

**MASTER DEVELOPMENT DRAINAGE PLAN
AND FINAL DRAINAGE REPORT
AMENDMENT
FOR
COTTAGES AT DRY CREEK**

February 2024

Prepared for:

BCC Management, LLC
Attn: Brian Schumann
150 Wuthering Heights Drive
Colorado Springs, CO 80921

Prepared By:

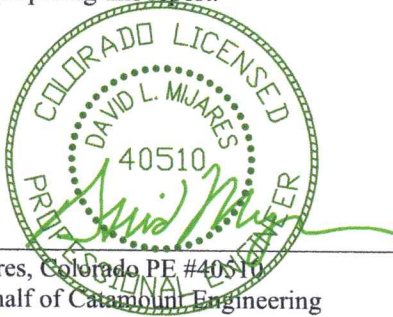


JOB NUMBER:20-270

MASTER DEVELOPMENT DRAINAGE PLAN AND FINAL DRAINAGE REPORT AMENDMENT FOR COTTAGES AT DRY CREEK

Engineer's Statement:

This report and plan for the drainage design of COTTAGES AT DRY CREEK was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the City of Colorado Springs Drainage Criteria Manual and is in conformity with the master plan of the drainage basin. I understand that the City of Colorado Springs does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing this report.



David L. Mijares, Colorado PE #40510
For and on behalf of Catamount Engineering

Date 2/12/24

Developer's Statement:

BCC MANAGEMENT LLC hereby certifies that the drainage facilities for COTTAGES AT DRY CREEK shall be constructed according to the design presented in this report. I understand that the City of Colorado Springs does not and will not assume liability for the drainage facilities designed and/or certified by my engineer and that are submitted to the City of Colorado Springs pursuant to section 7.7.906 of the City Code; and cannot, on behalf of COTTAGES AT DRY CREEK guarantee that final drainage design review will absolve BCC MANAGEMENT, LLC and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the final plat does not imply approval of my engineer's drainage design.

Schumann Communications PSP

Name of Developer
Brian Schumann 2/13/24

Authorized Signature Date

BRIAN SCHUMANN

Printed Name
TRUSTEE

Title

Address

City of Colorado Springs Only:

Filed in accordance with Section 7.7.906 of the Code of the City of Colorado Springs, 2001, as amended.

Emir Nagy

For City Engineer

2/27/2024
Date

CONDITIONS:

MASTER DEVELOPMENT DRAINAGE PLAN AND FINAL DRAINAGE REPORT AMENDMENT FOR COTTAGES AT DRY CREEK

PURPOSE

The purpose of this drainage report amendment is to update the previously approved drainage report with minor site revisions in the current development plan amendment. The development plan amendment relocated residential duplexes within basins A2, B2, and C2. Area of disturbance and impervious ratios within basins A2 and B2 were not modified with unit relocation. The remaining basins and infrastructure were not affected by unit relocation. The 'in-review' HGL amendment was also included in this drainage report amendment at the request of SWENT. Additionally relocation of units allowed for reconfiguration of proposed pond C removing proposed retaining walls. Scope of the amendment is to verify calculations provided in the approved drainage report and revise details to conform with submitted development plan. Total disturbed area for the development is 471,743 square feet.

Calculations affected by the amendment are highlighted in blue in the appendix.

The site is contained within the Dry Creek Drainage Basin and outfalls to Dry Creek. The parcel was previously studied in the preliminary drainage report Corporate Centre Filing No. 3 dated February 2021, prepared by Catamount Engineering and the 'MASTER DEVELOPMENT PLAN AND FINAL DRAINAGE REPORT FOR THE COTTAGES AT DRY CREEK', approved 5/10/23 and prepared by Catamount Engineering.

DEVELOPED DRAINAGE BASINS

See Proposed Conditions Drainage Map

Only basins affected by the development plan amendment are discussed in the amendment.

The site 'Proposed Drainage' plan, is provided in the appendix.

BASIN A-

A2 (3.20 Acres, $Q_5=2.8$ cfs, $Q_{100}=7.3$ cfs)

Basin A2 (3.20 Acres, $Q_5=2.8$ cfs, and $Q_{100}=7.3$ cfs) consists of the northern and eastern basin of the development; bordering along Mark Dabbling Blvd. Basin A2 primarily consists of the north half of the site's residential development, including the landscape and rear lot swale drainage. Runoff within Basin A2 will primarily sheet flow southwest toward the rear lot proposed drainage swale and be conveyed by a private CDOT Type D inlet and conveyed in an 18" private HDPE to confluence with runoff from Basin A1 pipe design point P1.

BASIN B-

B2 (1.92 Acres, $Q_5=2.5$ cfs, $Q_{100}=6.0$ cfs)

Basin B2 (1.92 Acres, $Q_5=2.5$ cfs, and $Q_{100}=6.0$ cfs) consists of the northeastern portion of the southerly half of the development; bordering along Mark Dabbling Blvd. Basin B2 primarily consists of residential development, including the landscape and rear lot swale drainage. Runoff within Basin B2 will primarily sheet flow southwest toward the rear lot proposed drainage swale and be conveyed by a private CDOT Type D inlet and conveyed in an 18" private HDPE to confluence with runoff from Basin B1 pipe design point P3.

BASIN C-

C2 (1.42 Acres, $Q_5=1.8$ cfs, $Q_{100}=4.7$ cfs)

Basin C2 (1.42 Acres, $Q_5=1.8$ cfs, and $Q_{100}=4.7$ cfs) consists of the Southeastern portion of the southerly half of the development; bordering along Mark Dabbling Blvd. Basin C2 primarily consists of the residential development, including the landscape and rear lot swale drainage. Runoff within Basin B2 will primarily sheet flow east to private EDB C.

STORM SEWER

Only basins affected by the development plan amendment are discussed in the amendment.

Runoff from Basin B2 of $Q_5=2.5$ cfs, $Q_{100}=6.0$ cfs will be conveyed in a grass lined swale and collected in a private Type D inlet. Captured flow will be conveyed in a private 18" HDPE to pipe design point P3. Combined flows from P3 of $Q_5=4.2$ cfs, $Q_{100}=9.2$ cfs will be conveyed in a private 18" HDPE storm sewer to pipe design point P4. Combined flows from P4 of $Q_5=4.5$ cfs, $Q_{100}=9.8$ cfs will be conveyed in a private 18" HDPE storm sewer to private extended detention basin B.

Hydraulic grade line calculations were developed utilizing UDSEWER 2009 Version 1.4.0.25. Rational method peak flows for the initial and major storm events as developed in the final drainage report were used for hydraulic analysis.

Tailwater assumptions (for both minor and major storm events) at the discharge into each of the proposed permanent control measure structure – Extended Detention Basins (A, B, & C) utilized the respective water surface elevation (WSE) of each event and associated EDB.

Peak flows from the major event do not exceed 1.0' below finished ground surface elevation. On Site flows are directed through the private full-spectrum extended detention basin prior to release to the proposed Storm Sewer System.

The analysis in the report appendix provides more detailed calculations for the system in accordance with the requirements of the City of Colorado Springs Drainage Criteria Manual Vol. I. The storm sewer plan and profile drawings have been submitted concurrently with this analysis.

See calculations in the report appendix.

EXTENDED DETENTION BASINS

Only basins affected by the development plan amendment are discussed in the amendment.

This project proposes to develop 12.78 acres within the Dry Creek major drainage basin which necessitates water quality treatment and full-spectrum detention per the criteria of the City of Colorado Springs Drainage Criteria Manual Volume 2.

EDB C

The proposed private and full spectrum Extended Detention Basin located in the southerly section of the portion of the development has 2.60 tributary acres of development with an average imperviousness of 62.50%. Full spectrum pond development routed hydrograph results indicated 0.050 acre-ft of water quality capture volume after runoff reduction ponding to an elevation of 6553.12, an EURV volume of 0.19-acre ft ponding to a depth of 6554.94, and a total volume of 0.291 acre-ft ponding to an elevation of 6555.52 providing full spectrum detention including the 100-YR event.

Runoff generated within the site will be conveyed to the pond through storm sewer systems or as direct sheetflow. The storm sewer systems will outfall directly to 12" concrete forebays providing 66 cubic feet of volume and with baffle providing adequate protection at discharge point. The concrete forebays require a total volume of 49 cubic feet of volume (2% of the design WQCV). The forebay will be constructed of a concrete slab with sides conforming to the pond slopes and 1' wall with a 3.2" rectangular notch which outfalls to the proposed trickle channel at the downstream end.

The pond will be constructed with 4:1 minimum side slopes to be vegetated per the final landscape plan. A 2' wide by 6" deep concrete trickle channel with a 0.5% longitudinal slope will convey low flows across the pond bottom to the micropool/outlet structure. The trickle channel will outfall to a 5' long by 4' wide by 2.5' deep concrete micropool. The micropool will provide a surface area of 16 square feet and an initial surcharge volume of 5.3 cubic feet utilizing an 4" initial surcharge depth.

The outlet structure will consist of a concrete box with orifice plate and screen providing water quality outlet and weir with trash rack for larger storm outfall. The pond will outfall $Q_5=0.1$ cfs, $Q_{100}=1.9$ cfs through a private 12" HDPE pipe system to existing public storm sewer in the southerly portion of the site. Runoff will continue in an existing 48" RCP to outfall within Monument Creek adjacent to the easterly limits of Mark Dabbling Blvd.

The emergency spillway will consist of a 20' weir along the easterly end of the pond at an elevation of 6254.55. The 20' weir will convey developed undetained flows a depth of 0.32' and consist of 12" depth of type L soil riprap.

Outfall from EDB C to the existing 48" RCP increases flows by $Q_5=0.1$ cfs, $Q_{100}=2.0$ cfs. At the existing MH the pipe slope changes from 1.03% upstream to 25.70% downstream to outfall directly to Monument Creek. The existing outfall consists of a 25' long by 24' wide 5' depth of $d_{50}=30$ " riprap.

See Calculations in the Appendix

4-STEP PROCESS

RUNOFF REDUCTION

The total development disturbance is not changing with the Development Plan Amendment. Runoff reduction calculations were revised to reflect the Development Plan Amendment changes. The development addresses Low Impact Development strategies primarily through the utilization of landscape swales within sides and rear of proposed residential buildings and directing runoff from buildings and walkways through swales with minimal longitudinal grade prior to outfall to storm conveyance systems. Runoff reduction through routing of unconnected impervious areas through receiving swales and buffer areas was calculated utilizing MHFD UD-BMP Version 3.07. Overall reduction of WQCV for the development is 55%. See appendix for calculations.——

DRAINAGE METHODOLOGY

This drainage report was prepared in accordance to the criteria established in the City of Colorado Springs Drainage Criteria Manual Volumes 1 as revised January 2021 and 2 as revised December 2020.

The rational method for drainage basin study areas of less than 100 acres was utilized in the analysis. For the Rational Method, flows were calculated for the 2, 5, 10, 25, 50, and 100-year recurrence intervals. The average runoff coefficients, ‘C’ values, are taken from Table 6-6 and the Intensity-Duration-Frequency curves are taken from Figure 6-5 of the City Drainage Criteria Manual. Time of concentration for overland flow and storm drain or gutter flow are calculated per Section 3.2 of the City Drainage Criteria Manual. Calculations for the Rational Method are shown in the Appendix of this report.

Mile High Flood District methodology was utilized for determination of the conceptual extended detention basin design. Details and analysis of final storm drain conveyance and collection system will be developed in the final drainage report submitted with the re-plat of the Corporate Centre Filing No. 3 subdivision. The MHFD-Detention v_4.03 spreadsheet was utilized in development of extended detention basin sizing. Calculations are included in the appendix of this report.

A grading and erosion control plan has been approved by Colorado Springs Stormwater Engineering for the proposed phases of development. MHFD UD-Sewer calculations were utilized in the hydraulic grade line analysis.

SUMMARY

This Drainage Report Amendment is in conformance with the City of Colorado Springs Drainage Criteria Manual, Volumes 1&2, May 2014 editions (Volume 1 as revised January 2021 and Volume 2 as revised December 2020). Mark Dabling Cottages will require that flows be treated for water quality and be detained to historic levels prior to release from the site. Site runoff and storm drain and appurtenances will not adversely affect the downstream and surrounding developments. This report is in general conformance with all previously approved reports which included this site. Private storm facilities will be owned or maintained by the Homeowner's Association.

REFERENCES:

City of Colorado Springs Engineering Division Drainage Criteria Manual Volume 1 as revised January 2021 and Volume 2 as revised December 2020

“Study of the Dry Creek Drainage Basin”, prepared by KKBNA, dated February 1985

Urban Storm Drainage Criteria Manual, Volumes I-III, Mile High Flood District (MHFD)

FEMA Flood Insurance Rate Map Number 08041C0512 G, effective December 7, 2018

Natural Resources Conservation Service Web Soil Survey

“MASTER DEVELOPMENT DRAINAGE PLAN AND FINAL DRAINAGE REPORT FOR COTTAGES AT DRY CREEK”, prepared by Catamount Engineering, approved April 2023.

APPENDIX

CALCULATIONS

BASIN	AREA TOTAL (Acres)	C ₅	C ₁₀₀				CONVEYANCE TC						TT				
				Length (ft)	Height (ft)	TI (min)	Length (ft)	Height (ft)	C _v	Slope (%)	Velocity (fps)	TC (min)	TOTAL (min)	I ₅ (in/hr)	I ₁₀₀ (in/hr)	Q ₅ (c.f.s.)	Q ₁₀₀ (c.f.s.)
A1	1.80	0.78	0.87	45	1	3.0	1108	23	20	2.1%	2.9	6.4	9.4	4.2	7.1	5.9	11.1
ROOF	0.04	0.73	0.81														
PAVEMENT	1.49	0.90	0.96														
LANDSCAPE	0.27	0.12	0.39														
A2	3.20	0.35	0.55	153	1.5	16.8	830	18	7	2.2%	1.0	13.4	30.2	2.5	4.1	2.8	7.3
ROOF	0.92	0.73	0.81														
PAVEMENT	0.23	0.90	0.96														
LANDSCAPE	2.05	0.12	0.39														
A3	0.07	0.79	0.88	15	1	1.2	100	2	20	2.0%	2.8	0.6	5.0	5.2	8.7	0.3	0.5
ROOF	0.00	0.73	0.81										<i>MIN</i>				
PAVEMENT	0.06	0.90	0.96														
LANDSCAPE	0.01	0.12	0.39														
A4	0.18	0.17	0.42	25	6	2.9	0	0	7	0.0%	0.0	0.0	5.0	5.2	8.7	0.2	0.7
ROOF	0.00	0.73	0.81										<i>MIN</i>				
GRAVEL	0.02	0.59	0.70														
LANDSCAPE	0.16	0.12	0.39														
B1	0.69	0.80	0.89	81	1.5	4.0	486	7	20	1.4%	2.4	3.4	7.4	4.6	7.7	2.5	4.7
ROOF	0.04	0.73	0.81														
PAVEMENT	0.57	0.90	0.96														
LANDSCAPE	0.08	0.12	0.39														
B2	1.92	0.41	0.59	100	2.2	9.6	423	4.5	7	1.1%	0.7	9.8	19.3	3.1	5.3	2.5	6.0
ROOF	0.73	0.73	0.81														
PAVEMENT	0.15	0.90	0.96														
LANDSCAPE	1.04	0.12	0.39														
B3	0.13	0.73	0.81	22	0.4	2.6	120	2.4	7	2.0%	1.0	2.0	5.0	5.2	8.7	0.5	0.9
ROOF	0.13	0.73	0.81										<i>MIN</i>				
PAVEMENT	0.00	0.90	0.96														
LANDSCAPE	0.00	0.12	0.39														

Calculated by: DLM
Date: 24.01.03

BASIN	AREA TOTAL (Acres)	CONVEYANCE TC											TT				
		C ₅	C ₁₀₀	Length	Height	TI	Length	Height	C _v	Slope	Velocity	TC	TOTAL	I ₅	I ₁₀₀	Q ₅	Q ₁₀₀
				(ft)	(ft)	(min)	(ft)	(ft)		(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
B4	0.20	0.12	0.39	40	6	4.6	10	0.2	7	2.0%	1.0	0.2	5.0	5.2	8.7	0.1	0.7
ROOF	0.00	0.73	0.81										MIN				
PAVEMENT	0.00	0.90	0.96														
LANDSCAPE	0.20	0.12	0.39														
C1	0.60	0.80	0.89	79	1.5	3.9	297	5	20	1.7%	2.6	1.9	5.8	4.9	8.3	2.4	4.4
ROOF	0.03	0.73	0.81														
PAVEMENT	0.50	0.90	0.96														
LANDSCAPE	0.07	0.12	0.39														
C2	1.42	0.36	0.56	100	2	10.6	242	4	7	1.7%	0.9	4.5	15.1	3.5	5.9	1.8	4.7
ROOF	0.42	0.73	0.81														
PAVEMENT	0.11	0.90	0.96														
LANDSCAPE	0.89	0.12	0.39														
C3	0.58	0.78	0.87	56	1.2	3.4	219	3	20	1.4%	2.3	1.6	8.6	4.4	7.3	2.0	3.7
ROOF	0.10	0.73	0.81														
PAVEMENT	0.41	0.90	0.96			POND-C	180	2.5	7	1.4%	0.8	3.6					
LANDSCAPE	0.07	0.12	0.39														
D1	1.91	0.12	0.39	73	6.5	7.3	1036	20	7	1.9%	1.0	17.8	25.1	2.7	4.6	0.6	3.4
ROOF	0.00	0.73	0.81														
PAVEMENT	0.00	0.90	0.96														
LANDSCAPE	1.91	0.12	0.39														
D2	1.17	0.12	0.39	70	14	5.5	488	4	7	0.8%	0.6	12.8	18.3	3.2	5.4	0.5	2.5
ROOF	0.00	0.73	0.81														
PAVEMENT	0.00	0.90	0.96														
LANDSCAPE	1.17	0.12	0.39														
D3	1.19	0.12	0.39	64	14	5.1	428	4.5	7	1.1%	0.7	9.9	15.1	3.5	5.9	0.5	2.7
ROOF	0.00	0.73	0.81														
PAVEMENT	0.00	0.90	0.96														
LANDSCAPE	1.19	0.12	0.39														
D4	0.06	0.38	0.58	12	2	1.8	22	3	20	13.6%	7.4	0.0	5.0	5.2	8.7	0.1	0.3
ROOF	0.00	0.73	0.81										MIN				
PAVEMENT	0.02	0.90	0.96														
LANDSCAPE	0.04	0.12	0.39														

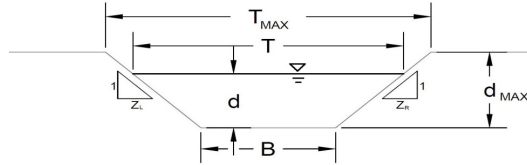
Calculated by: DLM
Date: 24.01.03

DESIGN POINT	AREA TOTAL (Acres)	C ₅	C ₁₀₀	TT		I ₅ (in/hr)	I ₁₀₀ (in/hr)	Q ₅ (c.f.s.)	Q ₁₀₀ (c.f.s.)
				TOTAL (min)					
1	2.00	0.48	0.65	15.1		3.5	5.9	3.4	7.6
BASIN C2	1.42	0.36	0.56	15.1					
BASIN C3	0.58	0.78	0.87	8.6					
P1	5.00	0.51	0.67	30.2		2.5	4.1	6.2	13.8
BASIN A1	1.80	0.78	0.87	9.4					
BASIN A2	3.20	0.35	0.55	30.2					
P2	5.07	0.51	0.67	30.2		2.5	4.1	6.4	14.1
BASIN A3	0.07	0.79	0.88	5.0					
PIPE DESIGN POINT P1	5.00	0.51	0.67	30.2					
P3	2.61	0.52	0.67	19.3		3.1	5.3	4.2	9.2
BASIN B1	0.69	0.80	0.89	7.4					
BASIN B2	1.92	0.41	0.59	19.3					
P4	2.74	0.53	0.68	19.3		3.1	5.3	4.5	9.8
BASIN B3	0.13	0.73	0.81	5.0					
PIPE DESIGN POINT P3	2.61	0.52	0.67	19.3					
POND A	5.25	0.50	0.66	30.2		2.5	4.1	6.5	14.4
BASIN A4	0.18	0.17	0.42	5.00					
PIPE DESIGN POINT P2	5.07	0.51	0.67	30.2					
POND B	2.94	0.50	0.66	19.3		3.1	5.3	4.6	10.2
BASIN B4	0.20	0.12	0.39	5.0					
PIPE DESIGN POINT P4	2.74	0.53	0.68	19.3					
POND C	2.60	0.56	0.70	15.1		3.5	5.9	5.1	10.8
BASIN C1	0.60	0.80	0.89	5.8					
DESIGN POINT 1	2.00	0.48	0.65	15.1					

Calculated by: DLM
Date: 24.01.03

AREA INLET IN A TRAPEZOIDAL GRASS-LINED CHANNEL

Cottages at Dry Creek
Basin A2



Grass Type	Limiting Manning's n
A	0.06
B	0.04
C	0.033
D	0.03
E	0.024

Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E)
 Manning's n (Leave cell D16 blank to manually enter an n value)
 Channel Invert Slope
 Bottom Width
 Left Side Slope
 Right Side Slope

A, B, C, D or E
 n = 0.022
 S₀ = 0.0200 ft/ft
 B = 3.00 ft
 Z1 = 33.00 ft/ft
 Z2 = 33.00 ft/ft

Check one of the following soil types:

Soil Type:	Max. Velocity (V _{MAX})	Max Froude No. (F _{MAX})
Sandy	5.0 fps	0.50
Non-Sandy	7.0 fps	0.80

Choose One:

Sandy

Non-Sandy

Max. Allowable Top Width of Channel for Minor & Major Storm
 Max. Allowable Water Depth in Channel for Minor & Major Storm

	Minor Storm	Major Storm	
T _{MAX}	26.00	26.00	feet
d _{MAX}	1.00	1.00	feet

Maximum Channel Capacity Based On Allowable Top Width

Max. Allowable Top Width
 Water Depth
 Flow Area
 Wetted Perimeter
 Hydraulic Radius
 Manning's n based on NRCS Vegetal Retardance
 Flow Velocity
 Velocity-Depth Product
 Hydraulic Depth
 Froude Number
Max. Flow Based On Allowable Top Width

	Minor Storm	Major Storm	
T _{MAX}	26.00	26.00	feet
d	0.35	0.35	feet
A	5.05	5.05	sq ft
P	26.01	26.01	feet
R	0.19	0.19	feet
n	0.022	0.022	
V	3.21	3.21	fps
VR	0.62	0.62	ft ² /s
D	0.19	0.19	feet
Fr	1.28	1.28	
Q _T	16.23	16.23	cfs

Maximum Channel Capacity Based On Allowable Water Depth

Max. Allowable Water Depth
 Top Width
 Flow Area
 Wetted Perimeter
 Hydraulic Radius
 Manning's n based on NRCS Vegetal Retardance
 Flow Velocity
 Velocity-Depth Product
 Hydraulic Depth
 Froude Number
Max. Flow Based On Allowable Water Depth

	Minor Storm	Major Storm	
d _{MAX}	1.00	1.00	feet
T	69.00	69.00	feet
A	36.00	36.00	square feet
P	69.03	69.03	feet
R	0.52	0.52	feet
n	0.022	0.022	
V	6.21	6.21	fps
VR	3.24	3.24	ft ² /s
D	0.52	0.52	feet
Fr	1.51	1.51	
Q _d	223.40	223.40	cfs

Allowable Channel Capacity Based On Channel Geometry

MINOR STORM Allowable Capacity is based on Top Width Criterion
MAJOR STORM Allowable Capacity is based on Top Width Criterion

	Minor Storm	Major Storm	
Q _{allow}	16.23	16.23	cfs
d _{allow}	0.35	0.35	ft

Water Depth in Channel Based On Design Peak Flow

Design Peak Flow
Water Depth
 Top Width
 Flow Area
 Wetted Perimeter
 Hydraulic Radius
 Manning's n based on NRCS Vegetal Retardance
 Flow Velocity
 Velocity-Depth Product
 Hydraulic Depth
 Froude Number

	Minor Storm	Major Storm	
Q _d	2.80	7.30	cfs
d	0.16	0.25	feet
T	13.75	19.40	feet
A	1.36	2.78	square feet
P	13.76	19.40	feet
R	0.10	0.14	feet
n	0.022	0.022	
V	2.05	2.62	fps
VR	0.20	0.38	ft ² /s
D	0.10	0.14	feet
Fr	1.15	1.22	

Warning 04

Minor storm max. allowable capacity GOOD - greater than flow given on sheet 'Q-Peak'
 Major storm max. allowable capacity GOOD - greater than flow given on sheet 'Q-Peak'

AREA INLET IN A TRAPEZOIDAL GRASS-LINED CHANNEL

Cottages at Dry Creek
Basin A2

Inlet Design Information (Input)

Type of Inlet

Inlet Type = CDOT Type D (In Series & Depressed)

Angle of Inclined Grate (must be ≤ 30 degrees)

Width of Grate

Length of Grate

Open Area Ratio

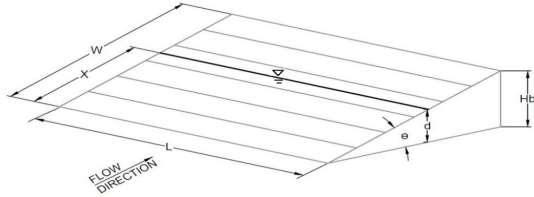
Height of Inclined Grate

Clogging Factor

Grate Discharge Coefficient

Orifice Coefficient

Weir Coefficient



$\theta =$	0.00	degrees
$W =$	3.00	feet
$L =$	6.00	feet
$A_{RATIO} =$	0.70	
$H_B =$	0.00	feet
$C_f =$	0.38	
$C_d =$	0.72	
$C_o =$	0.48	
$C_w =$	1.53	

Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)

	MINOR	MAJOR
$d =$	1.16	1.25

Grate Capacity as a Weir

Submerged Side Weir Length

Inclined Side Weir Flow

Base Weir Flow

Interception without Clogging

Interception with Clogging

	MINOR	MAJOR	
$X =$	6.00	6.00	feet
$Q_{ws} =$	20.16	22.43	cfs
$Q_{wb} =$	14.40	16.02	cfs
$Q_{wi} =$	54.73	60.87	cfs
$Q_{wi} =$	34.20	38.04	cfs

Grate Capacity as an Orifice

Interception without Clogging

Interception with Clogging

$Q_{oi} =$	52.01	53.89	cfs
$Q_{oii} =$	32.51	33.68	cfs

Total Inlet Interception Capacity (assumes clogged condition)

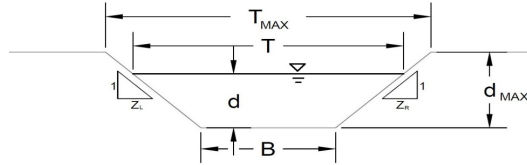
Inlet Capacity IS GOOD for Minor and Major Storms ($> Q_{PEAK}$)

$Q_a =$	32.51	33.68	cfs
Bypassed Flow, $Q_b =$	0.00	0.00	cfs
Capture Percentage = $Q_a/Q_o = C\%$	100	100	%

Warning 04: Froude No. exceeds USDCM Volume I recommendation.

AREA INLET IN A TRAPEZOIDAL GRASS-LINED CHANNEL

Cottages at Dry Creek
Basin B2



Grass Type	Limiting Manning's n
A	0.06
B	0.04
C	0.033
D	0.03
E	0.024

Analysis of Trapezoidal Grass-Lined Channel Using SCS Method

NRCS Vegetal Retardance (A, B, C, D, or E)
Manning's n (Leave cell D16 blank to manually enter an n value)
Channel Invert Slope
Bottom Width
Left Side Slope
Right Side Slope

A, B, C, D or E
n = 0.022
S₀ = 0.0080 ft/ft
B = 3.00 ft
Z₁ = 33.00 ft/ft
Z₂ = 33.00 ft/ft

Check one of the following soil types:

Soil Type:	Max. Velocity (V _{MAX})	Max Froude No. (F _{MAX})
Sandy	5.0 fps	0.50
Non-Sandy	7.0 fps	0.80

Choose One:

Sandy

Non-Sandy

Max. Allowable Top Width of Channel for Minor & Major Storm
Max. Allowable Water Depth in Channel for Minor & Major Storm

	Minor Storm	Major Storm	
T _{MAX} =	26.00	26.00	feet
d _{MAX} =	1.00	1.00	feet

Maximum Channel Capacity Based On Allowable Top Width

Max. Allowable Top Width
Water Depth
Flow Area
Wetted Perimeter
Hydraulic Radius
Manning's n based on NRCS Vegetal Retardance
Flow Velocity
Velocity-Depth Product
Hydraulic Depth
Froude Number
Max. Flow Based On Allowable Top Width

	Minor Storm	Major Storm	
T _{MAX} =	26.00	26.00	ft
d =	0.35	0.35	ft
A =	5.05	5.05	sq ft
P =	26.01	26.01	ft
R =	0.19	0.19	ft
n =	0.022	0.022	
V =	2.03	2.03	fps
VR =	0.39	0.39	ft ² /s
D =	0.19	0.19	ft
Fr =	0.81	0.81	
Q _T =	10.27	10.27	cfs

Maximum Channel Capacity Based On Allowable Water Depth

Max. Allowable Water Depth
Top Width
Flow Area
Wetted Perimeter
Hydraulic Radius
Manning's n based on NRCS Vegetal Retardance
Flow Velocity
Velocity-Depth Product
Hydraulic Depth
Froude Number
Max. Flow Based On Allowable Water Depth

	Minor Storm	Major Storm	
d _{MAX} =	1.00	1.00	feet
T =	69.00	69.00	feet
A =	36.00	36.00	square feet
P =	69.03	69.03	feet
R =	0.52	0.52	feet
n =	0.022	0.022	
V =	3.92	3.92	fps
VR =	2.05	2.05	ft ² /s
D =	0.52	0.52	feet
Fr =	0.96	0.96	
Q _d =	141.29	141.29	cfs

Allowable Channel Capacity Based On Channel Geometry

MINOR STORM Allowable Capacity is based on Top Width Criterion
MAJOR STORM Allowable Capacity is based on Top Width Criterion

	Minor Storm	Major Storm	
Q _{allow} =	10.27	10.27	cfs
d _{allow} =	0.35	0.35	ft

Water Depth in Channel Based On Design Peak Flow

Design Peak Flow
Water Depth
Top Width
Flow Area
Wetted Perimeter
Hydraulic Radius
Manning's n based on NRCS Vegetal Retardance
Flow Velocity
Velocity-Depth Product
Hydraulic Depth
Froude Number

	Minor Storm	Major Storm	
Q _d =	2.50	6.00	cfs
d =	0.19	0.28	feet
T =	15.54	21.34	feet
A =	1.76	3.38	square feet
P =	15.55	21.35	feet
R =	0.11	0.16	feet
n =	0.022	0.022	
V =	1.42	1.77	fps
VR =	0.16	0.28	ft ² /s
D =	0.11	0.16	feet
Fr =	0.74	0.79	

Minor storm max. allowable capacity GOOD - greater than flow given on sheet 'Q-Peak'
Major storm max. allowable capacity GOOD - greater than flow given on sheet 'Q-Peak'

AREA INLET IN A TRAPEZOIDAL GRASS-LINED CHANNEL

Cottages at Dry Creek
Basin B2

Inlet Design Information (Input)

Type of Inlet

Inlet Type = CDOT Type D (In Series & Depressed)

Angle of Inclined Grate (must be ≤ 30 degrees)

Width of Grate

Length of Grate

Open Area Ratio

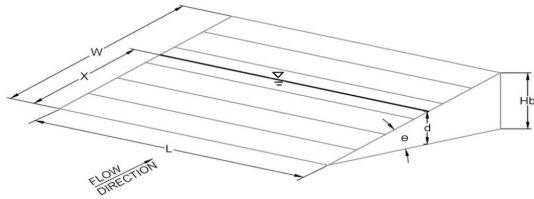
Height of Inclined Grate

Clogging Factor

Grate Discharge Coefficient

Orifice Coefficient

Weir Coefficient



θ =	0.00	degrees
W =	3.00	feet
L =	6.00	feet
ARATIO =	0.70	
H_b =	0.00	feet
C_f =	0.38	
C_d =	0.72	
C_o =	0.48	
C_w =	1.53	

Water Depth at Inlet (for depressed inlets, 1 foot is added for depression)

	MINOR	MAJOR
d =	1.19	1.28

Grate Capacity as a Weir

Submerged Side Weir Length

Inclined Side Weir Flow

Base Weir Flow

Interception without Clogging

Interception with Clogging

	MINOR	MAJOR	
X =	6.00	6.00	feet
Q_{ws} =	20.87	23.23	cfs
Q_{wb} =	14.91	16.59	cfs
Q_{wi} =	56.65	63.04	cfs
Q_{wi} =	35.41	39.40	cfs

Grate Capacity as an Orifice

Interception without Clogging

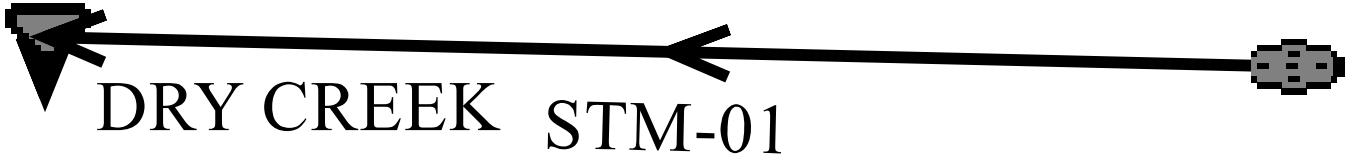
Interception with Clogging

Q_{oi} =	52.62	54.52	cfs
Q_{oii} =	32.88	34.08	cfs

Total Inlet Interception Capacity (assumes clogged condition)

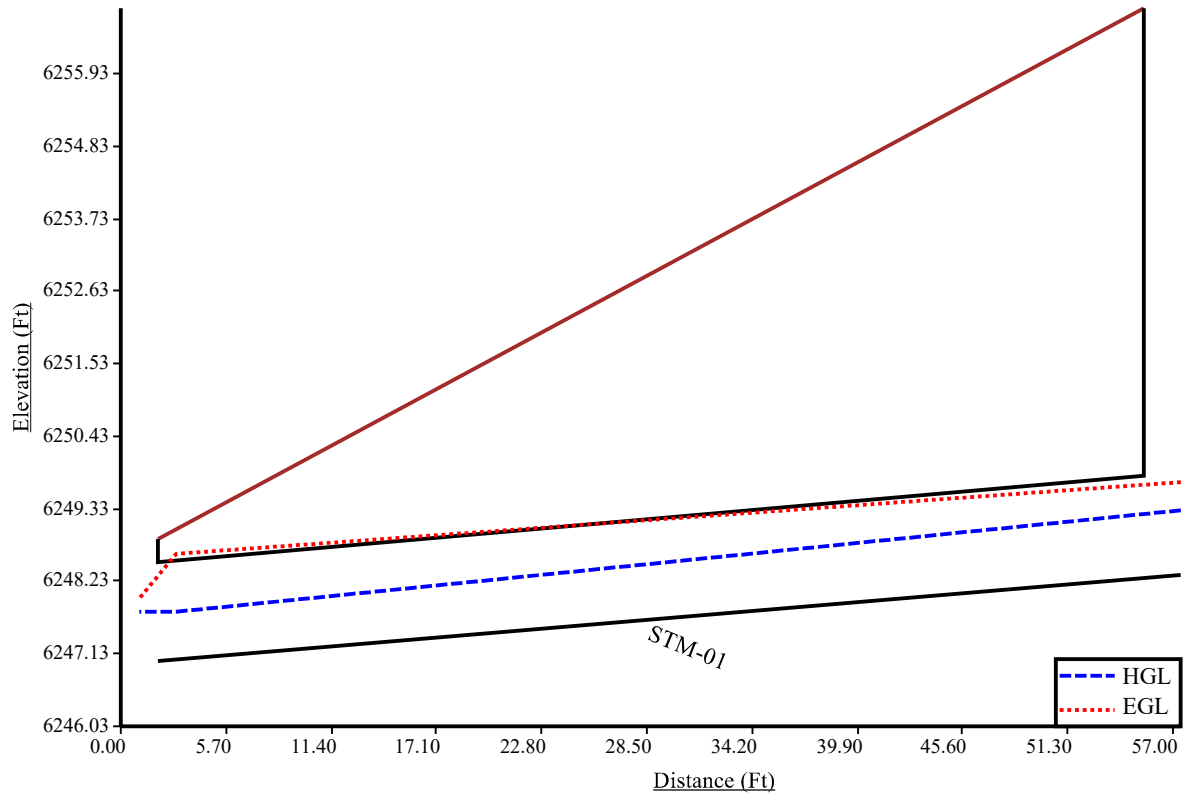
Inlet Capacity IS GOOD for Minor and Major Storms (> Q PEAK)

Q_a =	32.88	34.08	cfs
Bypassed Flow, Q_b =	0.00	0.00	cfs
Capture Percentage = Q_a/Q_o = C%	100	100	%



DRY CREEK STM-01

STM-01 5YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/14/2023 11:20:23 AM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 1 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 5
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6247.77

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
DRY CREEK	6248.87	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-01	6256.92	6.40	6.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

		Local Contribution				Total Design Flow				
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment
DRY CREEK	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-01	0.00	0.00	0.00	0.00	6.40	0.00	0.00	0.00	6.40	

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Manning's n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-01	57.41	6247.02	2.3	6248.33	0.015	0.00	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

	Full Flow Capacity	Critical Flow	Normal Flow	

Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
STM-01	13.79	7.80	11.74	5.24	8.62	7.66	1.81	Supercritical	6.40	0.00	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

		Existing		Calculated		Used				
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-01	6.40	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6247.77

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-01	6247.02	6248.33	0.00	0.00	6247.77	6249.31	6248.65	1.09	6249.74

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi}² / (2 * g)

- Lateral loss = $V_{fo}^2 / (2 * g)$ - Junction Loss $K * V_{fi}^2 / (2 * g)$.
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft

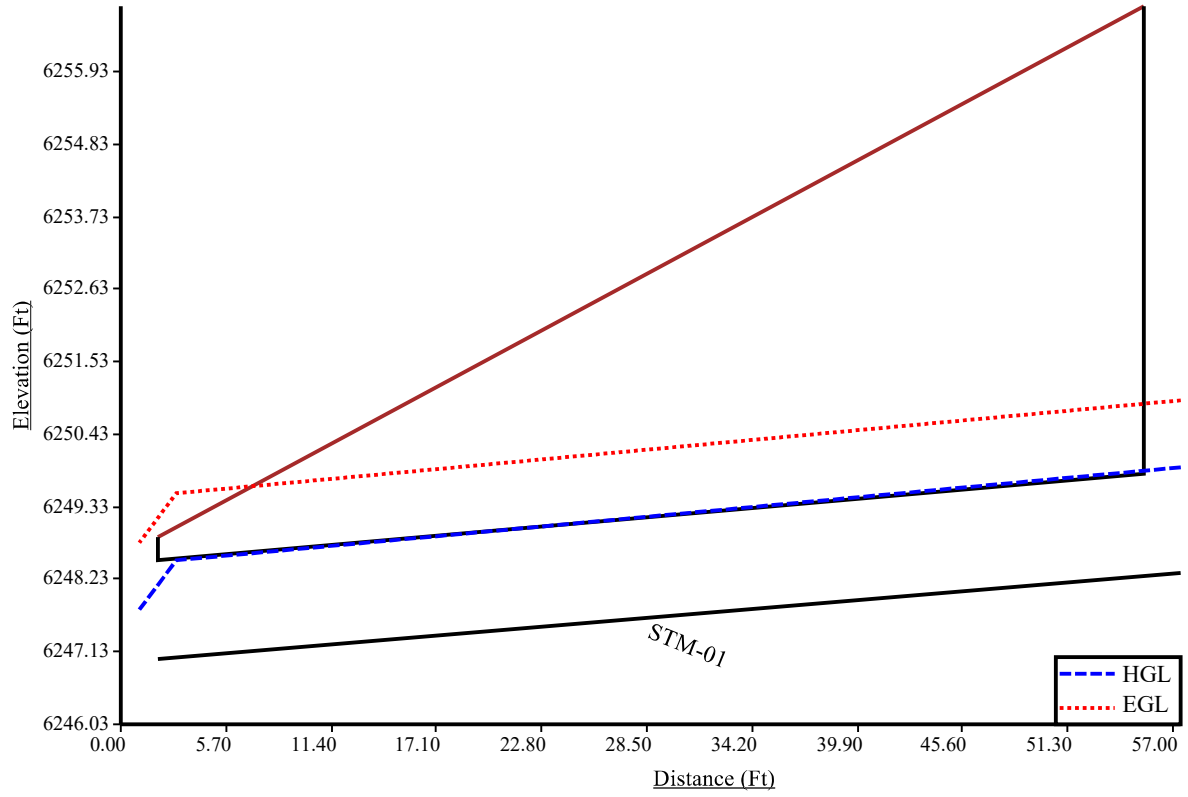
The minimum trench width is 2.00 ft

					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-01	57.41	2.50	4.00	4.92	0.00	2.39	0.14	16.68	9.13	6.88	96.27	Sewer Too Shallow

Total earth volume for sewer trenches = 96 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: $(\text{equivalent diameter in inches} / 12) + 1$ inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

STM-01 100YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/14/2023 10:57:14 AM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 1 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6247.77

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
FS-EDB A	6248.87	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-01	6256.92	14.30	14.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

		Local Contribution				Total Design Flow				
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment
FS-EDB A	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-01	0.00	0.00	0.00	0.00	14.30	0.00	0.00	0.00	14.30	

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-01	57.41	6247.02	2.3	6248.33	0.015	0.00	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

	Full Flow Capacity	Critical Flow	Normal Flow	

STM-01	6247.02	6248.33	0.00	0.00	6248.52	6249.93	6249.54	1.41	6250.95
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- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ^ 2/(2*g)
- Lateral loss = V_{fo} ^ 2/(2*g)- Junction Loss K * V_{fi} ^ 2/(2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

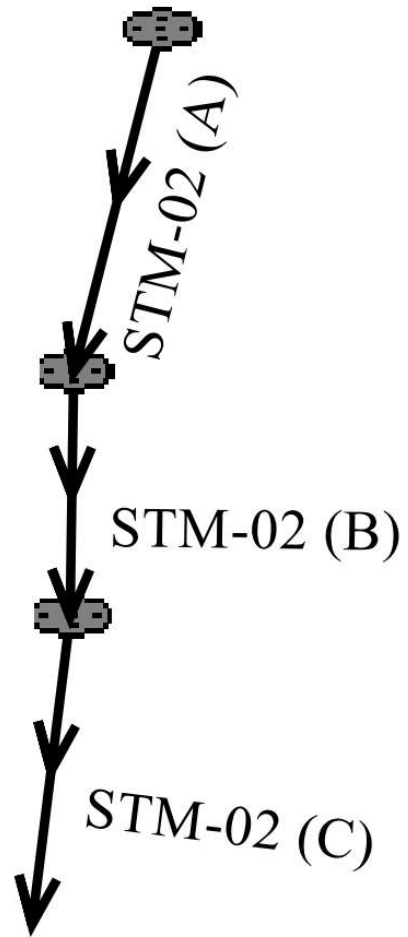
Excavation Estimate:

The trench side slope is 1.0 ft/ft
The minimum trench width is 2.00 ft

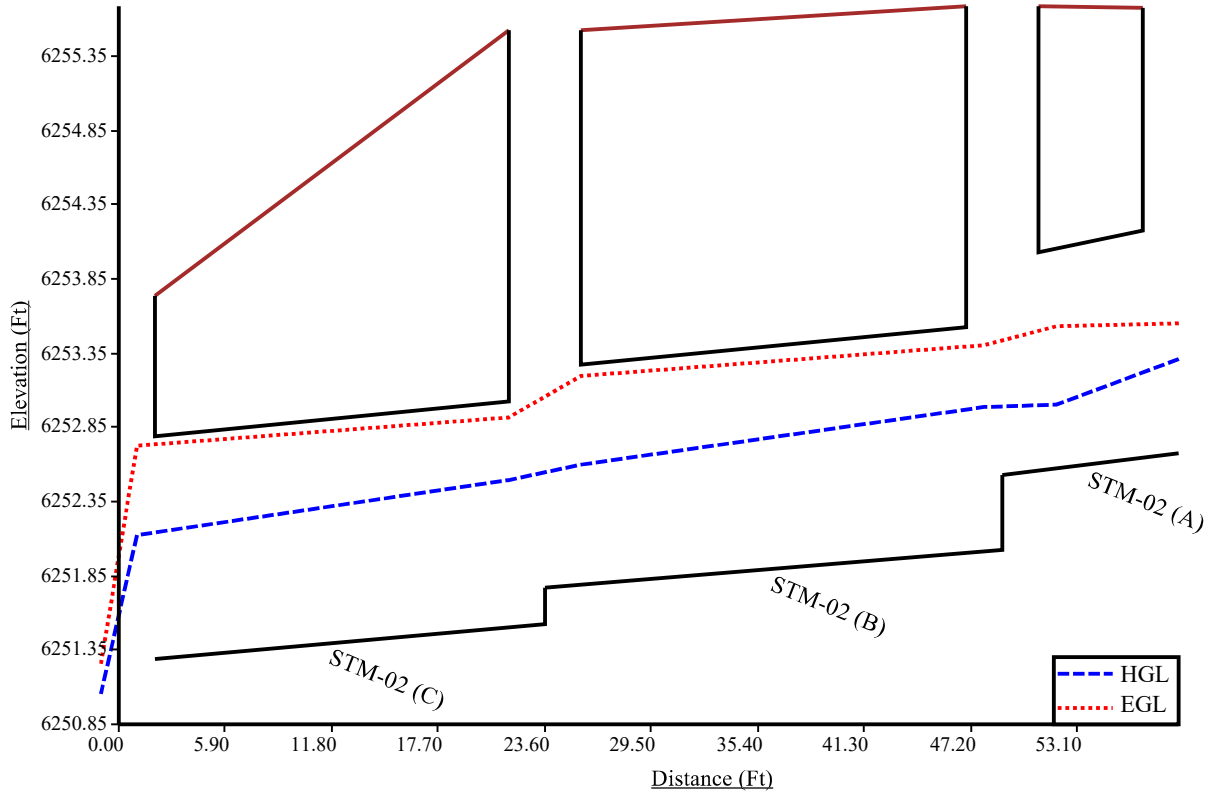
					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-01	57.41	2.50	4.00	4.92	0.00	2.39	0.14	16.68	9.13	6.88	96.27	Sewer Too Shallow

Total earth volume for sewer trenches = 96 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.



STM-02 5YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/14/2023 3:11:27 PM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 2 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 5
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6251.06

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
FOREBAY	6253.74	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-02 (C)	6255.53	6.30	0.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-02 (B)	6255.69	6.20	3.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-02 (A)	6255.68	2.80	2.80	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

		Local Contribution				Total Design Flow				
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment
FOREBAY	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-02 (C)	0.00	0.00	0.00	0.00	0.30	0.00	0.00	0.00	6.30	
STM-02 (B)	0.00	0.00	0.00	0.00	3.50	0.00	0.00	0.00	6.20	
STM-02 (A)	0.00	0.00	0.00	0.00	2.80	0.00	0.00	0.00	2.80	

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-02 (C)	23.60	6251.29	1.0	6251.53	0.013	0.00	0.00	CIRCULAR	18.00 in	18.00 in
STM-02 (B)	25.34	6251.78	1.0	6252.03	0.013	0.05	0.00	CIRCULAR	18.00 in	18.00 in

STM-02 (A)	9.78	6252.53	1.5	6252.68	0.013	0.05	0.00	CIRCULAR	18.00 in	18.00 in
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Sewer Flow Summary:

Element Name	Full Flow Capacity		Critical Flow		Normal Flow				Flow (cfs)	Surcharged Length (ft)	Comment
	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition			
STM-02 (C)	10.53	5.96	11.64	5.21	10.03	6.23	1.33	Supercritical	6.30	0.00	
STM-02 (B)	10.53	5.96	11.55	5.18	9.93	6.20	1.34	Supercritical	6.20	0.00	
STM-02 (A)	12.90	7.30	7.62	3.93	5.70	5.83	1.75	Supercritical	2.80	0.00	

- A Froude number of 0 indicates that pressurized flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

Element Name	Peak Flow (cfs)	Cross Section	Existing		Calculated		Used			Comment
			Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	
STM-02 (C)	6.30	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
STM-02 (B)	6.20	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
STM-02 (A)	2.80	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6251.06

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-02 (C)	6251.29	6251.53	0.00	0.00	6252.13	6252.50	6252.73	0.19	6252.92
STM-02 (B)	6251.78	6252.03	0.01	0.00	6252.60	6252.99	6253.20	0.21	6253.41
STM-02 (A)	6252.53	6252.68	0.00	0.00	6253.01	6253.32	6253.54	0.02	6253.56

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * $V_{fi}^2 / (2 * g)$
- Lateral loss = $V_{fo}^2 / (2 * g)$ - Junction Loss K * $V_{fi}^2 / (2 * g)$.
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft
 The minimum trench width is 2.00 ft

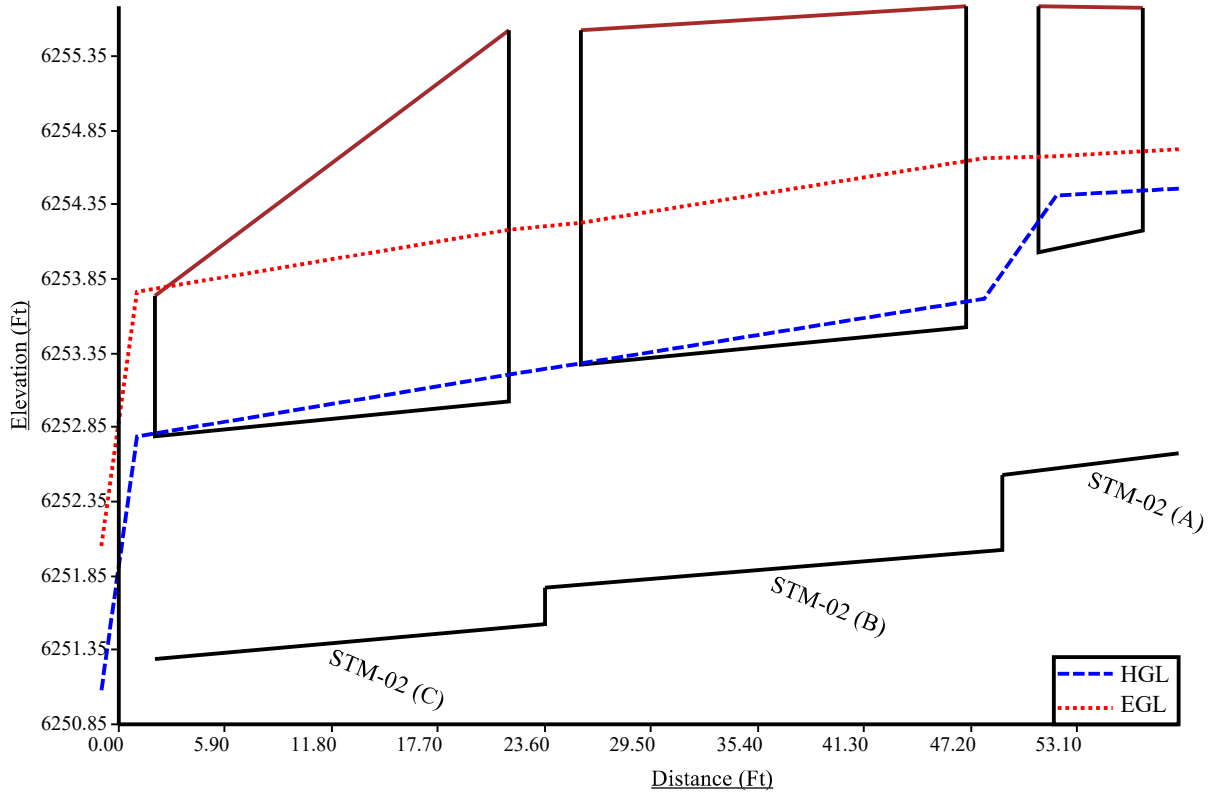
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		
STM-02 (C)	23.60	2.50	4.00	4.92	0.00	2.99	0.74	7.50	4.54	2.29	15.32	Sewer Too Shallow
STM-02 (B)	25.34	2.50	4.00	4.92	7.01	4.30	2.05	6.82	4.20	1.95	20.54	
STM-02 (A)	9.78	2.50	4.00	4.92	5.81	3.70	1.45	5.50	3.54	1.29	6.50	

Total earth volume for sewer trenches = 42 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.

- Six inches for pipes less than 60 inches.
- Eight inches for all larger sizes.

STM-02 100YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/14/2023 3:14:37 PM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 2 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6251.06

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
FOREBAY	6253.74	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-02 (C)	6255.53	14.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-02 (B)	6255.69	13.80	6.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-02 (A)	6255.68	7.30	2.80	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

		Local Contribution				Total Design Flow				
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment
FOREBAY	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-02 (C)	0.00	0.00	0.00	0.00	0.20	0.00	0.00	0.00	14.00	
STM-02 (B)	0.00	0.00	0.00	0.00	6.50	0.00	0.00	0.00	13.80	
STM-02 (A)	0.00	0.00	0.00	0.00	2.80	0.00	0.00	0.00	7.30	

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-02 (C)	23.60	6251.29	1.0	6251.53	0.013	0.00	0.00	CIRCULAR	18.00 in	18.00 in
STM-02 (B)	25.34	6251.78	1.0	6252.03	0.013	0.05	0.00	CIRCULAR	18.00 in	18.00 in

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6251.06

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-02 (C)	6251.29	6251.53	0.00	0.00	6252.79	6253.21	6253.77	0.42	6254.19
STM-02 (B)	6251.78	6252.03	0.05	0.00	6253.29	6253.72	6254.23	0.44	6254.67
STM-02 (A)	6252.53	6252.68	0.01	0.00	6254.42	6254.46	6254.68	0.05	6254.73

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi}² / (2 * g)
- Lateral loss = V_{fo}² / (2 * g) - Junction Loss K * V_{fi}² / (2 * g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

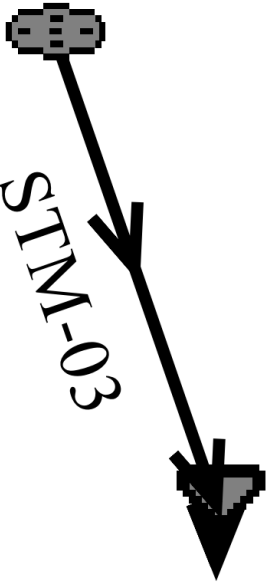
The trench side slope is 1.0 ft/ft

The minimum trench width is 2.00 ft

Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		
STM-02 (C)	23.60	2.50	4.00	4.92	0.00	2.99	0.74	7.50	4.54	2.29	15.32	Sewer Too Shallow
STM-02 (B)	25.34	2.50	4.00	4.92	7.01	4.30	2.05	6.82	4.20	1.95	20.54	
STM-02 (A)	9.78	2.50	4.00	4.92	5.81	3.70	1.45	5.50	3.54	1.29	6.50	

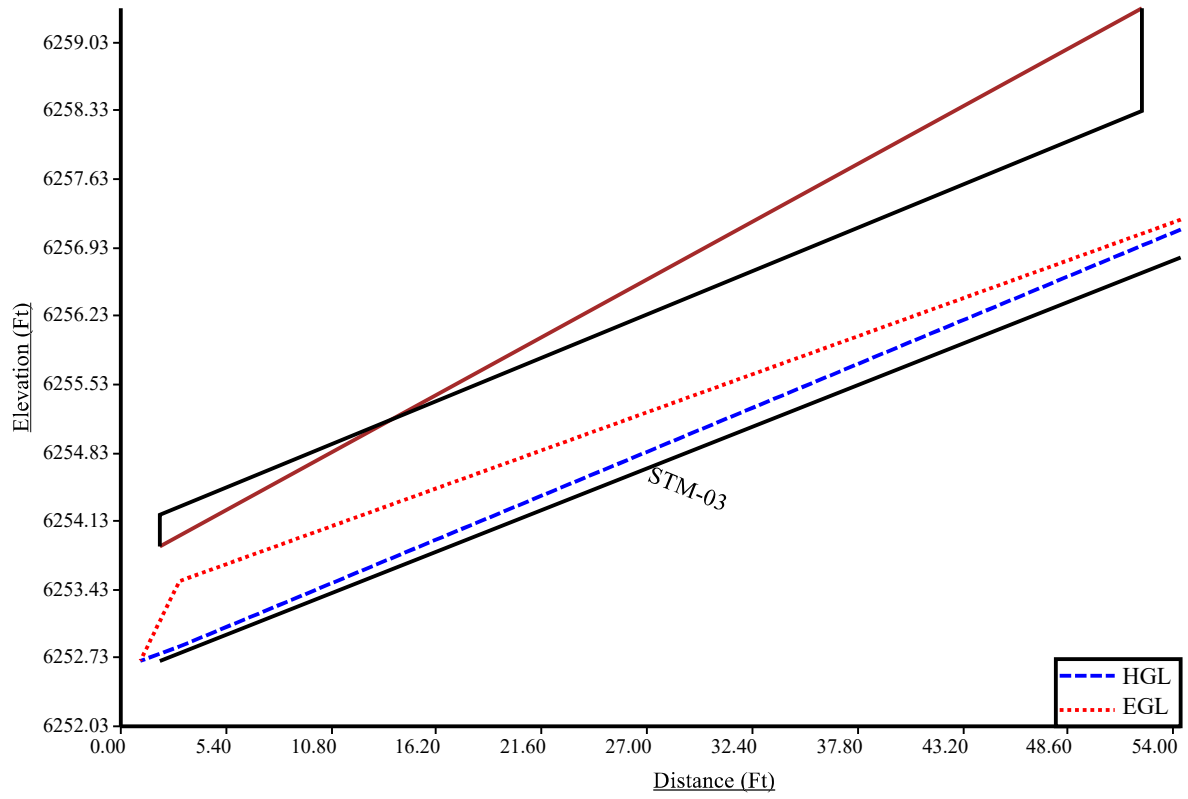
Total earth volume for sewer trenches = 42 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: $(\text{equivalent diameter in inches}/12)+1$ inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.



DRY CREEK

STM-03 5YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/14/2023 1:11:23 PM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 3 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 5
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6252.70

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
DRY CREEK SCULPTED DROP	6253.87	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-03	6259.38	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

		Local Contribution				Total Design Flow				
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment
DRY CREEK SCULPTED DROP	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.60	

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-03	54.38	6252.70	7.6	6256.83	0.013	0.00	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

	Full Flow Capacity	Critical Flow	Normal Flow	

Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
STM-03	29.04	16.43	3.45	2.54	1.79	6.57	3.63	Supercritical	0.60	0.00	

- A Froude number of 0 indicates that pressurized flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

		Existing		Calculated		Used				
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-03	0.60	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6252.70

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-03	6252.70	6256.83	0.00	0.00	6252.85	6257.12	6253.52	3.70	6257.22

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi}² / (2*g)

- Lateral loss = $V_{fo}^2 / (2 * g)$ - Junction Loss $K * V_{fi}^2 / (2 * g)$.
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft

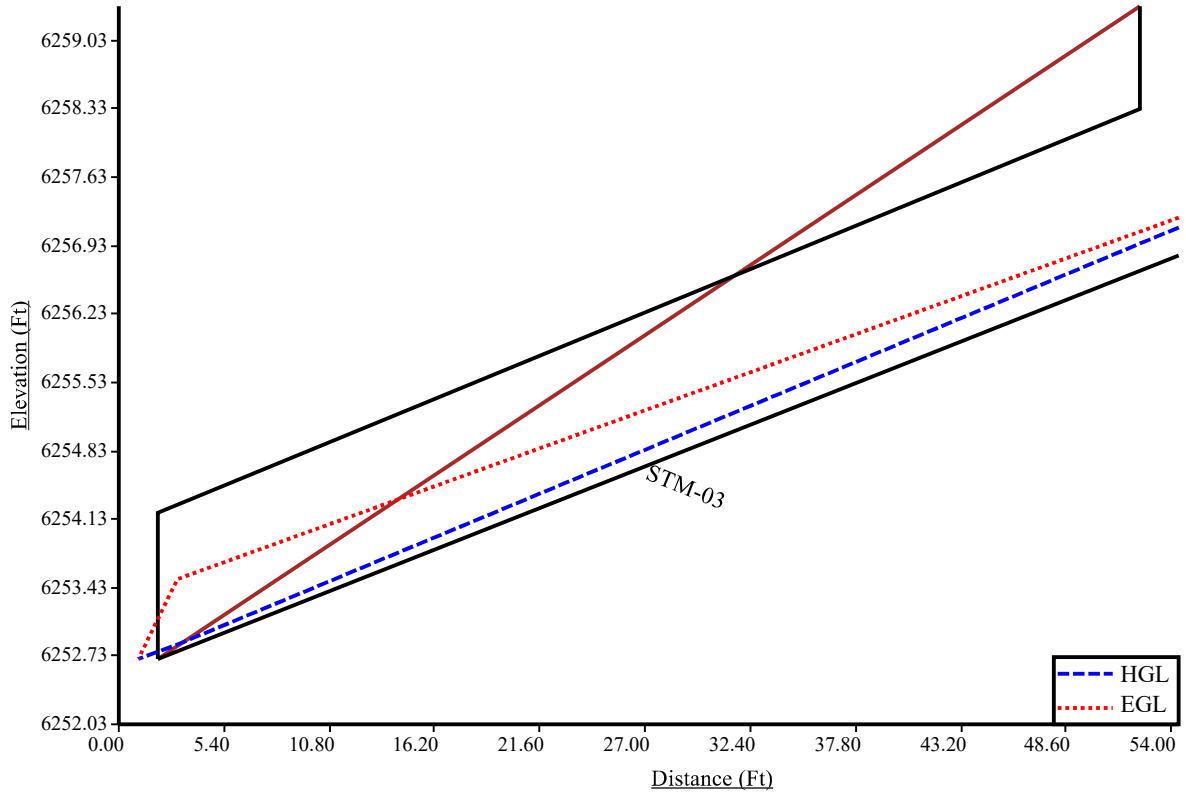
The minimum trench width is 2.00 ft

					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-03	54.38	2.50	4.00	4.92	0.00	1.71	0.00	4.92	3.09	0.84	19.63	Sewer Too Shallow

Total earth volume for sewer trenches = 20 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: $(\text{equivalent diameter in inches} / 12) + 1$ inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

STM-03 100YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/14/2023 1:09:13 PM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 3 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6252.70

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
DRY CREEK SCULPTED DROP	6253.87	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-03	6259.38	3.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

		Local Contribution				Total Design Flow				
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment
DRY CREEK SCULPTED DROP	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	3.40	

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Manning's n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-03	54.38	6252.70	7.6	6256.83	0.013	0.00	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

	Full Flow Capacity	Critical Flow	Normal Flow	

Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
STM-03	29.04	16.43	8.44	4.18	4.16	11.00	3.92	Supercritical	3.40	0.00	

- A Froude number of 0 indicates that pressurized flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

		Existing		Calculated		Used				
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-03	3.40	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6252.70

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-03	6252.70	6256.83	0.00	0.00	6253.04	6257.53	6254.92	2.88	6257.80

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi}² / (2 * g)

- Lateral loss = $V_{fo}^2 / (2 * g)$ - Junction Loss $K * V_{fi}^2 / (2 * g)$.
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft

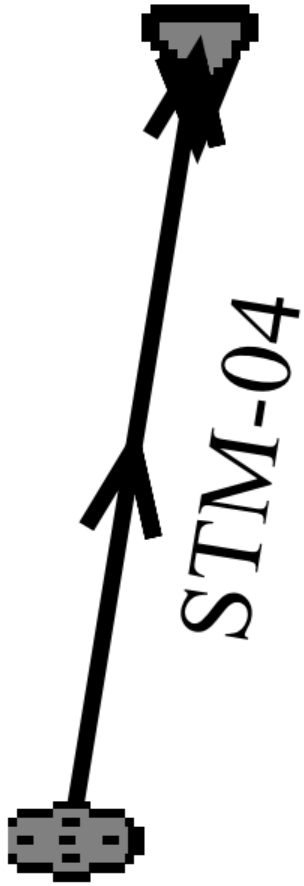
The minimum trench width is 2.00 ft

					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-03	54.38	2.50	4.00	4.92	0.00	1.71	0.00	4.92	3.09	0.84	19.63	Sewer Too Shallow

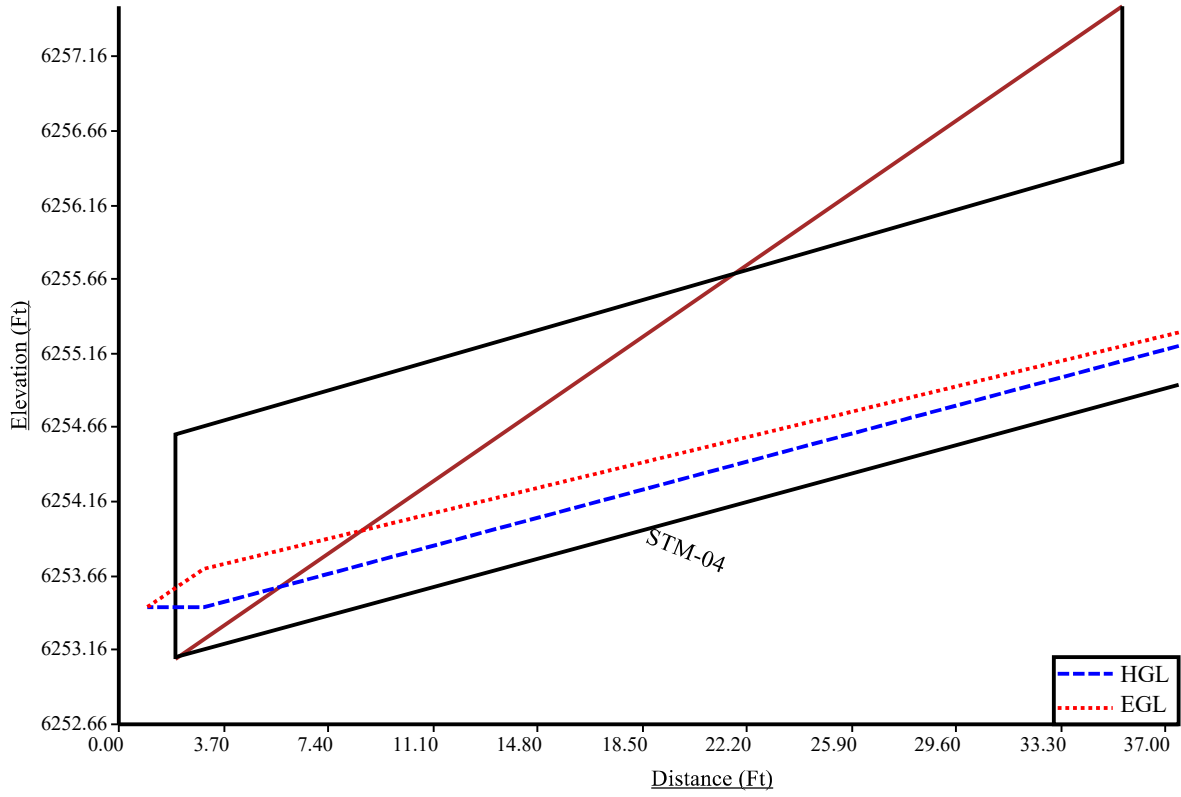
Total earth volume for sewer trenches = 20 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: $(\text{equivalent diameter in inches} / 12) + 1$ inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

DRY CREEK



STM-04 5YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/14/2023 1:24:49 PM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 4 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 5
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6253.45

Manhole Input Summary:

Element Name	Ground Elevation (ft)	Given Flow		Sub Basin Information						
		Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
DRY DREEK SCULPTED DROP	6253.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-04	6257.50	0.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
DRY DREEK SCULPTED DROP	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	Surface Water Present (Upstream)
STM-04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.50	Surface Water Present (Downstream)

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-04	37.45	6253.11	4.9	6254.95	0.013	0.00	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

Element Name	Full Flow Capacity		Critical Flow		Normal Flow				Flow (cfs)	Surcharged Length (ft)	Comment
	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition			
STM-04	23.31	13.19	3.14	2.42	1.82	5.34	2.92	Supercritical	0.50	0.00	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

Element Name	Peak Flow (cfs)	Cross Section	Existing		Calculated		Used			Comment
			Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	
STM-04	0.50	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6253.45

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-04	6253.11	6254.95	0.00	0.00	6253.45	6255.21	6253.71	1.59	6255.30

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.

- Bend loss = Bend K * V_{fi} ^ 2/(2*g)
- Lateral loss = V_{fo} ^ 2/(2*g)- Junction Loss K * V_{fi} ^ 2/(2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft

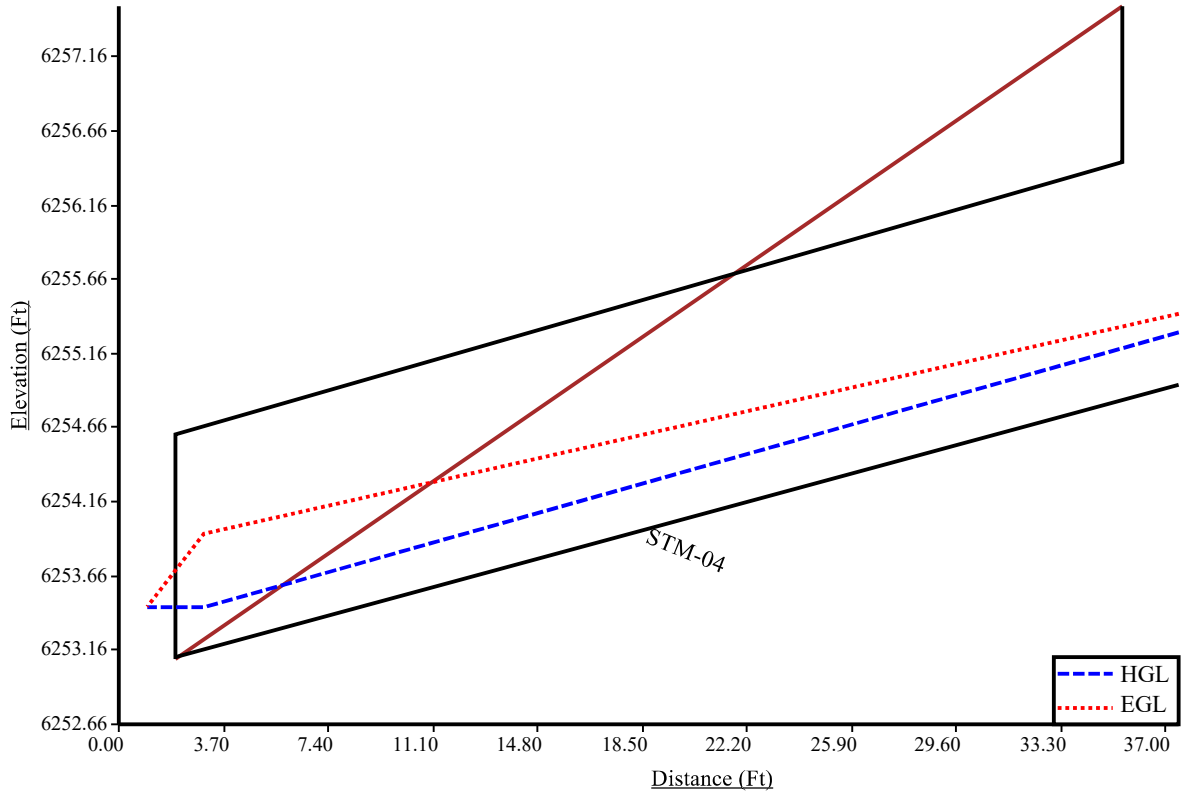
The minimum trench width is 2.00 ft

					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-04	37.45	2.50	4.00	4.92	0.00	0.53	0.00	4.92	3.09	0.84	9.47	Sewer Too Shallow

Total earth volume for sewer trenches = 9 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

STM-04 100YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/14/2023 1:22:59 PM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 4 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6253.45

Manhole Input Summary:

Element Name	Ground Elevation (ft)	Given Flow		Sub Basin Information						
		Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
DRY DREEK SCULPTED DROP	6253.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-04	6257.50	0.90	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
DRY DREEK SCULPTED DROP	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	Surface Water Present (Upstream)
STM-04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.90	Surface Water Present (Downstream)

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-04	37.45	6253.11	4.9	6254.95	0.013	0.00	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

	Full Flow Capacity		Critical Flow		Normal Flow						
Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
STM-04	23.31	13.19	4.24	2.83	2.42	6.37	3.02	Supercritical	0.90	0.00	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-04	0.90	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6253.45

	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
Element Name	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-04	6253.11	6254.95	0.00	0.00	6253.45	6255.30	6253.95	1.48	6255.43

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.

- Bend loss = Bend K * V_{fi} ^ 2/(2*g)
- Lateral loss = V_{fo} ^ 2/(2*g)- Junction Loss K * V_{fi} ^ 2/(2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

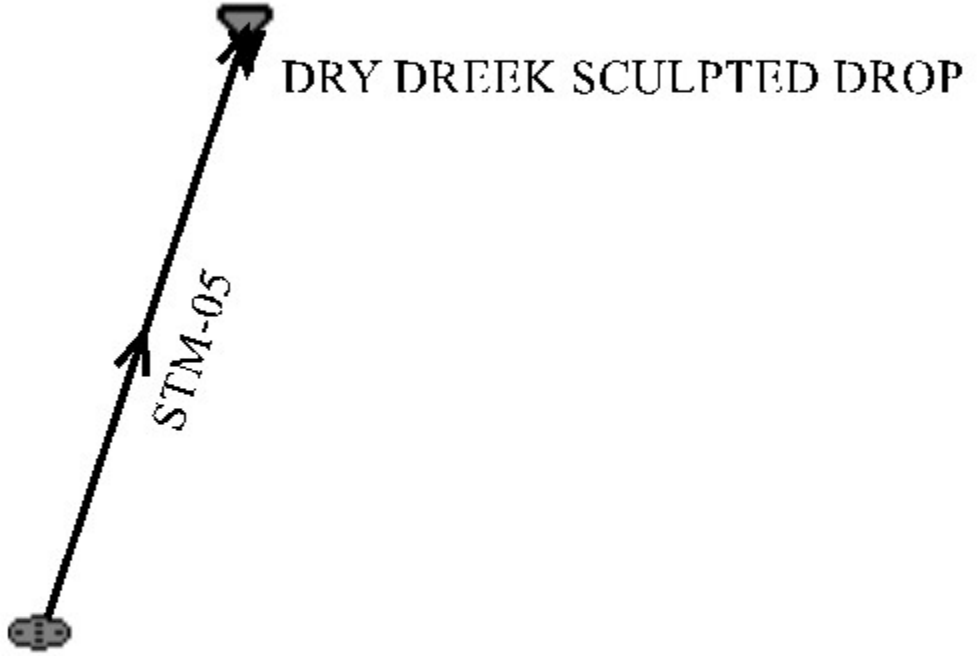
The trench side slope is 1.0 ft/ft

The minimum trench width is 2.00 ft

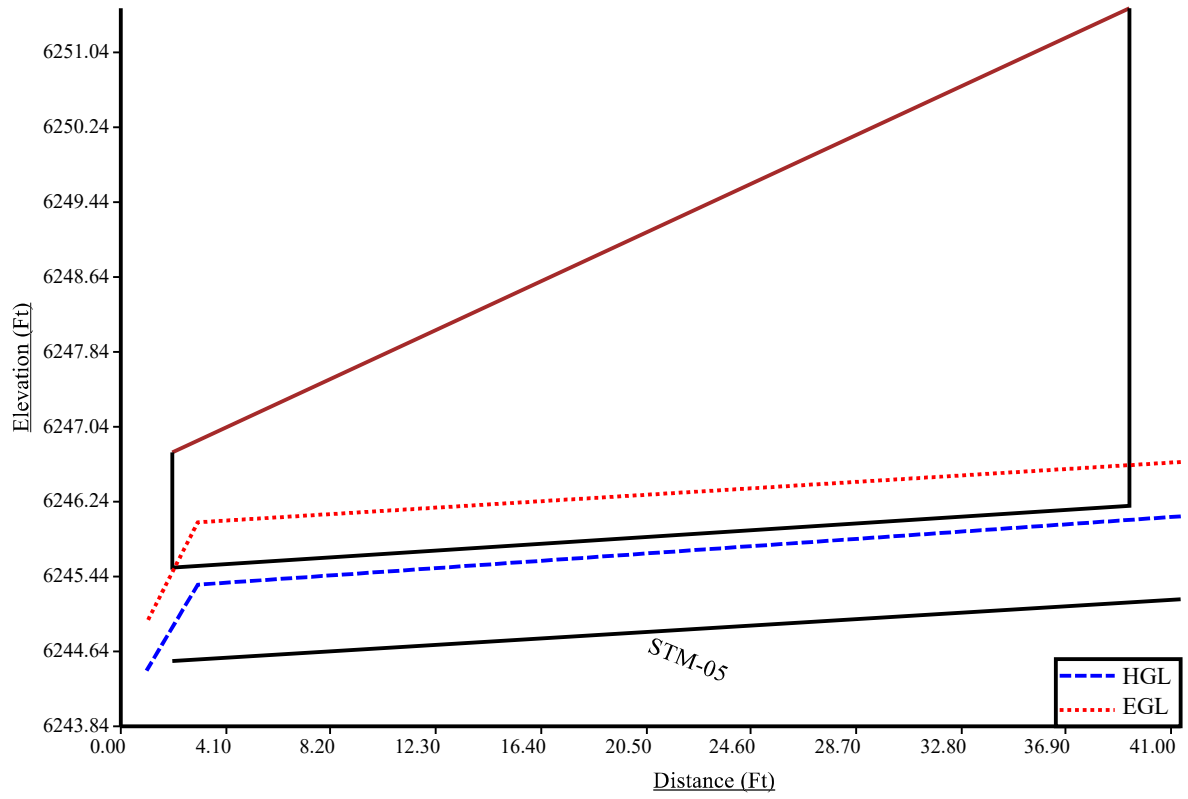
					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-04	37.45	2.50	4.00	4.92	0.00	0.53	0.00	4.92	3.09	0.84	9.47	Sewer Too Shallow

Total earth volume for sewer trenches = 9 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.



STM-05 5YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/19/2023 11:50:00 AM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 5 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6244.44

Manhole Input Summary:

Element Name	Given Flow			Sub Basin Information						
	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
DRY DREEK SCULPTED DROP	6246.77	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-05	6251.51	4.50	0.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
DRY DREEK SCULPTED DROP	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-05	0.00	0.00	0.00	0.00	0.30	0.00	0.00	0.00	4.50	

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-05	41.37	6244.54	1.6	6245.20	0.013	0.00	0.00	CIRCULAR	12.00 in	12.00 in

Sewer Flow Summary:

Full Flow Capacity	Critical Flow	Normal Flow

Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
STM-05	4.51	5.75	10.64	6.11	9.80	6.55	1.22	Supercritical	4.50	0.00	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-05	4.50	CIRCULAR	12.00 in	12.00 in	18.00 in	18.00 in	12.00 in	12.00 in	0.79	Height is too small. Width is too small. Existing height is smaller than the suggested height. Existing width is smaller than the suggested width.

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6244.44

	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
Element Name	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)

STM-05	6244.54	6245.20	0.00	0.00	6245.36	6246.09	6246.02	0.64	6246.67
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- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ^ 2/(2*g)
- Lateral loss = V_{fo} ^ 2/(2*g)- Junction Loss K * V_{fi} ^ 2/(2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

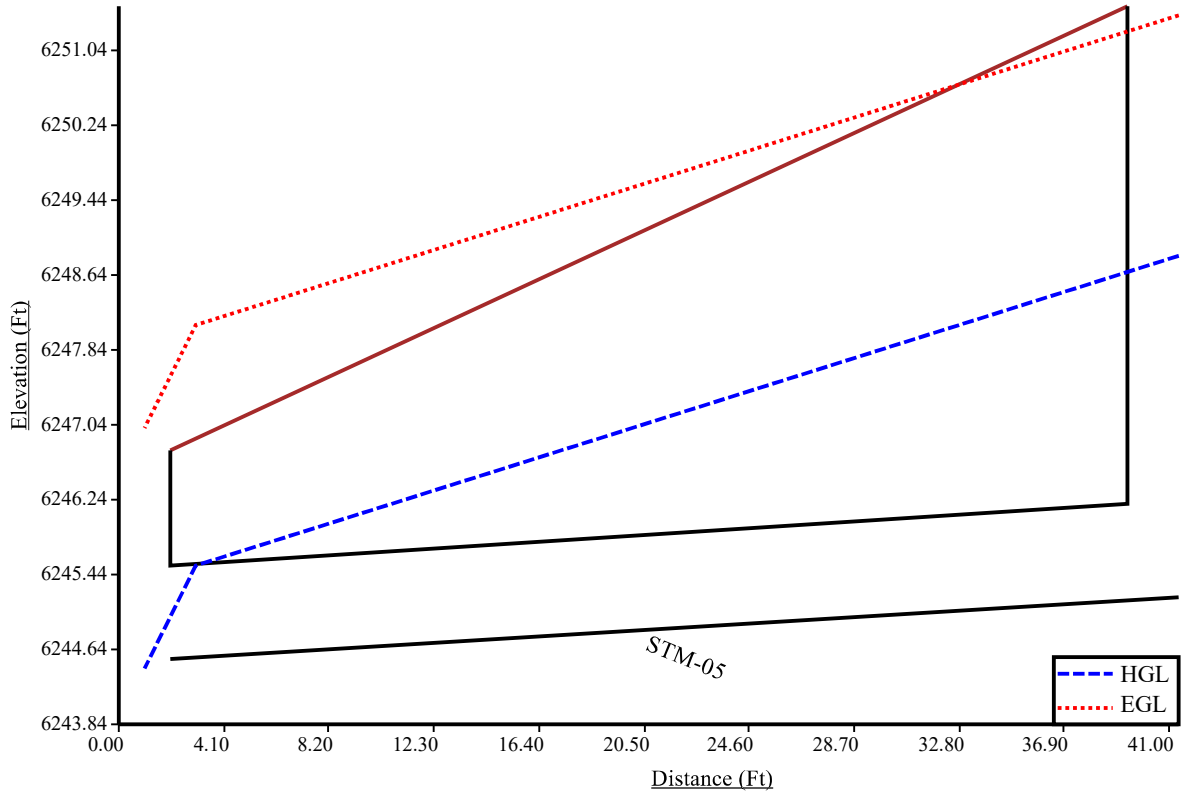
The trench side slope is 1.0 ft/ft
The minimum trench width is 2.00 ft

					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-05	41.37	2.00	4.00	4.33	4.46	2.73	1.06	12.62	6.81	5.14	44.83	Sewer Too Shallow

Total earth volume for sewer trenches = 45 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

STM-05 100YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/19/2023 11:46:20 AM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 5 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6244.44

Manhole Input Summary:

Element Name	Given Flow			Sub Basin Information						
	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
DRY DREEK SCULPTED DROP	6246.77	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-05	6251.51	10.10	0.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
DRY DREEK SCULPTED DROP	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-05	0.00	0.00	0.00	0.00	0.50	0.00	0.00	0.00	10.10	

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Manning's n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-05	41.37	6244.54	1.6	6245.20	0.013	0.00	0.00	CIRCULAR	12.00 in	12.00 in

Sewer Flow Summary:

Full Flow Capacity	Critical Flow	Normal Flow

Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
STM-05	4.51	5.75	12.00	12.86	12.00	12.86	0.00	Pressurized	10.10	41.37	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-05	10.10	CIRCULAR	12.00 in	12.00 in	18.00 in	18.00 in	12.00 in	12.00 in	0.79	Height is too small. Width is too small. Existing height is smaller than the suggested height. Existing width is smaller than the suggested width. Exceeds max. Depth/Rise

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6244.44

	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
Element Name	Downstream (ft)	Upstream (ft)	Bend Loss	Lateral Loss	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss	Upstream (ft)

			(ft)	(ft)				(ft)	
STM-05	6244.54	6245.20	0.00	0.00	6245.54	6248.85	6248.11	3.31	6251.41

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ^ 2/(2*g)
- Lateral loss = V_{fo} ^ 2/(2*g)- Junction Loss K * V_{fi} ^ 2/(2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

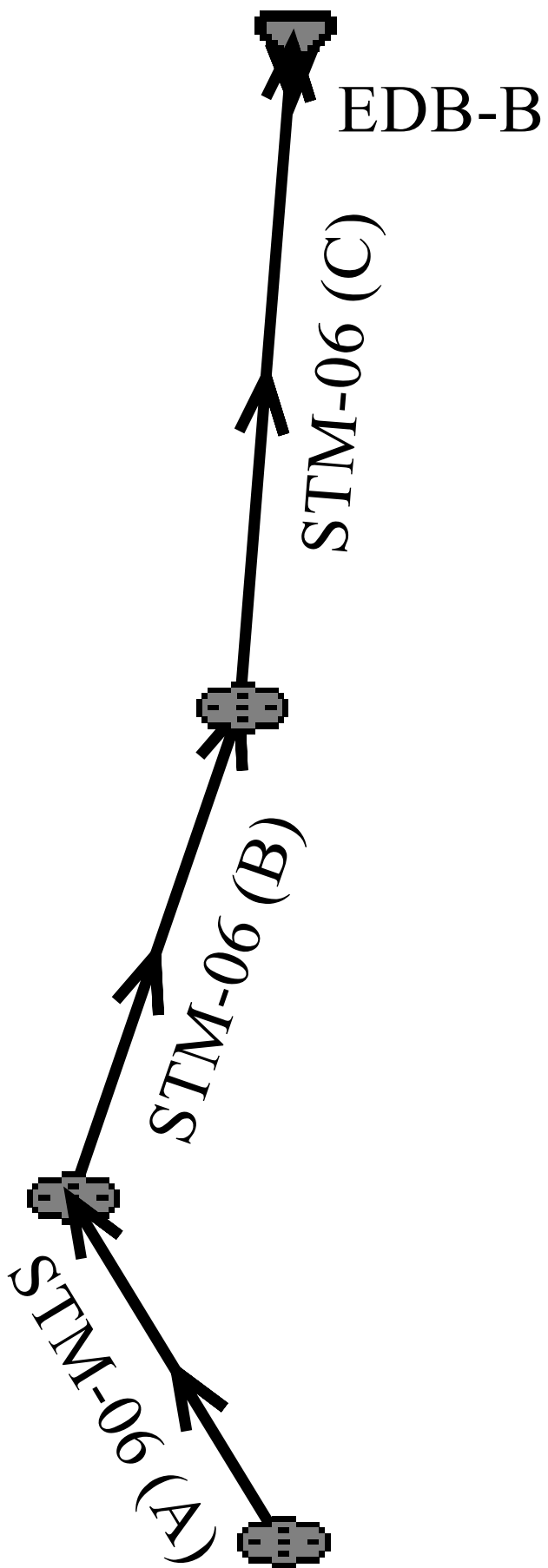
The trench side slope is 1.0 ft/ft

The minimum trench width is 2.00 ft

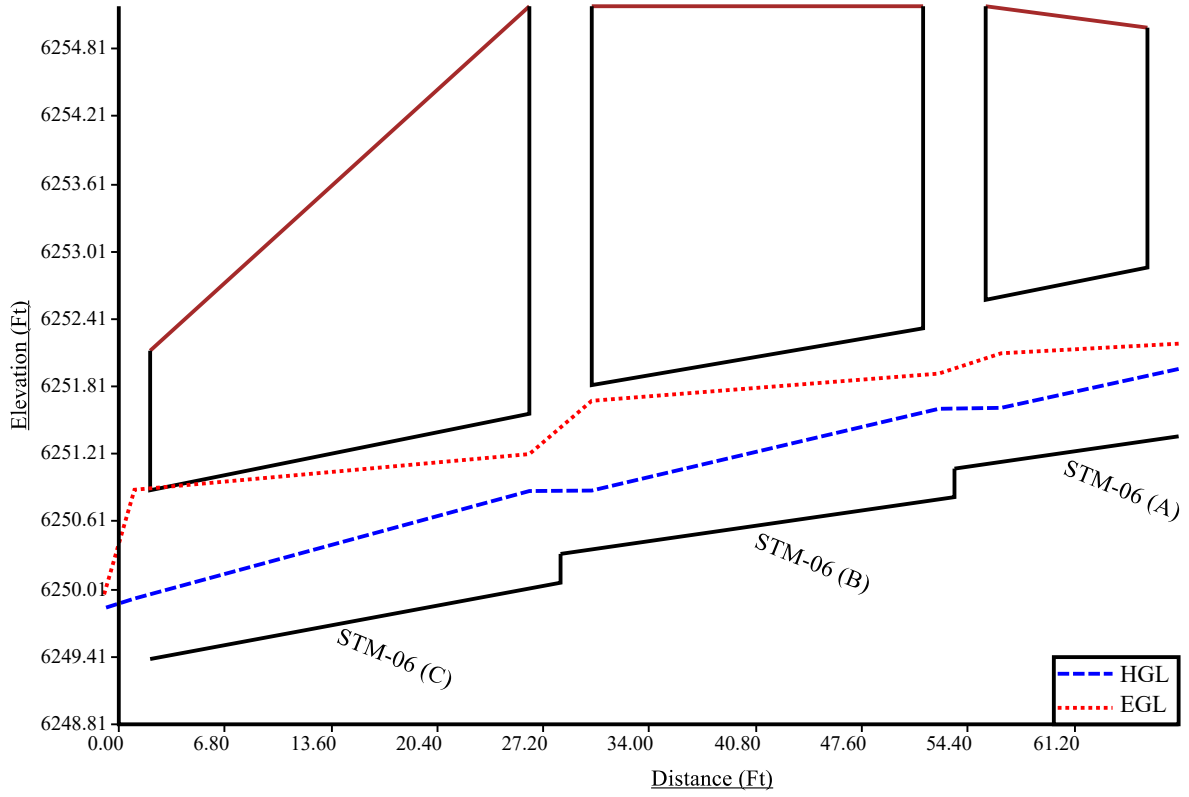
					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-05	41.37	2.00	4.00	4.33	4.46	2.73	1.06	12.62	6.81	5.14	44.83	Sewer Too Shallow

Total earth volume for sewer trenches = 45 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.



STM-06 5YR



<p>Program: UDSEWER Math Model Interface 2.1.1.4</p> <p>Run Date: 2/16/2024 11:12:27 AM</p>	<h2 style="margin: 0;">UDSewer Results Summary</h2> <p>Project Title: 20-270 Mark Dabbling Storm 6 HGL Project Description: Default system</p>
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 5
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6249.84

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
EDB-B	6252.13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

STM-06 (C)	6255.19	4.50	0.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-06 (B)	6255.19	4.20	1.70	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-06 (A)	6255.00	2.50	2.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
EDB-B	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-06 (C)	0.00	0.00	0.00	0.00	0.30	0.00	0.00	0.00	4.50	
STM-06 (B)	0.00	0.00	0.00	0.00	1.70	0.00	0.00	0.00	4.20	
STM-06 (A)	0.00	0.00	0.00	0.00	2.50	0.00	0.00	0.00	2.50	

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Manning's n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-06 (C)	28.30	6249.39	2.4	6250.07	0.013	0.00	0.00	CIRCULAR	18.00 in	18.00 in
STM-06 (B)	25.23	6250.33	2.0	6250.83	0.013	0.05	0.00	CIRCULAR	18.00 in	18.00 in
STM-06 (A)	14.37	6251.08	2.0	6251.37	0.013	0.25	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

Element Name	Full Flow Capacity		Critical Flow		Normal Flow				Flow (cfs)	Surcharged Length (ft)	Comment
	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition			
STM-06 (C)	16.32	9.23	9.77	4.59	6.46	7.89	2.21	Supercritical	4.50	0.00	
STM-06 (B)	14.90	8.43	9.42	4.49	6.54	7.24	2.01	Supercritical	4.20	0.00	
STM-06 (A)	14.90	8.43	7.18	3.80	4.99	6.26	2.02	Supercritical	2.50	0.00	

- A Froude number of 0 indicates that pressurized flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-06 (C)	4.50	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
STM-06 (B)	4.20	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
STM-06 (A)	2.50	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6249.84

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-06 (C)	6249.39	6250.07	0.00	0.00	6249.93	6250.88	6250.90	0.32	6251.21
STM-06 (B)	6250.33	6250.83	0.00	0.00	6250.89	6251.62	6251.69	0.24	6251.93
STM-06 (A)	6251.08	6251.37	0.01	0.00	6251.62	6251.97	6252.11	0.09	6252.19

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi}² / (2 * g)
- Lateral loss = V_{fo}² / (2 * g) - Junction Loss K * V_{fi}² / (2 * g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft

The minimum trench width is 2.00 ft

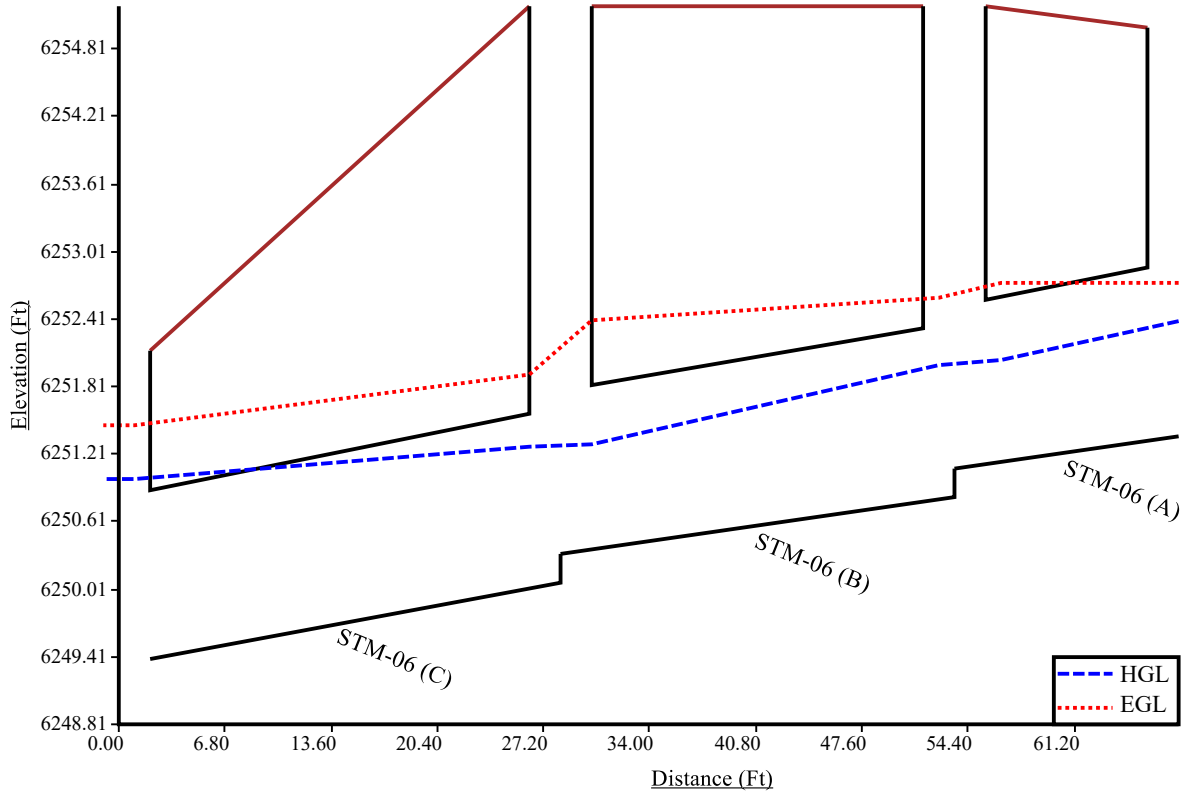
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		

STM-06 (C)	28.30	2.50	4.00	4.92	4.98	3.28	1.03	9.74	5.66	3.41	26.09	Sewer Too Shallow
STM-06 (B)	25.23	2.50	4.00	4.92	9.23	5.41	3.16	8.22	4.90	2.65	27.13	
STM-06 (A)	14.37	2.50	4.00	4.92	7.71	4.65	2.40	6.76	4.17	1.92	12.29	Sewer Too Shallow

Total earth volume for sewer trenches = 66 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

STM-06 100YR



<p>Program: UDSEWER Math Model Interface 2.1.1.4</p> <p>Run Date: 2/16/2024 11:16:06 AM</p>	<h2 style="text-align: center;">UDSewer Results Summary</h2> <p>Project Title: 20-270 Mark Dabbling Storm 6 HGL Project Description: Default system</p>
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6250.99

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
EDB-B	6252.13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

STM-06 (C)	6255.19	9.80	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-06 (B)	6255.19	9.20	3.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-06 (A)	6255.00	6.00	6.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
EDB-B	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-06 (C)	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	9.80	
STM-06 (B)	0.00	0.00	0.00	0.00	3.20	0.00	0.00	0.00	9.20	
STM-06 (A)	0.00	0.00	0.00	0.00	6.00	0.00	0.00	0.00	6.00	

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-06 (C)	28.30	6249.39	2.4	6250.07	0.013	0.00	0.00	CIRCULAR	18.00 in	18.00 in
STM-06 (B)	25.23	6250.33	2.0	6250.83	0.013	0.05	0.00	CIRCULAR	18.00 in	18.00 in
STM-06 (A)	14.37	6251.08	2.0	6251.37	0.013	0.25	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

Element Name	Full Flow Capacity		Critical Flow		Normal Flow				Flow (cfs)	Surcharged Length (ft)	Comment
	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition			
STM-06 (C)	16.32	9.23	14.49	6.43	10.06	9.65	2.06	Supercritical Jump	9.80	6.47	
STM-06 (B)	14.90	8.43	14.07	6.21	10.23	8.87	1.87	Supercritical	9.20	0.00	
STM-06 (A)	14.90	8.43	11.35	5.11	7.95	7.97	1.98	Supercritical	6.00	0.00	

- A Froude number of 0 indicates that pressurized flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-06 (C)	9.80	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
STM-06 (B)	9.20	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
STM-06 (A)	6.00	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6250.99

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-06 (C)	6249.39	6250.07	0.00	0.00	6250.99	6251.28	6251.47	0.45	6251.92
STM-06 (B)	6250.33	6250.83	0.02	0.00	6251.30	6252.00	6252.40	0.20	6252.60
STM-06 (A)	6251.08	6251.37	0.04	0.00	6252.05	6252.39	6252.73	0.00	6252.73

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi}² / (2 * g)
- Lateral loss = V_{fo}² / (2 * g) - Junction Loss K * V_{fi}² / (2 * g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft

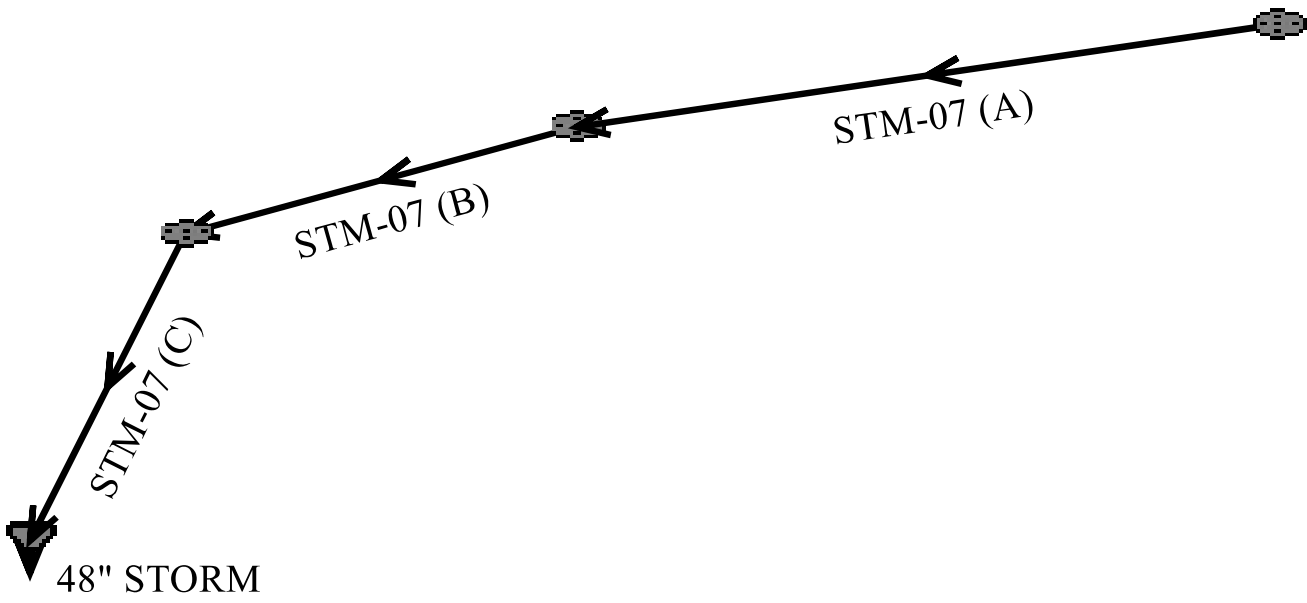
The minimum trench width is 2.00 ft

Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		

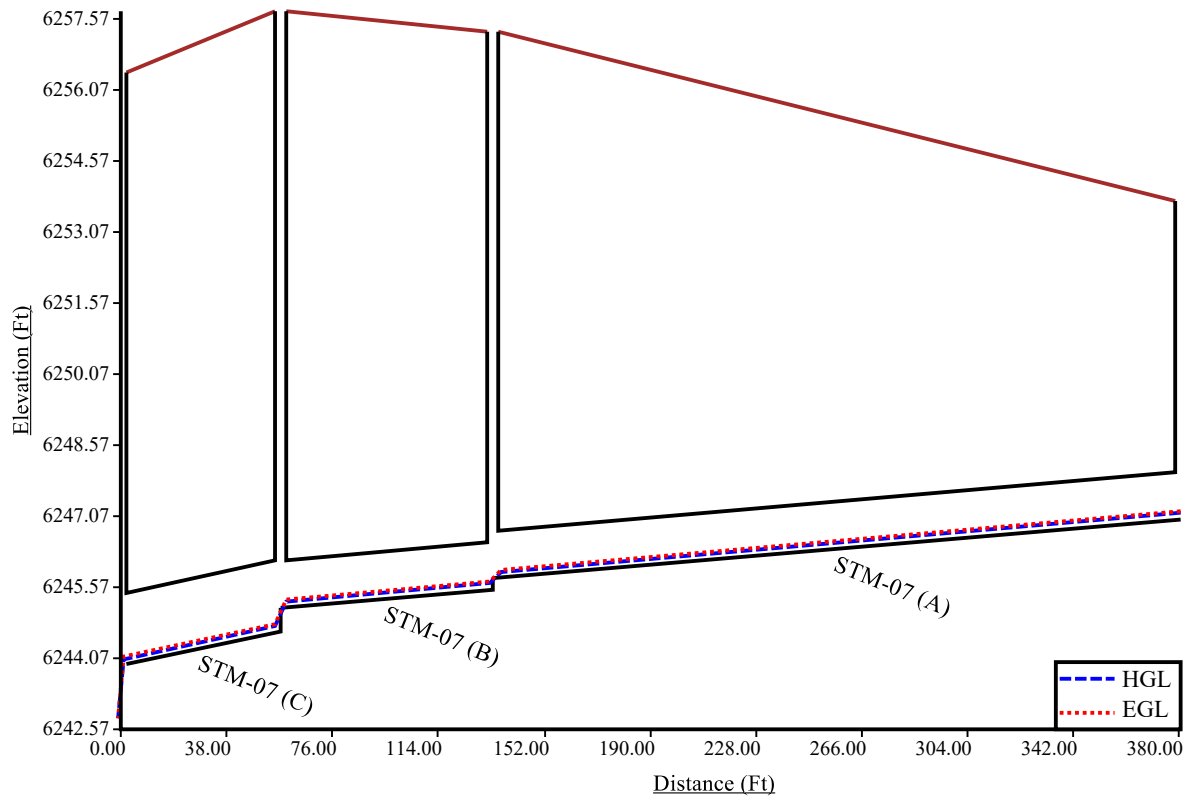
STM-06 (C)	28.30	2.50	4.00	4.92	4.98	3.28	1.03	9.74	5.66	3.41	26.09	Sewer Too Shallow
STM-06 (B)	25.23	2.50	4.00	4.92	9.23	5.41	3.16	8.22	4.90	2.65	27.13	
STM-06 (A)	14.37	2.50	4.00	4.92	7.71	4.65	2.40	6.76	4.17	1.92	12.29	Sewer Too Shallow

Total earth volume for sewer trenches = 66 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.



STM-07 5YR



<p>Program: UDSEWER Math Model Interface 2.1.1.4</p> <p>Run Date: 2/16/2024 1:07:28 PM</p>	<h2 style="margin: 0;">UDSewer Results Summary</h2> <p>Project Title: 20-270 Mark Dabbling Storm 7 HGL Project Description: Default system</p>
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 5
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6242.81

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
48" STORM	6256.43	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

STM-07 (C)	6257.72	0.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-07 (B)	6257.29	0.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-07 (A)	6253.72	0.10	0.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
48" STORM	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-07 (C)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.10	
STM-07 (B)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.10	
STM-07 (A)	0.00	0.00	0.00	0.00	0.10	0.00	0.00	0.00	0.10	

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Manning's n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-07 (C)	57.35	6243.95	1.2	6244.64	0.013	0.48	0.00	CIRCULAR	18.00 in	18.00 in
STM-07 (B)	76.11	6245.14	0.5	6245.52	0.013	0.05	0.00	CIRCULAR	12.00 in	12.00 in
STM-07 (A)	246.92	6245.77	0.5	6247.00	0.013	0.08	0.00	CIRCULAR	12.00 in	12.00 in

Sewer Flow Summary:

Element Name	Full Flow Capacity		Critical Flow		Normal Flow				Flow (cfs)	Surcharged Length (ft)	Comment
	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition			
STM-07 (C)	11.54	6.53	1.39	1.59	1.19	2.01	1.37	Supercritical	0.10	0.00	
STM-07 (B)	2.53	3.22	1.55	1.69	1.63	1.56	0.90	Subcritical	0.10	0.00	Velocity is Too Low
STM-07 (A)	2.53	3.22	1.55	1.69	1.63	1.56	0.90	Subcritical	0.10	0.00	Velocity is Too Low

- A Froude number of 0 indicates that pressurized flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-07 (C)	0.10	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
STM-07 (B)	0.10	CIRCULAR	12.00 in	12.00 in	18.00 in	18.00 in	12.00 in	12.00 in	0.79	Height is too small. Width is too small. Existing height is smaller than the suggested height. Existing width is smaller than the suggested width.
STM-07 (A)	0.10	CIRCULAR	12.00 in	12.00 in	18.00 in	18.00 in	12.00 in	12.00 in	0.79	Height is too small. Width is too small. Existing height is smaller than the suggested height. Existing width is smaller than the suggested width.

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6242.81

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-07 (C)	6243.95	6244.64	0.00	0.00	6244.05	6244.76	6244.11	0.68	6244.80
STM-07 (B)	6245.14	6245.52	0.00	0.00	6245.27	6245.66	6245.31	0.38	6245.70
STM-07 (A)	6245.77	6247.00	0.00	0.00	6245.89	6247.15	6245.94	1.24	6247.18

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ² / (2 * g)
- Lateral loss = V_{fo} ² / (2 * g) - Junction Loss K * V_{fi} ² / (2 * g).

- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft

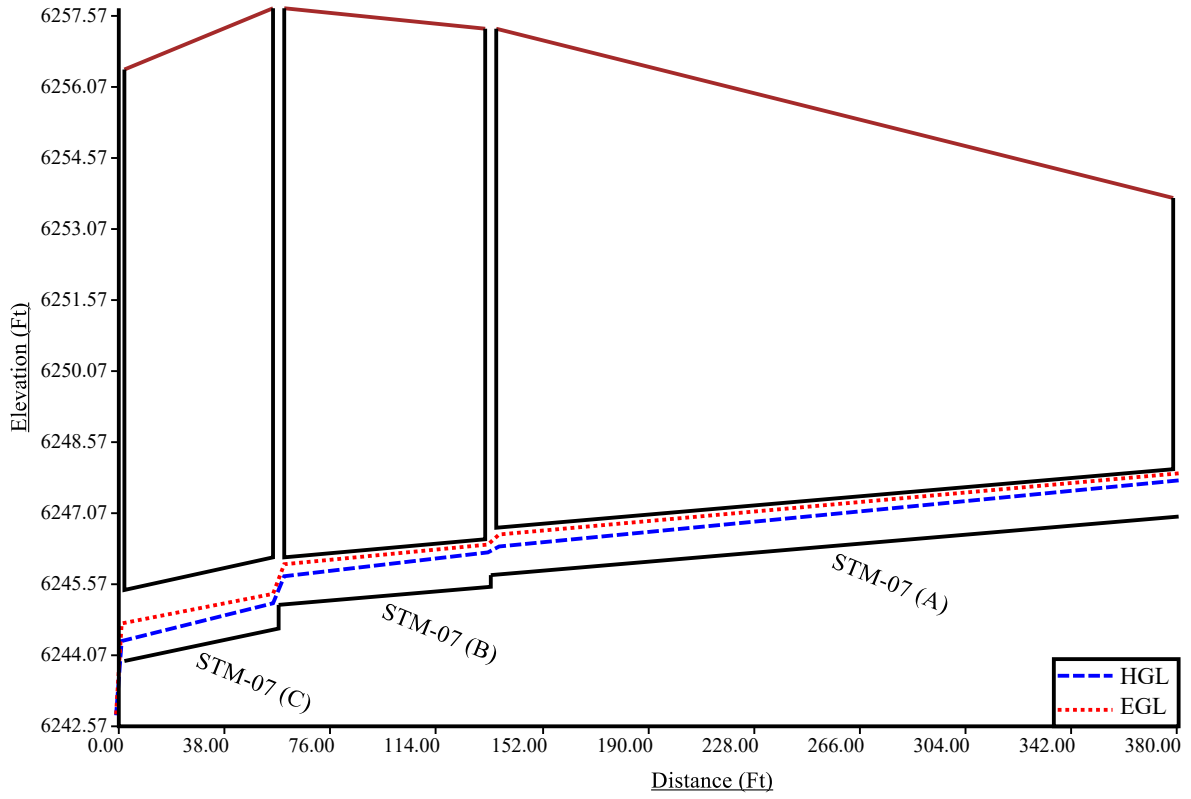
The minimum trench width is 2.00 ft

Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		
STM-07 (C)	57.35	2.50	4.00	4.92	24.46	13.02	10.77	25.66	13.62	11.37	354.73	
STM-07 (B)	76.11	2.00	4.00	4.33	25.16	13.08	11.41	23.54	12.27	10.60	437.67	
STM-07 (A)	246.92	2.00	4.00	4.33	23.05	12.02	10.36	13.44	7.22	5.55	876.55	

Total earth volume for sewer trenches = 1669 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

STM-07 100YR



<p>Program: UDSEWER Math Model Interface 2.1.1.4</p> <p>Run Date: 2/16/2024 1:09:06 PM</p>	<h2 style="text-align: center;">UDSewer Results Summary</h2> <p>Project Title: 20-270 Mark Dabbling Storm 7 HGL Project Description: Default system</p>
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6242.81

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
48" STORM	6256.43	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

STM-07 (C)	6257.72	2.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-07 (B)	6257.29	2.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-07 (A)	6253.72	2.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
48" STORM	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-07 (C)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.00	
STM-07 (B)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.00	
STM-07 (A)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.00	

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-07 (C)	57.35	6243.95	1.2	6244.64	0.013	0.48	0.00	CIRCULAR	18.00 in	18.00 in
STM-07 (B)	76.11	6245.14	0.5	6245.52	0.013	0.05	0.00	CIRCULAR	12.00 in	12.00 in
STM-07 (A)	246.92	6245.77	0.5	6247.00	0.013	0.08	0.00	CIRCULAR	12.00 in	12.00 in

Sewer Flow Summary:

Element Name	Full Flow Capacity		Critical Flow		Normal Flow				Flow (cfs)	Surcharged Length (ft)	Comment
	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition			
STM-07 (C)	11.54	6.53	6.40	3.55	5.07	4.89	1.57	Supercritical	2.00	0.00	
STM-07 (B)	2.53	3.22	7.24	4.04	8.06	3.57	0.81	Subcritical	2.00	0.00	
STM-07 (A)	2.53	3.22	7.24	4.04	8.06	3.57	0.81	Subcritical	2.00	0.00	

- A Froude number of 0 indicates that pressurized flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-07 (C)	2.00	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
STM-07 (B)	2.00	CIRCULAR	12.00 in	12.00 in	18.00 in	18.00 in	12.00 in	12.00 in	0.79	Height is too small. Width is too small. Existing height is smaller than the suggested height. Existing width is smaller than the suggested width.
STM-07 (A)	2.00	CIRCULAR	12.00 in	12.00 in	18.00 in	18.00 in	12.00 in	12.00 in	0.79	Height is too small. Width is too small. Existing height is smaller than the suggested height. Existing width is smaller than the suggested width.

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6242.81

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-07 (C)	6243.95	6244.64	0.00	0.00	6244.37	6245.17	6244.75	0.62	6245.37
STM-07 (B)	6245.14	6245.52	0.01	0.00	6245.74	6246.24	6246.00	0.42	6246.41
STM-07 (A)	6245.77	6247.00	0.01	0.00	6246.37	6247.76	6246.62	1.29	6247.91

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi}² / (2*g)
- Lateral loss = V_{fo}² / (2*g) - Junction Loss K * V_{fi}² / (2*g).

- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

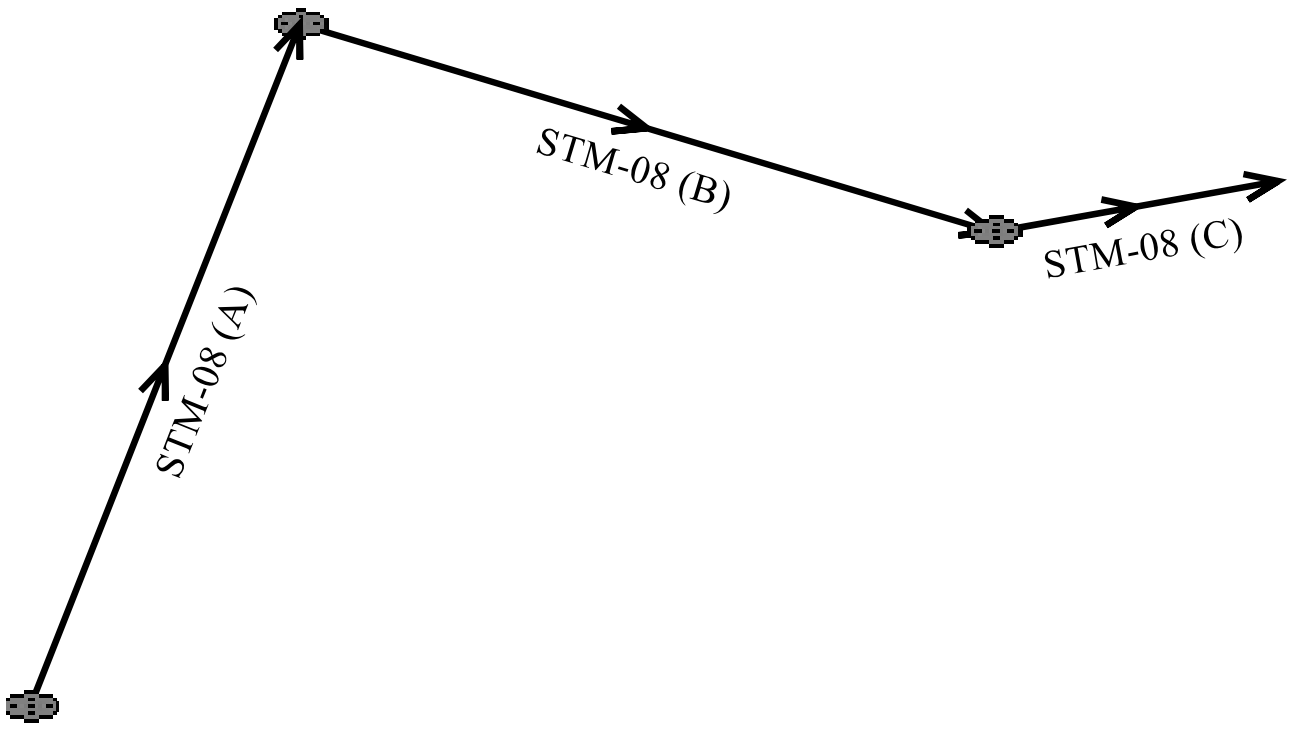
The trench side slope is 1.0 ft/ft

The minimum trench width is 2.00 ft

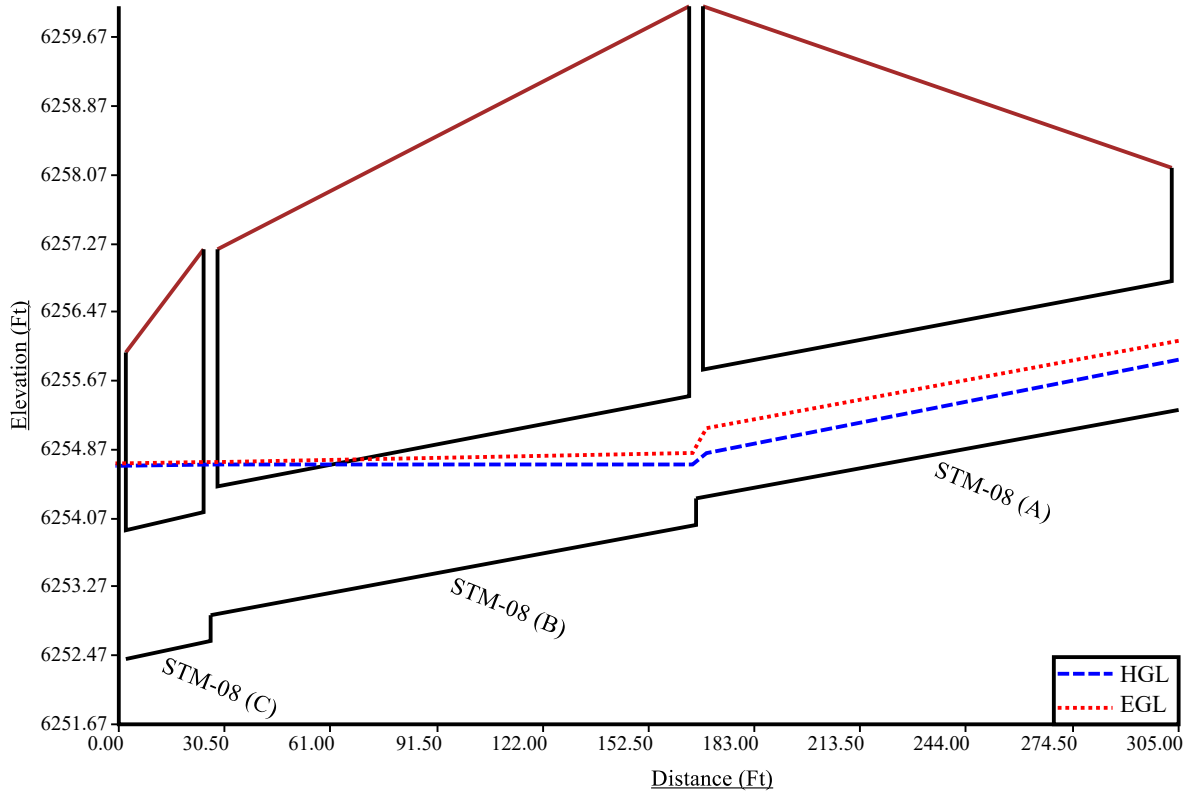
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		
STM-07 (C)	57.35	2.50	4.00	4.92	24.46	13.02	10.77	25.66	13.62	11.37	354.73	
STM-07 (B)	76.11	2.00	4.00	4.33	25.16	13.08	11.41	23.54	12.27	10.60	437.67	
STM-07 (A)	246.92	2.00	4.00	4.33	23.05	12.02	10.36	13.44	7.22	5.55	876.55	

Total earth volume for sewer trenches = 1669 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.



STM-08 5 YR



<p>Program: UDSEWER Math Model Interface 2.1.1.4</p> <p>Run Date: 2/16/2024 1:37:20 PM</p>	<h2 style="text-align: center;">UDSewer Results Summary</h2> <p>Project Title: 20-270 Mark Dabbling Storm 8 HGL Project Description: Default system</p>
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 5
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6254.68

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
EDB-C	6256.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

STM-08 (C)	6257.20	2.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-08 (B)	6260.03	2.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-08 (A)	6258.15	2.40	2.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
EDB-C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-08 (C)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.40	
STM-08 (B)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.40	
STM-08 (A)	0.00	0.00	0.00	0.00	2.40	0.00	0.00	0.00	2.40	

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-08 (C)	26.41	6252.43	0.8	6252.64	0.013	0.00	0.00	CIRCULAR	18.00 in	18.00 in
STM-08 (B)	139.75	6252.94	0.8	6253.99	0.013	0.05	0.00	CIRCULAR	18.00 in	18.00 in
STM-08 (A)	138.94	6254.30	0.7	6255.33	0.013	0.38	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

Element Name	Full Flow Capacity		Critical Flow		Normal Flow				Flow (cfs)	Surcharged Length (ft)	Comment
	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition			
STM-08 (C)	9.42	5.33	7.03	3.75	6.20	4.45	1.28	Pressurized	2.40	26.41	
STM-08 (B)	9.13	5.17	7.03	3.75	6.30	4.36	1.24	Supercritical Jump	2.40	36.51	
STM-08 (A)	9.07	5.13	7.03	3.75	6.32	4.33	1.23	Supercritical	2.40	0.00	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-08 (C)	2.40	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
STM-08 (B)	2.40	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
STM-08 (A)	2.40	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6254.68

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-08 (C)	6252.43	6252.64	0.00	0.00	6254.68	6254.69	6254.71	0.01	6254.72
STM-08 (B)	6252.94	6253.99	0.00	0.00	6254.70	6254.70	6254.72	0.11	6254.83
STM-08 (A)	6254.30	6255.33	0.01	0.00	6254.83	6255.92	6255.12	1.02	6256.13

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi}² / (2*g)
- Lateral loss = V_{fo}² / (2*g) - Junction Loss K * V_{fi}² / (2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft

The minimum trench width is 2.00 ft

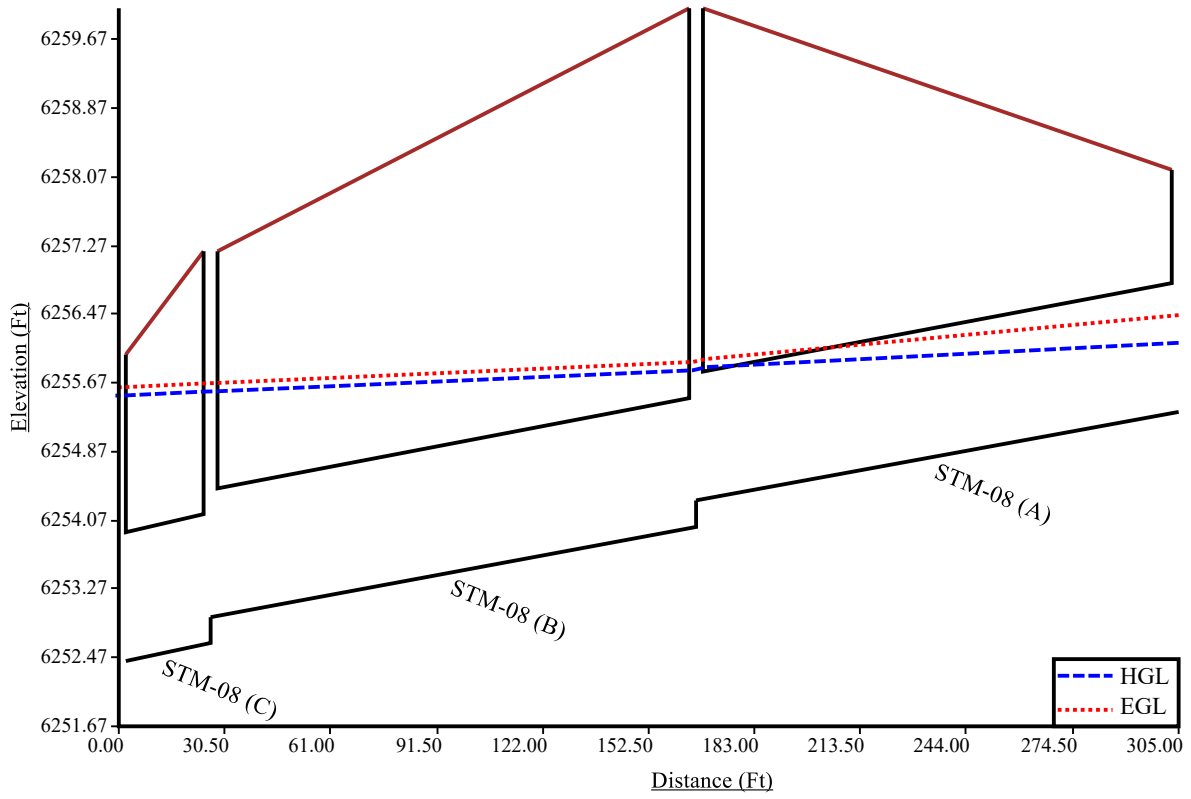
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		
STM-08 (C)	26.41	2.50	4.00	4.92	6.64	4.11	1.86	8.62	5.10	2.85	24.20	

STM-08 (B)	139.75	2.50	4.00	4.92	8.02	4.80	2.55	11.58	6.58	4.33	179.81	
STM-08 (A)	138.94	2.50	4.00	4.92	10.96	6.27	4.02	5.14	3.36	1.11	145.40	

Total earth volume for sewer trenches = 349 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

STM-08 100 YR



<p>Program: UDSEWER Math Model Interface 2.1.1.4</p> <p>Run Date: 2/16/2024 1:32:30 PM</p>	<h2 style="text-align: center;">UDSewer Results Summary</h2> <p>Project Title: 20-270 Mark Dabbling Storm 8 HGL Project Description: Default system</p>
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6255.52

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
EDB-C	6256.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

STM-08 (C)	6257.20	4.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-08 (B)	6260.03	4.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-08 (A)	6258.15	4.40	4.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
EDB-C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-08 (C)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	4.40	
STM-08 (B)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	4.40	
STM-08 (A)	0.00	0.00	0.00	0.00	4.40	0.00	0.00	0.00	4.40	

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-08 (C)	26.41	6252.43	0.8	6252.64	0.013	0.00	0.00	CIRCULAR	18.00 in	18.00 in
STM-08 (B)	139.75	6252.94	0.8	6253.99	0.013	0.05	0.00	CIRCULAR	18.00 in	18.00 in
STM-08 (A)	138.94	6254.30	0.7	6255.33	0.013	0.38	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

Element Name	Full Flow Capacity		Critical Flow		Normal Flow				Flow (cfs)	Surcharged Length (ft)	Comment
	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition			
STM-08 (C)	9.42	5.33	9.65	4.56	8.65	5.24	1.23	Pressurized	4.40	26.41	
STM-08 (B)	9.13	5.17	9.65	4.56	8.81	5.12	1.19	Pressurized	4.40	139.75	
STM-08 (A)	9.07	5.13	9.65	4.56	8.84	5.09	1.18	Supercritical Jump	4.40	9.11	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-08 (C)	4.40	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
STM-08 (B)	4.40	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	
STM-08 (A)	4.40	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6255.52

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-08 (C)	6252.43	6252.64	0.00	0.00	6255.52	6255.57	6255.62	0.05	6255.66
STM-08 (B)	6252.94	6253.99	0.00	0.00	6255.57	6255.81	6255.67	0.24	6255.91
STM-08 (A)	6254.30	6255.33	0.04	0.00	6255.85	6256.13	6255.95	0.51	6256.46

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ² / (2*g)
- Lateral loss = V_{fo} ² / (2*g) - Junction Loss K * V_{fi} ² / (2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft

The minimum trench width is 2.00 ft

Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		
STM-08 (C)	26.41	2.50	4.00	4.92	6.64	4.11	1.86	8.62	5.10	2.85	24.20	

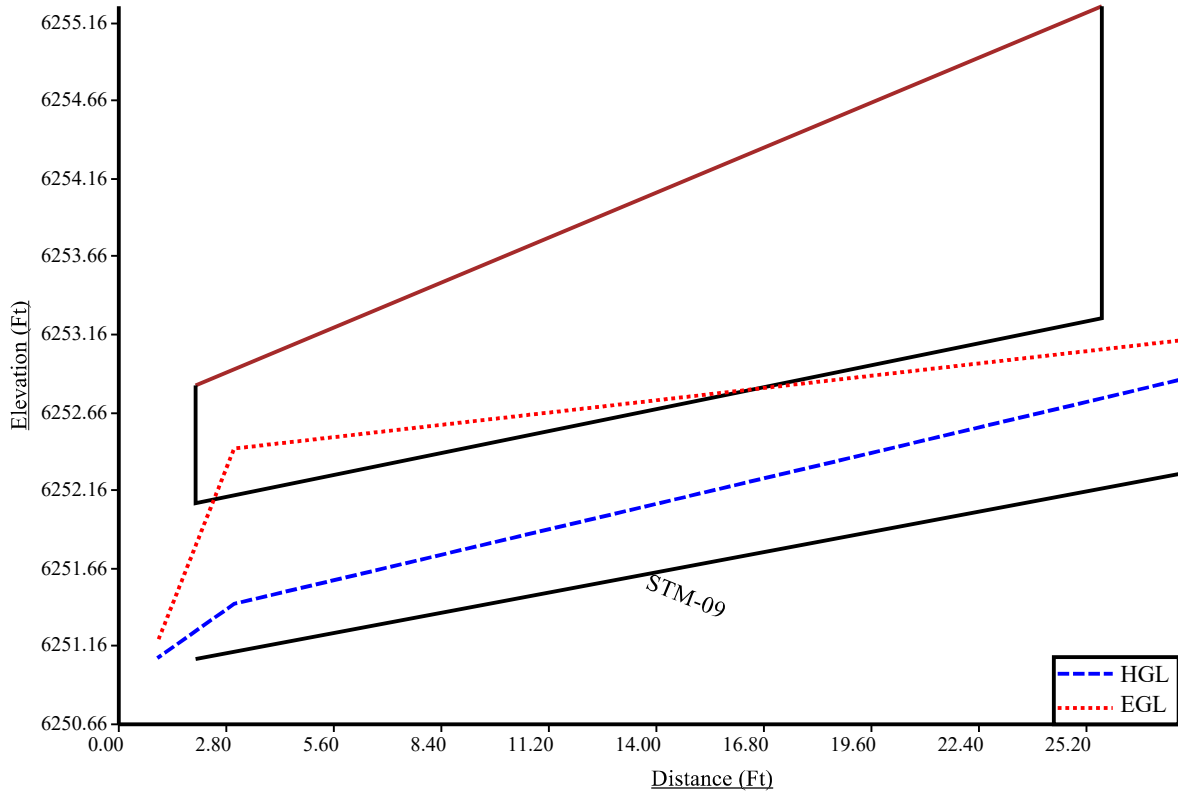
STM-08 (B)	139.75	2.50	4.00	4.92	8.02	4.80	2.55	11.58	6.58	4.33	179.81	
STM-08 (A)	138.94	2.50	4.00	4.92	10.96	6.27	4.02	5.14	3.36	1.11	145.40	

Total earth volume for sewer trenches = 349 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.



STM-09 5YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/18/2023 3:49:05 PM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 9 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 5
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6251.09

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
EDB-C	6252.84	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-09	6255.27	2.00	2.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

		Local Contribution				Total Design Flow				
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment
EDB-C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-09	0.00	0.00	0.00	0.00	2.00	0.00	0.00	0.00	2.00	

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-09	27.60	6251.08	4.3	6252.27	0.013	0.20	0.00	CIRCULAR	12.00 in	12.00 in

Sewer Flow Summary:

	Full Flow Capacity	Critical Flow	Normal Flow	

Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
STM-09	7.41	9.43	7.24	4.04	4.26	8.01	2.76	Supercritical	2.00	0.00	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-09	2.00	CIRCULAR	12.00 in	12.00 in	18.00 in	18.00 in	12.00 in	12.00 in	0.79	Height is too small. Width is too small. Existing height is smaller than the suggested height. Existing width is smaller than the suggested width.

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6251.09

	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
Element Name	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)

STM-09	6251.08	6252.27	0.00	0.00	6251.44	6252.87	6252.43	0.69	6253.13
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- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ^ 2/(2*g)
- Lateral loss = V_{fo} ^ 2/(2*g)- Junction Loss K * V_{fi} ^ 2/(2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

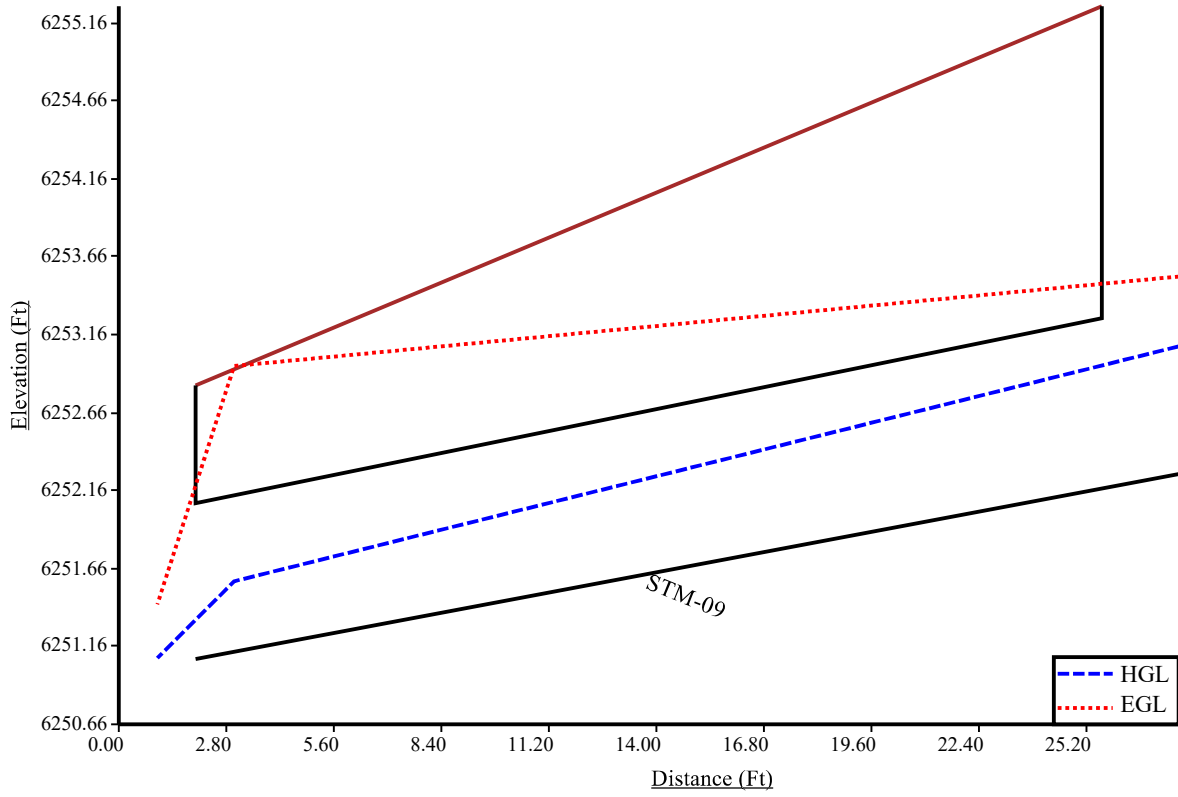
The trench side slope is 1.0 ft/ft
The minimum trench width is 2.00 ft

					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-09	27.60	2.00	4.00	4.33	0.00	2.26	0.59	6.00	3.50	1.83	11.80	Sewer Too Shallow

Total earth volume for sewer trenches = 12 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

STM-09 100YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/18/2023 3:47:36 PM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 9 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6251.09

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
EDB-C	6252.84	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-09	6255.27	3.70	3.70	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

		Local Contribution				Total Design Flow				
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment
EDB-C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-09	0.00	0.00	0.00	0.00	3.70	0.00	0.00	0.00	3.70	

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-09	27.60	6251.08	4.3	6252.27	0.013	0.20	0.00	CIRCULAR	12.00 in	12.00 in

Sewer Flow Summary:

	Full Flow Capacity	Critical Flow	Normal Flow	

Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
STM-09	7.41	9.43	9.83	5.37	6.00	9.43	2.65	Supercritical	3.70	0.00	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-09	3.70	CIRCULAR	12.00 in	12.00 in	18.00 in	18.00 in	12.00 in	12.00 in	0.79	Height is too small. Width is too small. Existing height is smaller than the suggested height. Existing width is smaller than the suggested width.

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6251.09

	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
Element Name	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)

STM-09	6251.08	6252.27	0.00	0.00	6251.58	6253.09	6252.96	0.57	6253.54
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- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ^ 2/(2*g)
- Lateral loss = V_{fo} ^ 2/(2*g)- Junction Loss K * V_{fi} ^ 2/(2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

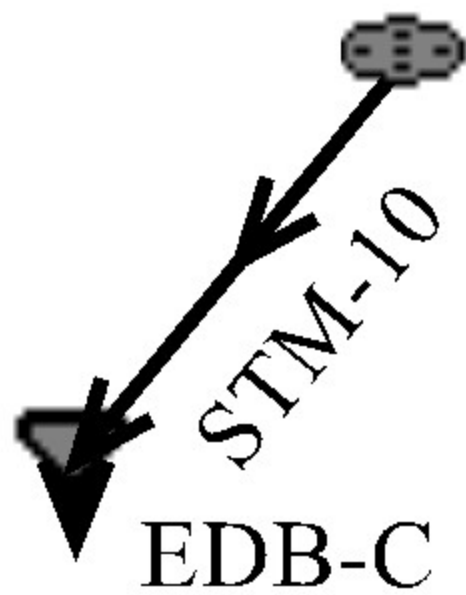
Excavation Estimate:

The trench side slope is 1.0 ft/ft
The minimum trench width is 2.00 ft

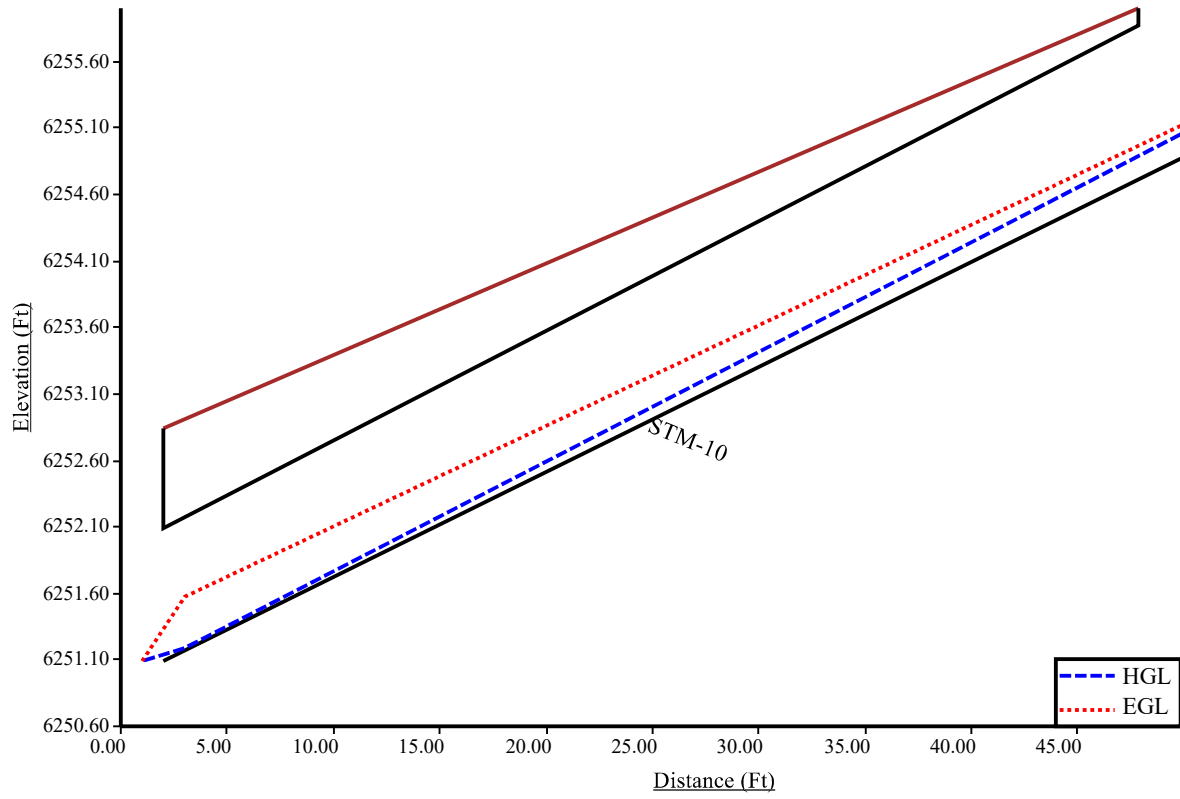
					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-09	27.60	2.00	4.00	4.33	0.00	2.26	0.59	6.00	3.50	1.83	11.80	Sewer Too Shallow

Total earth volume for sewer trenches = 12 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.



STM-10 5YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/19/2023 8:20:30 AM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 10 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 5
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6251.09

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
EDB-C	6252.84	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-10	6256.00	0.20	0.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

		Local Contribution				Total Design Flow				
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment
EDB-C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-10	0.00	0.00	0.00	0.00	0.20	0.00	0.00	0.00	0.20	

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-10	49.83	6251.09	7.6	6254.87	0.013	0.00	0.00	CIRCULAR	12.00 in	12.00 in

Sewer Flow Summary:

	Full Flow Capacity	Critical Flow	Normal Flow	

Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
STM-10	9.84	12.53	2.20	2.03	1.18	4.99	3.39	Supercritical	0.20	0.00	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-10	0.20	CIRCULAR	12.00 in	12.00 in	18.00 in	18.00 in	12.00 in	12.00 in	0.79	Height is too small. Width is too small. Existing height is smaller than the suggested height. Existing width is smaller than the suggested width.

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6251.09

	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
Element Name	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)

STM-10	6251.09	6254.87	0.00	0.00	6251.19	6255.05	6251.57	3.54	6255.12
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- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ^ 2/(2*g)
- Lateral loss = V_{fo} ^ 2/(2*g)- Junction Loss K * V_{fi} ^ 2/(2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

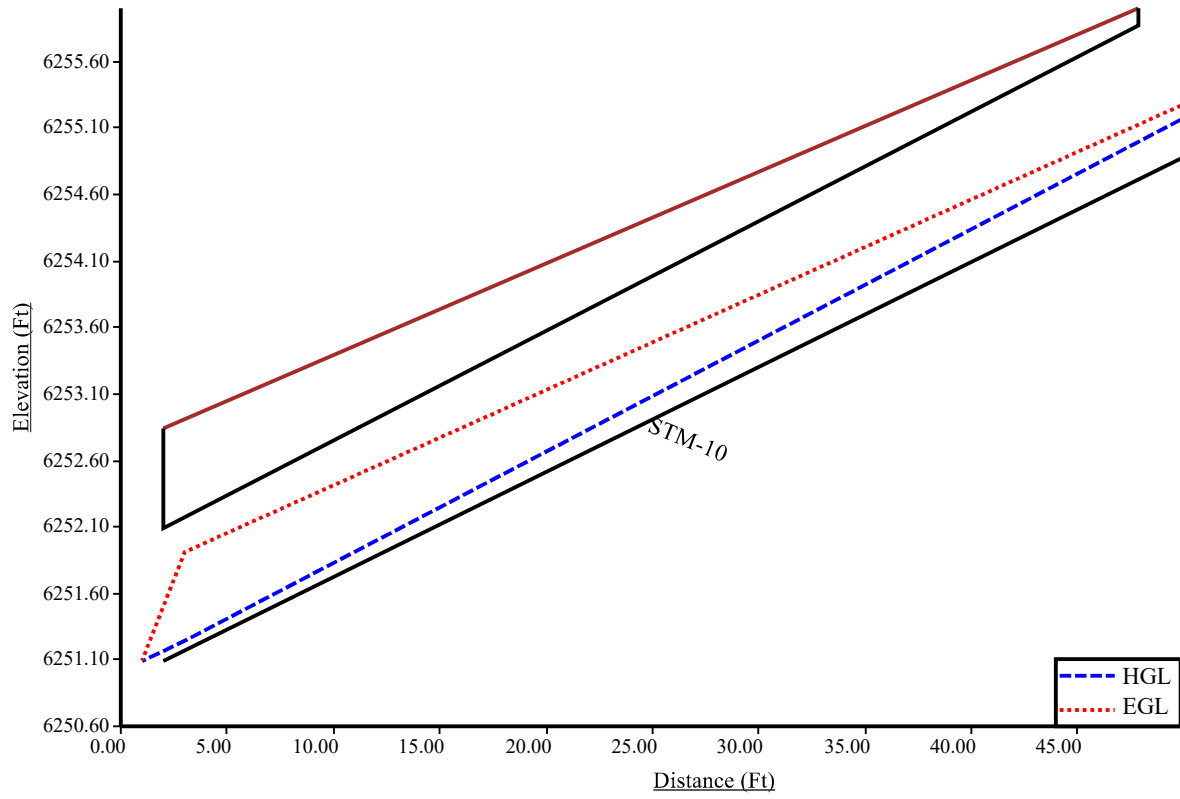
The trench side slope is 1.0 ft/ft
The minimum trench width is 2.00 ft

					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-10	49.83	2.00	4.00	4.33	0.00	2.25	0.58	4.33	1.63	0.00	13.18	Sewer Too Shallow

Total earth volume for sewer trenches = 13 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

STM-10 100YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/19/2023 8:18:35 AM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 10 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6251.09

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
EDB-C	6252.84	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-10	6256.00	0.50	0.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

		Local Contribution				Total Design Flow				
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment
EDB-C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-10	0.00	0.00	0.00	0.00	0.50	0.00	0.00	0.00	0.50	

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-10	49.83	6251.09	7.6	6254.87	0.013	0.00	0.00	CIRCULAR	12.00 in	12.00 in

Sewer Flow Summary:

	Full Flow Capacity	Critical Flow	Normal Flow	

Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
STM-10	9.84	12.53	3.52	2.61	1.84	6.56	3.55	Supercritical	0.50	0.00	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

			Existing		Calculated		Used			
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-10	0.50	CIRCULAR	12.00 in	12.00 in	18.00 in	18.00 in	12.00 in	12.00 in	0.79	Height is too small. Width is too small. Existing height is smaller than the suggested height. Existing width is smaller than the suggested width.

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6251.09

	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
Element Name	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)

STM-10	6251.09	6254.87	0.00	0.00	6251.24	6255.16	6251.91	3.36	6255.27
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- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ^ 2/(2*g)
- Lateral loss = V_{fo} ^ 2/(2*g)- Junction Loss K * V_{fi} ^ 2/(2*g).
- Friction loss is always Upstream EGL - Downstream EGL.

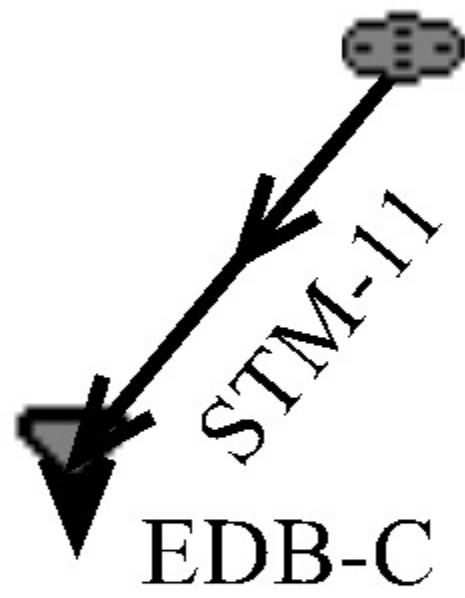
Excavation Estimate:

The trench side slope is 1.0 ft/ft
The minimum trench width is 2.00 ft

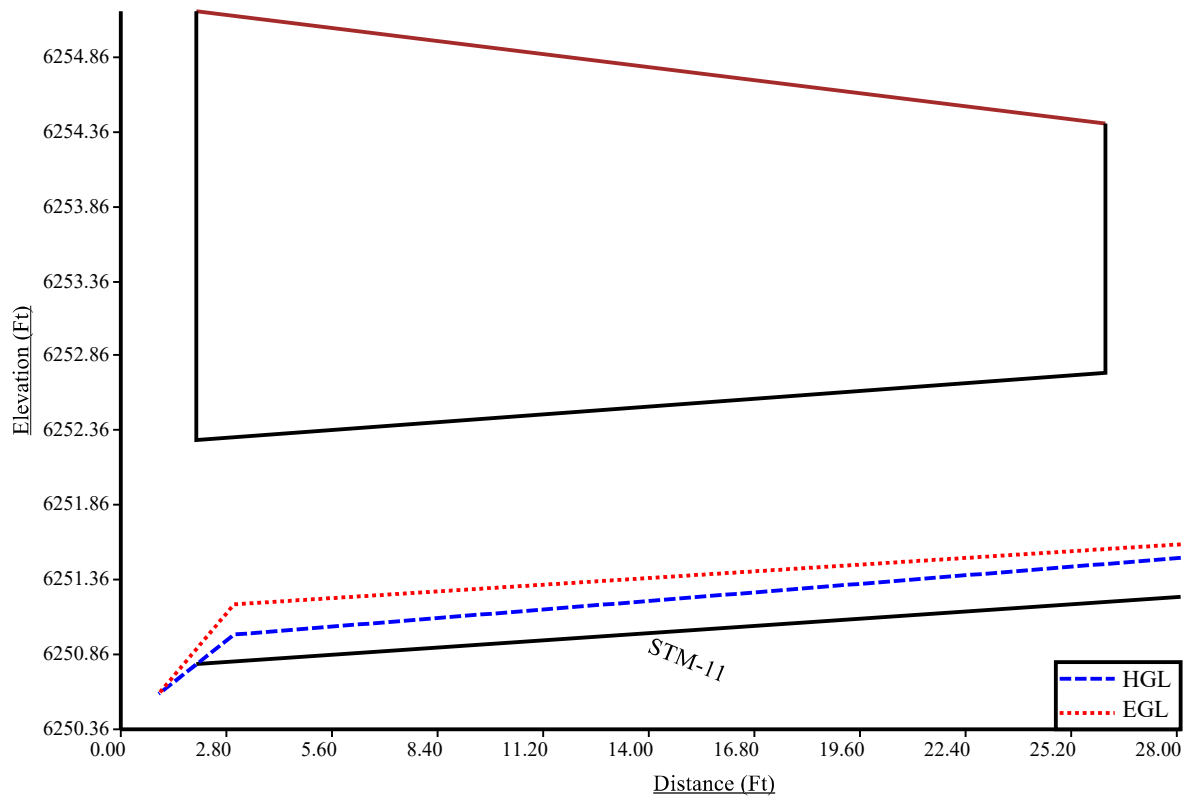
					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-10	49.83	2.00	4.00	4.33	0.00	2.25	0.58	4.33	1.63	0.00	13.18	Sewer Too Shallow

Total earth volume for sewer trenches = 13 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.



STM-11 5YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/18/2023 4:14:21 PM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 11 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 5
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6250.60

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
EDB-C	6255.17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-11	6254.42	0.50	0.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

		Local Contribution				Total Design Flow				
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment
EDB-C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-11	0.00	0.00	0.00	0.00	0.50	0.00	0.00	0.00	0.50	

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Manning's n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-11	28.10	6250.80	1.6	6251.25	0.013	0.00	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

	Full Flow Capacity	Critical Flow	Normal Flow	

Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
STM-11	13.33	7.54	3.14	2.42	2.38	3.61	1.72	Supercritical	0.50	0.00	

- A Froude number of 0 indicates that pressured flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

		Existing		Calculated		Used				
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-11	0.50	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6250.60

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-11	6250.80	6251.25	0.00	0.00	6251.00	6251.51	6251.20	0.40	6251.60

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi}² / (2 * g)

- Lateral loss = $V_{fo}^2 / (2 * g)$ - Junction Loss $K * V_{fi}^2 / (2 * g)$.
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft

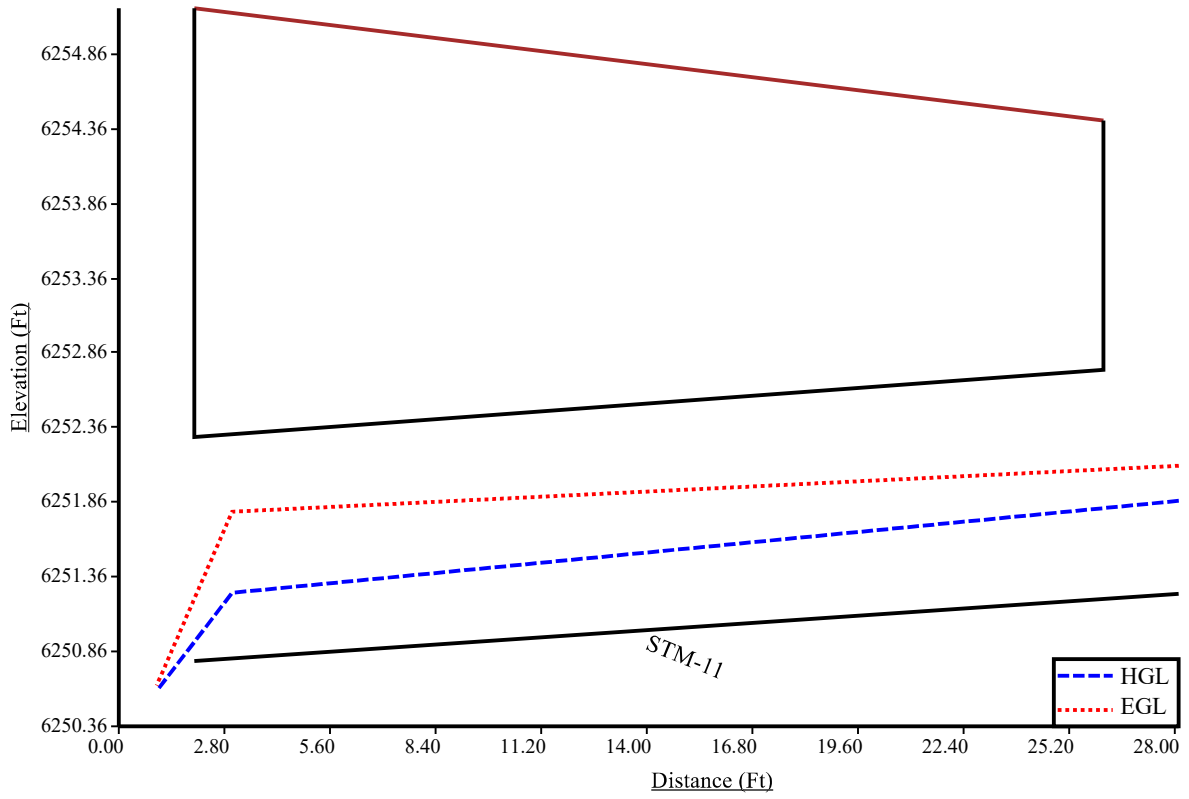
The minimum trench width is 2.00 ft

					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-11	28.10	2.50	4.00	4.92	8.24	4.91	2.66	5.84	3.71	1.46	23.61	Sewer Too Shallow

Total earth volume for sewer trenches = 24 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: $(\text{equivalent diameter in inches} / 12) + 1$ inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

STM-11 100YR



Program: UDSEWER Math Model Interface 2.1.1.4 Run Date: 7/18/2023 4:08:54 PM	UDSewer Results Summary Project Title: 20-270 Mark Dabbling Storm 11 HGL Project Description: Default system
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6250.60

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
EDB-C	6255.17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
STM-11	6254.42	2.70	2.70	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

		Local Contribution				Total Design Flow				
Element Name	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	Comment
EDB-C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
STM-11	0.00	0.00	0.00	0.00	2.70	0.00	0.00	0.00	2.70	

Sewer Input Summary:

		Elevation			Loss Coefficients			Given Dimensions		
Element Name	Sewer Length (ft)	Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
STM-11	28.10	6250.80	1.6	6251.25	0.013	0.00	0.00	CIRCULAR	18.00 in	18.00 in

Sewer Flow Summary:

	Full Flow Capacity	Critical Flow	Normal Flow	

Element Name	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition	Flow (cfs)	Surcharged Length (ft)	Comment
STM-11	13.33	7.54	7.48	3.89	5.49	5.91	1.81	Supercritical	2.70	0.00	

- A Froude number of 0 indicates that pressurized flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

		Existing		Calculated		Used				
Element Name	Peak Flow (cfs)	Cross Section	Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	Comment
STM-11	2.70	CIRCULAR	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	18.00 in	1.77	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6250.60

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
STM-11	6250.80	6251.25	0.00	0.00	6251.26	6251.87	6251.80	0.31	6252.11

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi}² / (2 * g)

- Lateral loss = $V_{fo}^2 / (2 * g)$ - Junction Loss $K * V_{fi}^2 / (2 * g)$.
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

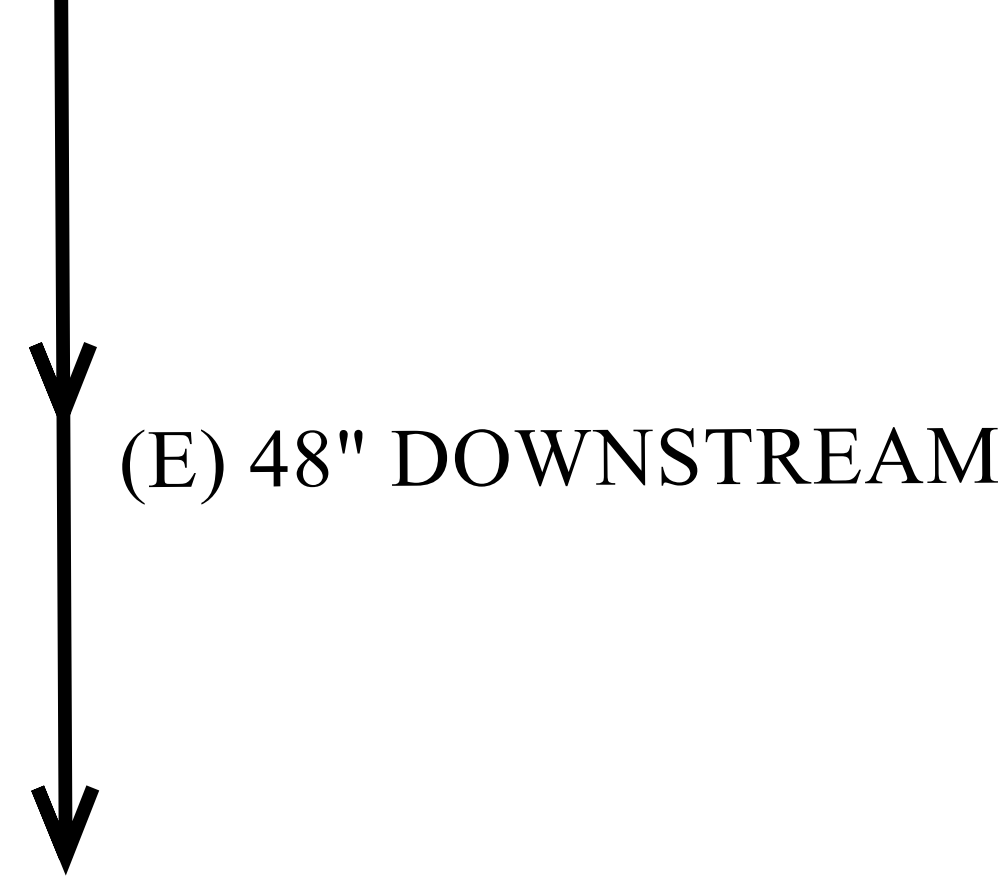
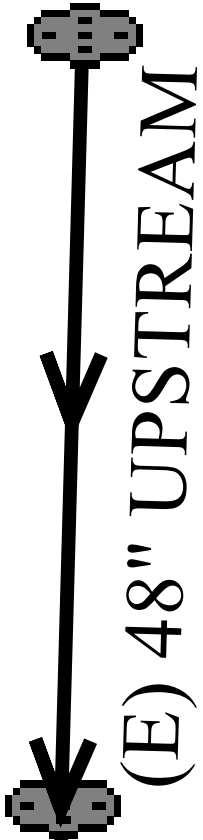
The trench side slope is 1.0 ft/ft

The minimum trench width is 2.00 ft

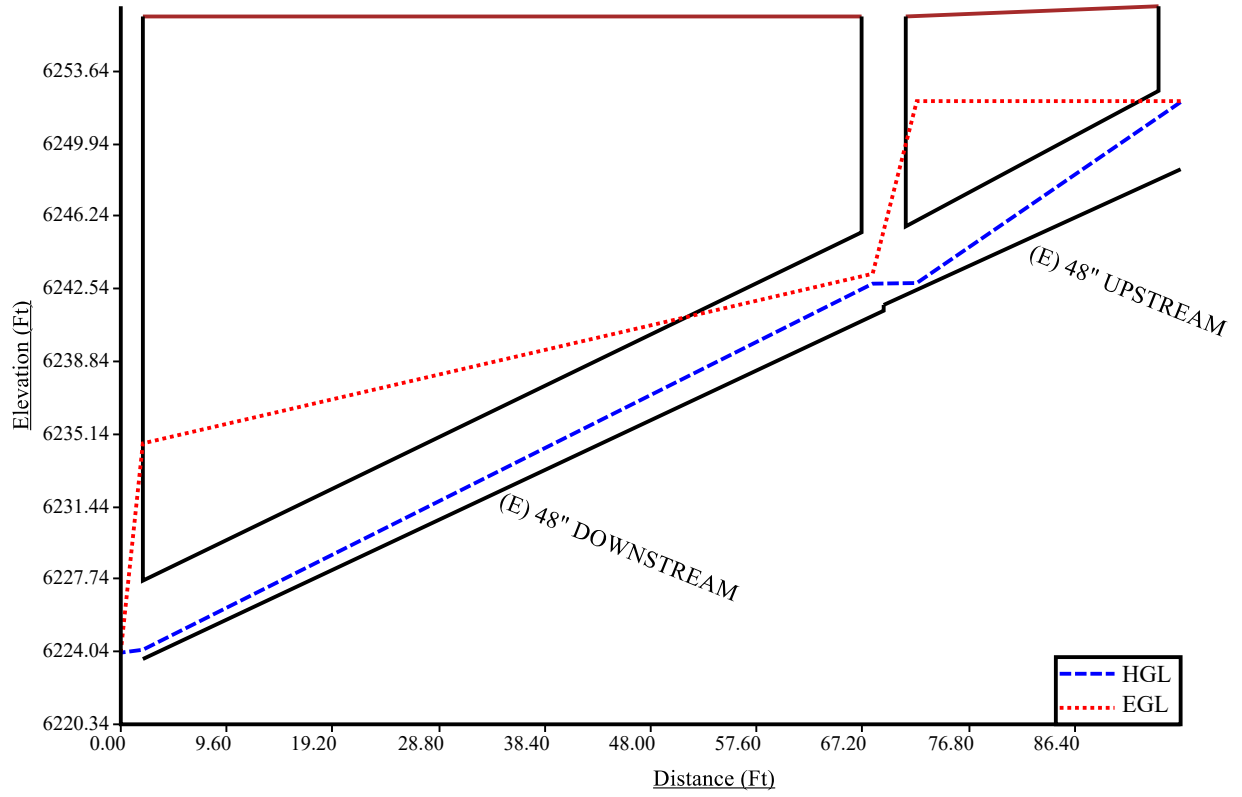
					Downstream			Upstream				
Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)	Volume (cu. yd)	Comment
STM-11	28.10	2.50	4.00	4.92	8.24	4.91	2.66	5.84	3.71	1.46	23.61	Sewer Too Shallow

Total earth volume for sewer trenches = 24 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: $(\text{equivalent diameter in inches} / 12) + 1$ inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.



(E) 48" STORM



<p>Program: UDSEWER Math Model Interface 2.1.1.4</p> <p>Run Date: 2/16/2024 12:58:58 PM</p>	<h2 style="margin: 0;">UDSewer Results Summary</h2> <p>Project Title: 20-270 Mark Dabbling EX 48" HGL</p> <p>Project Description: Default system</p>
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System Input Summary

Rainfall Parameters

Rainfall Return Period: 100
Rainfall Calculation Method: Formula

One Hour Depth (in):
Rainfall Constant "A": 28.5
Rainfall Constant "B": 10
Rainfall Constant "C": 0.786

Rational Method Constraints

Minimum Urban Runoff Coeff.: 0.20
Maximum Rural Overland Len. (ft): 500
Maximum Urban Overland Len. (ft): 300
Used UDFCD Tc. Maximum: Yes

Sizer Constraints

Minimum Sewer Size (in): 18.00
Maximum Depth to Rise Ratio: 0.90
Maximum Flow Velocity (fps): 18.0
Minimum Flow Velocity (fps): 2.0

Backwater Calculations:

Tailwater Elevation (ft): 6224.00

Manhole Input Summary:

		Given Flow		Sub Basin Information						
Element Name	Ground Elevation (ft)	Total Known Flow (cfs)	Local Contribution (cfs)	Drainage Area (Ac.)	Runoff Coefficient	5yr Coefficient	Overland Length (ft)	Overland Slope (%)	Gutter Length (ft)	Gutter Velocity (fps)
48" OUTFALL	6256.43	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
(E) 48" DOWNSTREAM	6256.43	22.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
(E) 48" UPSTREAM	6256.95	20.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Manhole Output Summary:

Element Name	Local Contribution					Total Design Flow				Comment
	Overland Time (min)	Gutter Time (min)	Basin Tc (min)	Intensity (in/hr)	Local Contrib (cfs)	Coeff. Area	Intensity (in/hr)	Manhole Tc (min)	Peak Flow (cfs)	
48" OUTFALL	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
(E) 48" DOWNSTREAM	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	22.00	
(E) 48" UPSTREAM	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	20.00	

Sewer Input Summary:

Element Name	Sewer Length (ft)	Elevation			Loss Coefficients			Given Dimensions		
		Downstream Invert (ft)	Slope (%)	Upstream Invert (ft)	Mannings n	Bend Loss	Lateral Loss	Cross Section	Rise (ft or in)	Span (ft or in)
(E) 48" DOWNSTREAM	69.10	6223.67	25.7	6241.43	0.013	0.00	0.00	CIRCULAR	48.00 in	48.00 in
(E) 48" UPSTREAM	26.90	6241.73	25.7	6248.64	0.013	0.05	0.46	CIRCULAR	48.00 in	48.00 in

Sewer Flow Summary:

Element Name	Full Flow Capacity		Critical Flow		Normal Flow				Flow (cfs)	Surcharged Length (ft)	Comment
	Flow (cfs)	Velocity (fps)	Depth (in)	Velocity (fps)	Depth (in)	Velocity (fps)	Froude Number	Flow Condition			
(E) 48" DOWNSTREAM	730.16	58.10	16.59	5.71	5.72	26.03	8.03	Supercritical	22.00	0.00	Velocity is Too High
(E) 48" UPSTREAM	730.16	58.10	15.79	5.55	5.46	25.29	7.99	Supercritical	20.00	0.00	Velocity is Too High

- A Froude number of 0 indicates that pressurized flow occurs (adverse slope or undersized pipe).
- If the sewer is not pressurized, full flow represents the maximum gravity flow in the sewer.
- If the sewer is pressurized, full flow represents the pressurized flow conditions.

Sewer Sizing Summary:

Element Name	Peak Flow (cfs)	Cross Section	Existing		Calculated		Used			Comment
			Rise	Span	Rise	Span	Rise	Span	Area (ft ²)	
(E) 48" DOWNSTREAM	22.00	CIRCULAR	48.00 in	48.00 in	18.00 in	18.00 in	48.00 in	48.00 in	12.57	
(E) 48" UPSTREAM	20.00	CIRCULAR	48.00 in	48.00 in	18.00 in	18.00 in	48.00 in	48.00 in	12.57	

- Calculated diameter was determined by sewer hydraulic capacity rounded up to the nearest commercially available size.
- Sewer sizes should not decrease downstream.
- All hydraulics were calculated using the 'Used' parameters.

Grade Line Summary:

Tailwater Elevation (ft): 6224.00

Element Name	Invert Elev.		Downstream Manhole Losses		HGL		EGL		
	Downstream (ft)	Upstream (ft)	Bend Loss (ft)	Lateral Loss (ft)	Downstream (ft)	Upstream (ft)	Downstream (ft)	Friction Loss (ft)	Upstream (ft)
(E) 48" DOWNSTREAM	6223.67	6241.43	0.00	0.00	6224.15	6242.81	6234.67	8.65	6243.32
(E) 48" UPSTREAM	6241.73	6248.64	0.00	0.03	6242.84	6252.07	6252.12	0.00	6252.12

- Bend and Lateral losses only apply when there is an outgoing sewer. The system outfall, sewer #0, is not considered a sewer.
- Bend loss = Bend K * V_{fi} ^ 2 / (2 * g)
- Lateral loss = V_{fo} ^ 2 / (2 * g) - Junction Loss K * V_{fi} ^ 2 / (2 * g).
- Friction loss is always Upstream EGL - Downstream EGL.

Excavation Estimate:

The trench side slope is 1.0 ft/ft
 The minimum trench width is 2.00 ft

Element Name	Length (ft)	Wall (in)	Bedding (in)	Bottom Width (ft)	Downstream			Upstream			Volume (cu. yd)	Comment
					Top Width (ft)	Trench Depth (ft)	Cover (ft)	Top Width (ft)	Trench Depth (ft)	Cover (ft)		
(E) 48" DOWNSTREAM	69.10	5.00	6.00	7.83	62.52	33.68	28.34	27.00	15.92	10.58	1571.25	
(E) 48" UPSTREAM	26.90	5.00	6.00	7.83	26.41	15.62	10.29	13.62	9.23	3.89	144.09	

Total earth volume for sewer trenches = 1715 cubic yards.

- The trench was estimated to have a bottom width equal to the outer pipe diameter plus 36 inches.
- If the calculated width of the trench bottom is less than the minimum acceptable width, the minimum acceptable width was used.
- The sewer wall thickness is equal to: (equivalent diameter in inches/12)+1 inches
- The sewer bedding thickness is equal to:
 - Four inches for pipes less than 33 inches.
 - Six inches for pipes less than 60 inches.
 - Eight inches for all larger sizes.

Design Procedure Form: Extended Detention Basin (EDB)

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 3

Designer: David Mijares
Company: Catamount Engineering
Date: February 13, 2024
Project: cottages at dry creek
Location: EDB C

<p>1. Basin Storage Volume</p> <p>A) Effective Imperviousness of Tributary Area, I_a</p> <p>B) Tributary Area's Imperviousness Ratio ($i = I_a / 100$)</p> <p>C) Contributing Watershed Area</p> <p>D) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm</p> <p>E) Design Concept (Select EURV when also designing for flood control)</p> <p>F) Design Volume (WQCV) Based on 40-hour Drain Time ($V_{DESIGN} = (1.0 * (0.91 * i^3 - 1.19 * i^2 + 0.78 * i) / 12 * Area)$)</p> <p>G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume ($V_{WQCV\ OTHER} = (d_6 * V_{DESIGN} * 0.43)$)</p> <p>H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)</p> <p>I) NRCS Hydrologic Soil Groups of Tributary Watershed i) Percentage of Watershed consisting of Type A Soils ii) Percentage of Watershed consisting of Type B Soils iii) Percentage of Watershed consisting of Type C/D Soils</p> <p>J) Excess Urban Runoff Volume (EURV) Design Volume For HSG A: $EURV_A = 1.68 * i^{1.28}$ For HSG B: $EURV_B = 1.36 * i^{1.08}$ For HSG C/D: $EURV_{C/D} = 1.20 * i^{1.08}$</p> <p>K) User Input of Excess Urban Runoff Volume (EURV) Design Volume (Only if a different EURV Design Volume is desired)</p>	<p>$I_a =$ <input type="text" value="62.2"/> %</p> <p>$i =$ <input type="text" value="0.622"/></p> <p>Area = <input type="text" value="2.590"/> ac</p> <p>$d_6 =$ <input type="text" value=""/></p> <div style="border: 1px solid black; padding: 5px; margin: 5px 0;"> <p>Choose One</p> <p><input checked="" type="radio"/> Water Quality Capture Volume (WQCV)</p> <p><input type="radio"/> Excess Urban Runoff Volume (EURV)</p> </div> <p>$V_{DESIGN} =$ <input type="text" value=""/> ac-ft</p> <p>$V_{DESIGN\ OTHER} =$ <input type="text" value=""/> ac-ft</p> <p>$V_{DESIGN\ USER} =$ <input type="text" value="0.021"/> ac-ft</p> <p>HSG $A =$ <input type="text" value=""/> % HSG $B =$ <input type="text" value=""/> % HSG $C/D =$ <input type="text" value=""/> %</p> <p>EURV$_{DESIGN} =$ <input type="text" value=""/> ac-ft</p> <p>EURV$_{DESIGN\ USER} =$ <input type="text" value=""/> ac-ft</p>
<p>2. Basin Shape: Length to Width Ratio (A basin length to width ratio of at least 2:1 will improve TSS reduction.)</p>	<p>L : W = <input type="text" value="4.3"/> : 1</p>
<p>3. Basin Side Slopes</p> <p>A) Basin Maximum Side Slopes (Horizontal distance per unit vertical, 4:1 or flatter preferred)</p>	<p>Z = <input type="text" value="4.00"/> ft / ft</p>
<p>4. Inlet</p> <p>A) Describe means of providing energy dissipation at concentrated inflow locations:</p>	<p>_____</p> <p>_____</p> <p>_____</p>
<p>5. Forebay</p> <p>A) Minimum Forebay Volume ($V_{FMN} =$ <input type="text" value="1"/> % of the WQCV)</p> <p>B) Actual Forebay Volume</p> <p>C) Forebay Depth ($D_F =$ <input type="text" value="12"/> inch maximum)</p> <p>D) Forebay Discharge</p> <p>i) Undetained 100-year Peak Discharge</p> <p>ii) Forebay Discharge Design Flow ($Q_F = 0.02 * Q_{100}$)</p> <p>E) Forebay Discharge Design</p> <div style="border: 1px solid black; padding: 5px; margin: 5px 0;"> <p>Choose One</p> <p><input type="radio"/> Berm With Pipe</p> <p><input checked="" type="radio"/> Wall with Rect. Notch</p> <p><input type="radio"/> Wall with V-Notch Weir</p> </div> <p>F) Discharge Pipe Size (minimum 8-inches)</p> <p>G) Rectangular Notch Width</p>	<p>$V_{FMN} =$ <input type="text" value="0.000"/> ac-ft</p> <p>$V_F =$ <input type="text" value="0.002"/> ac-ft</p> <p>$D_F =$ <input type="text" value="12.0"/> in</p> <p>$Q_{100} =$ <input type="text" value="11.00"/> cfs</p> <p>$Q_F =$ <input type="text" value="0.22"/> cfs</p> <p>Flow too small for berm w/ pipe</p> <p>Calculated $D_P =$ <input type="text" value=""/> in</p> <p>Calculated $W_N =$ <input type="text" value="3.2"/> in</p>

Design Procedure Form: Extended Detention Basin (EDB)

Designer: David Mijares
Company: Catamount Engineering
Date: February 13, 2024
Project: cottages at dry creek
Location: EDB C

<p>6. Trickle Channel</p> <p>A) Type of Trickle Channel</p> <p>F) Slope of Trickle Channel</p>	<div style="border: 1px solid black; padding: 5px; margin-bottom: 10px;"> Choose One <input checked="" type="radio"/> Concrete <input type="radio"/> Soft Bottom </div> <p>S = <input style="width: 50px;" type="text" value="0.0050"/> ft / ft</p>
<p>7. Micropool and Outlet Structure</p> <p>A) Depth of Micropool (2.5-foot minimum)</p> <p>B) Surface Area of Micropool (10 ft² minimum)</p> <p>C) Outlet Type</p> <p>D) Smallest Dimension of Orifice Opening Based on Hydrograph Routing (Use UD-Detention)</p> <p>E) Total Outlet Area</p>	<p>D_M = <input style="width: 50px;" type="text" value="2.5"/> ft</p> <p>A_M = <input style="width: 50px;" type="text" value="16"/> sq ft</p> <div style="border: 1px solid black; padding: 5px; margin-bottom: 10px;"> Choose One <input checked="" type="radio"/> Orifice Plate <input type="radio"/> Other (Describe): </div> <hr/> <p align="center">See UD-DETENTION FOR OUTFALL</p> <hr/> <p>D_{orifice} = <input style="width: 50px;" type="text"/> inches</p> <p>A_{orifice} = <input style="width: 50px;" type="text"/> square inches</p>
<p>8. Initial Surcharge Volume</p> <p>A) Depth of Initial Surcharge Volume (Minimum recommended depth is 4 inches)</p> <p>B) Minimum Initial Surcharge Volume (Minimum volume of 0.3% of the WQCV)</p> <p>C) Initial Surcharge Provided Above Micropool</p>	<p>D_{IS} = <input style="width: 50px;" type="text" value="4"/> in</p> <p>V_{IS} = <input style="width: 50px;" type="text"/> cu ft</p> <p>V_s = <input style="width: 50px;" type="text" value="5.3"/> cu ft</p>
<p>9. Trash Rack</p> <p>A) Water Quality Screen Open Area: $A_t = A_{ot} * 38.5 * (e^{-0.095D})$</p> <p>B) Type of Screen (If specifying an alternative to the materials recommended in the USDCM, indicate "other" and enter the ratio of the total open are to the total screen are for the material specified.)</p> <p style="margin-left: 40px;">Other (Y/N): <input style="width: 50px;" type="text" value="N"/></p> <p>C) Ratio of Total Open Area to Total Area (only for type 'Other')</p> <p>D) Total Water Quality Screen Area (based on screen type)</p> <p>E) Depth of Design Volume (EURV or WQCV) (Based on design concept chosen under 1E)</p> <p>F) Height of Water Quality Screen (H_{TR})</p> <p>G) Width of Water Quality Screen Opening (W_{opening}) (Minimum of 12 inches is recommended)</p>	<p>A_t = <input style="width: 50px;" type="text"/> square inches</p> <hr/> <hr/> <hr/> <p>User Ratio = <input style="width: 50px;" type="text"/></p> <p>A_{total} = <input style="width: 50px;" type="text"/> sq. in.</p> <p>H = <input style="width: 50px;" type="text"/> feet</p> <p>H_{TR} = <input style="width: 50px;" type="text"/> inches</p> <p>W_{opening} = <input style="width: 50px;" type="text"/> inches</p>

Design Procedure Form: Extended Detention Basin (EDB)

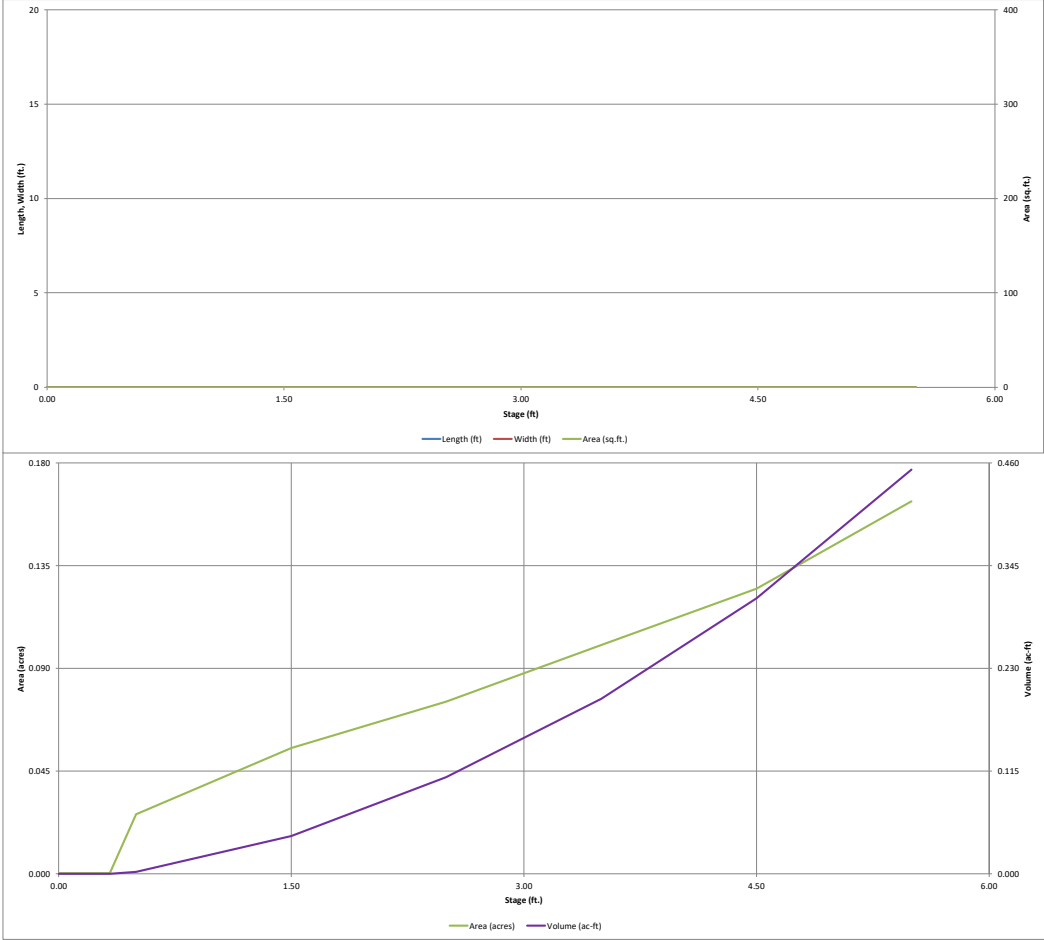
Sheet 3 of 3

Designer: David Mijares
Company: Catamount Engineering
Date: February 13, 2024
Project: cottages at dry creek
Location: EDB C

<p>10. Overflow Embankment</p> <p>A) Describe embankment protection for 100-year and greater overtopping:</p> <p>B) Slope of Overflow Embankment (Horizontal distance per unit vertical, 4:1 or flatter preferred)</p>	<p>_____</p> <p>_____</p> <p>_____</p> <p style="text-align: center;">Ze = 4.00 ft / ft</p>
<p>11. Vegetation</p>	<p>Choose One</p> <p><input type="radio"/> Irrigated</p> <p><input type="radio"/> Not Irrigated</p>
<p>12. Access</p> <p>A) Describe Sediment Removal Procedures</p>	<p>_____</p> <p>_____</p> <p>_____</p> <p>_____</p> <p>_____</p>

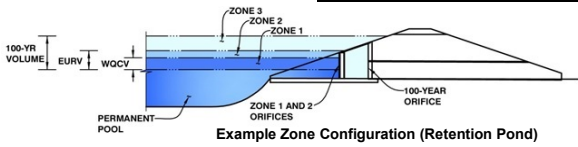
Notes: _____

DETENTION BASIN STAGE-STORAGE TABLE BUILDER



Detention Basin Outlet Structure Design

Project: COTTAGES AT DRY CREEK
Basin ID: EDB C



	Stage (ft)	Zone Volume (ac-ft)	Outlet Type
Zone 1 (User)	1.05	0.021	Orifice Plate
Zone 2 (EURV)	3.54	0.178	Orifice Plate
Zone 3 (100-year)	4.36	0.091	Weir&Pipe (Restrict)
		0.291	Total

User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP)

Underdrain Orifice Invert Depth = ft (distance below the filtration media surface)
Underdrain Orifice Diameter = inches

Calculated Parameters for Underdrain

Underdrain Orifice Area = ft²
Underdrain Orifice Centroid = feet

User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP)

Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft)
Orifice Plate: Orifice Vertical Spacing = inches
Orifice Plate: Orifice Area per Row = inches

Calculated Parameters for Plate

WQ Orifice Area per Row = ft²
Elliptical Half-Width = feet
Elliptical Slot Centroid = feet
Elliptical Slot Area = ft²

User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest)

	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	1.50	2.90					
Orifice Area (sq. inches)	0.44	0.79	0.79					

	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								

User Input: Vertical Orifice (Circular or Rectangular)

	Not Selected	Not Selected	
Invert of Vertical Orifice =	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Depth at top of Zone using Vertical Orifice =	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Vertical Orifice Diameter =	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Vertical Orifice

	Not Selected	Not Selected	
Vertical Orifice Area =	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	ft ²
Vertical Orifice Centroid =	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>	feet

User Input: Overflow Weir (Dropbox) and Grate (Flat or Sloped)

	Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	<input type="text" value="3.54"/>	<input type="text" value="N/A"/>	ft (relative to basin bottom at Stage = 0 ft)
Overflow Weir Front Edge Length =	<input type="text" value="4.00"/>	<input type="text" value="N/A"/>	feet
Overflow Weir Slope =	<input type="text" value="0.00"/>	<input type="text" value="N/A"/>	H:V (enter zero for flat grate)
Horiz. Length of Weir Sides =	<input type="text" value="4.00"/>	<input type="text" value="N/A"/>	feet
Overflow Grate Open Area % =	<input type="text" value="70%"/>	<input type="text" value="N/A"/>	% grate open area/total area
Debris Clogging % =	<input type="text" value="50%"/>	<input type="text" value="N/A"/>	%

Calculated Parameters for Overflow Weir

	Zone 3 Weir	Not Selected	
Height of Grate Upper Edge, H ₁ =	<input type="text" value="3.54"/>	<input type="text" value="N/A"/>	feet
Over Flow Weir Slope Length =	<input type="text" value="4.00"/>	<input type="text" value="N/A"/>	feet
Grate Open Area / 100-yr Orifice Area =	<input type="text" value="58.77"/>	<input type="text" value="N/A"/>	should be ≥ 4
Overflow Grate Open Area w/o Debris =	<input type="text" value="11.20"/>	<input type="text" value="N/A"/>	ft ²
Overflow Grate Open Area w/ Debris =	<input type="text" value="5.60"/>	<input type="text" value="N/A"/>	ft ²

User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice)

	Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	<input type="text" value="0.33"/>	<input type="text" value="N/A"/>	ft (distance below basin bottom at Stage = 0 ft)
Outlet Pipe Diameter =	<input type="text" value="12.00"/>	<input type="text" value="N/A"/>	inches
Restrictor Plate Height Above Pipe Invert =	<input type="text" value="3.50"/>	<input type="text" value="N/A"/>	inches

Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate

	Zone 3 Restrictor	Not Selected	
Outlet Orifice Area =	<input type="text" value="0.19"/>	<input type="text" value="N/A"/>	ft ²
Outlet Orifice Centroid =	<input type="text" value="0.17"/>	<input type="text" value="N/A"/>	feet
Half-Central Angle of Restrictor Plate on Pipe =	<input type="text" value="1.14"/>	<input type="text" value="N/A"/>	radians

User Input: Emergency Spillway (Rectangular or Trapezoidal)

Spillway Invert Stage = ft (relative to basin bottom at Stage = 0 ft)
Spillway Crest Length = feet
Spillway End Slopes = H:V
Freeboard above Max Water Surface = feet

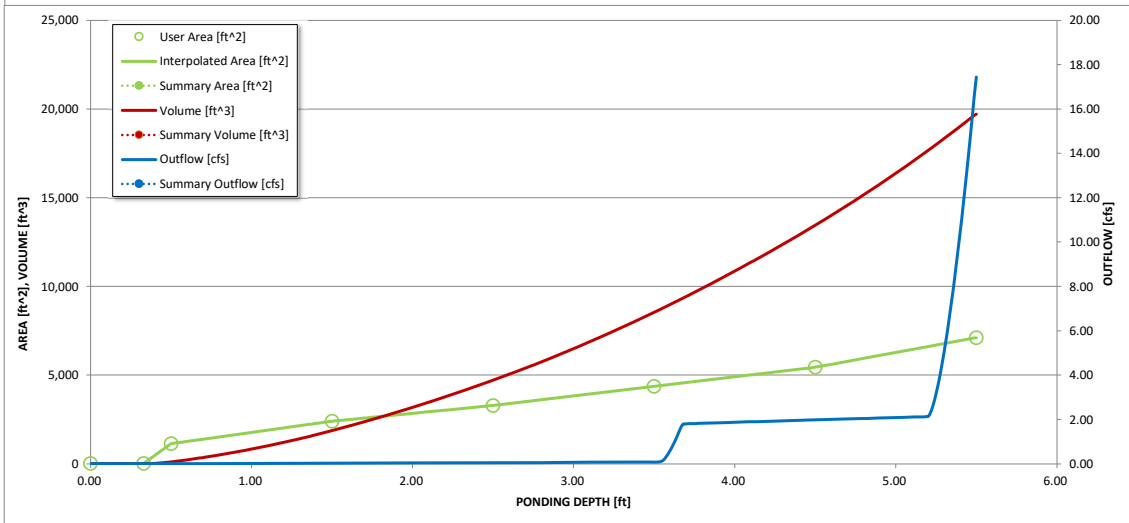
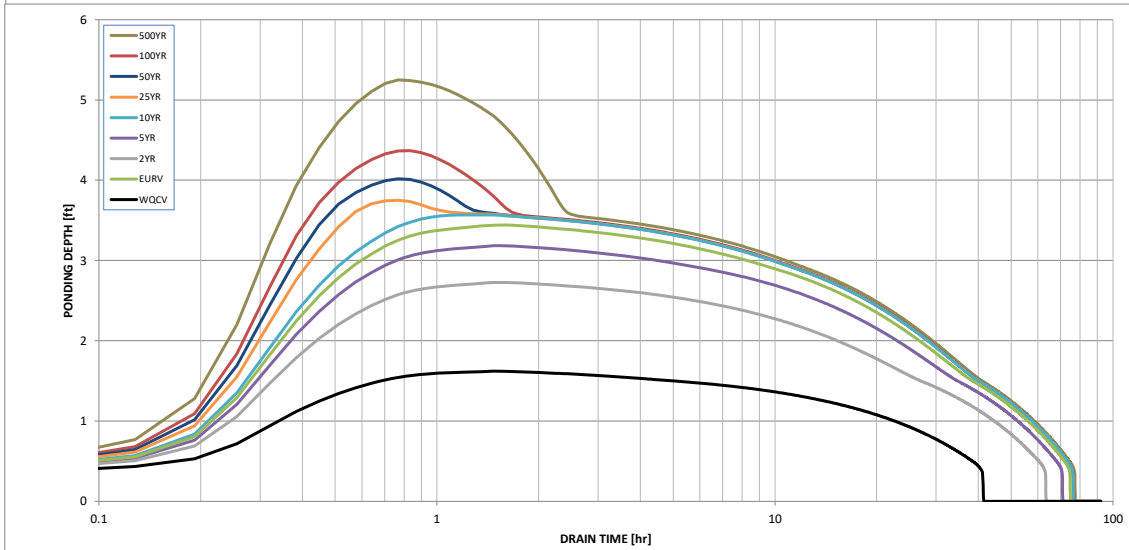
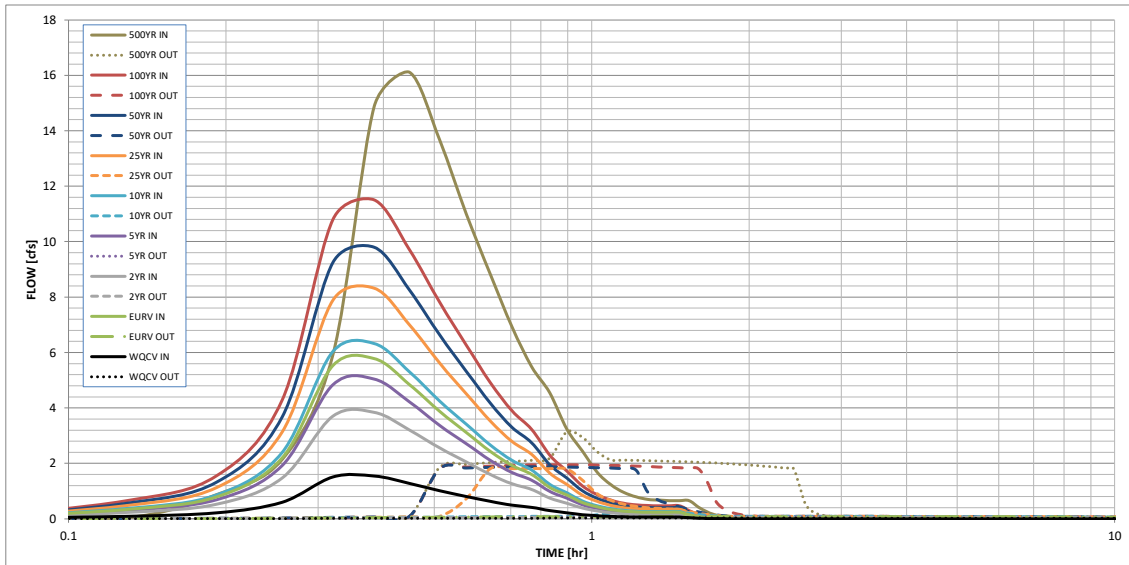
Calculated Parameters for Spillway

Spillway Design Flow Depth = feet
Stage at Top of Freeboard = feet
Basin Area at Top of Freeboard = acres

Routed Hydrograph Results

	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year	500 Year
Design Storm Return Period =									
One-Hour Rainfall Depth (in) =	0.53	1.07	1.19	1.50	1.75	2.00	2.25	2.52	3.29
Calculated Runoff Volume (acre-ft) =	0.053	0.199	0.132	0.174	0.218	0.287	0.338	0.397	0.556
OPTIONAL Override Runoff Volume (acre-ft) =									
Inflow Hydrograph Volume (acre-ft) =	0.052	0.199	0.132	0.173	0.217	0.286	0.338	0.397	0.555
Predevelopment Unit Peak Flow, q (cfs/acre) =	0.00	0.00	0.00	0.01	0.02	0.23	0.48	0.78	1.41
Predevelopment Peak Q (cfs) =	0.0	0.0	0.0	0.0	0.1	0.6	1.2	2.0	3.7
Peak Inflow Q (cfs) =	1.5	5.8	3.8	5.0	6.3	8.3	9.8	11.5	16.1
Peak Outflow Q (cfs) =	0.0	0.1	0.1	0.1	0.3	1.8	1.9	2.0	3.1
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	2.4	5.0	3.0	1.5	1.0	0.9
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Overflow Grate 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1	Spillway
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	0.0	0.2	0.2	0.2	0.2
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	39	68	59	65	69	67	66	64	61
Time to Drain 99% of Inflow Volume (hours) =	41	72	62	69	74	73	72	72	71
Maximum Ponding Depth (ft) =	1.62	3.44	2.73	3.18	3.57	3.75	4.02	4.37	5.25
Area at Maximum Ponding Depth (acres) =	0.06	0.10	0.08	0.09	0.10	0.11	0.11	0.12	0.15
Maximum Volume Stored (acre-ft) =	0.050	0.190	0.125	0.165	0.202	0.222	0.250	0.291	0.411

Detention Basin Outlet Structure Design



S-A-V-D Chart Axis Override

	X-axis	Left Y-Axis	Right Y-Axis
minimum bound			
maximum bound			

Channel Report

Trickle Channel EDB C

Triangular

Side Slopes (z:1) = 4.00, 4.00

Total Depth (ft) = 0.50

Invert Elev (ft) = 1.00

Slope (%) = 0.50

N-Value = 0.012

Calculations

Compute by: Known Q

Known Q (cfs) = 0.22

Highlighted

Depth (ft) = 0.18

Q (cfs) = 0.220

Area (sqft) = 0.13

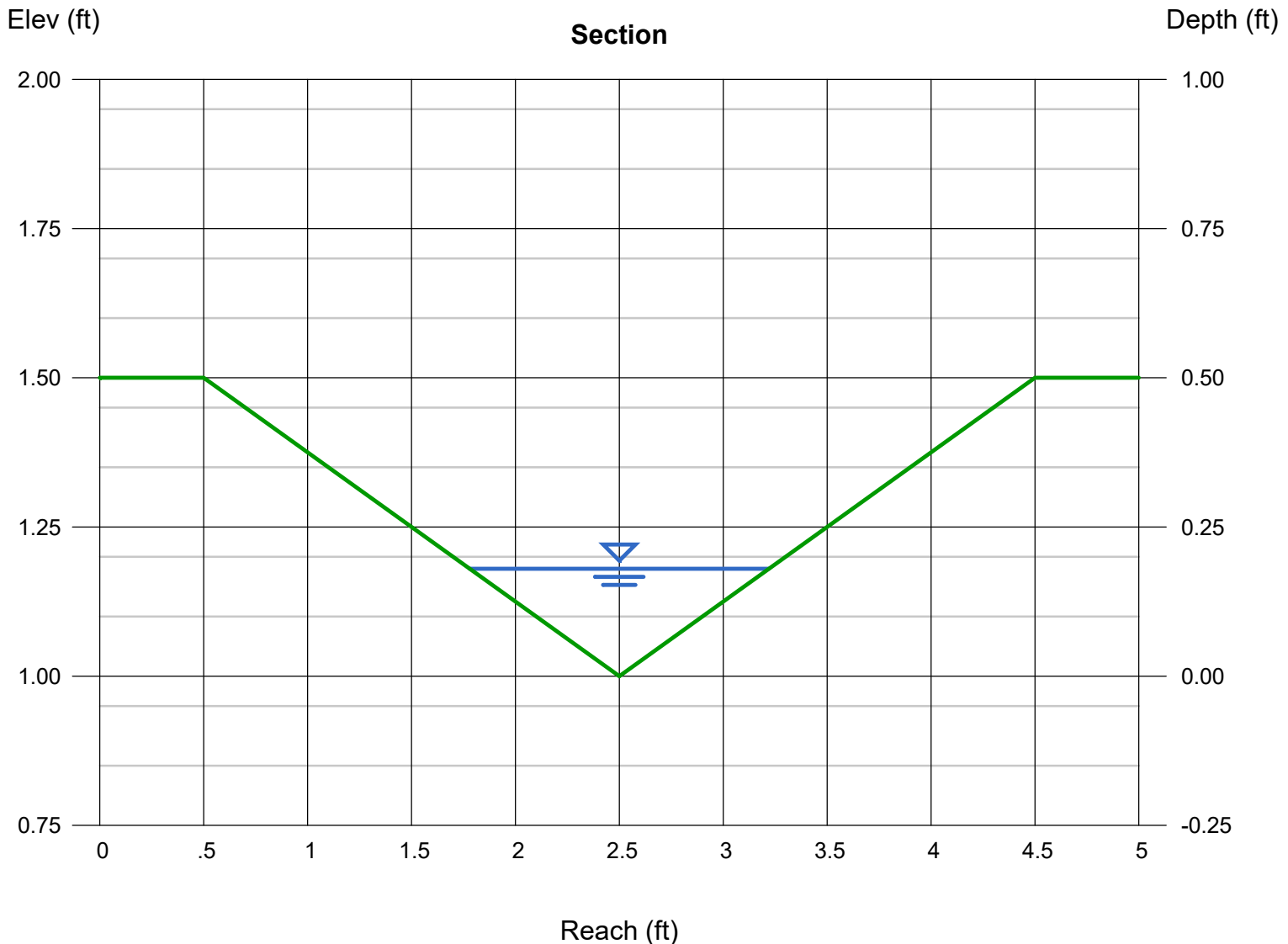
Velocity (ft/s) = 1.70

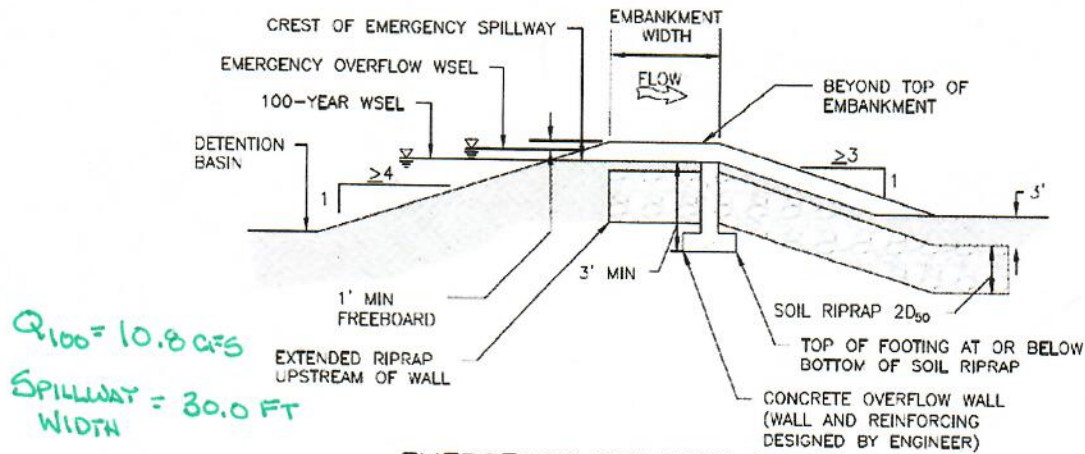
Wetted Perim (ft) = 1.48

Crit Depth, Yc (ft) = 0.18

Top Width (ft) = 1.44

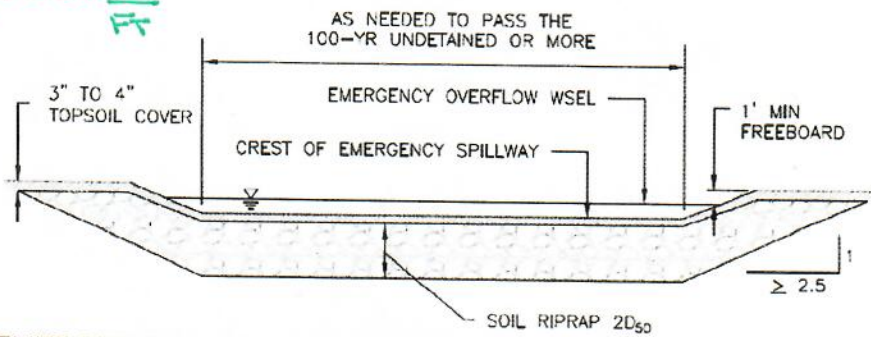
EGL (ft) = 0.22





$Q_{100} = 10.8 \text{ cfs}$
 Spillway = 30.0 FT WIDTH
 UNIT DISCHARGE = 0.36 cfs/ft

EMERGENCY SPILLWAY PROFILE



EMERGENCY SPILLWAY SECTION AND SPILLWAY CHANNEL

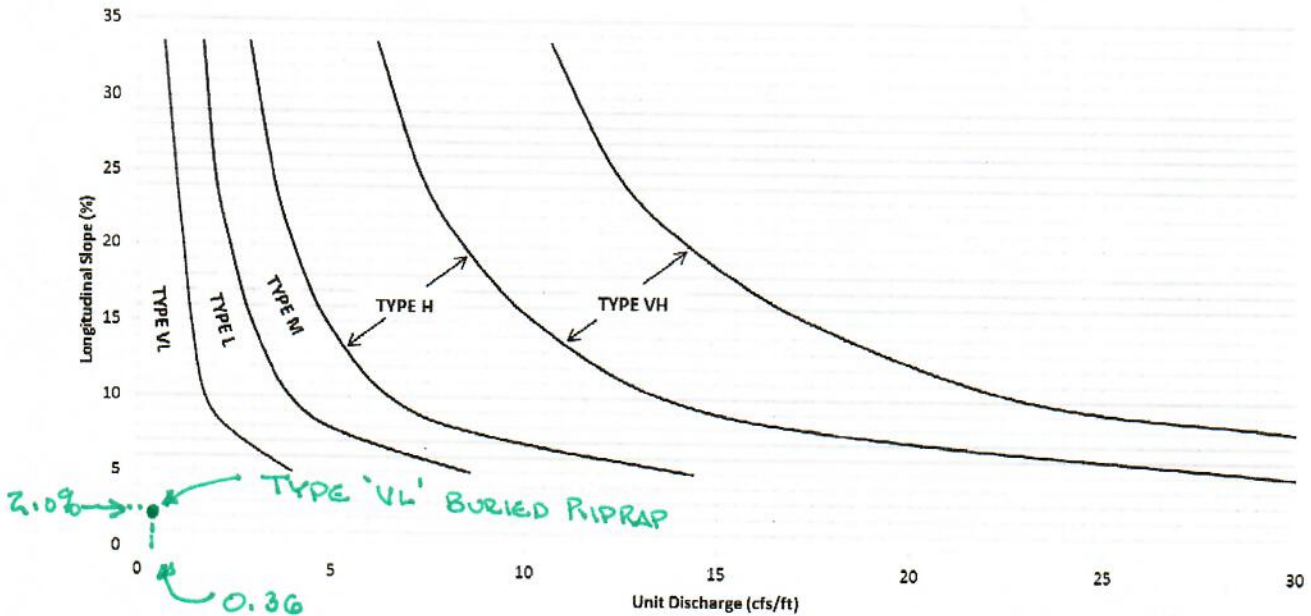


Figure 12-21. Embankment protection details and rock sizing chart (adapted from Arapahoe County)

Design Procedure Form: Runoff Reduction

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 1

Designer: David Mijares
Company: Catamount Engineering
Date: February 26, 2024
Project: COTTAGES AT DRY CREEK
Location: TOTAL

SITE INFORMATION (User Input in Blue Cells)

WQCV Rainfall Depth = 0.60 inches
 Depth of Average Runoff Producing Storm, d_s = 0.43 inches (for Watersheds Outside of the Denver Region, Figure 3-1 in USDCM Vol. 3)

Area Type	DCIA	SPA	UIA:RPA	DCIA	SPA	UIA:RPA	DCIA	SPA	UIA:RPA	DCIA	SPA	UIA:RPA
Area ID	A1 IMP	A1 PERV	A1-DC-RPA	A2-IMP	A2 PERV	A2-DC-RPA	B-IMP	B-PERV	B-DC-RPA	C-IMP	C-PERV	C-DC-RPA
Downstream Design Point ID	A	A	A	A	A	A	B	B	B	C	C	C
Downstream BMP Type	EDB	EDB	EDB	EDB	EDB	EDB	EDB	EDB	EDB	EDB	EDB	EDB
DCIA (ft ²)	32,083	--	--	35,629	--	--	28,361	--	--	22,205	--	--
UIA (ft ²)	--	--	37,008	--	--	26,214	--	--	33,161	--	--	48,360
RPA (ft ²)	--	--	11,456	--	--	12,078	--	--	9,564	--	--	10,437
SPA (ft ²)	--	41,657	--	--	34,732	--	--	56,980	--	--	31,818	--
HSG A (%)	--	100%	100%	--	100%	100%	--	100%	100%	--	100%	100%
HSG B (%)	--	0%	0%	--	0%	0%	--	0%	0%	--	0%	0%
HSG C/D (%)	--	0%	0%	--	0%	0%	--	0%	0%	--	0%	0%
Average Slope of RPA (ft/ft)	--	--	0.020	--	--	0.020	--	--	0.015	--	--	0.010
UIA:RPA Interface Width (ft)	--	--	15.00	--	--	15.00	--	--	10.00	--	--	15.00

CALCULATED RUNOFF RESULTS

Area ID	A1 IMP	A1 PERV	A1-DC-RPA	A2-IMP	A2 PERV	A2-DC-RPA	B-IMP	B-PERV	B-DC-RPA	C-IMP	C-PERV	C-DC-RPA
UIA:RPA Area (ft ²)	--	--	48,464	--	--	38,292	--	--	42,725	--	--	58,797
L / W Ratio	--	--	16.00	--	--	16.00	--	--	16.00	--	--	16.00
UIA / Area	--	--	0.7636	--	--	0.6846	--	--	0.7761	--	--	0.8225
Runoff (in)	0.50	0.00	0.00	0.50	0.00	0.00	0.50	0.00	0.00	0.50	0.00	0.00
Runoff (ft ³)	1337	0	0	1485	0	0	1182	0	0	925	0	0
Runoff Reduction (ft ³)	0	2083	1542	0	1737	1092	0	2849	1382	0	1591	2015

CALCULATED WQCV RESULTS

Area ID	A1 IMP	A1 PERV	A1-DC-RPA	A2-IMP	A2 PERV	A2-DC-RPA	B-IMP	B-PERV	B-DC-RPA	C-IMP	C-PERV	C-DC-RPA
WQCV (ft ³)	1337	0	1542	1485	0	1092	1182	0	1382	925	0	2015
WQCV Reduction (ft ³)	0	0	1542	0	0	1092	0	0	1382	0	0	2015
WQCV Reduction (%)	0%	0%	100%	0%	0%	100%	0%	0%	100%	0%	0%	100%
Untreated WQCV (ft ³)	1337	0	0	1485	0	0	1182	0	0	925	0	0

CALCULATED DESIGN POINT RESULTS (sums results from all columns with the same Downstream Design Point ID)

Downstream Design Point ID	A	B	C									
DCIA (ft ²)	67,712	28,361	22,205									
UIA (ft ²)	63,222	33,161	48,360									
RPA (ft ²)	23,534	9,564	10,437									
SPA (ft ²)	76,389	56,980	31,818									
Total Area (ft ²)	230,857	128,066	112,820									
Total Impervious Area (ft ²)	130,934	61,522	70,565									
WQCV (ft ³)	5,456	2,563	2,940									
WQCV Reduction (ft ³)	2,634	1,382	2,015									
WQCV Reduction (%)	48%	54%	69%									
Untreated WQCV (ft ³)	2,821	1,182	925									

CALCULATED SITE RESULTS (sums results from all columns in worksheet)

Total Area (ft ²)	471,743
Total Impervious Area (ft ²)	263,021
WQCV (ft ³)	10,959
WQCV Reduction (ft ³)	8,031
WQCV Reduction (%)	55%
Untreated WQCV (ft ³)	4,928

USED TO SIZE WQCV FOR POND 'C'

Design Procedure Form: Runoff Reduction

UD-BMP (Version 3.07, March 2018)

Sheet 1 of 1

Designer: David Mijares
Company: Catamount Engineering
Date: February 13, 2024
Project: COTTAGES AT DRY CREEK
Location: TOTAL

SITE INFORMATION (User Input in Blue Cells)

WQCV Rainfall Depth = 0.60 inches
 Depth of Average Runoff Producing Storm, d_e = 0.43 inches (for Watersheds Outside of the Denver Region, Figure 3-1 in USDCM Vol. 3)

Area Type	DCIA	SPA	UIA:RPA	DCIA	SPA	UIA:RPA	DCIA	SPA	UIA:RPA	DCIA	SPA	UIA:RPA
Area ID	A1 IMP	A1 PERV	A1-DC-RPA	A2-IMP	A2 PERV	A2-DC-RPA	B-IMP	B-PERV	B-DC-RPA	C-IMP	C-PERV	C-DC-RPA
Downstream Design Point ID	A	A	A	A	A	A	B	B	B	C	C	C
Downstream BMP Type	EDB	EDB	EDB	EDB	EDB	EDB	EDB	EDB	EDB	EDB	EDB	EDB
DCIA (ft ²)	32,083	--	--	35,629	--	--	28,361	--	--	22,205	--	--
UIA (ft ²)	--	--	37,008	--	--	26,214	--	--	33,161	--	--	48,360
RPA (ft ²)	--	--	11,456	--	--	12,078	--	--	9,564	--	--	10,437
SPA (ft ²)	--	41,657	--	--	34,732	--	--	56,980	--	--	31,818	--
HSG A (%)	--	100%	100%	--	100%	100%	--	100%	100%	--	100%	100%
HSG B (%)	--	0%	0%	--	0%	0%	--	0%	0%	--	0%	0%
HSG C/D (%)	--	0%	0%	--	0%	0%	--	0%	0%	--	0%	0%
Average Slope of RPA (ft/ft)	--	--	0.020	--	--	0.020	--	--	0.015	--	--	0.010
UIA:RPA Interface Width (ft)	--	--	15.00	--	--	15.00	--	--	10.00	--	--	15.00

CALCULATED RUNOFF RESULTS

Area ID	A1 IMP	A1 PERV	A1-DC-RPA	A2-IMP	A2 PERV	A2-DC-RPA	B-IMP	B-PERV	B-DC-RPA	C-IMP	C-PERV	C-DC-RPA
UIA:RPA Area (ft ²)	--	--	48,464	--	--	38,292	--	--	42,725	--	--	58,797
L / W Ratio	--	--	16.00	--	--	16.00	--	--	16.00	--	--	16.00
UIA / Area	--	--	0.7636	--	--	0.6846	--	--	0.7761	--	--	0.8225
Runoff (in)	0.50	0.00	0.00	0.50	0.00	0.00	0.50	0.00	0.00	0.50	0.00	0.00
Runoff (ft ³)	1337	0	0	1485	0	0	1182	0	0	925	0	0
Runoff Reduction (ft ³)	0	2083	1542	0	1737	1092	0	2849	1382	0	1591	2015

CALCULATED WQCV RESULTS

Area ID	A1 IMP	A1 PERV	A1-DC-RPA	A2-IMP	A2 PERV	A2-DC-RPA	B-IMP	B-PERV	B-DC-RPA	C-IMP	C-PERV	C-DC-RPA
WQCV (ft ³)	1337	0	1542	1485	0	1092	1182	0	1382	925	0	2015
WQCV Reduction (ft ³)	0	0	1542	0	0	1092	0	0	1382	0	0	2015
WQCV Reduction (%)	0%	0%	100%	0%	0%	100%	0%	0%	100%	0%	0%	100%
Untreated WQCV (ft ³)	1337	0	0	1485	0	0	1182	0	0	925	0	0

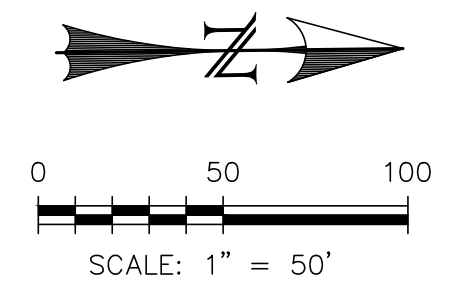
CALCULATED DESIGN POINT RESULTS (sums results from all columns with the same Downstream Design Point ID)

Downstream Design Point ID	A	B	C									
DCIA (ft ²)	67,712	28,361	22,205									
UIA (ft ²)	63,222	33,161	48,360									
RPA (ft ²)	23,534	9,564	10,437									
SPA (ft ²)	76,389	56,980	31,818									
Total Area (ft ²)	230,857	128,066	112,820									
Total Impervious Area (ft ²)	130,934	61,522	70,565									
WQCV (ft ³)	5,456	2,563	2,940									
WQCV Reduction (ft ³)	2,634	1,382	2,015									
WQCV Reduction (%)	48%	54%	69%									
Untreated WQCV (ft ³)	2,821	1,182	925									

CALCULATED SITE RESULTS (sums results from all columns in worksheet)

Total Area (ft ²)	471,743
Total Impervious Area (ft ²)	263,021
WQCV (ft ³)	10,959
WQCV Reduction (ft ³)	6,031
WQCV Reduction (%)	55%
Untreated WQCV (ft ³)	4,928

DRAINAGE MAP



AREA CALCULATIONS						
AREA ID	TOTAL AREA (SQ FT)	DCIA AREA (SQ FT)	SPA AREA (SQ FT)	UIA AREA (SQ FT)	RPA AREA (SQ FT)	WOCV REDUCTION
A	230857	67712	76389	63222	23534	48%
B	128066	28361	56980	33161	9564	54%
C	112820	22205	31818	48360	10437	69%
TOTAL	471743					55%



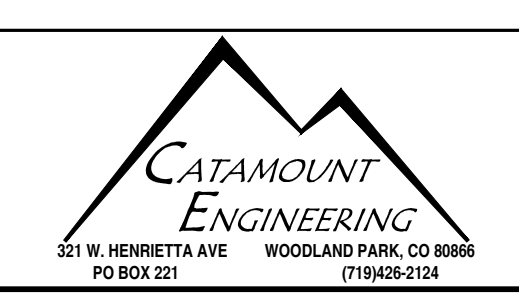
RUNOFF REDUCTION LEGEND

- AREA ID 3
- SURFACE SHEET FLOW DIRECTION
- PROPERTY BOUNDARY
- RIGHT-OF-WAY
- LOT LINE
- (E) STORM SEWER, INLET, MH
- (P) STORM SEWER, INLET, MH
- DRAINAGE BASIN BOUNDARY
- (P) DRAINAGE SWALE
- (E) STREAMSIDE OVERLAY OUTER
- (E) STREAMSIDE OVERLAY INNER
- (E) FLOODPLAIN ZONE - AE
- (E) FLOODPLAIN ZONE - X

REV.	DESCRIPTION	DATE
1	DEVELOPMENT PLAN AMENDMENT	1/3/24

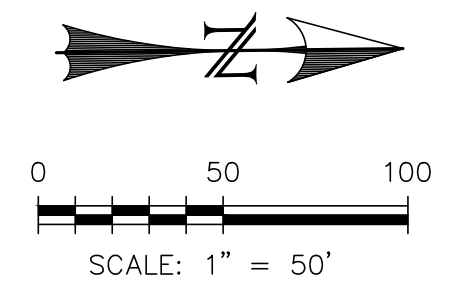
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BCC MANAGEMENT, LLC
 150 WUTHERING HEIGHTS DRIVE
 COLORADO SPRINGS, CO 80921



**MARK DRABLING COTTAGES
 NORTH PORTION**
RUNOFF REDUCTION

DESIGNED BY: DLM	DRAWN BY: DLM
SCALE: 1" = 100'	DATE: 12/20/22
JOB NUMBER: 20-270	SHEET: 1 OF 1



AREA CALCULATIONS						
AREA ID	TOTAL AREA (SQ FT)	DCIA AREA (SQ FT)	SPA AREA (SQ FT)	UIA AREA (SQ FT)	RPA AREA (SQ FT)	WQCV REDUCTION
A	230857	67712	76389	63222	23534	48%
B	128066	28361	56980	33161	9564	54%
C	112820	22205	31818	48360	10437	69%
TOTAL	471743					55%



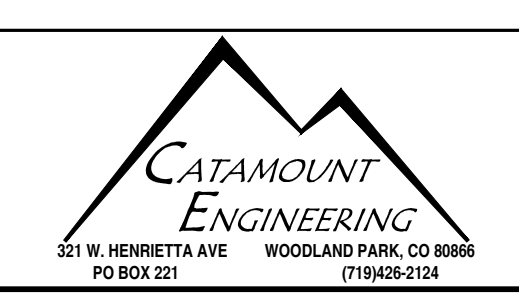
RUNOFF REDUCTION LEGEND

- AREA ID 3
- SURFACE SHEET FLOW DIRECTION
- PROPERTY BOUNDARY
- RIGHT-OF-WAY
- LOT LINE
- (E) STORM SEWER, INLET, MH
- (P) STORM SEWER, INLET, MH
- DRAINAGE BASIN BOUNDARY
- (P) DRAINAGE SWALE
- (E) STREAMSIDE OVERLAY OUTER
- (E) STREAMSIDE OVERLAY INNER
- (E) FLOODPLAIN ZONE - AE
- (E) FLOODPLAIN ZONE - X

REV.	DESCRIPTION	DATE
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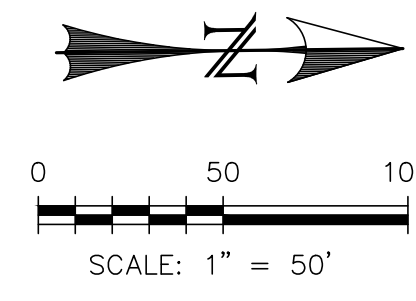


PREPARED FOR:
 BCC MANAGEMENT, LLC
 150 WUTHERING HEIGHTS DRIVE
 COLORADO SPRINGS, CO 80921



MARK DRABLING COTTAGES
 SOUTH PORTION
 RUNOFF REDUCTION

DESIGNED BY: DLM	DRAWN BY: DLM
SCALE: 1" = 100'	DATE: 12/20/22
JOB NUMBER: 20-270	SHEET: 1 OF 1



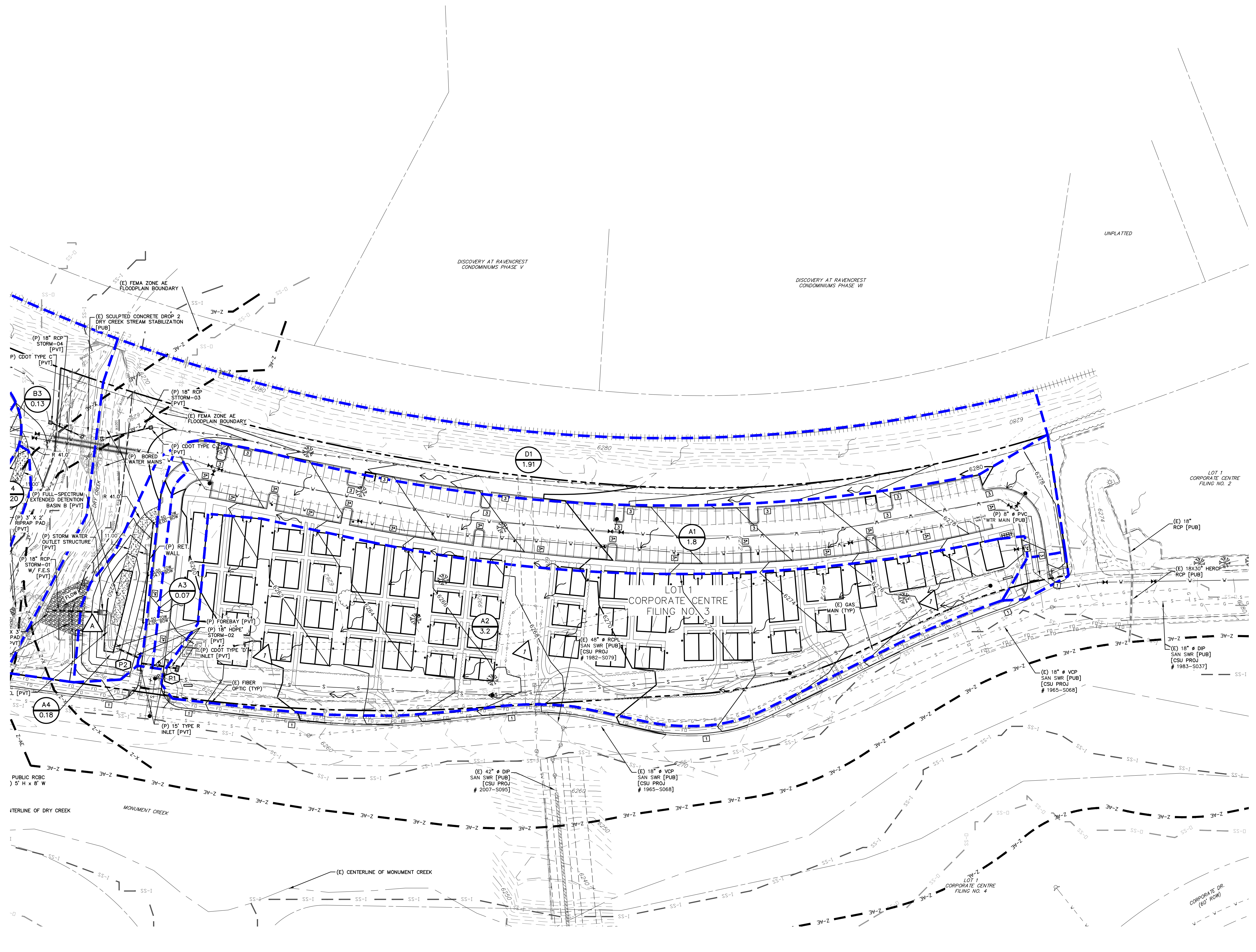
REVISED PER 11/05/24 DP AMENDMENT

PROPOSED DRAINAGE BASINS			
BASIN	AREA (ACRES)	Q5 (CFS)	Q100 (CFS)
A1	1.80	5.9	11.1
A2	3.20	2.8	7.3
A3	0.07	0.3	0.5
A4	0.18	0.2	0.7
B1	0.69	2.5	4.7
B2	1.92	2.5	6.0
B3	0.13	0.5	0.9
B4	0.20	0.1	0.7
C1	0.60	2.4	4.4
C2	1.42	1.8	4.7
C3	0.58	2.0	3.7
D1	1.91	0.6	3.4
D2	1.17	0.5	2.5
D3	1.19	0.5	2.7
D4	0.06	0.1	0.3

PROPOSED DESIGN POINTS		
BASIN	Q5 (CFS)	Q100 (CFS)
1	3.4	7.6
P1	6.2	13.8
P2	6.4	14.1
P3	4.2	9.2
P4	4.5	9.8
POND A	6.5	14.4
POND B	4.6	10.2
POND C	5.1	10.8

DRAINAGE LEGEND

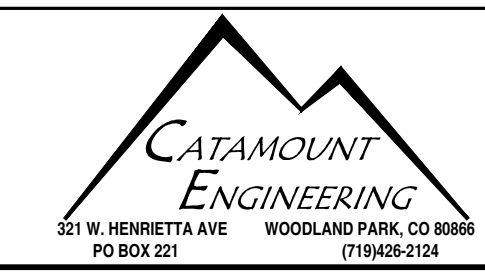
- BASIN IDENTIFIER
- BASIN AREA [AC]
- DESIGN POINT IDENTIFIERS
- PIPE DESIGN POINT
- EXISTING (E)
- PROPOSED (P)
- CURB AND GUTTER TYPE 1
- TYPE 3 SPILL
- TYPE 3 CARRY
- EASEMENT ESMT (E), PUB (P), PRIVATE (PVT), FUTURE (F)
- SLOPE/DIRECTION 1.00%
- SURFACE SHEET FLOW DIRECTION
- PROPERTY BOUNDARY
- RIGHT-OF-WAY
- LOT LINE
- (E) CONTOUR, INDEX
- (E) CONTOUR
- (P) CONTOUR, INDEX
- (P) CONTOUR
- (E) UG ELECTRIC
- (E) FIBER OPTIC
- (E) GAS MAIN
- (E) UG TELEPHONE
- (E) SANITARY MAIN, MH
- (E) STORM SEWER, INLET, MH
- (E) WATER MAIN, VALVE, FH
- (P) STORM SEWER, INLET, MH
- DRAINAGE BASIN BOUNDARY
- (P) DRAINAGE SWALE
- (E) STREAMSIDE OVERLAY OUTER
- (E) STREAMSIDE OVERLAY INNER
- (E) FLOODPLAIN ZONE - AE
- (E) FLOODPLAIN ZONE - X



REV.	DESCRIPTION	DATE
1	DEVELOPMENT PLAN AMENDMENT	1/3/24

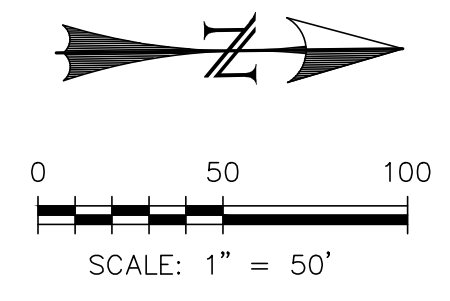
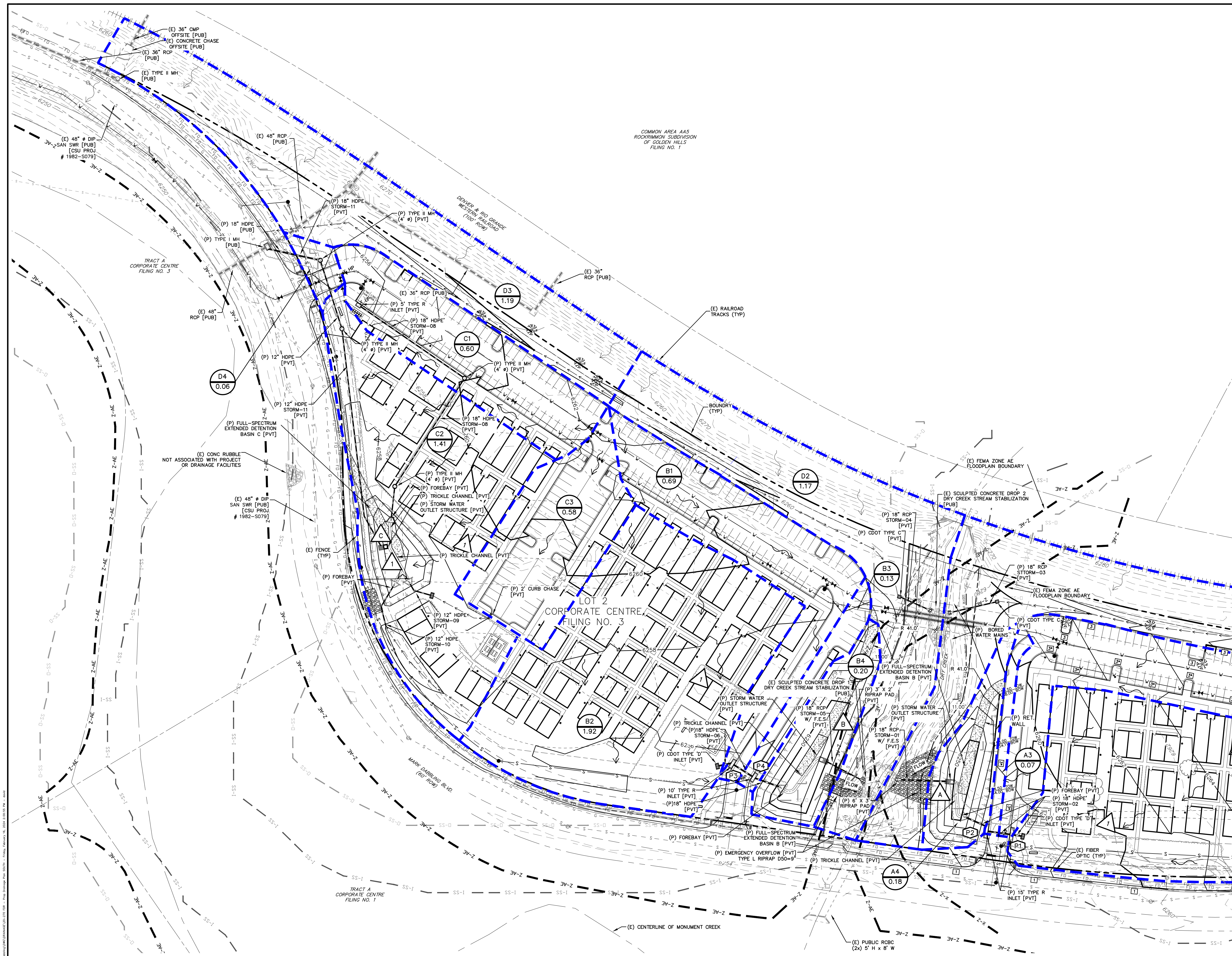
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BCC MANAGEMENT, LLC
150 WUTHERING HEIGHTS DRIVE
COLORADO SPRINGS, CO 80921



MARK DRABLING COTTAGES
NORTH PORTION
PROPOSED DRAINAGE PLAN

DESIGNED BY: DLM	DRAWN BY: DLM
SCALE: 1" = 50'	DATE: 2/11/21
JOB NUMBER: 20-270	SHEET: 1 OF 1



REVISED PER 11/05/24 DP AMENDMENT

PROPOSED DRAINAGE BASINS			
BASIN	AREA (ACRES)	Q5 (CFS)	Q100 (CFS)
A1	1.80	5.9	11.1
A2	3.20	2.8	7.3
A3	0.07	0.3	0.5
A4	0.18	0.2	0.7
B1	0.69	2.5	4.7
B2	1.92	2.5	6.0
B3	0.13	0.5	0.9
B4	0.20	0.1	0.7
C1	0.60	2.4	4.4
C2	1.42	1.8	4.7
C3	0.58	2.0	3.7
D1	1.91	0.6	3.4
D2	1.17	0.5	2.5
D3	1.19	0.5	2.7
D4	0.06	0.1	0.3

PROPOSED DESIGN POINTS		
BASIN	Q5 (CFS)	Q100 (CFS)
1	3.4	7.6
P1	6.2	13.8
P2	6.4	14.1
P3	4.2	9.2
P4	4.5	9.8
POND A	6.5	14.4
POND B	4.6	10.2
POND C	5.1	10.8

DRAINAGE LEGEND

BASIN IDENTIFIER
 BASIN AREA [AC]

DESIGN POINT IDENTIFIERS

PIPE DESIGN POINT

EXISTING (E)
 PROPOSED (P)
 CURB AND GUTTER
 TYPE 1
 TYPE 3 SPILL
 TYPE 3 CARRY

EASEMENT
 PUBLIC (PUB)
 PRIVATE (PVT)
 FUTURE (F)

SLOPE/DIRECTION
 SURFACE SHEET FLOW DIRECTION

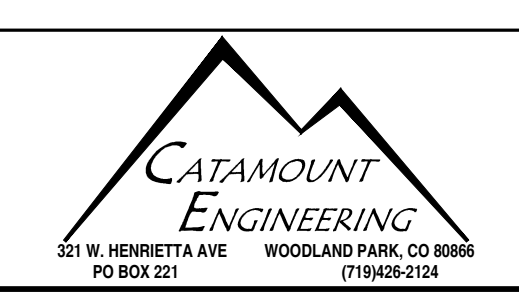
PROPERTY BOUNDARY
 RIGHT-OF-WAY
 LOT LINE
 (E) CONTOUR, INDEX
 (P) CONTOUR, INDEX
 (P) CONTOUR
 (E) CONTOUR
 (E) UG ELECTRIC
 (E) FIBER OPTIC
 (E) GAS MAIN
 (E) UG TELEPHONE
 (E) SANITARY MAIN, MH
 (E) STORM SEWER, INLET, MH
 (E) WATER MAIN, VALVE, FH
 (P) STORM SEWER, INLET, MH

DRAINAGE BASIN BOUNDARY
 (P) DRAINAGE SWALE
 (E) STREAMSIDE OVERLAY OUTER
 (E) STREAMSIDE OVERLAY INNER
 (E) FLOODPLAIN ZONE - AE
 (E) FLOODPLAIN ZONE - X

REV.	DESCRIPTION	DATE
1	DEVELOPMENT PLAN AMENDMENT	1/3/24



PREPARED FOR:
BCC MANAGEMENT, LLC
 150 WUTHERING HEIGHTS DRIVE
 COLORADO SPRINGS, CO 80921



MARK DRABLING COTTAGES
 SOUTH PORTION
PROPOSED DRAINAGE PLAN

DESIGNED BY:	DLM	DRAWN BY:	DLM
SCALE:	1" = 100'	DATE:	2/11/21
JOB NUMBER	20-270	SHEET	1 OF 1