

Broadmoor Bluffs Eto

MICROFICHERD

ADDENDUM TO THE
FINAL DRAINAGE REPORT FOR
BROADMOOR BLUFFS DRIVE AND FARTHING DRIVE AND
FINAL DRAINAGE REPORT FOR
THE SCHOOL SITE AT
BROADMOOR BLUFFS ESTATES
A PORTION OF
CHEYENNE MOUNTAIN RANCH
COLORADO SPRINGS, COLORADO

NOT TO BE
CHECKED OUT

RECEIVED
PUBLIC ENGINEER
C. SPRINGS
OCT 15 1984
AM
7:30 AM



DREXEL, BARRELL & CO.

ENGINEERS — SURVEYORS

1700 38TH STREET

BOULDER, COLORADO 80301

(303) 442-4338

MICROFICHERD

ADDENDUM TO THE
FINAL DRAINAGE REPORT FOR
BROADMOOR BLUFFS DRIVE AND FARTHING DRIVE AND
FINAL DRAINAGE REPORT FOR
THE SCHOOL SITE AT
BROADMOOR BLUFFS ESTATES
A PORTION OF
CHEYENNE MOUNTAIN RANCH
COLORADO SPRINGS, COLORADO

PREPARED FOR:

GATES LAND COMPANY
155 WEST LAKE AVENUE
COLORADO SPRINGS, COLORADO 80906
(303) 576-8515

PREPARED BY:

DREXEL, BARRELL & CO.
1700 38TH STREET
BOULDER, COLORADO 80301
(303) 442-4338

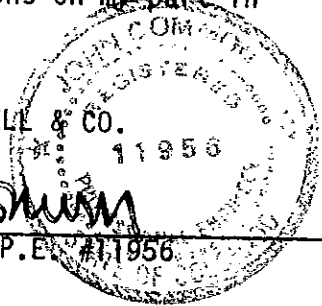
DATE PREPARED: OCTOBER 8, 1984
E-3146
(0155R)

CERTIFICATIONS

The attached drainage plan and report entitled "Addendum to the Final Drainage Report for Broadmoor Bluffs Drive and Farthing Drive and Final Drainage Report for the School Site at Broadmoor Bluffs Estates" were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by the negligent acts, errors, or omissions on my part in preparing this report.

For: DREXEL, BARRELL & CO.

By: John Common
John Common, P.E. #11956



The developer has read and will comply with all of the requirements specified in this drainage report as approved by the City Engineer.

By : Robert F. Svejksky
Robert F. Svejksky
Title : Director of Engineering
Address: 155 West Lake Avenue
Colorado Springs, CO 80906

City of Colorado Springs:

Filed in accordance with Section 15-3-906 of the Code of the City of Colorado Springs, 1980, as amended.

City Engineer:

John Common

Date:

10/24/84

Conditions:

CONDITIONS:

- 1) All berms and swales shown on the drainage plan to be privately maintained.
- 2) Gates Land Co. to accept and maintain developed flows onto their property.

FLOODPLAIN STATEMENT

FOR
BROADMOOR BLUFFS ESTATES

Broadmoor Bluffs Estates including the elementary school site is not in a designated Floodplain as shown on the Flood Insurance Rating Maps.

ADDENDUM TO THE
FINAL DRAINAGE REPORT FOR
BROADMOOR BLUFFS DRIVE AND FARTHING DRIVE
AND
FINAL DRAINAGE REPORT FOR
THE SCHOOL SITE AT
BROADMOOR BLUFFS ESTATES
COLORADO SPRINGS, COLORADO

LOCATION

Broadmoor Bluffs Estates is a proposed single-family residential development. The subdivision includes approximately 59.22 acres of residential lots. An adjacent property of 11.8 acres has been set aside for Elementary School No. 4, Cheyenne Mountain School District No. 12. These areas are located in the SE1/4 of the SE1/4 of Section 6, and in the NE1/4, the East 1/2 of the NW1/4 and the NE1/4 of the SW1/4 of Section 7, all in T15S, R66W of the 6th P.M., Colorado Springs, Colorado. More generally, the area lies west of Colorado State Highway No. 115, across from the Fort Carson Military Reservation. It is bounded on the north by Broadmoor Bluffs Park No. 2 and 4; on the west by Broadmoor Bluffs Filing No. 8 and Neal Ranch Filing No. 2. The remaining surrounding properties are unplatted and owned by Gates Land Company.

INTENT

This report is an Addendum to the City approved Final Drainage Report for Broadmoor Bluffs Drive and Farthing Drive prepared by Drexel, Barrell & Co., and dated August 31, 1984. It is also a Final Drainage Report for the Elementary School Site at Broadmoor Bluffs Estates. The proposed development of the elementary school site south of Farthing Drive will result in a slight increase in tributary flows to the street. This necessitated a recalculation of capacities of Farthing Drive and related drainage facilities. Flows which originate on the school site but are not tributary to Farthing Drive have also been analyzed to determine any possible need for the development of additional drainage facilities. This report does not address internal drainage at the School Site but only considers the storm run-off developed on the property as it leaves the site.

DESIGN REFERENCES

The drainage design criteria was taken from the City of Colorado Springs "Determination of Storm Runoff Criteria Manual". Flows from the school site which outfall to Farthing Drive were calculated using the modified SCS methodology for the 6 hour initial 5 year, and major 100 year rainfalls. No flows over 500 cfs occur, so all culverts were sized to pass the 5 year flows with no backwater and pass the 100 year flows with no overtopping of the curbs. Storm sewers were designed so as to not allow curb and gutter flow to exceed 12 cfs with the initial rainfall and allow major rainfall to be channelized within the right-of-way. Hydrologic soil groups were determined from maps published by the Soil Conservation Service. School site flows which outfall to an existing swale ("C") to the south of the property were calculated using the rational method, since the basin is less than 20 acres in size.

EXISTING DRAINAGE CHARACTERISTICS

Two major drainage basins were established in the Final Drainage Report for Broadmoor Bluffs Drive and Farthing Drive. Each basin contains at least one existing drainage swale. The southerly basin, "I", outfalls runoff from approximately 84.7 acres to a swale which carries flows to a pair of existing 72" culverts under Colorado State Highway No. 115, located approximately 1250 feet south of the Academy Boulevard overpass. Farthing Drive flows are included in Basin "I".

Existing site conditions range from grassy 6% slopes, in Basins K & L, to heavily vegetated slopes ranging from 8 to 65% in Basins A through E. The soils are predominantly of the razor series with some ustic torrifuvents existing around Basins K, L & the Academy overpass area, in addition to Jarre-Tecolote complex in Basins A, B, C and D. The existing drainage swales are generally heavily vegetated; ranging from natural grasses to scrub oak.

DESIGN DRAINAGE CHARACTERISTICS

As indicated by the Final Drainage Report for Broadmoor Bluffs Drive and Farthing Drive, approximately 39.9 acres (offsite Basins 1 & 2) are tributary to major Basin I. Two forks from Swale "A" extend westerly through the single-family area and eventually pick up these flows. Future culverts will be required beneath Cardiff Circle to pass these flows. The two forks merge within Basin G and continue easterly, paralleling the proposed Farthing Drive. This swale dissipates in Basin J and the storm runoff turns into sheet flow. To contain this sheet flow and effectively pass it under Broadmoor Bluffs Drive, a temporary swale section is proposed across Basin J. This swale will direct flows to a proposed 48" culvert at the intersection of Farthing and Broadmoor Bluffs Drives. These flows will then be directed to an existing major swale outfalling to the previously mentioned twin 72" culverts under Colorado State Highway No. 115.

The flows generated in Farthing Drive and in Basin "O" of the school site are to be picked up by a series of inlets at the intersection of Farthing Drive and Broadmoor Bluffs Drive and directed to the same outfall as discussed above. Basin J is proposed as a future commercial area. With the existing topography, and proposed street grades, it would be difficult to direct future design runoff from Basin J to the 48" culvert. Therefore a 36" culvert is proposed to release flows from this basin. In the event, prior to street construction, this area should be designated for another use, this culvert may be redesigned.

Additional school site flows (Basin "P") will outfall to the two 72" culverts south of Academy Blvd. at Highway 115, but are to be routed to this point through an existing swale ("C") located to the south of Farthing Drive. At the time of future Broadmoor Bluffs Drive construction to the south of its intersection with Farthing Drive, it will be necessary to provide a culvert or other means of passing Basin "P" flows across the roadway.

Swales "A" & "C" are to remain natural and privately maintained. Future culverts, in this area, have been preliminary sized and will be detailed with the final drainage report for the single-family area.

CONCLUSION

This study slightly modifies the flows to be passed along and under Broadmoor Bluffs Drive and Farthing Drive. The intent is to provide sufficient design criteria for the street construction at this time. The calculations indicate that previously designed and approved drainage facilities are adequate to carry additional flows to Farthing Drive due to school site development. A slight modification in the Farthing Drive design was necessary to provide sufficient street flow capacity.

Additional flows developed on the school property will be directed to an existing swale ("C") located to the south of the site. These flows from the school site appear to negligibly increase flows in the existing channel. Based upon inspection of the respective times of concentration, peak storm run-off flows from the school site will enter the existing channel long before the peak run-off arrives from the upstream basin. Hence the run-off from the School Site should have little or no impact on the existing channel. The channel will be studied further in future reports as development within the basin progresses.

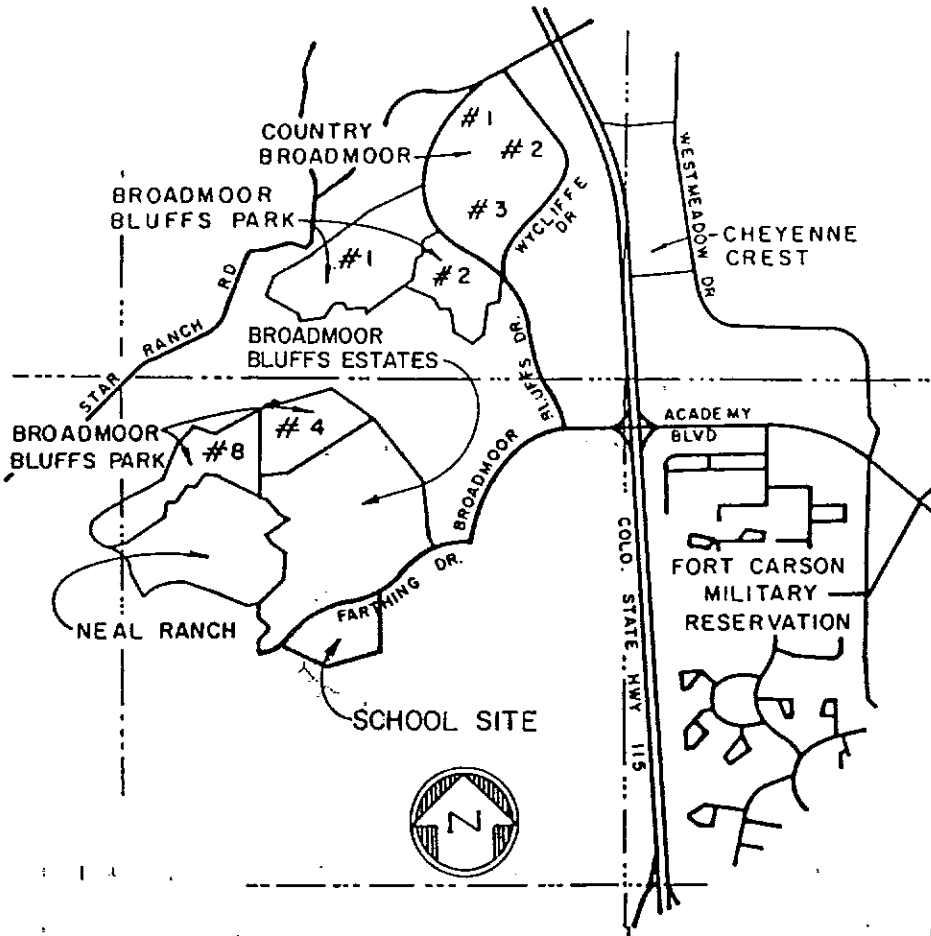
Copies of the calculations, with support material, follow for your review. By agreement with the City of Colorado Springs, no drainage basin fees are paid by Gates Land Company. Drainage structure cost estimates calculated in the "Final Drainage Report for Broadmoor Bluffs Drive and Farthing Drive" will remain the same. The drainage facilities proposed in the Final Report for Broadmoor Bluffs Drive and Farthing Drive will be built and paid for by Gates Land Company. A copy of the drainage plan has been included for your review.

Respectfully submitted,

Constell Sturdevant

Constell Sturdevant
Drexel, Barrell & Co.

EXHIBIT "A"



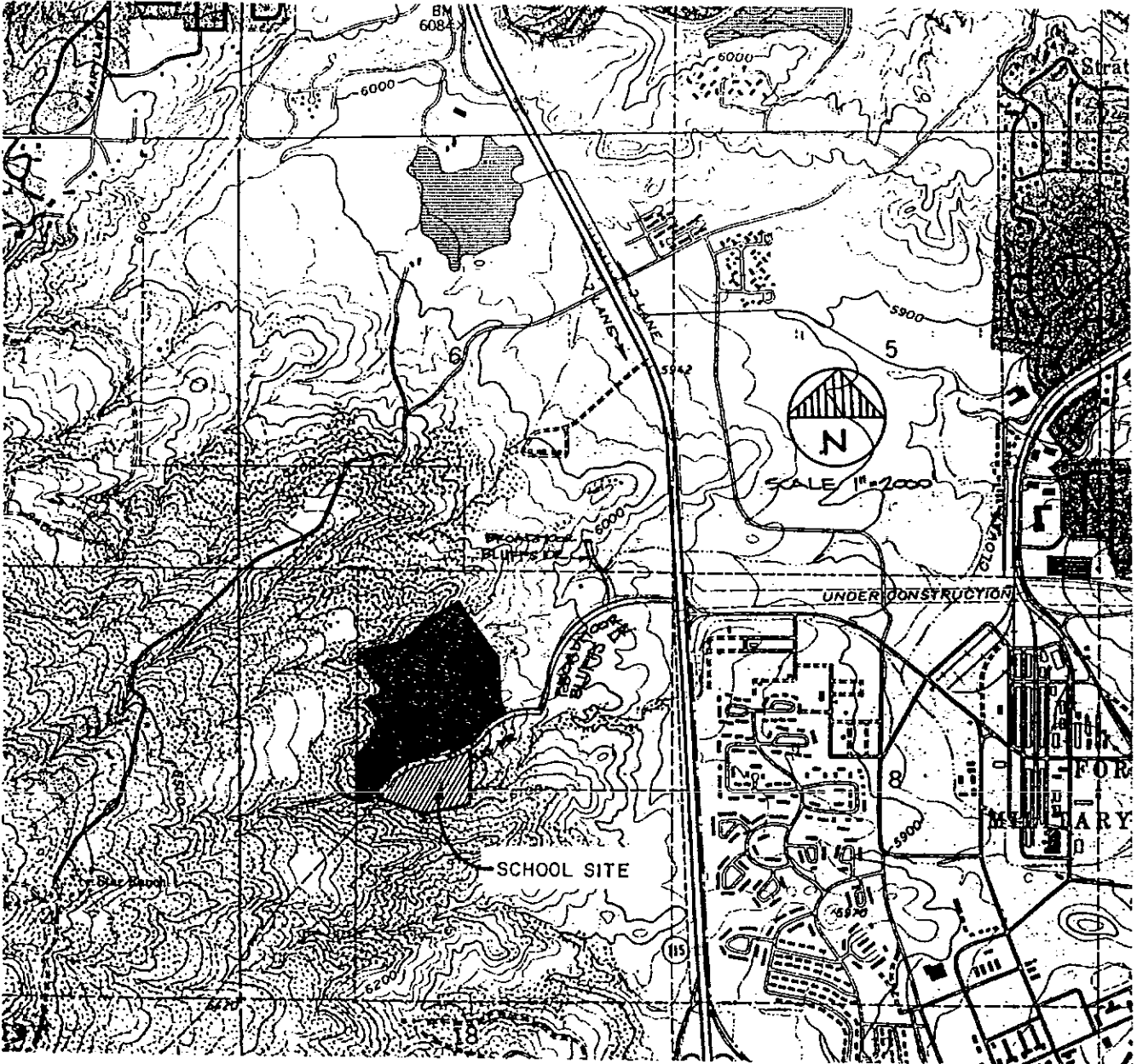
VICINITY MAP

SCALE : 1" = 2000'

BENCH MARKS

GATES GRID NO. 55,000 N
105,000 E
ELEVATION = 5959.26 (U.S.G.S.)

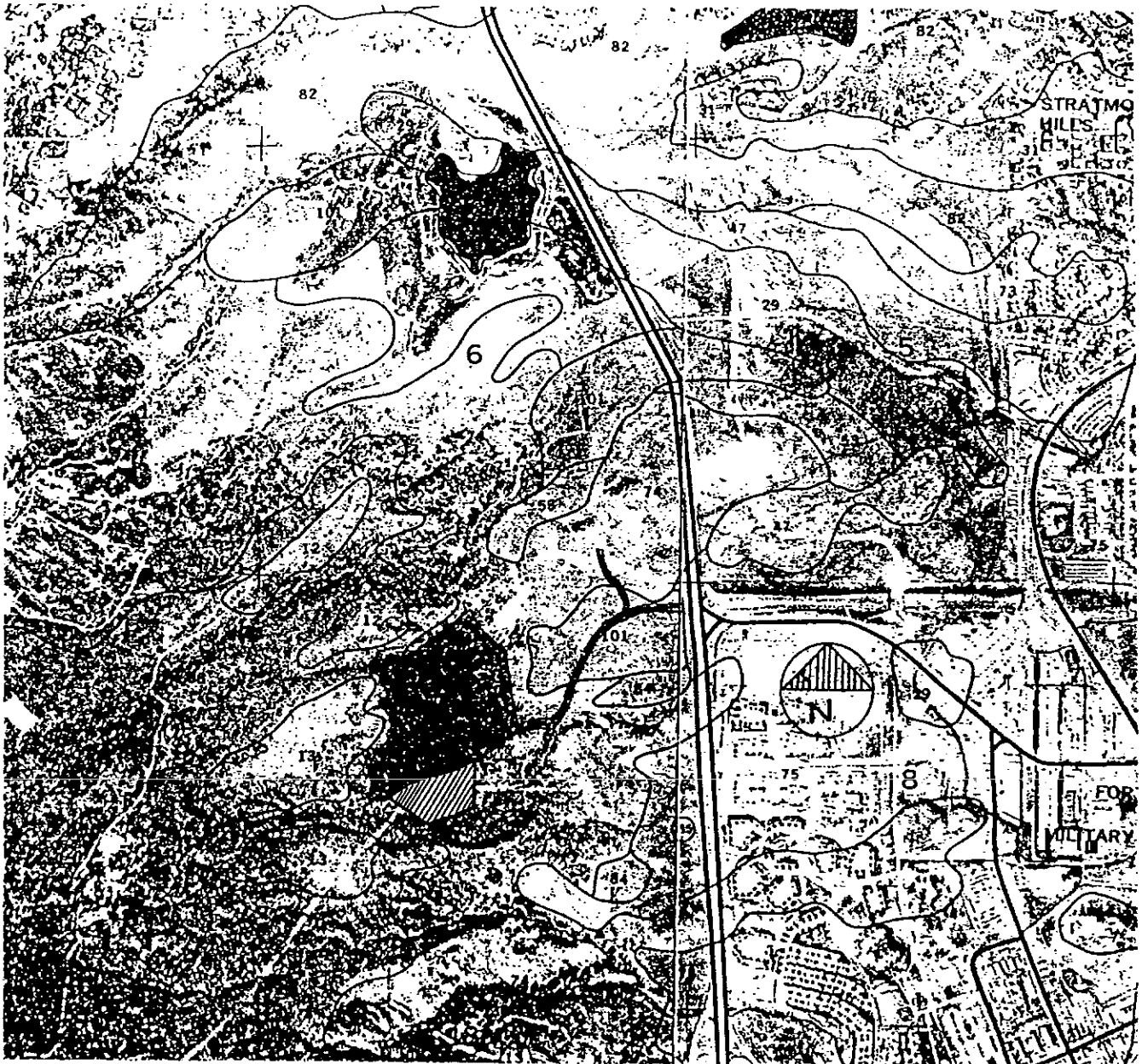
EXHIBIT "A1"



U.S.G.S.
VICINITY MAP

SCALE: 1" = 2000'

EXHIBIT "B"



SOILS MAP

SCALE · 1" = 2000'

SEE NEXT PAGE FOR
DESCRIPTIONS.

EXHIBIT "B"
HYDROLOGIC SOILS GROUPS
FOR
BROADMOOR BLUFFS ESTATES STUDY .

| <u>No.</u> | <u>Classification</u> | <u>Hydrologic Group</u> |
|------------|-----------------------|-------------------------|
| 12 | Bresser | B |
| 13 | Bresser | B |
| 38 | Jarre Tecolote Series | B |
| 74 | Razor | C |
| 84 | Stapleton | B |
| 101 | Ustic Torrifuvents | B |

EXHIBIT "C"

STREET CAPACITY AND INLET
SIZING CALCULATIONS

| | |
|--------------------------|--------|
| Project | Job No |
| BROADMOOR BLUFFS ESTATES | E-3098 |

| | | |
|--------|-----|--------------|
| Client | By | Date |
| GATES | JGS | 25 SEPT 1984 |

BASIN "D" AREA = 2.01 ACRES SCHOOL SITE

SOIL GROUP = 74 (C) USE C+B LN = 94

T_c : 270' OVERLAND @ 8%

VELOCITY = 0.7 f/s $t_c = 270 / (60)(0.7) = 6.4 \text{ MIN.}$

225' ASPHALT FLOW @ 5%

VELOCITY = 4.5 f/s $t_c = 225 / (60)(4.5) = 0.8 \text{ MIN}$

$T_c = 6.4 + 0.8 = 7.2 \text{ MIN.} = 0.12 \text{ h.}$

$q_p = 1220 \text{ CSM/INCH}$

$Q_5 = 1.49 \text{ IN.}$

$Q_{100} = 2.84 \text{ IN.}$

$Q_5 = 1220 * (2.01/640)(1.49) = 5.7 \text{ CFS}$

$\frac{QA}{640}$
0.0047

$Q_{100} = 1220 * (2.01/640)(2.84) = 10.9 \text{ CFS}$

0.0089

STREET CAPACITY + INLET SIZING

BASIN "A" UNCHANGED

BASIN "H" (FLOW TO 17+00) 50/50 SPLIT EXCEPT S. SIDE RECEIVES BASIN "O"

1/2 ST. $QA/640$ 5 YR = 0.0032 100 YR = 0.0056

S 1/2 STREET $\Sigma QA/640 = 0.0003 + 0.0032 + 0.0047 = 0.0082 \text{ 5 YR}$
 $0.0007 + 0.0056 + 0.0089 = 0.0152 \text{ 100 YR}$

$T_c = 90' \text{ CURB FLOW @ } 7\% \quad 0.3 \text{ MIN}$

950' CURB FLOW @ 10% 2.6 MIN

BASIN "O" 7.2 MIN

10.1 MIN = 0.17 h. $q_p = 1120 \text{ CSM/IN.}$

$Q_5 = 1120 * (0.0082) = 9.2 \text{ CFS}$

$Q_{100} = 1120 * (0.0152) = 17.0 \text{ CFS}$

| | | | |
|--------------------------|-----|---------------|--|
| Project | | Job No | |
| BROADMOOR BLUFFS ESTATES | | E-3098 | |
| Client | By | Date | |
| GATES | JGS | 25 SEPT. 1984 | |

BASIN "H" CONTINUED

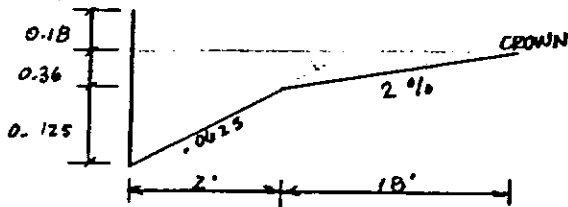
N 1/2 STREET

TOTAL "QA/640"
 5YR : 0.0031 + 0.0032 = 0.0063
 100 YR : 0.0087 + 0.0056 = 0.0143

$T_c = 7.1 \text{ MIN} + 3.3 \text{ MIN} = 10.4 \text{ MIN} = 0.17 \text{ HOUR}$

$Q_p = 1120 \text{ GPM/INCH}$
 $Q_5 = 1120 * 0.0063 = 7.1 \text{ CFS}$
 $Q_{100} = 1120 * 0.0143 = 16.0 \text{ CFS}$

CHECK ST. CAPACITY $S = 6\%$



$S = 0.10$
 $n = 0.016$

| | | |
|-----------------------|-------------|----------------------|
| $\frac{1}{2}n = 1000$ | $d = 0.485$ | $Q = 27 \text{ CFS}$ |
| $\frac{2}{3}n = 1000$ | $d = 0.36$ | $Q = 11 \text{ CFS}$ |
| $\frac{1}{3}n = 3125$ | $d = 0.36$ | $Q = 36 \text{ CFS}$ |

ALLOWABLE = 52 CFS * 0.2 (RP) = 10.4 CFS TO CROWN OK

| | | |
|------------------------------------|-----------|-----------------------|
| Project BEADMOR BLUFFS ESTATES. | | Job No E-3098 |
| Client GATES | By JGS | Date 25 SEPT. 1984 |

BASIN "I" (FLOW TO STA 10+00) AREA = 1.16 ACRES

1/2 ST. QA/640 = 0.0017 5 YR
0.00295 100 YR

5 1/2 STREET
Σ QA/640 = 0.0017 + 0.0082 = 0.0099
0.00295 + 0.0152 = 0.01815

Tc: 10.1 MIN + 2.1 MIN = 12.2 MIN = 0.2 h

γp = 1060 CSM/IN

qs = 1060 * (0.0099) = 10.5 CFS q100 = 1060 * 0.01815 = 19.2 CFS

N 1/2 STREET
Σ QA/640 = 0.0017 + 0.0063 = 0.008
0.00295 + 0.0143 = 0.01725

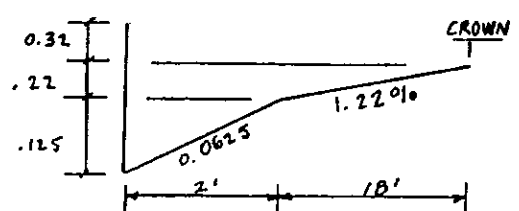
Tc = 10.4 MIN + 2.1 MIN = 12.5 MIN = 0.21 h

γp = 1050 CSM/IN

qs = 1050 * 0.008 = 8.4 CFS q100 = 1050 * 0.01725 = 18.1 CFS

STREET CAPACITY

SOUTH SIDE HAS ROTATING X-SLOPE
STA 11+50 R SLOPE = 6.13% X-SLOPE = 1.22% η = 0.016



| | | |
|------------|-----------|-----------------|
| z/n = 1000 | d = 0.345 | Q = 8.0 CFS |
| z/n = 1000 | d = 0.22 | Q = 2.5 CFS |
| z/n = 5123 | d = 0.22 | Q = 13.0 CFS |
| | | <u>18.5 CFS</u> |

ALLOWABLE Q' = (18.5) * (0.40)^{RF} = 7.4 CFS

| | | | |
|--|--|-------------------------|------------------------------|
| Project BROADMOOR BLUFFS ESTATES | | Job No E-3098 | |
| Client GATES | | By JGS | Date 25 SEPT. 1984 |

BASIN "I" CONTINUED

N SIDE HAS TYPICAL SECTION

STATION 10+75 & SLOPE = 4.4% X-SLOPE = 2%

TABLE 5 INTERPOLATION = $89.4 \text{ CFS} / 2 = 44.7 \text{ CFS}$ $\frac{1}{2}$ ST. OK

STATION CHECK (13+00)

17+00 \rightarrow $S \frac{1}{2}$ $T_c = 10.1 \text{ MIN}$ $q_5 = 9.2$ $q_{100} = 17.0$

400' CURBFLOW AT 10% = 1.1 MIN

$QA/640 = (1.87)(0.18)/640 = 0.00054$ 5 yr

$(3.27)(0.18)/640 = 0.00092$ 100 yr

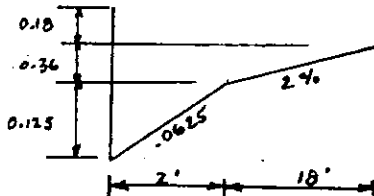
$\Sigma QA/640 = 0.0082 + 0.00054 = 0.00874$ 5 YR

$0.0152 + 0.00092 = 0.01612$ 100 YR

TOTAL $T_c = 10.1 + 1.1 = 11.2 = 0.19 \text{ h} \Rightarrow q_p = 1080 \text{ CSM/H}$

$q_5 = 1080 * 0.00874 = 9.4 \text{ CFS}$ $q_{100} = 1080 * 0.01612 = 17.4 \text{ CFS}$

STREET CAPACITY $S = 0.10$ $n = 0.016$



$z/n = 1000$ $d = 0.485$ $Q = 27 \text{ CFS}$

$z/n = 1000$ $d = 0.36$ $Q = 12 \text{ CFS}$

$z/n = 3125$ $d = 0.36$ $Q = 36 \text{ CFS}$

51 CFS

ALLOWABLE = $(51)(0.2) = 10.2 \text{ CFS}$ OK

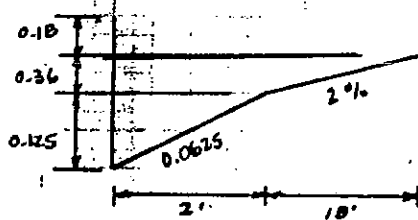
$S = 10\%$ 6' INLET = 6.12 CFS @ 11+50

@ 13+00, 10%, $q_5 = 9.4$, $(.6)(9.4) = 5.64 \Rightarrow$ 6' INLET

| | | | |
|--|--|-------------------------|------------------------------|
| Project BROADMOOR BLUFFS ESTATES | | Job No E-3098 | |
| Client GATES | | By JGS | Date 25 SEPT. 1984 |

IF NORMAL AT 11+50 IS CAPACITY SUFFICIENT?

ASSUME \bar{x} SLOPE = 6.13% X-SLOPE = 2% $\eta = 0.015$



| | | |
|--------------|-------------|---------------------------|
| $Z/n = 1000$ | $d = 0.485$ | $Q = 21 \text{ cfs}$ |
| $Z/n = 1000$ | $d = 0.36$ | $Q = 9 \text{ cfs}$ |
| $Z/n = 3125$ | $d = 0.36$ | $Q = 28 \text{ cfs}$ |
| | | $\Sigma = 40 \text{ cfs}$ |

ALLOWABLE = (40 cfs)(0.4) = 16 cfs OK

- LEAVE INLETS IN SAME LOCATION.
- REDESIGN TRANSITION FROM BROADMOOR BLUFFS TO FARTHING DRIVE.
- USE ONLY 100' V.G.

JGS/CS 12 Oct. 1984

Pursuant to the vertical realignment of Farthing Drive, dated Oct. 8, 1984, the following calculations were performed to show the agreement between calculated 5 year flows + allowable street capacities.

ALLOWABLE CAPACITY at STA 11+30 $S = 0.0552$ $R = 0.216$

Typical Section, as above: $Q = 20 \text{ cfs}$
 (for slope = 5.5%) $Q = 9 \text{ cfs}$
 $Q = 26 \text{ cfs}$
 $\Sigma = 37 \text{ cfs}$

Allowable = $(37)(0.45) = 16.7 \text{ cfs}$ → use 17 cfs for 5 year flow

From Basin I: $q_{5} = 16.5 \text{ cfs}$
 $q_{100} = 19.2 \text{ cfs}$

6' Inlet Capacity = 8.7 cfs
 5 year pick-up = 6.3 cfs 5 year flow by = 4.9 cfs
 100 year pick-up = 8.7 cfs 100 year flow by = 10.5 cfs

EXHIBIT "D"

SCHOOL SITE DEVELOPED RUN-OFF
CALCULATIONS

| | |
|--|-------------------------|
| Project <i>Chey. Mtn. / School Site</i> | Job No <i>E-3146</i> |
|--|-------------------------|

| | | |
|------------------------|-----------------|------------------------|
| Client <i>Gates</i> | By <i>PS</i> | Date <i>10-5-84</i> |
|------------------------|-----------------|------------------------|

✓ BIB 9OCT84

Total Site Area : *11.8 ac.* *7203 2797*
**462 2741*

Basin Use : *"0" Drains to Farthing Dr.* *2470*

A = 2.0 Ac.

| Use: | Area; A _o : | C |
|-----------------|------------------------|--------------------------------|
| Drive + Parking | <i>0.9</i> | <i>0.90</i> |
| Open Space | <i>1.1</i> | <i>0.50</i> |
| | <u><i>2.0</i></u> | <u><i>0.55 (Composite)</i></u> |

(see Basin "0" Calculations)

T_c = 0.12 hrs. (from previous calcs - Jim Sokolowski)
I₅ = 5.2 in/hr. I₁₀₀ = 7.9 *see p.1, Exhibit C*

Q₅ = CIA = (0.55)(5.2)(2) = 5.7 cfs → *these flows included in Broadmoor Bluffs estates street flows to Farthing Drive. (Basin "0")*

*Q₁₀₀ = CIA = (0.55)(7.9)(2) = 8.7 cfs**

** This calculates as lower than the number designed for using the SCS method, so street design is conservative.*

Basin "P": Release to existing swales to East/South
A = 11.8 - 2.0 = 9.8 ac.

| Use: | Area; A _o : | C |
|-----------------------------|------------------------|--------------------------------|
| Buildings/Roofs | <i>1.6</i> | <i>0.90</i> |
| Asphalt Drives + Play Areas | <i>0.3</i> | <i>0.90</i> |
| Gravel Play Areas | <i>1.7</i> | <i>0.70</i> |
| Open Space | <i>7.2</i> | <i>0.50</i> |
| | <u><i>9.8 ac.</i></u> | <u><i>0.42 (Composite)</i></u> |

T_c = 0.07 hr A elev. = 24' L = 660'
I₅ = 6.1 in/hr I₁₀₀ = 9.0 in/hr

Q₅ = CIA = (0.42)(6.1 in/hr)(9.8 ac.) = 25.1 cfs
Q₁₀₀ = (0.42)(9.0 in/hr)(9.8 ac.) = 37.0 cfs

| | | | |
|---|----------|------------------|--|
| Project Chey. Mtn. / School Site | | Job No E-3146 | |
| Client Gates | By CS | Date 10-5-84 | |
| ✓ BTB 9 OCT 84 | | | |
| <p>Basin "P" Historic Flows</p> <p style="margin-left: 100px;"> $T_0 = 0.07 \text{ hr}$ $I = 6.1 \text{ in/hr}$ $C = 0.30$ </p> <p style="margin-left: 100px;"> $Q = CIA = (0.30)(6.1)(9.8) = 17.9 \text{ cfs}$ </p> <p style="margin-left: 100px;"> \therefore This results in only a 7.2 cfs increase in flow downstream due to development. </p> <p>Checking possible impact on Swale "C" due to Basin "O" flows:</p> <p>Swale "C" drainage basin is approximately 350 ac. in size + corresponds to Basins V. and VII of a Master Drainage Plan for Cheyenne Mtn. Ranch presently in progress at Drexel, Barrell, & Co. These basins are based on previous basin divisions made by Hartell-, Pfeifferberger & Assoc. dated May 17, 1971. This tributary basin is also comparable to Basin A-96 identified in "Drainage Study, Fort Carson, Colorado" prepared by Higgenbotham & Assoc., Morgan & Assoc., Inc, and Karcich & Weber, Inc. for the U.S. Army Corps of Engineers.</p> | | | |

| | |
|---|-------------------------|
| Project <i>Qhey Mtn./School Site</i> | Job No <i>E-2146</i> |
|---|-------------------------|

| | | |
|------------------------|-----------------|-------------------------|
| Client <i>Gates</i> | By <i>CS</i> | Date <i>10-10-84</i> |
|------------------------|-----------------|-------------------------|

ON: I + VII

Basin II: Area = 258 ac. + 18.5 ac. not prev. included = 276.5 ac.

ON:

| Use | Soil Type | Acreage | % Area | CN | % CN |
|--------------------------------|-----------|---------|--------|----|------|
| Industrial, | B | 4 | 1.4 | 88 | 1.2 |
| Industrial | C | 24 | 8.7 | 91 | 9.9 |
| Multi-Family 6 units/ac | C | 10.0 | 3.6 | 90 | 3.3 |
| School Site: | C | 9.8 | 3.5 | 76 | 2.7 |
| Park Area | C | 16.0 | 5.8 | 74 | 4.3 |
| Single-Family 1 Unit/Ac. | B | 11.0 | 4.0 | 68 | 2.7 |
| Single-Family 2.4 Units/Ac. | B | 13.5 | 4.9 | 72 | 3.5 |
| Single-Family* 2 Units - Ac | B | 69.0 | 25.0 | 72 | 18.0 |
| Open Space* Fair Condition | | 118.7 | 42.9 | 69 | 29.6 |
| | | 276.5 | 100.0 | | 73. |

* These areas are presently unplatted + these assumptions have been made regarding future development.

$T_c = 1500'$ at 6% slope from Figure 15.2. $V = 8.0$ fps for alluvial fans
 $T_t = (1500') / (4.8 \text{ ft/s}) (60 \text{ s/min}) = 2.1 \text{ min}$

$4000'$ at 20% slope:
 $V = 6.9$ fps for grassed waterways
 $T_t = 9.7 \text{ min}$

$1500'$ at 12% slope: $V = 5.2$ fps for grassed waterways
 $T_t = 14.4 \text{ min}$

| | | |
|-----------------------------------|--|------------------|
| Project Chey Mtn / School Site | | Job No E-3146 |
|-----------------------------------|--|------------------|

| | | |
|-----------------|----------|------------------|
| Client Gates | By CS | Date 10-10-84 |
|-----------------|----------|------------------|

Basin V, cont. $T_0 = 3.1 \text{ min} + 9.7 \text{ min} + 14.4 \text{ min}$
 $= 27.2 \text{ min} = 0.45 \text{ hr.}$

$q_p = 780 \text{ csm/in}$

$CN = 73 \quad Q = 1.18 \text{ in}$

$Q_{100} = (276.5 \text{ ac}) / 640 \text{ ac/mi}^2 \times (1.18 \text{ in}) (780 \text{ csm/in})$
 $= 398 \text{ cfs}$

| | | |
|------------------------------------|----------|------------------|
| Project Chey. Mtn / School Site | | Job No E-3146 |
| Client Gates | By OS | Date 10-10-84 |

Basin VII : Area = 73.5 ac.

Corresponds to Basins 1, 2, A, H, I, O, E, Q, F, & G of Broadmoor Bluffs Estates (see previously approved drainage study).

For Basins A, H, I, O :

$$\text{Area} = 0.015 \text{ mi}^2$$

$$CN = 89$$

$$T_c = 0.32 \text{ hr.}$$

$$Q = 2.36 \text{ in}$$

$$q_p = 900 \text{ csm/inch}$$

$$Q = (0.015 \text{ mi}^2)(2.36 \text{ in})(900 \text{ csm/inch})$$

$$= 31.9 \text{ cfs}$$

For Basins 1, 2, B, C, G, F :

$$\text{Area} = 0.100 \text{ mi}^2$$

$$CN = 75$$

$$T_c = 0.47 \text{ hr.}$$

$$Q = 1.30 \text{ in}$$

$$q_p = 750 \text{ csm/in}$$

$$Q = (0.100)(1.30)(750)$$

$$= 100 \text{ cfs } (99.8 \text{ cfs})$$

$$Q_{\text{total}} = 99.8 + 31.9 + 398$$

$$= 530 \text{ cfs}$$

{ the school outflow of 37 cfs accounts for only about 7% of these flows.

Also, the school outflow will arrive at the channel in approximately 0.07 hr (4.2 min), while the T_c for the upper basins are around half an hour. Thus, the peak from the school site will reach Swale "C" prior to upper basin peak flows, and have a negligible impact on the hydrograph peak for the basin.

EXHIBIT "E"
CHARTS, USED IN CALCULATIONS

1/11

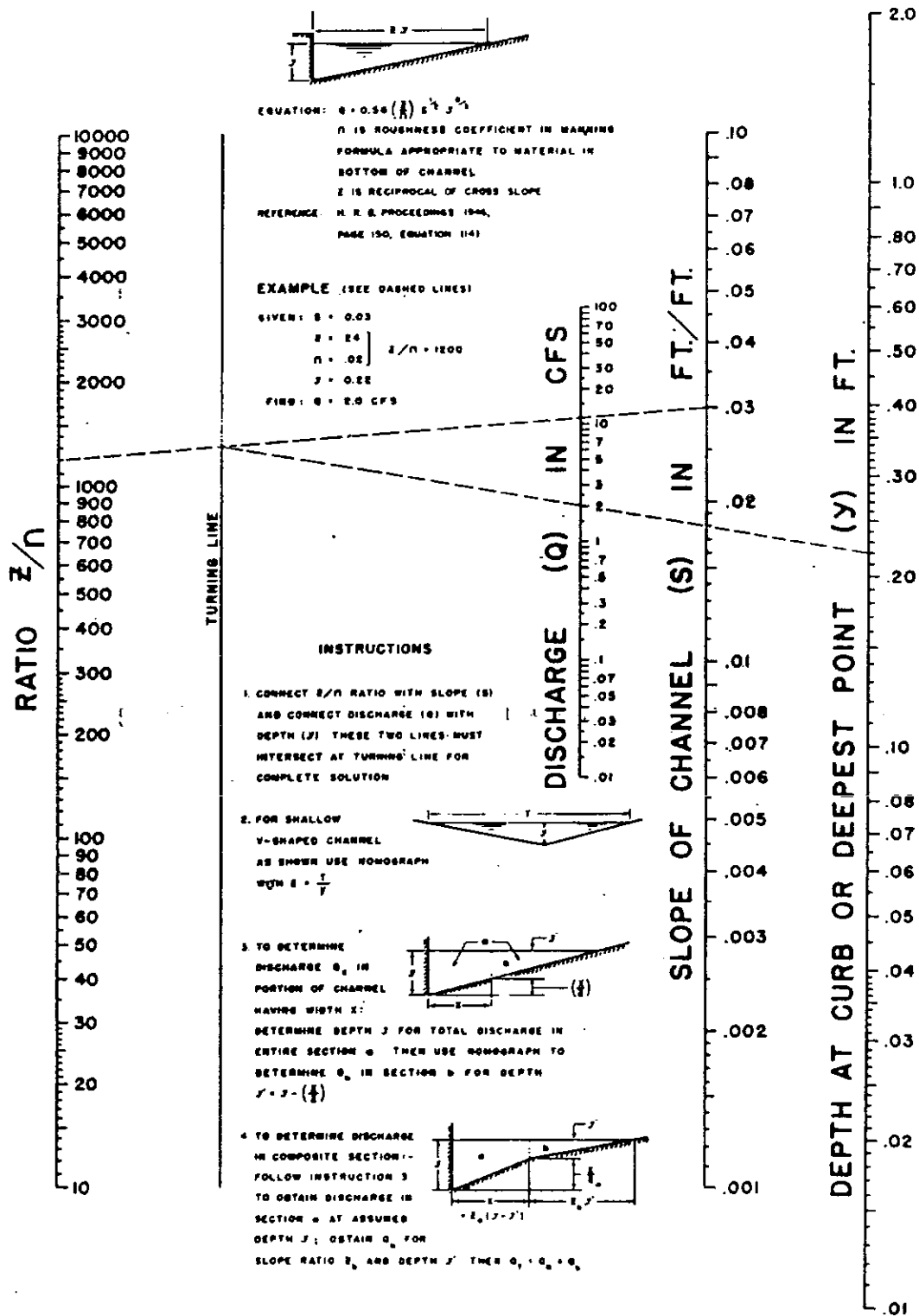


FIGURE 6-1. NOMOGRAPH FOR FLOW IN TRIANGULAR GUTTERS.

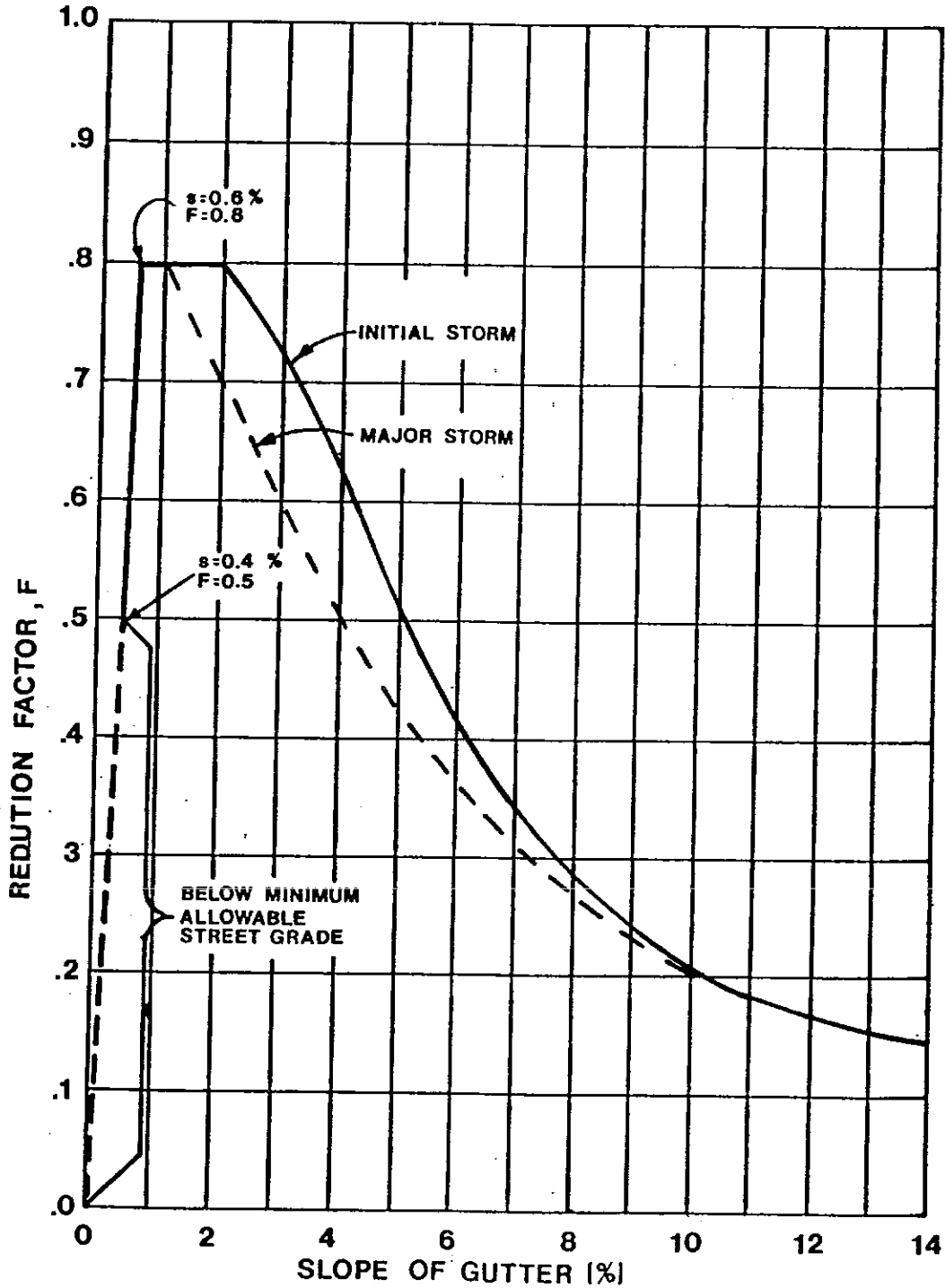


FIGURE 6-2 REDUCTION FACTOR FOR ALLOWABLE GUTTER CAPACITY LOCAL AND COLLECTOR STREETS

APPLY REDUCTION FACTOR FOR APPLICABLE SLOPE TO THE THEORETICAL GUTTER CAPACITY TO OBTAIN ALLOWABLE GUTTER CAPACITY APPROACHING ARTERIAL STREET

Table 5 Permissible Drainage Street Capacities with 8" Vertical Curbs *
 8" Curb - Full Storm Water Capacity (with level curbs)

| S | 34' Residential | | 36' Residential | | 40' Residential | | 34' One-Way Art. | | 60' & 76' Arterial | | S % |
|-----|-----------------|-------|-----------------|-------|-----------------|-------|------------------|------|--------------------|------|-----|
| | FPS | CFS | FPS | CFS | FPS | CFS | FPS | CFS | FPS | CFS | |
| 0.5 | 4.08 | 28.9 | 4.02 | 29.5 | 3.90 | 30.1 | | 20.0 | | 20.0 | 0.5 |
| 1.0 | 5.76 | 40.9 | 5.70 | 41.7 | 5.51 | 42.6 | | 30.0 | | 30.0 | 1.0 |
| 1.5 | 7.06 | 50.1 | 6.97 | 51.1 | 6.75 | 52.2 | 6.97 | 30.0 | 6.97 | 30.0 | 1.5 |
| 2.0 | 8.15 | 57.8 | 8.05 | 59.0 | 7.79 | 60.2 | 8.05 | 34.0 | 8.05 | 34.0 | 2.0 |
| 2.5 | 9.11 | 64.7 | 9.00 | 65.9 | 8.71 | 67.4 | 9.00 | 36.0 | 9.00 | 36.0 | 2.5 |
| 3.0 | 9.98 | 70.9 | 9.86 | 72.2 | 9.54 | 73.8 | 9.86 | 38.0 | 9.86 | 38.0 | 3.0 |
| 3.5 | 10.78 | 76.5 | 10.65 | 78.0 | 10.31 | 79.7 | 10.65 | 40.0 | 10.65 | 40.0 | 3.5 |
| 4.0 | 11.52 | 81.8 | 11.38 | 83.4 | 11.02 | 85.2 | 11.38 | 42.0 | 11.38 | 42.0 | 4.0 |
| 4.5 | 12.22 | 86.8 | 12.07 | 88.5 | 11.69 | 90.4 | 12.07 | 43.0 | 12.07 | 43.0 | 4.5 |
| 5.0 | 12.89 | 91.5 | 12.73 | 93.3 | 12.32 | 95.3 | 12.73 | 45.0 | 12.73 | 45.0 | 5.0 |
| 5.5 | 13.52 | 95.9 | 13.35 | 97.8 | 12.92 | 99.9 | 13.35 | 47.0 | 13.35 | 47.0 | 5.5 |
| 6.0 | 14.12 | 100.0 | 13.94 | 102.2 | 13.49 | 104.3 | 13.94 | 49.0 | 13.94 | 49.0 | 6.0 |

* Intermediate Values may be Obtained by Arithmetic Interpolation

4/12

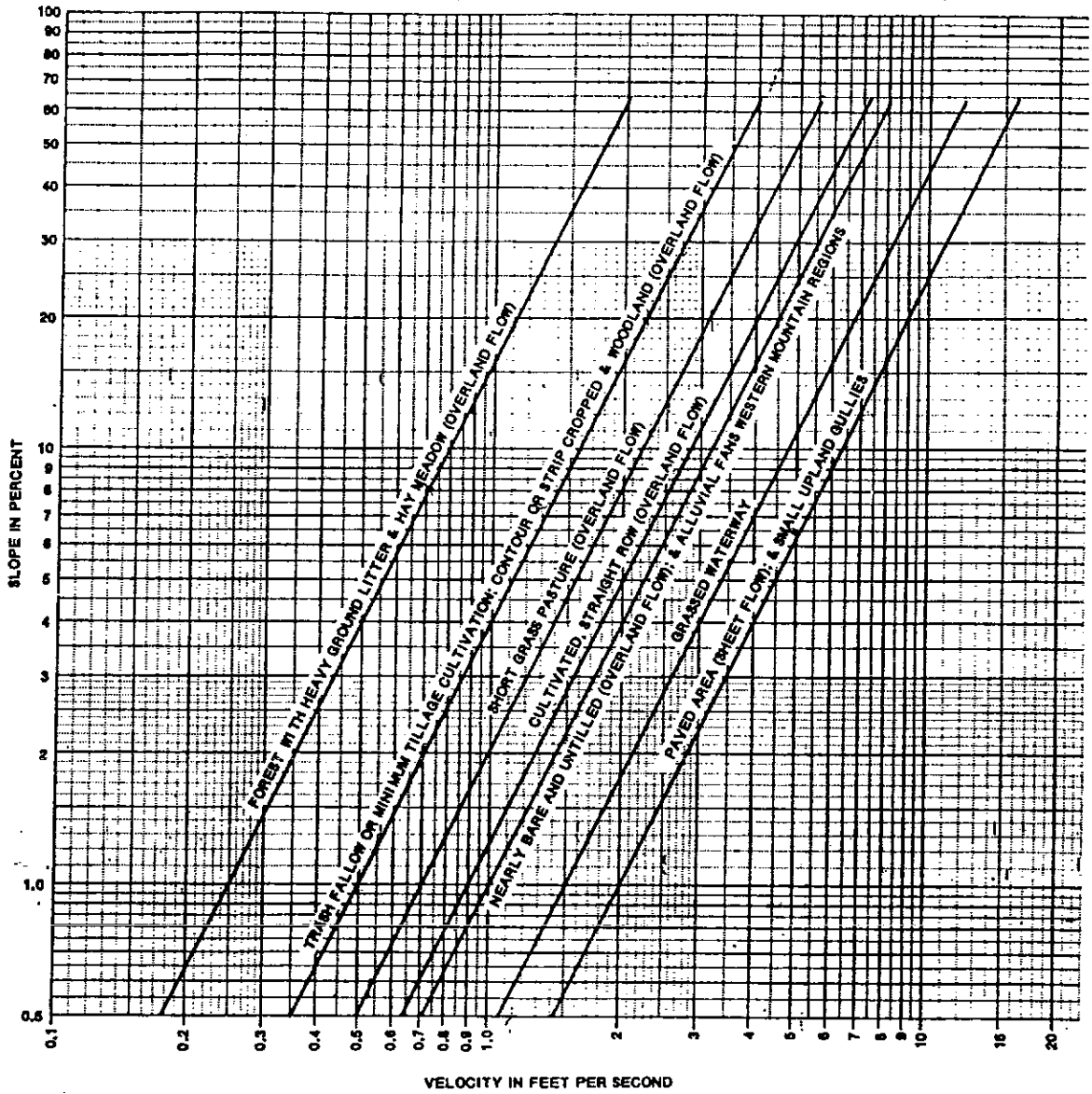


Figure 15.2.—Velocities for upland method of estimating T_c