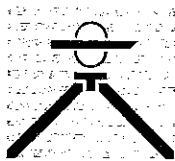
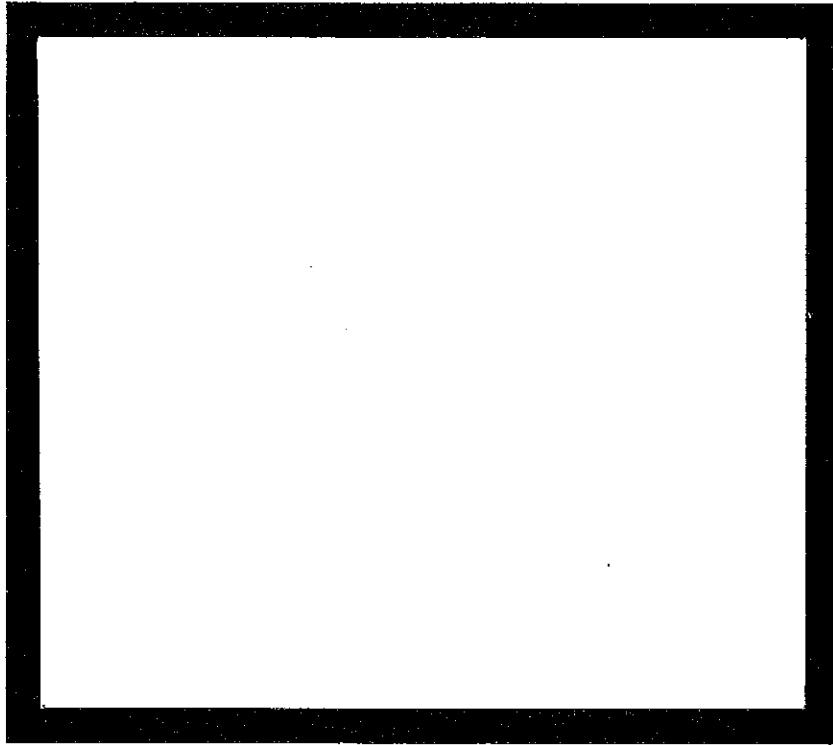


**NOT TO BE  
CHECKED OUT**



**Drexel Barrell**

**Engineers/Surveyors  
Incorporated**

**Boulder,  
Colorado Springs**

4840 Pearl East Circle  
Suite 114  
Boulder, Colorado 80301

303 442 4338

**MASTER DEVELOPMENT DRAINAGE PLAN  
FOR REGIONAL  
DETENTION PONDS  
AT BROADMOOR BLUFFS  
COLORADO SPRINGS, COLORADO**

Prepared By:

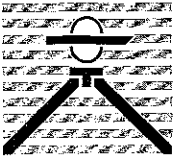
**DREXEL BARRELL  
4840 Pearl East Circle  
Suite 114  
Boulder, Colorado 80301**

Prepared For:

**GATES LAND COMPANY  
202 E. Cheyenne Mountain Blvd.  
Colorado Springs, Colorado  
80906**

Date: January 24, 1989  
Revised: May 31, 1989  
Revised: October 26, 1989  
Revised: February 28, 1990  
Revised: February 8, 1991  
Revised: May 13, 1991  
Revised: June 17, 1993  
Revised: April 19, 1994

EW-1011  
(0280R.RM)



Drexel Barrell

RECEIVED

AUG 28 1996

CITY OF COLORADO SPRINGS

Engineers/Surveyors  
Incorporated

Letter of Transmittal

Boulder,  
Colorado Springs

To: CITY OF C.S. Date 8/26/96

6365 Corporate Drive  
Colorado Springs,  
Colorado 80919

STRAWMASTER & SUBDIVISION  
101 WEST CASTILLA  
CS CO 80903

- Via Carrier
- Time Delivered By \_\_\_\_\_
- Mail
- Fed Express/Express Mail
- Phone Number \_\_\_\_\_
- Other \_\_\_\_\_

719 260 0887  
719 260 8352 Fax

Attention ROBIN KIDDER

Job No. EW-1011

RE: MDDP for Regional Detention Ponds  
at Broadmoor Bluffs

We are sending you:

- Prints  Original  \_\_\_\_\_
- Sepia  Report  \_\_\_\_\_

No. Copies	Dwg. No.	Description
<u>1</u>		<u>Revision to Det. Pond No. 2 Construction Estimate</u>

These are transmitted

as checked below:

- For your information  As requested  For your processing
- For your approval  Other Amend report

Remarks

Robin  
It has been brought to our attention  
that the 96" RCP quantity is incorrect  
as shown on page 7 in the above  
mentioned report. Attached is an amended  
table. Please attach to your reports on file.

Thank You

Copy to: Bob Szejtkovsky Signed: [Signature]  
file

**DETENTION POND NO. 2 (SOUTH) (revised\*)**

<b>ITEM</b>	<b>QTY</b>	<b>UNIT</b>	<b>UNIT \$</b>	<b>TOTAL</b>
Earthwork	34,000	CY	\$2	\$68,000
Seeding	8	AC	\$2,000	\$16,000
Rip-rap	330	CY	\$50	\$16,500
96" RCP*	250	LF	\$325	\$81,250
Inlet	L.S.	L.S.	\$15,000	\$15,000
Low Flow Channel	1500	LF	\$60	\$90,000
Emergency Spillway				
Cut off walls	L.S.	L.S.	\$50,000	\$50,000
<b>SUBTOTAL</b>				<b>\$336,750</b>
Contingencies (15%)				\$50,513
Legal, Engineering & Admin costs (15%)				\$50,513
<b>SUBTOTAL</b>				<b>\$437,776</b>
Land 7.2 acres @ \$15,200/AC				\$109,440
<b>TOTAL</b>				<b>\$547,216</b>

\* 96"RCP length reduced from 750' to 250'

**Engineer's Statement:**

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City/County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



*FOR REVIEW & APPROVAL*



**Developer's Statement:**

I, the developer have read and will comply all of the requirements specified in this drainage report and plan.

Gates Land Co.  
Business Name

By: \_\_\_\_\_

Title: \_\_\_\_\_

Address: 202 E. Cheyenne Mountain Blvd.  
Colorado Springs, Co 80906

**Developer's Statement:**

I, the developer have read and will comply all of the requirements specified in this drainage report and plan.

\_\_\_\_\_  
Business Name

By: \_\_\_\_\_

Title: \_\_\_\_\_

Address: \_\_\_\_\_  
\_\_\_\_\_

**Developer's Statement:**

I, the developer have read and will comply all of the requirements specified in this drainage report and plan.

\_\_\_\_\_  
Business Name

By: \_\_\_\_\_

Title: \_\_\_\_\_

Address: \_\_\_\_\_  
\_\_\_\_\_

**Developer's Statement:**

I, the developer have read and will comply all of the requirements specified in this drainage report and plan.

\_\_\_\_\_  
Business Name

By: \_\_\_\_\_

Title: \_\_\_\_\_

Address: \_\_\_\_\_  
\_\_\_\_\_

**Developer's Statement:**

I, the developer have read and will comply all of the requirements specified in this drainage report and plan.

\_\_\_\_\_  
Business Name

By: \_\_\_\_\_

Title: \_\_\_\_\_

Address: \_\_\_\_\_  
\_\_\_\_\_

**Developer's Statement:**

I, the developer have read and will comply all of the requirements specified in this drainage report and plan.

\_\_\_\_\_  
Business Name

By: \_\_\_\_\_

Title: \_\_\_\_\_

Address: \_\_\_\_\_  
\_\_\_\_\_

**Developer's Statement:**

I, the developer have read and will comply all of the requirements specified in this drainage report and plan.

\_\_\_\_\_  
Business Name

By: \_\_\_\_\_

Title: \_\_\_\_\_

Address: \_\_\_\_\_  
\_\_\_\_\_

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## GENERAL LOCATION AND DESCRIPTION

### Purpose

The purpose of this study is to provide a schematic design and cost allocation for proposed regional detention ponds located at Broadmoor Bluffs just west of State Highway 115. The contributing drainage area is partially developed and consists of numerous owners and developments. The need for regional detention ponds has been documented by the Master Drainage Study for Neal Ranch and updates (Reference 4 and 5). Regional detention ponds are necessary to reduce developed discharge to historic rates in accordance with requirements of the City of Colorado Springs Drainage Criteria Manual.

This study is not intended to serve as a Master Development Drainage Plan for the entire basin and does not include all elements normally required by the Drainage Criteria Manual of the City of Colorado Springs (Reference 1). The report also does not address detention ponds or drainage improvements for which Broadmoor Bluffs is the only contributing drainage area. It is recognized that detention facilities and other drainage improvements will be necessary for Broadmoor Bluffs, however, these will be addressed at a later date as development of Broadmoor Bluffs occurs. Only regional detention facilities are addressed in this report. The study is prepared for Gates Land Company (owners of Broadmoor Bluffs), however, it is anticipated that other upstream landowners with potential future development will participate in funding of the detention facilities shown in this study.

The intent of this most recent edition (April 19, 1993) is to incorporate City of Colorado Springs review comments, reflect changes in ownership within the basin and to update known land use data for the Broadmoor Master Plans which, according to current plans, will be less intensely developed than indicated previously. Minor changes were made to drainage areas in the computer model due to more accurate mapping available for individual parcels. Original basin boundaries were based on USGS quad sheets. These changes do not result in significant changes to basin hydrology and do not affect the overall concept. In addition, two regional detention ponds at Broadmoor Bluffs and three temporary detention areas are evaluated in this report. The location of the proposed detention ponds is shown on Sheet 1 of the drainage plans included with this report. The temporary detention areas were constructed in Mountain Oaks Filing No. 2 (Reference 6) and Country Walk at Broadmoor and Glen Oaks at Broadmoor Filing No. 2 (References 7 and 8).

### Location

Broadmoor Bluffs is located in Section 7 and the South 1/2 of Section 6, T15S, R66W, City of Colorado Springs, El Paso County, Colorado. It is bordered on the east by State Highway 115, on the north by Broadmoor Valley, on the west by Broadmoor Oaks and the J.L. Ranch and on the south by the Bensburg Estate. Fort Carson lies immediately east of State Highway 115. The location of Broadmoor Bluffs is shown on Figure 1 in the Appendix.

## Zoning & Revisions

The existing plan as submitted herein is accurate for the current zoning of the property within the project. Zoning changes, road alignments and other elements are currently being considered for the project and as of the date of this edition have not been approved or completed their processing processed through the City to a level which would reflect sufficient need to update this report. The developer will revise and resubmit all maps, hydrological data and this report when approvals are secured for such zoning and alignment changes from the City. It shall be each developers responsibility to demonstrate that the changes are "minor", and create no substantiative increases or consequences to release rates presented herein.

## Description

The total drainage area evaluated in this study is 2.55 square miles (1630 acres) and extends from State Highway 115 on the east side to the top of Cheyenne Mountain approximately 2-3/4 miles west of State Highway 115. Slopes range from approximately 100% on the mountain in the western portion of the basin to approximately 10% or less in the eastern portion of the basin. Several unnamed channels traverse the drainage area from the west to east and discharge from the drainage areas is conveyed under State Highway 115 by several culverts. Some existing temporary, privately maintained detention ponds to the West provide some flood control at the present time. These will be discussed in more detail later in this report.

Soils consist primarily of rock outcrops in the extreme western portion of the basin, sandy and rocky loam (Bresser and Jarre-Tecolote Complex) in the central portion of the basin and clayey soils (Razor and Razor-Midway complex) in the eastern portion of the basin.

Portions of the basin are currently developed including the northwestern portion of Broadmoor Bluffs and portions of Broadmoor Oaks. No part of the basin is within an identified floodplain as designated on current FEMA Flood Insurance Rate Maps (Reference 9). Based on field observation, no wetland vegetation appears to be present on the detention pond sites and a Corps of Engineers 404 permit will either not be required or will most likely consist of a nationwide permit, since the disturbed channel is less than an acre. These items shall be verified during final design.

## DRAINAGE DESIGN CRITERIA

### Regulations

#### Governing Criteria

This study was conducted in conformance with the Drainage Criteria Manual of the City of Colorado Springs/El Paso County (Reference 1). The design basis is the 10 year and 100 year 24 hour rainfall event for fully developed conditions.

#### State of Colorado Dam Safety Criteria

Neither of the detention ponds presented herein fall within the jurisdiction of the State Engineer's, Safety of Dams Division. Detention Pond #1 (North) has been designed to be a dry pond whose emergency spillway depth to outfall pipe invert (as defined by the regulations of the State Engineer) is less than 10 feet. Detention Pond #2 (South) is a multipurpose embankment which consists of roadway embankment fill and detention of flood flows; as such, this structure is exempt from State of Colorado jurisdiction.

#### Hydrologic and Hydraulic Criteria

Hydrologic and hydraulic criteria for this study are based on the Drainage Criteria Manual (DCM). Storm discharges were developed for the 10-year and 100-year storm using the Soil Conservation Service TR-20 Computer Program (Reference 3). Discharges were computed for a 24-hour Type IIA rainfall as designated in the DCM. Rainfall depths for the 24-hour rainfall are 4.6 inches and 3.0 inches for the 100-year and 10-year storm respectively. Time of concentrations are determined by combining overland travel times with channel travel times in accordance with the DCM.

The runoff curve number is based on the DCM or SCS publications (Reference 11) for a given land use, soil type and hydrologic soil group. The standard dimensionless unit hydrograph included with TR-20 is also utilized to generate storm hydrographs.

The developer may utilize wetlands mitigation credits in both of the ponds to offset disturbances in other areas.

Hydraulic design parameters are in general obtained from the DCM. Hydraulic parameters used include friction factors, orifice and weir coefficients for the schematic design of detention pond outlet structures.

## DRAINAGE BASINS AND SUB-BASINS

For evaluation of historic conditions, the entire drainage basin was divided into 8 subbasins. For evaluation of developed conditions, the basin was divided into 16 sub-basins. Basin boundaries as currently approved for zoning & roadway alignments are shown on the Land Use/Ownership Map included in the appendix of this report.

## DRAINAGE FACILITY DESIGN

### Design Criteria

A detention pond was evaluated for each of the two basins with drainage areas extending to more than one owner. The detention ponds were evaluated for the 10-year and 100-year storm for a 24-hour rainfall durations. Release rates are designed to be equal to or less than historic at locations where actual historic flows occur.

All regional detention ponds will be constructed to city regulations as required. After construction and acceptance by the city, the detention ponds will become publicly owned and maintained. The detention ponds will consist of earthen embankments with two stage outlet structures to control both a 10-year and 100-year flood. A large pipe and inlet structure will control the 100-year flood and a smaller pipe will control 10-year or smaller floods. The embankment and pond area will have a 4:1 maximum slope to facilitate maintenance. An emergency spillway will be provided to safely convey flows in excess of the 100-year discharge or in the event that the outlet structure becomes inoperable. Current design approach contemplates an emergency spillway with a capacity for passing the peak 100 year developed flow with the ponds full.

### Design Details - Regional Detention Ponds

Detention Pond No. 1 is located just south of Broadmoor Bluffs Drive on the west side of State Highway 115. The structure consists of earth fill along the State Highway 115 right of way to a maximum height of less than 10 feet. Two outlet structures release a total of 430 cfs compared to a historic rate of 460 cfs for the 100-year, 24-hour storm.

Two release structures are shown for Pond 1 to split flow according to historic discharge points. The total 100-year release rate is 430 cfs versus a total downstream capacity of 590 cfs. This should be examined in more detail during final design. Downstream capacity was not evaluated beyond the existing culverts at State Highway 115.

Detention Pond No. 2 is located just west of the State Highway 115 right of way and north of the Bensburg Estate property. This structure consists of earth fill to a maximum height of approximately 28 feet. However based on criteria, it will not be subject to state dam safety requirements. The outlet structure as shown releases a total of 1280 cfs compared to a historic discharge of 1360 cfs for the 100-year, 24-hour storm. The capacity of existing culverts at State Highway 115 is 850 cfs. It should be emphasized that the designs developed in this study are schematic and subject to revision as additional information is developed.

### Design Details - Temporary Detention

Three temporary detention facilities have been constructed with recent site development within the basins and are evaluated schematically in this study.

A 120" structural plate culvert was constructed under Broadmoor Bluffs Drive at the south end of the Country Walk at Broadmoor, No. 4 subdivision. This culvert was designed to provide temporary storage for the subdivision and has a storage volume of 15,050 cu. ft. (0.35 acre-feet)(Reference 7 and 8). This culvert is located on the stream that flows to Regional Detention Pond No. 2 in Drainage Basin 164. The total storage requirement for the 100-year storm at Regional Detention Pond No. 2 is 43.0 acre-feet and assuming that the storage at the 120" culvert reduces the volume required at Regional Detention Pond No. 2 by an equivalent amount, the 100-year reservoir elevation would only be reduced by approximately 0.1 feet and would not have a significant effect on construction cost. The 120" culvert was thus omitted from the TR-20 model for the evaluation.

A 90" culvert was also constructed under Broadmoor Bluffs Drive near the south boundary of Glen Oaks at Broadmoor. This culvert was designed to provide temporary storage for the subdivision and has a storage capacity of 40,504 cu.ft. (0.93 acre-feet). Assuming that the storage at the 90" culvert reduces the volume required at Regional Detention Pond No. 2 by an equivalent amount, the 100-year reservoir elevation would be reduced by approximately 0.2 to 0.3 feet. The 90" culvert is also omitted from the TR-20 model for the evaluation due to the relatively minor effect on the cost of Regional Detention Pond No. 2.

A 60" culvert was constructed as part of Mountain Oaks Subdivision No. 2 in a park located at the downstream end of Basin 061 and provides detention storage of approximately 24354 cu.ft. (0.56 ac.ft.). The culvert is further restricted by a 27" diameter orifice placed at the inlet of the 60" culvert and is intended to provide detention for the Mountain Oaks Subdivision. This structure was evaluated in the TR-20 model both with and without the 27" orifice. Without the orifice, the effect of the detention storage is negligible and has no effect on the 100-year flood elevation of Regional Detention Pond No. 1. With the 27" orifice in place, the temporary detention pond would be overtopped due to flows generated by upstream development. The effect of this temporary detention pond is also negligible and is not included in the final TR-20 results presented in this report. TR-20 printouts for the analysis of the 60" culvert are not included in this report but are available for reference upon request.

### Cost Estimate/Allocation

The construction cost estimates and cost allocation information is provided herein for the use of the developers in establishing cost sharing for the facilities.

The following cost estimates are based on schematic designs presented in this report and are subject to revision during final design. Cost allocations are prorated based on the percentage increase of runoff curve number and the drainage area as shown on Sheet 1 of the drainage plans. The extreme western portion of the basins and U.S. Government property are assumed to remain undeveloped in the future and are omitted from the cost allocation. Areas that were final platted as of January 1994 or specified as park are omitted from the cost allocation. Land acquisition (approximately 12.9 acres for Pond No. 1 and 7.2 acres for Pond No. 2) will be necessary and should be made in accordance with current City policy at the time of construction. No land costs are included in the following cost estimates.

### CONSTRUCTION COST ESTIMATE

#### Detention Pond No. 1 (North)

<u>Item</u>	<u>Quantity</u>	<u>Unit</u>	<u>Price</u>	<u>Total</u>
Earthwork (fill)	40,000	C.Y.	\$2/C.Y.	\$ 80,000
Seeding	11	AC.	\$2000/AC.	22,000
Riprap	170	C.Y.	\$50/C.Y.	8,500
78" RCP	160	L.F.	\$225/L.F.	36,000
54" RCP	180	L.F.	\$100/L.F.	18,000
Concrete risers		L.S.		12,000
Low Flow Channel	950	L.F.	\$50/L.F.	47,500
Riprap Emergency Spillway	900	C.Y.	\$50/C.Y.	45,000
Subtotal				\$269,000
Contingencies (15%)				40,350
Legal, engineering and administrative costs (15%)				<u>40,350</u>
Sub-Total				\$349,700
Land 12.9 Ac. @ \$15,200/AC				<u>196,000</u>
Total				<u>\$545,780</u>

**Detention Pond No. 2 (South)**

<u>Item</u>	<u>Quantity</u>	<u>Unit</u>	<u>Price</u>	
Earthwork	34,000	C.Y.	\$2/C.Y.	\$ 68,000
Seeding	8	AC.	\$2000/AC.	16,000
Riprap	330	C.Y.	\$50/C.Y.	16,500
96" RCP	750	L.F.	\$325/L.F.	243,750
Inlet		L.S.		15,000
Low Flow Channel	1500	L.F.	\$60/L.F.	90,000
Emergency Spillway				
Cutoff Walls	L.S.			<u>50,000</u>
Subtotal				\$499,250
Contingencies (15%)	74,900			
Legal, engineering and				
administrative costs (15%)				<u>74,900</u>
Sub-Total				\$649,050
Land 7.2 Ac. @ \$15,200/AC				<u>\$109,440</u>
Total				<u>\$758,480</u>

All costs based on 1994 dollars (not adjusted for inflation). The runoff curve number is a hydrologic parameter that is based on soil type and land use and is an indicator of the runoff volume from a particular site. Clay soils are less permeable and have a higher curve number than sandy soils, indicating that a larger portion of rainfall will run off and contribute to streamflow downstream. Soil types are classified as A, B, C or D by the SCS with "A" soils being the most permeable and with lower curve numbers and "D" soils being the least permeable with higher curve numbers.

Land use also affects the curve number and "wooded" areas have lower curve numbers than range or pasture conditions. For developed conditions, more dense development results in a higher curve number and thus greater runoff for a given rainfall. The cost allocation shown on the following page is based on the percentage increase in average curve number for each owner from historic to developed condition. To determine the average curve number a curve number is computed for each segment with a different drainage basin, land use or soil type for each owner and averaged based on the area for each owner. Detailed information for each segment is included in Section E at the calculation in the Appendix of this report.

## CONCLUSIONS

This study presents schematic designs and cost estimates for 2 regional detention ponds to serve onsite and offsite drainage areas. The detention ponds are intended to reduce developed flows from the basin to historic discharge rates. Detention Pond No. 1 has an estimated total cost of \$349,700 allocated among 4 upstream owners. Detention Pond No. 2 has an estimated cost of \$649,050 allocated among 7 upstream owners. Costs for land acquisition of approximately 12.6 acres for Pond No. 1 and 7.2 acres for Pond No. 2 will also be necessary and are not included in the above costs. This is a no-fee drainage basin by the terms of the annexation agreement.

## RECOMMENDATIONS

The primary purpose of this study is to establish the procedure for allocating costs of proposed detention facilities to owners within each drainage basin. The following recommendations should apply to further design of the sites and cost allocation to each owner:

- The drainage basin should be converted to a fee basin to provide funding for the final design and construction of the two regional detention ponds shown in this report. The drainage basin fees included in this report apply only to the two regional detention ponds. Costs for other required drainage facilities within the basin should be the responsibility of individual owners.
- Flood routing of the inflow hydrographs should be refined with final design to reflect the final design of each detention pond and insure that discharges are at or below the historic rates for the 10-year and 100-year storms.
- Cost allocations for developers in this report are based on preliminary designs. Final cost allocations, if possible, should be based on a final design or constructed cost.
- This report shall be submitted for review to the Colorado Department of Transportation and Fort Carson. Additional revisions and updates shall also be provided to CDOT and Fort Carson.

Reviewed by,

Prepared by,

Clifford R. Brockman  
Colorado P.E. No. 22117

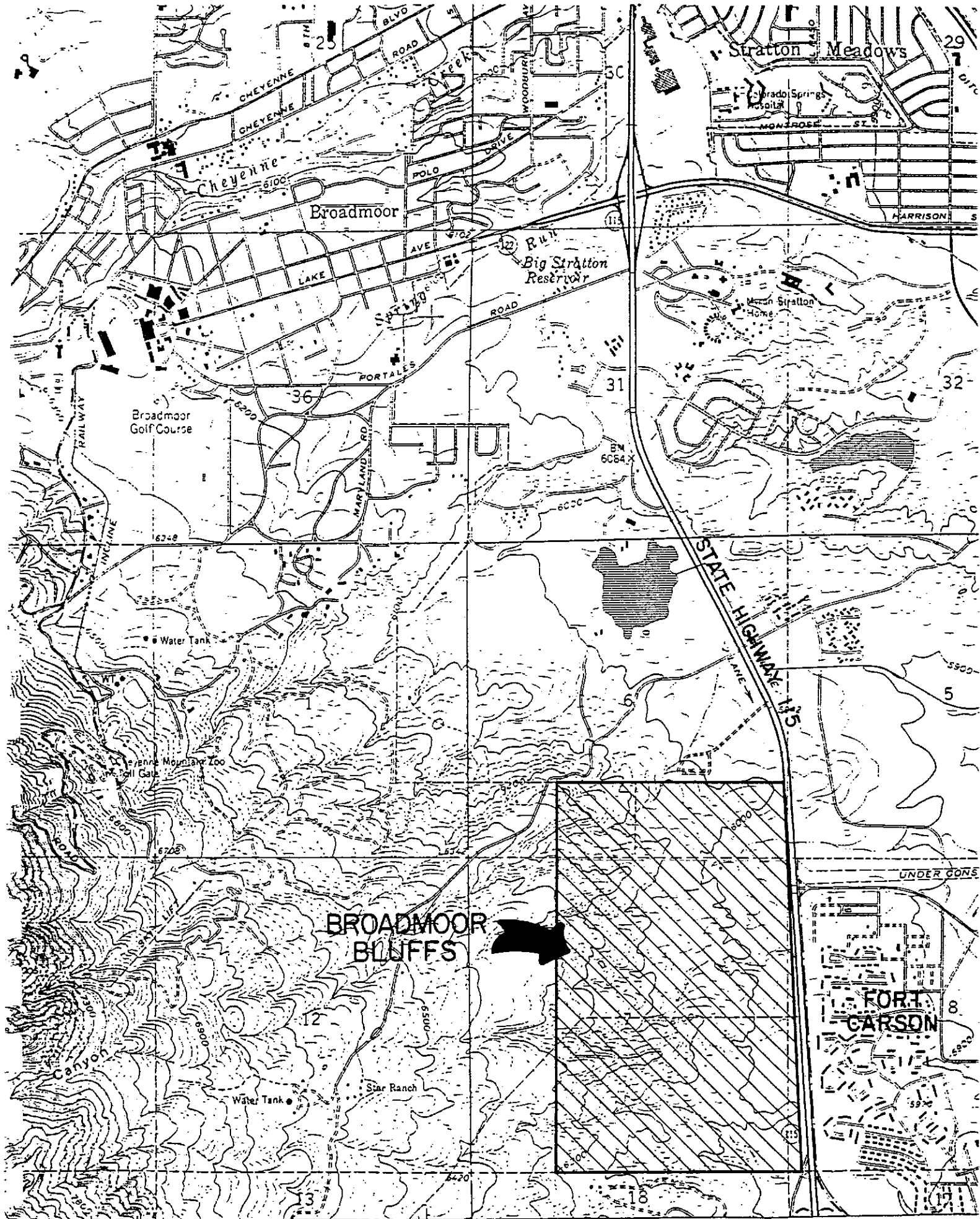
Roger L. Mieden  
Colorado P.E. 23830



## REFERENCES

1. City of Colorado Springs/El Paso County Drainage Criteria Manual; City of Colorado Springs, HDR Infrastructure, Inc., and El Paso County, November 1991.
2. Soil Survey of El Paso County Area, Colorado, United States Department of Agriculture, Soil Conservation Service, June 1981.
3. Technical Release No. 20, User's Manual, Project Formulation - Hydrology (1982 Version), United States Department of Agriculture, Soil Conservation Service, May 1982.
4. Master Drainage Study for Neal Ranch, Weiss Consulting Engineers, Inc., June 24, 1987.
5. Neal Ranch Master Drainage Plan Update, Broadmoor Oaks Filing 3, 4, 7, 8, 9 and 10, Oliver E. Watts, July 21, 1988.
6. Preliminary and Final Drainage Plan and Report, Mountain Oaks Subdivision Filing No. 2, Oliver E. Watts, Consulting Engineer, December 14, 1990.
7. Preliminary and Final Drainage Study, Glen Oaks at Broadmoor, Country Walk at Broadmoor, Glen Oaks at Broadmoor Filing No. 2, Donell Jeffries, October 17, 1988.
8. Country Walk at Broadmoor No. 4, letter report, Jeffries Engineering, June 16, 1992.
9. Flood Insurance Rate Map, City of Colorado Springs, El Paso County, Community Panel Number 080060 0290B, Federal Emergency Management Agency, December 18, 1986.
10. Urban Hydrology for Small Watersheds, Technical Release No. 55, United States Department of Agriculture, Soil Conservation Service, January 1975.
11. Procedures for Determining Peak Flows in Colorado, Soil Conservation Service, U.S. Department of Agriculture, March 1980.

## APPENDIX



S13
S14 R. 67 W. 150'
S15 R. 66 W.
(CHEYENNE MOUNTAIN) 5061 III NE
PENROSE 78 MI
CANON CITY 46 MI

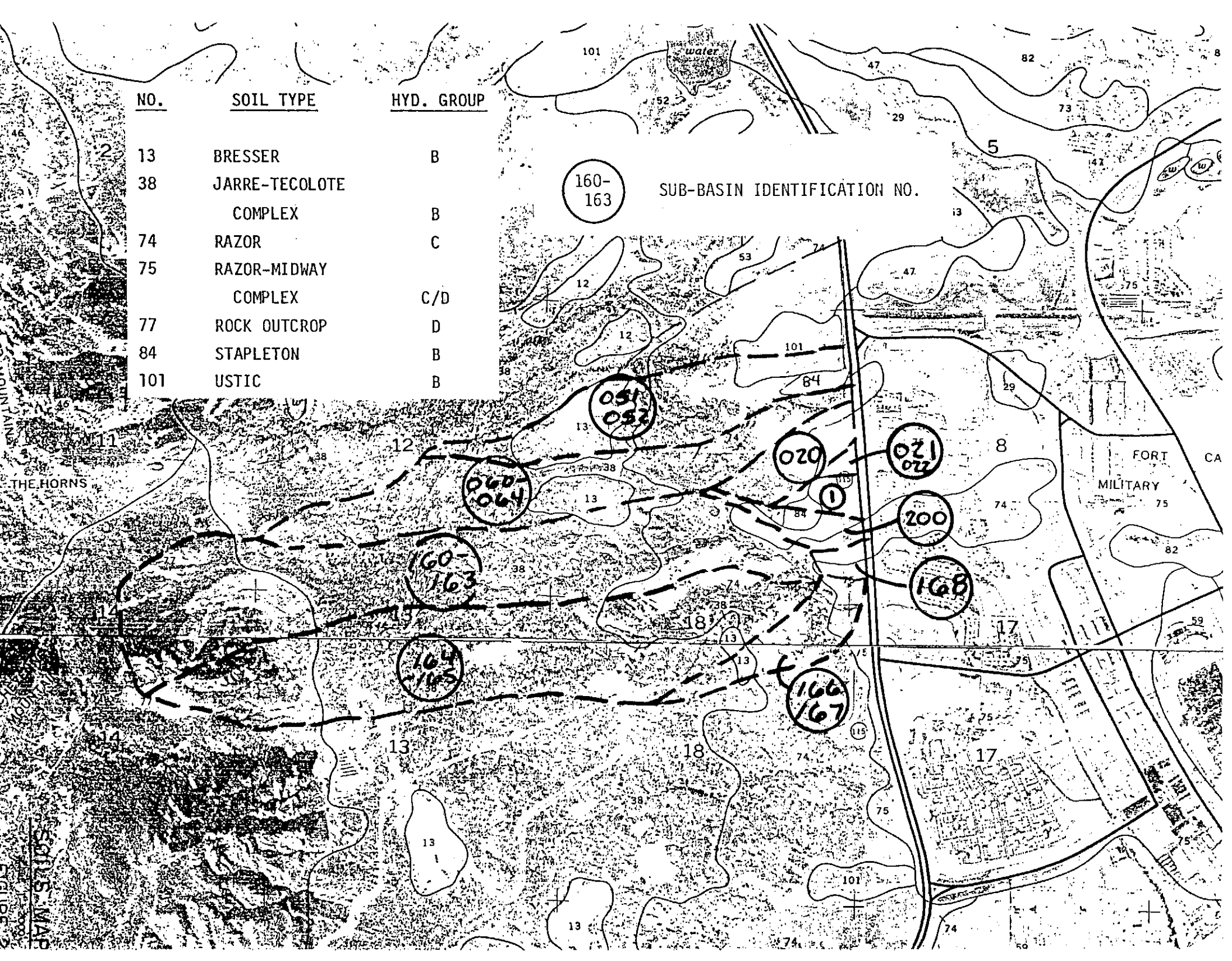
**VICINITY MAP**

SCALE: 1" = 2000'

<u>NO.</u>	<u>SOIL TYPE</u>	<u>HYD. GROUP</u>
13	BRESSER	B
38	JARRE-TECOLOTE COMPLEX	B
74	RAZOR	C
75	RAZOR-MIDWAY COMPLEX	C/D
77	ROCK OUTCROP	D
84	STAPLETON	B
101	USTIC	B

160-163

SUB-BASIN IDENTIFICATION NO.



SOILS MAP  
ENGINEER

Project REGIONAL DETENTION PONDS AT BROADMOOR BLUFFS		Job No EW-1011
Client GATES LAND CO.	By RM	Date 6/17/93

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SCHEMATIC STRUCTURE DESIGN	D1-D15
CURVE NOS. (BASIN & OWNER)	E1-E11
TEMPORARY DETENTION FACILITIES	F1-F8
MISCELLANEOUS CORRESPONDENCE	G1

Project CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (TR-20) Job No E-3729

Client GATES By Rm Date 5 JUNE 83

RAINFALL DATA

ALL BASINS WILL BE EVALUATED FOR THE 10-YEAR AND 100-YEAR RAINFALLS FOR RAINFALL DURATIONS OF 2 HRS. AND 24 HRS. IN ACCORDANCE WITH THE CITY OF COLORADO SPRINGS/EL PASO COUNTY DRAINAGE CRITERIA MANUAL (DCM)

24-HR. PRECIPITATION

$P_{10}(24\text{-HR.}) = 3.0 \text{ IN.}$  (FIG. 5-4d, DCM)  
 $P_{100}(24\text{-HR.}) = 4.6 \text{ IN.}$  (FIG. 5-4e, DCM)

2-HR. PRECIPITATION

2-HR. PRECIPITATION AMOUNTS ARE DERIVED FROM 2-YR., 6-HR. & 24-HR. AND 100-YR., 6-HR. & 24-HR. VALUES AS DESCRIBED IN THE DCM.

2-YR., 6-HR. PRECIP. = 1.6" =  $X_1$  (FIG. 5-4a, DCM)  
 2-YR., 24-HR. PRECIP. = 2.0" =  $X_2$  (" 5-4c, ")  
 100-YR., 6-HR. " = 3.4" =  $X_3$  (" 5-4b, ")  
 100-YR., 24-HR. " = 4.6" =  $X_4$  (" 5-4e, ")  
 ELEV. (IN HUNDREDS) = 65 =  $Z$

2-YR., 1-HR. PRECIP. ( $Y_2$ )  
 $= 0.218 + 0.709 [(X_1)(X_1/X_2)]$   
 $= 0.218 + 0.709 [(1.6)(1.6/2.0)] = 1.13 \text{ IN.}$

100-YR., 1-HR. PRECIP. ( $Y_{100}$ )  
 $= 1.897 + 0.439 [(X_3)(X_3/X_4)] = .008Z$   
 $= 1.897 + 0.439 [(3.4)(3.4/4.6)] = .008(65)$   
 $= 2.48 \text{ IN.}$

Project DRAINAGE W. OF SH 115

Job No  
E-3729

Client GATES,

By RM

Date 3/31/89  
REV. 10/26/39

### HISTORIC CONDITIONS (REVISED $T_c$ 's)

#### BASIN 200

$$T_i: L = 500' \text{ (PASTURE)}$$

$$S = \frac{6148 - 6060}{500} = 18\%$$

$$C = .30 \text{ (PASTURE C/D SOILS)}$$

$$T_i = \frac{1.87(1.1 - C)\sqrt{L}}{\sqrt[3]{S}} = \frac{1.87(1.1 - .30)\sqrt{500}}{\sqrt[3]{18}}$$

$$T_i = 12.8 \text{ MIN.}$$

$$T_f: L = 1600 \text{ FT.}$$

$$S = \frac{6060 - 5969}{1600} = 5.75\%$$

ASSUME CHANNEL w/ 5' B.W.

2.5:1 S/S & 2' DEPTH

$m = .035$  (EARTH w/ SOME ROCKS & VEG.)

$$Q = 239 \text{ CFS } V = 11.9 \text{ } F_r = 1.8$$

$$T_f = \frac{1600}{60(11.9)} = 2.2$$

$$T_c = 12.8 + 2.2 = 15.0 \text{ MIN.} = 0.25 \text{ HR.}$$

#### BASIN 001

$$T_i: L = 500'$$

$$C = .30 \text{ (PASTURE C/D)}$$

$$S = \frac{6106 - 6014}{500} = 18\%$$

$$C = .30 \text{ (PASTURE C/D SOILS)}$$

$$T_i = \frac{1.87(1.1 - .30)\sqrt{500}}{\sqrt[3]{18}} = 12.8 \text{ MIN.}$$

$$T_f: L = 900'$$

ASSUME CHAN. w/ 5' B.W. 2' DEPTH

$$2.5:1 \text{ S/S } S = \frac{6014 - 5964}{900} = 5.5\% \text{ } m = .035$$

$$Q = 233 \text{ } V = 11.7 \text{ } F_r = 1.8$$

$$T_f = \frac{900}{60(11.7)} = 1.3 \text{ MIN.}$$

$$T_c: T_c = 12.8 + 1.3 = 14.1 \text{ MIN.} = 0.24 \text{ HR}$$

Project DEAINAGE W. OF S.H. 115 Job No E-3729

Client GATES By Rm Date 3/31/89  
REV. 10/26/89

EASIN 020 (INCLUDES BASINS 020, 021, 022)

$T_i: L = 500'$   
 $S = 6220 - 6116 / 500 = .21$

C = .30 (PASTURE C/D SOILS)

$T_i = \frac{1.87(1.1 - .30)\sqrt{500}}{3\sqrt{.21}} = 12.1 \text{ MIN.}$

$T_4: L = 400'$   
 $S = 6116 - 6050 / 400 = 17\%$

SWALE 17% n = .040 B.W. = 5' d = 1' z.s = 1 s/s

$Q = 92.5 \quad V = 12.3 \quad F_r = 2.5$

$T_4 = \frac{400}{60(12.3)} = 0.5 \text{ MIN.}$

$L = 900'$   
 $S = 6650 - 5970 / 900 = 9\%$

B.W. = 5' s/s = 2.5:1 n = .040 d = 1.5

$Q = 147 \quad V = 11.2$

$T_4 = \frac{900}{60(11.2)} = 1.3$

$L = 1000'$   
 $S = 5970 - 5944 / 800 = 3.3\%$

B.W. = 5' S = 3.3 n = .035 d = 2 SS = 2.5:1

$Q = 181 \quad V = 9.0 \quad F_r = 1.4$

$T_4 = \frac{1000}{60(9.0)} = 1.9 \text{ MIN.}$

$T_c = 12.1 + 0.5 + 1.3 + 1.9 = 15.8 \text{ MIN.} = 0.26 \text{ HR.}$



Project DRAINAGE W. OF SH 115

Job No  
E-3729

Client GATES

By Rm

Date 3/31/89  
Rev. 10/26/89 #2/28/90

BASIN 021 - INCLUDED w/ 020

~~$T_i: L = 500$   
 $S = \frac{5990 - 5960}{500} = 6.0\%$   
 $C = 0.30$  (PASTURE C/D SOILS)  
 $T_i = \frac{1.87(1.1 - .30)\sqrt{500}}{\sqrt{6.0}} = 18.4 \text{ MIN.}$   
 $T_f$  NEGLIGIBLE  
 $T_c: T_c = T_i = 18.4 \text{ MIN.} = 0.31 \text{ HRS.}$~~

BASIN 050 (DEVELOPED BASINS 051 & 052 COMBINED)

$T_i: L = 500 \text{ FT.}$   
 $S = \frac{34}{500} = 6.8\%$   
 $C = 0.25$  (PASTURE A/B)  
 $T_i = \frac{1.87(1.1 - .25)\sqrt{500}}{\sqrt{6.8}} = 18.8 \text{ MIN.}$   
 $T_f: L = 2100$   
 $S = \frac{260'}{2100} = 12.4\%$   
 $RWS d = 0.5 \quad S = 2.5:1 \quad n = 0.040$   
 $Q = 22.4 \quad V = 7.2 \quad F = 2.0$   
 $T_f = \frac{2100}{1.2(60)} = 4.9$   
 $L = 4300$   
 $S = \frac{6390 - 5750}{4300} = 7.9 \quad d = 1.5 \quad B.W. = 5 \quad z = 2.5 \quad n = 0.040$   
 $Q = 137 \quad V = 10.5 \quad F = 1.8$   
 $T_f = \frac{2100}{60(7.9)} = 4.4$   
 $T_c: 18.8 + 4.9 + 4.4 = 28.1 \text{ MIN.} = 0.47 \text{ HR.}$

Project DRAINAGE W. OF SH 115 Job No E-3729

Client GATES By Rm Date 3/31/89  
REV: 10/26/83

BASIN 060 (INCL. BASINS 060-064)

$T_i: L=500'$   
 $S = 60'/500' = 12\%$   
 $C = .25$  (PASTURE A/B SOILS)  
 $T_i = \frac{1.87(1.1-.25)\sqrt{500}}{\sqrt[3]{12}} = 15.5 \text{ MIN.}$

$T_f: L=3600'$   
 $S = 6820-6400/3600 = 11.7\%$   
 $BW = 5' \quad d = 0.5' \quad z = 2.5 \quad n = 0.040$   
 $Q = 22 \quad V = 7.0 \quad F_r = 1.9 \quad T_f = \frac{3600}{60(7)} = 8.6 \text{ MIN.}$

$L = 6000'$   
 $S = 6400-5960/6000 = 7.3\%$   
 $BW = 5' \quad d = 1.5' \quad z = 2.5 \quad n = 0.035$   
 $Q = 151 \quad V = 11.5 \quad F_r = 2.0 \quad T_f = \frac{6000}{60(11.5)} = 8.7$

$T_c = 15.5 + 8.6 + 8.7 = 32.8 \text{ MIN.} = 0.55 \text{ HR.}$

BASIN 160 (INCLUDES BASINS 160-163)

$T_i: L=500'$   
 $C = .15$  (FOREST C/D)  
 $S = 33\% \pm$   
 $T_i = \frac{1.87(1.1-.15)\sqrt{500}}{\sqrt[3]{33}} = 12.4 \text{ MIN.}$

$T_f: L=3700'$   
 $S = \frac{7800-7000}{3700} = 35\%$   
 $B = 5' \quad D = 0.5' \quad z = 3 \quad n = 0.040$   
 $Q = 39 \quad V = 11.9 \quad F_r = 3.3 \quad T_f = \frac{3700}{60(11.9)} = 5.2 \text{ MIN.}$

Project DRAINAGE W. OF SH 115 Job No E-3729

Client GATES By Rm Date 3/31/89  
REV. 10/26/87 & 2/28/90

$$L = 5200$$

$$S = \frac{7000 - 6400}{5200} = 11.5\%$$

$$BW = 10' \quad D = 1' \quad Z = 3:1 \quad n = 0.040$$

$$Q = 141 \quad V = 10.8 \quad F = 2.1$$

$$T_T = \frac{5200}{60(10.8)} = 8.0 \text{ MIN.}$$

$$L = 5000'$$

$$S = \frac{6400 - 5980}{5000} = 8.4\%$$

$$BW = 15' \quad D = 2.5 \quad Z = 3.0:1 \quad n = 0.040$$

$$Q = 905 \quad V = 16.1 \quad F = 2.1$$

$$T_T = \frac{5000}{60(16.1)} = 5.2 \text{ MIN.}$$

$$T_c = 12.4 + 5.2 + 8.0 + 5.2 = 30.8 \text{ MIN.} = 0.51 \text{ HR.}$$

BASIN 164 (INCL. BASINS 164 & 165)

$$T_i: L = 500'$$

$$C = 0.15 \text{ (FOREST C/D) - SOME } \bar{C} \text{ ALSO - CONSERVATION}$$

$$S = \frac{40'}{500} = 8.0\%$$

$$T_i = \frac{1.87(1.1 - 0.15)\sqrt{500}}{\sqrt[3]{8}} = 19.9 \text{ MIN.}$$

$$T_T: L = 3700'$$

$$RW = 5 \quad S:S = 2.5:1 \quad n = 0.040 \quad S = \frac{9260 - 7320}{3700} = 5.3\% \quad d = 1.0$$

$$Q = 163 \quad V = 22.0 \quad F = 4.4$$

$$T_T = \frac{3700}{60(22)} = 2.8 \text{ MIN.}$$

$$L = 4400 \quad RW = 5 \quad S = 3:1 \quad n = 0.040 \quad S = \frac{7200 - 6400}{4400} = 18.2\% \quad d = 1.0$$

$$Q = 94 \quad V = 11.8 \quad F = 2.4$$

$$T_T = \frac{4400}{60(11.8)} = 6.2 \text{ MIN.}$$

Project DRAINAGE W. OF SH. 115	Job NR E-3729
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Client GATES	By Rm	Date 3/31/89 REV. 12/26/88
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### BASIN 164 (CONT.)

$$L = 6600'$$

$$S = \frac{6600 - 5960}{6600} = 9.7\%$$

$$D = 1.5 \quad BW = 10 \quad n = 0.040 \quad Z = 3$$

$$Q = 271 \quad V = 12.5 \quad F_r = 2.1$$

$$T_f = \frac{6600}{60(12.5)} = 8.8 \text{ min.}$$

$$T_c = 19.9 + 2.8 + 6.2 + 8.8 = 37.7 \text{ MIN.} \approx 0.63 \text{ HR.}$$

### BASIN 166 (INCL. BASINS 166 & 167)

$$T_i: L = 500'$$

$$S = \frac{40}{500} = 8\%$$

C = 0.25 (PASTURE A/B) - SOME C @ LOWER END - NO SIGNIFICANT EFFECT

$$T_i = \frac{1.87(1.1 - 0.25)\sqrt{500}}{\sqrt[3]{8}} = 17.8 \text{ MIN.}$$

$$T_f: L = 3500'$$

$$S = \frac{6600 - 5960}{3500} = 8.6\%$$

$$BW = 10 \quad D = 1 \quad n = 0.035 \quad S = 8.6 \quad Z = 3$$

$$Q = 139 \quad V = 10.7 \quad F_r = 2.1$$

$$T_f = \frac{3500}{60(10.7)} = 5.5 \text{ MIN.}$$

$$T_c = 17.8 + 5.5 = 23.3 \text{ MIN.} \approx 0.39 \text{ HR.}$$

Project DRAINAGE W. OF SH 115	Job No E-3729
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Client GATES	By RM	Date 3/31/89
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BASIN 168

$$T_1: L = 400'$$

$$S = \frac{6024 - 5970}{400} = 8.5\%$$

$$C = .30 \quad (\text{CID - PASTURE})$$

$$T_1 = \frac{1.87(1.1 - .30)\sqrt{400}}{\sqrt[3]{8.5}} = 14.7 \text{ MIN.}$$

$$T_2: L = 950'$$

$$S = \frac{5970 - 5960}{950} = 3.2\%$$

$$B = 5; \quad D = 1.0 \quad n = .040 \quad S = 3.11$$

$$Q = 42 \quad V = 5.3 \quad F = 1.1$$

$$T_2 = \frac{950}{60(5.3)} = 3.0$$

$$T_c = 14.7 + 3.0 = 17.7 \text{ MIN.} = 0.30 \text{ HR.}$$

Project DRAINAGE W. OF SH 115	Job No E-3729
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Client GATES	By RM	Date 3/31/89 REV. 2/23/90
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## DEVELOPED CONDITIONS

REVISED TIME OF CONCENTRATION  
FOR DEVELOPED CONDITIONS (ALL BASINS  
REVISED PER CITY COMMENTS)

### BASIN 060

$$T_f: C = 0.35 \quad \text{---} \quad \text{(REFS - } \frac{1}{2} \text{ AC. - B. SOL.)}$$

$$L = 300$$

$$S = \frac{18}{300} = 6\%$$

$$T_f = \frac{1.87(1.1 - 0.35)\sqrt{300}}{3\sqrt{6}} = 13.4 \text{ MIN.}$$

$$T_f: L = 1200' \text{ (SWALE/CHANNEL)}$$

$$EW = 10$$

$$S = \frac{100}{1200} = 8.3\%$$

$$n = 0.15 \text{ (CONC.)}$$

$$Z = 4, D = 1$$

$$Q = 330 \quad V = 24 \text{ USE } 20 \text{ FPS MAX.}$$

$$T_f = \frac{1200}{60(20)} = 1.0 \text{ MIN.}$$

$$L = 3500' \text{ (STORM SEWER)}$$

$$S = \frac{120}{1900} = 6.3\%$$

$$\text{ASSUME } 300 \text{ CFS } \pm \text{ DREN'D. } @ \text{ 0.13} = 44.8''$$

$$\Rightarrow V = 27 \text{ FPS}$$

$$T_f = \frac{1900}{27(60)} = 1.2 \text{ MIN.}$$

$$T_c = 13.4 + 1.0 + 1.2 = 15.6 \text{ MIN.} = 0.26 \text{ HR.}$$

Project DRAINAGE W. OF SH 115 Job No E-3729

Client GATES By Rn1 Date 3/31/89

BASIN 061

$T_i: L = 300'$   
 $S = 10.7\%$   
 $C = 0.35$  (RES 1/2 - B SORS)

$T_i = \frac{1.87(1.1 - 0.35)\sqrt{300}}{\sqrt[3]{10}} = 11.3 \text{ MIN.}$

$L = 2200$

$S = 6780 - 6600 / 2200 = 8.2$

ASSUME STORM SEWER @ 8.2% Q ≈ 100% (THEY STATE RAIN)

DRAIN @ 28" V = 23.0 FPS

$T_f = \frac{2200}{60(23)} = 1.6 \text{ MIN.}$

$L = 3500'$

(ASSUME IMPROVED NAT. CHANNEL)

$S = 6580 - 6240 / 3500 = 9.7\%$

RW = 25 S = 9.7 z = 4 D = 0.8' n = 0.40

Q = 209 V = 9.2 F = 2

$T_f = \frac{3500}{60(9.2)} = 6.3 \text{ MIN.}$

$T_c = 11.3 + 1.6 + 6.3 = 19.2 \text{ MIN.} = 0.32 \text{ HR.}$

BASIN 160

$T_i: T_i = 12.4 \text{ MIN. (SAME AS HIST.)}$

$T_f: T_f \#1 = 5.2 \text{ MIN. (SAME AS HIST.)}$

$T_f \#2$  IMPROVED CHAN.

BW = 20 z = 4:1 D = .8 n = 0.40 S = 11.5%

Q = 185 V = 9.9 L = 5200

$T_f = \frac{5200}{60(9.9)} = 8.8 \text{ MIN.}$

Project DRAINAGE W. OF SH 115	Job No E-3729
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Client GATES	By Rm	Date 3/31/89
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$$T_+ \#3: L=5000'$$

$$S=8.4\%$$

ASSUME IMPROVED CHAN.

$$B.W.=30' \quad D=1.0 \quad Z=4 \quad n=.040$$

$$Q=338 \quad V=10.0$$

$$T_+ = \frac{5000}{60(10.0)} = 8.3 \text{ min.}$$

$$T_c: T_c = 12.4 + 5.2 + 8.8 + 8.3 = 34.7 \text{ MIN.} = 0.58 \text{ HR.}$$

### BASIN 164

$$T_i: T_i = 19.9 \text{ MIN (NO CHANGE FROM HISTORIC)}$$

$$T_+ : T_{+1} = 2.8 \text{ MIN. (SAME AS HIST.)}$$

$$T_{+2}: L=2100 \text{ (NAT. CHANNEL)}$$

$$S = \frac{7160 - 6800}{2100} = 17.1$$

$$B.W.=5 \quad D=1' \quad S=3:1 \quad n=.040$$

$$Q=97 \quad V=12.2$$

$$T_{+2} = \frac{2100}{12.2(60)} = 2.9 \text{ MIN.}$$

$$T_{+3}: \text{IMPROVED CHANNEL}$$

$$L=2300' \quad B.W.=20 \quad Z=4 \quad n=.040 \quad D=1$$

$$S = \frac{6800 - 6600}{2300} = 8.7\% \quad Q=236 \quad V=9.8 \quad T_+ = \frac{2300}{60(9.8)} = 3.9$$

$$L=6600 \quad B.W.=30' \quad D=1.0 \quad Z=4 \quad n=.040 \quad S=9.7\%$$

$$Q=364 \quad V=10.7$$

$$T_{+4} = \frac{6600}{60(10.7)} = 10.3 \text{ MIN.}$$

$$T_c = 19.9 + 2.8 + 2.9 + 3.9 + 10.3 = 39.8 \text{ MIN.} = 0.66 \text{ HR.}$$



Project <b>DRAINAGE W. OF SH 115</b>	Job No <b>E-3729</b>
Client <b>GATES</b>	By <b>R.M.</b>
Date <b>3/31/89</b>	

BASIN 020

$T_i: L = 200'$   
 $C = 0.70$  (LT. IND. - D SOILS)  
 $S = 6088 - 6055 / 200 = 16.5\%$   
 $T_i = \frac{1.87(1.1 - 0.70)\sqrt[3]{200}}{\sqrt[3]{16.5}} = 4.2 \text{ MIN.}$

$T_f: L = 1100'$  (STORM SEWER / CHAN.)  
 $Q \approx 150$   
 $S = 6090 - 5950 / 1100 = 9\%$   
 $@ n = 0.013 \text{ \& } Q = 150 \text{ DRAIN} = 32" \quad V = 26 \text{ FPS.}$   
 $T_f = \frac{1100}{60(26)} = 0.7 \text{ MIN.}$

$T_c = 4.2 + 0.7 = 4.9 \text{ MIN.} = .08 \text{ HR. USE } .10 \text{ MIN.}$

BASIN 021

USE  $T_c = 0.10$  (MINIMUM) (SMALL BASIN)

BASIN 022

USE  $T_c = 0.10 \text{ HR.}$  (MINIMUM) (SMALL BASIN)

BASIN 051

USE  $T_c = 0.10 \text{ HR.}$

BASIN 052

$T_i: L = 200'$   
 $C = 0.70$  (LT. IND. C/D SOILS)  
 $S = 10' / 200 = 5\%$   
 $T_i = \frac{1.87(1.1 - 0.70)\sqrt[3]{200}}{\sqrt[3]{5}} = 6.2 \text{ MIN.}$

$T_f: L = 1500'$  (STORM SEWER)  
 $S = 5\% \pm$   
 $Q \approx 150 \quad @ n = .013 \text{ DRAIN} = 36 \quad V = 21$   
 $T_f = \frac{1500}{60(21)} = 1.2$   
 $T_c = 6.2 + 1.2 = 7.4 \text{ MIN.} = 0.14 \text{ HR.}$

Project DRAINAGE W. OF SH 115

 Job No  
E-3729

 Client  
GATES

 By  
RM

 Date  
3/31/89  
REV. 2/25/90

### RASIN 062

$$T_i: L = 200'$$

$$C = 0.45 \quad (\text{S.F. } 1.5/\text{ac.}) \quad (\text{'C' SOILS})$$

$$S = \frac{25}{200} = 12.5\%$$

$$T_i = \frac{1.87(1.1 - 0.45)\sqrt{200}}{\sqrt[3]{12.5}} = 7.3 \text{ MIN.}$$

$$T_f: L = 2400' \quad (\text{SWALE / CHANNEL})$$

$$S = \frac{6230 - 6040}{2400} = 7.9\%$$

$$BW = 15 \quad d = 0.8 \quad Z = 4 \quad n = 0.035$$

$$Q = 134 \quad V = 9.2 \quad \text{USE DROPS TO RED. V TO 7 FPS}$$

$$T_f = \frac{2400}{60(7)} = 5.7 \text{ MIN.}$$

$$T_c = 7.3 + 5.7 = 13.0 \text{ MIN.} = 0.22 \text{ HR.}$$

### RASIN 063

$$T_i: L = 300'$$

$$C = 0.40 \quad (\text{'D' SOILS - RES.})$$

$$S = 10\%$$

$$T_i = \frac{1.87(1.1 - 0.40)\sqrt{300}}{\sqrt[3]{10}} = 10.5 \text{ MIN.}$$

$$T_f: L = 2700' \quad (\text{IMPROVED / STAB. CHAN.})$$

$$S = \frac{6230 - 6000}{2700} = 8.5\%$$

$$BW = 20' \quad S = 8.5\% \quad Z = 4 \quad n = 0.040 \quad d = 1.0$$

$$Q = 340 \quad V = 10.0$$

$$T_f = \frac{2700}{60(10)} = 4.5 \text{ MIN.}$$

$$T_c = 10.5 + 4.5 = 15.0^{\text{MIN}} = 0.25 \text{ HR.}$$

Project DRAINAGE W. OF SH 115 Job No E-3729

Client GATES By Rm Date 3/31/89  
REV. 2/28/90

### BASIN 064

$T_i: L = 200'$   
 $S = 10'/200 = 5\%$   
 $C = 0.70$  (D'SOUS - INDUST.)  
 $T_i = \frac{1.87(1.1-0.70)\sqrt{200}}{\sqrt[3]{5}} = 6.2 \text{ min.}$

$T_f L = 2400'$   
 $S = 6030 - 5950 / 2400 = 3.3\%$

IMPROVED CHANNEL

$BW = 30 \quad D = 1.5 \quad Z = 4 \quad n = 0.40$

$Q = 428 \quad V = 7.9$

$T_f = \frac{2400}{60(7.9)} = 5.1 \text{ min.}$

$T_c = 6.2 + 5.1 = 11.3 \text{ min.} = 0.19 \text{ HR.}$

### BASIN 162

$T_i: L = 200'$   
 $C = 0.40$  (C" SOIL - RES. 1 UNIT/AC.)  
 $S = 32'/200 = 16\%$   
 $T_i = \frac{1.87(1.1-0.40)\sqrt{200}}{\sqrt[3]{16}} = 7.4 \text{ min.}$

$T_f L = 1700'$   
 $BW = 30 \quad D = 1.5 \quad Z = 4 \quad n = 0.40 \quad S = 120'/1700 = 7.1\%$   
 $Q = 628 \quad V = 11.6 \quad F_r = 1.8$   
 $T_f = \frac{1700}{60(11.6)} = 2.4$

$T_c = 7.4 + 2.4 = 9.8 \text{ min.} = 0.16$

### BASIN 163

SMALL AREA - USE  $T_c = 0.10$

Project <i>DRAINAGE</i>		Job No E-3729
Client <i>GATES</i>	By Rm	Date 3/31/89

BASIN 165

$T_i: L = 200'$   
 $S = 7\%$   
 $C = 0.40$  (RES. - D.)  
 $T_i = \frac{1.87(1.1 - 0.40)\sqrt{200}}{\sqrt[3]{7}} = 9.7 \text{ MIN.}$

$T_f: L = 3200$   
 $S = \frac{6190 - 5960}{3200} = 7.2\%$   
 B.W. = 30' D = 1.5 Z = 4 n = 0.040  
 $Q = 632 \quad V = 11.7$   
 $T_f = \frac{3200}{60(11.7)} = 4.6 \text{ MIN.}$

$T_c = 9.7 + 4.6 = 14.3 \text{ MIN.} = 0.24 \text{ HR.}$

BASIN 167

$T_i: L = 200'$   
 $S = 10\%$   
 $C = 0.70$  (LT. IND. - C/D SOILS)  
 $T_i = \frac{1.87(1.1 - 0.70)\sqrt{200}}{\sqrt[3]{10}} = 4.9 \text{ MIN.}$

$T_f: L = 1500'$  (ASSUME C&G)  
 $S = 60/1500 = 4\%$   
 $Q \approx 25 \quad n = 0.18 \quad d = 6" \Rightarrow Q \approx 40 \quad V = 6.6$   
 $T_f = \frac{1500}{60(6.6)} = 3.8 \text{ MIN.}$

$L = 2900'$  (ST. S.)  
 $S = \frac{300}{2900} = 10\%$   
 $Q \approx 75 \quad n = 0.13 \quad DREQ. = 24 \quad V = 23$   
 $T_f = \frac{2900}{60(23)} = 2.1$   
 $T_c = 4.9 + 3.8 + 2.1 = 10.8 \text{ MIN.} = 0.18 \text{ HR.}$

Project CHEYENNE MOUNTAIN RANCH TR-20 Job No. E-3729

Client GATES By RM Date 9 JUNE 88

REACH ROUTING COEFFICIENTS FOR SCS TR-20  
CHANNEL ROUTING

$Q = X A^m$  DEVELOP DEPTH-DISCHARGE-AREA  
CURVE BASED ON REPRESENTATIVE  
CROSS SECTION

REACH 060 - 062  
L = 2400 FT.

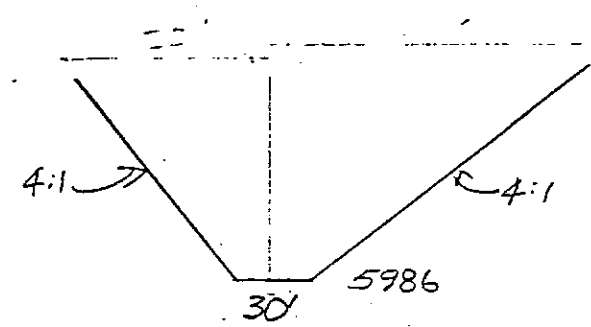


B.W. = 15'  
AVG. SLOPE 4/1  
n = .035  
S = 7.9%

ELEV.	DEPTH	Q (CFS)	V (FPS)	A (FT. <sup>2</sup> )
6140	0	0	0	0
6141	1	198	10.4	19.0
6142	2	707	15.4	45.9
6143	3	1554	19.2	81.
6144	4	2786	22.5	124.
6140.5	2.5	59.	7.0	8.

Project <u>CHEYENNE Mtn. RANCH</u> <u>TR-20</u>	Job No <u>E-3729</u>
Client <u>GATES</u>	By <u>RM</u> Date <u>9 JUNE 88</u>

REACH 062-064  
 L=2400'  
 S=3.3%



n=0.40  
 AVG. S/S = 4

<u>ELEV.</u>	<u>D.</u>	<u>Q</u>	<u>V</u>	<u>A</u>
5986.	0	0	0	0
5988	2	712	9.4	76.
5990	4	2537	13.8	184.
5992	6	5579	17.2	324.
5986.5	0.5	65.	4.1	16.

Project CHEYENNE Mtn. RANCH  
TR-20

Job No. E-3729

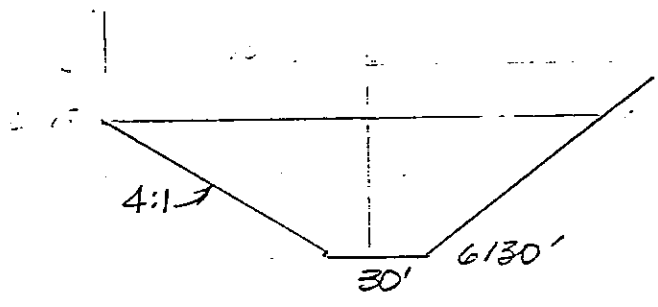
Client GATES

By RM

Date 9 June 88

REACH 061-063

L = 2700'  
n = .040  
s = 8.5%



AVG. S/S = ~~6:1~~ 4:1

ELEV.	D	Q	V	A
6130	0	0	0	0
6132	2	1142	15.0	76.
6134	4	4072	22.1	184.
6130.5	0.5	105.	6.5	16i.
6131	1.0	340	10.0	34.

REACH 063-064

L = 2400'

SEE REACH 062-064 FOR HYDRAULIC CHAR.

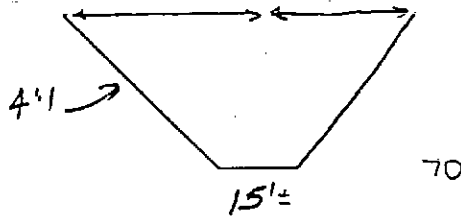
Project CHEYENNE Mtn. RANCH Job No E-3729  
TR-20

Client GATES By Rm Date 9 JUNE 88

REACH 021-022

L = 1700

n = 0.40



AVG. SIDE SLOPE ~~3.75:1~~ 4:1

S = 20/260 = 7.7%

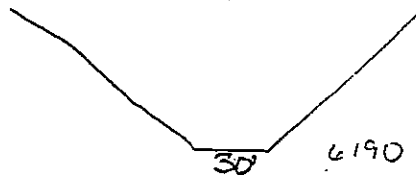
ELEV.	D	Q	V	A
59.70	0	0	0	0
72	2	610	13.3	46.
<del>74</del>	<del>4</del>	...	...	...
<del>75</del>	<del>5</del>	...	...	...
70.5	.5	51.	6.0	9.

REACH 160-161

L = 1100

n = 0.40

S = 20/160 = 12.5%



AVG. SLOPE 4:1

ELEV.	D	Q	V	A
6190	0	0	0	0
6192	2	1385	18.2	76.
6194	4	4938	26.8	184.
6190.5	0.5	127.	7.9	16.



Project CHEYENNE Mtn. Ranch Job No E-3729  
TR-20

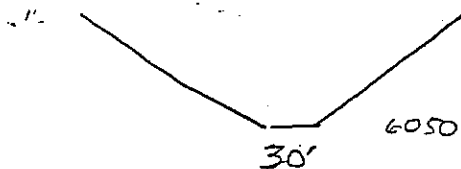
Client GATES By FM Date 9 JUNE 83

REACH 161-162

L = 1700'

n = 0.040

S = 7.1%



AVG. SIDE SLOPE 4.0:1

<u>ELEV.</u>	<u>D</u>	<u>Q</u>	<u>V</u>	<u>A</u>
6050	0	0	0	0
6052	2	1044	13.7	76.
6053	3	2174	17.3	126.
6054	4	3722	20.2	184.
6051	1	311	9.2	34.

REACH 162-163

L = 900'

n = .040

S = 30/900 = 3.3%



AVG. SIDE SLOPE 4:1

<u>ELEV.</u>	<u>D</u>	<u>Q</u>	<u>V</u>	<u>A</u>
5980	0	0	0	0
82	2	712	9.4	76.
84	4	2537	13.8	184.
<del>85</del>	<del>5</del>			
<del>86</del>	<del>6</del>			

81 1 212. 6.2 34.

Project CHEYENNE MTN. RANCH TR-20		Job No E-3729	
Client GATES	By RAJ	Date 9 June 88	

REACH 164-165

L = 3200  
 n = .040  
 S = 1.2%



AUG. SIDESLOPE 4:1

<u>ELEV.</u>	<u>D</u>	<u>Q</u>	<u>V</u>	<u>A</u>
6010	0	0	0	0
6012	2	1051	13.8	76.
6014	4	3148	20.4	184.
<del>6015</del>	<del>5</del>			
<del>6016</del>	<del>6</del>			
6011	1	313	9.2	34.

Project CHEYENNE Mtn. Ranch TR-20 Job No E-3729

Client SATES By Rm Date 6/14/89 REV. 5/30/89 & 2/28/90

DES. FT.  $\Delta$  +  $\Delta$  COMBINED  
STRUCTURE 1 (ALT 1 - 24 HR. STORM) (STR. 020 IN TR-20)

ELEV. - STORAGE		INC. TST.		
ELEV.	AREA (IN. <sup>2</sup> )	AREA (AC)	VOL. (AF)	VOL. (AF)
43	0+0	0	0	0
44	0.17+0.37	0.11	0.06	0.06
46	0.85+1.10	0.44	0.55	0.61
45	1.92+2.50	1.01	1.45	2.06
50	4.55+4.65	2.11	3.12	5.18
52	7.75+9.35	3.70	5.81	10.99
54	23.6	5.42	9.12	20.11
56	29.2	6.70	12.12	32.23

HIST. DISCHARGE  
~~HISTORIC  
 $Q_{10}$  HIST = 115 CFS (24 HR) } BASIN C60  
 $Q_{100}$  HIST = 320 CFS (24 HR.)  
 $Q_{10}$  HIST = 60 CFS (24 HR.) } BASIN O20  
 $Q_{100}$  HIST = 135 CFS (24 HR.)~~

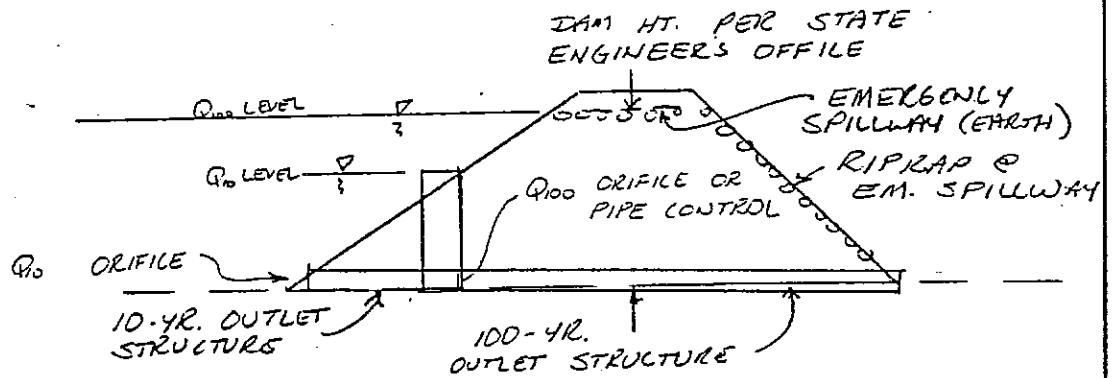
SEE SHT. D6 FOR REVISED HIST. Q & RELEASE RATE

ALLOWABLE RELEASE RATE  
~~$Q_{10} = 115 + 60 = 175$  CFS  
 $Q_{100} = 320 + 135 = 455$  CFS~~

NOTE: THE ABOVE ALLOWABLE RELEASE RATES ARE BASED ON HISTORIC Q<sub>A</sub> AT TWO CULVERTS @ SH 115 AND RELEASE TO TWO DIFFERENT POINTS TO CORRESPOND TO HISTORIC DRAINAGE PATTERNS. IF IT IS DETERMINED THAT ONE RELEASE POINT CAN BE USED, ONLY ONE OUTLET STRUCTURE WILL BE NECESSARY. THIS SHOULD BE EVALUATED FURTHER IN FUTURE DESIGN.

Project	CHEYENNE MTN. RANCH TR-20	Job No	E-3729
Client	GATES	By	Rm
		Date	6/14/83 REV. 5/20/89 & 2/22/90

### TYPICAL OUTLET STRUCTURE - POND 1 & 2



ASSUME 6' HEAD TO CONTROL Q10  
FIND ORIFILE SIZE

$$Q = CA\sqrt{2gH}$$

$$C = 0.6 \text{ (WEIR COEFFICIENT)}$$

A: ORIFILE AREA (SF)

Q: RELEASE RATE (CFS)

Q10 HIST. 60 CFS (EASIN 560)

$$60 = 0.6 A \sqrt{64.4(5.0)}$$

$$A = 5.57 \text{ SF} \quad D = 32" \quad \frac{1}{2} D = 1.25 \rightarrow H = 6 - 1.25 = 4.75$$

$$H = 4.75 \approx 5.0 \checkmark$$

Q10 (HIST.) = 115 CFS (EASIN 560)

ASSUME H = 4'

$$115 = 0.6 A \sqrt{64.4(4)}$$

$$A = 11.94 \text{ SF} \quad D = 46.8" \quad \frac{1}{2} D = 1.95 \quad H = 6 - 1.95 = 4.05$$

Project CHEYENNE Mtn. RANCH		Job No E-3729
TR-20		
Client GATES	By R.M.	Date 6/14/88 REV. 5/30/89

PRELIM. - SEE SHT. 6 FOR REVISED ELEV. @  
ELEV. - DISCHARGE

ELEV.	$A_1 = 5.57$ $H_1 (32' / 20' \approx)$ $A_0$	$Q_1$	$A_2 = 10.38$ $H_2 (44' / 20' \approx)$	$Q_2$	FRICTION H.P.	$Q_{TOT.}$	VOL.	
43	0	0	0	0		0	0	
44	0.5	1.95	6.6	0.5	7.8	2.30	14.4	0.06
46	1.67	A.F. 34.7	1.5	54.6	9.26	89.3	0.61	
48	3.67	51.4	3.17	89.0	FF	140.4	2.06	
49	4.67	53.0	4.17	102.1	↓	160.0	3.62	
50		60		15-			5.18	
52		↓					10.99	
54							20.11	
56							32.23	

FROM PRELIM. RUN. ELEV. MAX. @  $Q_{10} = 24' 52.5 \pm$  FOR  $Q_{10} = 24'$   
 ASSUME 2.5' D. ORIFICE @ 020      ASSUME 3' D CRIF @ 060  
 $H = 52.5 - (43 + 1.25) = 8.25$        $H = 52.5 - (43 + 1.5) = 8.0$

$60 = 0.6 A \sqrt{64.4 (8.25)}$        $115 = 0.6 A \sqrt{64.4 (8.0)}$   
 $A = 4.37 \text{ SF}$  ,  $D = 2.35'$        $A = 8.44 \text{ SF}$   $D = 3.28'$

$D = 23.2''$  DIA

$D = 39.4''$   
(39.7'')

ELEV.	$H_1$	$A_P$	$Q_1$	$H_2$	$A_1$	$Q_2$	$Q_T$	VOL.
43	0	0	0	0	0	0	0	0
44	0.5	1.78	6.1	0.5	2.11	7.2	13.3	0.06
46	1.83	4.34	28.3	1.5	7.31	43.1	71.4	0.61
48	3.83	↓	40.9	3.47	7.34	65.8	106.7	2.06
50	5.83	↓	50.5	5.47	↓	82.7	133.2	5.18
51.0	6.83	↓	54.6	6.47	↓	89.9	144.5	8.09
52.5	8.33	↓	60.3	7.97	↓	99.8	160.1	13.27

$Q_{100}$  CRIFICE - BASIN 060

$Q_{100-24} (CHST) = 320 (060) + 135 (020) = 455$

060 -  $Q_{100} = 320$  CFS      ASSUME 4.5' CRIFICE

$H \approx 56 - (42 + 2.25) = 11.75'$

$320 = 0.6 A \sqrt{64.4 (11.75)}$        $A = 19.39 \text{ S.F.}$   $D = 59.6''$  (4.97')

Project CHEYENNE Mtn. Ranch TR-20 Job No E-3729

Client GATES By RM Date 6/14/88 REV. 5/20/89

@ 060  
ASSUME 8'x8' RISER - WEIR LENGTH 32'  
WEIR CREST EL. 52.5  
 $Q = 3.1 L H^{3/2}$

ASSUME ORIFICE @ 42.0  
MAX. WSEL @ 56.0  
 $Q_R = 320$  CFS

ASSUME 48" ORIF.  
 $H = 56 - (42 + 2.0) = 12.0'$

$320 = 0.6 A \sqrt{64.4 (12.0)}$  A = 19.19 S.F. D = 4.94' x

ASSUME 54" ORIF.  
 $H = 56 - (42 + 2.25) = 11.75'$

$320 = 0.6 (A) \sqrt{64.4 (11.75)}$  A = 19.39 S.F. D = 4.97' ✓

@ 53  
 $Q_U = 3.1 (32) (0.5)^{3/2} = 35.1$  CFS  
 $Q_0 = 0.6 (7.34) \sqrt{64.4 (8.47)}$  = 102.9  
 $Q_T = 35.1 + 102.9 = 138.0$

@ 54  
 $Q_U = 3.1 (32) (1.5)^{3/2} = 182.2$  CFS  
 $Q_0 = 0.6 (7.34) \sqrt{64.4 (9.47)}$  = 108.8 CFS @ 10 YR CRIFICE  
 $Q_T = 182.2 + 108.8 = 291.0$  (>  $Q_{100}$  HIST. = 283 - ORIFICE CONTINUED)  
 $H = 54 - (42 + \frac{4.67}{2}) = 9.67'$   
A = 17.15 S.F.

$Q_0 = 0.6 (17.15) \sqrt{64.4 (9.67)}$  = 256.8 CFS

@ 56  
H = 11.67 FT.  
A = 17.15 S.F.  
 $Q_0 = 0.6 (17.15) \sqrt{64.4 (11.67)}$  = 282.1 CFS

Project CHEYENNE Mtn. RANCH TR-20		Job NR E-3729	
Client GATES	By RM	Date 6/14/38 REV. 5/30/89	

Gros ORIFICE - RASIN OZO

Q<sub>100-24</sub> HIST. = 135 CFS  
 ASSUME 3.5' ORIFICE ✓  
 H<sub>2</sub> 56 - (42 + 1.75) = 12.25'

$$Q = CA\sqrt{2gH}$$

$$135 = 0.6 A\sqrt{64.4(12.25)}$$

$$A = 8.01 \text{ SF} \quad D = 38.3" (3.19')$$

ASSUME 6'x6' RISER (L. 24' WEIR @ CREST EL 52.5)

@ 53.0

$$Q_w = CLH^{3/2} = 3.1(24)(0.5)^{3/2} = 26.3 \text{ CFS}$$

$$Q_o = CA\sqrt{2gH} = 0.6(4.34)\sqrt{64.4(8.83)} = 62.1$$

$$Q_T = 26.3 + 62.1 = 88.4 \text{ CFS}$$

@ 54.0

$$Q_w = 3.1(24)(1.5)^{3/2} = 137.7 \text{ CFS}$$

$$Q_o = 0.6(4.34)\sqrt{64.4(9.83)} = 65.5 \text{ CFS}$$

$$Q_T = 137.7 + 65.5 = 203.2 \quad (> Q_{\text{ALLOWABLE}} - \text{Gros ORIFICE CONTROL})$$

$$Q_o = 0.6(2.01)\sqrt{64.4(10.25)} = 123.5 \text{ CFS}$$

@ 56.0

$$Q_o = 135 \text{ CFS (FROM ORIG. DESIGN ABOVE)}$$

Project CHEYENNE MOUNTAIN RANCH DRAINAGE WEST OF HIGHWAY 115		Job No E-3729
Client GATES	By RM	Date 29 JULY 89 REV. 5/30/89
		REV. 10/26/89 " 2/23/90

## DETENTION POND No. 1 (REVISED)

MODIFY DETENTION POND NO. 1 TO PROVIDE DETENTION STORAGE FOR BASINS O51, O52, O21 & O22 IN ADDITION TO OTHER BASINS (TOT. IS NOW FOR DESIGN PTS. 1-4)

BASIN	HISTORIC FLOW		
	IA	Q <sub>10</sub>	Q <sub>100</sub>
O60	.545	60	290
O20	.078	180	770
		140	460

REVISE OUTLET CAPACITY TO EQUAL NEW HISTORIC DISCHARGES

STRUCTURE 20 REVISED (DATA FILE E-3729.F2D)  
REV. 10/26/89

ELEV.	Q <sub>TOT.</sub>	Q <sub>OUT</sub>		
43	0	0	PREDATE REVISED $Q_{TOT-NEW} = \frac{140}{220} \times Q_{TOT}$	
44	27	17.		
46	98	62.		
48	147	94.		
50	183	116.		
51.8	199	127.		
2ND STAGE → 52.5	220	140		
53	313	240		$Q_{NEW} = \frac{220}{460} \times Q_{TOT}$ 460/600
54	525	403		
56	580	445		
57	600	460		

FROM TR-20 RESULTS (DEVELOPED Q STRUCTURE 20)  
 $Q_{10}$  OUTFLOW = ~~210~~ 140 CFS. ✓ (≅ 265 CFS HIST.)  
 $Q_{100}$  OUTFLOW = ~~560~~ 460 CFS ✓ (≅ 670 CFS HIST.)



Project CHEYENNE MOUNTAIN RANCH DRAINAGE W. OF SH 115	Job No CE-3729
Client GATES	By RM      Date 2/3/91

DETENTION POND NO. 2 (STRUCTURE 80 IN TR-20)

<u>ELEVATION - STORAGE</u>			
<u>ELEV.</u>	<u>AREA (AC.)</u>	<u>INC. VOL. (AC-FT.)</u>	<u>TOT. VOL. (AC-FT.)</u>
5960	0.52	0	0
65	1.26	4.45	4.45
67.5	1.43	3.36	7.81
70	1.84	4.09	11.90
72.5	2.34	5.23	17.13
75	3.06	6.75	23.88
77.5	3.70	8.45	32.33
80	4.12	9.78	42.11
82.5	4.68	11.00	53.11

OUTLET DESIGN

ASSUME  $Q \approx 400$  CFS @ ELEV. 75 ( $Q_o$ )  
 INV. @ 5960  $H = 14'$  (4' HIGH ORIFICE)  
 $\Rightarrow$  ORIFICE SIZE = 5' HIGH x 4.6' WIDE  
 $Q_o = 0.61 (23.2) \sqrt{64.4 (H)}$

<u>ELEV.</u>	<u>H</u>	<u><math>Q_o</math></u>
60	0	0
65	2.5	180
67.5	5	254
70	7.5	311
72.5	10	359
75	12.5	402.
77.5	15.0	440

Project CHEYENNE MTN. RANCH  
 DRAINAGE  $\omega$  / OF SH 115

Job No  
 CE-3729

Client GATES

By RM

Date 2/8/91

<u>ELEV.</u>	<u>H</u>	<u>Q</u>
80	16	1280
82.5	18.5	1380

(NOTE: 8'H x 8.17' W ORIFICE  
 FOR  $Q_{100} - Q = 0.61(65.40) \sqrt{64.4(H)}$

Project CHEYENNE Mtn. RANCH DRAINAGE W. OF SH 115		Job No E-3729	
Client GATES	By R.M.	Date 3 AUG. 88 REV. 5/30/89 & 2/28/90	

QUANTITY / COST ESTIMATE - DETENTION POND 1

EXC. - 54,000 C.Y. } TO ELEV. 60 - CONSERV.  
 FILL - 39,600 C.Y. } USE 40,000 AS FILL QUAN.

SEED / MULCH / FERTILIZE

250' x 1800' ÷ 43,560 = 10.3 AC. → 11 AC.

LOW FLOW CHANNEL 1' DEEP 2% SLOPE 10' R.W. 4:1 S'S PROX.  
 Q=62 NS% Q<sub>100</sub> INFLOW 1.5" THICK ROCK 10.5" BEDDING  
 ⇒ 1.35 C.Y. / LF. x 35 / LF. x 150' = 70 C.Y.

OUTFALL STRUCTURE DESIGN (EARTHEN EMERG. SPILLWAY TO BE PROVIDED BY FINAL DESIGN)

NORTH - BARREL LENGTH - 160 FT. IN 43 OUT 42  
 RISER HT. - 7.5 FT.

SOUTH - BARREL LENGTH - 180 FT. IN 43 OUT 41  
 RISER HT. - 7.5'

NORTH OUTLET - Q<sub>100</sub> = 420 CFS  
 ASSUME 2/3 TW @ 43 (APPROX. TOP OF 100%)  
 ΔH = 55.0 - 48 = 7'

CHECK SIZE → PRESSURE FLOW  
 Q = 420 H = 7'  
 n = .015  
 K<sub>1</sub> = .K<sub>2</sub> = 1.0  
 L = 160'

d = 72 → Q = 340  
 d = 78 → Q = 403 V = 12.2  
 d = 84" → Q = 472 CFS USE 78" → IMP. 15.67

RISER : Q<sub>100</sub> = 420 Q<sub>10</sub> = 150 Q<sub>20</sub> = 270 CFS  
 H = 3.1  
 Q = 3.1 L H<sup>3/2</sup> 270 = 3.1 L (3.1)<sup>3/2</sup>  
 L = 16'  
 USE 7' x 7' 1/2" (CONCRETE)

# DREXEL, BARRELL & CO. EARTHWORK CALCULATIONS

JOB NO. E-3729  
 DATE 8/3/88  
 CALC. BY: Rm  
 CHECKED BY: \_\_\_\_\_

PAGE: 1/1

PROJECT: CHEYENNE MTR. RANCH DET POND 1

CLIENT: GATES

STATION	CUT	FILL	AVE. CUT	AVE. FILL	DISTANCE	VOL. CUT	VOL. FILL	REMARKS
10+00	0	0						
10+50	0	60	0	30	50	0	56	
12+30	144	200	72	130	180	480	267	
14+30	1016	104	530	152	200	4296	1126	
15+70	1634	16	1325	60	140	6870	311	
16+40	2128	14	1581	15	70	4877	39	
17+00	1816	16	1772	15	60	4382	33	
17+70	845	605	1330.5	310.5	70	3449	805	
18+40	1578	32	1311.5	318.5	70	3141	826	
19+30	4592	0	3285	16	90	10,283	53	
20+00	2208	320	3400	160	70	8815	415	
20+65	989	1008	1578.5	664	65	3848	1599	
21+65	115	1288	552	1148	100	2044	4252	
23+35	122	1370	118.5	1329	170	746	8368	
26+45	0	954	51	1162	310	700	13,341	
29+50	0	128	0	541	305	0	6111	
30+85	0	0	0	64	135	0	320	
					20851	55931	28,522	

Project CHEYENNE MTN. RANCH  
DRAINAGE W. OF SH 115

Job No  
E-3729

Client GATES

By RM Date 3 Aug. 88

RISER CONCRETE - 4 WALLS \* 8' x 7.5' x 1' THICK = 240 CF  
 BASE 9 x 9 x 1 = 81  
 TOT. 321 CF / 27  
 = 11.9 C.Y.  
 USE 12

RIPRAP & BEDDING

ASSUME 20' WIDE x 30' LONG x 4' THICK = 27  
 = 89 C.Y.

SOUTH OUTLET

$Q_{100} = 160$  CFS  
 $n = .015$   
 $L = 180'$   
 $K_e = K_o = 1.0$   
 $\Delta H = 55.0 - 48 = 7'$   
 $48" \rightarrow Q = 139$   
 $54" \rightarrow Q = 180 \checkmark$

RIPRAP 20' x 30' x 3.5' / 27 = 78 (TOT 167)

~~CULVERT @ DES. PT. (6)~~

~~$Q_{100} = 460$  CFS  
 $H/W/D = 1.5$  6' HIGH BOX  $\rightarrow 60$  CFS/FT.  
 $460/60 = 7.67'$  USE 8' WIDE x 6' HIGH BOX  
 VOL (10" WALLS) =  $\frac{10}{12} \times 12' \div 27 = 0.37$   
 10" FLOOR TOP 2 x 10'  $\frac{10}{12} \div 27 = 0.62$   
 $0.99$  C.Y. / L.F. = 2501 L.F.  
 $\times 250$  / L.Y. = 2501 L.F.  
 USE = 275 / L.F.~~

<b>Project</b> CHEYENNE MOUNTAIN RANCH DRAINAGE W. OF SH 115	<b>Job No</b> CE-3729
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<b>Client</b> GATES	<b>By</b> RM	<b>Date</b> OCT. 26, 1989
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EMERGENCY SPILLWAY FOR POND 1:

$Q_{100} = 430 \text{ CFS (OUTFLOW)}$

WEIR EQN:  $Q = CLH^{3/2}$

$C = 3.1$

$L = \text{WEIR LENGTH}$

$H = \text{DEPTH}$

ASSUME 2' FLOW DEPTH @ CREST

$440 = 3.1 (L) (2)^{3/2}$

$\Rightarrow L = 50.2 \text{ FT. (REASONABLE)}$

LENGTH OF SPILLWAY  $\approx 150'$

SLOPE = 55 = 40' / 150' = 10%

TRY 40' BOTTOM WIDTH TRAP. CHANNEL

$BW = 40'$

$n = .040 \text{ (RIPRAP)}$

$Z = 4:1 \quad S = 10\%$

$d = 1.0 \text{ FT.}$

$Q = 490 \text{ CFS}$

$V = 11.0 \text{ FPS}$

ASSUME

$50' \text{ WIDE RIPRAP} \times 150' \text{ LONG} \times 3' \text{ THICK} \div 27 =$

$833 \text{ C.Y. RIPRAP USE } 900 \text{ C.Y. @ } 50'$

Project CHEYENNE Mtn. RANCH  
DRAINAGE W. OF SH 115

Job No  
CE-3729

Client GATES

By [Signature]

Date 2/8/91

QUANTITY / COST EST. - POND NO. 2

EARTH FILL EST. - DETENTION POND #2

(ASSUME 16' TOP, 4:1 S/S, TOP ELEV. 87.0)

STA.	H(FT.)	A(SF)	A(AVG.)	L(FT.)	V(CF)	V(CY)
0	0	0				
			154	210	32,340	1198
2+10	7	308				
			658	170	111,860	4143
3+80	14	1008				
			1074	240	257,760	9547
6+20	15	1140				
			1074	40	42,960	1591
6+60	14	1008				
			1074	20	21,480	796
6+80	15	1140				
			1284	5	6420	238
6+85	17	1428				
			2388	35	83,580	3096
7+20	27	3348				
			3844	10	38,440	1424
7+30	31	4340				
			4340	30	130,200	4822
7+60	31	4340				
			2884	40	115,360	4273
8+00	17	1428				
			948	50	47,400	1756
8+50	9	468				
			234	45	10,530	390
8+95	0	0				

Σ 895 ✓ 898,330 33,274

34,000 C.Y.

Project CHEYENNE MTN. RANCH  
DRAINAGE W. OF SH 115

Job No  
E-3729

Client GATES

By RMI Date 3 AUG. 88  
REV. 2/8/91

QUANTITY / COST ESTIMATE - DETENTION POND 2

OUTFALL STRUCTURE

BARREL LENGTH - 250 FT. IN 59 OUT 55  
RISE HT. - 10 FT. ±

L = 250'  
Q = 1340 CFS  
n = .013  
H = 10'

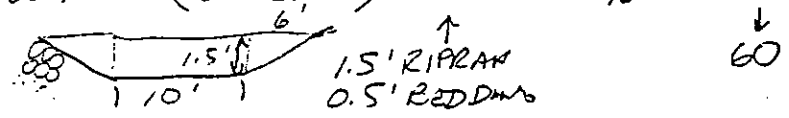
d = 90' → Q = 637 × 3 = 1911 CFS  
d = 96' → Q = 730 × 3 = 2190  
d = 102' → Q = 830

RIPRAP 50' × 40' × 4.5 ÷ 27 = 330 C.Y.

RISE Q<sub>100</sub> = 2200  
Q<sub>10</sub> = 850  
Q<sub>avg12</sub> = 1350 CFS  
H = 5'  
1350 = 2.1 L (5)<sup>3/2</sup>  
L = 39'

LOW FLOW CHAN. 2% SLOPE ± n = .040  
10' B.W. 4:1 5/8 1.5' DEEP  
Q = 132 CFS (~ 7% Q<sub>avg</sub> INFLOW) ✓

VOL. / FT. = (10' + 12.37') × 2' THICK × <sup>35</sup>/<sub>100</sub> ÷ 27 = 58 / C.F.





Project	CHEYENNE Mtn. RANCH DRAINAGE W. OF SH 115	Job No	CE-3729
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Client	GATES	By	RAJ	Date	26 OCT. 1989 REV. 2/28/90 & 2/8/91
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EMERGENCY SPILLWAY - POND #2

$Q_{100}$  (OUTFLOW) = 1320 CFS

LENGTH = 800' ±

$S = \frac{81-54}{800} = 3.4\%$

TRAPEZOIDAL CHANNEL

60' B.W.

3:1 S/S

$n = 0.40$

w/  $d = 2'$   $Q = 1350$  CFS  $V = 10.2$

RIPRAP  $70' \times 800' \times 3' \div 27 = 6222$  C.Y.

(NOT PRACTICAL)

TRY EARTH CHANNEL. w/ 5 8' DEEP CONCRETE

CUTOFF WALLS

$5 \times 80' \text{ LONG} \times 8' \text{ DEEP} \times 1.5' \text{ THICK} \div 27$

= 177.8 C.Y. CONCRETE

@ 250/C.Y. = \$44,444

↓  
\$50,000

Project CHEYENNE Mtn. RANUH DRAINAGE W. OF SH 115		Job No CE-3729
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Client GATES	By RM	Date 10/26/89 REV. 2/28/90
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CURVE NUMBERS/LAND USE:

LAND USE FOR DEVELOPED CONDITIONS IS OBTAINED FROM CURRENT MASTER PLANS FOR BROADMOOR, EL POMAR, NEAL RANCH, STAR RANCH, J.L. RANCH AND CHEYENNE MOUNTAIN RANCH. NO MASTER PLANS ARE AVAILABLE FOR THE U.S. GOV'T., MILDRED BEISSIG PROPERTY OR THE BENSBUIG ESTATE. IT IS ASSUMED THAT NO DEVELOPMENT WILL OCCUR ON THE BEISSIG PROPERTY. THE U.S. GOVERNMENT IS ASSUMED TO BE UNDEVELOPED. (A PREVIOUS DRAINAGE STUDY FOR THE NEAL RANCH (REF. 5) DETERMINED THAT ANY DEVELOPMENT ON THE U.S. GOV'T. SITE WAS OFFSET BY DETENTION AT ROAD CROSSINGS). FOR THE BENSBUIG ESTATE, A DENSITY OF 4 RESIDENTIAL UNITS PER ACRE IS ASSUMED. IF ACTUAL DENSITY IS GREATER THAN THAT, SOME ONSITE DETENTION MAY BE REQUIRED. DEVELOPED CURVE NOS. ARE BASED ON THE DCM. HISTORIC CURVE NUMBERS ARE DERIVED FROM REF. 8 AND ASSUME A 20% <sup>COVER</sup> PONDEROSA PINE/OAK COVER IN THE WESTERN PORTION OF THE BASIN, A 60% <sup>COVER</sup> PONDEROSA PINE/OAK IN THE EASTERN PORTION OF THE BASIN, AND RANGE IN FAIR CONDITION FOR THE UNWOODED PORTIONS OF THE BASIN. ALL CURVE NUMBERS ARE BASED ON ANTECEDANT MOISTURE CONDITION 2.

DEVELOP-  
MENT

**REGIONAL DETENTION PONDS AT BROADMOOR BLUFFS  
BASIN CURVE NUMBER - DEVELOPED AND HISTORIC CONDITIONS**

BASIN	OWNER	SOIL TYPE	DRAINAGE AREA (AC)	DEV. LAND USE	DEV. CN	DEV. CN * DA	DEV. AVG. OWNER CN	DEV. AVG. BASIN CN	HIST. LAND USE	HIST. CN	HIST. CN*DA	HIST.AVG. OWNER CN	HIST.AVG. BASIN CN
52	GATES	B	23.7	INDUST.	88	2085.6	88.0	88.0	RANGE	69	1635.3	69.0	69.0
	TOTAL		23.7			2085.6					1635.3		
64	GATES	B	15.7	INDUST.	88	1381.6	90.0	90.0	RANGE	69	1083.3	75.6	75.6
		C	30.8	INDUST.	91	2802.8			RANGE	79	2433.2		
	TOTAL	46.5	4184.4	3516.5									
20	GATES	C	8.8	INDUST.	91	800.8	91.6	91.6	RANGE	79	695.2	80.4	80.4
		C/D	10.9	INDUST.	92	1002.8			RANGE	81.5	888.4		
	TOTAL	19.7	1803.6	1583.6									
22	GATES	C	5.9	INDUST	91	536.9	91.6	91.6	RANGE	79	466.1	80.6	80.6
		C/D	10.5	INDUST	92	966.0			RANGE	81.5	855.8		
	TOTAL	16.4	1502.9	1321.9									
1	GATES	B	2.4	INDUST.	88	211.2	91.2	91.2	RANGE	69	165.6	79.2	79.2
		C	2.2	INDUST.	91	200.2			RANGE	79.0	173.8		
		C/D	10.7	INDUST.	92	984.4			RANGE	81.5	872.1		
		TOTAL	15.3	1395.8	1211.5								
200	GATES	B	4.2	INDUST.	88	369.6	90.8	90.8	RANGE	69	289.8	77.8	77.8
		C/D	8.4	INDUST.	92	772.8			RANGE	81.5	684.6		
		C	4.5	INDUST.	91	409.5			RANGE	79	355.5		
		TOTAL	17.1	1551.9	1329.9								
168	GATES	C	10.6	INDUST.	91	964.6	91.3	91.3	RANGE	79	837.4	79.8	79.8
		C/D	4.6	INDUST.	92	423.2			RANGE	81.5	374.9		
	TOTAL	15.2	1387.8	1212.3									
167	GATES	C/D	8.6	INDUST.	92	791.2	91.7	91.7	RANGE	81.5	700.9	80.7	80.7
		C	4.0	INDUST.	91	364.0			RANGE	79	316.0		
	TOTAL	12.6	1155.2	1016.9									
51	GATES	C	1.7	SCHOOL	79	134.3	83.9	83.9	WOODS	60	102.0	64.2	64.2
		C	2.5	COMM.	94	235.0			WOODS	60	150.0		
		B	2.5	SCHOOL	69	172.5			RANGE	69	172.5		
		C	3.6	S.F. - 1.7	79.7	286.9			WOODS	60	216.0		
		B	4.4	COMM.	92	404.8			RANGE	69	303.6		
		TOTAL	14.7	1233.5	944.1								
		62	GATES-F.P.	B	21.9	S.F. - 1.0			68	1489.2	71.2		
GATES-F.P.	C	7.7	S.F. - 1.0	79	608.3	WOODS	60	462.0					
GATES-F.P.	C	4.0	PARK	74	296.0	WOODS	60	240.0					
TOTAL	33.6	2393.5	1906.5										
63	GATES	C	2.5	S.F. - 1.9	79.9	199.8	79.2	79.2	WOODS	60	150.0	59.7	59.7
		C	19.6	SCHOOL	79	1548.4			WOODS	60	1176.0		
		C	20.8	M.F. - 6.0	86.5	1799.2			WOODS	60	1248.0		
		C	4.3	S.F. - 1.3	79.3	341.0			WOODS	60	258.0		
		B	4.7	S.F. - 1.3	68.6	322.4			WOODS	55	258.5		
		C	19.2	O.S.	74	1420.8			WOODS	60	1152.0		
		TOTAL	71.1	5631.6	4242.5								

11/23

REGIONAL DETENTION PONDS AT BROADMOOR BLUFFS  
 BASIN CURVE NUMBER - DEVELOPED AND HISTORIC CONDITIONS

BASIN	OWNER	SOIL TYPE	DRAINAGE AREA (AC)	DEV. LAND USE	DEV. CN	DEV. CN * DA	DEV. AVG. OWNER CN	DEV. AVG. BASIN CN	HIST. LAND USE	HIST. CN	HIST. CN*DA	HIST.AVG. OWNER CN	HIST.AVG. BASIN CN
21	GATES	C	13.4	S.F. - 1.0	79	1058.6	79.0	79.0	RANGE	79	1058.6	79.0	79.0
	TOTAL		13.4			1058.6					1058.6		
162	GATES	C	24.1	O.S.	74	1783.4	77.9	77.9	WOODS	60	1446.0	61.1	61.1
		C/D	4.5	O.S.	81.5	366.8			WOODS	65	292.5		
		C/D	3.5	M.F. - 6.0	88	308.0			WOODS	65	227.5		
		C	4.9	M.F. - 6.0	86.5	423.9			WOODS	60	294.0		
	TOTAL		37.0			2882.0	2882.0	2260.0					
163	GATES	C	2.6	M.F. - 8.0	90	234.0	90.7	90.7	WOODS	60	156.0	63.6	63.6
	TOTAL	C/D	7.0	M.F. - 8.0	91	637.0			WOODS	65	455.0		
			9.6			871.0					611.0		
165	GATES	C	28.7	M.F. - 8.0	90	2583.0	82.1	82.1	WOODS	60	1722.0	59.6	59.6
		C	18.1	O.S.	74	1339.4			WOODS	60	1086.0		
		B	3.8	O.S.	61	231.8			WOODS	55	209.0		
	TOTAL		50.6			4154.2	4154.2	3017.0					
161	GATES	B	12.1	S.F. - 1.0	68	822.8	74.4	74.4	WOODS	55	665.5	57.6	57.6
	GATES/NR	C	17.9	S.F. - 1.0	79	1414.1			WOODS	60	1074.0		
		B	4.8	S.F. - 3.5	73.5	352.8			WOODS	55	264.0		
	TOTAL		34.8			2589.7			2589.7	2003.5			
166	BENSBURG	B	4.8	S.F. - 2.0	70	336	78.7	78.7	RANGE	69	331.2	77.7	77.7
		C	15.4	S.F. - 2.0	80	1232			RANGE	79	1216.6		
		C/D	6.0	S.F. - 2.0	82.5	495			RANGE	81.5	489		
	TOTAL		26.2			2063.0	2063.0	2036.8					
60	SELLON NR #2 - F.P.	B	15.0	S.F. - 2.4	70.8	1062.0	72.3	72.3	WOODS	55	825.0	55.0	55.0
	SELLON NR#3 - F.P.	B	11.2	S.F. - 2.3	70.6	790.7			WOODS	55	616.0		
	SELLON NR #5 - F.P.	B	10.5	M.F. - 7.0	82.5	866.3			WOODS	55	577.5		
	SELLON BO #5 - F.P.	B	1.0	S.F. - 3.0	72	72.0			WOODS	55	55.0		
	SELLON BO #5 - F.P.	B	3.0	PARK	61	183.0			WOODS	55	165.0		
	SELLON	B	9.3	SCHOOL	69	641.7			WOODS	55	511.5		
	SUBTOTAL SELLON		50.0			3615.7			3615.7	2750.0			
	MLV (DEV. CN PER O.E. WATTS STUDY)	B	3.2	S.F. - 2.0	69.8	223.4			WOODS	55	176.0		
	SUBTOT. MLV		3.2			223.4			223.4	176.0			
	TOTAL		53.2			3839.0			3839.0	2926.0			

E3111

REGIONAL DETENTION PONDS AT BROADMOOR BLUFFS  
 BASIN CURVE NUMBER - DEVELOPED AND HISTORIC CONDITIONS

BASIN	OWNER	SOIL TYPE	DRAINAGE AREA (AC)	DEV. LAND USE	DEV. CN	DEV. CN * DA	DEV. AVG. OWNER CN	DEV. AVG. BASIN CN	HIST. LAND USE	HIST. CN	HIST. CN*DA	HIST.AVG. OWNER CN	HIST.AVG. BASIN CN
61	SELLON - F.P.	B	5.9	PARK	61	359.9			WOODS	55	324.5		
	SELLON	B	5.1	SCHOOL	69	351.9			WOODS	55	280.5		
	SELLON - F.P.	B	2.0	PARK	61	122.0			WOODS	55	110.0		
	SELLON - BO #5	B	1.4	S.F. - 3.0	72	100.8			WOODS	55	77.0		
	SELLON - BO #8	B	2.9	S.F. - 1.9	69.8	202.4			WOODS	55	159.5		
	SELLON - MO #2	B	18.4	S.F. - 3.5	73.5	1352.4			WOODS	55	1012.0		
	SELLON - BO #3 - F.P.(DEV CN PER WATTS)	B	6.7	S.F. 2.2	70.2	470.3			WOODS	55	368.5		
	SUBTOT. SELLON		42.4			2959.8	69.8				2332.0	55.0	
	MLV	B	15.0	S.F. - 2.0	69.8	1047.0			WOODS	55	825.0		
	MLV	B	0.3	S.F. - 2.0	70	21.0			WOODS	55	16.5		
	SUBTOT. MLV		15.3			1068.0	69.8				841.5	55.0	
	BROADMOOR	B	16.5	S.F. - 1.4	68.6	1131.9			WOODS	55	907.5		
		B	1.0	S.F. - 0.9	67.6	67.6			WOODS	55	55.0		
	SUBTOT. BROADMOOR		17.5			1199.5	68.5				962.5	55.0	
	GATES	B	0.5	S.F. - 3.5	73.5	36.8			WOODS	55	27.5		
	SUBTOT. GATES		0.5			36.8	73.5				27.5	55.0	
	STAR RANCH	B	30.0	S.F. - 5.1	77.8	2334.0			WOODS	55	1650.0		
	SUBTOT. STAR RANCH		30.0			2334.0	77.8				1650.0	55.0	
	TOTAL BASIN		105.7			7598.0		71.9			5813.5		55.0
	160	SELLON MO #2 - F.P.	B	6.8	S.F. - 3.5	73.5	499.8			WOODS	55	374.0	
SELLON BO #1 - F.P.		B	4.5	S.F. - 2.2	70.4	316.8			WOODS	55	247.5		
SELLON		B	1.6	S.F. - 2.4	70.8	113.3			WOODS	55	88.0		
SELLON BO #3 - F.P.		B	20.3	S.F. - 2.2	70	1421.0			WOODS	55	1116.5		
SELLON BO #4		B	5.5	S.F. - 2.2	70	385.0			WOODS	55	302.5		
PER OE WATTS STUDY)		B	0.7	S.F. - 2.4	70.3	49.2			WOODS	55	38.5		
SELLON - PARK		B	5.0	PARK	61	305.0			WOODS	55	275.0		
SUBTOTAL - SELLON			44.4			3090.1	69.6				2442.0	55.0	
J.L. RANCH		B	23.1	O.S.	55	1270.5			WOODS	55	1270.5		
J.L. RANCH		B	1.1	O.S.	55	60.5			WOODS	55	60.5		
J.L. RANCH		B	6.6	S.F. - 2.0	70	462.0			WOODS	55	363.0		
J.L. RANCH		B	11.3	S.F. - 2.0	70	791.0			WOODS	55	621.5		
SUBTOTAL J.L. RANCH			42.1			2584.0	61.4				2315.5	55.0	
MLV		B	5.6	S.F. - 2.0	69.8	390.9			WOODS	55	308.0		
MLV		B	4.0	S.F. - 2.0	70	280.0			WOODS	55	220.0		
MLV		B	3.5	S.F. - 2.4	69.8	244.3			WOODS	55	192.5		
MLV		B	1.3	S.F. - 1.9	69.8	90.7			WOODS	55	71.5		
MLV		B	42.0	S.F. - 1.9	69.8	2931.6			WOODS	55	2310.0		
SUBTOTAL MLV			56.4			3937.5	69.8				3102.0	55.0	
GATES		B	3.2	S.F. - 3.5	73.5	235.2			WOODS	55	176.0		
SUBTOTAL GATES		3.2			235.2	73.5				176.0	55.0		

E4111

REGIONAL DETENTION PONDS AT BROADMOOR BLUFFS  
 BASIN CURVE NUMBER - DEVELOPED AND HISTORIC CONDITIONS

BASIN	OWNER	SOIL TYPE	DRAINAGE AREA (AC)	DEV. LAND USE	DEV. CN	DEV. CN * DA	DEV. AVG. OWNER CN	DEV. AVG. BASIN CN	HIST. LAND USE	HIST. CN	HIST. CN*DA	HIST.AVG. OWNER CN	HIST.AVG. BASIN CN
160 CONT.	BROADMOOR	B	32.9	S.F. - 0.8	67.7	2227.3			WOODS	55	1809.5		
	BROADMOOR	B	62.1	O.S.	55	3415.5			WOODS	55	3415.5		
	BROADMOOR	D	10.7	O.S.	81	866.7			WOODS	81	866.7		
	BROADMOOR	D	93.0	O.S.	81	7533.0			WOODS	81	7533.0		
	SUBTOTAL BROADMOOR		198.7			14042.5	70.7				13624.7	68.6	
	M. BEISSIG	D	17.0	O.S.	81	1377.0			WOODS	81	1377.0		
	SUBTOTAL BEISSIG		17.0			1377.0	81.0				1377.0	81.0	
	STAR RANCH	B	17.5	M.F. - 5.1	77.8	1361.5			WOODS	55	962.5		
	SUBTOTAL STAR RANCH		17.5			1361.5	77.8				962.5	55.0	
	TOTAL BASIN		379.3			26627.8		70.2			23999.7		63.3
164	BENSBURG	C	40.2	S.F. - 2.0	80	3216.0			WOODS	60	2412.0		
	BENSBURG	B	25.3	S.F. - 2.0	70	1771.0			WOODS	55	1391.5		
	SUBTOTAL BENSBURG		65.5			4987.0	76.1				3803.5	58.1	
	J.L. RANCH	C	4.7	O.S.	60	282.0			WOODS	60	282.0		
	J.L. RANCH	C	0.5	S.F. - 2.0	80	40.0			WOODS	60	30.0		
	J.L. RANCH	B	5.7	O.S.	55	313.5			WOODS	55	313.5		
	J.L. RANCH	B	7.7	O.S.	55	423.5			WOODS	55	423.5		
	J.L. RANCH	B	1.7	O.S.	55	93.5			WOODS	55	93.5		
	J.L. RANCH	B	1.9	O.S.	55	104.5			WOODS	55	104.5		
	J.L. RANCH	B	9.6	S.F. - 2.0	70	672.0			WOODS	55	528.0		
	J.L. RANCH	B	3.1	S.F. - 2.0	70	217.0			WOODS	55	170.5		
	J.L. RANCH	B	2.0	S.F. - 3.0	72	144.0			WOODS	55	110.0		
	J.L. RANCH	B	1.2	S.F. - 1.0	68	81.6			WOODS	55	66.0		
	J.L. RANCH	B	18.2	S.F. - 2.0	70	1274.0			WOODS	55	1001.0		
	J.L. RANCH	B	4.0	S.F. - 2.0	70	280.0			WOODS	55	220.0		
	J.L. RANCH	B	1.7	O.S.	55	93.5			WOODS	55	93.5		
	J.L. RANCH	C	0.5	S.F. - 2.0	80	40.0			WOODS	60	30.0		
	SUBTOTAL J.L. RANCH		62.5			4059.1	64.9				3466.0	55.5	
	SELLON	B	0.8	S.F. - 2.7	71.4	57.1			WOODS	55	44.0		
	SELLON BO #7 (DEV CN PER OE WATTS STUDY)	B	37.3	S.F. - 2.4	70.9	2644.6			WOODS	55	2051.5		
	SUBTOTAL SELLON		38.1			2701.7	70.9				2095.5	55.0	
	MLV	B	20.8	S.F. - 1.5	69	1435.2			WOODS	55	1144.0		
	MLV	B	5.9	S.F. - 2.7	71.4	421.3			WOODS	55	324.5		
	MLV	B	1.8	S.F. - 2.2	70.4	126.7			WOODS	55	99.0		
	MLV	B	0.8	S.F. - 2.0	70	56.0			WOODS	55	44.0		
	MLV	B	8.3	S.F. - 2.0	70	581.0			WOODS	55	456.5		
	MLV	B	4.8	S.F. - 1.2	68.4	328.3			WOODS	55	264.0		
	MLV	B	3.4	S.F. - 1.9	69.8	237.3			WOODS	55	187.0		
	MLV	B	4.9	S.F. - 1.9	69.8	342.0			WOODS	55	269.5		
	MLV	B	13.3	S.F. - 1.9	69.8	928.3			WOODS	55	731.5		
MLV	B	22.5	S.F. - 1.9	69.8	1570.5			WOODS	55	1237.5			
SUBTOTAL MLV		86.5			6026.7	69.7				4757.5	55.0		

ES/11

**REGIONAL DETENTION PONDS AT BROADMOOR BLUFFS  
BASIN CURVE NUMBER - DEVELOPED AND HISTORIC CONDITIONS**

BASIN	OWNER	SOIL TYPE	DRAINAGE AREA (AC)	DEV. LAND USE	DEV. CN	DEV. CN * DA	DEV. AVG. OWNER CN	DEV. AVG. BASIN CN	HIST. LAND USE	HIST. CN	HIST. CN*DA	HIST.AVG. OWNER CN	HIST.AVG. BASIN CN
164 CONT.	U.S. GOVERNMENT	B	36.0	O.S.	55	1980.0			WOODS	55	1980.0		
	U.S. GOVERNMENT	D	48.0	O.S.	81	3888.0			WOODS	81	3888.0		
	U.S. GOVERNMENT	D	46.5	O.S.	81	3766.5			WOODS	81	3766.5		
	SUBTOTAL - U.S. GOV.		130.5			9634.5	73.8				9634.5	73.8	
	M. BEISSIG	D	176.0	O.S.	81	14256.0			WOODS	81	14256.0		
	SUBTOTAL BEISSIG		176.0			14256.0	81.0				14256.0	81.0	
	BROADMOOR	B	11.6	S.F. - 0.8	67.5	783.0			WOODS	55	638.0		
	BROADMOOR	B	18.4	O.S.	55	1012.0			WOODS	55	1012.0		
	BROADMOOR	D	10.0	O.S.	81	810.0			WOODS	81	810.0		
	BROADMOOR	D	22.0	O.S.	81	1782.0			WOODS	81	1782.0		
	SUBTOTAL BROADMOOR		62.0			4387.0	70.8				4242.0	68.4	
	BASIN TOTAL		621.1			46052.0		74.1			42255.0		68.0

E6/11

**REGIONAL DETENTION PONDS AT BROADMOOR BLUFFS  
OWNER CURVE NUMBERS - DETENTION POND NO. 1**

BASIN	OWNER	SOIL TYPE	DRAINAGE AREA (AC)	DEV. LAND USE	DEV. CN	DEV. CN * DA	DEV. AVG. OWNER CN	HIST. LAND USE	HIST. CN	HIST. CN*DA	HIST.AVG. OWNER CN
52	GATES	B	23.7	INDUST.	88	2085.6		RANGE	69	1635.3	
64	GATES	B	15.7	INDUST.	88	1381.6		RANGE	69	1083.3	
64		C	30.8	INDUST.	91	2802.8		RANGE	79	2433.2	
20	GATES	C	8.8	INDUST.	91	800.8		RANGE	79	695.2	
20		C/D	10.9	INDUST.	92	1002.8		RANGE	81.5	888.4	
22	GATES	C	5.9	INDUST.	91	536.9		RANGE	79	466.1	
22		C/D	10.5	INDUST.	92	966.0		RANGE	81.5	855.8	
51	GATES	C	1.7	SCHOOL	79	134.3		WOODS	60	102.0	
51		C	2.5	COMM.	94	235.0		WOODS	60	150.0	
51		B	2.5	SCHOOL	69	172.5		RANGE	69	172.5	
51		C	3.6	S.F. - 1.7	79.7	286.9		WOODS	60	216.0	
51		B	4.4	COMM.	92	404.8		RANGE	69	303.6	
63	GATES	C	2.5	S.F. - 1.9	79.9	199.8		WOODS	60	150.0	
63		C	19.6	SCHOOL	79	1548.4		WOODS	60	1176.0	
63		C	20.8	M.F. - 6.0	86.5	1799.2		WOODS	60	1248.0	
63		C	4.3	S.F. - 1.3	79.3	341.0		WOODS	60	258.0	
63		B	4.7	S.F. - 1.3	68.6	322.4		WOODS	55	258.5	
63		C	19.2	O.S.	74	1420.8		WOODS	60	1152.0	
21	GATES	C	13.4	S.F. - 1.0	79	1058.6		RANGE	79	1058.6	
61	GATES	B	0.5	S.F. - 3.5	73.5	36.8		WOODS	55	27.5	
	<b>TOTAL GATES</b>		<b>206</b>			<b>17536.9</b>	<b>85.1</b>			<b>14329.9</b>	<b>69.6</b>
60	SELLON	B	9.3	SCHOOL	69	641.7		WOODS	55	511.5	
61	SELLON	B	5.1	SCHOOL	69	351.9		WOODS	55	280.5	
61	SELLON - BO #5	B	1.4	S.F. - 3.0	72	100.8		WOODS	55	77.0	
61	SELLON - BO #8	B	2.9	S.F. - 1.9	69.8	202.4		WOODS	55	159.5	
61	SELLON - MO #2	B	18.4	S.F. - 3.5	73.5	1352.4		WOODS	55	1012.0	
	<b>TOTAL SELLON</b>		<b>37.1</b>			<b>2649.2</b>	<b>71.4</b>			<b>2040.5</b>	<b>55.0</b>
61	MLV	B	0.3	S.F. - 2.0	70	21.0		WOODS	55	16.5	
60	MLV (DEV. CN PER O.E. V	B	3.2	S.F. - 2.0	69.8	223.4		WOODS	55	176.0	
61	MLV	B	15	S.F. - 2.0	69.8	1047.0		WOODS	55	825.0	
	<b>TOTAL MLV</b>		<b>18.5</b>			<b>1291.4</b>	<b>69.8</b>			<b>1017.5</b>	<b>55.0</b>
61	BROADMOOR	B	16.5	S.F. - 1.4	68.6	1131.9		WOODS	55	907.5	
61		B	1	S.F. - 0.9	67.6	67.6		WOODS	55	55.0	
	<b>TOTAL BROADMOOR</b>		<b>17.5</b>			<b>1199.5</b>	<b>68.5</b>			<b>962.5</b>	<b>55.0</b>
61	STAR RANCH	B	30	S.F. - 5.1	77.8	2334.0		WOODS	55	1650.0	
	<b>TOTAL STAR RANCH</b>		<b>30</b>			<b>2334.0</b>	<b>77.8</b>			<b>1650.0</b>	<b>55.0</b>

E711



**REGIONAL DETENTION PONDS AT BROADMOOR BLUFFS  
OWNER CURVE NUMBERS - DETENTION POND NO. 2**

BASIN	OWNER	SOIL TYPE	DRAINAGE AREA (AC)	DEV. LAND USE	DEV. CN	DEV. CN * DA	DEV. AVG. OWNER CN	HIST. LAND USE	HIST. CN	HIST. CN*DA	HIST.AVG. OWNER CN
162	GATES	C	24.1	O.S.	74.0	1783.4		WOODS	60.0	1446.0	
162		C/D	4.5	O.S.	81.5	366.8		WOODS	65.0	292.5	
162		C/D	3.5	M.F. - 6.0	88.0	308.0		WOODS	65.0	227.5	
162		C	4.9	M.F. - 6.0	86.5	423.9		WOODS	60.0	294.0	
163	GATES	C	2.6	M.F. - 8.0	90.0	234.0		WOODS	60.0	156.0	
163		C/D	7	M.F. - 8.0	91.0	637.0		WOODS	65.0	455.0	
165	GATES	C	28.7	M.F. - 8.0	90.0	2583.0		WOODS	60.0	1722.0	
165		C	18.1	O.S.	74.0	1339.4		WOODS	60.0	1086.0	
165		B	3.8	O.S.	61.0	231.8		WOODS	55.0	209.0	
161	GATES	B	12.1	S.F. - 1.0	68.0	822.8		WOODS	55.0	665.5	
161		C	17.9	S.F. - 1.0	79.0	1414.1		WOODS	60.0	1074.0	
161	GATES/NR	B	4.8	S.F. - 3.5	73.5	352.8		WOODS	55.0	264.0	
160	GATES	B	3.2	S.F. - 3.5	73.5	235.2		WOODS	55.0	176.0	
	<b>TOTAL GATES</b>		<b>135.2</b>			<b>10732.1</b>	<b>79.4</b>			<b>8067.5</b>	<b>59.7</b>
160	SELLON	B	1.6	S.F. - 2.4	70.8	113.3		WOODS	55.0	88.0	
160	SELLON BO #4	B	5.5	S.F. - 2.2	70.0	385.0		WOODS	55.0	302.5	
160	SELLON BO #7 (DEV. CN	B	0.7	S.F. - 2.4	70.3	49.2		WOODS	55.0	38.5	
164	SELLON	B	0.8	S.F. - 2.7	71.4	57.1		WOODS	55.0	44.0	
164	SELLON BO #7 (DEV CN F	B	37.3	S.F. - 2.4	70.9	2644.6		WOODS	55.0	2051.5	
	<b>TOTAL SELLON</b>		<b>45.9</b>			<b>3249.2</b>	<b>70.8</b>			<b>2524.5</b>	<b>55.0</b>
160	J.L. RANCH	B	23.1	O.S.	55.0	1270.5		WOODS	55.0	1270.5	
160	J.L. RANCH	B	1.1	O.S.	55.0	60.5		WOODS	55.0	60.5	
160	J.L. RANCH	B	6.6	S.F. - 2.0	70.0	462.0		WOODS	55.0	363.0	
160	J.L. RANCH	B	11.3	S.F. - 2.0	70.0	791.0		WOODS	55.0	621.5	
164	J.L. RANCH	C	4.7	O.S.	60.0	282.0		WOODS	60.0	282.0	
164	J.L. RANCH	C	0.5	S.F. - 2.0	80.0	40.0		WOODS	60.0	30.0	
164	J.L. RANCH	B	5.7	O.S.	55.0	313.5		WOODS	55.0	313.5	
164	J.L. RANCH	B	7.7	O.S.	55.0	423.5		WOODS	55.0	423.5	
164	J.L. RANCH	B	1.7	O.S.	55.0	93.5		WOODS	55.0	93.5	
164	J.L. RANCH	B	1.9	O.S.	55.0	104.5		WOODS	55.0	104.5	
164	J.L. RANCH	B	9.6	S.F. - 2.0	70.0	672.0		WOODS	55.0	528.0	
164	J.L. RANCH	B	3.1	S.F. - 2.0	70.0	217.0		WOODS	55.0	170.5	
164	J.L. RANCH	B	2	S.F. - 3.0	72.0	144.0		WOODS	55.0	110.0	
164	J.L. RANCH	B	1.2	S.F. - 1.0	68.0	81.6		WOODS	55.0	66.0	
164	J.L. RANCH	B	18.2	S.F. - 2.0	70.0	1274.0		WOODS	55.0	1001.0	
164	J.L. RANCH	B	4	S.F. - 2.0	70.0	280.0		WOODS	55.0	220.0	
164	J.L. RANCH	B	1.7	O.S.	55.0	93.5		WOODS	55.0	93.5	

**REGIONAL DETENTION PONDS AT BROADMOOR BLUFFS  
OWNER CURVE NUMBERS - DETENTION POND NO. 2**

BASIN	OWNER	SOIL TYPE	DRAINAGE AREA (AC)	DEV. LAND USE	DEV. CN	DEV. CN * DA	DEV. AVG. OWNER CN	HIST. LAND USE	HIST. CN	HIST. CN*DA	HIST.AVG. OWNER CN
164	J.L. RANCH	C	0.5	S.F. - 2.0	80.0	40.0		WOODS	60.0	30.0	
	<b>TOTAL J.L. RANCH</b>		<b>104.6</b>			<b>6643.1</b>	<b>63.5</b>			<b>5781.5</b>	<b>55.3</b>
160	MLV	B	5.6	S.F. - 2.0	69.8	390.9		WOODS	55.0	308.0	
160	MLV	B	3.5	S.F. - 2.4	69.8	244.3		WOODS	55.0	192.5	
160	MLV	B	1.3	S.F. - 1.9	69.8	90.7		WOODS	55.0	71.5	
160	MLV	B	4	S.F. - 2.0	70.0	280.0		WOODS	55.0	220.0	
160	MLV	B	42	S.F. - 1.9	69.8	2931.6		WOODS	55.0	2310.0	
164	MLV	B	5.9	S.F. - 2.7	71.4	421.3		WOODS	55.0	324.5	
164	MLV	B	1.8	S.F. - 2.2	70.4	126.7		WOODS	55.0	99.0	
164	MLV	B	0.8	S.F. - 2.0	70.0	56.0		WOODS	55.0	44.0	
164	MLV	B	20.8	S.F. - 1.5	69.0	1435.2		WOODS	55.0	1144.0	
164	MLV	B	8.3	S.F. - 2.0	70.0	581.0		WOODS	55.0	456.5	
164	MLV	B	4.8	S.F. - 1.2	68.4	328.3		WOODS	55.0	264.0	
164	MLV	B	3.4	S.F. - 1.9	69.8	237.3		WOODS	55.0	187.0	
164	MLV	B	4.9	S.F. - 1.9	69.8	342.0		WOODS	55.0	269.5	
164	MLV	B	13.3	S.F. - 1.9	69.8	928.3		WOODS	55.0	731.5	
164	MLV	B	22.5	S.F. - 1.9	69.8	1570.5		WOODS	55.0	1237.5	
	<b>TOTAL MLV</b>		<b>142.9</b>			<b>9964.2</b>	<b>69.7</b>			<b>7859.5</b>	<b>55.0</b>
160	BROADMOOR	B	32.9	S.F. - 0.8	67.7	2227.3		WOODS	55.0	1809.5	
164	BROADMOOR	B	11.6	S.F. - 0.8	67.5	783.0		WOODS	55.0	638.0	
	<b>TOTAL BROADMOOR</b>		<b>44.5</b>			<b>3010.3</b>	<b>67.6</b>			<b>2447.5</b>	<b>55.0</b>
160	STAR RANCH	B	17.5	M.F. - 5.1	77.8	1361.5		WOODS	55.0	962.5	
	<b>TOTAL STAR RANCH</b>		<b>17.5</b>			<b>1361.5</b>	<b>77.8</b>			<b>962.5</b>	<b>55.0</b>
164	BENSBURG	C	40.2	S.F. - 2.0	80.0	3216.0		WOODS	60.0	2412.0	
164	BENSBURG	B	25.3	S.F. - 2.0	70.0	1771.0		WOODS	55.0	1391.5	
	<b>TOTAL BENSBURG</b>		<b>65.5</b>			<b>4987.0</b>	<b>76.1</b>			<b>3803.5</b>	<b>58.1</b>

E911

Project MASTER DEVELOPMENT DRAINAGE PLAN REGIONAL DETENTION PONDS AT ROADMOOR BLUFFS	Job No EW-1011
Client GATES LAND CO.	By Rm Date 6/16/93

HISTORIC CURVE NOS. FOR TR-20

BASIN 060 (DEV. BASINS 051-064)

<u>BASIN</u>	<u>D.A.</u>	<u>HIST. CN</u>	<u>DA x CN</u>
051	14.7 AC.	64.2	944.1
052	23.7	69.0	1635.3
060	53.2	55.0	2926.0
061	105.7	55.0	5813.5
062	33.6	56.7	1906.5
063	71.1	59.7	4242.5
064	46.5	75.6	3516.5
	<u>348.5 AC.</u>		<u>20,984.4</u>

0.545 SQ. MI.

$$CN = \frac{20,984.4}{348.5} = 60.2$$

BASIN 020 (DEV. BASINS 020, 021, 022)

<u>BASIN</u>	<u>D.A.</u>	<u>HIST. CN</u>	<u>DA x CN</u>
020	19.7 (.031)	80.4	1583.6
021	13.4 (.021)	79.0	1058.6
022	16.4 (.026)	80.6	1321.9
	<u>49.5 AC.</u>		<u>3964.1</u>
	(.078 MI. <sup>2</sup> )		

$$CN = \frac{3964.1}{49.5} = 80.1$$

BASIN 001

DA = 15.3 AC. (.024 SQ. MI.)

CN = 79.2 (FROM CN SPREADSHEET)

Project <u>MASTER DEVELOPMENT DRAINAGE PLAN</u> <u>REGIONAL DETENTION PONDS AT BROADMOOR BLUFFS</u>	Job No <u>EW-1011</u>
Client <u>GATES LAND CO.</u>	By <u>Rm</u> Date <u>6/16/93</u>

BASIN 200

D.A. = 17.1 AC. (.027 SQ. MI.)

CN = 77.8 (PER CN SPREADSHEET)

BASIN 160 (DEV. BASINS 160-163)

<u>BASIN</u>	<u>D.A.</u>	<u>HIST CN</u>	<u>DA x CN</u>
160	379.3	63.0	23999.7
161	34.8	57.6	2003.5
162	37.0	61.1	2260.0
163	<u>9.6</u>	63.6	<u>611.0</u>
	460.7 AC. (.720 SQ. MI.)		28,874.2

$$CN = \frac{28,874.2}{460.7} = 62.7$$

BASIN 164 (DEV. BASINS 164 & 165)

<u>BASIN</u>	<u>D.A.</u>	<u>HIST. CN</u>	<u>DA x CN</u>
164	621.1 (970)	68.0	42,255
165	<u>50.6 (079)</u>	59.6	<u>3017.0</u>
	671.7 AC. (1.049)		45,272

$$CN = \frac{45,272}{671.7} = 67.4$$

BASIN 168

D.A. = 15.2 AC. (.024 SQ. MI.) CN = 79.8 (FROM CN SPREADSHEET)

BASIN 166 (DEV. BASINS 166 & 167)

<u>BASIN</u>	<u>DA</u>	<u>HIST CN</u>	<u>CN x DA</u>
166	26.2	77.7	2036.8
167	12.6	80.7	1016.9
	DA = 38.8 (.061 SQ. MI.)		CN = $\frac{2036.8 + 1016.9}{38.8} = 78.7$

TABLE 5-5  
 RUNOFF CURVE NUMBERS FOR HYDROLOGIC SOIL  
 COVER COMPLEXES - URBAN AND SUBURBAN CONDITIONS 1/  
 (Antecedent Moisture Condition II)  
 (From: U.S. Dept. of Agriculture,  
 Soil Conservation Service, 1977)

<u>Land Use</u>	<u>Hydrologic Soil Group</u>			
	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>
Open spaces, lawns, parks, golf courses, cemeteries, etc.				
Good condition: grass cover on 75% or more of the area	39*	61	74	80
Fair condition: grass cover on 50% to 75% of the area	49*	69	79	84
Commercial and Business areas (85% Impervious)	89*	92	94	95
Industrial Districts 72% Impervious)	81*	88	91	93
Residential: <u>2/</u>				
<u>Acres per Dwelling Unit</u>	<u>Average %</u>			
	<u>Impervious</u> <sup>3/</sup>			
1/8 acre or less	65	77*	85	90
1/4 acre	38	61*	75	83
1/3 acre	30	57*	72	81
1/2 acre	25	54*	70	80
1 acre	20	51*	68	79
Paved parking lots, roofs, driveways, etc.	98	98	98	98
Streets and Roads:				
paved with curbs and storm sewers	98	98	98	98
gravel	76*	85	89	91
dirt	72*	82	87	89

1/ For a more detailed description of agricultural land use curve numbers, refer to the National Engineering Handbook (U.S. Dept. of Agriculture, Soil Conservation Service, 1972).

2/ Curve numbers are computed assuming the runoff from the house and driveway is directed towards the street with a minimum of roof water directed to lawns where additional infiltration could occur.

3/ The remaining pervious areas (lawn) are considered to be in good pasture condition for these curve numbers.

\* Not to be used wherever overlot grading or filling is to occur.

Project MASTER DEVELOPMENT DRAINAGE PLAN REGIONAL DETENTION PONDS AT BROADMOOR BLUFFS		Job No EW-1011
Client GATES LAND CO.	By RM	Date 6/11/93

REVIEW/EVALUATE TEMPORARY DETENTION PONDS PRESENTED IN PRELIMINARY AND FINAL DRAINAGE STUDY, GLEN OAKS AT BROADMOOR, COUNTRY WALK AT BROADMOOR, GLEN OAKS AT BROADMOOR FILING NO. 2, DONNELL JEFFRIES, OCT. 17, 1988 AND COUNTRY WALK AT BROADMOOR NO. 4 (LETTER REPORT), JEFFRIES ENGINEERING, JUNE 16, 1992.

DETENTION AVAILABLE AT 120"/84" CM CULVERT @ BROADMOOR BLUFFS DRIVE @ SOUTH END OF DEVELOPMENT. (COUNTRYWALK AT BROADMOOR NO. 4). = 15,060 CU. FT.

TR-20 PRINTOUT OF DETENTION POND NO. 2

⇒ 100-YR. ELV. = 5980.4  
 " " VOL. = 43.9 AC. FT.  
 " " AREA OF POOL = 4.21 AC.

ASSUME STORAGE IS 100% EFFECTIVE (I.E. 1 AC.-FT. STORAGE @ TEMP. POND REDUCE VOLUME OF POND 2 BY 1 AC.-FT. (MOST LIKELY NOT 100% EFFECTIVE))

$$\text{REDUCTION IN DAM HEIGHT} \approx \frac{15,060}{4.21 \times 43,560} = 0.08'$$

REDUCTION IN DAM HEIGHT < 0.1' -  
NOT SIGNIFICANT.

Project MASTER DEVELOPMENT DRAINAGE PLAN REGIONAL DETENTION PONDS AT BROADMOOR BLUFFS	Job No EW-1011	
Client GATES LAND Co.	By RM	Date 6/11/93

REVIEW/EVALUATE TEMPORARY DETENTION POND AT 90" CM CULVERT UNDER BROADMOOR BLUFFS DRIVE NEAR THE SOUTH BOUNDARY OF GLEN OAKS @ BROADMOOR

VOLUME AVAILABLE 40,504 CU.FT. @ ELEV. 37.2  
RISE CREST ELEV. 35.7

$$\text{REDUCTION IN DAM HEIGHT} \approx \frac{40,504}{4.21 \times 43,560} \approx 0.22'$$

REDUCTION IN DAM HEIGHT  $\approx 0.2'$  WILL NOT HAVE A SIGNIFICANT EFFECT ON COST. IN ADDITION, THE HOUSE JUST SOUTH OF THE OUTLET STRUCTURE HAS A WALK-OUT LEVEL THAT APPEARS TO BE ONLY 12" ABOVE THE TOP OF RISE ELEVATION AND IS LESS THAN THE ELEVATION OF BROADMOOR BLUFFS DRIVE AT THAT LOCATION. FLOWS IN EXCESS OF DESIGN FLOWS OR PARTIAL BLOCKING OF THE OUTLET STRUCTURE COULD POTENTIALLY RESULT IN FLOODING OF THE LOWER LEVEL OF THE HOUSE.

Project CHEYENNE MOUNTAIN RANCH RESIDUAL DETENTION		Job No EW-1011
Client GATES	By RM	Date 6/11/93

ADD ADDITIONAL DETENTION POND TO MODEL (STRUCTURE NO. 7D).

REFERENCE: - DRAINAGE REPORT, MOUNTAIN OAKS SUBDIVISION NO. 2 BY OLIVER E. WATTS, DECEMBER 14, 1990.

- LETTER FROM OLIVER E. WATTS TO BOB ADAMCZYK, JAN. 10, 1991.

AS-BUILT ELEVATION STORAGE CURVE (PER 1/10/91 LETTER)

<u>ELEV.</u>	<u>STORAGE (AC.-FT.)</u>
39.7	0
42.0	0.01
44.0	0.03
46.0	0.09
48.0	0.22
50.0	0.56
50.9	0.67*
51.5	0.74*
53.0	0.93*

\* - STORAGE ABOVE ELEV. 50.0 EXTRAPOLATED BASED ON ASSUMED POOL AREA OF 5364 SQ. FT. (AREA @ 50.0) - CONSERVATIVE



Project CHEYENNE MOUNTAIN RANCH REGIONAL DETENTION Job No EW-1011

Client GATES By RM Date 6/11/93

ELEVATION - DISCHARGE CURVE BASED ON PG. 5  
OF 9. OLIVER E. WATTS DRAINAGE STUDY,  
MOUNTAIN OAKS SUBDIVISION NO. 2.

CHECK  $\frac{2}{16}$  27" RESTRICTOR

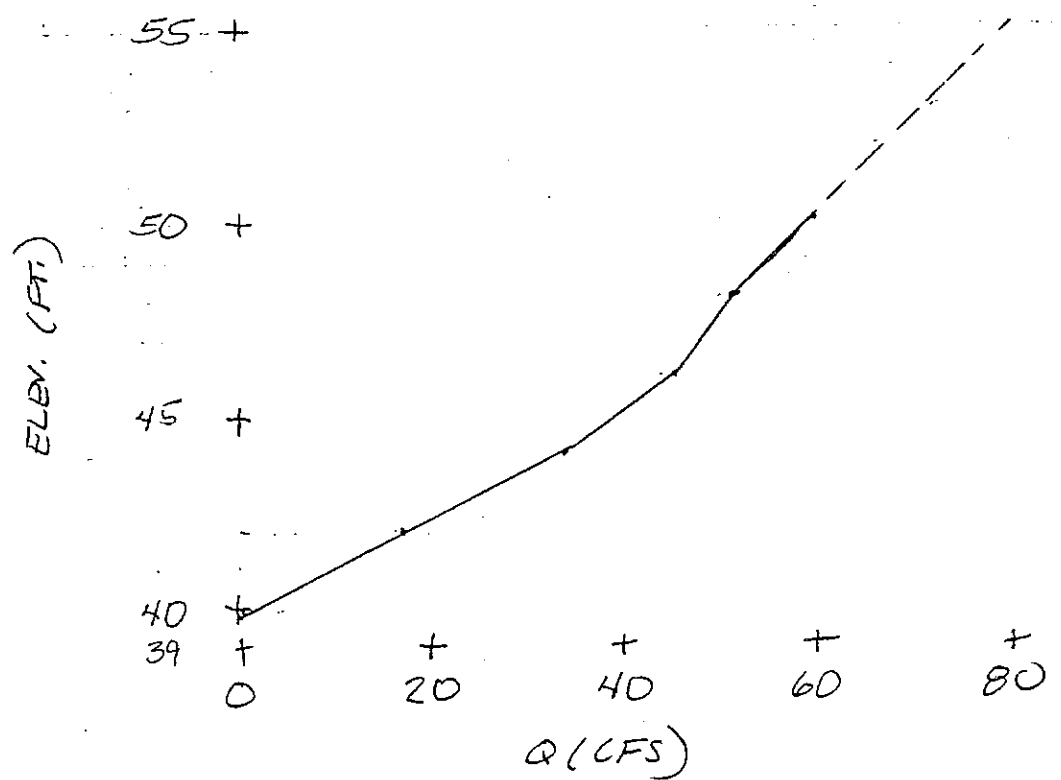
<u>ELEV.</u>	<u>Q</u>
39.7	0
42.0	33
44.0	99
46.0	163
48.0	219
50.0	259

Project CHEYENNE Mtn. RANCH REGIONAL DETENTION		Job No EW-1011	
Client GATES	By RM	Date 6/11/93	

27" RESTRICTOR

ELEV.	Q
39.7	0
42	17.2
44	34.0
46	45.0
48	51.
50	60
50.9	63
51.5	79
53.0	640

$(65 + 3.1(10))(.6)^{3/2}$   
 $(72 + 3.1(100))(1.5)^{3/2}$



REC'D JAN 11 1991 11:18

OLIVER E. WATTS, PE-LS  
 CONSULTING ENGINEER, INC.  
 614 ELKTON DRIVE  
 COLORADO SPRINGS, COLORADO 80907  
 719-593-0173

January 10, 1991

Bob Adamczyk  
 City Engineering Division  
 30 South Nevada Ave #403  
 P.O. Box 1575, Mail Code 435  
 Colorado Springs, CO 80901

SUBJECT: Mountain Oaks Filing No. 2  
 Drainage Design

Dear Bob

Enclosed for your review and approval are the original and two prints of drawing 90-1926-02, temporary detention modifications for the Broadmoor Oaks Subdivision, Filing No. 2.

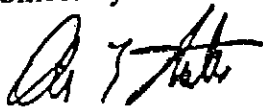
The detailed computations and schematic design for this plan were filed in the Mountain Oaks Subdivision Filing No. 2 drainage report on December 19, 1990. This design is based on a current as-built survey, and the storage curve may be compared with the one on page 5 of the computations in the report, as follows:

Elev.	Report			As-Built		
	PR -SI-	A -SF-	V -CF-	PR -SI-	A -SF-	V -CF-
39.73	0	0	0	0	0	0
						8
40			308.7	0.15	60	8
						106
41				0.38	152	114
						198
42	0.68		308.7	0.61	244	312
						332
43			1412	1.05	420	644
						570
44	2.85	1140	1721	1.80	720	1214
						1044
45			3680	3.42	1368	2258

						1724
46	6.35	2540	5401	5.20	2080	3982
						2482
47			6764	7.21	2884	6464
						3246
48	10.56	4224	12165	9.02	3608	9710
						4010
49			11180	11.03	4412	13720
						4888
50	17.3	6956	23385	13.41	5364? 153	24354

The storage required to provide the required detention, according to the drainage report, was 23,687 CF, which would interpolate at elevation 50.88. This is the elevation chosen for the overflow spillway put on the South abutment of the fill, and freeboard to elevation 51.5 is provided for a berm along the Westerly side of the roadway.

Sincerely



Oliver E. Watts  
Consulting Engineer

Encl

cc: Dave Sellon w/encl

Computations  
Mountain Oaks Subdivision No. 2

O.E.Watts  
November 30, 1990

STORAGE DATA: 60" CMP w/mfes, Inlet Control, Condition (1)

ELEV	STORAGE DATA			OUTLET CAPACITY									
	PR -SI-	A -SF-	V -CF-	60" CMP		36" CMP		30" CMP		27" CMP		18" CMP	
				HW/D	CFS	HW/D	CFS	HW/D	CFS	HW/D	CFS	HW/D	CFS
39.73	0	0	0	0	0	0	0	0	0	0	0	0	0
			308.7		33		23.2		19.8		17.2		10
42	0.68	272	308.7	0.45	33	0.76	23.2	0.91	19.8	1.01	17.2	1.51	10
			1412		66		29.8		20.2		16.8		6
44	2.85	1140	1721	0.85	99	1.42	53	1.71	40	1.90	34	2.85	16
			3680		64		20		14		11		5
46	6.35	2540	5401	1.25	163	2.09	73	2.51	54	2.79	45	4.18	21
			6764		56		17		9		6		4
48	10.56	4224	12165	1.65	219	2.76	90	3.31	63	3.68	51	5.51	25
			11180		40		11		9		9		
6250	17.3	6956	23345	2.05	259	3.42	101	4.11	72	4.56	60	6.85	

## STATE OF COLORADO

## DEPARTMENT OF HIGHWAYS

District II  
905 Erie - P.O. Box 536  
Pueblo, Colorado 81002  
(719) 546-5400



October 17, 1989

Mr. Robert F. Svejkovsky, P.E.  
Drexel Barrell  
740 Wooten Road  
Suite 108  
Colorado Springs, CO 80915

Dear Mr. Svejkovsky:

This letter is in response to your request for the Colorado Department of Highways to provide written agreement to accept historic flows to its culverts for your drainage study area west of State Highway 115 between Academy and O'Connell Boulevards.

It is Department policy that "Drainage to the state highway right-of-way shall not exceed the undeveloped historic flow. The use of controlled flow detention ponds shall be considered to control this flow from developed properties".

Subject to review of the drainage report, the Department, as stated above, will agree to accept the historic flow. To expedite the process and perhaps avoid revisions, it would be beneficial for CDOH to review the drainage report concurrent with the City of Colorado Springs.

If you have any questions or need additional information, please feel free to contact me at (719) 546-5405.

Sincerely,

A handwritten signature in cursive script that reads "Robert D. Torres".

Robert D. Torres  
District Design Engineer

RECEIVED  
10-18-89

**TR-20 PRINTOUT  
HISTORIC CONDITIONS**

6/11/93  
 HISTORIC CONDITION  
 DATAFILE:  
 EW1011 EX.TR

1

\*\*\*\*\*80-80 LIST OF INPUT DATA FOR TR-20 HYDROLOGY\*\*\*\*\*

JOB TR-20	FULLPRINT	SUMMARY				
TITLE	CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)					
TITLE	EXISTING CONDITIONS (6/11/93)					
5 RAINFL 7	0.2500					
8	0.0000	0.0005	0.0015	0.0030	0.0045	
8	0.0060	0.0080	0.0100	0.0120	0.0143	
8	0.0165	0.0188	0.0210	0.0233	0.0255	
8	0.0278	0.0320	0.0390	0.0460	0.0530	
8	0.0600	0.0750	0.1000	0.4000	0.7000	
8	0.7250	0.7500	0.7650	0.7800	0.7900	
8	0.8000	0.8100	0.8200	0.8250	0.8300	
8	0.8350	0.8400	0.8450	0.8500	0.8550	
8	0.8600	0.8638	0.8675	0.8713	0.8750	
8	0.8788	0.8825	0.8863	0.8900	0.8938	
8	0.8975	0.9013	0.9050	0.9083	0.9115	
8	0.9148	0.9180	0.9210	0.9240	0.9270	
8	0.9300	0.9325	0.9350	0.9375	0.9400	
8	0.9425	0.9450	0.9475	0.9500	0.9525	
8	0.9550	0.9575	0.9600	0.9625	0.9650	
8	0.9675	0.9700	0.9725	0.9750	0.9775	
8	0.9800	0.9813	0.9825	0.9838	0.9850	
8	0.9863	0.9875	0.9888	0.9900	0.9913	
8	0.9925	0.9938	0.9950	0.9963	0.9975	
8	0.9988	1.0000	1.0000	1.0000	1.0000	
9 ENDTBL						
5 RAINFL 8	0.08333					
8	0.000	0.020	0.057	0.139	0.289	
8	0.539	0.659	0.715	0.758	0.796	
8	0.828	0.860	0.892	0.924	0.956	
8	0.988	1.013	1.032	1.051	1.070	
8	1.089	1.108	1.127	1.144	1.157	
9 ENDTBL						
5 RAINFL 9	0.08333					
8	0.000	0.010	0.040	0.086	0.166	
8	0.306	0.556	0.696	0.776	0.838	
8	0.888	0.928	0.968	1.008	1.028	
8	1.048	1.060	1.072	1.084	1.096	
8	1.108	1.120	1.132	1.144	1.156	
9 ENDTBL						
6 RUNOFF 1 060	6 0.545	60.2	0.55	1 1	1 1	1
6 RUNOFF 1 020	6 0.078	80.1	0.26	1 1	1 1	1
6 RUNOFF 1 001	6 0.024	79.2	0.24	1 1	1 1	1
6 RUNOFF 1 200	6 0.027	77.8	0.25	1 1	1 1	1
6 RUNOFF 1 160	6 0.720	62.7	0.51	1 1	1 1	1
6 RUNOFF 1 164	5 1.049	67.4	0.63	1 1	1 1	1
6 ADDHYD 4 164	5 6 7			1 1	1 1	1

1

\*\*\*\*\*80-80 LIST OF INPUT DATA (CONTINUED)\*\*\*\*\*

6 RUNOFF 1 166	6 0.061	78.7	0.39	1 1	1 1	1
6 ADDHYD 4 166	6 7 5			1 1	1 1	1
6 RUNOFF 1 168	6 0.024	79.8	0.30	1 1	1 1	1
ENDATA						
7 INCREM 6	0.1					
7 COMPUT 7 060 168	0.0	3.0	1.0	7 2	01 10	
ENDCMP 1						
7 COMPUT 7 060 168	0.0	4.6	1.0	7 2	01 99	
ENDCMP 1						
ENDJOB 2						

0\*\*\*\*\*END OF 80-80 LIST\*\*\*\*\*

1



COMPUTER PROGRAM FOR PROJECT FORMULATION - HYDROLOGY USER NOTES

THE USERS MANUAL FOR THIS PROGRAM IS THE MAY 1982 DRAFT OF TR-20. CHANGES FROM THE 2/14/74 VERSION INCLUDE:

REACH ROUTING - THE MODIFIED ATT-KIN ROUTING PROCEDURE REPLACES THE CONVEX METHOD. INPUT DATA PREPARED FOR PREVIOUS PROGRAM VERSIONS USING CONVEX ROUTING COEFFICIENTS WILL NOT RUN ON THIS VERSION.

THE PREFERRED TYPE OF DATA ENTRY IS CROSS SECTION DATA REPRESENTATIVE OF A REACH. IT IS RECOMMENDED THAT THE OPTIONAL CROSS SECTION DISCHARGE-AREA PLOTS BE OBTAINED WHENEVER NEW CROSS SECTION DATA IS ENTERED. THE PLOTS SHOULD BE CHECKED FOR REASONABLENESS AND ADEQUACY OF INPUT DATA FOR THE COMPUTATION OF "M" VALUES USED IN THE ROUTING PROCEDURE.

GUIDELINES FOR DETERMINING OR ANALYZING REACH LENGTHS AND COEFFICIENTS (X,M) ARE AVAILABLE IN THE USERS MANUAL. SUMMARY TABLE 2 DISPLAYS REACH ROUTING RESULTS AND ROUTING PARAMETERS FOR COMPARISON AND CHECKING.

HYDROGRAPH GENERATION - THE PROCEDURE TO CALCULATE THE INTERNAL TIME INCREMENT AND PEAK TIME OF THE UNIT HYDROGRAPH HAVE BEEN IMPROVED. PEAK DISCHARGES AND TIMES MAY DIFFER FROM THE PREVIOUS VERSION. OUTPUT HYDROGRAPHS ARE STILL INTERPOLATED, PRINTED, AND ROUTED AT THE USER SELECTED MAIN TIME INCREMENT.

INTERMEDIATE PEAKS - METHOD ADDED TO PROVIDE DISCHARGES AT INTERMEDIATE POINTS WITHIN REACHES WITHOUT ROUTING.

OTHER - THIS VERSION CONTAINS SOME ADDITIONS TO THE INPUT AND NUMEROUS MODIFICATIONS TO THE OUTPUT. USER OPTIONS HAVE BEEN MODIFIED AND AUGMENTED ON THE JOB RECORD, RAINTABLES ADDED, ERROR AND WARNING MESSAGES EXPANDED, AND THE SUMMARY TABLES COMPLETELY REVISED. THE HOLDOUT OPTION IS NOT OPERATIONAL AT THIS TIME.

PROGRAM QUESTIONS OR PROBLEMS SHOULD BE DIRECTED TO HYDRAULIC ENGINEERS AT THE SCS NATIONAL TECHNICAL CENTERS:

- CHESTER, PA (NORTHEAST) -- 215-499-3933, FORT WORTH, TX (SOUTH) -- 334-5242 (FTS)
- LINCOLN, NB (MIDWEST) -- 541-5318 (FTS), PORTLAND, OR (WEST) -- 423-4099 (FTS)
- OR HYDROLOGY UNIT, ENGINEERING DIVISION, LANHAM, MD -- 436-7383 (FTS).

PROGRAM CHANGES SINCE MAY 1982:

- 12/17/82 - CORRECT PEAK RATE FACTOR FOR USER ENTERED DIMHYD  
CORRECT REACH ROUTING PEAK TRAVEL TIME PRINTED WITH FULLPRINT OPTION
- 5/02/83 - CORRECT COMPUTATIONS FOR ---
  - 1. DIVISION OF BASEFLOW IN DIVERT OPERATION
  - 2. HYDROGRAPH VOLUME SPLIT BETWEEN BASEFLOW AND ABOVE BASEFLOW
  - 3. CROSS SECTION DATA PLOTTING POSITION
  - 4. INTERMEDIATE PEAK WHEN "FROM" AREA IS LARGER THAN "THRU" AREA
  - 5. STORAGE ROUTED REACH TRAVEL TIME FOR MULTYPEAK HYDROGRAPH
  - 6. ORDERING "FLOW-FREQ" FILE FROM SUMMARY TABLE #3 DATA
  - 7. BASEFLOW ENTERED WITH READHYD
  - 8. LOW FLOW SPLIT DURING DIVERT PROCEDURE #2 WHEN SECTION RATINGS START AT DIFFERENT ELEVATIONS
- ENHANCEMENTS ---
  - 1. REPLACE USER MANUAL ERROR CODES (PAGE 4-9 TO 4-11) WITH MESSAGES
  - 2. LABEL OUTPUT HYDROGRAPH FILES WITH CROSS SECTION/STRUCTURE, ALTERNATE AND STORM NO'S
- 09/01/83 - CORRECT INPUT AND OUTPUT ERRORS FOR INTERMEDIATE PEAKS  
CORRECT COMBINATION OF RATING TABLES FOR DIVERT  
CHECK REACH ROUTING PARAMETERS FOR ACCEPTABLE LIMITS  
ELIMINATE MINIMUM REACH TRAVEL TIME WHEN ATT-KIN COEFFICIENT EQUALS ONE

1

CUMULATIVE RAINFALL TABLE 7 TIME INCREMENT\* .25

8	.0000	.0005	.0015	.0030	.0045
8	.0060	.0080	.0100	.0120	.0143
8	.0165	.0188	.0210	.0233	.0255
8	.0278	.0320	.0390	.0460	.0530
8	.0600	.0750	.1000	.1400	.2000
8	.2250	.2500	.2650	.2800	.2900
8	.3000	.3100	.3200	.3250	.3300
8	.3350	.3400	.3450	.3500	.3550
8	.3600	.3638	.3675	.3713	.3750
8	.3788	.3825	.3863	.3900	.3938
8	.3975	.4013	.4050	.4083	.4115

8	.9148	.9180	.9210	.9240	.9270
8	.9300	.9325	.9350	.9375	.9400
8	.9425	.9450	.9475	.9500	.9525
8	.9550	.9575	.9600	.9625	.9650
8	.9675	.9700	.9725	.9750	.9775
8	.9800	.9813	.9825	.9838	.9850
8	.9863	.9875	.9888	.9900	.9913
8	.9925	.9938	.9950	.9963	.9975
8	.9988	1.0000	1.0000	1.0000	1.0000

9 ENDTBL

CUMULATIVE RAINFALL TABLE 8 TIME INCREMENT= .08

8	.0000	.0200	.0570	.1390	.2890
8	.5390	.6590	.7150	.7580	.7960
8	.8280	.8600	.8920	.9240	.9560
8	.9880	1.0130	1.0320	1.0510	1.0700
8	1.0890	1.1080	1.1270	1.1440	1.1570

9 ENDTBL

CUMULATIVE RAINFALL TABLE 9 TIME INCREMENT= .08

8	.0000	.0100	.0400	.0860	.1660
8	.3060	.5560	.6960	.7760	.8380
8	.8880	.9280	.9680	1.0080	1.0280
8	1.0480	1.0600	1.0720	1.0840	1.0960
8	1.1080	1.1200	1.1320	1.1440	1.1560

9 ENDTBL

1

TR20 XEQ CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011) JOB 1 PASS  
REV 09/01/83 EXISTING CONDITIONS (6/11/93) PAGE

STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 60	DATA FIELD VALUES =	.5450	RECORD ID	60.2000	.5500
OUTPUT HYDROGRAPH = 6						
OUTPUT OPTIONS IN EFFECT	PEAK HYD VOL SUM					
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 20	DATA FIELD VALUES =	.0780	RECORD ID	80.1000	.2600
OUTPUT HYDROGRAPH = 6						
OUTPUT OPTIONS IN EFFECT	PEAK HYD VOL SUM					
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 1	DATA FIELD VALUES =	.0240	RECORD ID	79.2000	.2400
OUTPUT HYDROGRAPH = 6						
OUTPUT OPTIONS IN EFFECT	PEAK HYD VOL SUM					
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 200	DATA FIELD VALUES =	.0270	RECORD ID	77.8000	.2500
OUTPUT HYDROGRAPH = 6						
OUTPUT OPTIONS IN EFFECT	PEAK HYD VOL SUM					
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 160	DATA FIELD VALUES =	.7200	RECORD ID	62.7000	.5100
OUTPUT HYDROGRAPH = 6						
OUTPUT OPTIONS IN EFFECT	PEAK HYD VOL SUM					
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 164	DATA FIELD VALUES =	1.0490	RECORD ID	67.4000	.6300
OUTPUT HYDROGRAPH = 5						
OUTPUT OPTIONS IN EFFECT	PEAK HYD VOL SUM					
STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 164	DATA FIELD VALUES =	.0000	RECORD ID	.0000	.0000
INPUT HYDROGRAPHS = 5,6	OUTPUT HYDROGRAPH = 7					
OUTPUT OPTIONS IN EFFECT	PEAK HYD VOL SUM					
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 166	DATA FIELD VALUES =	.0610	RECORD ID	78.7000	.3900
OUTPUT HYDROGRAPH = 6						
OUTPUT OPTIONS IN EFFECT	PEAK HYD VOL SUM					
STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 166	DATA FIELD VALUES =	.0000	RECORD ID	.0000	.0000
INPUT HYDROGRAPHS = 6,7	OUTPUT HYDROGRAPH = 5					
OUTPUT OPTIONS IN EFFECT	PEAK HYD VOL SUM					
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 168	DATA FIELD VALUES =	.0240	RECORD ID	79.8000	.3000
OUTPUT HYDROGRAPH = 6						
OUTPUT OPTIONS IN EFFECT	PEAK HYD VOL SUM					

1

EXECUTIVE CONTROL OPERATION INCREM

RECORD ID

MAIN TIME INCREMENT = .10 HOURS

EXECUTIVE CONTROL OPERATION COMPUT

RECORD ID

FROM XSECTION 60

TO XSECTION 168

STARTING TIME = .00 RAIN DEPTH = 3.00 RAIN DURATION= 1.00 RAIN TABLE NO.= 7 ANT. MOIST. COND= 2  
ALTERNATE NO.= 1 STORM NO.=10 MAIN TIME INCREMENT = .10 HOURS

OPERATION RUNOFF CROSS SECTION 60

OUTPUT HYDROGRAPH= 6

AREA= .55 SQ MI INPUT RUNOFF CURVE= 60. TIME OF CONCENTRATION= .55 HOURS

INTERNAL HYDROGRAPH TIME INCREMENT= .0733 HOURS

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.30	62.13	(RUNOFF)
9.99	6.10	(RUNOFF)
12.98	4.98	(RUNOFF)
19.94	3.71	(RUNOFF)
23.91	1.92	(RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .10 HOURS	DRAINAGE AREA = .55 SQ.MI.
5.00	DISCHG .00 .00 .00 .00 .00 .00 .00 .00 .00 .10 2.85		
6.00	DISCHG 13.89 35.47 55.46 62.12 56.29 45.65 36.69 31.12 26.49 22.80		
7.00	DISCHG 20.13 18.23 16.69 15.17 13.81 12.76 12.03 11.56 11.34 11.26		
8.00	DISCHG 11.23 11.07 10.54 9.56 8.47 7.52 6.90 6.52 6.28 6.14		
9.00	DISCHG 6.05 6.01 5.99 5.98 5.99 6.00 6.02 6.03 6.06 6.08		
10.00	DISCHG 6.10 6.07 5.94 5.70 5.41 5.16 4.99 4.88 4.83 4.80		
11.00	DISCHG 4.78 4.76 4.76 4.77 4.79 4.80 4.80 4.80 4.82 4.84		
12.00	DISCHG 4.85 4.86 4.87 4.89 4.91 4.92 4.92 4.93 4.95 4.97		
13.00	DISCHG 4.98 4.96 4.90 4.79 4.68 4.58 4.50 4.46 4.44 4.44		
14.00	DISCHG 4.43 4.41 4.37 4.31 4.25 4.21 4.18 4.16 4.16 4.15		
15.00	DISCHG 4.15 4.14 4.07 3.95 3.82 3.71 3.63 3.59 3.56 3.54		
16.00	DISCHG 3.53 3.53 3.53 3.53 3.54 3.54 3.54 3.55 3.55 3.56		
17.00	DISCHG 3.56 3.57 3.57 3.58 3.58 3.59 3.59 3.60 3.60 3.61		
18.00	DISCHG 3.62 3.62 3.63 3.63 3.64 3.64 3.65 3.65 3.66 3.66		
19.00	DISCHG 3.67 3.67 3.68 3.68 3.69 3.69 3.70 3.70 3.71 3.71		
20.00	DISCHG 3.71 3.66 3.48 3.16 2.80 2.48 2.25 2.11 2.03 1.98		
21.00	DISCHG 1.95 1.91 1.89 1.89 1.90 1.89 1.88 1.87 1.87 1.90		
22.00	DISCHG 1.89 1.88 1.88 1.89 1.90 1.90 1.89 1.89 1.90 1.91		
23.00	DISCHG 1.91 1.90 1.89 1.90 1.92 1.91 1.90 1.90 1.91 1.92		
24.00	DISCHG 1.91 1.84 1.64 1.29 .91 .60 .38 .24 .15 .10		
25.00	DISCHG .06 .04 .02 .01 .01 .00 .00 .00 .00 .00		

RUNOFF VOLUME ABOVE BASEFLOW = .34 WATERSHED INCHES, 119.32 CFS-HRS, 9.86 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION RUNOFF CROSS SECTION 20

OUTPUT HYDROGRAPH= 6

AREA= .08 SQ MI INPUT RUNOFF CURVE= 80. TIME OF CONCENTRATION= .26 HOURS

1

INTERNAL HYDROGRAPH TIME INCREMENT= .0347 HOURS

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.06	83.32	(RUNOFF)
7.95	4.16	(RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .10 HOURS	DRAINAGE AREA = .08 SQ.MI.
5.00	DISCHG .00 .00 .00 .00 .00 .00 .33 7.30 28.25 54.49		
6.00	DISCHG 77.62 80.21 48.37 24.75 15.62 12.03 10.06 7.96 6.67 6.25		
7.00	DISCHG 6.11 5.77 4.95 4.40 4.20 4.13 4.11 4.11 4.11 4.12		
8.00	DISCHG 4.13 3.82 3.00 2.44 2.22 2.14 2.10 2.09 2.09 2.09		
9.00	DISCHG 2.10 2.10 2.10 2.10 2.11 2.11 2.11 2.11 2.12 2.12		

10.00	DISCHG	2.12	2.04	1.84	1.70	1.64	1.60	1.59	1.61	1.61	1.61
11.00	DISCHG	1.59	1.59	1.61	1.62	1.61	1.60	1.60	1.62	1.63	1.62
12.00	DISCHG	1.61	1.61	1.62	1.63	1.63	1.61	1.61	1.63	1.64	1.63
13.00	DISCHG	1.62	1.59	1.51	1.47	1.43	1.41	1.41	1.42	1.43	1.42
14.00	DISCHG	1.41	1.39	1.35	1.33	1.32	1.32	1.32	1.32	1.32	1.32
15.00	DISCHG	1.32	1.29	1.20	1.14	1.12	1.11	1.10	1.10	1.10	1.10
16.00	DISCHG	1.10	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
17.00	DISCHG	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
18.00	DISCHG	1.11	1.12	1.12	1.12	1.12	1.12	1.12	1.12	1.12	1.12
19.00	DISCHG	1.12	1.12	1.12	1.12	1.12	1.12	1.12	1.12	1.12	1.12
20.00	DISCHG	1.12	1.04	.82	.68	.61	.57	.56	.57	.58	.57
21.00	DISCHG	.55	.55	.57	.58	.57	.55	.55	.57	.58	.57
22.00	DISCHG	.55	.55	.57	.58	.57	.55	.55	.57	.58	.57
23.00	DISCHG	.56	.55	.57	.58	.57	.56	.56	.57	.58	.57
24.00	DISCHG	.55	.46	.24	.09	.04	.01	.01	.00		

RUNOFF VOLUME ABOVE BASEFLOW = 1.26 WATERSHED INCHES, 63.36 CFS-HRS, 5.24 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION RUNOFF CROSS SECTION 1

OUTPUT HYDROGRAPH= 6

AREA= .02 SQ MI INPUT RUNOFF CURVE= 79. TIME OF CONCENTRATION= .24 HOURS

INTERNAL HYDROGRAPH TIME INCREMENT= .0320 HOURS

PEAK TIME (HRS)		PEAK DISCHARGE (CFS)				PEAK ELEVATION (FEET)							
6.05		24.34				(RUNOFF)							
TIME (HRS)	FIRST HYDROGRAPH POINT =	.00 HOURS				TIME INCREMENT =			.10 HOURS			DRAINAGE AREA =	.02 SQ. MI.
5.00	DISCHG	.00	.00	.00	.00	.00	.00	.05	2.10	8.68	16.69		
6.00	DISCHG	23.58	23.30	12.97	6.48	4.18	3.37	2.87	2.25	1.94	1.84		
7.00	DISCHG	1.81	1.70	1.44	1.29	1.24	1.23	1.22	1.23	1.23	1.23		
8.00	DISCHG	1.24	1.13	.86	.71	.65	.63	.63	.63	.63	.63		
9.00	DISCHG	.63	.63	.63	.63	.63	.63	.63	.63	.63	.63		
10.00	DISCHG	.63	.61	.54	.50	.49	.48	.48	.48	.48	.48		
11.00	DISCHG	.48	.48	.48	.49	.48	.48	.48	.49	.49	.48		
12.00	DISCHG	.48	.48	.49	.49	.49	.48	.48	.49	.49	.49		
13.00	DISCHG	.48	.47	.45	.44	.43	.42	.42	.43	.43	.43		
14.00	DISCHG	.42	.42	.40	.40	.40	.40	.40	.40	.40	.40		

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TR20 XEQ

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CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
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JOB 1 PASS 1  
PAGE 6

15.00	DISCHG	.40	.38	.36	.34	.33	.33	.33	.33	.33	.33
16.00	DISCHG	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33
17.00	DISCHG	.33	.33	.33	.33	.33	.33	.33	.33	.33	.33
18.00	DISCHG	.33	.34	.34	.34	.34	.34	.34	.34	.34	.34
19.00	DISCHG	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34
20.00	DISCHG	.34	.31	.24	.20	.18	.17	.17	.17	.17	.17
21.00	DISCHG	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17
22.00	DISCHG	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17
23.00	DISCHG	.17	.17	.17	.17	.17	.17	.17	.17	.17	.17
24.00	DISCHG	.17	.14	.06	.02	.01	.00				

RUNOFF VOLUME ABOVE BASEFLOW = 1.20 WATERSHED INCHES, 18.60 CFS-HRS, 1.54 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION RUNOFF CROSS SECTION 200

OUTPUT HYDROGRAPH= 6

AREA= .03 SQ MI INPUT RUNOFF CURVE= 78. TIME OF CONCENTRATION= .25 HOURS

INTERNAL HYDROGRAPH TIME INCREMENT= .0333 HOURS

PEAK TIME (HRS)		PEAK DISCHARGE (CFS)				PEAK ELEVATION (FEET)							
6.06		25.76				(RUNOFF)							
TIME (HRS)	FIRST HYDROGRAPH POINT =	.00 HOURS				TIME INCREMENT =			.10 HOURS			DRAINAGE AREA =	.03 SQ. MI.
5.00	DISCHG	.00	.00	.00	.00	.00	.00	.02	1.49	7.57	16.04		
6.00	DISCHG	23.85	24.75	14.25	7.19	4.64	3.68	3.13	2.46	2.09	1.98		
7.00	DISCHG	1.95	1.83	1.56	1.39	1.34	1.32	1.31	1.31	1.32	1.32		
8.00	DISCHG	1.33	1.22	.94	.77	.71	.68	.67	.67	.67	.67		
9.00	DISCHG	.67	.67	.68	.68	.68	.68	.68	.68	.68	.68		
10.00	DISCHG	.68	.66	.59	.55	.53	.52	.51	.52	.52	.52		
11.00	DISCHG	.51	.51	.52	.52	.52	.52	.52	.52	.53	.52		
12.00	DISCHG	.52	.52	.53	.53	.53	.52	.52	.53	.53	.53		
13.00	DISCHG	.52	.51	.49	.47	.46	.46	.46	.46	.46	.46		
14.00	DISCHG	.46	.45	.44	.43	.43	.43	.43	.43	.43	.43		
15.00	DISCHG	.43	.42	.39	.37	.36	.36	.36	.36	.36	.36		
16.00	DISCHG	.36	.36	.36	.36	.36	.36	.36	.36	.36	.36		

17.00	DISCHG	.36	.36	.36	.36	.36	.36	.36	.36	.36	.36
18.00	DISCHG	.36	.36	.36	.36	.36	.36	.36	.36	.36	.36
19.00	DISCHG	.36	.36	.36	.36	.36	.37	.37	.37	.37	.37
20.00	DISCHG	.37	.34	.26	.22	.20	.18	.18	.19	.19	.18
21.00	DISCHG	.18	.18	.19	.19	.18	.18	.18	.19	.19	.19
22.00	DISCHG	.18	.18	.19	.19	.19	.18	.18	.19	.19	.19
23.00	DISCHG	.18	.18	.19	.19	.19	.18	.18	.19	.19	.19
24.00	DISCHG	.18	.15	.07	.03	.01	.00				

RUNOFF VOLUME ABOVE BASEFLOW = 1.12 WATERSHED INCHES, 19.49 CFS-HRS, 1.61 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION RUNOFF CROSS SECTION 160

OUTPUT HYDROGRAPH= 6

AREA= .72 SQ MI INPUT RUNOFF CURVE= 63. TIME OF CONCENTRATION= .51 HOURS

INTERNAL HYDROGRAPH TIME INCREMENT= .0680 HOURS

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TR20 XEQ  
REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
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JOB 1 PASS 1  
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PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.25	121.89	(RUNOFF)
9.98	9.43	(RUNOFF)
13.87	6.75	(RUNOFF)
19.95	5.59	(RUNOFF)
23.92	2.88	(RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .10 HOURS	DRAINAGE AREA = .72 SQ.MI.
5.00	DISCHG .00 .00 .00 .00 .00 .00 .00 .00 .00 .94 9.09		
6.00	DISCHG 38.40 85.46 119.22 119.55 99.87 76.36 60.46 50.17 41.74 35.55		
7.00	DISCHG 31.16 28.34 25.86 23.34 21.11 19.43 18.39 17.89 17.67 17.57		
8.00	DISCHG 17.53 17.25 16.22 14.52 12.73 11.29 10.44 9.91 9.61 9.43		
9.00	DISCHG 9.33 9.28 9.26 9.26 9.27 9.29 9.31 9.34 9.37 9.40		
10.00	DISCHG 9.43 9.37 9.14 8.68 8.21 7.83 7.58 7.44 7.38 7.36		
11.00	DISCHG 7.33 7.30 7.30 7.33 7.35 7.36 7.35 7.36 7.40 7.43		
12.00	DISCHG 7.44 7.43 7.45 7.48 7.51 7.52 7.52 7.53 7.56 7.59		
13.00	DISCHG 7.60 7.56 7.45 7.27 7.09 6.93 6.81 6.76 6.75 6.75		
14.00	DISCHG 6.74 6.70 6.62 6.53 6.43 6.37 6.33 6.31 6.30 6.30		
15.00	DISCHG 6.30 6.27 6.14 5.94 5.73 5.56 5.46 5.40 5.37 5.35		
16.00	DISCHG 5.34 5.34 5.34 5.34 5.35 5.35 5.36 5.37 5.37 5.38		
17.00	DISCHG 5.39 5.39 5.40 5.41 5.41 5.42 5.43 5.43 5.44 5.45		
18.00	DISCHG 5.45 5.46 5.47 5.47 5.48 5.49 5.49 5.50 5.51 5.51		
19.00	DISCHG 5.52 5.53 5.53 5.54 5.55 5.55 5.56 5.57 5.57 5.58		
20.00	DISCHG 5.58 5.49 5.18 4.62 4.05 3.58 3.26 3.08 2.99 2.94		
21.00	DISCHG 2.89 2.84 2.82 2.84 2.85 2.84 2.81 2.81 2.83 2.85		
22.00	DISCHG 2.84 2.82 2.82 2.84 2.86 2.85 2.83 2.82 2.85 2.87		
23.00	DISCHG 2.86 2.84 2.83 2.86 2.87 2.87 2.84 2.84 2.86 2.88		
24.00	DISCHG 2.87 2.74 2.38 1.79 1.20 .74 .46 .28 .17 .11		
25.00	DISCHG .06 .04 .02 .01 .01 .00		

RUNOFF VOLUME ABOVE BASEFLOW = .42 WATERSHED INCHES, 196.05 CFS-HRS, 16.20 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION RUNOFF CROSS SECTION 164

OUTPUT HYDROGRAPH= 5

AREA= 1.05 SQ MI INPUT RUNOFF CURVE= 67. TIME OF CONCENTRATION= .63 HOURS

INTERNAL HYDROGRAPH TIME INCREMENT= .0840 HOURS

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.31	259.82	(RUNOFF)
9.98	17.54	(RUNOFF)
12.99	13.91	(RUNOFF)
19.95	10.01	(RUNOFF)
23.91	5.11	(RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .10 HOURS	DRAINAGE AREA = 1.05 SQ.MI.
5.00	DISCHG .00 .00 .00 .00 .00 .00 .00 .19 4.86 28.12		
6.00	DISCHG 82.85 160.91 230.30 259.43 242.28 204.20 163.02 130.93 107.84 90.34		
7.00	DISCHG 77.02 67.02 59.31 52.86 47.35 42.95 39.66 37.39 35.82 34.70		

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TR20 XEQ  
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CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
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JOB 1 PASS 1  
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8.00	DISCHG	34.01	33.31	31.95	29.60	26.71	23.96	21.74	20.21	19.20	18.52
9.00	DISCHG	18.09	17.81	17.64	17.53	17.47	17.45	17.45	17.46	17.48	17.51
10.00	DISCHG	17.54	17.48	17.20	16.64	15.92	15.20	14.61	14.21	13.96	13.82
11.00	DISCHG	13.71	13.63	13.59	13.58	13.59	13.60	13.60	13.60	13.63	13.66
12.00	DISCHG	13.68	13.69	13.70	13.73	13.77	13.80	13.81	13.82	13.85	13.89
13.00	DISCHG	13.91	13.87	13.74	13.51	13.23	12.94	12.69	12.52	12.43	12.38
14.00	DISCHG	12.35	12.29	12.18	12.04	11.88	11.74	11.63	11.56	11.52	11.50
15.00	DISCHG	11.48	11.43	11.29	11.03	10.71	10.40	10.15	9.97	9.86	9.79
16.00	DISCHG	9.75	9.72	9.71	9.70	9.70	9.70	9.70	9.71	9.71	9.72
17.00	DISCHG	9.73	9.74	9.75	9.76	9.77	9.78	9.79	9.80	9.81	9.82
18.00	DISCHG	9.82	9.83	9.84	9.85	9.86	9.87	9.88	9.89	9.90	9.91
19.00	DISCHG	9.92	9.93	9.94	9.94	9.95	9.96	9.97	9.98	9.99	10.00
20.00	DISCHG	10.00	9.89	9.53	8.66	8.02	7.18	6.48	5.99	5.69	5.49
21.00	DISCHG	5.35	5.24	5.16	5.13	5.12	5.10	5.07	5.05	5.06	5.07
22.00	DISCHG	5.08	5.06	5.05	5.06	5.08	5.09	5.07	5.06	5.07	5.09
23.00	DISCHG	5.10	5.08	5.07	5.08	5.10	5.11	5.09	5.08	5.09	5.11
24.00	DISCHG	5.10	4.97	4.56	3.83	2.95	2.11	1.43	.96	.65	.44
25.00	DISCHG	.30	.20	.13	.09	.06	.04	.02	.01	.01	.00

RUNOFF VOLUME ABOVE BASEFLOW = .60 WATERSHED INCHES, 407.26 CFS-HRS, 33.66 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION ADDHYD CROSS SECTION 164  
INPUT HYDROGRAPHS= 5,6 OUTPUT HYDROGRAPH= 7

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.29	379.08	(NULL)
9.98	26.97	(NULL)
12.98	21.51	(NULL)
19.95	15.61	(NULL)
23.91	7.99	(NULL)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .10 HOURS	DRAINAGE AREA = 1.77 SQ.MI.
5.00	DISCHG .00 .00 .00 .00 .00 .00 .00 .19 5.80 37.20		
6.00	DISCHG 121.25 246.37 349.52 378.98 342.15 280.56 223.48 181.11 149.58 125.89		
7.00	DISCHG 108.18 95.37 85.17 76.20 68.47 62.37 58.05 55.29 53.48 52.27		
8.00	DISCHG 51.54 50.57 48.17 44.12 39.44 35.25 32.18 30.12 28.80 27.94		
9.00	DISCHG 27.41 27.09 26.90 26.79 26.74 26.74 26.76 26.80 26.85 26.91		
10.00	DISCHG 26.97 26.85 26.33 25.32 24.13 23.03 22.18 21.65 21.35 21.17		
11.00	DISCHG 21.04 20.94 20.89 20.91 20.95 20.96 20.95 20.97 21.02 21.09		
12.00	DISCHG 21.12 21.13 21.15 21.22 21.28 21.32 21.32 21.35 21.41 21.48		
13.00	DISCHG 21.51 21.43 21.19 20.78 20.31 19.86 19.50 19.28 19.18 19.13		
14.00	DISCHG 19.08 18.98 18.81 18.56 18.31 18.11 17.96 17.87 17.82 17.80		
15.00	DISCHG 17.78 17.70 17.44 16.97 16.44 15.96 15.61 15.38 15.24 15.15		
16.00	DISCHG 15.09 15.06 15.05 15.04 15.05 15.05 15.06 15.07 15.09 15.10		
17.00	DISCHG 15.12 15.13 15.15 15.17 15.18 15.20 15.21 15.23 15.25 15.26		
18.00	DISCHG 15.28 15.29 15.31 15.33 15.34 15.36 15.37 15.39 15.41 15.42		
19.00	DISCHG 15.44 15.45 15.47 15.49 15.50 15.52 15.53 15.55 15.56 15.58		
20.00	DISCHG 15.58 15.38 14.71 13.49 12.07 10.75 9.74 9.08 8.68 8.43		

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TR20 XEQ CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011) JOB 1 PASS 1  
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21.00	DISCHG	8.24	8.08	7.99	7.96	7.97	7.94	7.89	7.86	7.89	7.92
22.00	DISCHG	7.92	7.88	7.87	7.90	7.94	7.94	7.90	7.89	7.92	7.96
23.00	DISCHG	7.95	7.92	7.91	7.94	7.98	7.97	7.94	7.93	7.96	7.99
24.00	DISCHG	7.97	7.71	6.94	5.62	4.15	2.86	1.88	1.24	.83	.55
25.00	DISCHG	.36	.24	.15	.10	.06	.04	.02	.01	.01	.00

RUNOFF VOLUME ABOVE BASEFLOW = .53 WATERSHED INCHES, 603.30 CFS-HRS, 49.86 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION RUNOFF CROSS SECTION 166  
OUTPUT HYDROGRAPH= 6  
AREA= .06 SQ MI INPUT RUNOFF CURVE= 79. TIME OF CONCENTRATION= .39 HOURS  
INTERNAL HYDROGRAPH TIME INCREMENT= .0520 HOURS

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.12	49.61	(RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .10 HOURS	DRAINAGE AREA = .06 SQ.MI.
5.00	DISCHG .00 .00 .00 .00 .00 .00 .08 1.83 9.00 22.47		
6.00	DISCHG 38.64 49.25 45.18 31.99 20.44 14.27 10.87 8.51 6.80 5.70		
7.00	DISCHG 5.11 4.69 4.20 3.73 3.41 3.23 3.15 3.10 3.09 3.08		
8.00	DISCHG 3.08 2.99 2.66 2.24 1.92 1.75 1.66 1.61 1.59 1.58		
9.00	DISCHG 1.57 1.57 1.57 1.57 1.57 1.58 1.58 1.58 1.58 1.58		

10.00	DISCHG	1.58	1.56	1.48	1.38	1.30	1.25	1.22	1.21	1.21	1.21
11.00	DISCHG	1.20	1.20	1.20	1.21	1.21	1.21	1.20	1.21	1.21	1.22
12.00	DISCHG	1.21	1.21	1.21	1.22	1.22	1.22	1.21	1.22	1.22	1.23
13.00	DISCHG	1.22	1.21	1.18	1.14	1.11	1.08	1.07	1.07	1.07	1.07
14.00	DISCHG	1.07	1.06	1.04	1.02	1.00	1.00	.99	.99	.99	.99
15.00	DISCHG	.99	.98	.95	.90	.87	.85	.84	.84	.83	.83
16.00	DISCHG	.83	.83	.83	.83	.83	.83	.83	.83	.83	.83
17.00	DISCHG	.84	.84	.84	.84	.84	.84	.84	.84	.84	.84
18.00	DISCHG	.84	.84	.84	.84	.84	.84	.84	.84	.84	.84
19.00	DISCHG	.84	.84	.84	.84	.84	.85	.85	.85	.85	.85
20.00	DISCHG	.85	.82	.73	.62	.53	.48	.45	.44	.44	.43
21.00	DISCHG	.43	.42	.42	.43	.43	.42	.42	.42	.43	.43
22.00	DISCHG	.42	.42	.42	.43	.43	.43	.42	.42	.43	.43
23.00	DISCHG	.43	.42	.42	.43	.43	.43	.42	.42	.43	.43
24.00	DISCHG	.43	.39	.30	.19	.10	.05	.03	.01	.01	.00

RUNOFF VOLUME ABOVE BASEFLOW = 1.17 WATERSHED INCHES, 46.03 CFS-HRS, 3.80 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION ADDHYD CROSS SECTION 166  
 INPUT HYDROGRAPHS= 6,7 OUTPUT HYDROGRAPH= 5

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TR20 XEQ CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011) JOB 1 PASS 1  
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PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.28	412.96	(NULL)
9.98	28.56	(NULL)
12.97	22.73	(NULL)
19.95	16.46	(NULL)
23.91	8.43	(NULL)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .10 HOURS	DRAINAGE AREA = 1.83 SQ.MI.
5.00	DISCHG .00 .00 .00 .00 .00 .00 .08	2.02 14.80 59.68	
6.00	DISCHG 159.89 295.62 394.70 410.97 362.60 294.83 234.35	189.62 156.38 131.59	
7.00	DISCHG 113.29 100.06 89.37 79.94 71.87 65.61 61.20	58.39 56.57 55.35	
8.00	DISCHG 54.62 53.55 50.83 46.36 41.36 37.00 33.84	31.73 30.39 29.52	
9.00	DISCHG 28.99 28.66 28.47 28.36 28.32 28.31 28.34	28.38 28.43 28.50	
10.00	DISCHG 28.56 28.42 27.82 26.70 25.43 24.28 23.40	22.86 22.56 22.38	
11.00	DISCHG 22.24 22.14 22.09 22.12 22.16 22.17 22.15	22.17 22.24 22.31	
12.00	DISCHG 22.33 22.34 22.36 22.43 22.51 22.54 22.54	22.56 22.63 22.71	
13.00	DISCHG 22.73 22.64 22.37 21.92 21.42 20.95 20.57	20.34 20.25 20.21	
14.00	DISCHG 20.15 20.04 19.84 19.58 19.32 19.10 18.96	18.86 18.82 18.79	
15.00	DISCHG 18.77 18.68 18.38 17.87 17.31 16.81 16.45	16.21 16.07 15.98	
16.00	DISCHG 15.92 15.89 15.88 15.87 15.88 15.89 15.90	15.91 15.92 15.94	
17.00	DISCHG 15.95 15.97 15.99 16.00 16.02 16.04 16.05	16.07 16.09 16.10	
18.00	DISCHG 16.12 16.13 16.15 16.17 16.18 16.20 16.22	16.23 16.25 16.26	
19.00	DISCHG 16.28 16.30 16.31 16.33 16.35 16.36 16.38	16.39 16.41 16.43	
20.00	DISCHG 16.43 16.20 15.44 14.11 12.60 11.23 10.18	9.51 9.12 8.87	
21.00	DISCHG 8.67 8.50 8.41 8.39 8.40 8.36 8.31	8.29 8.32 8.35	
22.00	DISCHG 8.34 8.30 8.29 8.33 8.37 8.36 8.32	8.31 8.35 8.39	
23.00	DISCHG 8.38 8.34 8.33 8.37 8.41 8.40 8.36	8.35 8.39 8.43	
24.00	DISCHG 8.40 8.10 7.24 5.81 4.25 2.91 1.91	1.25 .83 .55	
25.00	DISCHG .36 .24 .15 .10 .06 .04 .02	.01 .01 .00	

RUNOFF VOLUME ABOVE BASEFLOW = .55 WATERSHED INCHES, 649.34 CFS-HRS, 53.66 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION RUNOFF CROSS SECTION 168  
 OUTPUT HYDROGRAPH= 6  
 AREA= .02 SQ MI INPUT RUNOFF CURVE= 80. TIME OF CONCENTRATION= .30 HOURS  
 INTERNAL HYDROGRAPH TIME INCREMENT= .0400 HOURS

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.08	23.92	(RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .10 HOURS	DRAINAGE AREA = .02 SQ.MI.
5.00	DISCHG .00 .00 .00 .00 .00 .00 .05	1.58 6.64 14.10	
6.00	DISCHG 21.31 23.65 16.86 9.37 5.76 4.22 3.40	2.70 2.20 1.97	
7.00	DISCHG 1.89 1.79 1.58 1.39 1.31 1.27 1.26	1.25 1.25 1.25	
8.00	DISCHG 1.26 1.19 .98 .79 .70 .67 .65	.64 .64 .64	
9.00	DISCHG .64 .64 .64 .64 .64 .64 .64	.64 .64 .65	
10.00	DISCHG .65 .63 .58 .53 .51 .49 .49	.49 .49 .49	
11.00	DISCHG .49 .49 .49 .49 .49 .49 .49	.49 .50 .49	

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12.00	DISCHG	.49	.49	.49	.50	.50	.49	.49	.50	.50	.50
13.00	DISCHG	.49	.49	.47	.45	.44	.43	.43	.43	.44	.44
14.00	DISCHG	.43	.43	.42	.41	.40	.40	.40	.40	.40	.40
15.00	DISCHG	.40	.40	.37	.35	.34	.34	.34	.34	.34	.34
16.00	DISCHG	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34
17.00	DISCHG	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34
18.00	DISCHG	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34
19.00	DISCHG	.34	.34	.34	.34	.34	.34	.34	.34	.34	.34
20.00	DISCHG	.34	.33	.27	.22	.19	.18	.17	.17	.18	.17
21.00	DISCHG	.17	.17	.17	.18	.17	.17	.17	.17	.18	.17
22.00	DISCHG	.17	.17	.17	.18	.17	.17	.17	.17	.18	.17
23.00	DISCHG	.17	.17	.17	.18	.17	.17	.17	.17	.18	.17
24.00	DISCHG	.17	.15	.09	.04	.02	.01	.00			

RUNOFF VOLUME ABOVE BASEFLOW = 1.24 WATERSHED INCHES, 19.16 CFS-HRS, 1.58 ACRE-FEET; BASEFLOW = .00 CFS

EXECUTIVE CONTROL OPERATION ENDCMP

RECORD ID

COMPUTATIONS COMPLETED FOR PASS 1

1

EXECUTIVE CONTROL OPERATION COMPUT

RECORD ID

FROM XSECTION 60

TO XSECTION 168

STARTING TIME = .00 RAIN DEPTH = 4.60 RAIN DURATION = 1.00 RAIN TABLE NO. = 7 ANT. MOIST. COND = 2  
ALTERNATE NO. = 1 STORM NO. = 99 MAIN TIME INCREMENT = .10 HOURS

OPERATION RUNOFF CROSS SECTION 60

OUTPUT HYDROGRAPH = 6

AREA = .55 SQ MI INPUT RUNOFF CURVE = 60. TIME OF CONCENTRATION = .55 HOURS  
INTERNAL HYDROGRAPH TIME INCREMENT = .0733 HOURS

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.25	286.75	(RUNOFF)
9.97	15.64	(RUNOFF)
12.96	12.32	(RUNOFF)
19.91	8.77	(RUNOFF)
23.91	4.48	(RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .10 HOURS	DRAINAGE AREA = .55 SQ.MI.
5.00	DISCHG .00 .00 .00 .00 .00 .00 .00 .00 .93 10.14 47.82		
6.00	DISCHG 123.75 218.70 279.59 278.35 231.88 176.85 134.46 108.27 87.97 72.68		
7.00	DISCHG 62.04 54.54 48.75 43.55 39.02 35.54 33.08 31.48 30.70 30.33		
8.00	DISCHG 30.13 29.58 28.05 25.37 22.42 19.87 18.18 17.13 16.45 16.06		
9.00	DISCHG 15.80 15.65 15.57 15.53 15.52 15.52 15.53 15.56 15.59 15.62		
10.00	DISCHG 15.64 15.55 15.20 14.55 13.81 13.15 12.68 12.39 12.24 12.16		
11.00	DISCHG 12.10 12.04 12.02 12.04 12.06 12.07 12.05 12.06 12.10 12.13		
12.00	DISCHG 12.15 12.14 12.15 12.18 12.22 12.24 12.23 12.24 12.27 12.31		
13.00	DISCHG 12.32 12.26 12.10 11.84 11.55 11.28 11.08 10.96 10.91 10.90		
14.00	DISCHG 10.87 10.81 10.70 10.54 10.40 10.27 10.20 10.15 10.13 10.12		
15.00	DISCHG 10.11 10.06 9.88 9.59 9.26 8.99 8.80 8.68 8.61 8.57		
16.00	DISCHG 8.54 8.53 8.52 8.52 8.52 8.53 8.53 8.54 8.55 8.55		
17.00	DISCHG 8.56 8.57 8.57 8.58 8.59 8.60 8.60 8.61 8.62 8.63		
18.00	DISCHG 8.63 8.64 8.65 8.65 8.66 8.67 8.68 8.68 8.69 8.70		
19.00	DISCHG 8.70 8.71 8.72 8.72 8.73 8.74 8.75 8.75 8.76 8.77		
20.00	DISCHG 8.76 8.64 8.20 7.46 6.61 5.85 5.29 4.96 4.78 4.67		
21.00	DISCHG 4.58 4.49 4.45 4.45 4.46 4.45 4.42 4.40 4.42 4.45		
22.00	DISCHG 4.44 4.42 4.41 4.43 4.46 4.45 4.43 4.42 4.44 4.47		
23.00	DISCHG 4.46 4.44 4.43 4.45 4.48 4.47 4.44 4.43 4.46 4.48		
24.00	DISCHG 4.46 4.29 3.82 3.00 2.13 1.39 .89 .57 .36 .23		
25.00	DISCHG .14 .09 .06 .03 .02 .01 .00		

RUNOFF VOLUME ABOVE BASEFLOW = 1.09 WATERSHED INCHES, 381.79 CFS-HRS, 31.55 ACRE-FEET; BASEFLOW = .00 CFS



OPERATION RUNOFF CROSS SECTION 20  
 OUTPUT HYDROGRAPH= 6  
 AREA= .08 SQ MI INPUT RUNOFF CURVE= 80. TIME OF CONCENTRATION= .26 HOURS  
 INTERNAL HYDROGRAPH TIME INCREMENT= .0347 HOURS

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TR20 XEQ  
 REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
 EXISTING CONDITIONS (6/11/93)

JOB 1 PASS 2  
 PAGE 13

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.04	168.77	(RUNOFF)
7.95	7.57	(RUNOFF)
23.80	1.02	(RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS				TIME INCREMENT = .10 HOURS				DRAINAGE AREA = .08 SQ.MI.		
5.00	DISCHG	.00	.00	.00	.00	.00	4.55	34.21	84.36	130.77	
6.00	DISCHG	165.79	161.43	95.36	48.20	29.89	22.66	14.75	12.32	11.52	
7.00	DISCHG	11.25	10.60	9.08	8.07	7.69	7.54	7.50	7.49	7.50	
8.00	DISCHG	7.50	6.94	5.44	4.42	4.02	3.87	3.81	3.79	3.78	
9.00	DISCHG	3.79	3.79	3.79	3.80	3.80	3.80	3.81	3.81	3.81	
10.00	DISCHG	3.81	3.67	3.31	3.06	2.94	2.87	2.86	2.88	2.90	
11.00	DISCHG	2.86	2.86	2.88	2.90	2.89	2.86	2.86	2.89	2.89	
12.00	DISCHG	2.87	2.87	2.90	2.92	2.90	2.88	2.88	2.90	2.92	
13.00	DISCHG	2.88	2.83	2.70	2.61	2.55	2.51	2.53	2.55	2.53	
14.00	DISCHG	2.51	2.47	2.40	2.36	2.34	2.34	2.34	2.34	2.34	
15.00	DISCHG	2.34	2.28	2.12	2.02	1.98	1.96	1.96	1.95	1.95	
16.00	DISCHG	1.95	1.95	1.96	1.96	1.96	1.96	1.96	1.96	1.96	
17.00	DISCHG	1.96	1.96	1.96	1.96	1.96	1.96	1.96	1.96	1.96	
18.00	DISCHG	1.96	1.96	1.97	1.97	1.97	1.97	1.97	1.97	1.97	
19.00	DISCHG	1.97	1.97	1.97	1.97	1.97	1.97	1.97	1.97	1.97	
20.00	DISCHG	1.97	1.83	1.45	1.19	1.06	.99	.98	1.00	1.01	
21.00	DISCHG	.97	.97	1.00	1.01	1.00	.97	.97	1.00	1.01	
22.00	DISCHG	.97	.97	1.00	1.01	1.00	.97	.97	1.00	1.01	
23.00	DISCHG	.97	.97	1.00	1.02	1.00	.97	.97	1.00	1.02	
24.00	DISCHG	.97	.81	.43	.16	.06	.02	.01	.00		

RUNOFF VOLUME ABOVE BASEFLOW = 2.56 WATERSHED INCHES, 128.91 CFS-HRS, 10.65 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION RUNOFF CROSS SECTION 1  
 OUTPUT HYDROGRAPH= 6  
 AREA= .02 SQ MI INPUT RUNOFF CURVE= 79. TIME OF CONCENTRATION= .24 HOURS  
 INTERNAL HYDROGRAPH TIME INCREMENT= .0320 HOURS

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.02	51.21	(RUNOFF)
7.95	2.29	(RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS				TIME INCREMENT = .10 HOURS				DRAINAGE AREA = .02 SQ.MI.		
5.00	DISCHG	.00	.00	.00	.00	.00	1.22	10.78	26.48	40.50	
6.00	DISCHG	50.79	47.34	25.83	12.72	8.05	6.39	5.40	4.22	3.63	
7.00	DISCHG	3.38	3.16	2.67	2.40	2.30	2.27	2.26	2.26	2.27	
8.00	DISCHG	2.27	2.07	1.57	1.29	1.20	1.16	1.15	1.14	1.14	
9.00	DISCHG	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	
10.00	DISCHG	1.15	1.10	.99	.92	.88	.87	.86	.87	.88	
11.00	DISCHG	.86	.87	.87	.88	.87	.87	.87	.88	.88	
12.00	DISCHG	.87	.87	.88	.88	.88	.87	.87	.88	.89	
13.00	DISCHG	.87	.85	.81	.79	.77	.76	.76	.77	.77	

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TR20 XEQ  
 REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
 EXISTING CONDITIONS (6/11/93)

JOB 1 PASS 2  
 PAGE 14

14.00	DISCHG	.76	.75	.73	.71	.71	.71	.71	.71	.71
15.00	DISCHG	.71	.69	.64	.61	.60	.59	.59	.59	.59
16.00	DISCHG	.59	.59	.59	.59	.59	.59	.59	.59	.59
17.00	DISCHG	.59	.59	.59	.59	.59	.60	.60	.60	.60
18.00	DISCHG	.60	.60	.60	.60	.60	.60	.60	.60	.60
19.00	DISCHG	.60	.60	.60	.60	.60	.60	.60	.60	.60
20.00	DISCHG	.60	.55	.42	.35	.32	.30	.30	.30	.31
21.00	DISCHG	.29	.29	.30	.31	.30	.29	.29	.30	.31
22.00	DISCHG	.29	.29	.30	.31	.30	.29	.29	.30	.31
23.00	DISCHG	.29	.30	.30	.31	.30	.29	.30	.30	.31

24.00 DISCHG .29 .24 .11 .04 .01 .00

RUNOFF VOLUME ABOVE BASEFLOW = 2.48 WATERSHED INCHES, 38.40 CFS-HRS, 3.17 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION RUNOFF CROSS SECTION 200

OUTPUT HYDROGRAPH= 6

AREA= .03 SQ MI INPUT RUNOFF CURVE= 78. TIME OF CONCENTRATION= .25 HOURS

INTERNAL HYDROGRAPH TIME INCREMENT= .0333 HOURS

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.04	54.47	(RUNOFF)
7.95	2.51	(RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT =	.00 HOURS	TIME INCREMENT =	.10 HOURS	DRAINAGE AREA =	.03 SQ.MI.
5.00	DISCHG	.00 .00 .00 .00	.00 .00 .00 .00	.87 9.39 25.61 41.25		
6.00	DISCHG	53.45 51.87 29.21 14.53	9.17 7.16 6.02 4.71	3.99 3.77 2.48		
7.00	DISCHG	3.70 3.48 2.95 2.64	2.52 2.49 2.47 2.47	2.47 2.47 2.48		
8.00	DISCHG	2.48 2.29 1.76 1.44	1.32 1.27 1.26 1.25	1.25 1.25 1.25		
9.00	DISCHG	1.25 1.26 1.26 1.26	1.26 1.26 1.26 1.26	1.26 1.26 1.26		
10.00	DISCHG	1.26 1.22 1.09 1.01	.97 .95 .95 .96	.96 .96 .96		
11.00	DISCHG	.95 .95 .96 .96	.96 .95 .95 .96	.96 .97 .96		
12.00	DISCHG	.95 .95 .96 .97	.96 .96 .96 .97	.97 .97 .97		
13.00	DISCHG	.96 .94 .89 .87	.85 .83 .83 .84	.85 .85 .84		
14.00	DISCHG	.83 .82 .80 .78	.78 .78 .78 .78	.78 .78 .78		
15.00	DISCHG	.78 .76 .70 .67	.66 .65 .65 .65	.65 .65 .65		
16.00	DISCHG	.65 .65 .65 .65	.65 .65 .65 .65	.65 .65 .65		
17.00	DISCHG	.65 .65 .65 .65	.65 .65 .65 .65	.65 .65 .65		
18.00	DISCHG	.66 .66 .66 .66	.66 .66 .66 .66	.66 .66 .66		
19.00	DISCHG	.66 .66 .66 .66	.66 .66 .66 .66	.66 .66 .66		
20.00	DISCHG	.66 .61 .47 .39	.35 .33 .33 .33	.33 .34 .33		
21.00	DISCHG	.32 .32 .33 .34	.33 .32 .32 .32	.33 .34 .33		
22.00	DISCHG	.32 .32 .33 .34	.33 .32 .32 .32	.33 .34 .33		
23.00	DISCHG	.32 .32 .33 .34	.33 .32 .32 .32	.33 .34 .33		
24.00	DISCHG	.32 .27 .13 .05	.02 .01 .01 .00			

RUNOFF VOLUME ABOVE BASEFLOW = 2.36 WATERSHED INCHES, 41.17 CFS-HRS, 3.40 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION RUNOFF CROSS SECTION 160

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TR20 XEQ  
REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
EXISTING CONDITIONS (6/11/93)

JOB 1 PASS 2  
PAGE 15

OUTPUT HYDROGRAPH= 6

AREA= .72 SQ MI INPUT RUNOFF CURVE= 63. TIME OF CONCENTRATION= .51 HOURS

INTERNAL HYDROGRAPH TIME INCREMENT= .0680 HOURS

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.21	480.52	(RUNOFF)
9.97	22.64	(RUNOFF)
12.95	17.73	(RUNOFF)
19.94	12.51	(RUNOFF)
23.91	6.39	(RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT =	.00 HOURS	TIME INCREMENT =	.10 HOURS	DRAINAGE AREA =	.72 SQ.MI.
5.00	DISCHG	.00 .00 .00 .00	.00 .00 .00 .00	.03 2.69 27.37 104.00		
6.00	DISCHG	246.41 403.44 479.32 437.10	342.71 251.07 189.99 151.22	121.22 100.24		
7.00	DISCHG	85.50 76.10 68.24 60.75	54.23 49.38 46.43 44.97	44.22 43.83		
8.00	DISCHG	43.58 42.76 40.09 35.81	31.33 27.73 25.59 24.25	23.47 22.98		
9.00	DISCHG	22.71 22.55 22.47 22.44	22.43 22.44 22.47 22.51	22.55 22.60		
10.00	DISCHG	22.63 22.47 21.87 20.77	19.62 18.69 18.06 17.73	17.56 17.48		
11.00	DISCHG	17.40 17.32 17.30 17.35	17.39 17.39 17.36 17.37	17.44 17.50		
12.00	DISCHG	17.50 17.47 17.49 17.55	17.61 17.61 17.59 17.60	17.66 17.72		
13.00	DISCHG	17.72 17.61 17.33 16.91	16.47 16.09 15.81 15.67	15.63 15.63		
14.00	DISCHG	15.59 15.48 15.30 15.07	14.85 14.68 14.59 14.53	14.51 14.49		
15.00	DISCHG	14.48 14.40 14.11 13.64	13.14 12.75 12.52 12.37	12.29 12.24		
16.00	DISCHG	12.21 12.20 12.20 12.20	12.20 12.21 12.21 12.22	12.23 12.24		
17.00	DISCHG	12.25 12.26 12.27 12.28	12.29 12.30 12.31 12.31	12.32 12.33		
18.00	DISCHG	12.34 12.35 12.36 12.37	12.38 12.39 12.40 12.40	12.41 12.42		
19.00	DISCHG	12.43 12.44 12.45 12.46	12.47 12.48 12.48 12.49	12.50 12.51		
20.00	DISCHG	12.51 12.30 11.59 10.35	9.06 8.01 7.29 6.89	6.69 6.57		
21.00	DISCHG	6.46 6.35 6.31 6.33	6.35 6.33 6.28 6.27	6.31 6.35		
22.00	DISCHG	6.33 6.29 6.28 6.32	6.36 6.34 6.30 6.29	6.33 6.37		
23.00	DISCHG	6.36 6.31 6.30 6.35	6.39 6.37 6.32 6.31	6.35 6.39		
24.00	DISCHG	6.37 6.08 5.28 3.98	2.66 1.65 1.01 .62	.38 .23		
25.00	DISCHG	.14 .08 .05 .03	.01 .01 .01 .00			

RUNOFF VOLUME ABOVE BASEFLOW = 1.24 WATERSHED INCHES, 576.81 CFS-HRS, 47.67 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION RUNOFF CROSS SECTION 164

OUTPUT HYDROGRAPH= 5

AREA= 1.05 SQ MI INPUT RUNOFF CURVE= 67. TIME OF CONCENTRATION= .63 HOURS

INTERNAL HYDROGRAPH TIME INCREMENT= .0840 HOURS

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.28	804.17	(RUNOFF)
9.97	38.18	(RUNOFF)
12.97	29.62	(RUNOFF)
19.93	20.67	(RUNOFF)
23.91	10.49	(RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT =	.00 HOURS	TIME INCREMENT =	.10 HOURS	DRAINAGE AREA =	1.05 SQ.MI.
5.00	DISCHG	.00	.00	.00	.63	10.10 53.54 174.16

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TR20 XEQ CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011) JOB 1 PASS 2  
 REV 09/01/83 EXISTING CONDITIONS (6/11/93) PAGE 16

6.00	DISCHG	373.71	600.52	766.29	801.16	711.46	578.37	449.37	351.80	282.34	230.99
7.00	DISCHG	192.71	164.38	142.90	125.48	111.05	99.70	91.19	85.15	80.87	77.88
8.00	DISCHG	76.04	74.29	71.10	65.76	59.24	53.06	48.08	44.62	42.32	40.77
9.00	DISCHG	39.77	39.12	38.69	38.42	38.25	38.16	38.12	38.10	38.11	38.14
10.00	DISCHG	38.17	38.00	37.35	36.11	34.52	32.93	31.62	30.73	30.18	29.84
11.00	DISCHG	29.59	29.41	29.29	29.25	29.26	29.25	29.22	29.21	29.24	29.30
12.00	DISCHG	29.33	29.33	29.33	29.38	29.44	29.48	29.48	29.48	29.53	29.59
13.00	DISCHG	29.62	29.53	29.23	28.72	28.10	27.47	26.92	26.55	26.35	26.24
14.00	DISCHG	26.14	26.00	25.77	25.44	25.10	24.79	24.55	24.39	24.29	24.23
15.00	DISCHG	24.18	24.07	23.77	23.20	22.52	21.86	21.32	20.95	20.71	20.55
16.00	DISCHG	20.45	20.38	20.34	20.32	20.31	20.30	20.30	20.31	20.31	20.32
17.00	DISCHG	20.33	20.34	20.36	20.37	20.38	20.39	20.40	20.42	20.43	20.44
18.00	DISCHG	20.45	20.46	20.48	20.49	20.50	20.51	20.52	20.53	20.55	20.56
19.00	DISCHG	20.57	20.58	20.59	20.60	20.62	20.63	20.64	20.65	20.66	20.67
20.00	DISCHG	20.67	20.44	19.69	18.30	16.56	14.81	13.36	12.37	11.74	11.33
21.00	DISCHG	11.03	10.80	10.64	10.57	10.54	10.51	10.45	10.40	10.41	10.44
22.00	DISCHG	10.44	10.41	10.39	10.41	10.45	10.46	10.43	10.40	10.42	10.46
23.00	DISCHG	10.47	10.44	10.42	10.44	10.47	10.48	10.45	10.43	10.45	10.49
24.00	DISCHG	10.46	10.19	9.35	7.84	6.05	4.34	2.93	1.96	1.34	.91
25.00	DISCHG	.61	.41	.27	.18	.12	.08	.05	.03	.01	.01
26.00	DISCHG	.00									

RUNOFF VOLUME ABOVE BASEFLOW = 1.56 WATERSHED INCHES, 1054.65 CFS-HRS, 87.16 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION ADDHYD CROSS SECTION 164

INPUT HYDROGRAPHS= 5,6 OUTPUT HYDROGRAPH= 7

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.25	1273.17	(NULL)
9.97	60.82	(NULL)
12.96	47.35	(NULL)
19.94	33.19	(NULL)
23.91	16.88	(NULL)

TIME (HRS)	FIRST HYDROGRAPH POINT =	.00 HOURS	TIME INCREMENT =	.10 HOURS	DRAINAGE AREA =	1.77 SQ.MI.
5.00	DISCHG	.00	.00	.00	.66	12.79 80.91 278.16
6.00	DISCHG	620.12	1003.96	1245.61	1238.26	1054.17 829.45 639.36 503.01 403.56 331.23
7.00	DISCHG	278.21	240.48	211.14	186.23	165.28 149.08 137.63 130.12 125.09 121.71
8.00	DISCHG	119.62	117.05	111.19	101.57	90.58 80.79 73.67 68.87 65.79 63.75
9.00	DISCHG	62.48	61.67	61.16	60.86	60.69 60.60 60.59 60.61 60.67 60.73
10.00	DISCHG	60.80	60.47	59.23	56.88	54.14 51.62 49.69 48.46 47.75 47.32
11.00	DISCHG	46.99	46.73	46.59	46.60	46.65 46.64 46.58 46.58 46.68 46.80
12.00	DISCHG	46.83	46.80	46.82	46.93	47.05 47.09 47.07 47.08 47.19 47.31
13.00	DISCHG	47.33	47.13	46.56	45.63	44.57 43.56 42.73 42.22 41.98 41.87
14.00	DISCHG	41.73	41.48	41.07	40.51	39.94 39.47 39.14 38.92 38.80 38.73
15.00	DISCHG	38.66	38.47	37.87	36.84	35.66 34.61 33.84 33.32 33.00 32.79
16.00	DISCHG	32.66	32.58	32.54	32.51	32.51 32.51 32.52 32.53 32.55 32.56
17.00	DISCHG	32.58	32.60	32.62	32.65	32.67 32.69 32.71 32.73 32.75 32.77

1

TR20 XEQ CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011) JOB 1 PASS 2  
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18.00	DISCHG	32.79	32.81	32.83	32.86	32.88	32.90	32.92	32.94	32.96	32.98
19.00	DISCHG	33.00	33.02	33.04	33.06	33.08	33.10	33.12	33.14	33.16	33.18
20.00	DISCHG	33.18	32.73	31.28	28.66	25.61	22.82	20.65	19.26	18.42	17.90
21.00	DISCHG	17.49	17.15	16.95	16.90	16.90	16.84	16.72	16.67	16.72	16.80
22.00	DISCHG	16.78	16.70	16.67	16.73	16.81	16.80	16.72	16.69	16.76	16.83
23.00	DISCHG	16.83	16.75	16.72	16.78	16.86	16.85	16.77	16.74	16.81	16.88
24.00	DISCHG	16.83	16.26	14.63	11.82	8.71	5.98	3.94	2.58	1.72	1.14
25.00	DISCHG	.75	.49	.32	.21	.13	.08	.05	.03	.01	.01
26.00	DISCHG	.00									

RUNOFF VOLUME ABOVE BASEFLOW = 1.43 WATERSHED INCHES, 1631.46 CFS-HRS, 134.82 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION RUNOFF CROSS SECTION 166

OUTPUT HYDROGRAPH= 6

AREA= .06 SQ MI INPUT RUNOFF CURVE= 79. TIME OF CONCENTRATION= .39 HOURS

INTERNAL HYDROGRAPH TIME INCREMENT= .0520 HOURS

PEAK TIME (HRS) 6.10 PEAK DISCHARGE (CFS) 108.38 PEAK ELEVATION (FEET) (RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .10 HOURS	DRAINAGE AREA = .06 SQ.MI.								
5.00	DISCHG	.00	.00	.00	.00	.00	.00	1.25	10.23	32.44	63.04
6.00	DISCHG	92.80	108.36	95.30	66.10	41.68	28.62	21.43	16.56	13.07	10.86
7.00	DISCHG	9.65	8.82	7.88	6.98	6.36	6.03	5.86	5.77	5.74	5.72
8.00	DISCHG	5.71	5.53	4.92	4.14	3.55	3.23	3.06	2.98	2.93	2.91
9.00	DISCHG	2.89	2.89	2.89	2.89	2.89	2.89	2.90	2.90	2.90	2.90
10.00	DISCHG	2.90	2.86	2.71	2.52	2.37	2.28	2.23	2.21	2.21	2.21
11.00	DISCHG	2.19	2.18	2.19	2.20	2.20	2.20	2.19	2.20	2.21	2.21
12.00	DISCHG	2.20	2.19	2.20	2.21	2.22	2.21	2.20	2.21	2.22	2.22
13.00	DISCHG	2.21	2.19	2.13	2.06	2.00	1.96	1.93	1.93	1.94	1.94
14.00	DISCHG	1.93	1.91	1.87	1.84	1.81	1.80	1.79	1.79	1.79	1.79
15.00	DISCHG	1.79	1.77	1.70	1.62	1.56	1.53	1.51	1.50	1.50	1.50
16.00	DISCHG	1.49	1.49	1.49	1.49	1.49	1.50	1.50	1.50	1.50	1.50
17.00	DISCHG	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50
18.00	DISCHG	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.50	1.51	1.51
19.00	DISCHG	1.51	1.51	1.51	1.51	1.51	1.51	1.51	1.51	1.51	1.51
20.00	DISCHG	1.51	1.46	1.31	1.11	.95	.85	.80	.78	.78	.77
21.00	DISCHG	.76	.75	.75	.76	.77	.76	.75	.75	.76	.77
22.00	DISCHG	.76	.75	.75	.76	.77	.76	.75	.75	.76	.77
23.00	DISCHG	.76	.75	.75	.77	.77	.76	.75	.75	.77	.77
24.00	DISCHG	.76	.70	.53	.33	.18	.09	.05	.03	.01	.01
25.00	DISCHG	.00									

RUNOFF VOLUME ABOVE BASEFLOW = 2.43 WATERSHED INCHES, 95.76 CFS-HRS, 7.91 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION ADDHYD CROSS SECTION 166

INPUT HYDROGRAPHS= 6,7 OUTPUT HYDROGRAPH= 5

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TR20 REQ  
REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
EXISTING CONDITIONS (6/11/93)

JOB 1 PASS 2  
PAGE 18

PEAK TIME (HRS) 6.24 PEAK DISCHARGE (CFS) 1358.29 PEAK ELEVATION (FEET) (NULL)  
 9.97 63.73 (NULL)  
 12.96 49.57 (NULL)  
 19.93 34.70 (NULL)  
 23.91 17.65 (NULL)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .10 HOURS	DRAINAGE AREA = 1.83 SQ.MI.								
5.00	DISCHG	.00	.00	.00	.00	.00	.00	1.90	23.02	113.35	341.20
6.00	DISCHG	712.92	1112.31	1340.91	1304.36	1095.85	858.07	660.80	519.57	416.63	342.08
7.00	DISCHG	287.86	249.29	219.02	193.21	171.64	155.12	143.49	135.89	130.82	127.43
8.00	DISCHG	125.33	122.58	116.11	105.70	94.12	84.02	76.74	71.85	68.72	66.66
9.00	DISCHG	65.37	64.56	64.05	63.75	63.58	63.50	63.48	63.51	63.57	63.63
10.00	DISCHG	63.70	63.33	61.94	59.40	56.51	53.89	51.91	50.67	49.96	49.53
11.00	DISCHG	49.19	48.92	48.78	48.80	48.85	48.84	48.77	48.78	48.89	49.01
12.00	DISCHG	49.03	49.00	49.02	49.15	49.27	49.30	49.27	49.29	49.41	49.53
13.00	DISCHG	49.55	49.32	48.69	47.69	46.57	45.52	44.66	44.15	43.92	43.80
14.00	DISCHG	43.66	43.39	42.95	42.35	41.76	41.27	40.93	40.71	40.59	40.51
15.00	DISCHG	40.45	40.23	39.58	38.46	37.22	36.14	35.35	34.82	34.50	34.29
16.00	DISCHG	34.16	34.08	34.03	34.01	34.00	34.00	34.01	34.03	34.04	34.06
17.00	DISCHG	34.08	34.10	34.12	34.14	34.17	34.19	34.21	34.23	34.25	34.27

18.00	DISCHG	34.30	34.32	34.34	34.36	34.38	34.40	34.42	34.44	34.46	34.49
19.00	DISCHG	34.51	34.53	34.55	34.57	34.59	34.61	34.63	34.65	34.67	34.69
20.00	DISCHG	34.69	34.19	32.59	29.77	26.56	23.67	21.45	20.04	19.20	18.67
21.00	DISCHG	18.25	17.90	17.70	17.66	17.66	17.59	17.47	17.42	17.49	17.56
22.00	DISCHG	17.53	17.44	17.42	17.50	17.58	17.56	17.47	17.44	17.52	17.60
23.00	DISCHG	17.58	17.50	17.47	17.55	17.63	17.61	17.52	17.50	17.57	17.65
24.00	DISCHG	17.59	16.96	15.16	12.15	8.89	6.07	3.99	2.61	1.73	1.15
25.00	DISCHG	.75	.49	.32	.21	.13	.08	.05	.03	.01	.01
26.00	DISCHG	.00									

RUNOFF VOLUME ABOVE BASEFLOW = 1.46 WATERSHED INCHES, 1727.22 CFS-HRS, 142.74 ACRE-FEET; BASEFLOW = .00 CFS

OPERATION RUNOFF CROSS SECTION 168

OUTPUT HYDROGRAPH= 6  
 AREA= .02 SQ MI INPUT RUNOFF CURVE= 80. TIME OF CONCENTRATION= .30 HOURS  
 INTERNAL HYDROGRAPH TIME INCREMENT= .0400 HOURS

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.06	50.03	(RUNOFF)
7.95	2.31	(RUNOFF)

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .10 HOURS	DRAINAGE AREA = .02 SQ.MI.	
5.00	DISCHG .00 .00 .00 .00 .00 .00 .87	7.82	21.20	35.38
6.00	DISCHG 46.97 48.74 33.81 18.55 11.22 8.08 6.42	5.05	4.09	3.66
7.00	DISCHG 3.49 3.31 2.91 2.56 2.40 2.33 2.30	2.30	2.29	2.29
8.00	DISCHG 2.30 2.17 1.78 1.44 1.28 1.21 1.18	1.17	1.16	1.16
9.00	DISCHG 1.16 1.16 1.16 1.16 1.16 1.16 1.16	1.16	1.17	1.17

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TR20 XEQ CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011) JOB 1 PASS 2  
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10.00	DISCHG	1.17	1.14	1.04	.96	.91	.89	.88	.88	.89	.88
11.00	DISCHG	.88	.87	.88	.89	.88	.88	.88	.88	.89	.89
12.00	DISCHG	.88	.88	.89	.89	.89	.88	.88	.89	.89	.89
13.00	DISCHG	.88	.87	.84	.81	.79	.77	.77	.77	.78	.78
14.00	DISCHG	.77	.76	.74	.73	.72	.72	.72	.72	.72	.72
15.00	DISCHG	.72	.70	.66	.63	.61	.60	.60	.60	.60	.60
16.00	DISCHG	.60	.60	.60	.60	.60	.60	.60	.60	.60	.60
17.00	DISCHG	.60	.60	.60	.60	.60	.60	.60	.60	.60	.60
18.00	DISCHG	.60	.60	.60	.60	.60	.60	.60	.60	.60	.60
19.00	DISCHG	.60	.60	.60	.60	.60	.60	.60	.60	.60	.60
20.00	DISCHG	.60	.57	.47	.39	.34	.31	.30	.31	.31	.31
21.00	DISCHG	.30	.30	.30	.31	.31	.30	.30	.30	.31	.31
22.00	DISCHG	.30	.30	.30	.31	.31	.30	.30	.30	.31	.31
23.00	DISCHG	.30	.30	.30	.31	.31	.30	.30	.30	.31	.31
24.00	DISCHG	.30	.26	.16	.07	.03	.01	.01	.00		

RUNOFF VOLUME ABOVE BASEFLOW = 2.53 WATERSHED INCHES, 39.17 CFS-HRS, 3.24 ACRE-FEET; BASEFLOW = .00 CFS

EXECUTIVE CONTROL OPERATION ENDCMP RECORD ID  
 COMPUTATIONS COMPLETED FOR PASS 2

EXECUTIVE CONTROL OPERATION ENDJOB RECORD ID

1

TR20 XEQ CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011) JOB 1 SUMMARY  
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SUMMARY TABLE 1 - SELECTED RESULTS OF STANDARD AND EXECUTIVE CONTROL INSTRUCTIONS IN THE ORDER PERFORMED  
 (A STAR (\*) AFTER THE PEAK DISCHARGE TIME AND RATE (CFS) VALUES INDICATES A FLAT TOP HYDROGRAPH  
 A QUESTION MARK (?) INDICATES A HYDROGRAPH WITH PEAK AS LAST POINT.)

SECTION/ STRUCTURE ID	STANDARD CONTROL OPERATION	RAIN DRAINAGE AREA (SQ MI)	ANTEC TABLE #	MAIN MOIST COND	TIME INCREM (HR)	PRECIPITATION			RUNOFF AMOUNT (IN)	PEAK DISCHARGE		
						BEGIN (HR)	AMOUNT (IN)	DURATION (HR)		ELEVATION (FT)	TIME (HR)	RATE (CFS)

ALTERNATE 1 STORM 10														
+														
XSECTION	60	RUNOFF	.55	7	2	.10	.0	3.00	24.00	.34	---	6.30	62.13	114.0
XSECTION	20	RUNOFF	.08	7	2	.10	.0	3.00	24.00	1.26	---	6.06	83.32	1068.1
XSECTION	1	RUNOFF	.02	7	2	.10	.0	3.00	24.00	1.20	---	6.05	24.34	1014.1
XSECTION	200	RUNOFF	.03	7	2	.10	.0	3.00	24.00	1.12	---	6.06	25.76	954.2
XSECTION	160	RUNOFF	.72	7	2	.10	.0	3.00	24.00	.42	---	6.25	121.89	169.3
+														
XSECTION	164	RUNOFF	1.05	7	2	.10	.0	3.00	24.00	.60	---	6.31	259.82	247.7
XSECTION	164	ADDHYD	1.77	7	2	.10	.0	3.00	24.00	.53	---	6.29	379.08	214.3
XSECTION	166	RUNOFF	.06	7	2	.10	.0	3.00	24.00	1.17	---	6.12	49.61	813.3
XSECTION	166	ADDHYD	1.83	7	2	.10	.0	3.00	24.00	.55	---	6.28	412.96	225.7
XSECTION	168	RUNOFF	.02	7	2	.10	.0	3.00	24.00	1.24	---	6.08	23.92	996.7

ALTERNATE 1 STORM 99														
+														
XSECTION	60	RUNOFF	.55	7	2	.10	.0	4.60	24.00	1.09	---	6.25	286.75	526.1
XSECTION	20	RUNOFF	.08	7	2	.10	.0	4.60	24.00	2.56	---	6.04	168.77	2163.7
XSECTION	1	RUNOFF	.02	7	2	.10	.0	4.60	24.00	2.48	---	6.02	51.21	2133.9
XSECTION	200	RUNOFF	.03	7	2	.10	.0	4.60	24.00	2.36	---	6.04	54.47	2017.5
XSECTION	160	RUNOFF	.72	7	2	.10	.0	4.60	24.00	1.24	---	6.21	480.52	667.4
+														
XSECTION	164	RUNOFF	1.05	7	2	.10	.0	4.60	24.00	1.56	---	6.28	804.17	766.6
XSECTION	164	ADDHYD	1.77	7	2	.10	.0	4.60	24.00	1.43	---	6.25	1273.17	719.7
XSECTION	166	RUNOFF	.06	7	2	.10	.0	4.60	24.00	2.43	---	6.10	108.38	1776.8
XSECTION	166	ADDHYD	1.83	7	2	.10	.0	4.60	24.00	1.46	---	6.24	1358.29	742.2
XSECTION	168	RUNOFF	.02	7	2	.10	.0	4.60	24.00	2.53	---	6.06	50.03	2084.6

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TR20 XEQ  
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CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
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JOB 1 SUMMARY  
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SUMMARY TABLE 3 - DISCHARGE (CFS) AT XSECTIONS AND STRUCTURES FOR ALL STORMS AND ALTERNATES

XSECTION/ STRUCTURE ID	DRAINAGE AREA (SQ MI)	STORM NUMBERS.....	
		10	99
0 XSECTION 1	.02		
+			
ALTERNATE 1		24.34	51.21
0 XSECTION 20	.08		
+			
ALTERNATE 1		83.32	168.77
0 XSECTION 60	.55		
+			
ALTERNATE 1		62.13	286.75
0 XSECTION 160	.72		
+			
ALTERNATE 1		121.89	480.52
0 XSECTION 164	1.77		
+			
ALTERNATE 1		379.08	1273.17
0 XSECTION 166	1.83		
+			
ALTERNATE 1		412.96	1358.29
0 XSECTION 168	.02		
+			
ALTERNATE 1		23.92	50.03
0 XSECTION 200	.03		
+			
ALTERNATE 1		25.76	54.47

1 END OF 1 JOBS IN THIS RUN

**TR-20 PRINTOUT  
DEVELOPED CONDITIONS  
DETENTION POND NO. 1**

6/11/93

FUTURE CONDITIONS  
RETENTION POND NO. 1

DATAFILE:  
EW1011F1.TZ

\*\*\*\*\*80-80 LIST OF INPUT DATA FOR TR-20 HYDROLOGY\*\*\*\*\*

JOB TR-20 SUMMARY NOPLOTS  
TITLE CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
TITLE FUT. CONDITIONS (FULL DEV., 2 AND 24 HR. STORMS, ST. 20)

5	RAINFL 7	0.2500			
8		0.0000	0.0005	0.0015	0.0030
8		0.0060	0.0080	0.0100	0.0120
8		0.0165	0.0188	0.0210	0.0233
8		0.0278	0.0320	0.0390	0.0460
8		0.0600	0.0750	0.1000	0.4000
8		0.7250	0.7500	0.7650	0.7800
8		0.8000	0.8100	0.8200	0.8250
8		0.8350	0.8400	0.8450	0.8500
8		0.8600	0.8638	0.8675	0.8713
8		0.8788	0.8825	0.8863	0.8900
8		0.8975	0.9013	0.9050	0.9083
8		0.9148	0.9180	0.9210	0.9240
8		0.9300	0.9325	0.9350	0.9375
8		0.9425	0.9450	0.9475	0.9500
8		0.9550	0.9575	0.9600	0.9625
8		0.9675	0.9700	0.9725	0.9750
8		0.9800	0.9813	0.9825	0.9838
8		0.9863	0.9875	0.9888	0.9900
8		0.9925	0.9938	0.9950	0.9963
8		0.9988	1.0000	1.0000	1.0000

9	ENDTBL				
5	RAINFL 8	0.08333			
8		0.000	0.020	0.057	0.139
8		0.539	0.659	0.715	0.758
8		0.828	0.860	0.892	0.924
8		0.988	1.013	1.032	1.051
8		1.089	1.108	1.127	1.144

9	ENDTBL				
5	RAINFL 9	0.08333			
8		0.000	0.010	0.040	0.086
8		0.306	0.556	0.696	0.776
8		0.888	0.928	0.968	1.008
8		1.048	1.060	1.072	1.084
8		1.108	1.120	1.132	1.144

9	ENDTBL				
3	STRUCT 20				
8		5943.	0.0	0.00	
8		5944.	17.	0.06	
8		5946.	62.	0.61	
8		5948.	94.	2.06	
8		5950.	116.	5.18	
8		5951.	127.	8.09	

\*\*\*\*\*80-80 LIST OF INPUT DATA (CONTINUED)\*\*\*\*\*

8		5952.5	140.	13.27	
8		5953.	240.	15.55	
8		5954.	403.	20.11	
8		5956.	445.	32.23	
8		5957.	460.	38.0	

9	ENDTBL				
2	XSECTN 062	1.0			
8		6140.	0.0	0.0	
8		6140.5	59.	8.	
8		6141.	198.	19.	
8		6142.	707.	46.	
8		6143.	1554.	81.	
8		6145.	3047.	168.	

9	ENDTBL				
2	XSECTN 064	1.0			
8		5986.	0.0	0.0	
8		5986.5	65.	16.	
8		5988.	712.	76.	
8		5990.	2537.	184.	
8		5992.	5579.	324.	

9	ENDTBL				
2	XSECTN 063	1.0			
8		6130.	0.0	0.0	



8		6130.5	105.	16.
8		6131.	340.	34.
8		6132.	1142.	76.
8		6134.	4072.	184.
9	ENDTBL			
2	XSECTN 022	1.0		
8		5970.	0.0	0.0
8		5970.5	51.	9.
8		5972.	610.	46.
9	ENDTBL			
6	RUNOFF 1 051	6 0.023	83.9	0.10
6	RUNOFF 1 052	5 0.037	88.	0.14
6	ADDHYD 4 052	5 6 3		
6	RUNOFF 1 060	6 0.083	72.2	0.26
6	REACH 3 062	6 5 2400.		
6	RUNOFF 1 062	6 0.053	71.2	0.22
6	ADDHYD 4 062	5 6 7		
6	REACH 3 064	7 4 2400.		
6	RUNOFF 1 061	6 0.165	71.9	0.32
6	REACH 3 063	6 5 2700.		
6	RUNOFF 1 063	6 0.111	79.2	0.25
6	ADDHYD 4 063	5 6 7		
6	REACH 3 064	7 5 2400.		

1

\*\*\*\*\*80-80 LIST OF INPUT DATA (CONTINUED)\*\*\*\*\*

6	RUNOFF 1 064	6 0.073	90.	0.19				
6	ADDHYD 4 064	5 6 7						
6	ADDHYD 4 064	4 7 5						
6	RUNOFF 1 020	7 0.031	91.6	0.10				
6	ADDHYD 4 064	5 7 6						
6	ADDHYD 4 064	6 3 4						
6	RUNOFF 1 021	6 0.021	79.	0.10				
6	REACH 3 022	6 5 1700.						
6	RUNOFF 1 022	6 0.026	91.6	0.10				
6	ADDHYD 4 022	5 6 7						
6	ADDHYD 4 022	7 4 6			1 1 1			
6	RESVOR 2	20 6 5 5943.						
	ENDATA							
7	INCREM 6	0.05						
7	COMPUT 7 051	20 0.0	4.6	1.0	7 2 01 99			
	ENDCMP 1							
7	COMPUT 7 051	20 0.0	3.0	1.0	7 2 01 10			
	ENDCMP 1							
	ENDJOB 2							

0\*\*\*\*\*END OF 80-80 LIST\*\*\*\*\*

1

TR20 XEQ	CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN.EW-1011)	JOB 1	PASS 1
REV 09/01/83	FUT. CONDITIONS (FULL DEV., 2 AND 24 HR. STORMS, ST. 20)		PAGE 1

0 COMPUTER PROGRAM FOR PROJECT FORMULATION - HYDROLOGY USER NOTES

THE USERS MANUAL FOR THIS PROGRAM IS THE MAY 1982 DRAFT OF TR-20. CHANGES FROM THE 2/14/74 VERSION INCLUDE:

REACH ROUTING - THE MODIFIED ATT-KIN ROUTING PROCEDURE REPLACES THE CONVEX METHOD. INPUT DATA PREPARED FOR PREVIOUS PROGRAM VERSIONS USING CONVEX ROUTING COEFFICIENTS WILL NOT RUN ON THIS VERSION.

THE PREFERRED TYPE OF DATA ENTRY IS CROSS SECTION DATA REPRESENTATIVE OF A REACH. IT IS RECOMMENDED THAT THE OPTIONAL CROSS SECTION DISCHARGE-AREA PLOTS BE OBTAINED WHENEVER NEW CROSS SECTION DATA IS ENTERED. THE PLOTS SHOULD BE CHECKED FOR REASONABLENESS AND ADEQUACY OF INPUT DATA FOR THE COMPUTATION OF "M" VALUES USED IN THE ROUTING PROCEDURE.

GUIDELINES FOR DETERMINING OR ANALYZING REACH LENGTHS AND COEFFICIENTS (X,M) ARE AVAILABLE IN THE USERS MANUAL. SUMMARY TABLE 2 DISPLAYS REACH ROUTING RESULTS AND ROUTING PARAMETERS FOR COMPARISON AND CHECKING.

HYDROGRAPH GENERATION - THE PROCEDURE TO CALCULATE THE INTERNAL TIME INCREMENT AND PEAK TIME OF THE UNIT HYDROGRAPH HAVE BEEN IMPROVED. PEAK DISCHARGES AND TIMES MAY DIFFER FROM THE PREVIOUS VERSION. OUTPUT HYDROGRAPHS ARE STILL INTERPOLATED, PRINTED, AND ROUTED AT THE USER SELECTED MAIN TIME INCREMENT.

INTERMEDIATE PEAKS - METHOD ADDED TO PROVIDE DISCHARGES AT INTERMEDIATE POINTS WITHIN REACHES WITHOUT ROUTING.

OTHER - THIS VERSION CONTAINS SOME ADDITIONS TO THE INPUT AND NUMEROUS MODIFICATIONS TO THE OUTPUT. USER OPTIONS HAVE BEEN MODIFIED AND AUGMENTED ON THE JOB RECORD, RAINTABLES ADDED, ERROR AND WARNING MESSAGES EXPANDED, AND THE SUMMARY TABLES COMPLETELY REVISED. THE HOLDOUT OPTION IS NOT OPERATIONAL AT THIS TIME.

PROGRAM QUESTIONS OR PROBLEMS SHOULD BE DIRECTED TO HYDRAULIC ENGINEERS AT THE SCS NATIONAL TECHNICAL CENTERS:

CHESTER, PA (NORTHEAST) -- 215-499-3933, FORT WORTH, TX (SOUTH) -- 334-5242 (FTS)  
 LINCOLN, NB (MIDWEST) -- 541-5318 (FTS), PORTLAND, OR (WEST) -- 423-4099 (FTS)  
 OR HYDROLOGY UNIT, ENGINEERING DIVISION, LANHAM, MD -- 436-7383 (FTS).

PROGRAM CHANGES SINCE MAY 1982:

- 12/17/82 - CORRECT PEAK RATE FACTOR FOR USER ENTERED DIMHYD  
 CORRECT REACH ROUTING PEAK TRAVEL TIME PRINTED WITH FULLPRINT OPTION
- 5/02/83 - CORRECT COMPUTATIONS FOR ---
  1. DIVISION OF BASEFLOW IN DIVERT OPERATION
  2. HYDROGRAPH VOLUME SPLIT BETWEEN BASEFLOW AND ABOVE BASEFLOW
  3. CROSS SECTION DATA PLOTTING POSITION.
  4. INTERMEDIATE PEAK WHEN "FROM" AREA IS LARGER THAN "THRU" AREA
  5. STORAGE ROUTED REACH TRAVEL TIME FOR MULTYPEAK HYDROGRAPH .
  6. ORDERING "FLOW-FREQ" FILE FROM SUMMARY TABLE #3 DATA
  7. BASEFLOW ENTERED WITH READHYD
  8. LOW FLOW SPLIT DURING DIVERT PROCEDURE #2 WHEN SECTION RATINGS START AT DIFFERENT ELEVATIONS
- ENHANCEMENTS ---
  1. REPLACE USER MANUAL ERROR CODES (PAGE 4-9 TO 4-11) WITH MESSAGES
  2. LABEL OUTPUT HYDROGRAPH FILES WITH CROSS SECTION/STRUCTURE, ALTERNATE AND STORM NO'S
- 09/01/83 - CORRECT INPUT AND OUTPUT ERRORS FOR INTERMEDIATE PEAKS  
 CORRECT COMBINATION OF RATING TABLES FOR DIVERT  
 CHECK REACH ROUTING PARAMETERS FOR ACCEPTABLE LIMITS  
 ELIMINATE MINIMUM REACH TRAVEL TIME WHEN ATT-KIN COEFFICIENT EQUALS ONE

1

TR20 XEQ  
 REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
 FUT. CONDITIONS (FULL DEV., 2 AND 24 HR. STORMS, ST. 20)

JOB 1 PASS 1  
 PAGE 2

CUMULATIVE RAINFALL TABLE 7 TIME INCREMENT= .25

8	.0000	.0005	.0015	.0030	.0045
8	.0060	.0080	.0100	.0120	.0143
8	.0165	.0188	.0210	.0233	.0255
8	.0278	.0320	.0390	.0460	.0530
8	.0600	.0750	.1000	.4000	.7000
8	.7250	.7500	.7650	.7800	.7900
8	.8000	.8100	.8200	.8250	.8300
8	.8350	.8400	.8450	.8500	.8550
8	.8600	.8638	.8675	.8713	.8750
8	.8788	.8825	.8863	.8900	.8938
8	.8975	.9013	.9050	.9083	.9115
8	.9148	.9180	.9210	.9240	.9270
8	.9300	.9325	.9350	.9375	.9400
8	.9425	.9450	.9475	.9500	.9525
8	.9550	.9575	.9600	.9625	.9650
8	.9675	.9700	.9725	.9750	.9775
8	.9800	.9813	.9825	.9838	.9850
8	.9863	.9875	.9888	.9900	.9913
8	.9925	.9938	.9950	.9963	.9975
8	.9988	1.0000	1.0000	1.0000	1.0000

9 ENDTBL

CUMULATIVE RAINFALL TABLE 8 TIME INCREMENT= .08

8	.0000	.0200	.0570	.1390	.2890
8	.5390	.6590	.7150	.7580	.7960
8	.8280	.8600	.8920	.9240	.9560
8	.9880	1.0130	1.0320	1.0510	1.0700
8	1.0890	1.1080	1.1270	1.1440	1.1570

9 ENDTBL

CUMULATIVE RAINFALL TABLE 9 TIME INCREMENT= .08

8	.0000	.0100	.0400	.0860	.1660
8	.3060	.5560	.6960	.7760	.8380
8	.8880	.9280	.9680	1.0080	1.0280

8	1.0480	1.0600	1.0720	1.0840	1.0960
8	1.1080	1.1200	1.1320	1.1440	1.1560

9 ENDTBL  
1

TR20 XEQ  
REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
FUT. CONDITIONS (FULL DEV., 2 AND 24 HR. STORMS, ST. 20)

JOB 1 PASS 1  
PAGE 3

STRUCTURE DATA, STRUCTURE NO. 20

	ELEVATION	DISCHARGE	STORAGE
8	5943.00	.00	.00
8	5944.00	17.00	.06
8	5946.00	62.00	.61
8	5948.00	94.00	2.06
8	5950.00	116.00	5.18
8	5951.00	127.00	8.09
8	5952.50	140.00	13.27
8	5953.00	240.00	15.55
8	5954.00	403.00	20.11
8	5956.00	445.00	32.23
8	5957.00	460.00	38.00

9 ENDTBL

CROSS-SECTION DATA, CROSS-SECTION NO. 62 DRAINAGE AREA= 1.00 BANKFULL ELEV.= .00

	ELEVATION	DISCHARGE	END AREA
8	6140.00	.00	.00
8	6140.50	59.00	8.00
8	6141.00	198.00	19.00
8	6142.00	707.00	46.00
8	6143.00	1554.00	81.00
8	6145.00	3047.00	168.00

9 ENDTBL

CROSS-SECTION DATA, CROSS-SECTION NO. 64 DRAINAGE AREA= 1.00 BANKFULL ELEV.= .00

	ELEVATION	DISCHARGE	END AREA
8	5986.00	.00	.00
8	5986.50	65.00	16.00
8	5988.00	712.00	76.00
8	5990.00	2537.00	184.00
8	5992.00	5579.00	324.00

9 ENDTBL

CROSS-SECTION DATA, CROSS-SECTION NO. 63 DRAINAGE AREA= 1.00 BANKFULL ELEV.= .00

	ELEVATION	DISCHARGE	END AREA
8	6130.00	.00	.00
8	6130.50	105.00	16.00
8	6131.00	340.00	34.00
8	6132.00	1142.00	76.00

1

TR20 XEQ  
REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
FUT. CONDITIONS (FULL DEV., 2 AND 24 HR. STORMS, ST. 20)

JOB 1 PASS 1  
PAGE 4

8	6134.00	4072.00	184.00
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9 ENDTBL

CROSS-SECTION DATA, CROSS-SECTION NO. 22 DRAINAGE AREA= 1.00 BANKFULL ELEV.= .00

	ELEVATION	DISCHARGE	END AREA
8	5970.00	.00	.00
8	5970.50	51.00	9.00
8	5972.00	610.00	46.00

9 ENDTBL

STANDARD CONTROL OPERATION RUNOFF CROSS SECTION 51

RECORD ID

OUTPUT HYDROGRAPH = 6		DATA FIELD VALUES =	.0230	83.9000	.1000
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 52			RECORD ID	
OUTPUT HYDROGRAPH = 5		DATA FIELD VALUES =	.0370	88.0000	.1400
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 52			RECORD ID	
INPUT HYDROGRAPHS = 5,6	OUTPUT HYDROGRAPH = 3	DATA FIELD VALUES =	.0000	.0000	.0000
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 60			RECORD ID	
OUTPUT HYDROGRAPH = 6		DATA FIELD VALUES =	.0830	72.2000	.2600
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION REACH	CROSS SECTION 62			RECORD ID	
INPUT HYDROGRAPH = 6	OUTPUT HYDROGRAPH = 5	DATA FIELD VALUES =	2400.0000	.0000	.0000
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 62			RECORD ID	
OUTPUT HYDROGRAPH = 6		DATA FIELD VALUES =	.0530	71.2000	.2200
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 62			RECORD ID	
INPUT HYDROGRAPHS = 5,6	OUTPUT HYDROGRAPH = 7	DATA FIELD VALUES =	.0000	.0000	.0000
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION REACH	CROSS SECTION 64			RECORD ID	
INPUT HYDROGRAPH = 7	OUTPUT HYDROGRAPH = 4	DATA FIELD VALUES =	2400.0000	.0000	.0000
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 61			RECORD ID	
OUTPUT HYDROGRAPH = 6		DATA FIELD VALUES =	.1650	71.9000	.3200
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION REACH	CROSS SECTION 63			RECORD ID	

1

TR20 XEQ	CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)	JOB 1	PASS 1
REV 09/01/83	FUT. CONDITIONS (FULL DEV., 2 AND 24 HR. STORMS, ST. 20)		PAGE 5

INPUT HYDROGRAPH = 6	OUTPUT HYDROGRAPH = 5	DATA FIELD VALUES =	2700.0000	.0000	.0000
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 63			RECORD ID	
OUTPUT HYDROGRAPH = 6		DATA FIELD VALUES =	.1110	79.2000	.2500
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 63			RECORD ID	
INPUT HYDROGRAPHS = 5,6	OUTPUT HYDROGRAPH = 7	DATA FIELD VALUES =	.0000	.0000	.0000
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION REACH	CROSS SECTION 64			RECORD ID	
INPUT HYDROGRAPH = 7	OUTPUT HYDROGRAPH = 5	DATA FIELD VALUES =	2400.0000	.0000	.0000
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 64			RECORD ID	
OUTPUT HYDROGRAPH = 6		DATA FIELD VALUES =	.0730	90.0000	.1900
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 64			RECORD ID	
INPUT HYDROGRAPHS = 5,6	OUTPUT HYDROGRAPH = 7	DATA FIELD VALUES =	.0000	.0000	.0000
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 64			RECORD ID	
INPUT HYDROGRAPHS = 4,7	OUTPUT HYDROGRAPH = 5	DATA FIELD VALUES =	.0000	.0000	.0000
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 20			RECORD ID	
OUTPUT HYDROGRAPH = 7		DATA FIELD VALUES =	.0310	91.6000	.1000
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 64			RECORD ID	
INPUT HYDROGRAPHS = 5,7	OUTPUT HYDROGRAPH = 6	DATA FIELD VALUES =	.0000	.0000	.0000
OUTPUT OPTIONS IN EFFECT	SUM				
STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 64			RECORD ID	
INPUT HYDROGRAPHS = 6,3	OUTPUT HYDROGRAPH = 4	DATA FIELD VALUES =	.0000	.0000	.0000

OUTPUT OPTIONS IN EFFECT SUM

STANDARD CONTROL OPERATION RUNOFF CROSS SECTION 21  
 OUTPUT HYDROGRAPH = 6 DATA FIELD VALUES = .0210 RECORD ID 79.0000 .1000  
 OUTPUT OPTIONS IN EFFECT SUM

STANDARD CONTROL OPERATION REACH CROSS SECTION 22  
 INPUT HYDROGRAPH = 6 OUTPUT HYDROGRAPH = 5 DATA FIELD VALUES = 1700.0000 RECORD ID .0000 .0000  
 OUTPUT OPTIONS IN EFFECT SUM

STANDARD CONTROL OPERATION RUNOFF CROSS SECTION 22 RECORD ID

1

TR20 XEQ CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011) JOB 1 PASS 1  
 REV 09/01/83 FUT. CONDITIONS (FULL DEV., 2 AND 24 HR. STORMS, ST. 20) PAGE 6

OUTPUT HYDROGRAPH = 6 DATA FIELD VALUES = .0260 91.6000 .1000  
 OUTPUT OPTIONS IN EFFECT SUM

STANDARD CONTROL OPERATION ADDHYD CROSS SECTION 22 RECORD ID  
 INPUT HYDROGRAPHS = 5,6 OUTPUT HYDROGRAPH = 7 DATA FIELD VALUES = .0000 .0000 .0000  
 OUTPUT OPTIONS IN EFFECT SUM

STANDARD CONTROL OPERATION ADDHYD CROSS SECTION 22 RECORD ID  
 INPUT HYDROGRAPHS = 7,4 OUTPUT HYDROGRAPH = 6 DATA FIELD VALUES = .0000 .0000 .0000  
 OUTPUT OPTIONS IN EFFECT PEAK HYD VOL SUM

STANDARD CONTROL OPERATION RESVOR STRUCTURE 20 RECORD ID  
 INPUT HYDROGRAPH = 6 OUTPUT HYDROGRAPH = 5 DATA FIELD VALUES = 5943.0000 .0000 .0000  
 OUTPUT OPTIONS IN EFFECT SUM

EXECUTIVE CONTROL OPERATION INCREM RECORD ID  
 + MAIN TIME INCREMENT = .05 HOURS

EXECUTIVE CONTROL OPERATION COMPUT RECORD ID  
 + FROM XSECTION 51  
 + TO STRUCTURE 20  
 STARTING TIME = .00 RAIN DEPTH = 4.60 RAIN DURATION = 1.00 RAIN TABLE NO. = 7 ANT. MOIST. COND = 2  
 ALTERNATE NO. = 1 STORM NO. = 99 MAIN TIME INCREMENT = .05 HOURS

\*\*\*WARNING - LACK OF LOW FLOW DEFINITION FOR XSECT TABLE 22. MAX.FLOW LESS THAN 2ND TABLE VALUE.

OPERATION ADDHYD CROSS SECTION 22

PEAK TIME(HRS)	PEAK DISCHARGE(CFS)	PEAK ELEVATION(FEET)
6.03	1075.75	5973.25
7.98	57.73	5970.52
9.98	29.32	5970.29
12.79	22.37	5970.22
13.78	19.52	5970.19

TIME(HRS)	FIRST HYDROGRAPH POINT =	.00 HOURS	TIME INCREMENT =	.05 HOURS	DRAINAGE AREA =	.62 SQ.MI.
4.00	DISCHG	.00 .00 .00 .00	.00 .00 .00 .00	.02 .06	.12	
4.50	DISCHG	.18 .24 .30 .36	.44 .54 .64 .75	.87	.99	
5.00	DISCHG	1.11 1.55 2.44 3.22	3.92 4.55 5.85 8.14	10.19 11.99		
5.50	DISCHG	14.15 54.10 169.87 293.12	406.00 509.01 611.43 717.28	827.07 939.44		
6.00	DISCHG	1049.81 1064.71 938.04 829.31	734.91 637.55 535.75 439.94	357.93 292.62		
6.50	DISCHG	244.35 206.87 175.30 152.38	135.57 122.63 112.39 104.41	98.41 94.03		
7.00	DISCHG	90.94 87.13 81.60 77.10	73.43 70.13 67.11 64.49	62.37 60.75		
7.50	DISCHG	59.60 58.81 58.27 57.93	57.72 57.59 57.53 57.50	57.50 57.51		
8.00	DISCHG	57.52 55.85 51.72 48.10	44.93 41.91 39.04 36.48	34.37 32.74		
8.50	DISCHG	31.55 30.71 30.14 29.75	29.50 29.34 29.23 29.16	29.12 29.10		
9.00	DISCHG	29.09 29.09 29.09 29.10	29.10 29.11 29.12 29.13	29.15 29.16		
9.50	DISCHG	29.17 29.18 29.19 29.20	29.21 29.22 29.23 29.24	29.25 29.27		
10.00	DISCHG	29.27 28.87 27.88 27.00	26.23 25.49 24.75 24.05	23.46 23.00		

1

TR20 XEQ CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011) JOB 1 PASS 1  
 REV 09/01/83 FUT. CONDITIONS (FULL DEV., 2 AND 24 HR. STORMS, ST. 20) PAGE 7

10.50	DISCHG	22.64 22.42 22.31 22.25	22.22 22.22 22.20 22.15	22.10 22.06
11.00	DISCHG	22.02 22.02 22.06 22.10	22.14 22.19 22.20 22.17	22.14 22.11

11.50	DISCHG	22.07	22.07	22.12	22.16	22.20	22.25	22.26	22.23	22.19	22.16
12.00	DISCHG	22.13	22.13	22.17	22.21	22.26	22.30	22.32	22.28	22.25	22.22
12.50	DISCHG	22.19	22.18	22.23	22.27	22.31	22.36	22.37	22.34	22.31	22.28
13.00	DISCHG	22.24	22.06	21.69	21.36	21.07	20.80	20.51	20.21	19.95	19.74
13.50	DISCHG	19.58	19.49	19.47	19.47	19.48	19.51	19.51	19.47	19.43	19.39
14.00	DISCHG	19.35	19.24	19.03	18.85	18.69	18.54	18.41	18.29	18.20	18.13
14.50	DISCHG	18.08	18.05	18.02	18.01	18.00	18.00	17.99	17.99	17.99	18.00

RUNOFF VOLUME ABOVE BASEFLOW = 2.20 WATERSHED INCHES, 885.04 CFS-HRS, 73.14 ACRE-FEET; BASEFLOW = .00 CFS

EXECUTIVE CONTROL OPERATION ENDCMP

RECORD ID

COMPUTATIONS COMPLETED FOR PASS 1

EXECUTIVE CONTROL OPERATION COMPUT

RECORD ID

FROM XSECTION 51

TO STRUCTURE 20

STARTING TIME = .00 RAIN DEPTH = 3.00 RAIN DURATION= 1.00 RAIN TABLE NO.= 7 ANT. MOIST. COND= 2  
 ALTERNATE NO.= 1 STORM NO.=10 MAIN TIME INCREMENT = .05 HOURS

\*\*\*WARNING - LACK OF LOW FLOW DEFINITION FOR XSECT TABLE 62. MAX.FLOW LESS THAN 2ND TABLE VALUE.

\*\*\*WARNING - LACK OF LOW FLOW DEFINITION FOR XSECT TABLE 63. MAX.FLOW LESS THAN 2ND TABLE VALUE.

\*\*\*WARNING - LACK OF LOW FLOW DEFINITION FOR XSECT TABLE 22. MAX.FLOW LESS THAN 2ND TABLE VALUE.

OPERATION ADDHYD CROSS SECTION 22

PEAK TIME(HRS)	PEAK DISCHARGE(CFS)	PEAK ELEVATION(FEET)
6.02	494.64	5971.69
7.98	31.45	5970.31
9.98	16.13	5970.16
12.78	12.42	5970.12

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .05 HOURS	DRAINAGE AREA = .62 SQ.MI.
5.00	DISCHG .00 .00 .05 .14 .25 .38 .63	1.10 1.62 2.18	
5.50	DISCHG 2.96 16.78 63.83 123.81 182.52 235.91 285.81	334.41 383.88 435.25	
6.00	DISCHG 488.19 487.75 409.37 352.37 313.97 281.19 247.45	214.12 183.33 156.52	
6.50	DISCHG 134.71 115.78 98.35 85.27 75.63 68.30 62.58	58.12 54.71 52.13	
7.00	DISCHG 50.22 47.82 44.41 41.76 39.75 38.08 36.60	35.32 34.24 33.38	
7.50	DISCHG 32.72 32.23 31.88 31.64 31.48 31.39 31.33	31.31 31.30 31.31	
8.00	DISCHG 31.32 30.30 27.86 25.85 24.25 22.83 21.49	20.28 19.23 18.35	
8.50	DISCHG 17.67 17.15 16.76 16.49 16.30 16.17 16.08	16.02 15.98 15.96	
9.00	DISCHG 15.95 15.95 15.95 15.95 15.96 15.96 15.97	15.98 15.99 16.00	
9.50	DISCHG 16.01 16.02 16.03 16.04 16.05 16.05 16.07	16.07 16.08 16.09	
10.00	DISCHG 16.10 15.86 15.26 14.78 14.39 14.04 13.69	13.34 13.03 12.79	

TR20.XEQ

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
 FUT. CONDITIONS (FULL DEV., 2 AND 24 HR. STORMS, ST. 20)

JOB 1 PASS 2  
 PAGE 8

10.50	DISCHG	12.59	12.46	12.39	12.34	12.31	12.29	12.27	12.23	12.19	12.17
11.00	DISCHG	12.15	12.16	12.19	12.22	12.24	12.26	12.27	12.24	12.22	12.21
11.50	DISCHG	12.20	12.20	12.24	12.27	12.29	12.31	12.32	12.29	12.27	12.26
12.00	DISCHG	12.25	12.25	12.29	12.32	12.34	12.36	12.37	12.34	12.32	12.31
12.50	DISCHG	12.29	12.30	12.34	12.37	12.39	12.41	12.42	12.39	12.37	12.36
13.00	DISCHG	12.34	12.24	12.02	11.84	11.70	11.57	11.42	11.26	11.13	11.02
13.50	DISCHG	10.93	10.88	10.87	10.87	10.87	10.87	10.87	10.83	10.80	10.79
14.00	DISCHG	10.77	10.71	10.59	10.49	10.41	10.34	10.27	10.22	10.17	10.13
14.50	DISCHG	10.10	10.08	10.06	10.05	10.04	10.04	10.04	10.04	10.04	10.04

RUNOFF VOLUME ABOVE BASEFLOW = 1.07 WATERSHED INCHES, 432.05 CFS-HRS, 35.70 ACRE-FEET; BASEFLOW = .00 CFS

EXECUTIVE CONTROL OPERATION ENDCMP

RECORD ID

COMPUTATIONS COMPLETED FOR PASS 2

EXECUTIVE CONTROL OPERATION ENDJOB

RECORD ID

SUMMARY TABLE 1 - SELECTED RESULTS OF STANDARD AND EXECUTIVE CONTROL INSTRUCTIONS IN THE ORDER PERFORMED  
(A STAR(\*) AFTER THE PEAK DISCHARGE TIME AND RATE (CFS) VALUES INDICATES A FLAT TOP HYDROGRAPH  
A QUESTION MARK(?) INDICATES A HYDROGRAPH WITH PEAK AS LAST POINT.)

SECTION/ STRUCTURE ID	STANDARD CONTROL OPERATION	DRAINAGE AREA (SQ MI)	RAIN TABLE #	ANTEC MOIST COND	MAIN TIME INCREM (HR)	PRECIPITATION			RUNOFF AMOUNT (IN)	PEAK DISCHARGE			
						BEGIN (HR)	AMOUNT (IN)	DURATION (HR)		ELEVATION (FT)	TIME (HR)	RATE (CFS)	RATE (CSM)
ALTERNATE 1 STORM 99													
XSECTION 51	RUNOFF	.02	7	2	.05	.0	4.60	24.00	2.60	---	5.98	66.64	2897.4
XSECTION 52	RUNOFF	.04	7	2	.05	.0	4.60	24.00	2.98	---	5.99	113.42	3065.3
XSECTION 52	ADDHYD	.06	7	2	.05	.0	4.60	24.00	2.83	---	5.98	180.04	3000.6
XSECTION 60	RUNOFF	.08	7	2	.05	.0	4.60	24.00	1.66	---	6.06	135.33	1630.4
XSECTION 62	REACH	.08	7	2	.05	.0	4.60	24.00	1.66	6140.76	6.13	130.94	1577.6
XSECTION 62	RUNOFF	.05	7	2	.05	.0	4.60	24.00	1.59	---	6.04	87.70	1654.8
XSECTION 62	ADDHYD	.14	7	2	.05	.0	4.60	24.00	1.63	6141.02	6.08	207.95	1529.1
XSECTION 64	REACH	.14	7	2	.05	.0	4.60	24.00	1.63	5986.80	6.17	193.91	1425.8
XSECTION 61	RUNOFF	.17	7	2	.05	.0	4.60	24.00	1.64	---	6.09	244.04	1479.1
XSECTION 63	REACH	.17	7	2	.05	.0	4.60	24.00	1.64	6130.78	6.16	234.53	1421.4
XSECTION 63	RUNOFF	.11	7	2	.05	.0	4.60	24.00	2.19	---	6.04	241.17	2172.7
XSECTION 63	ADDHYD	.28	7	2	.05	.0	4.60	24.00	1.86	6131.13	6.09	443.11	1605.5
XSECTION 64	REACH	.28	7	2	.05	.0	4.60	24.00	1.86	5987.34	6.16	427.14	1547.6
XSECTION 64	RUNOFF	.07	7	2	.05	.0	4.60	24.00	3.17	---	6.00	226.47	3102.3
XSECTION 64	ADDHYD	.35	7	2	.05	.0	4.60	24.00	2.13	5987.68	6.08	573.60	1643.6
XSECTION 64	ADDHYD	.49	7	2	.05	.0	4.60	24.00	1.99	5988.04	6.11	749.53	1545.4
XSECTION 20	RUNOFF	.03	7	2	.05	.0	4.60	24.00	3.34	---	5.98	105.25	3395.1
XSECTION 64	ADDHYD	.52	7	2	.05	.0	4.60	24.00	2.07	5988.10	6.07	799.47	1549.4
XSECTION 64	ADDHYD	.58	7	2	.05	.0	4.60	24.00	2.15	5988.26	6.04	950.93	1650.9
XSECTION 21	RUNOFF	.02	7	2	.05	.0	4.60	24.00	2.19	---	5.98	53.31	2538.5
XSECTION 22	REACH	.02	7	2	.05	.0	4.60	24.00	2.18	5970.50	6.04	50.94	2425.5
XSECTION 22	RUNOFF	.03	7	2	.05	.0	4.60	24.00	3.34	---	5.98	88.27	3395.1
XSECTION 22	ADDHYD	.05	7	2	.05	.0	4.60	24.00	2.82	5970.72	5.99	134.69	2865.7
XSECTION 22	ADDHYD	.62	7	2	.05	.0	4.60	24.00	2.20	5973.25	6.03	1075.75	1726.7
STRUCTURE 20	RESVOR	.62	7	2	.05	.0	4.60	24.00	2.20	5955.24	6.36	429.09	688.8

ALTERNATE 1 STORM 10													
XSECTION 51	RUNOFF	.02	7	2	.05	.0	3.00	24.00	1.34	---	5.99	36.13	1570.9
XSECTION 52	RUNOFF	.04	7	2	.05	.0	3.00	24.00	1.63	---	5.99	64.78	1750.7
XSECTION 52	ADDHYD	.06	7	2	.05	.0	3.00	24.00	1.52	---	5.99	100.88	1681.3
XSECTION 60	RUNOFF	.08	7	2	.05	.0	3.00	24.00	.69	---	6.07	54.98	662.4
XSECTION 62	REACH	.08	7	2	.05	.0	3.00	24.00	.69	6140.43	6.15	50.96	614.0
XSECTION 62	RUNOFF	.05	7	2	.05	.0	3.00	24.00	.65	---	6.05	35.16	663.4

SUMMARY TABLE 1 - SELECTED RESULTS OF STANDARD AND EXECUTIVE CONTROL INSTRUCTIONS IN THE ORDER PERFORMED  
(A STAR(\*) AFTER THE PEAK DISCHARGE TIME AND RATE (CFS) VALUES INDICATES A FLAT TOP HYDROGRAPH  
A QUESTION MARK(?) INDICATES A HYDROGRAPH WITH PEAK AS LAST POINT.)

SECTION/ STRUCTURE ID	STANDARD CONTROL OPERATION	DRAINAGE AREA (SQ MI)	RAIN TABLE #	ANTEC MOIST COND	MAIN TIME INCREM (HR)	PRECIPITATION			RUNOFF AMOUNT (IN)	PEAK DISCHARGE			
						BEGIN (HR)	AMOUNT (IN)	DURATION (HR)		ELEVATION (FT)	TIME (HR)	RATE (CFS)	RATE (CSM)
ALTERNATE 1 STORM 10													
XSECTION 62	ADDHYD	.14	7	2	.05	.0	3.00	24.00	.67	6140.57	6.10	79.70	586.0
XSECTION 64	REACH	.14	7	2	.05	.0	3.00	24.00	.67	5986.51	6.21	68.97	507.1
XSECTION 61	RUNOFF	.17	7	2	.05	.0	3.00	24.00	.68	---	6.10	96.48	584.8

XSECTION	63	REACH	.17	7	2	.05	.0	3.00	24.00	.67	6130.42	6.19	87.72	531.7
XSECTION	63	RUNOFF	.11	7	2	.05	.0	3.00	24.00	1.04	---	6.05	115.37	1039.4
XSECTION	63	ADDHYD	.28	7	2	.05	.0	3.00	24.00	.82	6130.66	6.10	182.05	659.6
XSECTION	64	REACH	.28	7	2	.05	.0	3.00	24.00	.82	5986.74	6.19	168.07	608.9
XSECTION	64	RUNOFF	.07	7	2	.05	.0	3.00	24.00	1.78	---	6.01	131.97	1807.9
XSECTION	64	ADDHYD	.35	7	2	.05	.0	3.00	24.00	1.02	5986.93	6.07	250.48	717.7
XSECTION	64	ADDHYD	.49	7	2	.05	.0	3.00	24.00	.92	5987.05	6.11	301.65	621.9
XSECTION	20	RUNOFF	.03	7	2	.05	.0	3.00	24.00	1.92	---	5.98	63.82	2058.7
XSECTION	64	ADDHYD	.52	7	2	.05	.0	3.00	24.00	.98	5987.13	6.06	336.54	652.2
XSECTION	64	ADDHYD	.58	7	2	.05	.0	3.00	24.00	1.04	5987.34	6.03	427.13	741.5
XSECTION	21	RUNOFF	.02	7	2	.05	.0	3.00	24.00	1.03	---	5.99	26.61	1267.2
XSECTION	22	REACH	.02	7	2	.05	.0	3.00	24.00	1.03	5970.24	6.05	24.27	1155.5
XSECTION	22	RUNOFF	.03	7	2	.05	.0	3.00	24.00	1.92	---	5.98	53.53	2058.7
XSECTION	22	ADDHYD	.05	7	2	.05	.0	3.00	24.00	1.52	5970.56	5.99	74.42	1583.4
XSECTION	22	ADDHYD	.62	7	2	.05	.0	3.00	24.00	1.07	5971.69	6.02	494.64	794.0
STRUCTURE	20	RESVOR	.62	7	2	.05	.0	3.00	24.00	1.07	5952.51	6.50	141.09	226.5

1

TR20 XEQ CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011) JOB 1 SUMMARY  
 REV 09/01/83 FUT. CONDITIONS (FULL DEV., 2 AND 24 HR. STORMS, ST. 20) PAGE 11

SUMMARY TABLE 2 - SELECTED MODIFIED ATT-KIN REACH ROUTINGS IN ORDER OF STANDARD EXECUTIVE CONTROL INSTRUCTIONS  
 (A STAR (\*) AFTER VOLUME ABOVE BASE(IN) INDICATES A HYDROGRAPH TRUNCATED AT A VALUE EXCEEDING BASE + 10% OF PEAK  
 A QUESTION MARK(?) AFTER COEFF.(C) INDICATES PARAMETERS OUTSIDE ACCEPTABLE LIMITS, SEE PREVIOUS WARNINGS)

HYDROGRAPH INFORMATION										ROUTING PARAMETERS					PEAK				
XSEC REACH		INFLOW		OUTFLOW		INTERV. AREA		BASE-	VOLUME	MAIN	ITER-	Q AND A	PEAK	S/Q	ATT-	TRAVEL TIME			
ID	LENGTH (FT)	PEAK (CFS)	TIME (HR)	PEAK (CFS)	TIME (HR)	PEAK (CFS)	TIME (HR)	FLOW (CFS)	BASE (IN)	INCR (HR)	#	COEFF (X)	POWER (M)	FACTOR (K*)	O/I (Q*)	(K) (SEC)	COEFF (C)	AGE (HR)	MATIC (HR)
ALTERNATE		1	STORM	99															
62	2400	135	6.1	129	6.2			0	1.66	.05	1	3.21	1.40	.045	.957	183	.66	.10	.05
						207	6.1												
64	2400	207	6.1	193	6.2			0	1.63	.05	1	.919	1.54	.059	.934	257	.52	.05	.07
						---	---												
63	2700	243	6.1	234	6.2			0	1.64	.05	1	1.39	1.56	.036	.963	195	.63	.05	.05
						442	6.1												
64	2400	442	6.1	426	6.2			0	1.86	.05	1	.919	1.54	.035	.964	197	.63	.05	.06
						571	6.1												
22	1700	53	6.0	51	6.1			0	2.19	.05	1	1.80	1.52	.054	.965	195	.63	.05	.05
						134	6.0												
ALTERNATE		1	STORM	10															
62	2400	54	6.1	51	6.2			0	.69	.05	1	3.21	1.40	.061	.942	238	.55	.10	.07
						80	6.1												
64	2400	80	6.1	69	6.2			0	.67	.05	1	.919	1.54	.089	.864	358	.40	.10	.10
						---	---												
63	2700	96	6.1	88	6.2			0	.68	.05	1	1.39	1.56	.056	.909	272	.50	.10	.08
						182	6.1												
64	2400	182	6.1	168	6.2			0	.82	.05	1	.919	1.54	.050	.922	268	.50	.10	.08
						248	6.1												
22	1700	26	6.0	24	6.1			0	1.03	.05	1	1.80	1.52	.084	.917	247	.53	.05	.07
						74	6.0												

1



SUMMARY TABLE 3 - DISCHARGE (CFS) AT XSECTIONS AND STRUCTURES FOR ALL STORMS AND ALTERNATES

XSECTION/ STRUCTURE ID	DRAINAGE AREA (SQ MI)	STORM NUMBERS.....	
		10	99
0 STRUCTURE 20	.62		
+			
ALTERNATE 1		141.09	429.09
0 XSECTION 20	.03		
+			
ALTERNATE 1		63.82	105.25
0 XSECTION 21	.02		
+			
ALTERNATE 1		26.61	53.31
0 XSECTION 22	.62		
+			
ALTERNATE 1		494.64	1075.75
0 XSECTION 51	.02		
+			
ALTERNATE 1		36.13	66.64
0 XSECTION 52	.06		
+			
ALTERNATE 1		100.88	180.04
0 XSECTION 60	.08		
+			
ALTERNATE 1		54.98	135.33
0 XSECTION 61	.17		
+			
ALTERNATE 1		96.48	244.04
0 XSECTION 62	.14		
+			
ALTERNATE 1		79.70	207.95
0 XSECTION 63	.28		
+			
ALTERNATE 1		182.05	443.11
0 XSECTION 64	.58		
+			
ALTERNATE 1		427.13	950.93

1END OF 1 JOBS IN THIS RUN

**TR-20 PRINTOUT  
DEVELOPED CONDITIONS  
DETENTION POND NO. 2**

\*\*\*\*\*80-80 LIST OF INPUT DATA FOR TR-20 HYDROLOGY\*\*\*\*\*

JOB TR-20		SUMMARY NOPLOTS			
TITLE CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)					
TITLE FUT. COND. (FULL DEV., 10 AND 100 YR. STORMS, ST.80)					
5	RAINFL 7	0.2500			
8		0.0000	0.0005	0.0015	0.0030
8		0.0060	0.0080	0.0100	0.0120
8		0.0165	0.0188	0.0210	0.0233
8		0.0278	0.0320	0.0390	0.0460
8		0.0600	0.0750	0.1000	0.4000
8		0.7250	0.7500	0.7650	0.7800
8		0.8000	0.8100	0.8200	0.8250
8		0.8350	0.8400	0.8450	0.8500
8		0.8600	0.8638	0.8675	0.8713
8		0.8788	0.8825	0.8863	0.8900
8		0.8975	0.9013	0.9050	0.9083
8		0.9148	0.9180	0.9210	0.9240
8		0.9300	0.9325	0.9350	0.9375
8		0.9425	0.9450	0.9475	0.9500
8		0.9550	0.9575	0.9600	0.9625
8		0.9675	0.9700	0.9725	0.9750
8		0.9800	0.9813	0.9825	0.9838
8		0.9863	0.9875	0.9888	0.9900
8		0.9925	0.9938	0.9950	0.9963
8		0.9988	1.0000	1.0000	1.0000
9	ENDTBL				
5	RAINFL 8	0.08333			
8		0.000	0.020	0.057	0.139
8		0.539	0.659	0.715	0.758
8		0.828	0.860	0.892	0.924
8		0.988	1.013	1.032	1.051
8		1.089	1.108	1.127	1.144
9	ENDTBL				
5	RAINFL 9	0.08333			
8		0.000	0.010	0.040	0.086
8		0.306	0.556	0.696	0.776
8		0.888	0.928	0.968	1.008
8		1.048	1.060	1.072	1.084
8		1.108	1.120	1.132	1.144
9	ENDTBL				
3	STRUCT 80				
8		5960.	0.0	0.0	
8		5965.	180.	4.4	
8		5967.5	254.	7.8	
8		5970.	311.	11.9	
8		5972.5	359.	17.1	
8		5975.	402.	23.9	

\*\*\*\*\*80-80 LIST OF INPUT DATA (CONTINUED)\*\*\*\*\*

8		5977.5	440.	32.3
8		5980.	1280.	42.1
8		5982.5	1380.	53.1
9	ENDTBL			
3	STRUCT 81			
9	ENDTBL			
2	XSECTN 161	1.0		
8		6190.	0.0	0.0
8		6190.5	127.	16.
8		6192.	1385.	76.
9	ENDTBL			
2	XSECTN 162	1.0		
8		6050.	0.0	0.0
8		6051.	311.	34.
8		6052.	1044.	76.
8		6053.	2174.	126.
8		6054.	3722.	184.
9	ENDTBL			
2	XSECTN 163	1.0		
8		5980.	0.0	0.0
8		5981.	212.	34.
8		5982.	712.	76.
8		5984.	2537.	184.

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9 ENDTBL
2 XSECTN 165      1.0
8              6010.    0.0    0.0
8              6011.    313.    34.
8              6012.   1051.    76.
8              6014.   3748.   184.
9 ENDTBL
6 RUNOFF 1 160      6 0.593    70.2    0.58
6 REACH  3 161      6 5 1100.
6 RUNOFF 1 161      6 0.054    74.4    0.10
6 ADDHYD 4 161      5 6 7
6 REACH  3 162      7 5 1700.
6 RUNOFF 1 162      6 0.058    77.9    0.16
6 ADDHYD 4 162      5 6 7
6 REACH  3 163      7 5 900.
6 RUNOFF 1 163      6 0.015    90.7    0.10
6 ADDHYD 4 163      5 6 4
6 RUNOFF 1 164      6 0.970    74.5    0.66
6 REACH  3 165      6 5 3200.
6 RUNOFF 1 165      6 0.079    82.1    0.24
6 ADDHYD 4 165      5 6 7
6 ADDHYD 4 165      4 7 6
6 RESVOR 2 80 6 4 5960.

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1

\*\*\*\*\*80-80 LIST OF INPUT DATA (CONTINUED)\*\*\*\*\*

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ENDATA
7 INCREM 6          0.05
7 COMPUT 7 160      80 0.0      4.6      1.0      7 2 01 99
ENDCMP 1
7 COMPUT 7 160      80 0.0      3.0      1.0      7 2 01 10
ENDCMP 1
ENDJOB 2

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0\*\*\*\*\*END OF 80-80 LIST\*\*\*\*\*  
1

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TR20 XEQ          CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)          JOB 1  PASS 1
REV 09/01/83     FUT. COND. (FULL DEV., 10 AND 100 YR. STORMS, ST.80)                    PAGE 1

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COMPUTER PROGRAM FOR PROJECT FORMULATION - HYDROLOGY USER NOTES

THE USERS MANUAL FOR THIS PROGRAM IS THE MAY 1982 DRAFT OF TR-20. CHANGES FROM THE 2/14/74 VERSION INCLUDE:

REACH ROUTING - THE MODIFIED ATT-KIN ROUTING PROCEDURE REPLACES THE CONVEX METHOD. INPUT DATA PREPARED FOR PREVIOUS PROGRAM VERSIONS USING CONVEX ROUTING COEFFICIENTS WILL NOT RUN ON THIS VERSION.

THE PREFERRED TYPE OF DATA ENTRY IS CROSS SECTION DATA REPRESENTATIVE OF A REACH. IT IS RECOMMENDED THAT THE OPTIONAL CROSS SECTION DISCHARGE-AREA PLOTS BE OBTAINED WHENEVER NEW CROSS SECTION DATA IS ENTERED. THE PLOTS SHOULD BE CHECKED FOR REASONABLENESS AND ADEQUACY OF INPUT DATA FOR THE COMPUTATION OF "M" VALUES USED IN THE ROUTING PROCEDURE.

GUIDELINES FOR DETERMINING OR ANALYZING REACH LENGTHS AND COEFFICIENTS (X,M) ARE AVAILABLE IN THE USERS MANUAL. SUMMARY TABLE 2 DISPLAYS REACH ROUTING RESULTS AND ROUTING PARAMETERS FOR COMPARISON AND CHECKING.

HYDROGRAPH GENERATION - THE PROCEDURE TO CALCULATE THE INTERNAL TIME INCREMENT AND PEAK TIME OF THE UNIT HYDROGRAPH HAVE BEEN IMPROVED. PEAK DISCHARGES AND TIMES MAY DIFFER FROM THE PREVIOUS VERSION. OUTPUT HYDROGRAPHS ARE STILL INTERPOLATED, PRINTED, AND ROUTED AT THE USER SELECTED MAIN TIME INCREMENT.

INTERMEDIATE PEAKS - METHOD ADDED TO PROVIDE DISCHARGES AT INTERMEDIATE POINTS WITHIN REACHES WITHOUT ROUTING.

OTHER - THIS VERSION CONTAINS SOME ADDITIONS TO THE INPUT AND NUMEROUS MODIFICATIONS TO THE OUTPUT. USER OPTIONS HAVE BEEN MODIFIED AND AUGMENTED ON THE JOB RECORD, RAIN TABLES ADDED, ERROR AND WARNING MESSAGES EXPANDED, AND THE SUMMARY TABLES COMPLETELY REVISED. THE HOLDOUT OPTION IS NOT OPERATIONAL AT THIS TIME.

PROGRAM QUESTIONS OR PROBLEMS SHOULD BE DIRECTED TO HYDRAULIC ENGINEERS AT THE SCS NATIONAL TECHNICAL CENTERS:

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CHESTER, PA (NORTHEAST) -- 215-499-3933,          FORT WORTH, TX (SOUTH) -- 334-5242 (FTS)
LINCOLN, NB (MIDWEST)   -- 541-5318 (FTS),       PORTLAND, OR (WEST)    -- 423-4099 (FTS)
OR HYDROLOGY UNIT, ENGINEERING DIVISION, LANHAM, MD -- 436-7383 (FTS).

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PROGRAM CHANGES SINCE MAY 1982:

12/17/82 - CORRECT PEAK RATE FACTOR FOR USER ENTERED DIMHYD  
CORRECT REACH ROUTING PEAK TRAVEL TIME PRINTED WITH FULLPRINT OPTION

5/02/83 - CORRECT COMPUTATIONS FOR ---

1. DIVISION OF BASEFLOW IN DIVERT OPERATION
2. HYDROGRAPH VOLUME SPLIT BETWEEN BASEFLOW AND ABOVE BASEFLOW
3. CROSS SECTION DATA PLOTTING POSITION
4. INTERMEDIATE PEAK WHEN "FROM" AREA IS LARGER THAN "THRU" AREA
5. STORAGE ROUTED REACH TRAVEL TIME FOR MULTYPEAK HYDROGRAPH
6. ORDERING "FLOW-FREQ" FILE FROM SUMMARY TABLE #3 DATA
7. BASEFLOW ENTERED WITH READHYD
8. LOW FLOW SPLIT DURING DIVERT PROCEDURE #2 WHEN SECTION RATINGS START AT DIFFERENT ELEVATIONS

ENHANCEMENTS ---

1. REPLACE USER MANUAL ERROR CODES (PAGE 4-9 TO 4-11) WITH MESSAGES
2. LABEL OUTPUT HYDROGRAPH FILES WITH CROSS SECTION/STRUCTURE, ALTERNATE AND STORM NO'S

09/01/83 - CORRECT INPUT AND OUTPUT ERRORS FOR INTERMEDIATE PEAKS  
 CORRECT COMBINATION OF RATING TABLES FOR DIVERT  
 CHECK REACH ROUTING PARAMETERS FOR ACCEPTABLE LIMITS  
 ELIMINATE MINIMUM REACH TRAVEL TIME WHEN ATT-KIN COEFFICIENT EQUALS ONE

1

TR20 XEQ  
 REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
 FUT. COND. (FULL DEV., 10 AND 100 YR. STORMS, ST.80)

JOB 1 PASS 1  
 PAGE 2

CUMULATIVE RAINFALL TABLE 7                      TIME INCREMENT= .25

8	.0000	.0005	.0015	.0030	.0045
8	.0060	.0080	.0100	.0120	.0143
8	.0165	.0188	.0210	.0233	.0255
8	.0278	.0320	.0390	.0460	.0530
8	.0600	.0750	.1000	.4000	.7000
8	.7250	.7500	.7650	.7800	.7900
8	.8000	.8100	.8200	.8250	.8300
8	.8350	.8400	.8450	.8500	.8550
8	.8600	.8638	.8675	.8713	.8750
8	.8788	.8825	.8863	.8900	.8938
8	.8975	.9013	.9050	.9083	.9115
8	.9148	.9180	.9210	.9240	.9270
8	.9300	.9325	.9350	.9375	.9400
8	.9425	.9450	.9475	.9500	.9525
8	.9550	.9575	.9600	.9625	.9650
8	.9675	.9700	.9725	.9750	.9775
8	.9800	.9813	.9825	.9838	.9850
8	.9863	.9875	.9888	.9900	.9913
8	.9925	.9938	.9950	.9963	.9975
8	.9988	1.0000	1.0000	1.0000	1.0000

9 ENDTBL

CUMULATIVE RAINFALL TABLE 8                      TIME INCREMENT= .08

8	.0000	.0200	.0570	.1390	.2890
8	.5390	.6590	.7150	.7580	.7960
8	.8280	.8600	.8920	.9240	.9560
8	.9880	1.0130	1.0320	1.0510	1.0700
8	1.0890	1.1080	1.1270	1.1440	1.1570

9 ENDTBL

CUMULATIVE RAINFALL TABLE 9                      TIME INCREMENT= .08

8	.0000	.0100	.0400	.0860	.1660
8	.3060	.5560	.6960	.7760	.8380
8	.8880	.9280	.9680	1.0080	1.0280
8	1.0480	1.0600	1.0720	1.0840	1.0960
8	1.1080	1.1200	1.1320	1.1440	1.1560

9 ENDTBL

1

TR20 XEQ  
 REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
 FUT. COND. (FULL DEV., 10 AND 100 YR. STORMS, ST.80)

JOB 1 PASS 1  
 PAGE 3

STRUCTURE DATA, STRUCTURE NO. 80

	ELEVATION	DISCHARGE	STORAGE
8	5960.00	.00	.00
8	5965.00	180.00	4.40
8	5967.50	254.00	7.80
8	5970.00	311.00	11.90
8	5972.50	359.00	17.10
8	5975.00	402.00	23.90
8	5977.50	440.00	32.30
8	5980.00	1280.00	42.10
8	5982.50	1380.00	53.10

9 ENDTBL

STRUCTURE DATA, STRUCTURE NO. 81

ELEVATION DISCHARGE STORAGE

9 ENDTBL

CROSS-SECTION DATA, CROSS-SECTION NO. 161 DRAINAGE AREA= 1.00 BANKFULL ELEV.= .00

	ELEVATION	DISCHARGE	END AREA
8	6190.00	.00	.00
8	6190.50	127.00	16.00
8	6192.00	1385.00	76.00

9 ENDTBL

CROSS-SECTION DATA, CROSS-SECTION NO. 162 DRAINAGE AREA= 1.00 BANKFULL ELEV.= .00

	ELEVATION	DISCHARGE	END AREA
8	6050.00	.00	.00
8	6051.00	311.00	34.00
8	6052.00	1044.00	76.00
8	6053.00	2174.00	126.00
8	6054.00	3722.00	184.00

9 ENDTBL

CROSS-SECTION DATA, CROSS-SECTION NO. 163 DRAINAGE AREA= 1.00 BANKFULL ELEV.= .00

	ELEVATION	DISCHARGE	END AREA
8	5980.00	.00	.00
8	5981.00	212.00	34.00
8	5982.00	712.00	76.00

1

TR20 XEQ  
REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
FUT. COND. (FULL DEV., 10 AND 100 YR. STORMS, ST.80)

JOB 1 PASS 1  
PAGE 4

8	5984.00	2537.00	184.00
---	---------	---------	--------

9 ENDTBL

CROSS-SECTION DATA, CROSS-SECTION NO. 165 DRAINAGE AREA= 1.00 BANKFULL ELEV.= .00

	ELEVATION	DISCHARGE	END AREA
8	6010.00	.00	.00
8	6011.00	313.00	34.00
8	6012.00	1051.00	76.00
8	6014.00	3748.00	184.00

9 ENDTBL

STANDARD CONTROL OPERATION RUNOFF CROSS SECTION 160  
OUTPUT HYDROGRAPH = 6  
OUTPUT OPTIONS IN EFFECT SUM

DATA FIELD VALUES = .5930 RECORD ID 70.2000 .5800

STANDARD CONTROL OPERATION REACH CROSS SECTION 161  
INPUT HYDROGRAPH = 6 OUTPUT HYDROGRAPH = 5  
OUTPUT OPTIONS IN EFFECT SUM

DATA FIELD VALUES = 1100.0000 RECORD ID .0000 .0000

STANDARD CONTROL OPERATION RUNOFF CROSS SECTION 161  
OUTPUT HYDROGRAPH = 6  
OUTPUT OPTIONS IN EFFECT SUM

DATA FIELD VALUES = .0540 RECORD ID 74.4000 .1000

STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 161		RECORD ID
INPUT HYDROGRAPHS = 5,6	OUTPUT HYDROGRAPH = 7	DATA FIELD VALUES = .0000	.0000 .0000
OUTPUT OPTIONS IN EFFECT	SUM		
STANDARD CONTROL OPERATION REACH	CROSS SECTION 162		RECORD ID
INPUT HYDROGRAPH = 7	OUTPUT HYDROGRAPH = 5	DATA FIELD VALUES = 1700.0000	.0000 .0000
OUTPUT OPTIONS IN EFFECT	SUM		
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 162		RECORD ID
OUTPUT HYDROGRAPH = 6		DATA FIELD VALUES = .0580	77.9000 .1600
OUTPUT OPTIONS IN EFFECT	SUM		
STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 162		RECORD ID
INPUT HYDROGRAPHS = 5,6	OUTPUT HYDROGRAPH = 7	DATA FIELD VALUES = .0000	.0000 .0000
OUTPUT OPTIONS IN EFFECT	SUM		
STANDARD CONTROL OPERATION REACH	CROSS SECTION 163		RECORD ID
INPUT HYDROGRAPH = 7	OUTPUT HYDROGRAPH = 5	DATA FIELD VALUES = 900.0000	.0000 .0000
OUTPUT OPTIONS IN EFFECT	SUM		
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 163		RECORD ID
OUTPUT HYDROGRAPH = 6		DATA FIELD VALUES = .0150	90.7000 .1000
OUTPUT OPTIONS IN EFFECT	SUM		

1

TR20 XEQ	CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)	JOB 1	PASS 1
REV 09/01/83	FUT. COND. (FULL DEV., 10 AND 100 YR. STORMS, ST.80)		PAGE 5

STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 163		RECORD ID
INPUT HYDROGRAPHS = 5,6	OUTPUT HYDROGRAPH = 4	DATA FIELD VALUES = .0000	.0000 .0000
OUTPUT OPTIONS IN EFFECT	SUM		
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 164		RECORD ID
OUTPUT HYDROGRAPH = 6		DATA FIELD VALUES = .9700	74.5000 .6600
OUTPUT OPTIONS IN EFFECT	SUM		
STANDARD CONTROL OPERATION REACH	CROSS SECTION 165		RECORD ID
INPUT HYDROGRAPH = 6	OUTPUT HYDROGRAPH = 5	DATA FIELD VALUES = 3200.0000	.0000 .0000
OUTPUT OPTIONS IN EFFECT	SUM		
STANDARD CONTROL OPERATION RUNOFF	CROSS SECTION 165		RECORD ID
OUTPUT HYDROGRAPH = 6		DATA FIELD VALUES = .0790	82.1000 .2400
OUTPUT OPTIONS IN EFFECT	SUM		
STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 165		RECORD ID
INPUT HYDROGRAPHS = 5,6	OUTPUT HYDROGRAPH = 7	DATA FIELD VALUES = .0000	.0000 .0000
OUTPUT OPTIONS IN EFFECT	SUM		
STANDARD CONTROL OPERATION ADDHYD	CROSS SECTION 165		RECORD ID
INPUT HYDROGRAPHS = 4,7	OUTPUT HYDROGRAPH = 6	DATA FIELD VALUES = .0000	.0000 .0000
OUTPUT OPTIONS IN EFFECT	PEAK HYD VOL SUM		
STANDARD CONTROL OPERATION RESVOR	STRUCTURE 80		RECORD ID
INPUT HYDROGRAPH = 6	OUTPUT HYDROGRAPH = 4	DATA FIELD VALUES = 5960.0000	.0000 .0000
OUTPUT OPTIONS IN EFFECT	SUM		

EXECUTIVE CONTROL OPERATION INCREM		RECORD ID
+	MAIN TIME INCREMENT = .05 HOURS	

EXECUTIVE CONTROL OPERATION COMPUT		RECORD ID		
+	FROM XSECTION 160			
+	TO STRUCTURE 80			
STARTING TIME = .00	RAIN DEPTH = 4.60	RAIN DURATION = 1.00	RAIN TABLE NO. = 7	ANT. MOIST. COND = 2
ALTERNATE NO. = 1	STORM NO. = 99	MAIN TIME INCREMENT = .05 HOURS		

\*\*\* WARNING REACH 161 ATT-KIN COEFF.(C) GREATER THAN 0.667, CONSIDER REDUCING MAIN TIME INCREMENT \*\*\*

\*\*\* WARNING REACH 162 ATT-KIN COEFF.(C) GREATER THAN 0.667, CONSIDER REDUCING MAIN TIME INCREMENT \*\*\*

\*\*\* WARNING REACH 163 ATT-KIN COEFF.(C) GREATER THAN 0.667, CONSIDER REDUCING MAIN TIME INCREMENT \*\*\*

\*\*\* WARNING REACH 165 ATT-KIN COEFF.(C) GREATER THAN 0.667, CONSIDER REDUCING MAIN TIME INCREMENT \*\*\*

OPERATION ADDHYD CROSS SECTION 165

TR20 XEQ  
REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
FUT. COND. (FULL DEV., 10 AND 100 YR. STORMS, ST.80)

JOB 1 PASS 1  
PAGE 6

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.32	1668.28	6012.46
9.98	75.57	6010.24
12.99	57.95	6010.19

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .05 HOURS	DRAINAGE AREA = 1.77 SQ.MI.
4.50	DISCHG .00 .01 .02 .04 .05 .07 .08 .09 .11 .12		
5.00	DISCHG .14 .20 .32 .40 .47 .52 .69 .97 1.16 1.30		
5.50	DISCHG 1.51 9.11 34.58 80.97 154.52 245.33 347.91 467.41 612.49 788.74		
6.00	DISCHG 995.53 1197.07 1319.42 1402.04 1511.00 1609.69 1663.33 1658.00 1598.29 1498.13		
6.50	DISCHG 1372.42 1233.80 1092.05 958.33 841.93 744.36 663.65 595.21 536.38 485.66		
7.00	DISCHG 441.66 403.15 368.58 338.09 312.64 291.02 272.09 255.13 239.83 226.03		
7.50	DISCHG 213.67 202.73 193.17 184.99 178.08 172.31 167.53 163.60 160.36 157.71		
8.00	DISCHG 155.55 153.09 149.06 144.31 140.37 136.57 132.31 127.34 121.85 116.09		
8.50	DISCHG 110.36 104.91 99.91 95.52 91.79 88.72 86.23 84.21 82.55 81.20		
9.00	DISCHG 80.08 79.17 78.42 77.81 77.31 76.91 76.59 76.33 76.13 75.97		
9.50	DISCHG 75.84 75.74 75.66 75.61 75.57 75.54 75.53 75.52 75.53 75.54		
10.00	DISCHG 75.55 75.41 74.80 73.95 73.21 72.44 71.48 70.30 68.95 67.53		
10.50	DISCHG 66.11 64.76 63.53 62.45 61.51 60.74 60.10 59.57 59.13 58.78		
11.00	DISCHG 58.51 58.29 58.14 58.02 57.91 57.81 57.73 57.65 57.58 57.54		
11.50	DISCHG 57.52 57.51 57.53 57.55 57.56 57.56 57.56 57.54 57.53 57.54		
12.00	DISCHG 57.55 57.57 57.62 57.67 57.69 57.71 57.72 57.72 57.71 57.72		
12.50	DISCHG 57.75 57.77 57.82 57.87 57.90 57.91 57.93 57.92 57.91 57.93		
13.00	DISCHG 57.95 57.91 57.69 57.37 57.07 56.74 56.34 55.83 55.26 54.68		
13.50	DISCHG 54.11 53.57 53.09 52.68 52.32 52.01 51.76 51.53 51.34 51.21		
14.00	DISCHG 51.10 50.98 50.78 50.53 50.30 50.06 49.79 49.50 49.20 48.90		
14.50	DISCHG 48.61 48.34 48.11 47.90 47.73 47.59 47.47 47.38 47.31 47.25		

RUNOFF VOLUME ABOVE BASEFLOW = 1.76 WATERSHED INCHES, 2009.81 CFS-HRS, 166.09 ACRE-FEET; BASEFLOW = .00 CFS

EXECUTIVE CONTROL OPERATION ENDCMP

RECORD ID

COMPUTATIONS COMPLETED FOR PASS 1

EXECUTIVE CONTROL OPERATION COMPUT

RECORD ID

FROM XSECTION 160

TO STRUCTURE 80

STARTING TIME = .00 RAIN DEPTH = 3.00 RAIN DURATION = 1.00 RAIN TABLE NO. = 7 ANT. MOIST. COND = 2  
ALTERNATE NO. = 1 STORM NO. = 10 MAIN TIME INCREMENT = .05 HOURS

\*\*\* WARNING REACH 161 ATT-KIN COEFF. (C) GREATER THAN 0.667, CONSIDER REDUCING MAIN TIME INCREMENT \*\*\*

\*\*\*WARNING - LACK OF LOW FLOW DEFINITION FOR XSECT TABLE162. MAX.FLOW LESS THAN 2ND TABLE VALUE.

\*\*\* WARNING REACH 162 ATT-KIN COEFF. (C) GREATER THAN 0.667, CONSIDER REDUCING MAIN TIME INCREMENT \*\*\*

\*\*\* WARNING REACH 163 ATT-KIN COEFF. (C) GREATER THAN 0.667, CONSIDER REDUCING MAIN TIME INCREMENT \*\*\*

TR20 XEQ  
REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
FUT. COND. (FULL DEV., 10 AND 100 YR. STORMS, ST.80)

JOB 1 PASS 2  
PAGE 7

OPERATION ADDHYD CROSS SECTION 165

PEAK TIME (HRS)	PEAK DISCHARGE (CFS)	PEAK ELEVATION (FEET)
6.39	646.55	6011.45
9.99	38.53	6010.12
13.02	29.99	6010.10

TIME (HRS)	FIRST HYDROGRAPH POINT = .00 HOURS	TIME INCREMENT = .05 HOURS	DRAINAGE AREA = 1.77 SQ.MI.
5.00	DISCHG .00 .00 .00 .00 .00 .02 .07 .14 .22 .29		
5.50	DISCHG .38 2.59 9.65 19.50 34.09 57.61 91.92 135.14 185.44 244.69		
6.00	DISCHG 315.49 389.10 450.86 492.90 522.40 567.04 612.20 640.71 645.76 628.98		
6.50	DISCHG 594.95 549.00 496.73 442.38 391.02 347.22 311.11 280.75 254.67 231.98		



7.00	DISCHG	212.14	194.68	179.21	165.26	152.89	142.58	133.80	126.02	118.98	112.54
7.50	DISCHG	106.71	101.47	96.85	92.84	89.43	86.58	84.22	82.28	80.66	79.32
8.00	DISCHG	78.23	77.12	75.67	73.66	71.38	69.41	67.49	65.30	62.79	60.06
8.50	DISCHG	57.24	54.47	51.86	49.48	47.42	45.70	44.30	43.17	42.24	41.49
9.00	DISCHG	40.87	40.36	39.95	39.62	39.35	39.13	38.96	38.83	38.72	38.64
9.50	DISCHG	38.58	38.54	38.51	38.49	38.47	38.47	38.47	38.48	38.49	38.51
10.00	DISCHG	38.53	38.49	38.33	38.00	37.56	37.17	36.75	36.24	35.63	34.94
10.50	DISCHG	34.23	33.54	32.88	32.29	31.78	31.35	30.99	30.69	30.45	30.24
11.00	DISCHG	30.09	29.97	29.88	29.81	29.77	29.72	29.68	29.65	29.61	29.59
11.50	DISCHG	29.58	29.58	29.59	29.60	29.62	29.64	29.64	29.64	29.64	29.64
12.00	DISCHG	29.65	29.67	29.69	29.72	29.75	29.78	29.79	29.80	29.80	29.80
12.50	DISCHG	29.82	29.84	29.86	29.90	29.93	29.95	29.96	29.97	29.97	29.98
13.00	DISCHG	29.99	29.99	29.93	29.81	29.64	29.48	29.30	29.09	28.82	28.53
13.50	DISCHG	28.24	27.96	27.70	27.47	27.28	27.10	26.96	26.84	26.74	26.65
14.00	DISCHG	26.59	26.53	26.46	26.35	26.23	26.11	25.98	25.84	25.70	25.55
14.50	DISCHG	25.40	25.26	25.13	25.02	24.92	24.84	24.78	24.73	24.69	24.66

RUNOFF VOLUME ABOVE BASEFLOW = .76 WATERSHED INCHES, 864.54 CFS-HRS, 71.45 ACRE-FEET; BASEFLOW = .00 CFS

EXECUTIVE CONTROL OPERATION ENDCMP

COMPUTATIONS COMPLETED FOR PASS 2

RECORD ID

EXECUTIVE CONTROL OPERATION ENDJOB

RECORD ID

TR20 XEQ  
REV 09/01/83

CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011)  
FUT. COND. (FULL DEV., 10 AND 100 YR. STORMS, ST.80)

JOB 1 SUMMARY  
PAGE 8

SUMMARY TABLE 1 - SELECTED RESULTS OF STANDARD AND EXECUTIVE CONTROL INSTRUCTIONS IN THE ORDER PERFORMED  
(A STAR(\*) AFTER THE PEAK DISCHARGE TIME AND RATE (CFS) VALUES INDICATES A FLAT TOP HYDROGRAPH  
A QUESTION MARK(?) INDICATES A HYDROGRAPH WITH PEAK AS LAST POINT.)

SECTION/ STRUCTURE ID	STANDARD CONTROL OPERATION	DRAINAGE AREA (SQ MI)	RAIN TABLE #	ANTEC MOIST COND	MAIN TIME INCREM (HR)	PRECIPITATION			RUNOFF AMOUNT (IN)	PEAK DISCHARGE			
						BEGIN (HR)	AMOUNT (IN)	DURATION (HR)		ELEVATION (FT)	TIME (HR)	RATE (CFS)	RATE (CSM)
ALTERNATE 1 STORM 99													
XSECTION 160	RUNOFF	.59	7	2	.05	.0	4.60	24.00	1.51	---	6.24	567.45	956.9
XSECTION 161	REACH	.59	7	2	.05	.0	4.60	24.00	1.51	6191.03	6.24	567.45	956.9
XSECTION 161	RUNOFF	.05	7	2	.05	.0	4.60	24.00	1.83	---	5.99	118.46	2193.7
XSECTION 161	ADDHYD	.65	7	2	.05	.0	4.60	24.00	1.54	6191.04	6.24	579.04	895.0
XSECTION 162	REACH	.65	7	2	.05	.0	4.60	24.00	1.53	6051.36	6.29	578.26	893.8
XSECTION 162	RUNOFF	.06	7	2	.05	.0	4.60	24.00	2.09	---	6.01	131.87	2273.7
XSECTION 162	ADDHYD	.71	7	2	.05	.0	4.60	24.00	1.58	6051.39	6.29	595.35	844.5
XSECTION 163	REACH	.71	7	2	.05	.0	4.60	24.00	1.58	5981.77	6.29	595.35	844.5
XSECTION 163	RUNOFF	.01	7	2	.05	.0	4.60	24.00	3.25	---	5.98	50.17	3344.3
XSECTION 163	ADDHYD	.72	7	2	.05	.0	4.60	24.00	1.62	5981.78	6.29	599.59	832.8
XSECTION 164	RUNOFF	.97	7	2	.05	.0	4.60	24.00	1.82	---	6.28	1051.79	1084.3
XSECTION 165	REACH	.97	7	2	.05	.0	4.60	24.00	1.81	6011.99	6.35	1042.06	1074.3
XSECTION 165	RUNOFF	.08	7	2	.05	.0	4.60	24.00	2.44	---	6.03	191.19	2420.1
XSECTION 165	ADDHYD	1.05	7	2	.05	.0	4.60	24.00	1.86	6012.02	6.34	1077.25	1026.9
XSECTION 165	ADDHYD	1.77	7	2	.05	.0	4.60	24.00	1.76	6012.46	6.32	1668.28	943.1
STRUCTURE 80	RESVOR	1.77	7	2	.05	.0	4.60	24.00	1.75	5980.14	6.53	1285.70	726.8
ALTERNATE 1 STORM 10													
XSECTION 160	RUNOFF	.59	7	2	.05	.0	3.00	24.00	.60	---	6.27	202.68	341.8
XSECTION 161	REACH	.59	7	2	.05	.0	3.00	24.00	.60	6190.59	6.27	202.68	341.8
XSECTION 161	RUNOFF	.05	7	2	.05	.0	3.00	24.00	.79	---	5.99	54.04	1000.7
XSECTION 161	ADDHYD	.65	7	2	.05	.0	3.00	24.00	.61	6190.60	6.27	208.09	321.6
XSECTION 162	REACH	.65	7	2	.05	.0	3.00	24.00	.61	6050.66	6.34	206.11	318.6
XSECTION 162	RUNOFF	.06	7	2	.05	.0	3.00	24.00	.97	---	6.02	63.18	1089.2
XSECTION 162	ADDHYD	.71	7	2	.05	.0	3.00	24.00	.64	6050.69	6.33	213.82	303.3
XSECTION 163	REACH	.71	7	2	.05	.0	3.00	24.00	.64	5981.00	6.38	213.69	303.1
XSECTION 163	RUNOFF	.01	7	2	.05	.0	3.00	24.00	1.85	---	5.98	30.06	2003.9
XSECTION 163	ADDHYD	.72	7	2	.05	.0	3.00	24.00	.67	5981.01	6.38	216.25	300.4

XSECTION 164	RUNOFF	.97	7	2	.05	.0	3.00	24.00	.79	---	6.31	423.91	437.0
XSECTION 165	REACH	.97	7	2	.05	.0	3.00	24.00	.79	6011.14	6.40	414.51	427.3
XSECTION 165	RUNOFF	.08	7	2	.05	.0	3.00	24.00	1.21	---	6.04	96.89	1226.5
XSECTION 165	ADDHYD	1.05	7	2	.05	.0	3.00	24.00	.82	6011.16	6.39	430.31	410.2
XSECTION 165	ADDHYD	1.77	7	2	.05	.0	3.00	24.00	.76	6011.45	6.39	646.55	365.5

1

TR20 XEQ CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011) JOB 1 SUMMARY  
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SUMMARY TABLE 1 - SELECTED RESULTS OF STANDARD AND EXECUTIVE CONTROL INSTRUCTIONS IN THE ORDER PERFORMED  
 (A STAR(\*) AFTER THE PEAK DISCHARGE TIME AND RATE (CFS) VALUES INDICATES A FLAT TOP HYDROGRAPH  
 A QUESTION MARK(?) INDICATES A HYDROGRAPH WITH PEAK AS LAST POINT.)

SECTION/ STRUCTURE ID	STANDARD CONTROL OPERATION	DRAINAGE AREA (SQ MI)	RAIN TABLE #	ANTEC MOIST COND	MAIN TIME INCREM (HR)	PRECIPITATION			RUNOFF AMOUNT (IN)	PEAK DISCHARGE			
						BEGIN (HR)	AMOUNT (IN)	DURATION (HR)		ELEVATION (FT)	TIME (HR)	RATE (CFS)	RATE (CSM)
ALTERNATE	1	STORM	10										
+ STRUCTURE 80	RESVOR	1.77	7	2	.05	.0	3.00	24.00	.75	5972.54	6.74	359.77	203.4

1

TR20 XEQ CHEYENNE MOUNTAIN RANCH DRAINAGE STUDY (DREXEL BARRELL JN EW-1011) JOB 1 SUMMARY  
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SUMMARY TABLE 2 - SELECTED MODIFIED ATT-KIN REACH ROUTINGS IN ORDER OF STANDARD EXECUTIVE CONTROL INSTRUCTIONS  
 (A STAR(\*) AFTER VOLUME ABOVE BASE(IN) INDICATES A HYDROGRAPH TRUNCATED AT A VALUE EXCEEDING BASE + 10% OF PEAK  
 A QUESTION MARK(?) AFTER COEFF. (C) INDICATES PARAMETERS OUTSIDE ACCEPTABLE LIMITS, SEE PREVIOUS WARNINGS)

HYDROGRAPH INFORMATION										ROUTING PARAMETERS					PEAK				
XSEC ID	REACH LENGTH (FT)	INFLOW		OUTFLOW		INTERV. AREA		BASE- FLOW (CFS)	VOLUME ABOVE (IN)	MAIN TIME (HR)	ITER- ATION #	Q AND A EQUATION		PEAK RATIO (Q*)	S/Q (K)	ATT- KIN COEFF (C)	TRAVEL TIME STOR- KINE- (HR)		
		PEAK (CFS)	TIME (HR)	PEAK (CFS)	TIME (HR)	PEAK (CFS)	TIME (HR)					COEFF (X)	POWER (M)					FACTOR (K*)	
ALTERNATE	1	STORM	99																
+161	1100	567	6.3	567	6.3			0	1.51	.05	0	1.81	1.53	.003	1.000	54	1.00?	.00	.00
+162	1700	579	6.3	578	6.3			0	1.54	.05	1	1.54	1.51	.007	.999	100	.95?	.05	.03
+163	900	595	6.3	595	6.3			0	1.58	.05	0	1.05	1.51	.004	1.000	68	1.00?	.00	.00
+165	3200	1050	6.3	1042	6.3			0	1.82	.05	1	1.55	1.51	.014	.992	154	.74?	.05	.04
ALTERNATE	1	STORM	10																
+161	1100	201	6.3	201	6.3			0	.60	.05	0	1.81	1.53	.004	1.000	77	1.00?	.00	.00
+162	1700	207	6.3	206	6.3			0	.61	.05	1	1.54	1.51	.010	.994	142	.78?	.10	.04
+163	900	213	6.3	213	6.4			0	.64	.05	1	1.05	1.51	.005	1.000	96	.97?	.05	.03
+165	3200	423	6.3	414	6.4			0	.79	.05	1	1.55	1.51	.020	.979	209	.60	.10	.06

1

SUMMARY TABLE 3 - DISCHARGE (CFS) AT XSECTIONS AND STRUCTURES FOR ALL STORMS AND ALTERNATES

XSECTION/ STRUCTURE ID	DRAINAGE AREA (SQ MI)	STORM NUMBERS.....	
		10	99
0 STRUCTURE 80	1.77		
+			
ALTERNATE 1		359.77	1285.70
0 XSECTION 160	.59		
+			
ALTERNATE 1		202.68	567.45
0 XSECTION 161	.65		
+			
ALTERNATE 1		208.09	579.04
0 XSECTION 162	.71		
+			
ALTERNATE 1		213.82	595.35
0 XSECTION 163	.72		
+			
ALTERNATE 1		216.25	599.59
0 XSECTION 164	.97		
+			
ALTERNATE 1		423.91	1051.79
0 XSECTION 165	1.77		
+			
ALTERNATE 1		646.55	1668.28

LEND OF 1 JOBS IN THIS RUN