POND #2
* *

76 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

* *
77 KK * D1 * DETENTION VOLUME REQUIRED
* *

78 KO OUTPUT CONTROL VARIABLES
IPRNT 4 PRINT CONTROL
IPLOT 1 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 60 LAST ORDINATE PUNCHED OR SAVED
TIMINT .250 TIME INTERVAL IN HOURS

DETENTION BASIN #1

HYDROGRAPH ROUTING DATA

30 RS STORAGE ROUTING
NSTPS 1 NUMBER OF SUBREACHES
ITYP ELEV TYPE OF INITIAL CONDITION
RSVRIC 6110.50 INITIAL CONDITION
X .00 WORKING R AND D COEFFICIENT

31 SA AREA .1 4.1 5.8 6.5 7.8 9.2 10.6
32 SE ELEVATION 6110.40 6111.00 6113.00 6115.00 6120.00 6125.00 6130.00
33 SQ DISCHARGE 1. 4. 20. 30. 34. 36. 40.
34 SE ELEVATION 6110.40 6111.00 6113.00 6115.00 6120.00 6125.00 6130.00

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	.98	10.89	23.17	58.89	101.38	150.64
ELEVATION	6110.40	6111.00	6113.00	6115.00	6120.00	6125.00	6130.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.98	10.89	23.17	58.89	101.38	150.64
OUTFLOW	1.00	4.00	20.00	30.00	34.00	36.00	40.00
ELEVATION	6110.40	6111.00	6113.00	6115.00	6120.00	6125.00	6130.00

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION		
				RATIO 1	RATIO 2	
				.67	1.00	
HYDROGRAPH AT	H	.08	1	FLOW TIME	64. 6.00	133. 6.00
HYDROGRAPH AT	G	.31	1	FLOW TIME	102. 6.25	257. 6.25
HYDROGRAPH AT	F	.09	1	FLOW TIME	63. 6.00	134. 6.00
HYDROGRAPH AT	E	.13	1	FLOW TIME	152. 6.00	277. 6.00
HYDROGRAPH AT	D	.21	1	FLOW TIME	90. 6.25	207. 6.25
COMBINED AT	DEF	.43	1	FLOW TIME	262. 6.00	536. 6.00
HYDROGRAPH AT	B-1	.14	1	FLOW TIME	0. .25	0. .25
HYDROGRAPH AT	B	.46	1	FLOW TIME	73. 6.50	213. 6.50
COMBINED AT	B-TOT	.60	1	FLOW TIME	73. 6.50	213. 6.50
HYDROGRAPH AT	C	.02	1	FLOW TIME	37. 6.00	63. 6.00
COMBINED AT	BC	.62	1	FLOW TIME	79. 6.50	222. 6.50
COMBINED AT	BCDE	1.05	1	FLOW TIME	316. 6.00	662. 6.00
HYDROGRAPH AT	A	.07	1	FLOW TIME	32. 6.00	87. 6.00
COMBINED AT	DEBCA	1.12	1	FLOW TIME	347. 6.00	749. 6.00
HYDROGRAPH AT	I	.26	1	FLOW TIME	29. 6.75	90. 6.75
COMBINED AT	DEBCAI	1.38	1	FLOW TIME	352. 6.00	771. 6.00
ADJUSTED TO	D1	1.38	1	FLOW TIME	31. 9.00	35. 13.25

** PEAK STAGES IN FEET **

1	STAGE	6115.97	6122.46
	TIME	9.00	13.50

1 * NORMAL END OF HEC-1 ***
I RMAL END OF HEC-1

FUTURE CONDITIONS HEC-1 OUTPUT

*FIX											*FIX	003
*DIAGRAM											*DIAGRAM	002
	PETERSON AIR FORCE BASE, COLORADO SPRINGS, CO										ID	036
	HEC1 INPUT FILE PAFB-P1.HC1, FUTURE FLOWS										ID	036
	ID 10 AND 100-YEAR EVENTS - 24 HOUR DURATION - TYPE IIA										ID	036
IT	15	25JAN92	0	100							IT	040
	4	1									IO	039
	15	25JAN92	0								IN	038
JR	PREC	.67	1.0								JR	043
*											*	001
	L NORTH CENTRAL DRAINAGE AREA EAST OF PETERSON AND NORTH OF PAINE										KK	045
				21		60					KO	047
BA0.0825											BA	008
	4.5										PB	069
	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143	PC	070
PC0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530	PC	070	
PC0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900	PC	070	
	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550	PC	070
	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938	PC	070
PC0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270	PC	070	
PC0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525	PC	070	
	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775	PC	070
	.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913	PC	070
PC0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000					PC	070
	0	80									LS	056
	0.16										UD	112
*											*	001
	K NORTH DRAINAGE AREA WEST OF PETERSON, NORTH AND SOUTH OF PAINE										KK	045
	.0486										BA	008
LS	0	91									LS	056
UD	0.09										UD	112
											*	001
	J NORTHWEST DRAINAGE AREA										KK	045
BA	.1646										BA	008
LS	0	80									LS	056
	0.13										UD	112
											*	001
KK	I WEST DRAINAGE AREA										KK	045
BA	.0805										BA	008
	0	91									LS	056
UD	0.13										UD	112
*											*	001
	P OFFSITE BETWEEN 24 AND 94										KK	045
	0.0268										BA	008
LS	0	57									LS	056
UD	0.13										UD	112
											*	001
	Q OFFSITE AT NORTHEAST CORNER										KK	045
BA0.1575											BA	008
LS	0	91									LS	056
UD	0.22										UD	112
											*	001
KK	PQ COMBINE NORTHEAST OFFSITE FLOWS AT NORTH PROPERTY LINE										KK	045
	2										HC	030
											*	001
KK	M EAST OF SPACE COMMAND HEADQUARTERS										KK	045
KO				21		60					KO	047
	.0975										BA	008
	0	90									LS	056
UD	0.10										UD	112
*											*	001
	PQM COMBINED FLOW IN EAST SWALE AT SOUTHEAST CORNER OF FAMILY HOUSING										KK	045
	2										HC	030
*											*	001
KK	H CENTRAL DRAINAGE AREA ON EAST SIDE OF PETERSON BLVD NORTH OF STEWART										KK	045

KO 21 60
 BA .0745
 0 91
 0.14
 *
 KK C FAMILY HOUSING AREA
 21 60
 .2306
 LS 0 80
 0.25
 KK HC COMBINE BASINS H AND C, FLOW IN EAST 60" STORM SEWER
 HC 2
 HCPQM COMBINE BASINS H, C, AND M, FLOW IN SWALE AT 60" STORM SEWER
 HC 2
 *
 N EAST DRAINAGE AREA TO PROPOSED SWALE
 21 60
 BAO.1428
 0 63
 0.34
 KKHCPQM COMBINE BASINS H,C,P,Q,M AND N, FLOW IN SWALE AT DETENTION POND #11
 2
 KK G CENTRAL DRAINAGE AREA WEST OF PETERSON BLVD AND SOUTH OF STEWART
 KO 21 60
 0.0530
 0 91
 UD 0.08
 *
 F SOUTHWEST DRAINAGE AREA NORTH OF HAMILTON AND WEST OF MICHELL
 21 60
 BAO.1883
 0 67
 0.16
 KK GF COMBINE BASINS G AND F, FLOW IN HAMILTON COLLECTOR WEST OF MITCHELL
 2
 KK B EAST DRAINAGE AREA EAST OF MICHELL AND NORTH OF GOLF COURSE
 BA.06270
 0 65
 0.25
 *
 KK D SOUTH CENTRAL DRAINAGE AREA WEST OF MITCHELL AND SOUTH OF STEWART
 .0441
 0 91
 UD 0.12
 *
 BD COMBINE BASINS B AND D, FLOW IN MITCHELL COLLECTOR
 2
 *
 E SOUTH DRAINAGE AREA WEST OF MITCHELL AND NORTH OF HAMILTON
 .0222
 LS 0 91
 UD 0.08
 BDE COMBINE BASINS B,D AND E, FLOW IN MITCHELL COLLECTOR AT HAMILTON
 HC 2
 *
 GFBDE COMBINE BASINS G,F,B,D AND E, TOTAL FLOW AT HAMILTON AND MITCHELL
 2
 *
 A SOUTHEAST DRAINAGE AREA EAST OF MITCHELL AND NORTH OF HAMILTON

KO 047
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 KO 047
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 HC 030
 * 001
 KK 045
 HC 030
 * 001
 KK 045
 KO 047
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 HC 030
 * 001
 KK 045
 KO 047
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 HC 030
 * 001
 KK 045
 KO 047
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 HC 030
 * 001
 KK 045
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 HC 030
 * 001
 KK 045
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 HC 030
 * 001
 KK 045

KO 21 60
 BAO.0741
 0 65
 0.25
 *
 KKGFBDEA COMBINE BASINS G,F,B,D,E AND A, TOTAL FLOW IN HAMILTON COLLECTOR
 2
 KK 0 SOUTHEAST DRAIANGE AREA GOLF COURSE NORTH OF DETENTION POND #11
 21 60
 0.1822
 0 65
 UD 0.34
 KK TOTAL TOTAL FLOW FROM STUDY AREA TO DETENTION POND #11
 HC 3

KK D1 DETENTION VOLUME REQUIRED
 KO 21 60
 DETETIION BASIN #1
 1 ELEV 6110.5
 SA .1 4.14 5.82 6.47 7.84 9.17 10.55
 6110.4 6111 6113 6115 6120 6125 6130
 1 4 20 30 34 36 40
 6110.4 6111 6113 6115 6120 6125 6130
 *

KO 047
 BA 008
 LS 056
 UD 112
 * 001
 KK 045
 HC 030
 * 001
 KK 045
 KO 047
 BA 008
 LS 056
 UD 112
 * 001
 * 001
 KK 045
 HC 030
 * 001
 * 001
 KK 045
 KO 047
 KM 046
 RS 092
 SA 096
 SE 099
 SQ 104
 SE 099
 * 001
 ZZ 127

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* SEPTEMBER 1990 *
* VERSION 4.0 *
* RUN DATE 04/02/1992 TIME 11:15:15 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

```

X   X  XXXXXXX  XXXXX      X
X   X X      X   X      XX
X   X X      X           X
XXXXXXX XXXX  X      XXXXX X
X   X X      X           X
X   X X      X   X      X
X   X  XXXXXXX  XXXXX      XXX

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::::::::::::::::::::::::::::::::::::
::::::::::::::::::::::::::::::::::::
::: Full Microcomputer Implementation :::
::: by :::
::: Haestad Methods, Inc. :::
:::
::::::::::::::::::::::::::::::::::::
::::::::::::::::::::::::::::::::::::

```

37 Brookside Road * Waterbury, Connecticut 06708 * (203) 755-1666

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*** FIX ***

*DIAGRAM

```

1  ID  PETERSON AIR FORCE BASE, COLORADO SPRINGS, CO
2  ID  HEC1 INPUT FILE PAFB-P1.HC1, FUTURE FLOWS
3  ID  10 AND 100-YEAR EVENTS - 24 HOUR DURATION - TYPE IIA
4  IT   15 25JAN92      0    100
5  IO   4    1
6  IN   15 25JAN92      0
7  JR  PREC   .67    1.0
*

8  KK      L NORTH CENTRAL DRAINAGE AREA EAST OF PETERSON AND NORTH OF PAINE
9  KO                                  21          60
10 BA  0.0825
11 PB   4.5
12 PC  0.0000  0.0005  0.0015  0.0030  0.0045  0.0060  0.0080  0.0100  0.0120  0.0143
13 PC  0.0165  0.0188  0.0210  0.0233  0.0255  0.0278  0.0320  0.0390  0.0460  0.0530
14 PC  0.0600  0.0750  0.1000  0.4000  0.7000  0.7250  0.7500  0.7650  0.7800  0.7900
15 PC  0.8000  0.8100  0.8200  0.8250  0.8300  0.8350  0.8400  0.8450  0.8500  0.8550
16 PC  0.8600  0.8638  0.8675  0.8713  0.8750  0.8788  0.8825  0.8863  0.8900  0.8938
17 PC  0.8975  0.9013  0.9050  0.9083  0.9115  0.9148  0.9180  0.9210  0.9240  0.9270
18 PC  0.9300  0.9325  0.9350  0.9375  0.9400  0.9425  0.9450  0.9475  0.9500  0.9525
19 PC  0.9550  0.9575  0.9600  0.9625  0.9650  0.9675  0.9700  0.9725  0.9750  0.9775
20 PC  .9800  0.9813  0.9825  0.9838  0.9850  0.9863  0.9875  0.9888  0.9900  0.9913
21 PC  0.9925  0.9938  0.9950  0.9963  0.9975  0.9988  1.0000
22 LS   0    80
23 UD  0.16
*
*

24 KK      K NORTH DRAINAGE AREA WEST OF PETERSON, NORTH AND SOUTH OF PAINE
25 BA  .0486
26 LS   0    91
27 UD  0.09
*

28 KK      J NORTHWEST DRAINAGE AREA
29 BA  .1646
30 LS   0    80
31 UD  0.13
*

32 KK      I WEST DRAINAGE AREA
33 BA  .0805
34 LS   0    91
35 UD  0.13
*

36 KK      P OFFSITE BETWEEN 24 AND 94
37 BA  0.0268
38 LS   0    57
39 UD  0.13
*
    
```


LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

40 KK Q OFFSITE AT NORTHEAST CORNER
 41 BA 0.1575
 42 LS 0 91
 43 UD 0.22
 *

44 KK PQ COMBINE NORTHEAST OFFSITE FLOWS AT NORTH PROPERTY LINE
 45 HC 2
 *

46 KK M EAST OF SPACE COMMAND HEADQUARTERS
 47 KO 21 60
 48 BA .0975
 49 LS 0 90
 50 UD 0.10
 *

51 KK PQM COMBINED FLOW IN EAST SWALE AT SOUTHEAST CORNER OF FAMILY HOUSING
 52 HC 2
 *

53 KK H CENTRAL DRAINAGE AREA ON EAST SIDE OF PETERSON BLVD NORTH OF STEWART
 54 KO 21 60
 55 BA .0745
 56 LS 0 91
 57 UD 0.14
 *

58 KK C FAMILY HOUSING AREA
 59 KO 21 60
 60 BA .2306
 61 LS 0 80
 62 UD 0.25
 *

63 KK HC COMBINE BASINS H AND C, FLOW IN EAST 60" STORM SEWER
 64 HC 2
 *

65 KK HCPQM COMBINE BASINS H, C, AND M, FLOW IN SWALE AT 60" STORM SEWER
 66 HC 2
 *

67 KK N EAST DRAINAGE AREA TO PROPOSED SWALE
 68 KO 21 60
 69 BA 0.1428
 70 LS 0 63
 71 UD 0.34
 *

LINE	ID	1	2	3	4	5	6	7	8	9	10
72	KK	HCPQMN COMBINE BASINS H,C,P,Q,M AND N, FLOW IN SWALE AT DETENTION POND #11									
73	HC	2									
	*										
74	KK	G CENTRAL DRAIANGE AREA WEST OF PETERSON BLVD AND SOUTH OF STEWART									
75	KO					21					60
76	BA	0.0530									
77	LS	0		91							
78	UD	0.08									
	*										
79	KK	F SOUTHWEST DRAINAGE AREA NORTH OF HAMILTON AND WEST OF MICHELL									
80	KO					21					60
81	BA	0.1883									
82	LS	0		67							
83	UD	0.16									
	*										
84	KK	GF COMBINE BASINS G AND F, FLOW IN HAMILTON COLLECTOR WEST OF MITCHELL									
85	HC	2									
	*										
86	KK	B EAST DRAIANGE AREA EAST OF MICHELL AND NORTH OF GOLF COURSE									
87	BA	.06270									
88	LS	0		65							
89	UD	0.25									
	*										
90	KK	D SOUTH CENTRAL DRAINAGE AREA WEST OF MITCHELL AND SOUTH OF STEWART									
91	BA	.0441									
92	LS	0		91							
93	UD	0.12									
	*										
94	KK	BD COMBINE BASINS B AND D, FLOW IN MITCHELL COLLECTOR									
95	HC	2									
	*										
96	KK	E SOUTH DRAINAGE AREA WEST OF MITCHELL AND NORTH OF HAMILTON									
97	BA	.0222									
98	LS	0		91							
99	UD	0.08									
	*										
100	KK	BDE COMBINE BASINS B,D AND E, FLOW IN MITCHELL COLLECTOR AT HAMILTON									
101	HC	2									
	*										
102	KK	GFBDE COMBINE BASINS G,F,B,D AND E, TOTAL FLOW AT HAMILTON AND MITCHELL									
103	HC	2									
	*										

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
104	KK A SOUTHEAST DRAINAGE AREA EAST OF MITCHELL AND NORTH OF HAMILTON
105	KO 21 60
106	BA 0.0741
107	LS 0 65
108	UD 0.25
	*
109	KK GFBDEA COMBINE BASINS G,F,B,D,E AND A, TOTAL FLOW IN HAMILTON COLLECTOR
110	HC 2
	*
111	KK O SOUTHEAST DRAINAGE AREA GOLF COURSE NORTH OF DETENTION POND #11
112	KO 21 60
113	BA 0.1822
114	LS 0 65
115	UD 0.34
	*
	*
116	KK TOTAL TOTAL FLOW FROM STUDY AREA TO DETENTION POND #11
117	HC 3
	*
	*
118	KK D1 DETENTION VOLUME REQUIRED
119	KO 21 60
120	KM DETENTION BASIN #1
121	RS 1 ELEV 6110.5
122	SA .1 4.14 5.82 6.47 7.84 9.17 10.55
123	SE 6110.4 6111 6113 6115 6120 6125 6130
124	SQ 1 4 20 30 34 36 40
125	SE 6110.4 6111 6113 6115 6120 6125 6130
	*
126	ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK

LINE NO.	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW	(<---) RETURN OF DIVERTED OR PUMPED FLOW
8	L		
24		K	
28			J
32			I
36			P
40			Q
44		PQ.....	
46			M
51		PQM.....	
53			H
58			C
63		HC.....	
65		HCPQM.....	
67			N
72		HCPQMN.....	
74			G
79			F
84		GF.....	
86			B
90			D

*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* SEPTEMBER 1990 *
* VERSION 4.0 *
*
* RUN DATE 04/02/1992 TIME 11:15:15 *
*

*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*

PETERSON AIR FORCE BASE, COLORADO SPRINGS, CO
HEC1 INPUT FILE PAFB-P1.HC1, FUTURE FLOWS
10 AND 100-YEAR EVENTS - 24 HOUR DURATION - TYPE IIA

5 IO OUTPUT CONTROL VARIABLES
IPRNT 4 PRINT CONTROL
IPLOT 1 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 15 MINUTES IN COMPUTATION INTERVAL
IDATE 25JAN92 STARTING DATE
ITIME 0000 STARTING TIME
NQ 100 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 26JAN92 ENDING DATE
NDTIME 0045 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .25 HOURS
TOTAL TIME BASE 24.75 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
.67 1.00

*** **

*
8 KK * L * NORTH CENTRAL DRAINAGE AREA EAST OF PETERSON AND NORTH OF PAINE
* *

9 KO OUTPUT CONTROL VARIABLES

94	BD.....	.

96	E

100	BDE.....	.

102	GFBDE.....	.	.

104	A

109	GFBDEA.....	.	.

111	O

116	TOTAL.....	.	.	.
	V	.	.	.
	V	.	.	.
118	D1	.	.	.

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

26 LS SCS LOSS RATE

STRTL .20 INITIAL ABSTRACTION

CRVNBR 91.00 CURVE NUMBER

RTIMP .00 PERCENT IMPERVIOUS AREA

27 UD SCS DIMENSIONLESS UNITGRAPH

TLAG .09 LAG

UNIT HYDROGRAPH

5 END-OF-PERIOD ORDINATES

93. 26. 5. 1. 0.

* *** **

* * NORTHWEST DRAINAGE AREA

28 KK * J * NORTHWEST DRAINAGE AREA

* *

SUBBASIN RUNOFF DATA

29 BA SUBBASIN CHARACTERISTICS

TAREA .16 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

30 LS SCS LOSS RATE

STRTL .50 INITIAL ABSTRACTION

CRVNBR 80.00 CURVE NUMBER

RTIMP .00 PERCENT IMPERVIOUS AREA

31 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .13 LAG

UNIT HYDROGRAPH
5 END-OF-PERIOD ORDINATES

309. 93. 19. 4. 0.

*** **

* *
32 KK * I * WEST DRAINAGE AREA
* *

SUBBASIN RUNOFF DATA

33 BA SUBBASIN CHARACTERISTICS
TAREA .08 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

34 LS SCS LOSS RATE
STRTL .20 INITIAL ABSTRACTION
CRVNBR 91.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

35 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .13 LAG

UNIT HYDROGRAPH
5 END-OF-PERIOD ORDINATES

151. 45. 9. 2. 0.

* **

* *
36 KK * P * OFFSITE BETWEEN 24 AND 94
* *

.00 .00 .00 .00 .00 .00

42 LS SCS LOSS RATE
STRTL .20 INITIAL ABSTRACTION
CRVNBR 91.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

43 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .22 LAG

UNIT HYDROGRAPH
6 END-OF-PERIOD ORDINATES

182. 157. 47. 14. 4. 1.

* *** **

44 KK * PQ * COMBINE NORTHEAST OFFSITE FLOWS AT NORTH PROPERTY LINE
* *

45 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

-46 KK * M * EAST OF SPACE COMMAND HEADQUARTERS
* *

47 KO OUTPUT CONTROL VARIABLES
IPRNT 4 PRINT CONTROL
IPLOT 1 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 60 LAST ORDINATE PUNCHED OR SAVED
TIMINT .250 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

48 BA SUBBASIN CHARACTERISTICS
TAREA .10 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .01 .01 .01 .01

.02	.02	.30	.30	.03	.02	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

49 LS SCS LOSS RATE
 STRTL .22 INITIAL ABSTRACTION
 CRVNBR 90.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

50 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .10 LAG

UNIT HYDROGRAPH
 5 END-OF-PERIOD ORDINATES

187. 52. 10. 2. 0.

* *** **

 * *
 * *

51 KK * PQM * COMBINED FLOW IN EAST SWALE AT SOUTHEAST CORNER OF FAMILY HOUSING

52 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

** * **

 * *
 * *

53 KK * H * CENTRAL DRAINAGE AREA ON EAST SIDE OF PETERSON BLVD NORTH OF STEWART

54 KO OUTPUT CONTROL VARIABLES
 IPRNT 4 PRINT CONTROL
 IPLOT 1 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH
 IQUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 60 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .250 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

55 BA SUBBASIN CHARACTERISTICS
 TAREA .07 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

56 LS SCS LOSS RATE
 STRL .20 INITIAL ABSTRACTION
 CRVNBR 91.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

57 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .14 LAG

UNIT HYDROGRAPH
 5 END-OF-PERIOD ORDINATES

134. 46. 10. 2. 0.

* * * * *

58 KK * C * FAMILY HOUSING AREA

59 KO OUTPUT CONTROL VARIABLES

IPRNT	4	PRINT CONTROL
IPLT	1	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	60	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.250	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

60 BA SUBBASIN CHARACTERISTICS
 TAREA .23 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00	.00

.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
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.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00

61 LS SCS LOSS RATE
STRTL .50 INITIAL ABSTRACTION
CRVNBR 80.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

62 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .25 LAG

UNIT HYDROGRAPH
7 END-OF-PERIOD ORDINATES

225. 245. 82. 29. 10. 3. 1.

*** **

* *
63 KK * HC * COMBINE BASINS H AND C, FLOW IN EAST 60" STORM SEWER
* *

64 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

* *
65 KK * HCPQM * COMBINE BASINS H, C, AND M, FLOW IN SWALE AT 60" STORM SEWER
* *

66 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

* **

* *
67 KK * N * EAST DRAINAGE AREA TO PROPOSED SWALE
* *

68 KD OUTPUT CONTROL VARIABLES
IPRNT 4 PRINT CONTROL

IPLOT 1 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 60 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .250 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

69 BA SUBBASIN CHARACTERISTICS
 TAREA .14 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

70 LS SCS LOSS RATE
 STRTL 1.17 INITIAL ABSTRACTION
 CRVNBR 63.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

71 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .34 LAG

UNIT HYDROGRAPH
9 END-OF-PERIOD ORDINATES

81. 148. 82. 34. 14. 6. 2. 1. 0.

*** **

 * *
 * HCPQMN *
 * *

72 KK COMBINE BASINS H,C,P,Q,M AND N, FLOW IN SWALE AT DETENTION POND #11

73 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

* **

74 KK * *
 * G * CENTRAL DRAINAGE AREA WEST OF PETERSON BLVD AND SOUTH OF STEWART
 * *

75 KO OUTPUT CONTROL VARIABLES
 IPRNT 4 PRINT CONTROL
 IPLOT 1 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 60 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .250 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

76 BA SUBBASIN CHARACTERISTICS
 TAREA .05 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

77 LS SCS LOSS RATE
 STRTL .20 INITIAL ABSTRACTION
 CRVNBR 91.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

78 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .08 LAG

UNIT HYDROGRAPH
 5 END-OF-PERIOD ORDINATES
 102. 28. 6. 1. 0.

*** **

 * *
 79 KK * F * SOUTHWEST DRAINAGE AREA NORTH OF HAMILTON AND WEST OF MICHELL
 * *

80 KO OUTPUT CONTROL VARIABLES
 IPRNT 4 PRINT CONTROL
 IPLOT 1 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IPNCH 0 PUNCH COMPUTED HYDROGRAPH
 IQUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 60 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .250 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

81 BA SUBBASIN CHARACTERISTICS
 TAREA .19 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

82 LS SCS LOSS RATE
 STRTL .99 INITIAL ABSTRACTION
 CRVNBR 67.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

83 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .16 LAG

UNIT HYDROGRAPH
 5 END-OF-PERIOD ORDINATES

310. 134. 32. 8. 2.

* *** **

84 KK * GF * COMBINE BASINS G AND F, FLOW IN HAMILTON COLLECTOR WEST OF MITCHELL

85 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

86 KK * B * EAST DRAIANGE AREA EAST OF MICHELL AND NORTH OF GOLF COURSE

.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00

92 LS SCS LOSS RATE
STRTL .20 INITIAL ABSTRACTION
CRVNBR 91.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

93 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .12 LAG

UNIT HYDROGRAPH
5 END-OF-PERIOD ORDINATES

85. 24. 5. 1. 0.

*** **

94 KK * BD * COMBINE BASINS B AND D, FLOW IN MITCHELL COLLECTOR

95 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

* **

96 KK * E * SOUTH DRAINAGE AREA WEST OF MITCHELL AND NORTH OF HAMILTON

SUBBASIN RUNOFF DATA

97 BA SUBBASIN CHARACTERISTICS
TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .01 .01 .01 .01
.02 .02 .30 .30 .03 .02 .01 .01 .01 .01
.01 .01 .00 .00 .00 .00 .01 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00

98 LS SCS LOSS RATE
 STRTL .20 INITIAL ABSTRACTION
 CRVNBR 91.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

99 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .08 LAG

UNIT HYDROGRAPH
5 END-OF-PERIOD ORDINATES

43. 12. 2. 0. 0.

*** **

* *
00 KK * BDE * COMBINE BASINS B,D AND E, FLOW IN MITCHELL COLLECTOR AT HAMILTON
* *

01 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

* **

* *
.02 KK * GFBDE * COMBINE BASINS G,F,B,D AND E, TOTAL FLOW AT HAMILTON AND MITCHELL
* *

103 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

* **

* *
104 KK * A * SOUTHEAST DRAINAGE AREA EAST OF MITCHELL AND NORTH OF HAMILTON
* *

105 KO OUTPUT CONTROL VARIABLES
 IPRNT 4 PRINT CONTROL
 IPLOT 1 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 60 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .250 TIME INTERVAL IN HOURS

IPLOT 1 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH
 IQUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 60 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .250 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

113 BA SUBBASIN CHARACTERISTICS
 TAREA .18 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.50 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.01	.01	.01	.01
.02	.02	.30	.30	.03	.02	.01	.01	.01	.01	.01
.01	.01	.00	.00	.00	.00	.01	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

114 LS SCS LOSS RATE
 STRTL 1.08 INITIAL ABSTRACTION
 CRVNBR 65.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

115 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .34 LAG

UNIT HYDROGRAPH
9 END-OF-PERIOD ORDINATES

103. 189. 104. 43. 18. 7. 3. 1. 0.

*** **

16 KK * TOTAL * TOTAL FLOW FROM STUDY AREA TO DETENTION POND #11

17 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

* **

118 KK * *
 * D1 * DETENTION VOLUME REQUIRED
 * *

119 KO OUTPUT CONTROL VARIABLES
 IPRNT 4 PRINT CONTROL
 IPLOT 1 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 60 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .250 TIME INTERVAL IN HOURS

DETETIION BASIN #1

HYDROGRAPH ROUTING DATA

121 RS STORAGE ROUTING
 NSTPS 1 NUMBER OF SUBREACHES
 ITYP ELEV TYPE OF INITIAL CONDITION
 RSVRIC 6110.50 INITIAL CONDITION
 X .00 WORKING R AND D COEFFICIENT

22 SA	AREA	.1	4.1	5.8	6.5	7.8	9.2	10.6
123 SE	ELEVATION	6110.40	6111.00	6113.00	6115.00	6120.00	6125.00	6130.00
24 SQ	DISCHARGE	1.	4.	20.	30.	34.	36.	40.
125 SE	ELEVATION	6110.40	6111.00	6113.00	6115.00	6120.00	6125.00	6130.00

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	.98	10.89	23.17	58.89	101.38	150.64
ELEVATION	6110.40	6111.00	6113.00	6115.00	6120.00	6125.00	6130.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.98	10.89	23.17	58.89	101.38	150.64
OUTFLOW	1.00	4.00	20.00	30.00	34.00	36.00	40.00
ELEVATION	6110.40	6111.00	6113.00	6115.00	6120.00	6125.00	6130.00

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION		
				RATIO 1	RATIO 2	
				.67	1.00	
HYDROGRAPH AT	L	.08	1	FLOW TIME	74. 6.00	151. 6.00
DROGRAPH AT	K	.05	1	FLOW TIME	83. 6.00	138. 6.00
DROGRAPH AT	J	.16	1	FLOW TIME	161. 6.00	325. 6.00
HYDROGRAPH AT	I	.08	1	FLOW TIME	136. 6.00	227. 6.00
HYDROGRAPH AT	P	.03	1	FLOW TIME	2. 6.00	14. 6.00
HYDROGRAPH AT	Q	.16	1	FLOW TIME	216. 6.00	372. 6.00
COMBINED AT	PQ	.18	1	FLOW TIME	218. 6.00	387. 6.00
DROGRAPH AT	M	.10	1	FLOW TIME	160. 6.00	270. 6.00
COMBINED AT	PQM	.28	1	FLOW TIME	378. 6.00	657. 6.00
HYDROGRAPH AT	H	.07	1	FLOW TIME	124. 6.00	207. 6.00
HYDROGRAPH AT	C	.23	1	FLOW TIME	145. 6.00	316. 6.00
COMBINED AT	HC	.31	1	FLOW TIME	269. 6.00	523. 6.00
COMBINED AT	HCPQM	.59	1	FLOW TIME	647. 6.00	1180. 6.00
HYDROGRAPH AT	N	.14	1	FLOW TIME	21. 6.25	74. 6.25
COMBINED AT	HCPQMN	.73	1	FLOW TIME	658. 6.00	1225. 6.00
HYDROGRAPH AT	G	.05	1	FLOW TIME	91. 6.00	151. 6.00
DROGRAPH AT	F	.19	1	FLOW TIME	63. 6.00	184. 6.00
COMBINED AT	GF	.24	1	FLOW TIME	154. 6.00	335. 6.00
HYDROGRAPH AT	B	.06	1	FLOW	12.	38.

				TIME	6.25	6.25
DROGRAPH AT	D	.04	1	FLOW	75.	126.
				TIME	6.00	6.00
2 COMBINED AT	BD	.11	1	FLOW	86.	161.
				TIME	6.00	6.00
HYDROGRAPH AT	E	.02	1	FLOW	38.	63.
				TIME	6.00	6.00
2 COMBINED AT	BDE	.13	1	FLOW	124.	225.
				TIME	6.00	6.00
COMBINED AT	GFBDE	.37	1	FLOW	278.	560.
				TIME	6.00	6.00
DROGRAPH AT	A	.07	1	FLOW	15.	45.
				TIME	6.25	6.25
2 COMBINED AT	GFBDEA	.44	1	FLOW	290.	602.
				TIME	6.00	6.00
HYDROGRAPH AT	O	.18	1	FLOW	34.	108.
				TIME	6.25	6.25
3 COMBINED AT	TOTAL	1.36	1	FLOW	965.	1894.
				TIME	6.00	6.00
UTED TO	D1	1.36	1	FLOW	33.	37.
				TIME	8.75	14.25

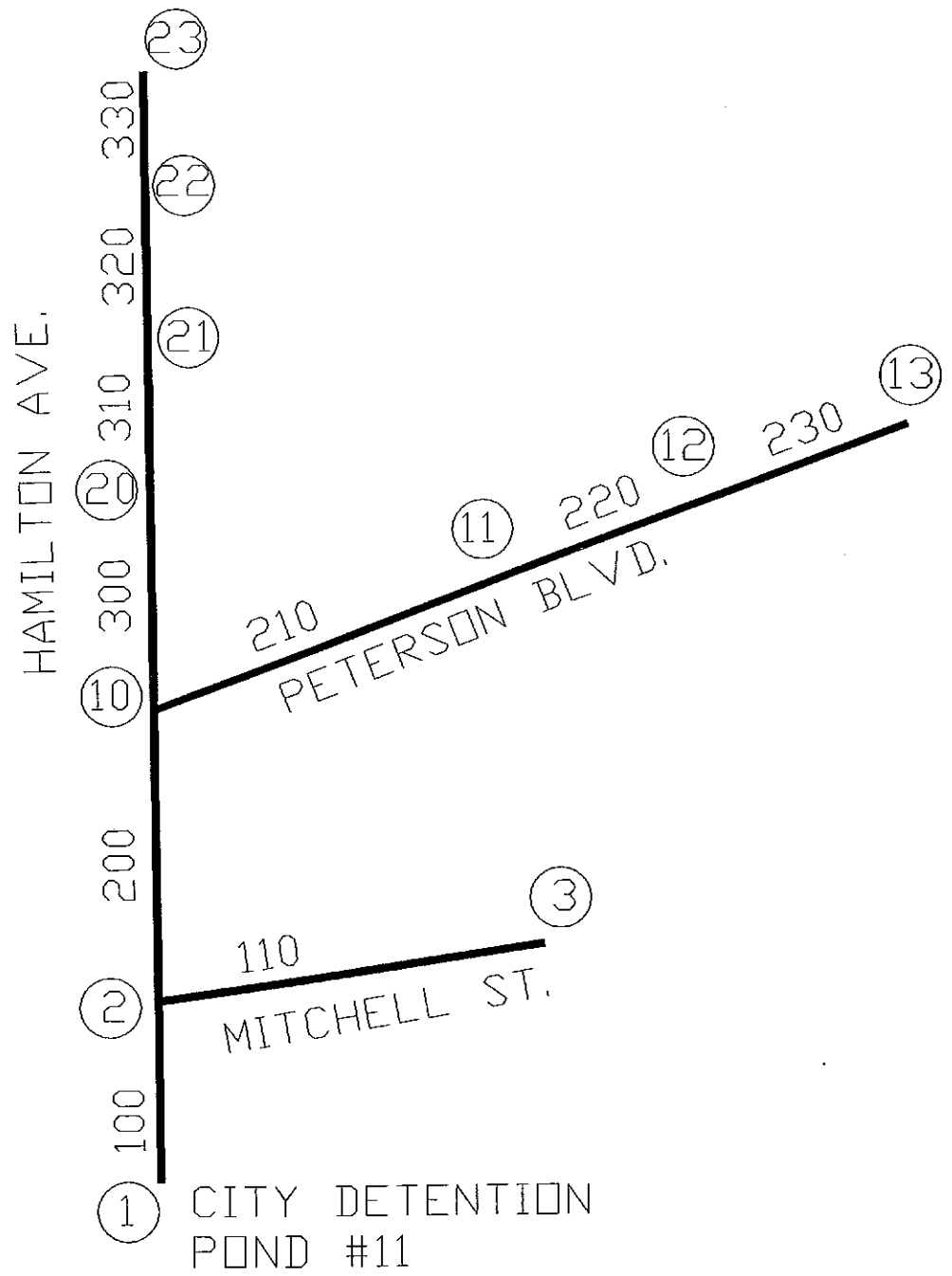
** PEAK STAGES IN FEET **

1	STAGE	6119.01	6126.36
	TIME	8.75	14.25

*** NORMAL END OF HEC-1 ***

NORMAL END OF HEC-1

PIPE CAPACITY CALCULATIONS



PAFB EXISTING MAIN STORM SEWER
UDSEWER COMPUTER MODEL

PETERSON AFB BASEWIDE DRAINAGE STUDY

EXISTING STORM SEWER CAPACITY CALCULATIONS

2, 18, 30, 1, 2, 1, .8, 500, 300, .2, N

2, 10

4.9, 3.8, 2.7, 2.2, 1.8, 1.4, .89

11

1, 6145, 0, 1, 100, 0, 0, 0

310, 0, 50, .7, 0, 0, 0, 0, 0

2, 6166, 100, 2, 110, 200, 0, 0

310, 0, 50, .7, 0, 0, 0, 0, 0

5, 6197, 110, 0, 0, 0, 0, 0

60, 0, 50, .7, 0, 0, 0, 0, 0

10, 6172, 200, 2, 210, 300, 0, 0

250, 0, 50, .7, 0, 0, 0, 0, 0

11, 6190, 210, 1, 220, 0, 0, 0

130, 0, 50, .7, 0, 0, 0, 0, 0

12, 6208, 220, 1, 230, 0, 0, 0

100, 0, 50, .7, 0, 0, 0, 0, 0

13, 6210, 230, 0, 0, 0, 0, 0

100, 0, 50, .7, 0, 0, 0, 0, 0

20, 6177, 300, 1, 310, 0, 0, 0

30, 0, 50, .7, 0, 0, 0, 0, 0

21, 6178, 310, 1, 320, 0, 0, 0

45, 0, 50, .7, 0, 0, 0, 0, 0

22, 6179, 320, 1, 330, 0, 0, 0

30, 0, 50, .7, 0, 0, 0, 0, 0

23, 6184, 330, 0, 0, 0, 0, 0

20, 0, 50, .7, 0, 0, 0, 0, 0

10

100, 2600, .81, 6159, .015, 0, 0, 1, 72, 0

110, 2470, 1.417, 6194, .015, 0, 0, 1, 36, 0

200, 1700, .453, 6166, .015, 0, 0, 1, 72, 0

210, 1200, 1.75, 6186, .015, 0, 0, 1, 48, 0

220, 1200, 1.175, 6201.7, .015, 0, 0, 1, 42, 0

230, 450, 1.18, 6207, .015, 0, 0, 1, 42, 0

300, 850, .447, 6169, .015, 0, 0, 1, 42, 0

310, 450, .489, 6171, .015, 0, 0, 1, 36, 0

320, 200, 1.35, 6174, .015, 0, 0, 1, 30, 0

330, 430, 1.395, 6180, .015, 0, 0, 1, 24, 0

=====

REPORT OF STORM SEWER SYSTEM DESIGN

USING UDSEWER-MODEL VERSION 2
DEVELOPED

BY

JAMES C.Y. GUO ,PHD, PE
DEPARTMENT OF CIVIL ENGINEERING, UNIVERSITY OF COLORADO AT DENVER
IN COOPERATION WITH
URBAN DRAINAGE AND FLOOD CONTROL DISTRICT
DENVER, COLORADO

=====

** EXECUTED BY HOLLAND WEST COMPANY- DENVER COLORADO
ON DATA 04-03-1992 AT TIME 06:48:03

** PROJECT TITLE :

PETERSON AFB BASEWIDE DRAINAGE STUDY

** RETURN PERIOD OF FLOOD IS 10 YEARS

RAINFALL INTENSITY TABLE IS GIVEN

** SUMMARY OF SUBBASIN RUNOFF PREDICTIONS

MANHOLE ID NUMBER	BASIN AREA * C	TIME OF CONCENTRATION			RAIN INCH/HR	I PEAK FLOW CFS
		OVERLAND To (MIN)	GUTTER Tf (MIN)	BASIN Tc (MIN)		
1.00	35.00	0.00	0.00	0.00	4.90	171.50
2.00	35.00	0.00	0.00	0.00	4.90	171.50
3.00	35.00	0.00	0.00	44.29	1.71	60.00
10.00	35.00	0.00	0.00	0.00	4.90	171.50
11.00	35.00	0.00	0.00	0.00	4.90	171.50
12.00	35.00	0.00	0.00	0.00	4.90	171.50
13.00	35.00	0.00	0.00	18.57	2.86	100.00
20.00	35.00	0.00	0.00	0.00	4.90	171.50
21.00	35.00	0.00	0.00	0.00	4.90	171.50
22.00	35.00	0.00	0.00	0.00	4.90	171.50
23.00	35.00	0.00	0.00	157.48	0.57	20.00

THE SHORTEST DESIGN RAINFALL DURATION IS FIVE MINUTES

DENVER REGIONAL DRAINAGE CRITERIA WAS NOT USED TO CHECK
THE COMPUTATION OF TIME OF CONCENTRATION

*** SUMMARY OF HYDRAULICS AT MANHOLES

MANHOLE ID	CNTRBTG AREA * C	RAINFALL DURATION MINUTES	RAINFALL INTENSITY INCH/HR	DESIGN PEAK FLOW CFS	GROUND ELEVATION FEET	WATER ELEVATION FEET	COMMENTS
1.00	0.00	0.00	0.00	310.00	6145.00	6135.00	OK
2.00	350.00	120.50	0.89	310.00	6166.00	6157.80	OK
3.00	35.00	44.29	1.71	60.00	6197.00	6193.49	OK
10.00	280.00	119.66	0.89	250.00	6172.00	6167.18	OK
11.00	105.00	79.05	1.24	130.00	6190.00	6185.39	OK
12.00	70.00	58.57	1.43	100.00	6208.00	6202.70	OK
13.00	35.00	18.57	2.86	100.00	6210.00	6208.58	OK
20.00	140.00	157.48	0.57	80.00	6177.00	6174.44	OK
21.00	105.00	174.29	0.43	45.00	6178.00	6177.59	OK
22.00	70.00	174.29	0.43	30.00	6179.00	6178.32	OK
23.00	35.00	157.48	0.57	20.00	6184.00	6181.95	OK

MEANS WATER ELEVATION IS LOWER THAN GROUND ELEVATION

THE TIME OF CONCENTRATION AT MANHOLE ID = 21 DECREASES DOWNSTREAM
 E TIME OF CONCENTRATION AT MANHOLE ID = 20 DECREASES DOWNSTREAM
 E TIME OF CONCENTRATION AT MANHOLE ID = 10 DECREASES DOWNSTREAM
 THE TIME OF CONCENTRATION AT MANHOLE ID = 2 DECREASES DOWNSTREAM
 CHECK THE GIVEN DESIGN FLOWS

* SUMMARY OF SEWER HYDRAULICS

NOTE: THE GIVEN FLOW DEPTH-TO-SEWER SIZE RATIO= .8

SEWER ID NUMBER	MANHOLE NUMBER UPSTREAM ID NO.	MANHOLE NUMBER DNSTREAM ID NO.	SEWER SHAPE	REQUIRED DIA(HIGH) (IN) (FT)	SUGGESTED DIA(HIGH) (IN) (FT)	EXISTING DIA(HIGH) (IN) (FT)	WIDTH (FT)
100.00	2.00	1.00	ROUND	70.32	72.00	72.00	0.00
110.00	3.00	2.00	ROUND	34.20	36.00	36.00	0.00
200.00	10.00	2.00	ROUND	72.33	78.00	72.00	0.00
210.00	11.00	10.00	ROUND	43.93	48.00	48.00	0.00
220.00	12.00	11.00	ROUND	42.90	48.00	42.00	0.00
230.00	13.00	12.00	ROUND	42.87	48.00	42.00	0.00
300.00	20.00	10.00	ROUND	47.30	48.00	42.00	0.00
310.00	21.00	20.00	ROUND	37.48	42.00	36.00	0.00
320.00	22.00	21.00	ROUND	26.61	27.00	30.00	0.00
330.00	23.00	22.00	ROUND	22.72	24.00	24.00	0.00

DIMENSION UNITS FOR ROUND AND ARCH SEWER ARE IN INCHES
 DIMENSION UNITS FOR BOX SEWER ARE IN FEET
 REQUIRED DIAMETER = COMPUTED; SUGGESTED DIAMETER = COMMERCIAL
 FOR A NEW SEWER, FLOW IS ANALYZED BY THE SUGGESTED SEWER SIZE; OTHERWISE,
 EXISTING SIZE IS USED

SEWER ID NUMBER	DESIGN Q IN CFS	Q P-FULL IN CFS	DEPTH YN FEET	CRTC DEPTH YC FEET	VELOCITY IN FPS	FROUDE NUMBER	COMMENTS
100.00	310.00	331.23	4.60	4.80	13.31	1.09	V-OK
110.00	60.00	69.00	2.16	2.49	11.00	1.36	V-OK
200.00	250.00	247.70	6.00	4.25	8.84	0.00	V-OK
210.00	130.00	165.13	2.67	3.39	14.56	1.67	V-OK
220.00	100.00	94.77	3.50	3.04	10.39	0.00	V-OK
230.00	100.00	94.97	3.50	3.04	10.39	0.00	V-OK

300.00	80.00	58.45	3.50	2.79	8.32	0.00	V-OK
310.00	45.00	40.53	3.00	2.12	6.37	0.00	V-OK
320.00	30.00	41.41	1.58	1.87	9.20	1.39	V-OK
330.00	20.00	23.22	1.43	1.60	8.31	1.27	V-OK

DUDE NUMBER=0 INDICATES THAT A PRESSURED FLOW OCCURS

SEWER ID NUMBER	SLOPE %	INVERT ELEVATION		BURIED DEPTH		COMMENTS
		UPSTREAM (FT)	DNSTREAM (FT)	UPSTREAM (FT)	DNSTREAM (FT)	
100.00	0.81	6153.00	6131.94	7.00	7.06	OK
110.00	1.42	6191.00	6156.00	3.00	7.00	OK
200.00	0.45	6160.00	6152.30	6.00	7.70	OK
210.00	1.75	6182.00	6161.00	4.00	7.00	OK
220.00	1.17	6198.20	6184.10	6.30	2.40	OK
230.00	1.18	6203.50	6198.19	3.00	6.31	OK
300.00	0.45	6165.50	6161.70	8.00	6.80	OK
310.00	0.49	6168.00	6165.80	7.00	8.20	OK
320.00	1.35	6171.50	6168.80	5.00	6.70	OK
330.00	1.39	6178.00	6172.00	4.00	5.00	OK

MEANS BURIED DEPTH IS GREATER THAN REQUIRED SOIL COVER OF 2 FEET

* SUMMARY OF HYDRAULIC GRADIENT LINE ALONG SEWERS

SEWER ID NUMBER	SEWER SURCHARGED		CROWN ELEVATION		WATER ELEVATION		FLOW CONDITION
	LENGTH FEET	LENGTH FEET	UPSTREAM FEET	DNSTREAM FEET	UPSTREAM FEET	DNSTREAM FEET	
100.00	2600.00	0.00	6159.00	6137.94	6157.80	6135.00	JUMP
110.00	2470.00	0.00	6194.00	6159.00	6193.49	6157.80	JUMP
200.00	1700.00	1700.00	6166.00	6158.30	6167.18	6157.80	PRSS'ED
210.00	1200.00	5.89	6186.00	6165.00	6185.39	6167.18	JUMP
220.00	1200.00	1200.00	6201.70	6187.60	6202.70	6185.39	PRSS'ED
230.00	450.00	450.00	6207.00	6201.69	6208.58	6202.70	PRSS'ED
300.00	850.00	850.00	6169.00	6165.20	6174.44	6167.18	PRSS'ED
310.00	450.00	450.00	6171.00	6168.80	6177.59	6174.44	PRSS'ED
320.00	200.00	200.00	6174.00	6171.30	6178.32	6177.59	PRSS'ED
330.00	430.00	326.99	6180.00	6174.00	6181.95	6178.32	JUMP

PRSS'ED=PRESSURED FLOW; JUMP=POSSIBLE HYDRAULIC JUMP; SUBCR=SUBCRITICAL FLOW

*** SUMMARY OF ENERGY GRADIENT LINE ALONG SEWERS

SEWER ID NO.	UPSTREAM MANHOLE		FRICTION		DOWNSTREAM MANHOLE				ENERGY FT
	MANHOLE ID NO.	ENERGY ELEV FT	LOSS FT	MANHOLE ID	BEND K	MAIN K	JCT LOSS		
100.00	2.00	6160.55	6157.80	25.55	1.00	0.00	0.00	0.00	6135.00
110.00	3.00	6195.37	6193.49	34.82	2.00	0.00	0.00	0.00	6160.55
200.00	10.00	6168.39	6167.18	7.84	2.00	0.00	0.00	0.00	6160.55
210.00	11.00	6188.68	6185.39	20.29	10.00	0.00	0.00	0.00	6168.39
220.00	12.00	6204.37	6202.70	15.69	11.00	0.00	0.00	0.00	6188.68

230.00	13.00	6210.26	6208.58	5.89	12.00	0.00	0.00	0.00	6204.37
300.00	20.00	6175.51	6174.44	7.11	10.00	0.00	0.00	0.00	6168.39
310.00	21.00	6178.22	6177.59	2.71	20.00	0.00	0.00	0.00	6175.51
320.00	22.00	6179.64	6178.32	1.42	21.00	0.00	0.00	0.00	6178.22
330.00	23.00	6183.02	6181.95	3.38	22.00	0.00	0.00	0.00	6179.64

BEND LOSS = BEND K * VHEAD IN SEWER.

MAINLINE LOSS = OUTFLOW VHEAD - JCT LOSS K * INFLOW VHEAD

JUNCTURE LOSS = 0 IF THE ABOVE DIFFERENCE IS LESS THAN ZERO

FRICTION LOSS = 0 MEANS IT IS NEGLIGIBLE OR POSSIBLE ERROR DUE TO JUMP.

FRICTION LOSS INCLUDES DROP AT MANHOLE

*** SUMMARY OF EARTH EXCAVATION VOLUME FOR COST ESTIMATE.

THE TRENCH SIDE SLOPE = 1

MANHOLE D NUMBER	GROUND ELEVATION FT	INVERT ELEVATION FT	MANHOLE HEIGHT FT
1.00	6145.00	6131.94	13.06
2.00	6166.00	6152.30	13.70
3.00	6197.00	6191.00	6.00
10.00	6172.00	6160.00	12.00
11.00	6190.00	6182.00	8.00
12.00	6208.00	6198.19	9.81
13.00	6210.00	6203.50	6.50
20.00	6177.00	6165.50	11.50
21.00	6178.00	6168.00	10.00
22.00	6179.00	6171.50	7.50
23.00	6184.00	6178.00	6.00

SEWER ID NUMBER	UPST ON GROUND FT	TRENCH WIDTH AT INVERT FT	DNST ON GROUND FT	TRENCH WIDTH AT INVERT FT	TRENCH LENGTH FT	WALL THICKNESS INCHES	EARTH VOLUME CUBIC YD
100.00	22.83	11.17	22.95	11.17	2600.00	7.00	18397.3
110.00	10.33	5.67	18.33	5.67	2470.00	4.00	6749.3
200.00	20.83	11.17	24.24	11.17	1700.00	7.00	11817.9
210.00	13.17	6.83	19.17	6.83	1200.00	5.00	4256.8
220.00	17.35	6.25	9.55	6.25	1200.00	4.50	3203.2
230.00	10.75	6.25	17.37	6.25	450.00	4.50	1253.5
300.00	20.75	6.25	18.35	6.25	850.00	4.50	3744.8
310.00	18.33	5.67	20.73	5.67	450.00	4.00	1902.9
320.00	13.92	5.08	17.32	5.08	200.00	3.50	562.9
330.00	11.50	4.50	13.50	4.50	430.00	3.00	796.1

TOTAL EARTH VOLUME FOR SEWER TRENCHES = 52684.57 CUBIC YARDS
SEWER FLOW LINE IS DETERMINED BY THE USER

EARTH VOLUME WAS ESTIMATED TO HAVE

BOTTOM WIDTH = DIAMETER OR WIDTH OF SEWER + 2 * B

B = ONE FEET WHEN DIAMETER OR WIDTH <= 48 INCHES

B = TWO FEET WHEN DIAMETER OR WIDTH > 48 INCHES

IF BOTTOM WIDTH < MINIMUM WIDTH, 2 FT, THE MINIMUM WIDTH WAS USED.

BACKFILL DEPTH UNDER SEWER WAS ASSUMED TO BE ONE FOOT

SEWER WALL THICKNESS = EQUIV LNT DIAMATER IN INCH / 12 + 1 IN INCHES

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 3, 1992
PAFB BASEWIDE DRAINAGE STUDY
72", PETERSON TO MITCHELL STREET

PROGRAM INPUT DATA:
DESCRIPTION

DESCRIPTION	VALUE
Culvert Diameter (feet).....	6.00
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0150
Entrance Loss Coefficient of Culvert Opening.....	0.20
Culvert Length (feet).....	2100.0
Culvert Slope (feet per foot).....	0.0040

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
100.0	9.00	3.84	2.38	2.75	2.69	2.75	7.90
120.0	9.00	4.29	3.17	3.06	2.96	3.06	8.26
140.0	9.00	4.73	4.09	3.36	3.21	3.36	8.59
160.0	9.00	5.17	5.16	3.66	3.44	3.66	8.86
180.0	9.00	5.60	6.38	3.97	3.66	6.00	6.37
200.0	9.00	6.03	7.73	4.29	3.86	6.00	7.07
220.0	9.00	6.47	9.23	4.66	4.06	6.00	7.78
240.0	9.00	6.91	10.87	5.13	4.24	6.00	8.49
<u>260.0</u>	9.00	7.55	12.65	6.00	4.42	6.00	9.20
280.0	9.00	7.92	14.58	6.00	4.58	6.00	9.90

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 3, 1992
PAFB BASEWIDE DRAINAGE STUDY
72", MITCHELL TO SWALE

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PROGRAM INPUT DATA:
DESCRIPTION                                                    VALUE
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Culvert Diameter (feet).....                               6.00
FHWA Chart Number (1,2 or 3).....                           1
Scale Number on Chart (Type of Culvert Entrance).....       1
Manning's Roughness Coefficient (n-value).....              0.0150
Entrance Loss Coefficient of Culvert Opening.....            0.20
Culvert Length (feet).....                                  3100.0
Culvert Slope (feet per foot).....                           0.0080
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PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
50.0	2.00	2.59	-20.23	1.59	1.88	1.59	8.35
75.0	2.00	3.25	-19.22	1.95	2.32	1.95	9.41
100.0	2.00	3.84	-17.93	2.27	2.69	2.27	10.20
125.0	2.00	4.40	-16.35	2.57	3.02	2.57	10.79
150.0	3.00	4.95	-14.46	2.84	3.33	2.84	11.37
175.0	3.00	5.49	-12.28	3.11	3.61	3.11	11.85
200.0	3.00	6.03	-9.78	3.38	3.86	3.38	12.17
225.0	3.00	6.58	-6.98	3.65	4.11	3.65	12.51
250.0	3.00	7.25	-3.88	3.92	4.33	3.92	12.79
300.0	3.00	8.50	3.26	4.51	4.73	4.51	13.17
325.0	3.00	9.28	7.28	4.87	4.91	4.87	13.22
350.0	3.00	10.12	11.62	5.40	5.07	5.07	13.74
375.0	3.00	11.02	16.26	6.00	5.21	5.21	14.38
400.0	3.00	11.99	21.21	6.00	5.33	5.33	15.06
425.0	4.00	13.01	26.46	6.00	5.44	5.44	15.77
450.0	4.00	14.10	32.02	6.00	5.53	5.53	16.51

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 3, 1992
PAFB BASEWIDE DRAINAGE STUDY
HAMILTON AVENUE COLLECTOR
42" SECTION BETWEEN VINCENT ST AND PETERSON BLVD

PROGRAM INPUT DATA:
DESCRIPTION

	VALUE
Culvert Diameter (feet).....	3.50
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0150
Entrance Loss Coefficient of Culvert Opening.....	0.20
Culvert Length (feet).....	800.0
Culvert Slope (feet per foot).....	0.0050

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater Inlet Control	Headwater Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
10.0	10.00	1.31	6.12	0.95	0.96	3.50	1.04
15.0	10.00	1.63	6.28	1.16	1.18	3.50	1.56
20.0	10.00	1.92	6.50	1.37	1.37	3.50	2.08
25.0	10.00	2.19	6.78	1.55	1.54	3.50	2.60
30.0	10.00	2.45	7.12	1.71	1.69	3.50	3.12
35.0	10.00	2.69	7.53	1.89	1.83	3.50	3.64
40.0	10.00	2.94	8.00	2.05	1.97	3.50	4.16
45.0	10.00	3.18	8.53	2.22	2.09	3.50	4.68
50.0	10.00	3.42	9.12	2.39	2.21	3.50	5.20
55.0	10.00	3.67	9.77	2.57	2.32	3.50	5.72
60.0	10.00	3.91	10.49	2.76	2.43	3.50	6.24
65.0	10.00	4.23	11.27	3.08	2.53	3.50	6.76
70.0	10.00	4.52	12.11	3.50	2.62	3.50	7.28

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 3, 1992
PAFB BASEWIDE DRAINAGE STUDY
HAMILTON AVENUE COLLECTOR
36" SECTION BETWEEN TRUAX ST AND VINCENT ST

PROGRAM INPUT DATA:

DESCRIPTION	VALUE
Culvert Diameter (feet).....	3.00
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0150
Entrance Loss Coefficient of Culvert Opening.....	0.20
Culvert Length (feet).....	550.0
Culvert Slope (feet per foot).....	0.0110

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
10.0	10.00	1.38	4.15	0.82	1.00	3.00	1.41
15.0	10.00	1.74	4.40	1.02	1.23	3.00	2.12
20.0	10.00	2.07	4.75	1.19	1.43	3.00	2.83
25.0	10.00	2.38	5.21	1.34	1.61	3.00	3.54
30.0	10.00	2.69	5.76	1.49	1.77	3.00	4.24
35.0	10.00	2.99	6.41	1.64	1.92	3.00	4.95
40.0	10.00	3.30	7.17	1.78	2.06	3.00	5.66
45.0	10.00	3.70	8.02	1.92	2.19	3.00	6.37
50.0	10.00	4.00	8.97	2.08	2.30	3.00	7.07
<u>55.0</u>	10.00	4.42	10.03	2.24	2.41	3.00	7.78
60.0	10.00	4.88	11.18	2.43	2.50	3.00	8.49
65.0	10.00	5.38	12.44	2.75	2.59	3.00	9.20

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 3, 1992
PAFB BASEWIDE DRAINAGE STUDY
HAMILTON AVENUE COLLECTOR
30" SECTION AT TRUAX STREET

PROGRAM INPUT DATA:
DESCRIPTION

DESCRIPTION	VALUE
Culvert Diameter (feet).....	2.50
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0150
Entrance Loss Coefficient of Culvert Opening.....	0.20
Culvert Length (feet).....	250.0
Culvert Slope (feet per foot).....	0.0110

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
10.0	10.00	1.50	7.52	0.88	1.06	2.50	2.04
15.0	10.00	1.92	7.87	1.10	1.31	2.50	3.06
20.0	10.00	2.32	8.35	1.30	1.52	2.50	4.07
25.0	10.00	2.72	8.96	1.50	1.70	2.50	5.09
30.0	10.00	3.21	9.72	1.69	1.87	2.50	6.11
25.0	10.00	2.72	8.96	1.50	1.70	2.50	5.09
30.0	10.00	3.21	9.72	1.69	1.87	2.50	6.11
<u>35.0</u>	10.00	3.70	10.61	1.93	2.01	2.50	7.13
40.0	10.00	4.32	11.63	2.29	2.13	2.50	8.15

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 3, 1992
PAFB BASEWIDE DRAINAGE STUDY
HAMILTON AVENUE COLLECTOR
24" SECTION BETWEEN OTTIS ST AND TRUAX ST

PROGRAM INPUT DATA:
DESCRIPTION

DESCRIPTION	VALUE
Culvert Diameter (feet).....	2.00
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0150
Entrance Loss Coefficient of Culvert Opening.....	0.20
Culvert Length (feet).....	550.0
Culvert Slope (feet per foot).....	0.0110

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
10.0	10.00	1.69	5.56	0.98	1.13	2.00	3.18
12.0	10.00	1.92	6.27	1.10	1.24	2.00	3.82
14.0	10.00	2.14	7.11	1.21	1.35	2.00	4.46
16.0	10.00	2.41	8.08	1.33	1.44	2.00	5.09
<u>18.0</u>	10.00	2.65	9.17	1.45	1.53	2.00	5.73
20.0	10.00	2.95	10.40	1.59	1.61	2.00	6.37

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 3, 1992
PAFB BASEWIDE DRAINAGE STUDY
36", MITHCELL STREET CULVERT
GLASOOW AVENUE TO 72" AT HAMILTON AVENUE

PROGRAM INPUT DATA:
DESCRIPTION

DESCRIPTION	VALUE
Culvert Diameter (feet).....	3.00
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0150
Entrance Loss Coefficient of Culvert Opening.....	0.20
Culvert Length (feet).....	2600.0
Culvert Slope (feet per foot).....	0.0120

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
20.0	9.00	2.07	-18.96	1.16	1.43	1.16	7.95
25.0	9.00	2.38	-17.13	1.31	1.61	1.31	8.42
30.0	9.00	2.69	-14.90	1.48	1.77	1.48	8.66
35.0	9.00	2.99	-12.26	1.59	1.92	1.59	9.18
40.0	9.00	3.30	-9.22	1.73	2.06	1.73	9.48
45.0	9.00	3.70	-5.78	1.87	2.19	1.87	9.74
50.0	9.00	4.00	-1.92	2.01	2.30	2.01	9.92
55.0	9.00	4.42	2.33	2.16	2.41	2.16	10.10
60.0	9.00	4.88	7.00	2.33	2.50	3.00	8.49
<u>65.0</u>	9.00	5.38	12.07	2.53	2.59	3.00	9.20

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 3, 1992
PAFB BASEWIDE DRAINAGE STUDY
48" PETERSON BLVD COLLECTOR
ENT AVE. TO HAMILTON AVE

PROGRAM INPUT DATA:
DESCRIPTION

DESCRIPTION	VALUE
Culvert Diameter (feet).....	4.00
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0150
Entrance Loss Coefficient of Culvert Opening.....	0.20
Culvert Length (feet).....	1500.0
Culvert Slope (feet per foot).....	0.0140

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
10.0	9.00	1.25	-11.89	0.71	0.92	0.71	6.69
20.0	9.00	1.82	-11.57	1.00	1.32	1.00	8.19
25.0	9.00	2.06	-11.32	1.11	1.48	1.11	8.74
30.0	9.00	2.29	-11.03	1.22	1.62	1.22	9.21
35.0	9.00	2.51	-10.68	1.33	1.76	1.33	9.61
40.0	9.00	2.72	-10.27	1.42	1.89	1.42	9.96
45.0	9.00	2.92	-9.81	1.52	2.01	1.52	10.30
50.0	9.00	3.12	-9.30	1.61	2.12	1.61	10.60
55.0	9.00	3.32	-8.73	1.69	2.23	1.69	10.87
60.0	9.00	3.52	-8.11	1.78	2.33	1.78	11.11
65.0	9.00	3.72	-7.44	1.87	2.43	1.87	11.30
70.0	9.00	3.92	-6.71	1.94	2.53	1.94	11.59
75.0	9.00	4.12	-5.92	2.02	2.62	2.02	11.77
80.0	9.00	4.32	-5.09	2.10	2.71	2.10	11.99
85.0	9.00	4.52	-4.19	2.18	2.79	2.18	12.11
90.0	9.00	4.79	-3.25	2.26	2.88	2.26	12.28
95.0	9.00	5.06	-2.25	2.34	2.95	2.34	12.44
100.0	9.00	5.22	-1.20	2.42	3.03	2.42	12.60
110.0	9.00	5.73	1.07	2.57	3.17	2.57	12.89
120.0	9.00	6.31	3.56	2.75	3.30	2.75	13.05
<u>130.0</u>	9.00	6.94	6.26	2.92	3.41	2.92	13.23
140.0	9.00	7.62	9.18	3.12	3.51	4.00	11.14

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 3, 1992
PAFB BASEWIDE DRAINAGE STUDY
PETERSON BLVD COLLECTOR
42" SECTION BETWEEN SELFRIDGE ST AND ENT AVE

PROGRAM INPUT DATA:

DESCRIPTION	VALUE
Culvert Diameter (feet).....	3.50
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0150
Entrance Loss Coefficient of Culvert Opening.....	0.20
Culvert Length (feet).....	2050.0
Culvert Slope (feet per foot).....	0.0110

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
10.0	7.00	1.31	-15.26	0.78	0.96	0.78	6.24
20.0	7.00	1.92	-14.40	1.11	1.37	1.11	7.61
30.0	7.00	2.45	-12.96	1.38	1.69	1.38	8.51
40.0	7.00	2.94	-10.94	1.62	1.97	1.62	9.21
50.0	7.00	3.42	-8.34	1.85	2.21	1.85	9.67
60.0	7.00	3.91	-5.17	2.07	2.43	2.07	10.13
70.0	7.00	4.52	-1.43	2.30	2.62	2.30	10.47
75.0	7.00	4.76	0.66	2.41	2.71	2.41	10.62
80.0	7.00	5.10	2.90	2.53	2.79	2.53	10.73
85.0	7.00	5.45	5.28	2.67	2.87	2.67	10.80
90.0	7.00	5.83	7.80	2.82	2.94	3.50	9.35
95.0	7.00	6.23	10.46	3.04	3.01	3.50	9.87
100.0	7.00	6.64	13.27	3.50	3.07	3.50	10.39

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 4, 1992
PAFB BASEWIDE DRAINAGE STUDY
48" STORM SEWER
SPACE COMMAND HEADQUARTERS

PROGRAM INPUT DATA:
DESCRIPTION

DESCRIPTION	VALUE
Culvert Diameter (feet).....	4.00
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0130
Entrance Loss Coefficient of Culvert Opening.....	0.20
Culvert Length (feet).....	4200.0
Culvert Slope (feet per foot).....	0.0090

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
100.0	2.00	5.22	-12.86	2.54	3.03	2.54	11.89
105.0	2.00	5.46	-10.63	2.64	3.10	2.64	11.95
110.0	2.00	5.73	-8.30	2.72	3.17	2.72	12.07
115.0	2.00	6.01	-5.85	2.82	3.24	2.82	12.15
120.0	2.00	6.31	-3.31	2.91	3.30	2.91	12.25
125.0	2.00	6.62	-0.65	3.01	3.36	3.01	12.33
130.0	2.00	6.94	2.11	3.06	3.41	3.06	12.59
135.0	2.00	7.27	4.97	3.25	3.46	3.25	12.36
140.0	2.00	7.62	7.94	3.38	3.51	3.51	11.98

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 4, 1992
PAFB BASEWIDE DRAINAGE STUDY
SAND CREEK 54" STORM SEWER
NEAR WEST ENTRANCE TO BASE

PROGRAM INPUT DATA:

DESCRIPTION	VALUE
Culvert Diameter (feet).....	4.50
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0130
Entrance Loss Coefficient of Culvert Opening.....	0.20
Culvert Length (feet).....	1150.0
Culvert Slope (feet per foot).....	0.0150

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
100.0	2.00	4.61	-9.84	2.01	2.94	2.01	14.52
120.0	2.00	5.34	-8.07	2.24	3.22	2.24	15.15
140.0	2.00	6.10	-6.02	2.46	3.48	2.46	15.70
160.0	2.00	7.04	-3.69	2.68	3.70	2.68	16.23
180.0	2.00	8.11	-1.09	2.91	3.89	2.91	16.55
200.0	2.00	9.31	1.79	3.15	4.04	3.15	16.84
220.0	2.00	10.63	4.95	3.38	4.15	3.38	17.16
240.0	2.00	12.08	8.40	3.68	4.24	3.68	17.23

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 4, 1992
PAFB BASEWIDE DRAINAGE STUDY
SAND CREEK 30" STORM SEWER
NEAR WEST ENTRANCE TO BASE

PROGRAM INPUT DATA:

DESCRIPTION	VALUE
Culvert Diameter (feet).....	3.00
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0150
Entrance Loss Coefficient of Culvert Opening.....	0.20
Culvert Length (feet).....	1850.0
Culvert Slope (feet per foot).....	0.0140

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
10.0	1.00	1.38	-23.31	0.78	1.00	0.78	6.90
15.0	1.00	1.74	-22.46	0.95	1.23	0.95	7.75
20.0	1.00	2.07	-21.33	1.11	1.43	1.11	8.40
25.0	1.00	2.38	-19.92	1.25	1.61	1.25	8.92
30.0	1.00	2.69	-18.22	1.39	1.77	1.39	9.35
35.0	1.00	2.99	-16.24	1.52	1.92	1.52	9.72
40.0	1.00	3.30	-13.97	1.65	2.06	1.65	10.06
45.0	1.00	3.70	-11.40	1.78	2.19	1.78	10.31
50.0	1.00	4.00	-8.55	1.91	2.30	1.91	10.55
55.0	1.00	4.42	-5.41	2.04	2.41	2.04	10.76
60.0	1.00	4.88	-1.99	2.17	2.50	2.17	10.97
65.0	1.00	5.38	1.73	2.33	2.59	2.33	11.02
70.0	1.00	5.91	5.73	2.53	2.66	2.53	11.01
75.0	1.00	6.49	10.02	3.00	2.72	2.72	11.14
80.0	1.00	7.11	14.61	3.00	2.77	2.77	11.73

TRAPEZOIDAL CHANNEL ANALYSIS
NORMAL DEPTH COMPUTATION

February 4, 1992
PAFB BASEWIDE DRAINAGE STUDY
PROPOSED EAST SWALE
SECTION OF SWALE EAST OF FAMILY HOUSING

PROGRAM INPUT DATA:
DESCRIPTION

	VALUE
Flow Rate (cubic feet per second).....	250.0
Channel Bottom Slope (feet per foot).....	0.0025
Manning's Roughness Coefficient (n-value).....	0.0300
Channel Side Slope - Left Side (horizontal/vertical)....	3.00
Channel Side Slope - Right Side (horizontal/vertical)...	3.00
Channel Bottom Width (feet).....	15.0

PROGRAM RESULTS:
DESCRIPTION

	VALUE
Normal Depth (feet).....	2.76
Flow Velocity (feet per second).....	3.90
Froude Number (Flow is Sub-Critical).....	0.482
Velocity Head (feet).....	0.24
Energy Head (feet).....	2.99
Cross-Sectional Area of Flow (square feet).....	64.11
Top Width of Flow (feet).....	31.53

TRAPEZOIDAL CHANNEL ANALYSIS
NORMAL DEPTH COMPUTATION

February 4, 1992
PAFB BASEWIDE DRAINAGE STUDY
PROPOSED EAST SWALE
MAXIMUM 100-YEAR FLOW IN SECTION EAST OF GOLF COURSE

PROGRAM INPUT DATA:
DESCRIPTION

	VALUE
Flow Rate (cubic feet per second).....	950.0
Channel Bottom Slope (feet per foot).....	0.0025
Manning's Roughness Coefficient (n-value).....	0.0300
Channel Side Slope - Left Side (horizontal/vertical)....	3.00
Channel Side Slope - Right Side (horizontal/vertical)...	3.00
Channel Bottom Width (feet).....	15.0

PROGRAM RESULTS:
DESCRIPTION

	VALUE
Normal Depth (feet).....	5.40
Flow Velocity (feet per second).....	5.63
Froude Number (Flow is Sub-Critical).....	0.526
Velocity Head (feet).....	0.49
Energy Head (feet).....	5.90
Cross-Sectional Area of Flow (square feet).....	168.69
Top Width of Flow (feet).....	47.43

TRAPEZOIDAL CHANNEL ANALYSIS
NORMAL DEPTH COMPUTATION

February 4, 1992
PAFB BASEWIDE DRAINAGE STUDY
PROPOSED EAST SWALE
SECTION OF SWALE EAST OF GOLF COURSE

PROGRAM INPUT DATA:
DESCRIPTION

	VALUE
Flow Rate (cubic feet per second).....	500.0
Channel Bottom Slope (feet per foot).....	0.0025
Manning's Roughness Coefficient (n-value).....	0.0300
Channel Side Slope - Left Side (horizontal/vertical)....	3.00
Channel Side Slope - Right Side (horizontal/vertical)...	3.00
Channel Bottom Width (feet).....	15.0

PROGRAM RESULTS:
DESCRIPTION

	VALUE
Normal Depth (feet).....	3.94
Flow Velocity (feet per second).....	4.74
Froude Number (Flow is Sub-Critical).....	0.505
Velocity Head (feet).....	0.35
Energy Head (feet).....	4.29
Cross-Sectional Area of Flow (square feet).....	105.55
Top Width of Flow (feet).....	38.62

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 4, 1992
PAFB BASEWIDE DRAINAGE STUDY
60" DIVERSION STORM SEWER
PROPOSED DRAINAGE AREA M

PROGRAM INPUT DATA:

DESCRIPTION	VALUE
Culvert Diameter (feet).....	5.00
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0130
Entrance Loss Coefficient of Culvert Opening.....	0.02
Culvert Length (feet).....	2800.0
Culvert Slope (feet per foot).....	0.0050

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
100.0	3.00	4.27	-5.56	2.62	2.85	2.62	9.59
120.0	3.00	4.83	-3.43	2.94	3.13	2.94	9.98
140.0	3.00	5.40	-0.95	3.25	3.39	3.25	10.36
160.0	3.00	6.11	1.87	3.60	3.63	3.60	10.58
180.0	3.00	6.69	5.05	4.00	3.84	4.00	10.69
<u>200.0</u>	3.00	7.48	8.58	5.00	4.04	4.04	11.78
220.0	3.00	8.35	12.46	5.00	4.21	4.21	12.47
240.0	3.00	9.30	16.69	5.00	4.36	4.36	13.22

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 4, 1992
PAFB BASEWIDE DRAINAGE STUDY

72

PROPOSED DRAINAGE AREAS H AND C

PROGRAM INPUT DATA:

DESCRIPTION	VALUE
Culvert Diameter (feet).....	6.00
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0130
Entrance Loss Coefficient of Culvert Opening.....	0.02
Culvert Length (feet).....	1600.0
Culvert Slope (feet per foot).....	0.0075

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
100.0	4.00	3.84	-6.57	2.14	2.69	2.14	11.05
120.0	4.00	4.29	-5.96	2.36	2.96	2.36	11.59
140.0	4.00	4.73	-5.27	2.57	3.21	2.57	12.11
160.0	4.00	5.17	-4.50	2.77	3.44	2.77	12.51
180.0	4.00	5.60	-3.65	2.97	3.66	2.97	12.92
200.0	4.00	6.03	-2.73	3.16	3.86	3.16	13.24
220.0	4.00	6.47	-1.72	3.35	4.06	3.35	13.55
240.0	4.00	6.91	-0.63	3.53	4.24	3.53	13.88
260.0	4.00	7.55	0.54	3.73	4.42	3.73	14.08
280.0	4.00	7.92	1.80	3.92	4.58	3.92	14.31
300.0	4.00	8.50	3.13	4.31	4.73	4.31	13.79
320.0	4.00	9.12	4.55	4.35	4.88	4.35	14.58
340.0	4.00	9.77	6.05	4.57	5.01	4.57	14.72

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 4, 1992
PAFB BASEWIDE DRAINAGE STUDY
48" STORM SEWER
PROPOSED DRAINAGE AREA K

PROGRAM INPUT DATA:

DESCRIPTION	VALUE
Culvert Diameter (feet).....	4.00
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0130
Entrance Loss Coefficient of Culvert Opening.....	0.02
Culvert Length (feet).....	2800.0
Culvert Slope (feet per foot).....	0.0050

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
20.0	2.00	1.82	-10.76	1.21	1.32	1.21	6.23
25.0	2.00	2.06	-10.36	1.36	1.48	1.36	6.67
30.0	2.00	2.29	-9.88	1.49	1.62	1.49	7.04
35.0	2.00	2.51	-9.34	1.62	1.76	1.62	7.33
40.0	2.00	2.72	-8.74	1.74	1.89	1.74	7.61
45.0	2.00	2.92	-8.06	1.86	2.01	1.86	7.84
50.0	2.00	3.12	-7.32	1.98	2.12	1.98	8.05
55.0	2.00	3.32	-6.50	2.10	2.23	2.10	8.25
60.0	2.00	3.52	-5.61	2.21	2.33	2.21	8.40
65.0	2.00	3.72	-4.66	2.33	2.43	2.33	8.58
70.0	2.00	3.92	-3.63	2.44	2.53	2.44	8.72
75.0	2.00	4.12	-2.54	2.56	2.62	2.56	8.84
80.0	2.00	4.32	-1.37	2.68	2.71	2.68	8.95
85.0	2.00	4.52	-0.13	2.80	2.79	2.80	9.03
90.0	2.00	4.79	1.18	2.93	2.88	2.93	9.14
95.0	2.00	5.06	2.56	3.07	2.95	3.07	9.19
100.0	2.00	5.22	4.01	3.22	3.03	3.22	9.22
<u>110.0</u>	2.00	5.73	7.13	4.00	3.17	3.17	10.30
<u>120.0</u>	2.00	6.31	10.52	4.00	3.30	3.30	10.83

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 4, 1992
PAFB BASEWIDE DRAINAGE STUDY
54" STORM SEWER
PROPOSED DRAINAGE AREA H

PROGRAM INPUT DATA:

DESCRIPTION	VALUE
Culvert Diameter (feet).....	4.50
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0130
Entrance Loss Coefficient of Culvert Opening.....	0.02
Culvert Length (feet).....	1500.0
Culvert Slope (feet per foot).....	0.0050

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
50.0	8.00	2.93	1.62	1.86	2.05	1.86	8.03
60.0	8.00	3.27	2.11	2.07	2.25	2.07	8.40
70.0	8.00	3.61	2.70	2.26	2.44	2.26	8.74
80.0	8.00	3.94	3.37	2.45	2.62	2.45	9.04
90.0	8.00	4.28	4.13	2.62	2.78	2.62	9.37
100.0	8.00	4.61	4.98	2.82	2.94	4.50	6.29
110.0	8.00	4.94	5.92	3.02	3.09	4.50	6.92
120.0	8.00	5.34	6.96	3.22	3.22	4.50	7.55
130.0	8.00	5.77	8.08	3.45	3.36	4.50	8.17
<u>140.0</u>	8.00	6.10	9.29	3.71	3.48	4.50	8.80
150.0	8.00	6.56	10.59	4.50	3.59	4.50	9.43
160.0	8.00	7.04	11.98	4.50	3.70	4.50	10.06

PIPE CULVERT ANALYSIS
COMPUTATION OF CULVERT PERFORMANCE CURVE

February 3, 1992
PAFB BASEWIDE DRAINAGE STUDY
OTIS STREET COLLECTOR
21" SECTION BETWEEN ENT AVE AND HAMILTON AVE

PROGRAM INPUT DATA:

DESCRIPTION	VALUE
Culvert Diameter (feet).....	1.75
FHWA Chart Number (1,2 or 3).....	1
Scale Number on Chart (Type of Culvert Entrance).....	1
Manning's Roughness Coefficient (n-value).....	0.0150
Entrance Loss Coefficient of Culvert Opening.....	0.20
Culvert Length (feet).....	1200.0
Culvert Slope (feet per foot).....	0.0080

PROGRAM RESULTS:

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
4.0	8.00	1.03	-0.54	0.69	0.73	0.69	4.55
6.0	8.00	1.34	0.79	0.86	0.92	0.86	5.07
8.0	8.00	1.60	2.66	1.03	1.05	1.75	3.33
10.0	8.00	1.87	5.05	1.20	1.18	1.75	4.16
<u>12.0</u>	8.00	2.21	7.98	1.40	1.29	1.75	4.99
14.0	8.00	2.52	11.43	1.75	1.39	1.75	5.82
16.0	8.00	2.93	15.42	1.75	1.48	1.75	6.65

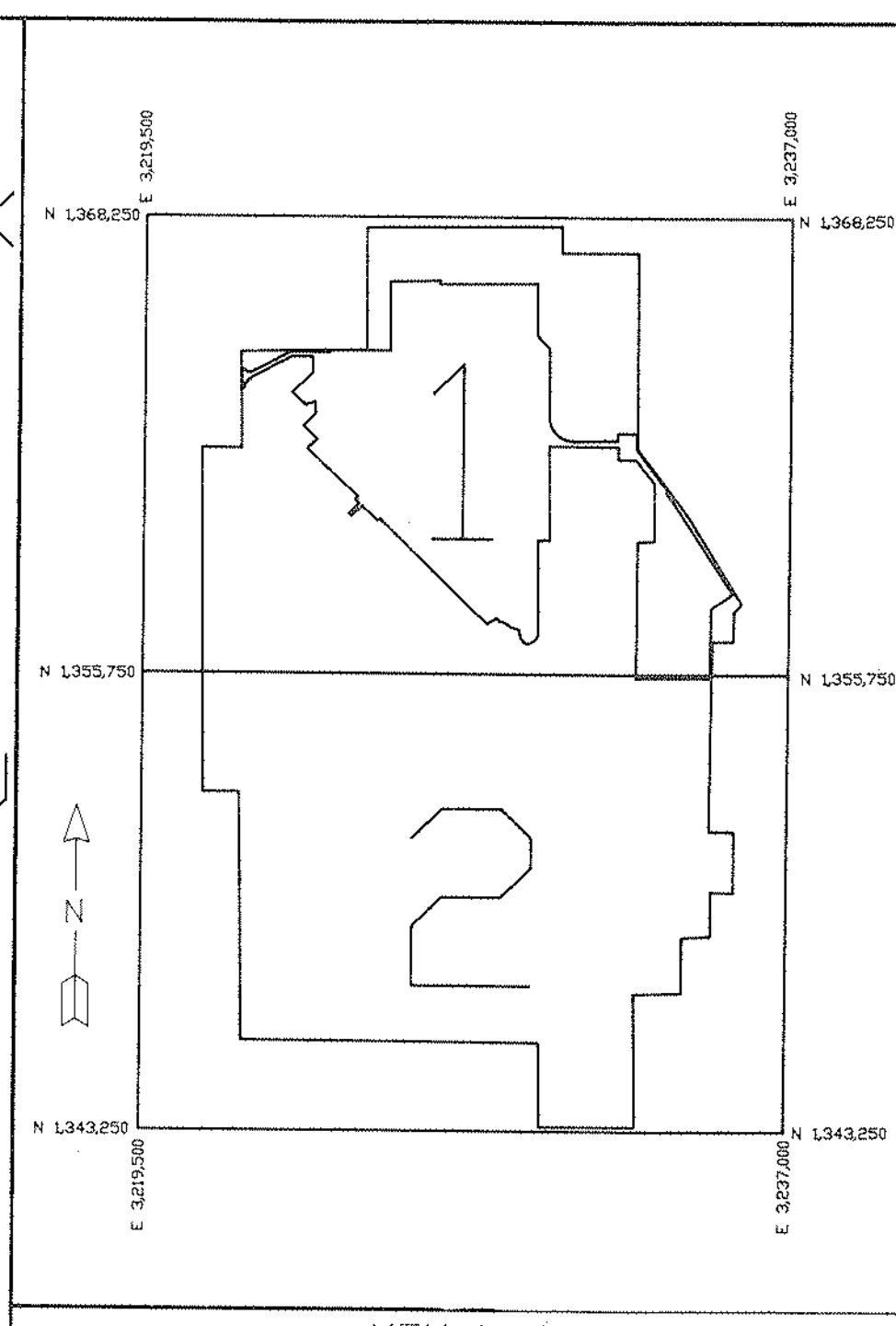


TABLE 1
EXISTING MAJOR DRAINAGE COLLECTOR

COLLECTOR	EXISTING CAPACITY (CFS)	EXISTING FLOWS (CFS) 10-YEAR	EXISTING FLOWS (CFS) 100-YEAR
Hamilton Avenue - Peterson to Mitchell - Mitchell to Det. Pond #3	250	262	536
	310	316	662
Mitchell Street	60	73	213
Peterson Boulevard	130	152	277
Space Command 48"	125	64	133
Sand Creek 54"	220	102	257
Sand Creek 30"	70	63	134

DRAINAGE AREA	AREA (MILES ²)	LAG (HRS)	% IMP. COVER	CURVE NUMBER
A	0.0741	0.22	20	68
B	0.4568	0.65	30	68
C	0.0227	0.09	90	94
D	2.2121	0.41	40	76
E	0.1257	0.19	75	97
F	0.0885	0.22	50	89
G	0.2985	0.39	40	72
H	0.0799	0.19	50	89
I	0.2561	0.72	10	65

- LEGEND
- ▨ DRAINAGE AREA BOUNDARY
 - ⊙ DRAINAGE AREA
 - INDEX CONTOUR
 - ~ INDEX DEPRESSION CONTOUR
 - ~ INTERMEDIATE CONTOUR
 - ~ INTERMEDIATE DEPRESSION CONTOUR
 - RETAINING WALL
 - x- FENCE
 - ⊠ RADIOD TOWER
 - ▲ BENCHMARK
 - FAIRWAY
 - 2001 P PERMANENT BUILDING
 - 2001 S SEMI-PERMANENT BUILDING
 - 2001 T TEMPORARY BUILDING
 - EXISTING STORM SEWER
 - PROPOSED DRAINAGE IMPROVEMENTS

TRUE NORTH
MAG. DEC. 11° 08'

ANNUAL CHANGE: 7.3' WEST

500 0 500 1000
SCALE IN FEET

AIRFIELD ELEVATION 6172 FT.
CONTOUR INTERVAL: 5 FT.

REV	DATE	DESCRIPTION	INITIAL
PLAN REVISIONS			

DEPARTMENT OF THE AIR FORCE
DIRECTORATE OF ENGINEERING & SERVICES DCS/LES - WASHINGTON, D.C.

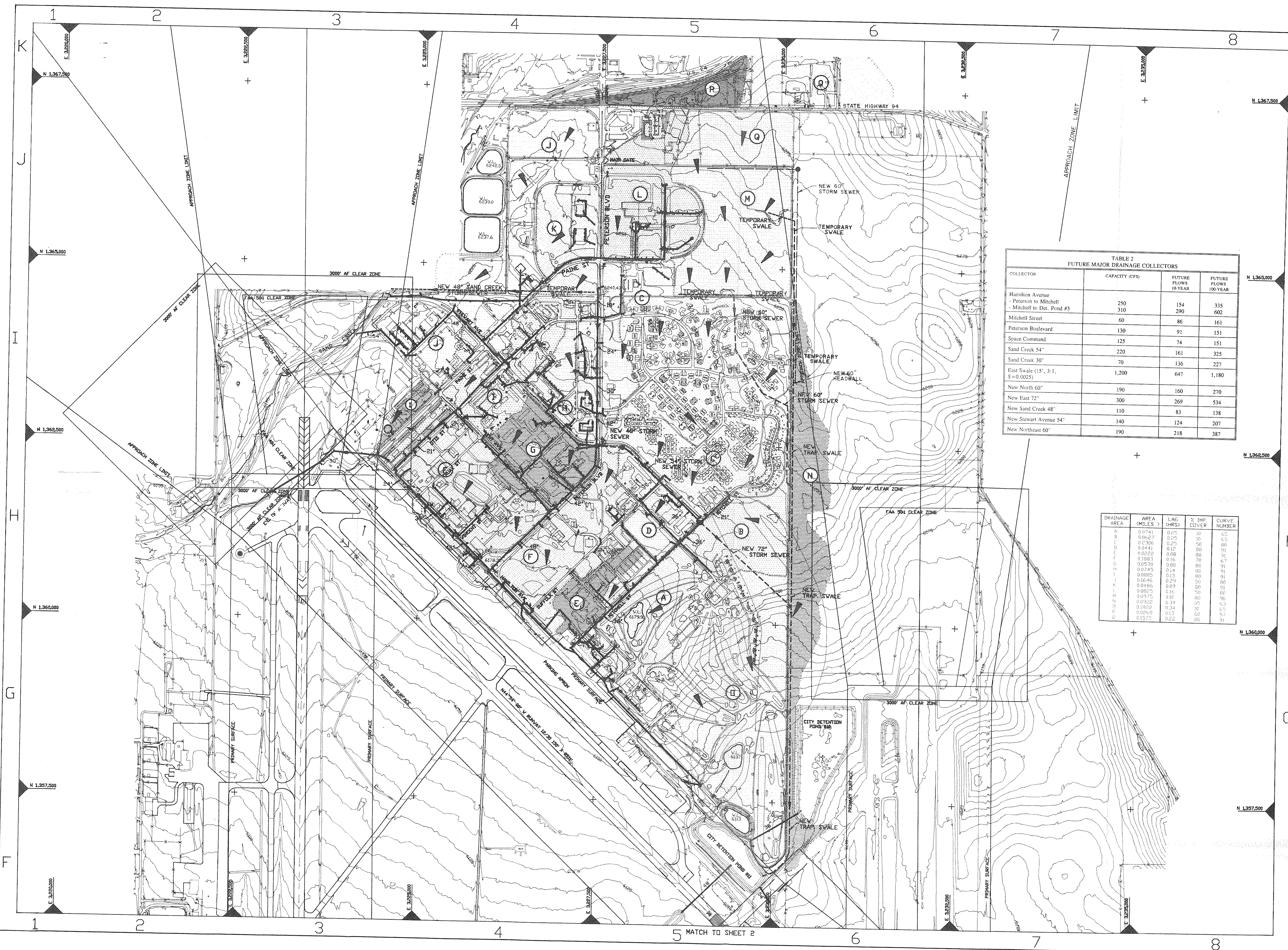
AIR FORCE SPACE COMMAND

COMPREHENSIVE PLAN
TAB G-3.1, EXISTING
STORM DRAINAGE MAP
PETERSON AIR FORCE BASE
COLORADO SPRINGS, COLORADO

SCALE: 1" = 500 FT. 2 APRIL 92
BASE COMPREHENSIVE PLAN DIRECTIVE AFR 86-4
ANALYTICAL SURVEYS, INC. COLORADO SPRINGS, COLORADO

SHEET 1 OF 1

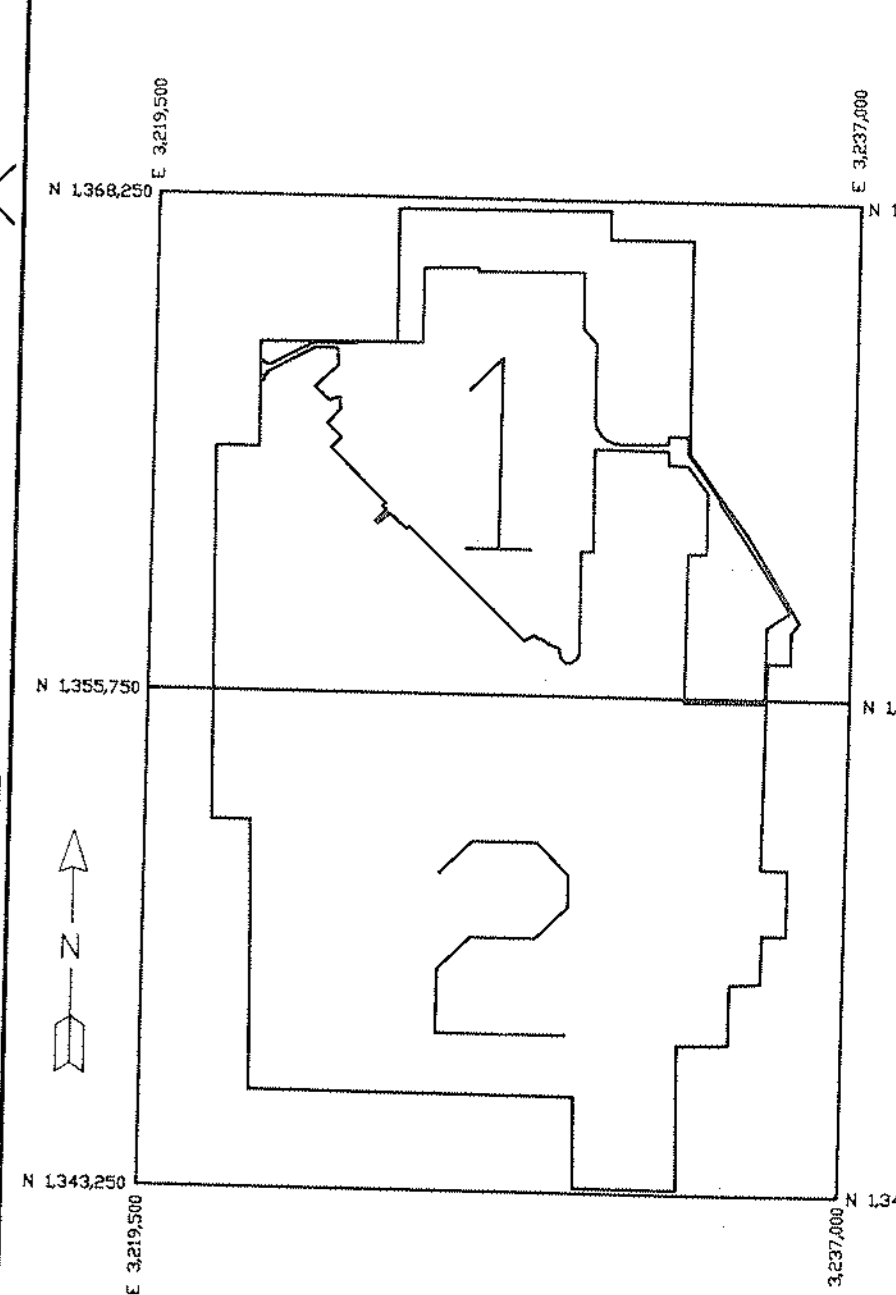
FIGURE 1



**TABLE 2
FUTURE MAJOR DRAINAGE COLLECTORS**

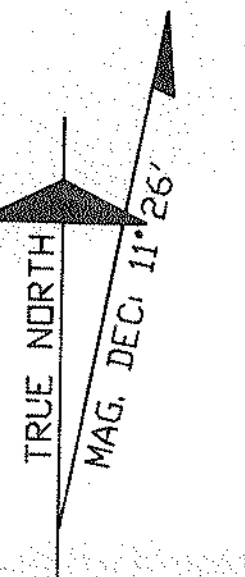
COLLECTOR	CAPACITY (CFS)	FUTURE FLOWS 10-YEAR	FUTURE FLOWS 100-YEAR
Hamilton Avenue - Peterson to Mitchell	250	154	335
Mitchell to Det. Pond #3	310	290	602
Mitchell Street	60	86	161
Peterson Boulevard	130	91	151
Space Command	125	74	151
Sand Creek 54"	220	161	325
Sand Creek 30"	70	136	227
East Swale (15', 3:1, S=0.0025)	1,200	647	1,180
New North 60"	190	160	270
New East 72"	300	269	534
New Sand Creek 48"	110	83	138
New Stewart Avenue 54"	140	124	207
New Northeast 60"	190	218	387

DRAINAGE AREA	AREA (MILES ²)	LAG (HRS)	% IMP COVER	CURVE NUMBER
A	0.0741	0.25	10	65
B	0.0627	0.25	90	65
C	0.2306	0.25	90	80
D	0.0441	0.12	80	91
E	0.0222	0.08	80	91
F	0.1983	0.16	70	67
G	0.0539	0.08	80	91
H	0.0745	0.14	80	91
I	0.0895	0.13	80	91
J	0.1646	0.29	50	80
K	0.0486	0.09	50	80
L	0.0825	0.16	50	80
M	0.0975	0.10	80	96
N	0.0922	0.24	10	63
O	0.1922	0.34	10	63
P	0.0268	0.13	60	57
Q	0.1275	0.22	85	91



- KEY MAP**
- DRAINAGE AREA BOUNDARY
 - DRAINAGE AREA
 - INDEX CONTOUR
 - INTERMEDIATE CONTOUR
 - INTERMEDIATE DEPRESSION CONTOUR
 - RETAINING WALL
 - FENCE
 - RADIO TOWER
 - BENCHMARK
 - FAIRWAY
 - PERMANENT BUILDING
 - SEMI-PERMANENT BUILDING
 - TEMPORARY BUILDING
 - EXISTING STORM SEWER
 - PROPOSED DRAINAGE IMPROVEMENTS

LEGEND



ANNUAL CHANGE: 7.3' WEST

SCALE IN FEET

AIRFIELD ELEVATION 6172 FT.
CONTOUR INTERVAL: 5 FT.

REV DATE	DESCRIPTION	INITIAL

DEPARTMENT OF THE AIR FORCE
DIRECTORATE OF ENGINEERING & SERVICES DCS/LEE - WASHINGTON, DC

AIR FORCE SPACE COMMAND

**COMPREHENSIVE PLAN
TAB G-3.2, FUTURE
STORM DRAINAGE PLAN**
PETERSON AIR FORCE BASE
COLORADO SPRINGS, COLORADO

SCALE: 1" = 500 FT., 2 APRIL 92
BASE COMPREHENSIVE PLAN DIRECTIVE AFR 86-4
ANALYTICAL SURVEYS, INC. COLORADO SPRINGS, COLORADO

TAB NO. G-3.2
SHEET 1 OF 1

FIGURE 2