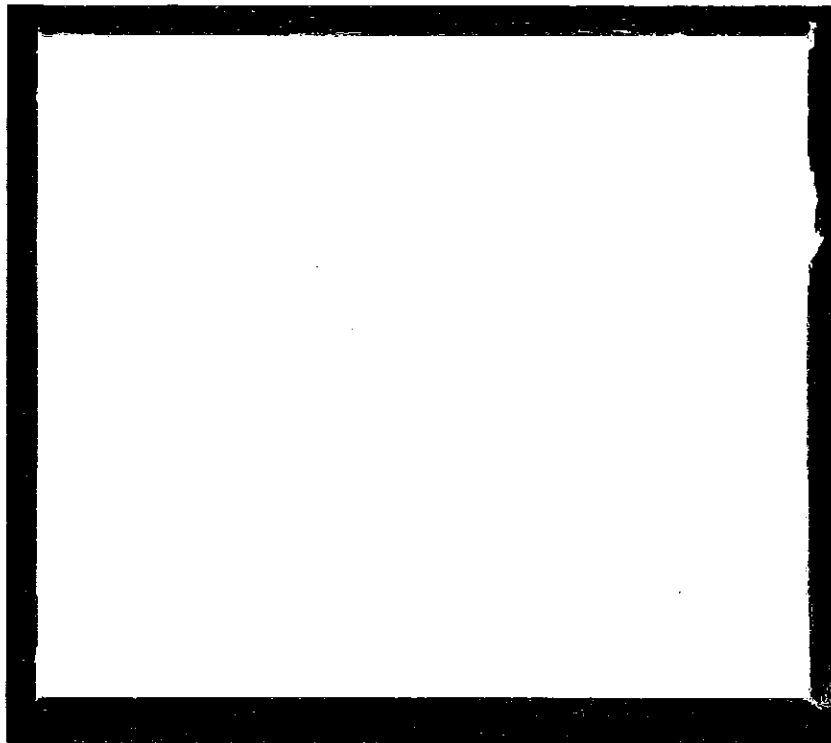


Broadmoor Bluffs Cst.



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COLORADO SPRINGS

DEC 19 1984

8,9,10,11,12,1,2,3,4,5,6

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COLORADO SPRINGS, CO
(719) 578-6212



DREXEL, BARRELL & CO.

ENGINEERS — SURVEYORS

1700 38TH STREET

BOULDER, COLORADO 80301

(303) 442-4338

MICROFICHED

FINAL DRAINAGE REPORT
FOR THE
SINGLE-FAMILY PORTION
OF
BROADMOOR BLUFFS ESTATES
COLORADO SPRINGS, COLORADO

PREPARED BY:

DREXEL, BARRELL & CO.
1700 38TH STREET
BOULDER, COLORADO 80301
(303) 442-4338

PREPARED FOR:

GATES LAND COMPANY
155 WEST LAKE AVENUE
COLORADO SPRINGS, CO 80906
(303) 829-5950

DECEMBER 12, 1984
E-3098
(0177R)

TABLE OF CONTENTS

<u>SUBJECT</u>	<u>PAGE</u>
Certifications	1
Floodplain Statement	2
Drainage Report	3
Location	3
Intent	3
Design References	3
Existing Drainage Characteristics	4
Design Drainage Characteristics	4
Conclusion	6
Appendix	7

APPENDICES

<u>SUBJECT</u>	<u>EXHIBIT</u>
Vicinity Map	A
Vicinity Map (U.S.G.S.)	A1
Hydrologic Soils Map	B
Individual Basin Data Summary Sheet	C
Individual Basin Flow Calculations	C1 thru 8
Street Flow Data Summary Sheet	D
Street Flow Analysis Calculations	D1 thru 24
Combined Basin Flow Data Summary Sheet	E
Combined Basin Flow Calculations	E1 thru 8
Storm Sewer Sizing Calculations	F1 thru 8
Proposed Drainage Structures Cost Estimate	G

DRAWINGS (Back Insert)

Final Drainage Plan

Dwg No. 3D 529

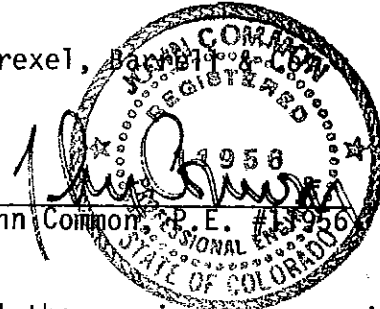
CERTIFICATIONS

The attached drainage plan and report, "Final Drainage Report for the Single-Family portion of Broadmoor Bluffs Estates", were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City for drainage reports and said report is in conformity with the Master Plan of the drainage basin. I accept responsibility for any liability caused by the negligent acts, errors, or omissions on my part in preparing this report.

For: Drexel, ~~James~~

By:

John Common, P.E. #18956



The developer has read and will comply with all the requirements specified in this drainage report as approved by the City Engineer.

By:

Robert F. Svejksky

Robert F. Svejksky

Title: Director of Engineering

Address: Gates Land Company

155 West Lake Avenue

Colorado Springs, CO 80906

City of Colorado Springs:

Filed in accordance with Section 15-3-906 of the Code of the City of Colorado Springs, 1980 as amended.

City Engineer:

John City Comm

Date:

1/9/85

Conditions:

FLOODPLAIN STATEMENT

The single-family portion of Broadmoor Bluffs Estates, as platted, does not lie in a designated special flood hazard area as indicated on the map index of the Flood Hazard Boundary Map H-01-35, for the City of Colorado Springs, prepared by the Department of Housing and Urban Development, Federal Insurance Administration (Community No. 080060A; latest revision 4/4/78).

FINAL DRAINAGE REPORT
FOR THE
SINGLE-FAMILY PORTION
OF
BROADMOOR BLUFFS ESTATES
COLORADO SPRINGS, COLORADO

LOCATION

Broadmoor Bluffs Estates is a proposed sixty-lot single-family residential and park development. The Subdivision, approximately 59.22 acres, is located in the SE1/4 of the SE1/4 of Section 6, and in the NE1/4, the East 1/2 of the NW1/4 and the NE1/4 of the SW1/4 of Section 7, all in T15S, R66W of the 6th P.M., Colorado Springs, Colorado. More generally, the area lies west of Colorado State Highway No. 115, across from the Fort Carson Military Reservation. It is bounded on the north by Broadmoor Bluffs Park Filing No. 2 and 4; on the west by Broadmoor Bluffs Park Filing No. 8 and Neal Ranch Filing No. 2. The remaining surrounding properties are unplatted and owned by Gates Land Company.

INTENT

A previous report entitled "Final Drainage Report for Broadmoor Bluffs Drive and Farthing Drive and Preliminary Drainage Report for the Single-Family Portion of Broadmoor Bluffs Estates" was submitted to the City of Colorado Springs and approved on September 24, 1984. (Ref: Drexel, Barrell & Co. Drawing-No. 3D 470 dated August 16, 1984 - Job No. E-3098).

The intent of this report is to finalize the study of the single-family area and establish the necessary drainage facilities required for the development of the subdivision.

Overall master drainage studies establishing guidelines for the preliminary and final reports on the single-family area, include the "Master Drainage Study for Cheyenne Mountain Ranch" prepared by Hartzell-Pfeiffenberger and Associates, Inc. dated May 17, 1971, and the "Master Drainage Report for Basin IV, IV-A, IV-B and VII-B, Cheyenne Mountain Ranch" prepared by Drexel, Barrell & Co. dated July 18, 1983. Tributary flows from the west were taken from the "Drainage Study for Neal Ranch Filing 2, Broadmoor Bluffs Park Filing No. 8, and Farthing Drive" prepared by KKBNA, Inc. in June 1984. A drainage report for "Broadmoor Bluffs Park Filing No. 4", prepared by Guenther Polok on May 10, 1982 was referenced for consistency of flows to the north.

Drainage patterns established in this final study are consistent with those established in the master reports and subsequent surrounding development analysis.

DESIGN REFERENCES

In addition to the previously mentioned drainage studies, the drainage design criteria was taken from the City of Colorado Springs "Determination of

Storm Runoff Criteria" manual. Flows were determined for the 6 hour initial 5 year, and major 100 year rainfalls. No flows over 500 cfs occur, so culverts were sized to pass the 5 year flows with no backwater and pass the 100 year flows with no overtopping of the curbs. Storm sewers were provided so as to not allow the initial rainfall to exceed 12 cfs within the 1/2 street flow and allow the major 100 year flows to be channelized within the rights-of-way.

Flows were analyzed using the modified SCS Method. Hydrologic soils groups were determined from maps published by the Soil Conservation Service.

The permissible drainage street capacities for 28 feet and 32 feet street widths, with 8" vertical curbs, are not listed in Table 5 of the Storm Runoff criteria; therefore, the method for determining theoretical and allowable curb flows is as described in the Denver Regional Council of Governments "Urban Storm Drainage Criteria Manual" as taken from the Bureau of Public Roads Publications. This method utilizes a nomograph for flow in triangular gutters to determine theoretical capacity then applies a reduction factor to arrive at an allowable capacity. The nomograph and reduction graph have been included with the calculations for your review.

EXISTING DRAINAGE CHARACTERISTICS

Two drainage swales carry flows easterly across the single-family area. Flow line grades vary from 5% to 25% and side slopes generally vary from 2:1 (2 horizontal to 1 vertical) to 5:1. The existing swales have naturally eroded to a rocky terrain and are mostly heavily vegetated with scrub oak and natural grasses. These swales define two major drainage basins in historical runoff.

As designed with the drainage report for Farthing and Broadmoor Bluffs Drives, the southerly swale parallels Farthing Drive and outfalls under Broadmoor Bluffs Drive through a 48" RCP; the northerly swale continues easterly to a 60" RCP under Broadmoor Bluffs Drive, north of the Academy interchange with Colorado State Highway No. 115. Some temporary swales have been constructed in the unplatted areas, east of the single-family platting, directing these swale flows to the previously mentioned outfalls under Broadmoor Bluffs Drive.

Existing site conditions in the single-family area are largely dense scrub oak on slopes ranging from 10 to 40% (10:1 to 2.5:1). The soils are predominantly of the Razor Series with some Jarre Tecolote Series existing along the steeper slopes of the western and northern portions of the platted lots.

At the present time, Farthing and Broadmoor Bluffs Drives are under construction with the proposed drainage structures as shown in that report partially in place.

DESIGN DRAINAGE CHARACTERISTICS

As previously mentioned, the two drainage swales across the single-family area define major runoff basins.

Approximately 39.9 offsite acres (Basins 1 and 2) are tributary to the two forks of the southern swale. Proposed grading along Cardiff Circle allows the runoff through major Basin "B" to be conveyed under the street. A 30" RCP is proposed to pass the 5 year flow of 15 cfs with a flow depth of 22-1/2". The 100 year flow of 48.9 cfs will require a headwater depth of 60". However this does not approach the street level nor encroach the proposed building envelope for Lot 43. Proposed runoff through minor Basin "C2" will be picked up by a storm sewer system and be directed into Basin "G". The storm sewer is designed to convey the 100 year flow of 44.2 cfs so as to not run over onto Gloucester Court. Again, grading along Cardiff Circle will allow for runoff in minor Basin "C3" to be passed through the storm sewer under the street.

The above two forks converge through major Basin "G" and will pass under Cardiff Circle again, through a 48" RCP. The 5 year flow of 37 cfs will require a headwater depth of 31" and a 62" headwater depth will be necessary for the 100 year flow of 107.8 cfs. These flows continue through minor Basin "J1" to a temporary swale section, east of the subdivision, provided with the drainage report for Farthing and Broadmoor Bluffs Drives.

Typical swale sections in Basins "B, C2 & G" shows Manning's flow depths for the 100 year runoff approximately 15" to 18" with velocities of 3 to 4 fps. All existing drainage swales are to remain natural except in areas where drainage structures are proposed.

Approximately 46.5 offsite acres (Basins 3, 4 & 5) are tributary to the northerly swale. The swale proceeds easterly through minor Basin E1 and does not cross any proposed streets. The 5 year flow of 42.9 cfs and 100 year flow of 127 cfs passes onto the unplatted land of Gates Land Company and eventually to the 60"-RCP under Broadmoor Bluffs Drive previously mentioned. A Manning's section at the end of Reginold Court shows 100 year flow depths of 36" with a velocity of 5.3 fps.

Access to residential lots at the ends of Cheshire and Reginold Courts will be across the northerly swale section and the means to cross this swale will be detailed with the respective lot development plan, as required by the City in hillside areas at the time of building permit application.

As shown on the drainage plan approximately 19 acres are tributary to the proposed street system and result in curb flow. The ultimate outfall along Cardiff Circle is the proposed sump inlets before Farthing Drive, and at the sump inlet at the end of Reginold Court. Intermediate inlets, on grade, at Cheshire Court and Cardiff Circle at minor Basin "C4" were designed to reduce the eventual down street peak flows at Reginold Court.

Theoretically, the southerly 1/2 of Cardiff Circle and Basins "F2/F3" are flowing to the sump condition in Cardiff Circle. Note: Cardiff Circle is on straight grade from the western intersection at Farthing Drive to the sump conditions before the eastern intersection with Farthing Drive. Gloucester, Cheshire, and Churchill Courts are uphill cul-de-sacs. Reginold Court is a downhill cul-de-sac. The northerly portion of Cardiff Circle, including Basins C1, C4, D1, D2, E2, E3 and E4, drain to the end of Reginold Court.

Calculations indicate the street flows in the north half of Cardiff Circle will spill into Reginold Court and not proceed southerly on Cardiff Circle.

The theoretical street capacities determined were reduced, significantly in some cases, using the recommended reduction factors. The allowable 1/2 street capacity was then determined to be adequate to contain even the 100 year flows. It is felt in this situation the reduction factors may not apply in all situations. The relative narrowness of the streets and expected lengths of driveways more likely generate a condition where on street parking will not occur and certainly not on both sides of a street. Therefore the applied reduction factors, accounting for flow obstruction primarily due to parked cars, probably act more as a safety factor than as a design reduction factor. Therefore, it could be assumed even the 100 year storm flows do not overtop the crown of the street; but for design analysis the reduction factors were applied.

Most of the curb inlets designed were upsized to the next inlet width to help alleviate runoff from the infrequent storms that seem common in the Colorado Springs area. This should help to even further reduce the 5 year storm flows. But this upsizing of inlets was not accounted for in the five year street flow analysis, a conservative approach.

Minimum 18" diameter rip-rap has been provided at culverts to protect against erosion and scouring. The 18" rock diameter should prevent mischevious displacement. Bedding details and bed sizes will be provided along with the street construction plans, as will culvert inverts and construction details.

CONCLUSION

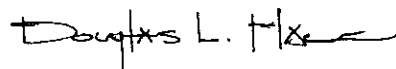
This study generates the storm flows through the single-family area and the adequate drainage improvements necessary to convey the runoff.

Basin runoff and flow patterns are consistant with the applicable Master Drainage Studies, on file with the City of Colorado Springs, as well as the preliminary drainage plan for the area.

Copies of the calculations, with support material, are included for your review. The estimated drainage structure costs are included as Exhibit "G". By agreement with the City of Colorado Springs, no drainage basin fees are paid by Gates Land Company. The proposed drainage facilities will be built and paid for by Gates Land Company.

A copy of the Drainage Plan, Drexel, Barrell & Co. Drawing No. 3D .529-Sheet 1 of 1, has been included in the insert.

Respectfully submitted,



Douglas L. Mann

Drexel, Barrell & Co.

APPENDIX

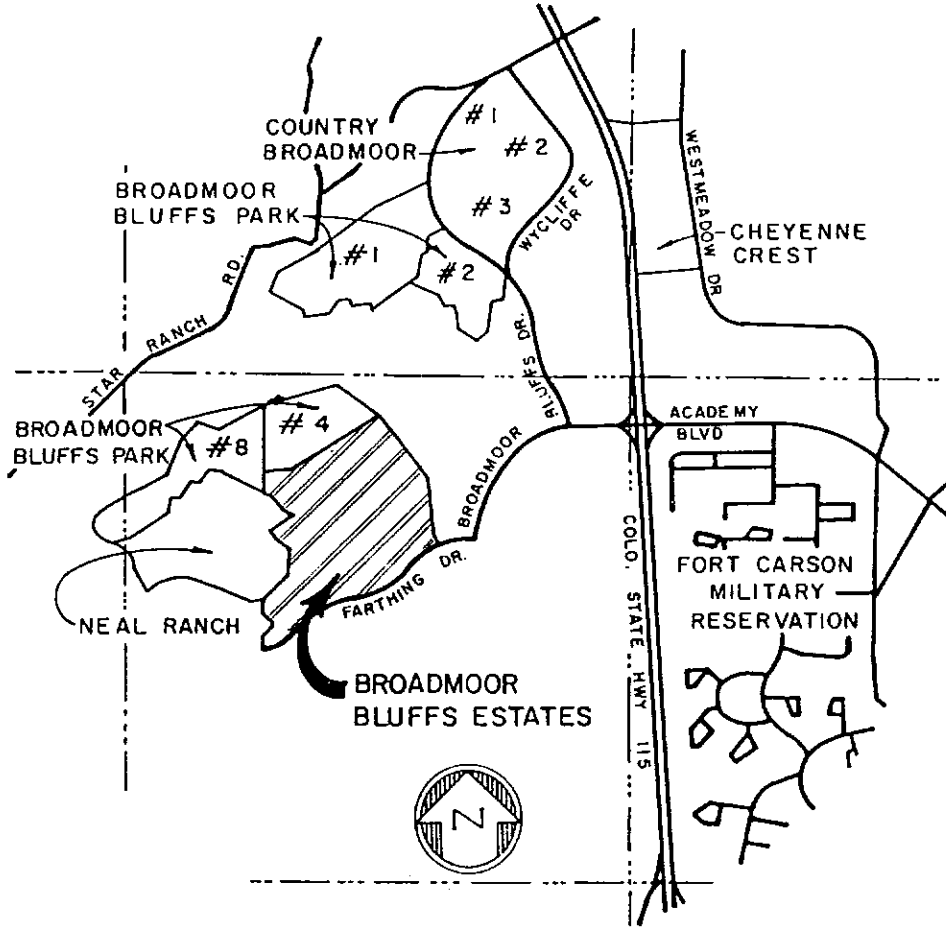
<u>SUBJECT</u>	<u>EXHIBIT</u>
Vicinity Map	A
Vicinity Map (U.S.G.S.)	A1
Hydrologic Soils Map	B
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Proposed Drainage Structures Cost Estimate	G

DRAWINGS (Back Insert)

Final Drainage Plan

Dwg No. 3D 529

EXHIBIT "A"



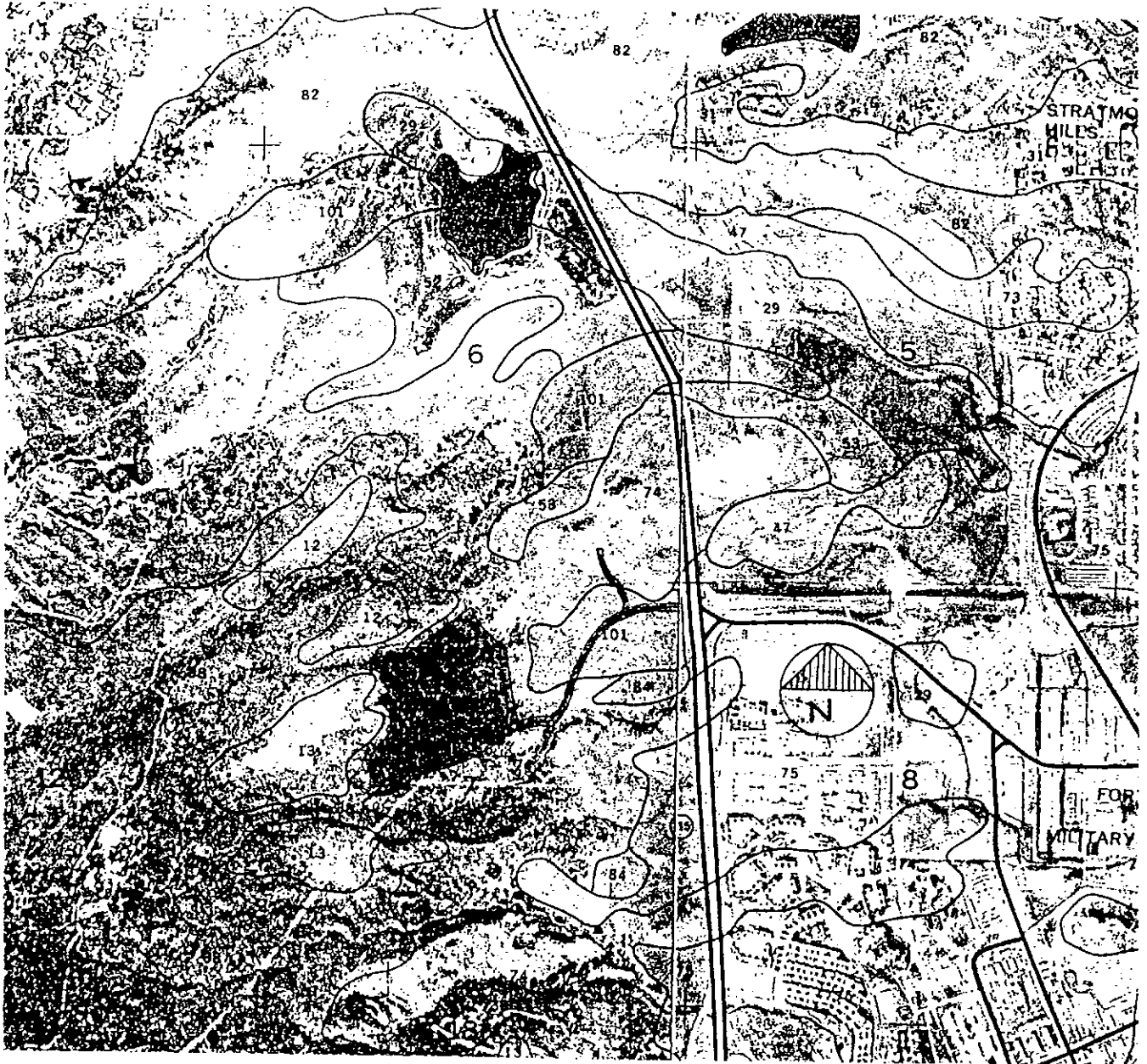
VICINITY MAP

SCALE - 1" = 2000'

BENCH MARKS

GATES GRID NO. 55,000 N
105,000 E
ELEVATION = 5959.26 (U.S.G.S.)

EXHIBIT "B"



SOILS MAP

SCALE : 1" = 2000'

SEE NEXT PAGE FOR
DESCRIPTIONS.

EXHIBIT "B"
HYDROLOGIC SOILS GROUPS
FOR
BROADMOOR BLUFFS ESTATES STUDY

<u>No.</u>	<u>Classification</u>	<u>Hydrologic Group</u>
12	Bresser	B
13	Bresser	B
38	Jarre Tecolote Series	B
74	Razor	C
84	Stapleton	B
101	Ustic Torrfluvents	B

EXHIBIT "C"
INDIVIDUAL BASIN FLOW ANALYSIS

EXHIBIT "C"
INDIVIDUAL BASIN DATA SUMMARY SHEET

<u>Basin Designation</u>	<u>Area (ac.)</u>	<u>CN</u>	<u>Tc (hr)</u>	<u>Q5 (in)</u>	<u>Q100 (in)</u>	<u>qp (csm/in)</u>	<u>q5 (cfs)</u>	<u>q100 (cfs)</u>
B	4.86	74	0.10	0.40	1.24	1280	3.9	12.1
C1	3.84	75	0.10	0.44	1.30	1280	3.4	10.0
C2	1.50	72	0.10	0.34	1.12	1280	1.0	3.4
C3	1.12	80	0.10	0.62	1.64	1280	1.4	3.7
C4	0.36	98	0.10	1.87	3.27	1280	1.3	2.4
D1	1.93	80	0.12	0.62	1.64	1240	2.3	6.1
D2	4.30	76	0.16	0.47	1.36	1140	3.6	10.4
E1	12.87	76	0.12	0.47	1.36	1220	11.5	33.4
E2	0.56	98	0.10	1.87	3.27	1280	2.1	3.7
E3	3.06	80	0.10	0.62	1.64	1280	3.8	10.0
E4	0.49	98	0.10	1.87	3.27	1280	1.8	3.2
F1	1.35	92	0.11	1.33	2.64	1260	3.5	7.0
F2	3.21	80	0.10	0.62	1.64	1280	4.0	10.5
F3	0.40	98	0.10	1.87	3.27	1280	1.5	2.6
G	9.02	77	0.23	0.51	1.43	1020	7.3	20.6
J1	4.10	80	0.10	0.62	1.64	1280	5.1	13.5

Project: BROADMOOR BLUFFS ESTATES EXHIBIT "C" Job No: E 3098

Client: GATES LAND CO. By: djm Date: DEC 10, 1984

CAD: MOORE 12-14-84

INDIVIDUAL BASIN FLOWS

BASIN A FLOWS TO FARTHING. IS PART OF DRAINAGE REPORT APPROVED FOR BROADMOOR BLUFFS & FARTHING DRIVES.
 RE: $Q_5 = 4.2 \text{ cfs}$ $Q_{100} = 11.6 \text{ cfs}$

BASIN B AREA = 4.86 AC.

SOIL GROUP	ACREAGE	USE	CN	%	%CN
38(B)	2.98	R 1/2	70	61.3	42.9
74(C)	1.88	R 1/2	80	38.7	30.9
	4.86			100	74

T_c : 125' OVERLAND AT 37% (2 fps) 1.0 MIN
 520' NATURAL SWALE AT 10% (4 fps) 2.2 MIN

$T_c = 3.2 \text{ MIN.} \approx 0.1 \text{ h}$

$q_p = 1280 \text{ csm/in}$

$Q_5 = 0.4 \text{ IN}$ $Q_{100} = 1.24 \text{ IN}$

$q_5 = 1280 \times 4.86 / 640 \times 0.4 = 3.9 \text{ cfs}$ $QA / 640 = .0030$

$q_{100} = 1280 \times 4.86 / 640 \times 1.24 = 12.1 \text{ cfs}$ $100 .0094$

BASIN C AREA = 3.84 AC.

SOIL GROUP	ACREAGE	USE	CN	%	%CN
38(B)	1.93	R 1/2	70	50.3	35.2
74(C)	1.91	R 1/2	80	49.7	39.8
	3.84			100	75

T_c : 200 LF OVERLAND AT 35% (2 fps) 1.7 MIN
 120 LF OVERLAND AT 16% (1.4 fps) 1.4 MIN
 250 LF CURB FLOW AT 2% (2.8 fps) 1.5 MIN

$q_p = 1280 \text{ csm/in}$

$Q_5 = 0.44 \text{ IN}$ $Q_{100} = 1.30 \text{ IN}$

$q_5 = 1280 \times 3.84 / 640 \times 0.44 = 3.4 \text{ cfs}$ $QA / 640 = .0026$

$q_{100} = 1280 \times 3.84 / 640 \times 1.30 = 10.0 \text{ cfs}$ $100 .0078$

Project BROADMOOR BLUFFS ESTATES		EXHIBIT "C"	Job No E 3098
Client GATES LAUR Co.	By djh	Date DEC. 10. 1984	

CNO: RODIE 12-14-84

BASIN C2 SEE pg. 7

BASIN C3 AREA = 1.12 AC

SOIL GROUP 74(C) USE R¹/₂ CN 80

T_c: 300 LF OVERLAND AT 10% (1.6 fps)
120 LF SWALE AT 10% (4 fps)

3.1 MIN
0.5 MIN
3.6 MIN ± 0.1 h

q_p = 1280 csm/in

Q₅ = 0.62 in Q₁₀₀ = 1.64 in

q₅ = 1280 × 1.12 / 640 × 0.62 = 1.4 cfs

q₁₀₀ = 1280 × 1.12 / 640 × 1.64 = 3.7 cfs

QA / 640
5 .0011
100 .0029

BASIN C4 SEE pg. 8

BASIN D2 AREA = 4.30 AC

SOIL GROUP	ACREAGE	USE	CN	%	% CN
38 (B)	1.93	R ¹ / ₂	70	44.9	31.4
74 (C)	<u>2.37</u>	R ¹ / ₂	80	<u>55.1</u>	<u>44.1</u>
	4.30			100	76

T_c: 280 LF OVERLAND AT 15% (1.4 fps)
320 LF OVERLAND AT 10% (1.1 fps)
150 LF CURB FLOW AT 2.5% (3.1 fps)
200 LF CURB FLOW AT 9.0% (6.0 fps)

3.3 MIN
4.8 MIN
0.8 MIN
0.6 MIN
9.5 MIN ± 0.1 h

q_p = 1140 csm/in

Q₅ = 0.47 in Q₁₀₀ = 1.36 in

q₅ = 1140 × 4.30 / 640 × 0.47 = 3.6 cfs

q₁₀₀ = 1140 × 4.30 / 640 × 1.36 = 10.4 cfs

QA / 640
5 .0032
100 .0091

BASIN D1 SEE pg 8

Project BROADMOOR BLUFFS ESTATES	EXHIBIT "C"	Job No E 3098
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Client GATES LAND CO	By dln	Date DEC. 10, 1984
--------------------------------	------------------	------------------------------

CAD: RDO III 12-17-84

BASIN E1 AREA = 12.87 AC

SOIL GROUP	ACREAGE	USE	CN	%	% CN
3B (B)	5.42	R 1/2	70	42.1	29.5
74 (C)	7.45	R 1/2	80	57.9	46.3
	12.87			100	76

T₂: 250 LF OVERLAPPING AT 30% (2 fps) 2.1 MIN.
 1200 LF NAT. SWALE AT 12% (4 fps) 5.0 MIN.
7.1 MIN ≈ 0.12 h

q_p = 1220 csm/in
 Q₅ = 0.47 in Q₁₀₀ = 1.36 in
 q₅ = 1220 * 12.87 / 640 * 0.47 = 11.5 cfs
 q₁₀₀ = 1220 * 12.87 / 640 * 1.36 = 33.4 cfs
Q_A / 640
 5 = 0.0095
 100 = 0.273

BASIN E2 AREA = 0.56 AC

SOIL GROUP	USE	CN
74 (C)	STREET	98

T ₂ : 150 LF CURB FLOW AT 7.5% (5.5 fps)	0.5 MIN
150 LF " AT 2.5% (3.1 fps)	0.8 MIN
200 LF " AT 9.0% (6.0 fps)	0.6 MIN
75 LF " AT 6.0% (4.8 fps)	0.3 MIN
225 LF " AT 9.2% (6.0 fps)	0.6 MIN
75 LF " AT 6.0% (4.8 fps)	0.3 MIN
	3.1 MIN ≈ 0.1 h

q_p = 1280 csm/in
 Q₅ = 1.87 in Q₁₀₀ = 3.27 in
 q₅ = 1280 * 0.56 / 640 * 1.87 = 2.1 cfs
 q₁₀₀ = 1280 * 0.56 / 640 * 3.27 = 3.7 cfs
Q_A / 640
 5 = 0.0016
 100 = 0.0029

Project: BROADMOOR BLUFFS ESTATES EXHIBIT "C" Job No: E 3098

Client: GATES LAND CO By: djm Date: DEC 10, 1984

CRD: ROOT III 12-14-84

BASIN E3 AREA = 3.06 AC

SOIL group 74 (C) USE: R 1/2 CN 80

Tc: 200 LF OVERTHAW AT 22% (1.7 fps)	2.0 MIN.
220 LF OVERTHAW AT 9% (1.0 fps)	3.7 MIN
	<u>5.7 MIN. ± 0.1h</u>

$q_p = 1280 \text{ csm/in}$

$Q_5 = 0.62 \text{ in}$ $Q_{100} = 1.64 \text{ in}$

$q_5 = 1280 * 3.06/640 * 0.62 = 3.8 \text{ cfs}$

$q_{100} = 1280 * 3.06/640 * 1.64 = 10.0 \text{ cfs}$

$Q_A/640$
5 = .0030
100 = .0078

BASIN E4 AREA = 0.49 AC

SOIL group 74 (C) USE: STREET CN 98

Tc: 100 LF CURB FLOW AT 2.0% (2.8 fps)	0.6 MIN
150 LF " AT 10.0% (6.3 fps)	0.4 MIN
200 LF " AT 1% (2.0 fps)	1.7 MIN
150 LF " AT 6.2% (4.8 fps)	0.5 MIN
150 LF " AT 1.0% (2.0 fps)	1.3 MIN
	<u>4.5 MIN ± 0.1h</u>

$q_p = 1280 \text{ csm/in}$

$Q_5 = 1.87 \text{ in}$ $Q_{100} = 3.27 \text{ in}$

$q_5 = 1280 * 0.49/640 * 1.87 = 1.8 \text{ cfs}$

$q_{100} = 1280 * 0.49/640 * 3.27 = 3.2 \text{ cfs}$

$Q_A/640$
5 = .0014
100 = .0025

Project BROADMOOR BLUFFS ESTATES	EXHIBIT "C"	Job No E 3098
Client GATES LAND CO	By djh	Date DEC 10, 1984

CAD: ~~ROOT~~ 12-14-84

BASIN F1 SEE PAGE 7

BASIN F2 AREA = 3.21 ac

SOIL group 74(c) USE: R¹/₂ CN 80

TC: 215 LF OVERLAND AT 16%	(1.4 fps)	2.6 MIN
200 LF CURB FLOW AT 6%	(5 fps)	0.7 MIN
200 LF CURB FLOW AT 9%	(6 fps)	0.6 MIN
75 LF CURB FLOW AT 1%	(2 fps)	0.6 MIN
		4.5 MIN ≈ 0.1 h

$q_p = 1280 \text{ csm/in}$

$Q_5 = 0.62 \text{ in}$ $Q_{100} = 1.64 \text{ in}$

$q_5 = 1280 \times 3.21 / 640 \times 0.62 = 4.0 \text{ cfs}$		$QA/640$
$q_{100} = 1280 \times 3.21 / 640 \times 1.64 = 10.5 \text{ cfs}$		5 = .0031
		100 = .0082

BASIN F3 AREA = 0.40 ac

SOIL group 74(c) USE: STREET CN 98

TC: 350 LF CURB FLOW AT 6.0%	(5 fps)	1.0 MIN
200 LF CURB FLOW AT 9.0%	(6 fps)	0.6 MIN
75 LF CURB FLOW AT 1.0%	(2 fps)	0.6 MIN
		2.2 MIN ≈ 0.1 h

$q_p = 1280 \text{ csm/in}$

$Q_5 = 1.87 \text{ in}$ $Q_{100} = 3.27 \text{ in}$

$q_5 = 1280 \times 0.4 / 640 \times 1.87 = 1.5 \text{ cfs}$		$QA/640$
$q_{100} = 1280 \times 0.4 / 640 \times 3.27 = 2.6 \text{ cfs}$		5 = .0012
		100 = .0020

Project BROADMOOR BLUFFS ESTATES	EXHIBIT "C"	Job No. E 3098
Client GATES LAND CO.	By djh	Date DEC. 10. 1984

CAD: RODIE 12-14-84

BASIN G AREA = 9.02 AC

SOIL GROUP	ACREAGE	USE	CN	%	% CN
74 (C)	4.38	PARK	74	48.6	35.6
74 (C)	4.64	R ^{1/2}	80	51.4	41.2
	9.02			100	77

Tc: 270 LF OVERLAND AT 2.6% (0.55 fps) 8.2 MIN
 250 LF OVERLAND AT 16% (1.4 fps) 3.0 MIN
 575 LF NAT. SWALE AT 10% (4 fps) 2.4 MIN
13.6 MIN & 0.23h

$q_p = 1020 \text{ csm/in}$

$Q_5 = 0.51 \text{ in} \quad Q_{100} = 1.43 \text{ in}$

$q_5 = 1020 * 9.02 / 640 * 0.51 = 7.3 \text{ cfs}$

$q_{100} = 1020 * 9.02 / 640 * 1.43 = 20.6 \text{ cfs}$

QA / 640
5 = .0072
100 = .0202

BASIN J1 AREA = 4.10 AC

SOIL GROUP 74 (C) USE: R^{1/2} CN 80

Tc: 380 LF OVERLAND AT 13% (1.2 fps) 5.3 MIN & 0.1h

$q_p = 1280 \text{ csm/in}$

$Q_5 = 0.62 \text{ in} \quad Q_{100} = 1.64 \text{ in}$

$q_5 = 1280 * 4.1 / 640 * 0.62 = 5.1 \text{ cfs}$

$q_{100} = 1280 * 4.1 / 640 * 1.64 = 13.5 \text{ cfs}$

QA / 640
5 = .0040
100 = .0105

Project: BROADMOOR BLUFFS ESTATES EXHIBIT "C" Job No: E 3098

Client: GATES LAND CO. By: dlm Date: DEC 10. 1984

CAD: RDO III 12-14-84

BASIN C2 AREA 1.50 AC.

SOIL GROUP	ACREAGE	USE	CN	%	%CN
3B (B)	1.20	R 1/2	70	80	56.0
74 (C)	0.30	R 1/2	80	20	16.0
	<u>1.50</u>			<u>100</u>	<u>72</u>

Tc: 380 LF SWALE AT 15% (6 fps) | 1.1 MIN 1.01 h
 qp = 1280 csm/in

$Q_5 = 0.34 \text{ in}$ $Q_{100} = 1.12 \text{ in}$

	QA / 640
5	.0008
100	.0026

$q_5 = 1280 \times 1.5 / 640 \times 0.34 = 1.0 \text{ cfs}$
 $q_{100} = 1280 \times 1.5 / 640 \times 1.12 = 3.4 \text{ cfs}$

BASIN F1 AREA 1.35 AC.

SOIL GROUP	ACREAGE	USE	CN	%	%CN
74 (C)	0.90	STREET	98	66.7	65.3
74 (C)	0.45	R 1/2	80	33.3	26.7
	<u>1.35</u>			<u>100</u>	<u>92</u>

Tc: CURB FLOWS

100' AT 4%	4 fps	0.4 MIN
150' AT 6.9%	5 fps	0.5
225' AT 1.9%	2.8 fps	1.3
400' AT 2.8%	3 fps	2.2
350' AT 6%	4.8 fps	1.2
225' AT 9.2%	5.5 fps	0.7
100' AT 6.0%	4.8 fps	0.3
		<u>6.6 MIN 7' 0.11 h</u>

$q_p = 1260 \text{ csm/in}$

$Q_5 = 1.33 \text{ in}$ $Q_{100} = 2.64 \text{ in}$

	QA / 640
5	.0028
100	.0056

$q_5 = 1260 \times 1.35 / 640 \times 1.33 = 3.5 \text{ cfs}$
 $q_{100} = 1260 \times 1.35 / 640 \times 2.64 = 7.0 \text{ cfs}$

Project BROADMOOR BLUFFS ESTATES		Job No E 3098
Client GATES LAND CO	By dlh	Date DEC 10. 1984

CAO: R00III 12-14-84

BASIN C4 AREA = 0.36 Ac

SOIL group 74(c) USE: STREET CN = 98

Tc:	200' CURB FLOW AT 9.5% (5.5 fps)	0.6 MIN
	125' AT 12.0% (6.0 fps)	0.3
	100' AT 6% (4.8 fps)	0.4
	200' AT 2.8% (3 fps)	1.1
		2.4 MIN \approx 0.1 h

$q_p = 1280$ csm/in

$Q_5 = 1.87$ in $Q_{100} = 3.27$ in

$q_5 = 1280 \times 0.36 / 640 \times 1.87 = 1.3$ cf

$q_{100} = 1280 \times 0.36 / 640 \times 3.27 = 2.4$ cf

	QA/CA
	5 .0011
	100 .0018

BASIN B1 AREA = 1.93 Ac

SOIL group 74(c) USE: R/2 CN = 80

Tc:	360' OVERLAND AT 10% (1 fps)	6 MIN
	250' CURB AT 2.8% (3 fps)	1.4
		7.4 MIN \approx 0.12 h

$q_p = 1240$ csm/in

$Q_5 = 0.62$ in $Q_{100} = 1.64$ in

$q_5 = 1240 \times 1.93 / 640 \times 0.62 = 2.3$ cf

$q_{100} = 1240 \times 1.93 / 640 \times 1.64 = 6.1$ cf

	QA/CA
	5 .0019
	100 .0049

EXHIBIT "D"

STREET FLOW ANALYSIS CALCULATIONS

EXHIBIT "D"

STREET FLOW DATA SUMMARY SHEET

<u>Design Point</u>		<u>q5/q100 (cfs)</u>	<u>1/2 Street Capacity To Top Crown (cfs)</u>	<u>1/2 Street Capacity To Top Curb (cfs)</u>	<u>Inlet Size (ft) Capacity (cfs)</u>	<u>Inlet Pickup/by 5 Year (cfs)</u>	<u>Inlet Pickup/by 100 Year (cfs)</u>
Cardiff at Gloucester	W1/2	3.4/10.00	11.1	38.4			
	E1/2	1.1/ 1.9	11.1	38.4			
Cardiff at Inlet E	N1/2	4.7/12.3	11.1	38.4	6/13.2	2.8/1.9	5.4/6.9
Cheshire at Inlet D	S1/2	4.4/12.6	4.8	23.2	8/12.1	2.6/1.8	6.4/6.2
Cardiff at Cheshire	W1/2	5.4/17.1	9.5	35.2			
	E1/2	2.4/ 4.2	9.5	35.2			
Cardiff at Reginold	W1/2	3.5/ 7.0	9.5	35.2			
	E1/2	6.9/19.6	9.5	35.2			
Cardiff at Inlets A&B	W1/2	7.0/16.3	7.2	27.2	6/12.8	7.0/0	12.8/0
	E1/2	1.5/ 2.6	7.2	27.2	4/ 7.9	1.5/0	2.6/0
Reginold at Inlet C	W1/2	3.8/10.0		27.2			
	E1/2	7.5/19.8		27.2	8/18.4	10.2/0	18.4/8.6

Project: **BROADMOOR BLUFFS ESTATES** **EXHIBIT "D"** Job No: **E 3098**

Client: **GATES LAND CO** By: **djm** Date: **DEC. 10. 1984**

CNO: **KJO III 12-14-84**

SOUTHERLY 1/2 OF CARDIFF

AT GLOUCESTER AREA 0.29 ac CURB GRADE 2.8%

CN 98 $Q_5 = 1.87 \text{ in}$ $Q_{100} = 3.27 \text{ in}$

Tc: CURB FLOW	100' AT 4%	0.4 MIN
	150 6.9%	0.5
	225 1.9%	1.3
	100 2.8%	0.6

2.8 MIN USE 0.1 h

$q_p = 1280 \text{ csm/in}$

$q_5 = 1280 \times 0.29 / 640 \times 1.87 = 1.1 \text{ cfs}$ || ALLOW 1/2 ST TO TOP CROWN

$q_{100} = 1280 \times 0.29 / 640 \times 3.27 = 1.9 \text{ cfs}$ || 1.1 cfs SLEEP pg. 10

AT CHESHIRE AREA = 0.65 ac CURB GRADE 6.0%

CN 98 $Q_5 = 1.87 \text{ in}$ $Q_{100} = 3.27 \text{ in}$

Tc: PREVIOUS	2.8 MIN
+ 300' AT 2.8%	2.8 MIN
+ 320' AT 6.0%	0.9 MIN

6.5 MIN x 0.11 h

$q_p = 1260 \text{ csm/in}$

$q_5 = 1260 \times 0.65 / 640 \times 1.87 = 2.4 \text{ cfs}$ || ALLOW 1/2 STREET TO TOP

$q_{100} = 1260 \times 0.65 / 640 \times 3.27 = 4.2 \text{ cfs}$ || CROWN 9.5 cfs SEE pg. 12

AT REGINOLD CURB GRADE 6%

INDIVIDUAL BASIN F1

$q_5 = 3.5 \text{ cfs}$

$q_{100} = 7.0 \text{ cfs}$

AT 6% ALLOW FLOW TO TOP CROWN (1/2 STREET) 9.5 cfs SEE pg 12

AT 9.2% " (1/2 STREET) 6.5 cfs SEE pg 14

AT 9.2% top curb (1/2 STREET) 26.4 cfs SEE pg 15

Project BROADMOOR BLUFFS ESTATES EXHIBIT 'B'		Job No E 3098
Client GATES LAND CO	By H.M.	Date DEC. 10. 1984

CAD: ROUTE 12-18-84

AT SUMP INLET OFF PARTING

BASIN F1 + F2

$$Q_A/640 \quad 5 \quad , \quad .0031 + .0028 = .0059$$

$$100 \quad .0082 + .0056 = .0138$$

Tc: BASIN F1	6.6 MIN	
ACROSS F2	200' CURBFLOW AT 6%	0.7 MIN
	200' AT 9%	0.6
	75' AT 1%	0.6
		8.5 MIN 20.14h

$q_p = 1180 \text{ csm/in}$

$q_5 = 1180 \times .0059 = 7.0 \text{ cfs}$

$q_{100} = 1180 \times .0138 = 16.3 \text{ cfs}$

AT 6% ALLOW FLOW TO TOP CROWN (1/2 ST)	9.5 cfs	SEE pg 12
AT 6%	TOP CURB (1/2 ST) 39.9 cfs	SEE pg 13
AT 9%	TOP CURB (1/2 ST) 26.4 cfs	SEE pg 15
AT 1%	TOP CROWN (1/2 ST) 7.2 cfs	SEE pg 16
AT 1%	TOP CURB (1/2 ST) 27.2 cfs	SEE pg 17

6' SUMP INLET PICKUP 12.8 cfs

Project: BROADMOOR BLUFFS ESTATES EXHIBIT "B" Job No: E 3098

Client: GATES LAND CO. By: dlh Date: DEC. 10, 1984

CAD: TRAD III 12-14-84

NORTHERLY 1/2 OF GAROIFF

TO GLOUCESTER CURB GRADE 2.8%

BASIN C1 Tc: 4.6 MIN

q₅ = 3.4 cfs
q₁₀₀ = 10.0 cfs || ALLOW 1/2 ST. FLOW TO CROWN ||.1 cfs SEE PG. 10

TO PROPOSED INLET ON 2.8% GRADE C1 + C4

QA/L₁₀ = .0026 + .0011 = .0037
L₁₀₀ = .0078 + .0018 = .0096

Tc: BASIN C1 4.6 MIN

FLOW ACROSS C4 200' AT 2.8% 1.1 MIN

q₅ = 1280 csm/in Tc = 5.7 MIN OR C1 h

q₅ = 1280 * .0037 = 4.7 cfs
q₁₀₀ = 1280 * .0096 = 12.3 cfs

ALLOW 1/2 ST. AT 2.8% TO TOP CROWN ||.1 cfs SEE PG 10
TO TOP CURB 45.9 cfs SEE PG 11

4' INLET ON 2.8% ALLOW PICKUP 5.4 cfs

5 YEAR PICKUP 4.7 * .6 = 2.8 cfs BY 1.9 cfs
100 YEAR PICKUP 12.3 * .6 = 7.4 5.4 cfs BY 6.9 cfs

TO PROPOSED INLET IN CHESHIRE BASIN B2 + 3

Tc: 11.6 MIN

q₅ = 4.4 cfs 1/2 ST. CAPACITY ALLOW 4.8 cfs
q₁₀₀ = 12.6 cfs theoretical 20.2 cfs

6' CURB INLET ON 9% GRADE ALLOW 6.4 cfs

5-YEAR PICKUP 4.4 * 0.6 = 2.6 1.8 cfs by
100-YEAR PICKUP 12.6 * 0.6 = 7.6 6.4 6.2 cfs by

Project: **BROADMOOR BLUFFS ESTATES** **EXHIBIT "D"** Job No: **E 3098**

Client: **GATES LAND CO** By: **djh** Date: **DEC. 10, 1984**

CHD: **K00III 12-14-84**

REDUCE THE EFFECTIVE $\Phi A / GAO$ 'S OF AREAS TRIBUTARY TO THE PROPOSED INLETS TO ACCOUNT FOR FLOW BT TO DOWNSTREAM POINTS.

INLET AT CARDIFF

$\Phi A / GAO$	5	.0037	q	4.7	q by	1.9
	100	.0096	q	12.3	q by	6.9

$$1.9 / 4.7 = X / .0037 \quad X = .0015$$

$$6.9 / 12.3 = X / .0096 \quad X = .0054$$

INLET AT CHESTIRE

	5	.0041	q	4.4	q by	1.8
	100	.0117	q	12.6	q by	6.2

$$1.8 / 4.4 = X / .0041 \quad X = .0017$$

$$6.2 / 12.6 = X / .0117 \quad X = .0058$$

THE ABOVE EFFECTIVE $\Phi A / GAO$ SHALL BE UTILIZED IN CALCULATIONS DOWNSTREAM TO ACCOUNT FOR INLET INTERCEPTION.

Project: BROADMOOR BLUFFS ESTATES EXHIBIT "D" Job No: E 3098

Client: GATES LAND CO. By: dlh Date: DEC. 10, 1984

CAD: KOO III 12-14-84

TO CHESTIRE CURB GRADE 6%

	CHEST ADJ. D1	CHEST ADJ.	
QA/640	5	,0015 + ,0019 + ,0017	= ,0051
	100	,0054 + ,0049 + ,0058	= ,0161

Tc: THRU C4 5.7 MIN + 1.2 MIN = 6.9 MIN > TO INTERSECTION
 OR THRU D2 11.6 MIN + 0.4 MIN = 12.0 MIN

BACK THRU D2 TO AN EFFECTIVE AREA FOR TC = 6.9 MIN
 LOSE 2.1 AC OF BASIN D2 ALL OF D3 MIN. OF D1

ADJUST QA/640	5	,0017 / 4.3 * 2.2	= ,0009
FOR BASIN D2	100	,0058 / 4.3 * 2.2	= ,0030

CHECK BOTH FLOWS FOR THE LARGER PEAK

Tc = 12.0 MIN * 0.2 h qp = 1060 csm/in ← PEAK FLOW

qs = 1060 * ,0051 = 5.4 cfs
 q100 = 1060 * ,0161 = 17.1 cfs

Tc = 6.9 MIN * 0.12 h qp = 1220 csm/in

qs = 1220 * ,0043 = 5.2 cfs
 q100 = 1220 * ,0133 = 16.2 cfs

USE PEAK Tc AT 12 MIN

qs = 5.4 cfs
 q100 = 17.1 cfs

1/2 ST ALLOW TO CROWN AT 6% 9.5 cfs
 TO TOP CURB AT 6% 39.9 cfs

Project: BROADMOOR BLUFFS ESTATES EXHIBIT "D" Job No: E 3098

Client: GATES LAND CO By: djh Date: DEC. 10, 1984

CAO: ROD 12-14-84

TO REGINDLO TO CHESHIRE + E2 CURB GRADE 6%

$$Q_A / 640: \begin{matrix} 5 & .0051 + .0016 = .0067 \\ 100 & .0161 + .0029 = .0190 \end{matrix}$$

T_c: 12 MIN TO CHESHIRE

+ 75'	CURB AT 6%	.3 MIN
225	AT 9.2%	.6 MIN
75'	AT 6.0%	.3 MIN

T_c 13.2 MIN OR 0.22 h

$$q_p = 1030 \text{ cfm/in}$$

$$q_5 = 1030 \times .0067 = 6.9 \text{ cfs}$$

$$q_{100} = 1030 \times .0190 = 19.6 \text{ cfs}$$

ALLOW 1/2 AT 6% TO CROWN	9.5 cfs
TO TOP CURB	39.9 cfs

ALLOW 1/2 AT 9.2% TO CROWN	6.5 cfs
TO TOP CURB	26.4 cfs

TO SUMP INLET AT PARTING BASIN F3

$$q_5 = 1.5 \quad 4' \text{ SUMP INLET CAPACITY } 7.9 \text{ cfs}$$

$$q_{100} = 2.6$$

Project	BROADMOOR BLUFFS ESTATES	EXHIBIT "D"	Job No E 3098
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Client	GATES LAND Co.	By dlh	Date DEC. 10. 1984
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CAO: 700 III 12-14-84

SUMMARY OF FLOWS ALONG FARTHING

5 TR. SOUTHERLY 1/2 STREET FLOWS CONTAINED BETWEEN CROWN AND CURB ALL THE WAY.
 NORTHERLY 1/2 STREET FLOWS CONTAINED BETWEEN CROWN AND CURB TO REGINOLD.

100 TR. SOUTHERLY 1/2 STREET CONTAINED BETWEEN CROWN & CURB TO PAST REGINOLD, SPILLS OVER CROWN BUT IS WITHIN CURBS.
 NORTHERLY 1/2 STREET CONTAINED BETWEEN CROWN & CURB TO CHESHIRE THEN SPILLS OVER CROWN BUT IS WITHIN CURBS.

CHECK 100 YEAR FULL STREET FLOW AT REGINOLD.

$QA/640 \text{ } 100, .0190 + .0056 = .0246$

$T_c: 0.22 \text{ h see pg 6}$

$q_p = 1030$

$q_{100} = 1030 * .0246 = 25.4 \text{ cfs}$

STREET CAP AT TOP CURB = $35.7 * 2 = 70.4 \text{ cfs}$

100 TR. SPILL INTO REGINOLD = 12.7 cfs

CONTINUATION TO FARTHING 12.7 cfs

CHECK 100 YEAR FULL STREET FLOW AT SUMP INLETS IN CARBONIFF

$QA/640 \text{ } 100 \text{ } .0246/2 + .0082 + .0020 = .0225$

$T_c = 13.2 \text{ MIN} + 2.2 \text{ MIN} = 15.4 \text{ MIN } 0.26 \text{ h}$

$q_p = 980 \text{ csm/hr}$

$q_{100} = 980 * .0225 = 22.1 \text{ cfs OR } 11 \text{ cfs / SIDE}$

USE 4' INLET ON EAST CAP. 7.9

6' INLET ON WEST CAP. 12.8

Project BROADMOOR BLUFFS ESTATES	EXHIBIT "D"	Job No E 3098
Client GATES LAND CO.	By dlh	Date DEC 10, 1984

CAD: R00III 12-14-84

REGINOLD FLOWS

THEORETICAL 1/2 CARRIFF FLOW AT 9% 27.2 cfs
 IF NO CARS OBSTRUCT FLOW 1/2 STREET WILL CARRY
 SO ASSUME FULL 1/2 STREET BUMP INTO REGINOLD.

Flows: From E2 WILL BE CROSS STREET TO BASIN E4

EAST END OF REGINOLD

	To Reginold	E4	
QA/64	5	,0067	+ ,0014 = ,0081
	100	,0190	+ ,0025 = ,0215

$T_c = 13.2 \text{ MIN} + 4.5 \text{ MIN} = 17.7 \text{ MIN} \approx 0.30 \text{ h}$
 $q_p = 920 \text{ GPM/IN}$
 $q_5 = 920 * .0081 = 7.5 \text{ cfs}$
 $q_{100} = 920 * .0215 = 19.8 \text{ cfs}$

ALLOW STREET CAPACITY AT CARRIFF INTERSECTION 26.6 cfs
 1/2 STREET ALLOW TO TOP CURB AT 10% 20.2 cfs
 AT 1% 27.2 cfs

WEST END OF REGINOLD

BASIN E3
 $T_c = 5.7 \text{ MIN}$
 $q_5 = 3.8 \text{ cfs}$
 $q_{100} = 10.0 \text{ cfs}$

Project BROADMOOR BLUFFS ESTATES		EXHIBIT "B"	Job No E 3098
Client GATES LAND CO.	By JH	Date DEC. 10. 1984	

CAO: ROBERT 12-14-84

PEAK FLOWS AT REGINOLIO INLET

$$Q_A/640 \quad 5 \quad .0081 + .0030 = .0111$$

$$100 \quad .0215 + .0078 = .0293$$

$T_c = 12.7 \text{ MIN} = 0.3 \text{ h}$

$q_p = 920 \text{ csm/in}$

$q_s = 920 * .0111 = 10.2 \text{ cfs}$

$q_{100} = 920 * .0293 = 27.0 \text{ cfs}$

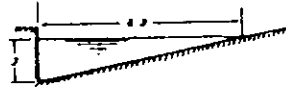
SUMP INLET 6' ALLOW CAPACITY 12.8 cfs
 8' 18.4 cfs

USE 8' INLET FOR INFREQUENT RAINFALL DRAINAGE

DRAINAGE CRITERIA MANUAL

STREETS
E 3098

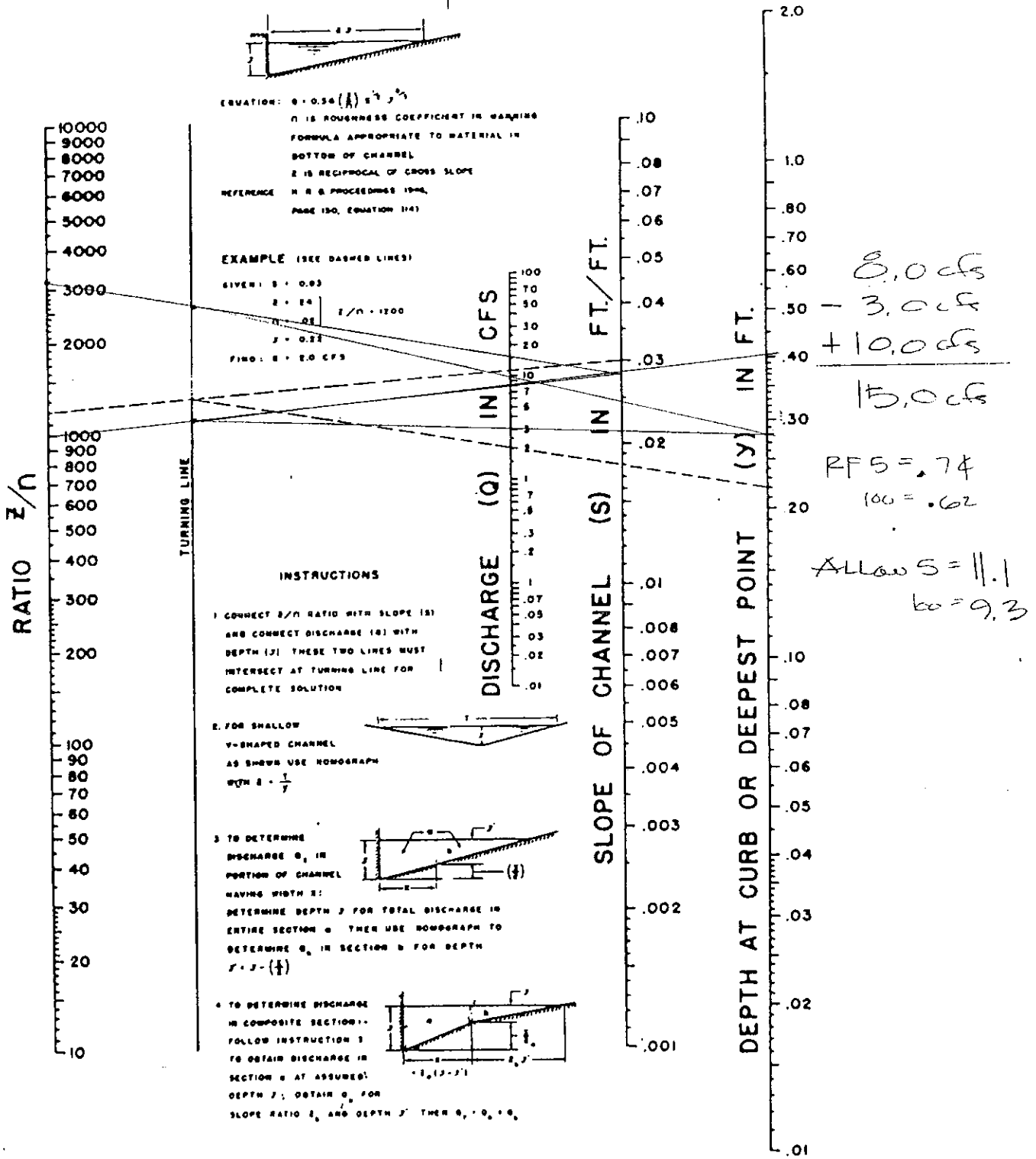
CARDIFF CIR
At 2.8%
Flow to top
Crown



EQUATION: $Q = 0.56 (K) S^{1.48} Z^{1.48}$
n IS ROUGHNESS COEFFICIENT IN MANNING
FORMULA APPROPRIATE TO MATERIAL IN
BOTTOM OF CHANNEL
Z IS RECIPROCAL OF CROSS SLOPE
REFERENCE: H. R. & PROCEEDINGS 1946,
PAGE 150, EQUATION 1141

EXAMPLE (SEE DASHED LINES)

GIVEN: $n = 0.03$
 $Z = 24$
 $S = 0.028$
FIND: $Q = 2.0$ CFS



INSTRUCTIONS

1. CONNECT Z/n RATIO WITH SLOPE (S) AND CONNECT DISCHARGE (Q) WITH DEPTH (Y). THESE TWO LINES MUST INTERSECT AT TURNING LINE FOR COMPLETE SOLUTION.
2. FOR SHALLOW V-SHAPED CHANNEL AS SHOWN USE NOMOGRAPH WITH $Z = \frac{1}{S}$.
3. TO DETERMINE DISCHARGE Q₁ IN PORTION OF CHANNEL HAVING WIDTH B: DETERMINE DEPTH Z FOR TOTAL DISCHARGE IN ENTIRE SECTION. THEN USE NOMOGRAPH TO DETERMINE Q₂ IN SECTION B FOR DEPTH $Z - (\frac{b}{S})$.
4. TO DETERMINE DISCHARGE IN COMPOSITE SECTION: FOLLOW INSTRUCTION 3 TO OBTAIN DISCHARGE IN SECTION B AT ASSUMED DEPTH Z; OBTAIN Q₂ FOR SLOPE RATIO S₂ AND DEPTH Z. THEN Q₁ = Q₂ + Q.

FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

CARBIFF CIR
AT 2.8%

Flow to
Top Curb

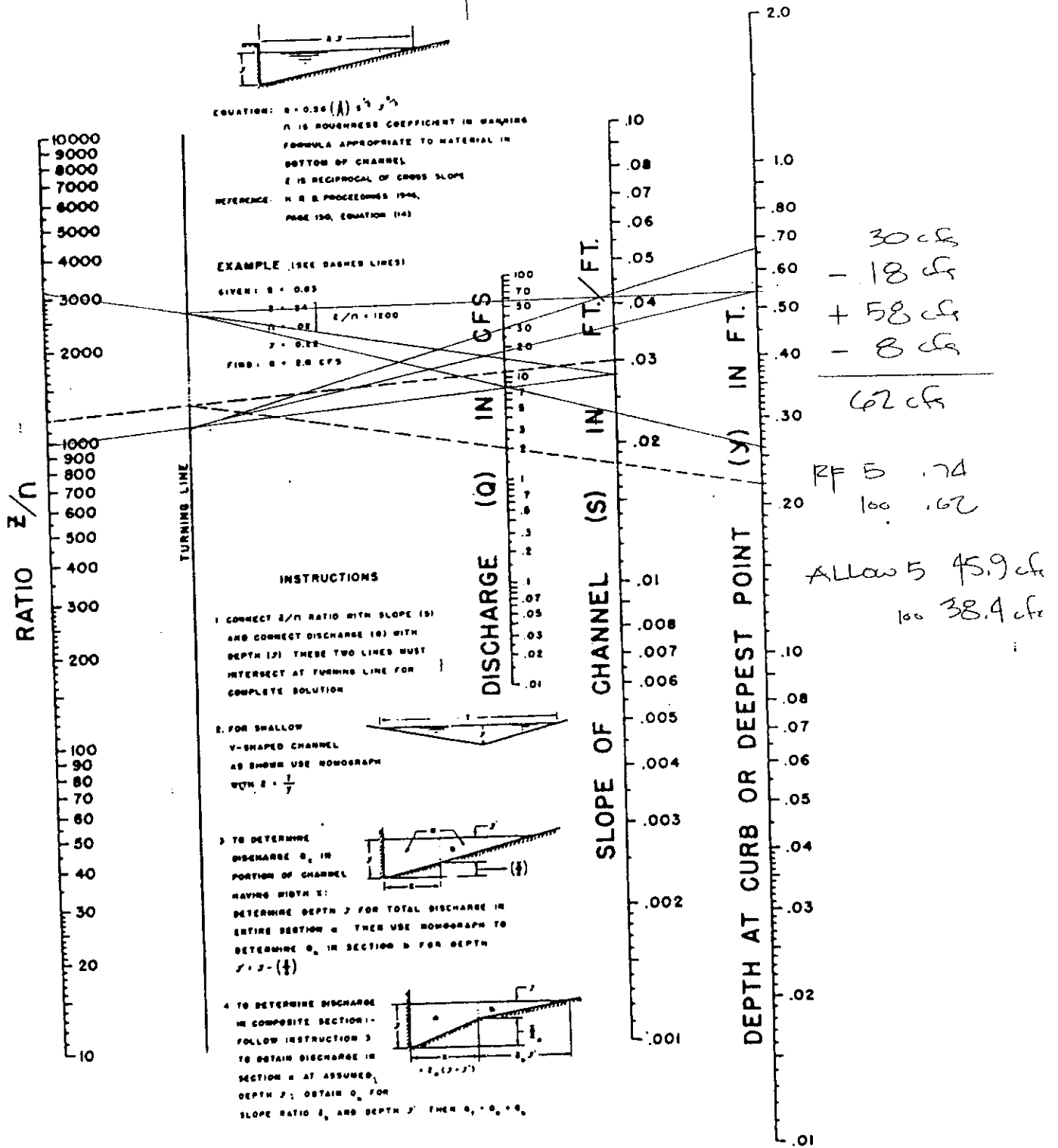
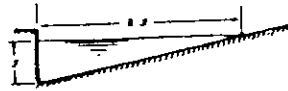


FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

DRAINAGE CRITERIA MANUAL

CARDIFF CIR,
AT 6%
V.C.

Flow TO
TOP CROWN



EQUATION: $Q = 0.36 (A) z^{2.48} j^{0.84}$

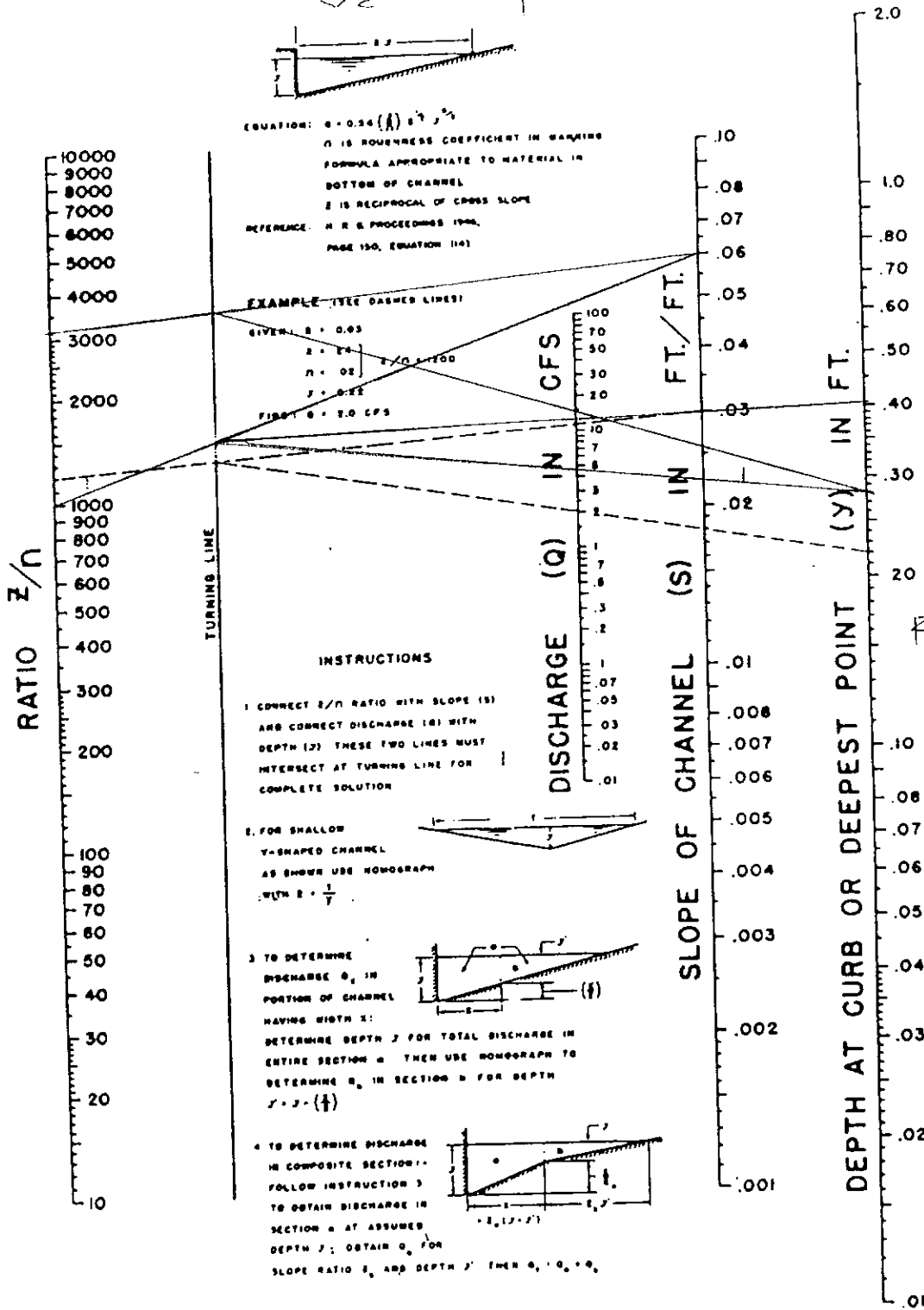
n IS ROUGHNESS COEFFICIENT IN MANNING
FORMULA APPROPRIATE TO MATERIAL IN
BOTTOM OF CHANNEL

z IS RECIPROCAL OF CROSS SLOPE

REFERENCE: H. R. & PROCEEDINGS 1946,
PAGE 150, EQUATION (14)

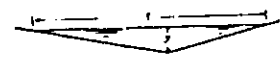
EXAMPLE (SEE DASHED LINES):

GIVEN: $z = 0.03$
 $n = 0.015$
 $j = 0.02$
FIND: $Q = 2.0$ CFS

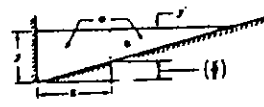


- INSTRUCTIONS
1. CONNECT z/n RATIO WITH SLOPE (S) AND CONNECT DISCHARGE (Q) WITH DEPTH (Y). THESE TWO LINES MUST INTERSECT AT TURNING LINE FOR COMPLETE SOLUTION.

2. FOR SHALLOW
V-SHAPED CHANNEL
AS SHOWN USE NOMOGRAPH
WITH $z = \frac{1}{S}$



3. TO DETERMINE
DISCHARGE Q_1 IN
PORTION OF CHANNEL
HAVING WIDTH x :
DETERMINE DEPTH z FOR TOTAL DISCHARGE IN
ENTIRE SECTION. THEN USE NOMOGRAPH TO
DETERMINE Q_2 IN SECTION x FOR DEPTH
 $z = z \cdot (\frac{x}{b})^2$



4. TO DETERMINE DISCHARGE
IN COMPOSITE SECTION:-
FOLLOW INSTRUCTION 3
TO OBTAIN DISCHARGE IN
SECTION x AT ASSUMED
DEPTH z ; OBTAIN Q_2 FOR
SLOPE RATIO S , AND DEPTH z . THEN $Q_1 + Q_2 = Q$



FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

CARDIFF CIK || Flow to
AT C.I. || TOP CURB
x.c.

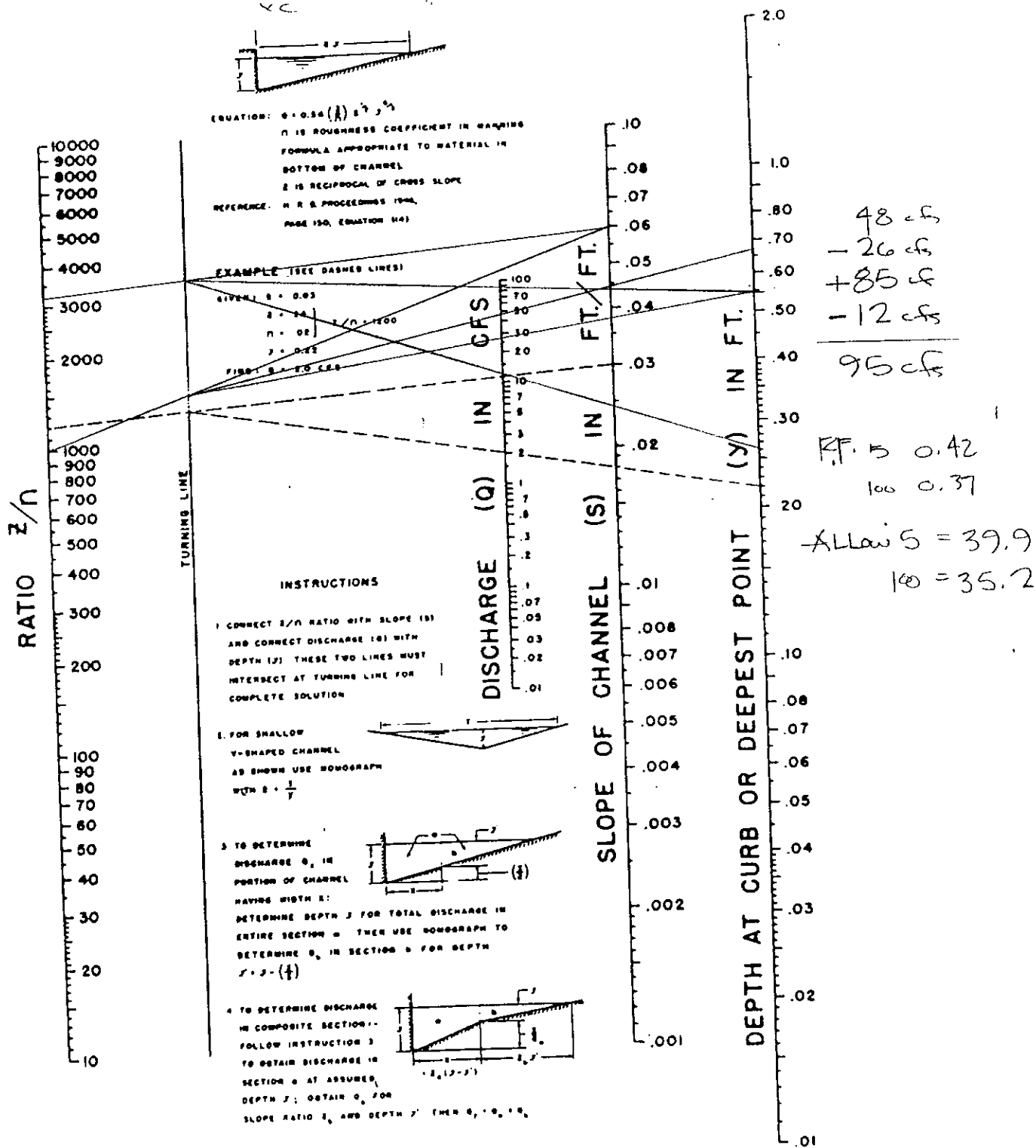


FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

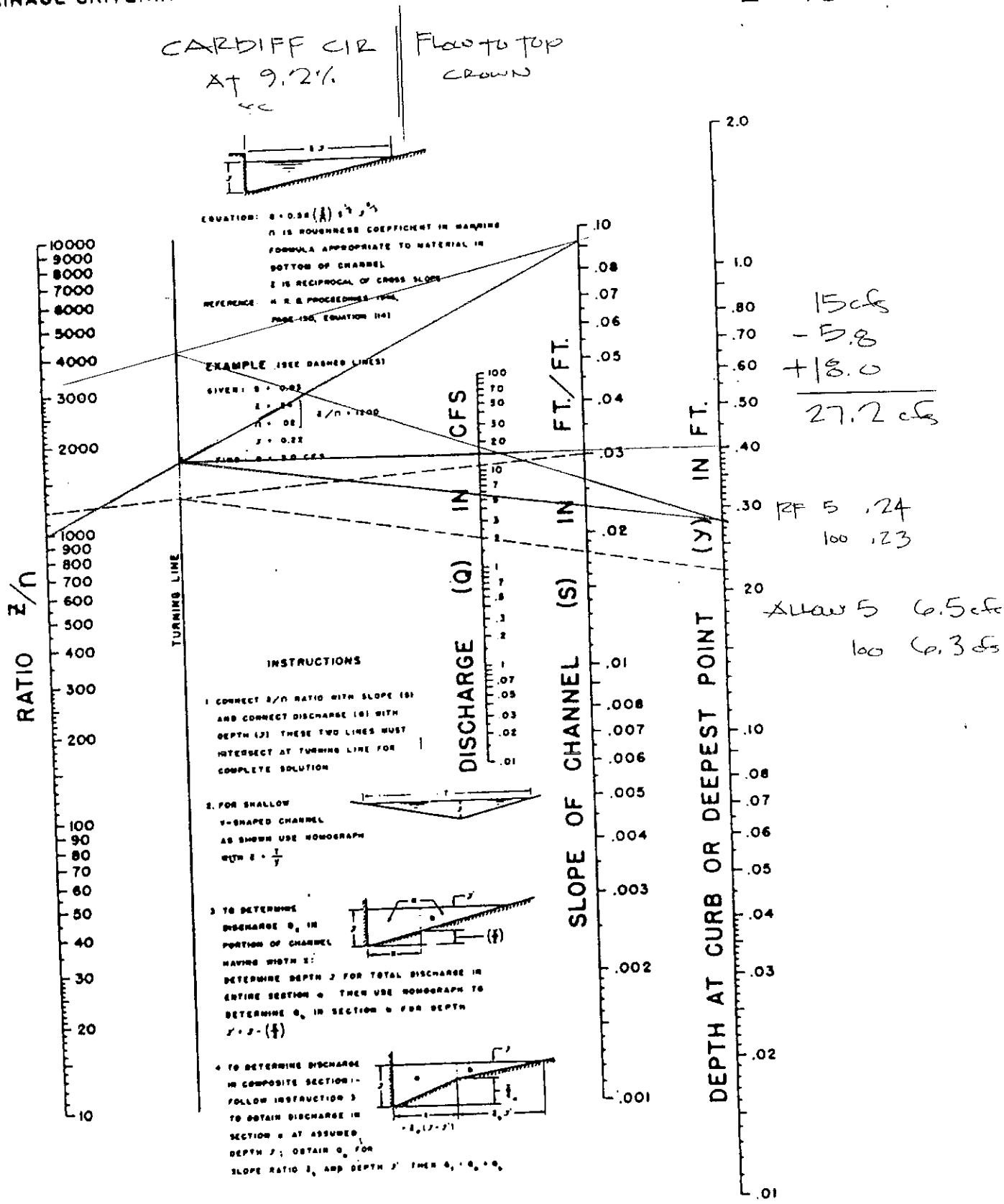


FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

CARDIFF CIR
AT 9.2%
Flow to Top
CURB

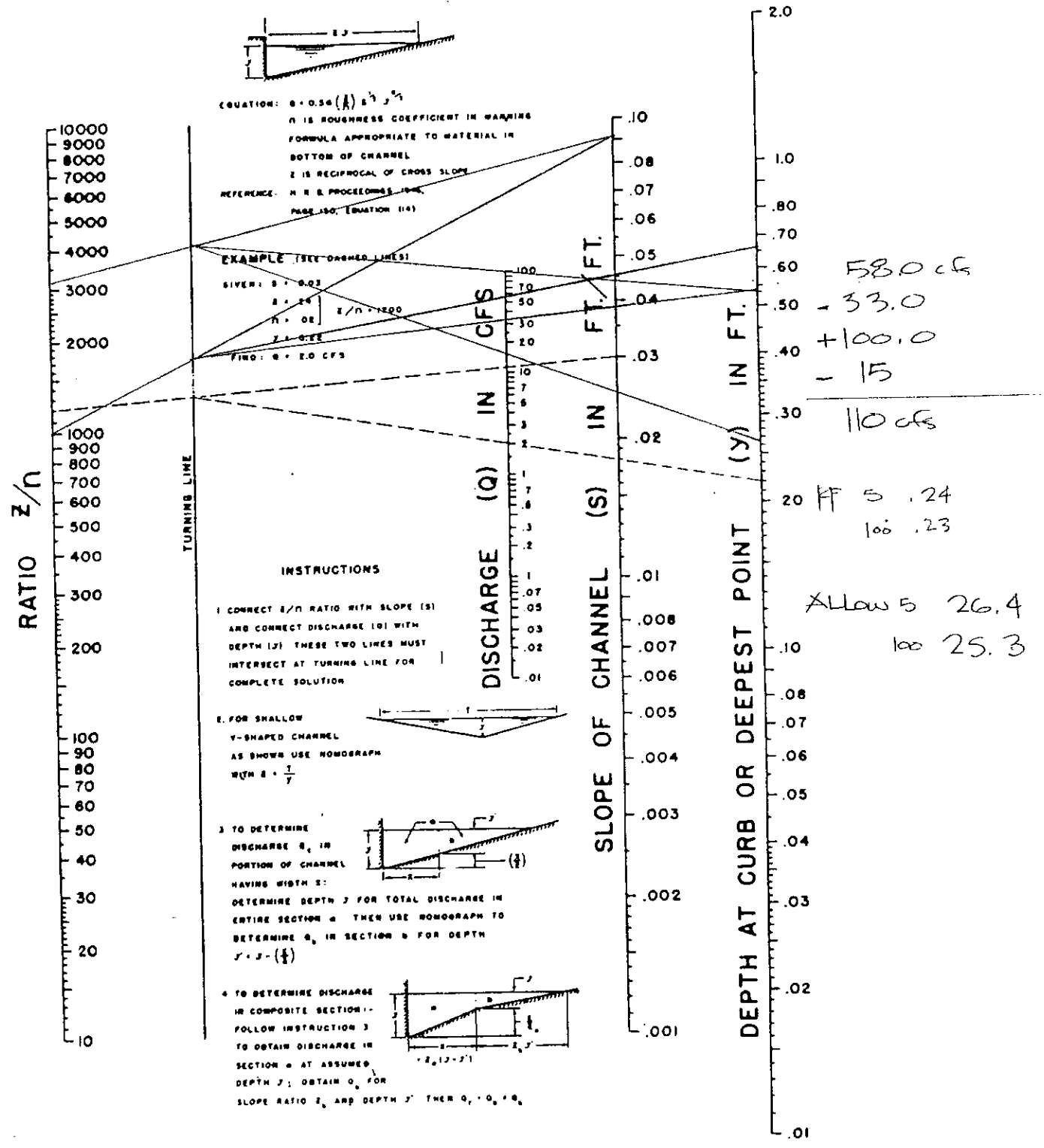


FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

CARBIFF CURB || Flow to
AT 1% || Top Crown

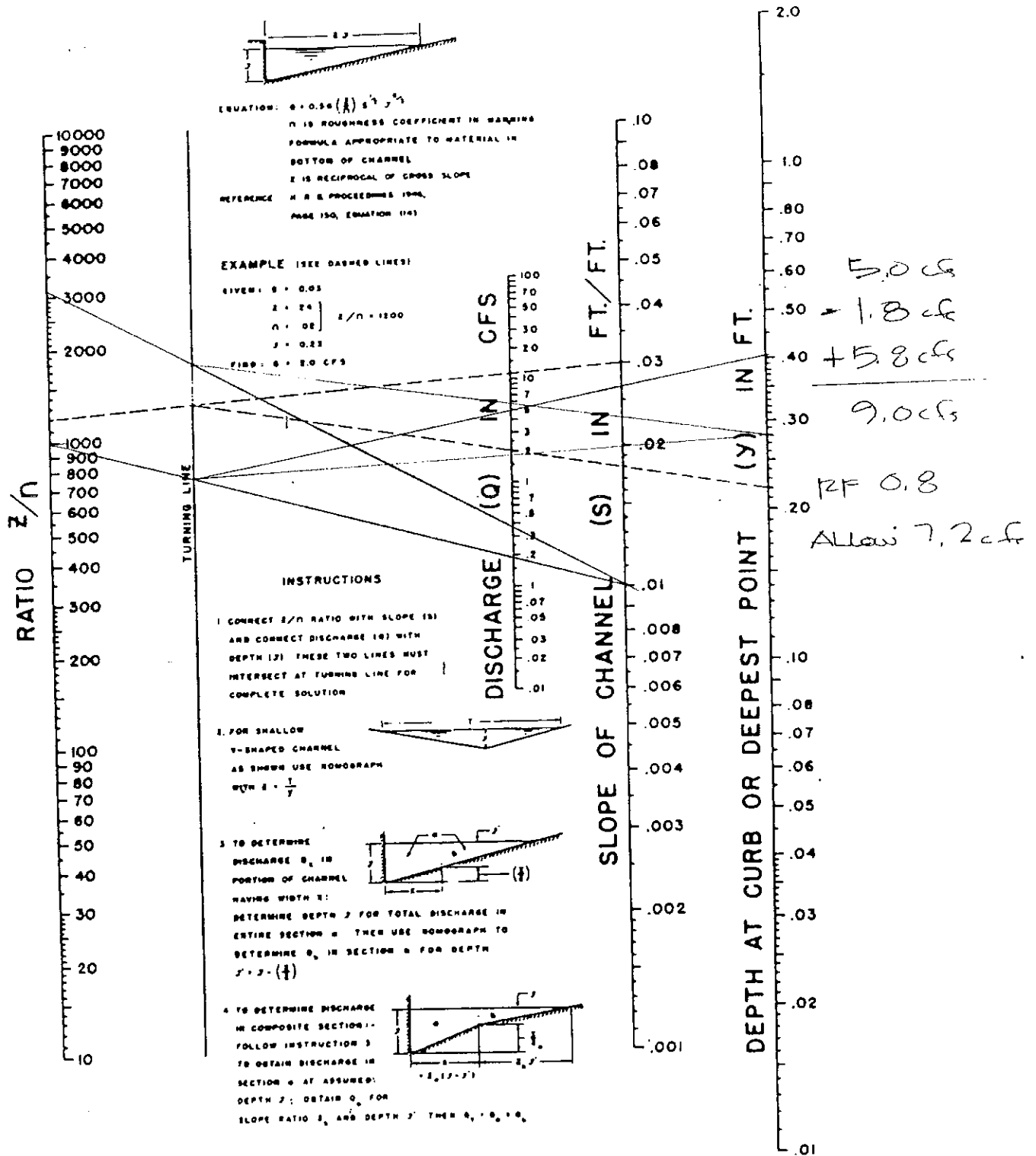


FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

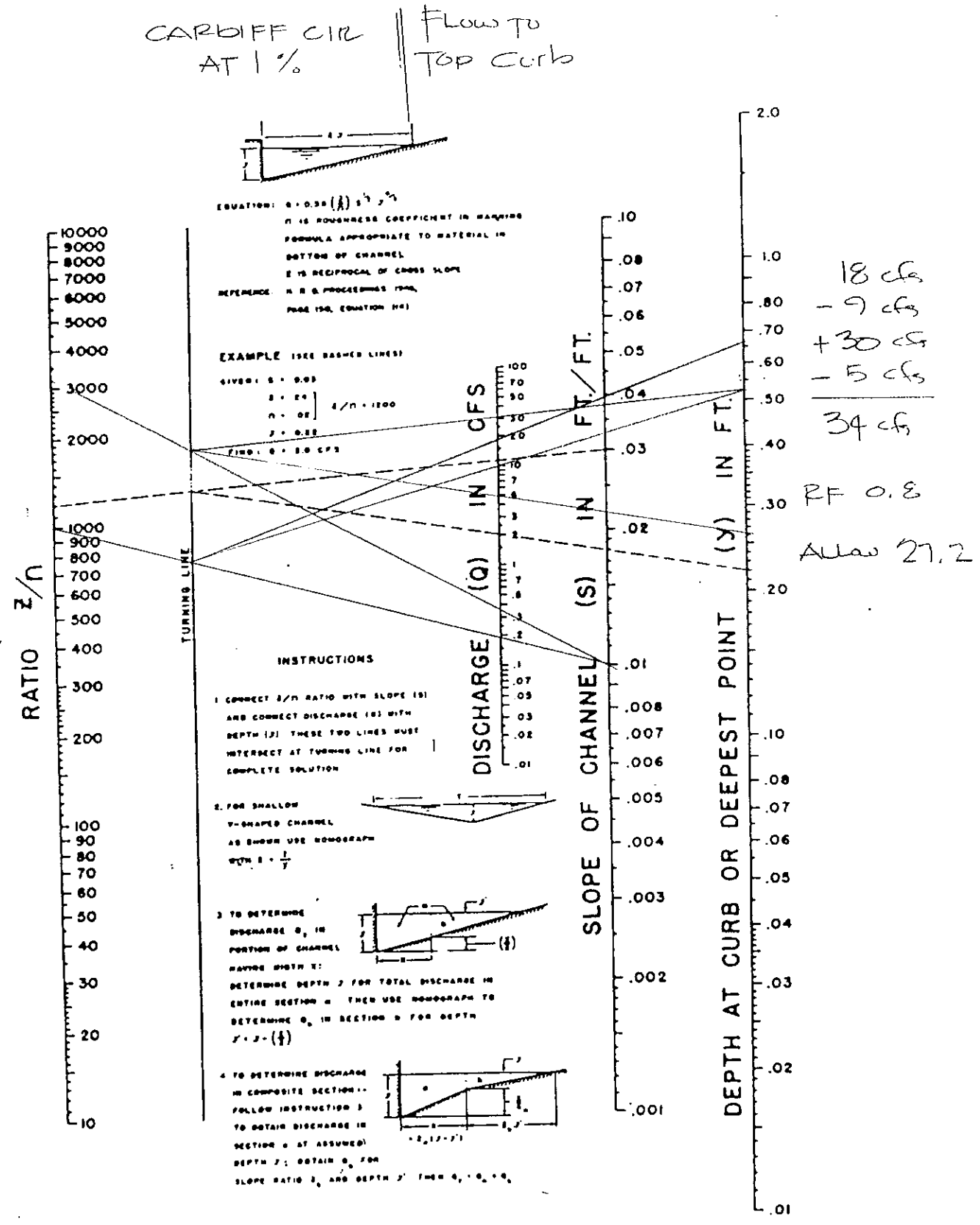


FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

CHESHIRE COURT ^{Flow to} ~~Top~~ ^{to} ~~Crown~~
At 9.0% v/c

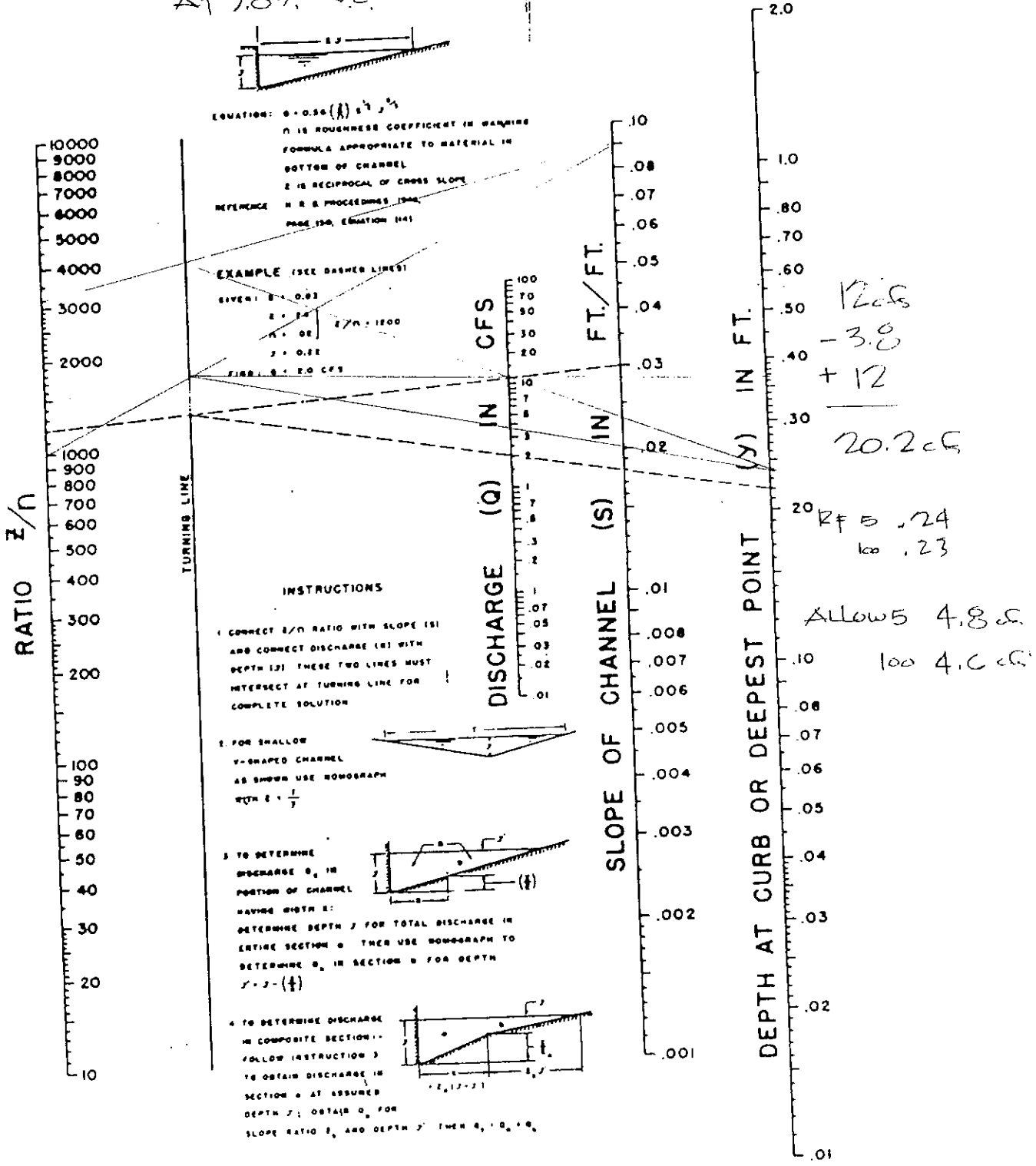


FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

CHESHIRE COURT || Flow TO TOP CURB

AT 9% VC.

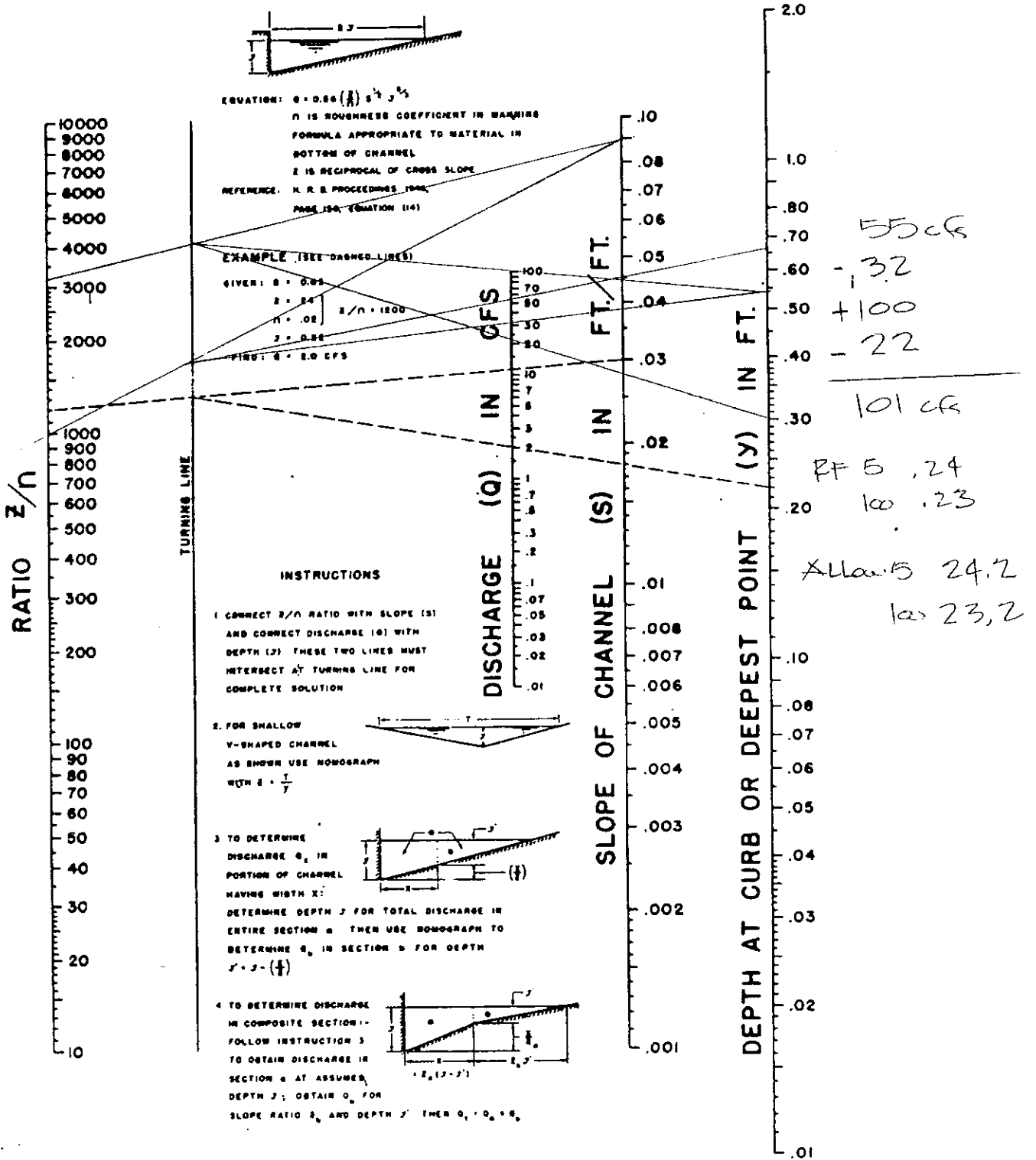
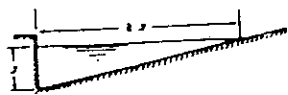


FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

REGULOID CT
AT INTERSECTION

3.3% CROSS FALL TO SOUTH
CURB TO GRADE 2%.
CAP TO TOP CURB.

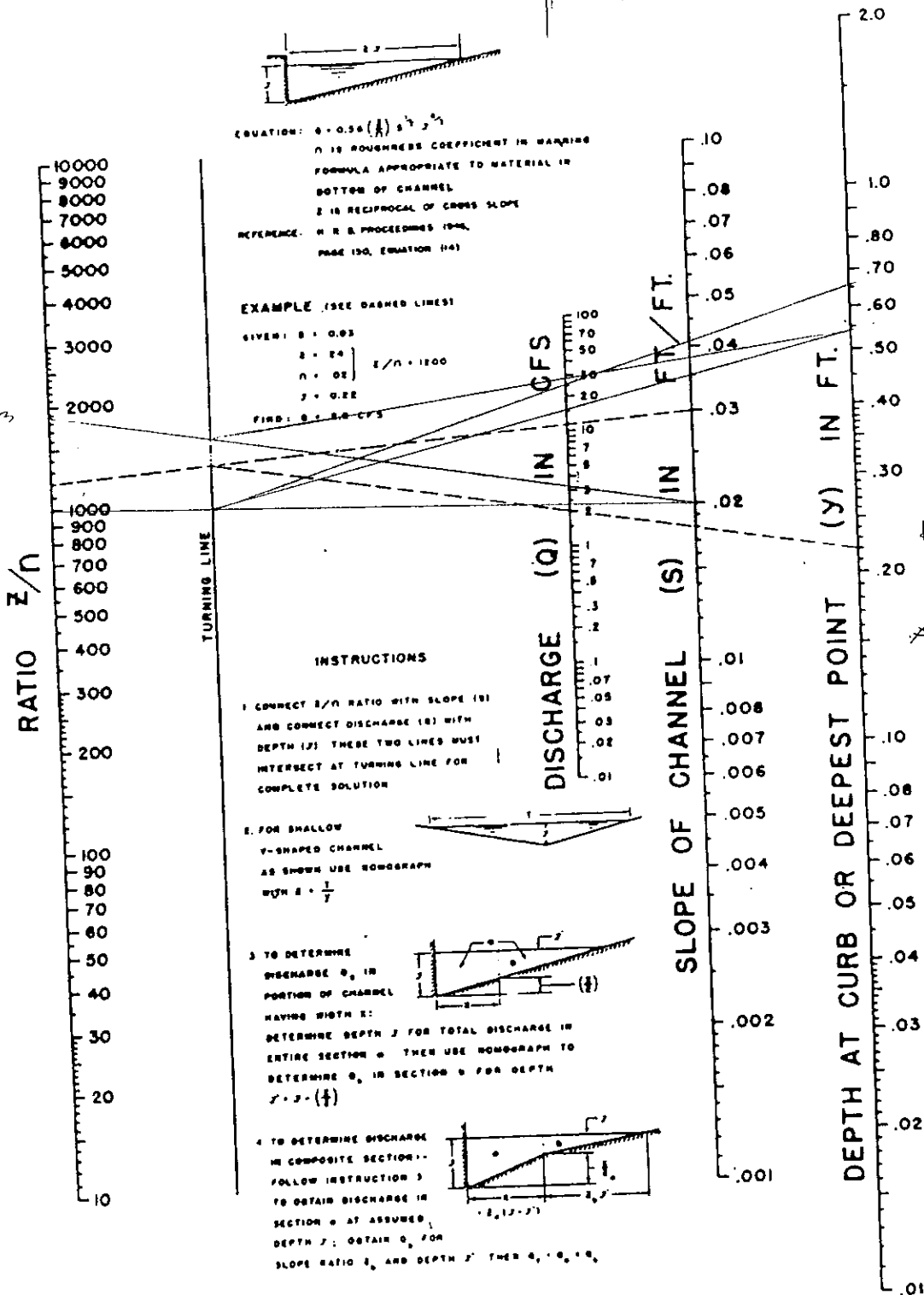
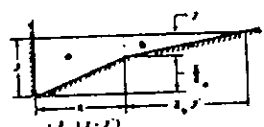
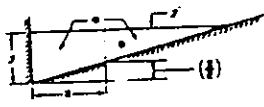
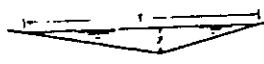


EQUATION: $Q = 0.56 (A) S^{3/2}$
 n IS ROUGHNESS COEFFICIENT IN MANNING
 FORMULA APPROPRIATE TO MATERIAL IN
 BOTTOM OF CHANNEL
 z IS RECIPROCAL OF CROSS SLOPE
 REFERENCE: H. R. & PROCEEDINGS 1946,
 PAGE 150, EQUATION (14)

EXAMPLE (SEE DASHED LINES)
 GIVEN: $z = 0.03$
 $z/n = 24$ $z/n = 1200$
 $n = 0.02$
 $z = 0.22$
 FIND: $Q = 5.0$ CFS

INSTRUCTIONS

1. CONNECT z/n RATIO WITH SLOPE (S) AND CONNECT DISCHARGE (Q) WITH DEPTH (Y); THESE TWO LINES MUST INTERSECT AT TURNING LINE FOR COMPLETE SOLUTION
2. FOR SHALLOW V-SHAPED CHANNEL AS SHOWN USE NOMOGRAPH WITH $z = \frac{1}{T}$
3. TO DETERMINE DISCHARGE Q_s IN PORTION OF CHANNEL HAVING WIDTH z : DETERMINE DEPTH y FOR TOTAL DISCHARGE IN ENTIRE SECTION z THEN USE NOMOGRAPH TO DETERMINE Q_s IN SECTION z FOR DEPTH $y = z \cdot (\frac{z}{z})$
4. TO DETERMINE DISCHARGE IN COMPOSITE SECTION: FOLLOW INSTRUCTION 3 TO OBTAIN DISCHARGE IN SECTION z AT ASSUMED DEPTH y ; OBTAIN Q_s FOR SLOPE RATIO S_s AND DEPTH y THEN $Q_s = Q_s \cdot S_s$



1893

25.0 cfs
 - 15.0 cfs
 + 28.0 cfs

 38 cfs

RF 5 0.5
 100 0.7

ALLOW 5 30.4 cfs
 100 26.6 cfs

FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

DRAINAGE CRITERIA MANUAL

STREETS
E3098

REGINOLD COURT || TO TOP
AT 10% VE || CROWN

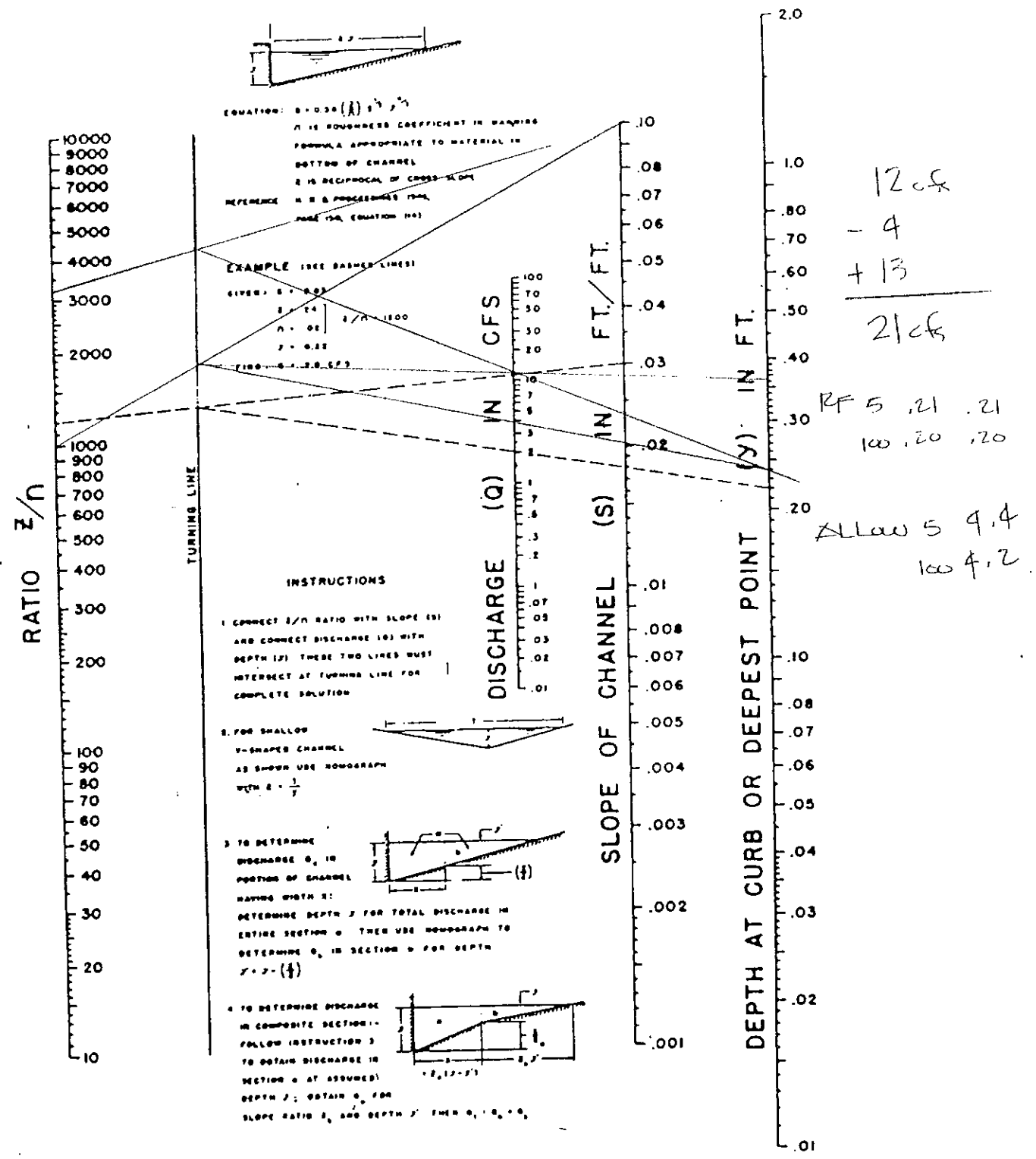


FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

DRAINAGE CRITERIA MANUAL

STREETS

E3098

REYNOLDS G. || Flow to TOP
AT 10% || CURB

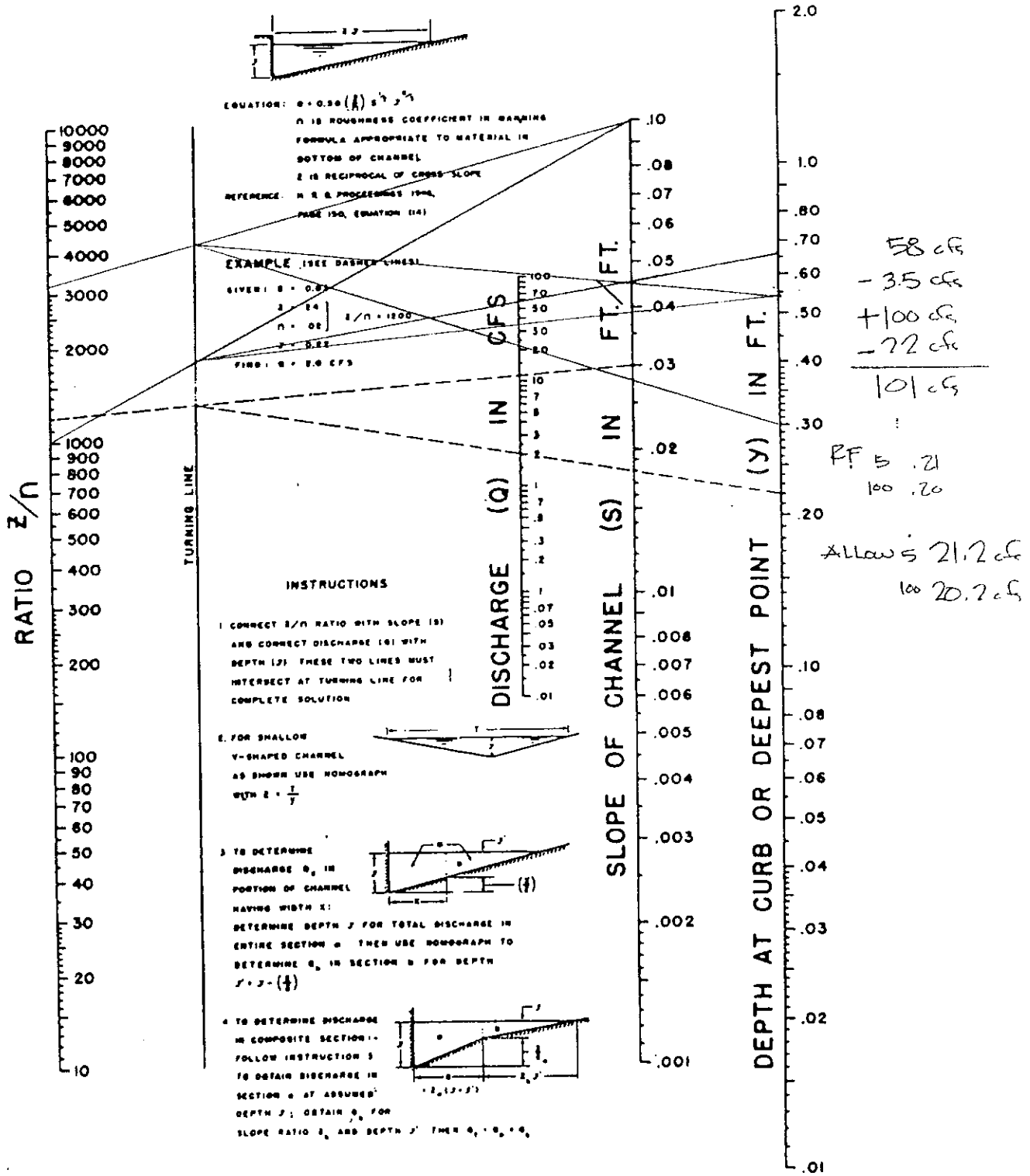
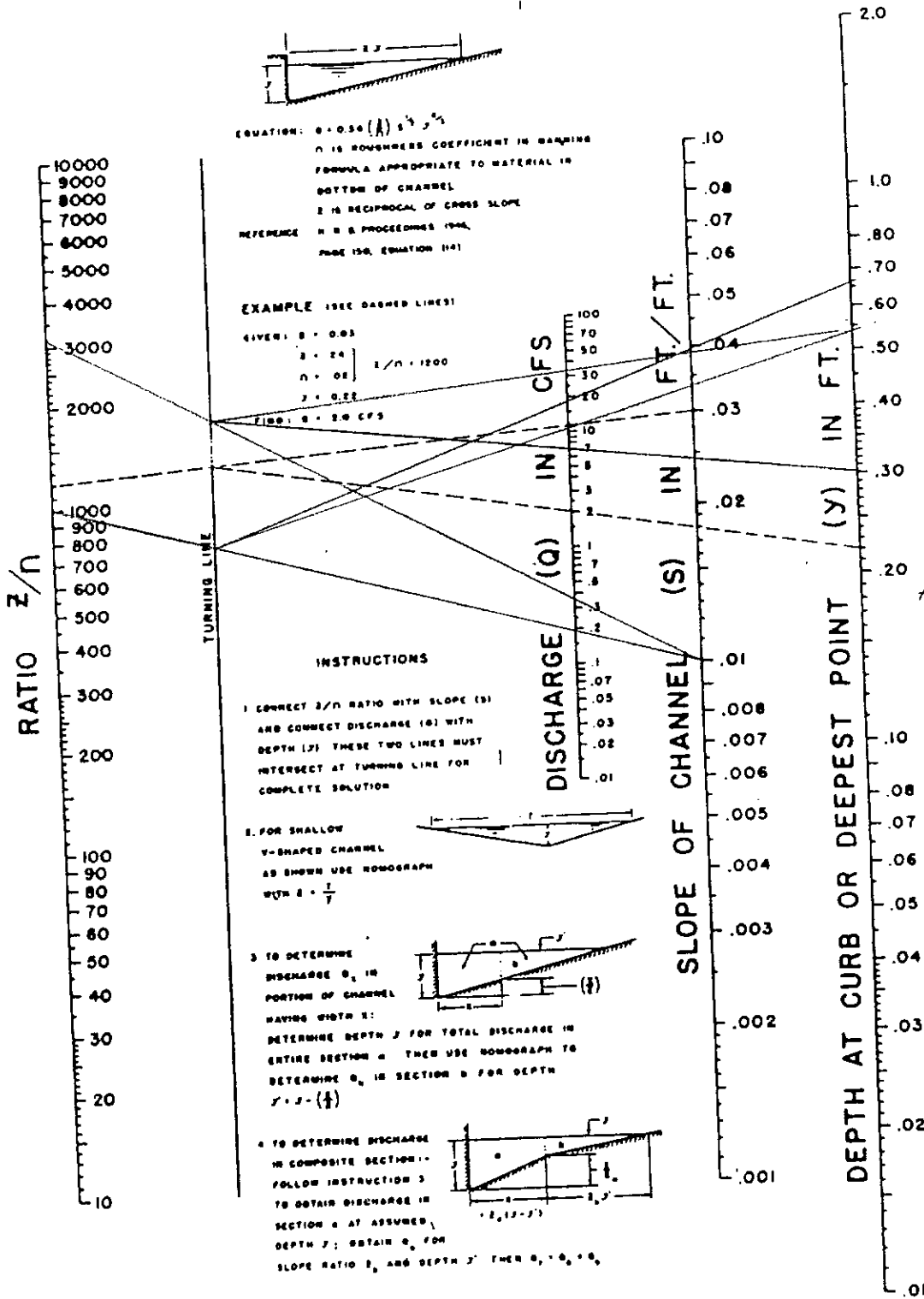


FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

REGIMOLD C_1 || Flow to Top
AT 1.0% || CURB



19cf
 - 11
 + 33
 - 7

 34cf

Rf 5.8
 to .8

Allow 5 27.2
 to 27.2

FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

EXHIBIT "B"
STREETS
E 3098
24/24

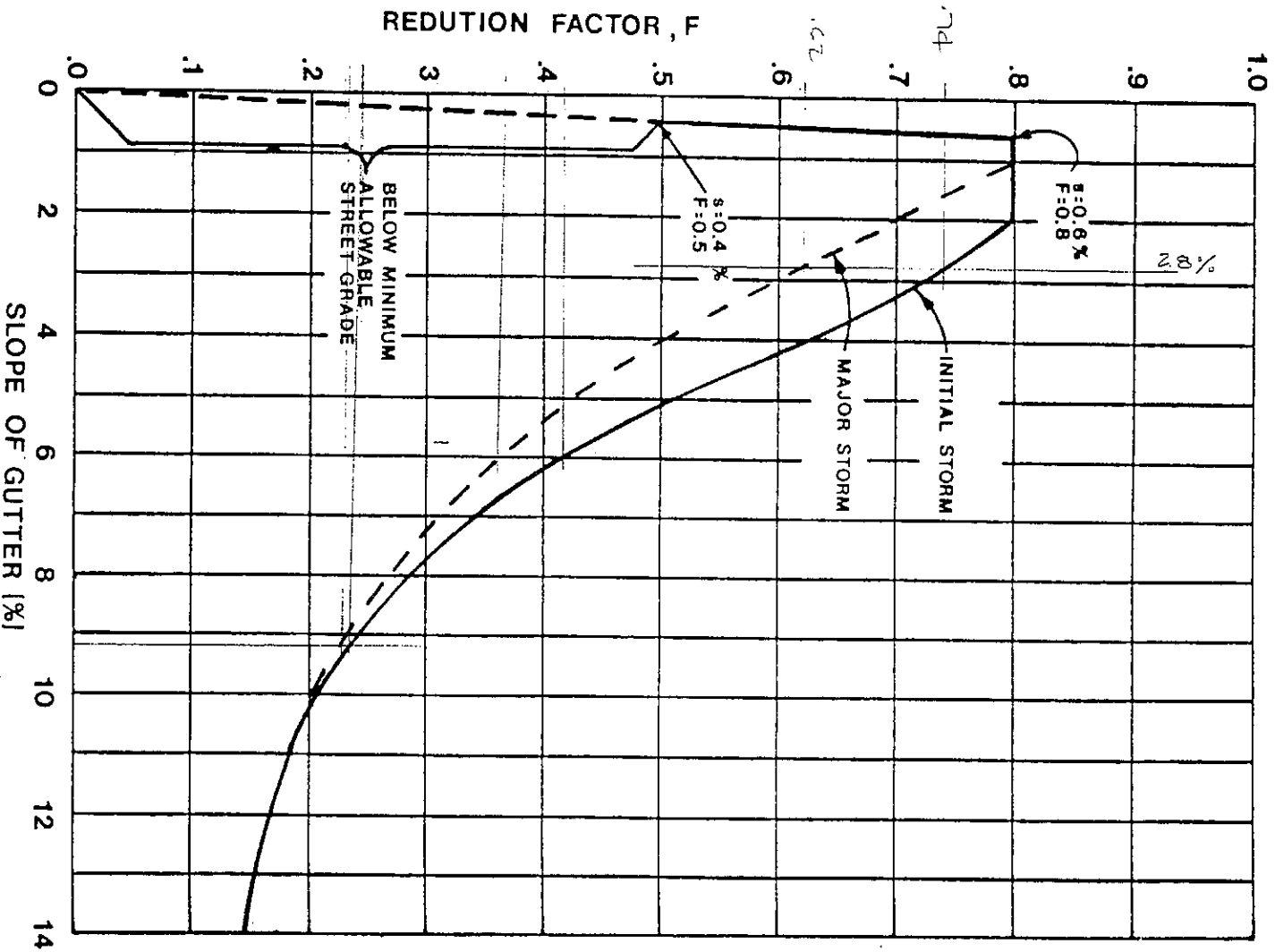


FIGURE 6-2 REDUCTION FACTOR FOR ALLOWABLE GUTTER CAPACITY LOCAL AND COLLECTOR STREETS

APPLY REDUCTION FACTOR FOR APPLICABLE SLOPE TO THE THEORETICAL GUTTER CAPACITY TO OBTAIN ALLOWABLE GUTTER CAPACITY APPROACHING ARTERIAL STREET

EXHIBIT "E"
OFFSITE AND ONSITE COMBINED BASIN FLOWS

EXHIBIT "E"
COMBINED BASIN DATA SUMMARY SHEET

(TOTAL PEAK FLOW AT A POINT)

<u>Through Basin</u>	<u>QA/640 (5)</u>	<u>QA/640 (100)</u>	<u>Tc (hr)</u>	<u>qp (csm/in)</u>	<u>q5 (cfs)</u>	<u>q100 (cfs)</u>
B (B+1)	0.0144	0.0470	0.21	1040	15.0	48.9
C2 (C2+2)	0.0154	0.0429	0.22	1030	15.9	44.2
C3 (pipe flow)	0.0165	0.0458	0.23	1010	16.7	46.2
G (thru C3 + thru B)	0.0403	0.1172	0.30	920	37.0	107.8
D2 (D2 + 3)	0.0041	0.0117	0.19	1080	4.4	12.6
E1 (E1+4+5+Inlet releases)	0.0488	0.1440	0.33	880	42.9	126.7
G (East of inlets)	0.0474	0.1330	0.30	920	43.6	122.4

Project BROADMOOR BLIFFS ESTATES	EXHIBIT "E"	Job No E 3098
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Client GATES LAND CO.	By djh	Date DEC 10, 1984
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CNO: KOOZE 12-17-84

OFFSITE BASINS 1-5 DERIVED FROM KKBNA STUDY

BASIN 1

KKBNA BASIN 4-1-6

AREA 21.5 ac Tc 0.17h Q₅ = 0.34 iu Q₁₀₀ = 1.12 iu
 q_p = 1100 csm/in q₅ = 12.6 q₁₀₀ = 41.4 cfs

"QA/QA0" 5 = .0114
 100 = .0376

BASIN 2

KKBNA BASINS	AREA	Q ₅	Q ₁₀₀	"QA/QA0" 5	100
4-1-1	3.5	.48	1.36	.0026	.0074
4-1-2	4.1	.48	1.36	.0031	.0087
4-1-4	2.7	.48	1.36	.0020	.0057
K-2-G	2.3	.48	1.36	.0017	.0049
4-1-4A	0.2	1.87	3.27	.0004	.0010
4-1-5	2.1	.48	1.36	.0016	.0045
4-1-7	3.4	.48	1.36	.0026	.0072
4-1-8	0.3	.82	1.94	.0006	.0009
				.0146	.0403

APPROX Tc 0.20h q_p = 1080 csm/in

q₅ = .0146 * 1080 = 15.8 cfs vs. 18.6 / REPORT

q₁₀₀ = .0403 * 1080 = 43.6 cfs vs. 52.8 / REPORT

BASIN 3

KKBNA BASIN 4-1-9

AREA = 1.2 ac Tc = 0.17h Q₅ = 0.48 iu Q₁₀₀ = 1.36 iu
 q_p = 1100 csm/in q₅ = 1.0 cfs q₁₀₀ = 2.8 cfs

"QA/QA0" 5 = .0009
 100 = .0026

Project BROADMOOR BLUFFS ESTATES EXHIBIT "E"	Job NR E 3098	
Client GATES LAND CO.	By dlh	Date DEC 10, 1984

CAD: KOO III 12-11-84

BASIN 4

KKBNA BASIN.	AREA	Q_5	Q_{100}	$"QA/CA_0"$ 5	100
K1 & K2	38.2	.35	1.14	.0209	.0680
H-7-2	5.2	.48	1.36	.0039	.0111
				.0248	.0791

APPROX. T_c 0.21 h $q_p = 1040 \text{ csm/in}$
 $q_5 = 1040 * .0248 = 25.8 \text{ cfs}$ vs. 33.3 / REPORT
 $q_{100} = 1040 * .0791 = 82.3 \text{ cfs}$ vs. 94.2 / REPORT

BASIN 5

KKBNA BASIN V-1-3
 AREA = 1.3 ac $T_c = 0.17 \text{ h}$ $Q_5 = 0.48 \text{ in}$ $Q_{100} = 1.36 \text{ in}$
 $q_p = 1100 \text{ csm/in}$ $q_5 = 1.1 \text{ cfs}$ $q_{100} = 3.0 \text{ cfs}$
 $"QA/CA_0"$ 5. 0.0010 100. 0.0028

NOTE: FOR FURTHER COMBINED BASIN FLOW CALCULATED ONTO SITE, WILL CONTINUE TO SUMMATE $"QA/CA_0"$ & DERIVE A NEW T_c THRU EACH FLOW TO DETERMINE q_p .

THRU BASIN B (B+1)

$"QA/CA_0"$ 5 YR .0030 + .0114 = .0144
 100 YR .0094 + .0376 = .0470

T_c : OFFSITE 10 MIN
 ONSITE 250' SWALE AT 7% (3.2 fps) 1.3 MIN
 370' SWALE AT 17% (5 fps) 1.2 MIN

$q_p = 1040 \text{ csm/in}$ 12.5 MIN @ 0.21 h.
 $q_5 = 1040 * 0.0144 = 15.0 \text{ cfs}$
 $q_{100} = 1040 * 0.0470 = 48.9 \text{ cfs}$

Project: BROADMOOR BLUFFS ESTATES EXHIBIT "E" Job No: E 3098

Client: GATES LAND CO By: dlh Date: DEC 10, 1984

CAO: ROO III 12-14-84

THRU BASIN C2 (C2+2)

"QA/640" 5YR .0008 + .0146 = .0154
 100YR .0026 + .0403 = .0429

T_e: OFFSITE 12 MIN
 ONSITE 200' SWALE AT 10% (4 f/s) 0.8 MIN
 200' SWALE AT 20% (7 f/s) 0.5 MIN

q_p = 1030 csm/in 13.3 MIN ≈ 0.22 h
 q₅ = 1030 * 0.0154 = 15.9 cfs
 q₁₀₀ = 1030 * 0.0429 = 44.2 cfs

THRU BASIN C3 (PIPE FLOW) CALC PEAK FLOW AT MH TO UNDER CARDIFF

"QA/640" 5YR .0154 + .0011 = .0165
 100YR .0429 + .0029 = .0458

T_e: UP TO BASIN 13.3 MIN 13.3
 THRU BASIN: 250 LF PIPE FLOW
 ASSUME 30" FULL ≈ 9 f/s 0.5 MIN

q_p = 1010 csm/in 13.8 MIN ≈ 1.23 h
 q₅ = 1010 * 0.0165 = 16.7 cfs
 q₁₀₀ = 1010 * 0.0458 = 46.2 cfs

PRORATE QA/640 TO ACCOUNT FOR INLET INTERCEPTION AT PIPE

5" QA/640 AT INLET (SEE PG D.3) .0037 q₅ = 4.7 q_{inlet} 2.8
 .0037 / 4.7 * 2.8 = .0022

100" QA/640 AT INLET (SEE PG D.3) .0096 q₁₀₀ = 12.3 q_{inlet} 5.4
 .0096 / 12.3 * 5.4 = .0042

q₅ AT PIPE (.0165 + .0022) * 1010 = 18.9 cfs
 q₁₀₀ AT PIPE (.0458 + .0042) * 1010 = 50.5 cfs

Project BROADMOOR BLUFFS ESTATES	EXHIBIT "E"	Job No E 3098
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Client GATES LAND CO.	By dlm	Date Dec 10, 1984
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CHO: RD III 12-14-84

THRU BASIN "G" (THRU C3 + THRU B)

"QA/640" 5YR .0144 + .0187 + .0072 = .0403
 100YR .0470 + .0500 + .0202 = .1172

Tc: NORTH ROUTE FROM C2

TO BASIN 13.8 MIN

THRU BASIN 600' SWALE AT 10% (4 fps) 2.5 MIN

250' SWALE AT 6% (3 fps) 1.4 MIN

17.7 MIN x 0.30h

SOUTH ROUTE FROM B

TO BASIN 12.5 MIN

THRU BASIN 250' SWALE AT 6% (3 fps) 1.4 MIN

570' SWALE AT 10% (4 fps) 2.4 MIN

250' SWALE AT 6% (3 fps) 1.4 MIN

17.7 MIN x 0.30h

$q_p = 920 \text{ csm/in } (T_c = 0.30h)$

$q_s = 920 \times 0.0403 = 37.0 \text{ cfs}$

$q_{100} = 920 \times 0.1172 = 107.8 \text{ cfs}$

THRU BASIN "D2" (D2+3)

"QA/640" 5YR .0032 + .0009 = .0041

100YR .0091 + .0026 = .0117

Tc: OFFSITE 55' OVERLAND AT 55% (2.4 fps) 0.4 MIN

100' OVERLAND AT 10% (1.0 fps) 1.7 MIN

2.1 MIN

ONSITE "B" 9.5 MIN

$T_c = 11.6 \text{ MIN} = 0.19 \text{ h}$

$q_p = 1080 \text{ csm/in}$

$q_s = 1080 \times 0.0041 = 4.4 \text{ cfs}$

$q_{100} = 1080 \times 0.0117 = 12.6 \text{ cfs}$

Project BROADMOOR BLUFFS ESTATES EXHIBIT "E" Job No E 3098

Client GATES LAND CO. By djh Date DEC. 10, 1984

CAD: ROD III 12-14-84

PRORATE "QA/640" PICKED UP BY INLET AT CHESHIRE

5 YR .0041 $q_5 = 4.4$ $q_{INLET} 2.6$ (pg D3)
 $.0041 / 4.4 * 2.6 = .0024$

100 YR .0117 $q_{100} = 12.6$ $q_{INLET} 6.4$ (pg D3)
 $.0117 / 12.6 * 6.4 = .0059$

USE LATER FOR FLOWS TO E1

THRU BASIN "E1" E4 + 4 + 5 + CHESHIRE & REGINOLD RELEASES
 (SEE pg D9)

$QA/640$ 5 YR $.0095 + .0248 + .0010 + .0024 + .0111 = .0488$
 $.0273 + .0791 + .0028 + .0059 + .0293 = .1440$

$T_c = .21 + .12 = 0.33$ h

$q_p = 880$ csm/in

$q_5 = 880 * .0488 = 42.9$ cfs

$q_{100} = 880 * .1440 = 126.7$ cfs

Flow AT END OF CHESHIRE COURT IN NATURAL SWALE

TRIBUTARY E1 = 2.8 ac $QA/640$ 5 YR $.47 * 2.8 / 640 = .0020$
 100 YR $1.36 * 2.8 / 640 = .0060$

+ 4 + 5

$QA/640$ 5 $.0020 + .0248 + .0010 = .0278$
 100 $.0060 + .0791 + .0028 = .0879$

$T_c = 0.21$ h

$q_p = 1050$

$q_5 = 1050 * .0278 = 29.2$ cfs

$q_{100} = 1050 * .0879 = 92.3$ cfs

Project	BROADMOOR BLUFFS ESTATES	EXHIBIT "E"	Job No E 3098
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Client	GATES LAND CO	By dlh	Date DEC 10, 1984
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CAO: ROO III 12-14-84

Flow AT END OF CULVERT (SUMP CONDITION ONCARDIFF)

Flow IN SWALE TO CULVERT + INLET RELEASE

$$QA/640 \text{ SYR } .0403 + .0059 + .0012 = .0474$$

$$100YR \quad .1172 + .0138 + .0020 = .1330$$

↑ AREA ↑ P1 D2 ↑ P1 C5

$T_c = .30h$

$q_p = 920$

$q_B = 920 * .0474 = 43.6 cfs$

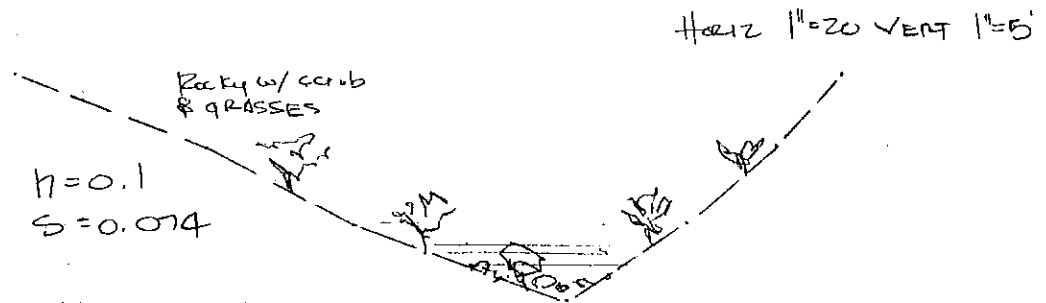
$q_{100} = 920 * .1330 = 122.4 cfs$

Project BROADMOOR BLUFFS ESTATES		EXHIBIT "E"	Job No E 3098
Client GATES LAND CO.	By djm	Date DEC. 10, 1984	

CKO: R00III 12-14-84

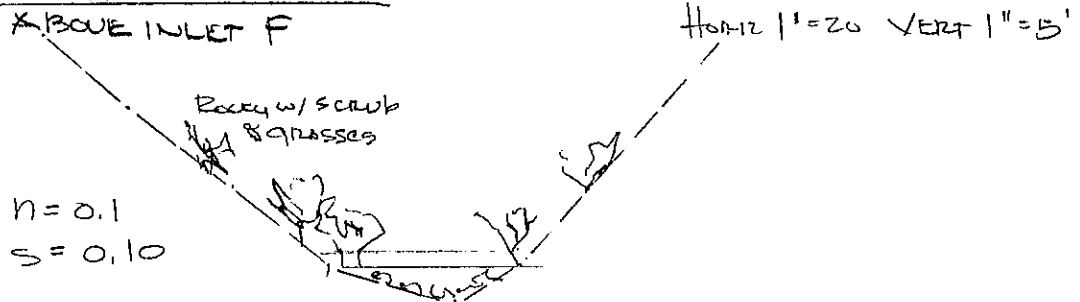
NATURAL SWALE FLOW CHECKS

TYPICAL SECTION BASIN "B" BEFORE CULVERT



if d = 2'	if d = 1.5'	if d = 1.25'	
A = 38sf	A = 22.5	A = 16.4	
WP = 35	WP = 27	WP = 22	
R = 1.09	R = 0.833	R = 0.744	
Q = 163 NQ	Q = 80.7 NQ	Q = 54.6	V = 3.3 fps <u>OK</u>

TYPICAL SECTION BASIN "C2" ABOVE INLET F



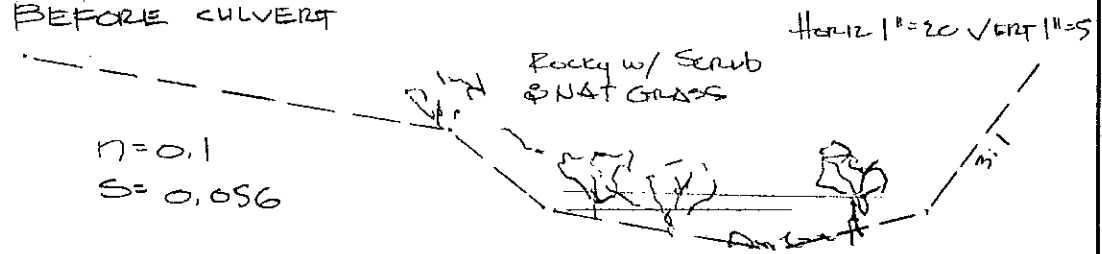
if d = 1'	if d = 1.25'	
A = 12sf	A = 17.3	
WP = 20	WP = 22	
R = 0.6	R = 0.79	
Q = 40.2 NQ	Q = 69.6	V = 4 fps <u>OK</u>

Project: **BROADMOCK BLUFFS ESTATES** EXHIBIT "E" Job No: **E 3098**

Client: **GATES LAND Co.** By: **djh** Date: **DEC. 10. 1984**

CRD: RUD III 12-14-84

TYPICAL SECTION BASIN "G" BEFORE CULVERT



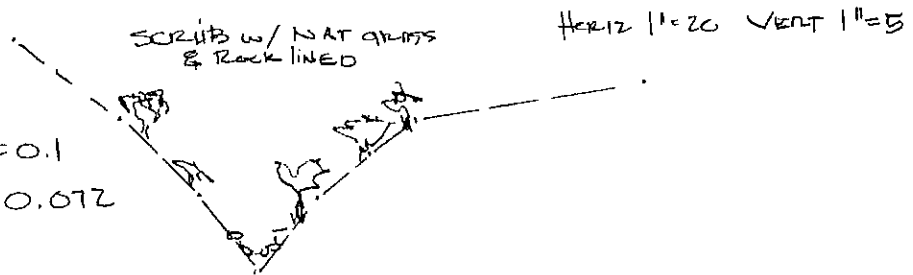
$n = 0.1$
 $S = 0.056$

if $d = 1'$
 $A = 22 \text{ sf}$
 $WP = 40$
 $R = 0.55$
 $Q = 52.1 \text{ cfs NG}$

if $d = 1.5'$
 $A = 43 \text{ sf}$
 $WP = 40$
 $R = 0.977$
 $Q = 152 \text{ cfs}$ $V = 3.6 \text{ fps}$ OK

TYPICAL SECTION BASIN E1

AT REGIMENTS ET



$n = 0.1$
 $S = 0.072$

if $d = 2'$
 $A = 13 \text{ sf}$
 $WP = 13.6$
 $R = 0.956$
 $Q = 50.4 \text{ cfs NG}$

if $d = 3'$
 $A = 32.4 \text{ sf}$
 $WP = 21'$
 $R = 1.544$
 $Q = 173 \text{ cfs}$ OK 5.3 fps

EXHIBIT "F"
STORM SEWER AND CULVERT CALCULATIONS

Project: **BROADMOOR BLUFFS ESTATES** **EXHIBIT "F"** Job No: **E 3098**

Client: **GATES LAND CO.** By: **d/h** Date: **DEC 10. 1984**

CRD: **RD III 12-14-84**

SIZE STORM PIPES

UNDER CARDIFF AT BASIN "B"

$q_5 = 15.0 \text{ cfs}$ $q_{100} = 48.9 \text{ cfs}$

TRY 30" RCP (SEE FOLLOWING CHARTS)

INLET CONTROL $H_w/d = 2.0$ $q = 50 \text{ cfs}$
 $H_w/d = 0.75$ $q = 15 \text{ cfs}$
 $H_w/d = 1.0$ $q = 24 \text{ cfs}$

GRAVITY FLOW AT 1.0% 40 cfs AT 9 FPS FULL

UNDER CARDIFF AT BASIN "G"

$q_5 = 37.0 \text{ cfs}$ $q_{100} = 107.8 \text{ cfs}$

TRY 48" RCP (SEE FOLLOWING CHARTS)

INLET CONTROL $H_w/d = 1.28$ $q = 108 \text{ cfs}$
 $H_w/d = 0.64$ $q = 37 \text{ cfs}$
 $H_w/d = 1.0$ $q = 78 \text{ cfs}$

GRAVITY FLOW AT 1% 140 cfs AT 12 FPS

INLET & PIPE SYSTEM AT GLOUCESTER

$q_5 = 15.9 \text{ cfs}$ $q_{100} = 44.2 \text{ cfs}$

DESIGN INLET OPENING TO INTERCEPT ROYR WITH $H_w = 2.5'$

$44.2 = .83 A \sqrt{2 \times 32.2 \times 2.5}$ $A = 4.2 \text{ SQ. FT.}$

ALLOW FOR TRASH PLUGGING $4.2 \times 1.5 = 6.3 \text{ SF OPENING}$

INLET MUST BE APPROX. 15' DEEP TO CLEAR UTIL. IN GLOUCESTER.

PIPE OUT TRY 30" RCP AT 1.2% GRAVITY FLOW = 45 cfs
 FROM MH TO MH PIPE GRADE 4.5% GRAVITY FLOW = 85 cfs

Project: BROADMOOR BLUFFS ESTATES EXHIBIT "F" Job No: E 3098

Client: GATES LAND CO By: d/h Date: DEC 10, 1984

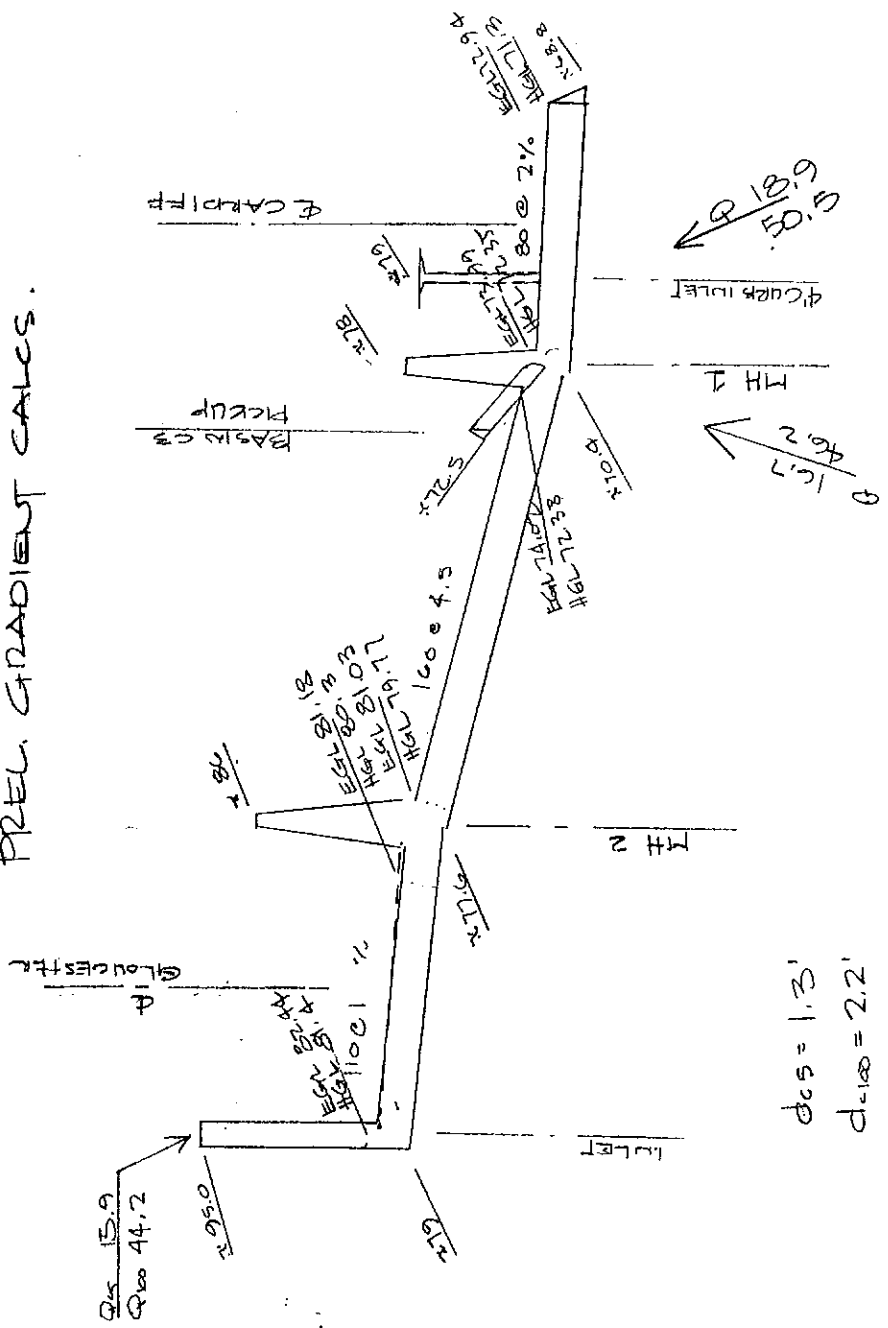
CAD: #00112-14-84

9 AT PIPE CROSSING CARDIFF (SEE PG E3)

$Q_{75} = 18.9 \text{ cfs}$ $Q_{100} = 50.5 \text{ cfs}$

30" CROSS CULVERT AT 2% GRAVITY FLOW 58 cfs $V = 14 \text{ fps}$

PREL. GRADIENT CALCS.



$d_{75} = 1.35'$ $d_{100} = 1.5'$
 $d_{75} = 2.25'$ $d_{100} = 2.3'$

$d_{75} = 1.3'$
 $d_{100} = 2.2'$

Project BROADMOOR BLUFFS ESTATES	EXHIBIT "F"	Job No E 3098
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Client GATES LAND CO	By dlh	Date DEC 10. 1984
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CAD: R00III 12-14-84

PRELIMINARY RUN THRU STORM SEWER AT BASIN C3
(GRADES MAY CHANGE WHEN UTILITIES ELEV. ARE ALL ESTABLISHED)

OUTFALL AT BASIN G

DESIGN Q = 50.5 cfs $n = 0.013$
 DIA PIPE = 30"
 AREA PIPE (FULL) = 4.91 SF
 $V = Q/A = 10.3 \text{ fps}$ $\sqrt{2/2g} = 1.64' = H_v$
 SET INV. AT 68.8
 $D = 2.5$
 71.3 HGL EGL 72.94

OUTFALL TO MH1

L = 80' D = 2.5' Q = 50.5 cfs A = 4.91
 $H_f = f \frac{LV^2}{2gd} = 1.05'$ $S_f = 0.0131$
 $S_o = 0.02$ OPEN CHANNEL FLOW BUT ASSUME FULL

MH 1 4' DIA MH

INV OUT = $80 \times 0.02 + 68.8 = 70.4$
 HGL₀ = $71.3 + 1.05 = 72.35$
 EGL₀ = $72.35 + 1.64 = 73.99$
 $D_u/D_o = 2.5/2.5 = 1.0$ $A/d_u = 4/2.5 = 1.6$
 FROM FIG 8.7 (DRECOG) $K_u = 0.02$ SET INV AT 70.5 Rounding at outlet
 $h_u = K_u \frac{V^2}{2g} = 0.2 \times \frac{10.3^2}{64.4} = 0.3$
 HGL_u = $72.35 + 0.3 = 72.38$ EGL_u = 74.02

MH1 TO MH2

L = 160 D = 30" Q = 44.2 cfs A = 4.91 SF V = 9.6 fps
 $S_f = 0.0100$ $S_o = 0.045$ OPEN CHANNEL FLOW

Project: **BROADMOOR BLUFFE ESTATES** **EXHIBIT "F"** Job No: **E 3098**

Client: **GATES LAND CO.** By: **dlp** Date: **DEC. 10, 1984**

CAD: **RDO III 12-14-84**

MH 2

OPEN CHANNEL FLOW THRU MH.

USE $H_L = .2 (H_{V_6} - H_{V_u})$

FIND H_{V_6} $d = 30"$ $S = 0.045$ $Q = 44.2 cfs$
FROM K & B TABLE 7-14

$Q = K' / n \cdot d^{8/3} S^{1/2}$ $K' = 0.235$

$D/d = .505$ & $d = 2.5 \Rightarrow D_n = 1.26'$

TABLE 7-4

$D/d = .505$ $C_a = 0.613$ $a = .613 \times 2.5^2 = 3.83 SF$

$V_6 = 44.2 / 3.83 = 11.5 fps$ $H_{V_6} = \sqrt{2/2g} = 2.07'$

FIND H_{V_u} - SET $S_o = SF$ ASSUME FULL FLOW

$V_u = 44.2 / 4.90 = 9.0 fps$ $H_{V_u} = 81 / 64.4 = 1.26$

$H_L = 0.2 (2.07 - 1.26) = 0.15$

CHECK UPSTREAM INV. BY EQUATING ENERGY GRADES

DS INV. $70.5 + (160 \times 0.045) = 77.7$

D_n + 1.26

$D D_{H_v}$ + 2.07

DS EGL 81.03

H_L + 0.15

US EGL 81.18

US H_v - 1.26

US DIA - 2.50

77.42 ?

SET INV US AT 77.8

$HGL_u = 77.8 + 2.5 = 80.3$

Project BROADMOOR BLUFFS ESTATES	EXHIBIT "F"	Job No E 3098
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Client GRAVES LAND CO	By dlm	Date DEC 10, 1984
--------------------------	-----------	----------------------

CRD: R00 III 12-14-84

MH 2 TO INLET

$$L=110 \quad D=36" \quad Q=44.2 \quad X=4.90 \text{ SF} \quad V=9.0 \text{ FPS}$$

$$V^2/2g = 1.26'$$

$$S_f = 0.01$$

SET S_o AT 0.01 ASSUME FULL FLOW

AT INLET

$$1.5V \text{ OUT } 72.9$$

$$HGL_o = 80.3 + (0.01 \times 110) = 81.4$$

$$EGL_o = 81.18 + 1.26 = 82.44$$

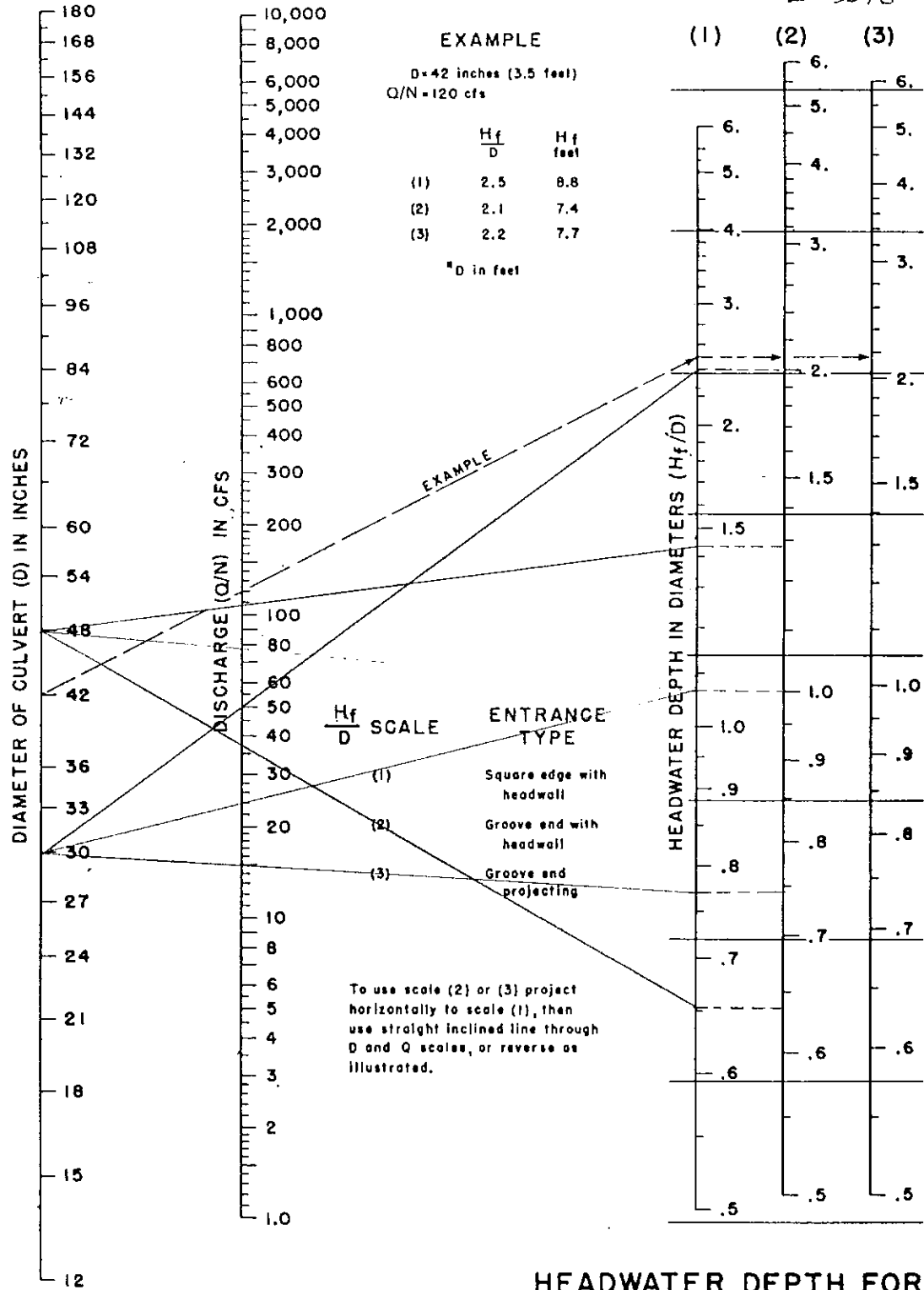
PREL. Rough Run thru shown no problems.

RECOMMEND SET PIPE UNDER GLOUCESTER AT 1.2%
BETWEEN MH 1 & 2 USE 24" PIPE TO SAVE COST.

NOTE: WHEN RELATIONSHIPS WITH OTHER UTILITY LINES IS
CALCULATED GRADES MAY SLIGHTLY VARY &
CALCULATIONS WILL BE FINALIZED & DETAILED.

Chart 11

E. 3098

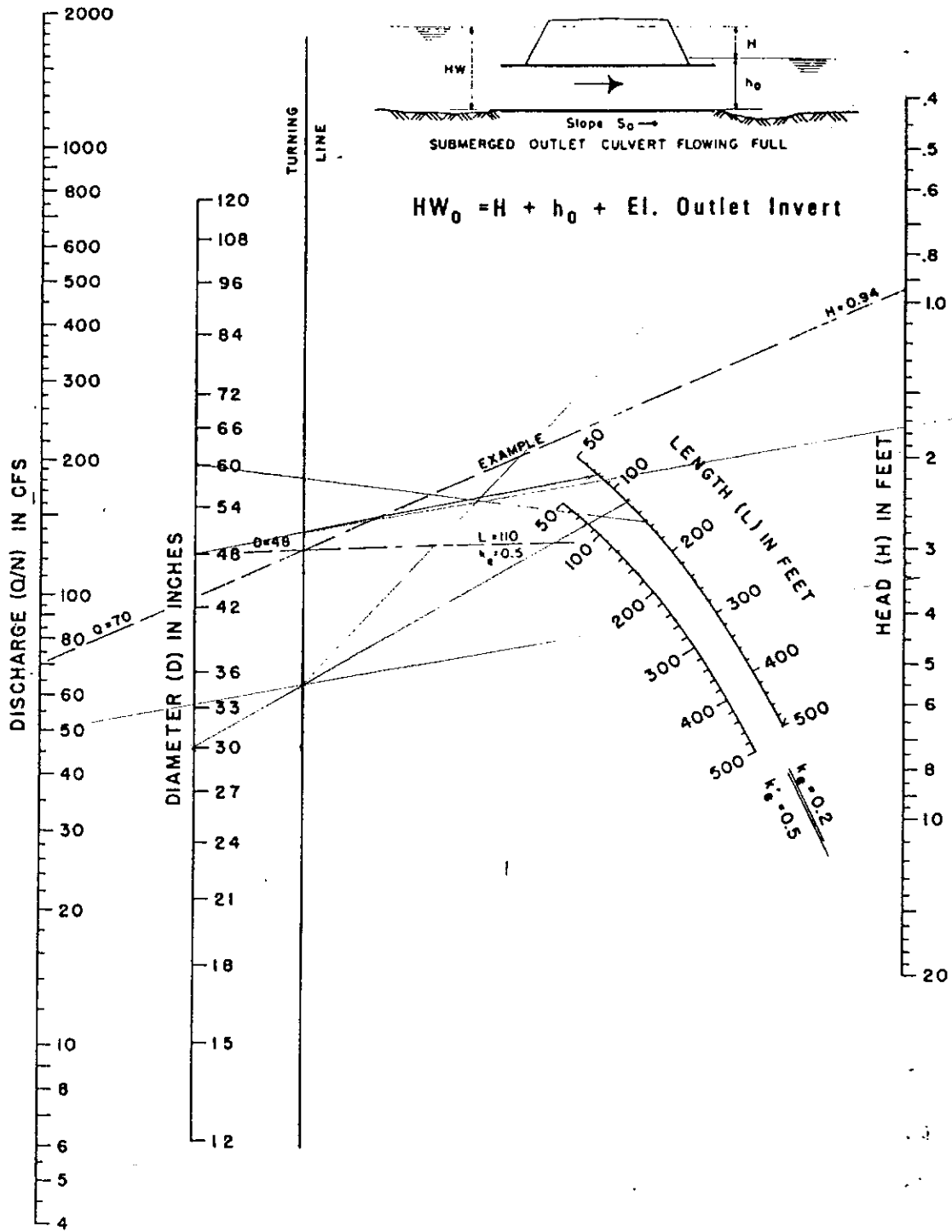


48" Rep

30" Rep

HEADWATER DEPTH FOR CONCRETE PIPE CULVERTS WITH INLET CONTROL

Chart 2



PROJECT: E 3098 GOTES

DESIGNER: dh

DATE: DEC 7 84

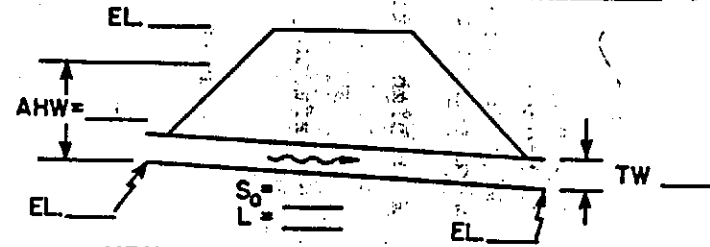
HYDROLOGIC AND CHANNEL INFORMATION

$Q_1 =$ _____ $TW_1 =$ _____
 $Q_2 =$ _____ $TW_2 =$ _____

(Q_1 = DESIGN DISCHARGE, SAY Q_{25}
 Q_2 = CHECK DISCHARGE, SAY Q_{50} OR Q_{100})

SKETCH

STATION: _____



MEAN STREAM VELOCITY = _____
 MAX. STREAM VELOCITY = _____

5-18

WEST
CARDIFF →

EAST
CARDIFF →

Figure 7

CULVERT DESCRIPTION (ENTRANCE TYPE)	Q	SIZE	HEADWATER COMPUTATION										CONTROLLING HW	OUTLET VELOCITY	COST	COMMENTS
			INLET CONT.		OUTLET CONTROL					HW = H + h ₀ - LS ₀						
			HW D	HW	K _e	H	d _c	$\frac{d_c + D}{2}$	TW	h ₀	LS ₀	HW				
RCP w/ FES	48.9	30"	2.0	5.0	0.2	3.4	2.3	2.4	1.2	2.4	1.2	4.6	INLET			
RCP w/ FES	15.0	30"	.74	1.85	0.2	0.3	1.3	1.9		1.9	1.2	1.0	INLET			
RCP w/ FES	107.8	48"	1.28	5.12	0.2	1.75	3.2	3.6		3.6	.74	4.6	INLET			
RCP w/ FES	37.0	48"	.64	2.56	0.2	.2	2.0	3.0		3.0	.74	2.46	INLET			

SUMMARY & RECOMMENDATIONS:

EXHIBIT "F"
 8/8
 E 3098

EXHIBIT "G"
DRAINAGE STRUCTURE COST ESTIMATE

EXHIBIT "G"

COST ESTIMATE
FOR THE
SINGLE-FAMILY PORTION
OF
BROADMOOR BLUFFS ESTATES

ITEM	UNIT	QUANTITY	UNIT COST	AMOUNT
18" RCP (C-76, Cl. III)	L.F.	374	\$ 25.00	\$ 9,350.00
24" RCP (C-76, Cl. III)	L.F.	160	35.00	5,600.00
30" RCP (C-76, Cl. III)	L.F.	310	50.00	15,500.00
48" RCP (C-76, Cl. III)	L.F.	74	75.00	5,550.00
18" RCP end section	Each	2	400.00	800.00
30" RCP end section	Each	3	650.00	1,950.00
48" RCP end section	Each	2	1,100.00	2,200.00
Std. 4' manholes	Each	2	1,500.00	3,000.00
Grated inlet (deep)	Each	1	4,000.00	4,000.00
Std. 4' D-10-R curb inlet	Each	1	1,500.00	1,500.00
Std. 6' D-10-R curb inlet	Each	2	2,000.00	4,000.00
Std. 8' D-10-R curb inlet	Each	2	3,000.00	6,000.00
18" dia. rip-rap	Cu Yd	400	50.00	<u>20,000.00</u>
			Total	\$79,450.00