

**MDDP AMENDMENT/PRELIMINARY DRAINAGE  
PLAN & REPORT  
FOR  
THE CREST AT WOODMEN  
PHASE 1 WEST, PHASE 2 EAST, PHASE 3 SOUTHEAST  
REDEVELOPMENT  
LOOART SUBDIVISION FILING No. 6  
Campus Drive and Woodmen Road  
Colorado Springs, Colorado**

**Developer:**

Crest at Woodmen, LLC  
431 North Weber  
Colorado Springs, CO 80903  
Contact: Steve Griggs  
Phone: 719.647.9211

**Prepared by:**

Galloway & Company, Inc.  
1755 Telstar Drive, Suite 107  
Colorado Springs, CO 80920  
Phone: 719.900.7220  
Fax: 303.770.3636  
Scott Brown, P.E.

Prepared: September 2018  
Revised: January 2019

**Certification Statements:**

This report and plan for the drainage design of The Crest at Woodmen Loourt Subdivision Filing No. 6 Phases 1, 2, & 3 was prepared by me (of under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the *City of Colorado Springs Drainage Criteria Manual* and is in conformity with the master plan of the drainage basin. I understand that the City of Colorado Springs does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



\_\_\_\_\_  
Scott Brown  
Registered Professional Engineer  
State of Colorado No. 45900

\_\_\_\_\_  
Date

01/30/2019

**Developer's Statement:**

Crest at Woodment, LLC hereby certifies that the drainage facilities for The Crest at Woodmen Loourt Subdivision Filing No. 6 - Phases 1, 2, & 3 shall be constructed according to the design presented in this report. I understand that the City of Colorado Springs does not and will not assume liability for the drainage facilities designed and/or certified by my engineer and that are submitted to the City of Colorado Springs pursuant to section 7.7.906 of the City Code; and cannot, on behalf of Crest at Woodmen, LLC, guarantee that final drainage design review will absolve Crest at Woodmen, LLC and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the final plat does not imply approval of my engineer's drainage design.

REALM REALTY  
\_\_\_\_\_  
Name of Developer

[Signature] 1/31/19  
\_\_\_\_\_  
Authorized Signature Date

CASEY SCALE  
\_\_\_\_\_  
Printed Name

ASSET MANAGER  
\_\_\_\_\_  
Title

431 North Weber, Colorado Springs, CO 80903  
Address:

**CITY OF COLORADO SPRINGS:**

Filed in accordance with Section 7.7.906 of the Code of the City of Colorado Springs, 2001, as amended.

Anna Bergmark  
\_\_\_\_\_  
For City Engineer

02/11/2019

\_\_\_\_\_  
Date

Conditions:

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## I. INTRODUCTION

This document is the Master Development Drainage Plan Amendment and Preliminary Drainage Report (MDDP/PDR) for The Crest at Woodmen - Phase 1 West, Phase 2 East, Phase 3 Southeast Project, which consists of redeveloping the property for commercial/retail uses.

The purpose of this report is to identify on and offsite drainage patterns, locate and identify tributary or downstream drainage features and facilities that impact the site and to identify drainage facility preliminary sizing and locations. An MDDP has been previously prepared for this site titled *Master Development Drainage Plan for the Crest at Woodmen – Looart Subdivision Filing No. 6* by Galloway & Company approved by the City on 5/17/18 (approved MDDP). This report will refine the conceptual design for the site since there is an updated site plan for the site. This report also discusses the changes from the approved MDDP, which entails including the proposed Campus Drive roadway and the location for Pond A moved from the southeast corner of the site to the southern end of the site.

## II. GENERAL LOCATION AND DESCRIPTION

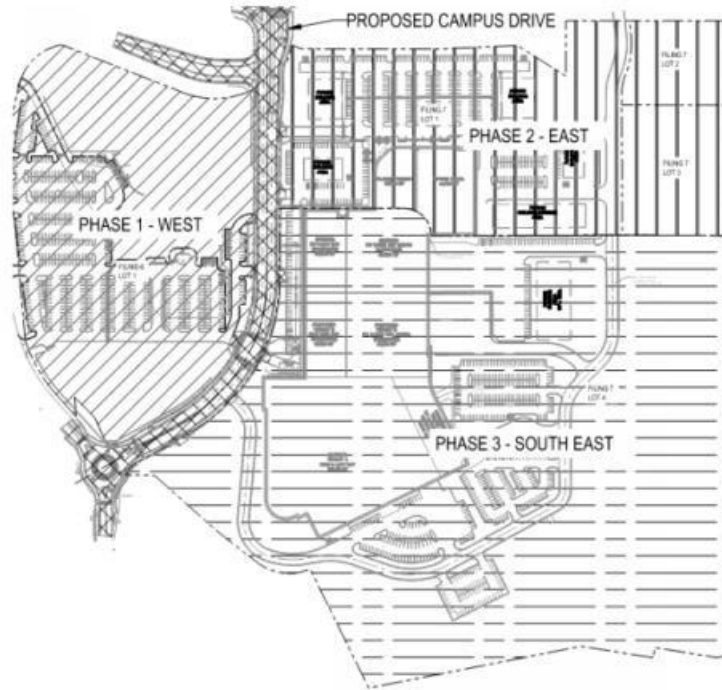
### A. Location

The Crest at Woodmen project property is located in the southwest one-quarter of Sections 8, Township 13 South, Range 66 West of the 6th Principal Meridian, in the City of Colorado Springs, El Paso County, Colorado. The development site is located south of E. Woodmen Road at Campus Drive in Colorado Springs, Colorado. This site is bounded by Woodmen Road to the north, Vincent Drive to the west, Yorkshire Estates to the east and Cottonwood Creek to the south. The site itself is currently developed with office and warehouse buildings and associated drives, parking, landscape and utilities. See the Vicinity Map in Appendix A.

The site currently covers an area of approximately 76.8 acres in size (Lot 1 Block 1 Looart Subdivision Filing 5). The site will be redeveloped into 4 phases: Campus Drive; Phase 1 West, Phase 2 East, and Phase 3 Southeast. Campus Drive is a proposed public road that runs north to south through the property and consists of approximately 2.6 acres, creating Lot 1 (west of Campus Dr.) and Lot 2 (east of Campus Dr.) as referenced in the Looart Filing 6 Plat (not yet recorded). A Preliminary/Final Drainage Report has been approved by the City for Campus Drive titled *Preliminary/Final Drainage Plan and Report for Crest at Woodmen Campus Drive Looart Subdivision Filing No. 6* (Campus FDR) by Galloway & Company approved 5/15/18.

The Crest at Woodmen Phase 1 West area (Looart Filing 6 Lot 1) examines approximately 15.6 acres and is bounded to the north and west by Vincent Drive, to the east by Campus Drive. Phases 2 and 3 will split Filing 6 – Lot 2 into 4 separate lots (reference the Filing 7 plat, to be recorded after Filing 6). The Crest at Woodmen Phase 2 East area (Looart Filing 7 Lots 1,2, and 3) examines approximately 17.0 acres and is bounded by the north by Woodmen Rd, by the west by Campus Drive, and by existing residential development to the east. Phase 2 - East is intended to be rezoned “PBC,” Planned Business Center, for the construction of

commercial/retail parcels. The Crest at Woodmen Phase 3 Southeast area (Looart Filing 7 Lot 4) examines approximately 41.8 acres and is bounded by the east by existing residential development and to the south by Cottonwood Creek. Refer to the Phasing exhibit below and in Appendix A.



According to the U.S. Department of Agriculture Natural Resources Conservation Service Soil Survey of El Paso County, Colorado the primary (82.3%) soil found is Blendon sandy loam; the remaining soils are Travessilla-Rock (9.7%) and Truckton sandy loam (11.4%). Blendon sandy loam are classified as Soil Conservation Service (SCS) hydrologic soil group “B”, Travessilla-Rock is classified as SCS hydrologic soil group “D” and Truckton sandy loam is classified as SCS hydrologic soil group “A”. For the purpose of this report, the drainage calculations used Type “B” to estimate the proposed runoff. A copy of the soil map as well as more detailed information regarding the individual soil properties can be found in Appendix A.

The proposed site is located within Zone X, as referenced from FEMA Flood Insurance Rate Map (08041C0516F).

### III. HISTORIC DRAINAGE PATTERNS AND FEATURES

The proposed project site is located within the Cottonwood Creek Drainage Basin as described in the Drainage Basin Planning Study (DBPS) prepared by URS in 1994. This study was later

modified by Ayres Associates in June of 2000. The study was modified to resolve high improvement costs associated with it and to address some unresolved issues.

For the purposes of this report historic refers to the pre-redeveloped state of the site. The pre-redeveloped state is depicted on the historic drainage map included in the appendices.

The proposed site is located in sub basin W2 of the Cottonwood Creek Basin per the DBPS. Subbasin W2 is approximately 79.7 acres in size.

The site is currently developed with multiple buildings and associated drives, parking and landscaping. There is a significant amount of trees and natural vegetation at the northwest corner of the site as well as along the west side of the site.

The topography of the site varies significantly across the property with the highest point of the site located in the northeast corner of the property. This high point, located at the northeast access (at Woodmen Road) is at an elevation of 6370. The existing drives and parking lots on site range in slopes from 2% to 7.4%. The open space areas range in slopes from 1% to 39%. The low point of the site is located at the southwest corner of the site where Vincent Drive crosses Cottonwood Creek.

In order to understand the existing hydrology, the project site was modeled in its current condition. The proposed project site comprises of portions of Basin W2 as identified in the Drainage Basin Planning Study prepared by URS. Outfall 20 corresponds to the Cottonwood Creek Tributary. For the purposes of the proposed project, Basin W2 was further subdivided as documented below, and shown on the Historic Drainage Map in Appendix E. However, in the current condition, there are 2 different outfall locations (southeast corner of Basin W2 and southwest corner of Basin W2, see Historic Drainage Map). A copy of the drainage map from the DBPS prepared by URS has been included for reference in Appendix B.

**BASIN W2a** is an 11.95 acre watershed which is comprised of open space and an existing water quality pond along the eastern edge of the site. This basin discharges via a grass swale at the southeast outfall of W2 ( $Q_5 = 2.8$  cfs,  $Q_{100} = 29.2$  cfs).

**Basin OS-E** is a 33.90 acre watershed ( $Q_5 = 151.1$  cfs,  $Q_{100} = 210.3$  cfs). This watershed covers the existing Yorkshire Estates Subdivision, portions of Woodmen Road, the existing Home Depot, REI, and other portions of the commercial development at the northwest corner of the Woodmen & Academy intersection. This basin is based upon information contained within the Woodmen Road Phase 1 improvements drainage report. This watershed outfalls into an existing water quality pond located on the subject property. Runoff in excess of the water quality volume overtops the pond and continues south through a stabilized channel to Cottonwood Creek.

**BASIN W2b** is a 2.56 acre watershed which is made up of portions of the existing parking lot on the north side of the site. Runoff from this basin enters the existing storm sewer system and ultimately discharges at the southeast outfall of W2 ( $Q_5 = 7.3$  cfs,  $Q_{100} = 16.4$  cfs).

**BASIN W2c** is a 1.56 acre watershed which is comprised of a portion of the existing building. Runoff generated from this basin enters the existing storm sewer system and ultimately discharges at the southeast outfall of W2 ( $Q_5 = 6.8$  cfs,  $Q_{100} = 12.2$  cfs).

**BASIN W2d** is a 5.07 acre watershed which is made up of a portion of the existing parking lot on the east side of the site. Stormwater generated from this basin enters the existing storm sewer system and ultimately discharges at the southeast outfall of W2 ( $Q_5 = 11.1$  cfs,  $Q_{100} = 27.5$  cfs).

**BASIN W2e** is a 4.23 acre watershed which contains a portion of the parking lot on the east side of the site. Runoff enters the existing storm sewer system and ultimately discharges at the southeast outfall of W2 ( $Q_5 = 11.4$  cfs,  $Q_{100} = 24.4$  cfs).

**BASIN W2f** is a 4.76 acre watershed containing a portion of the existing building. Runoff from this basin enters the existing storm sewer system and ultimately discharges at the southeast outfall of W2 ( $Q_5 = 20.6$  cfs,  $Q_{100} = 37.2$  cfs).

**BASIN W2g** is a 10.13 acre watershed which contains a portion of the existing parking lot at the southeast corner of the site. Stormwater from this basin enters the existing storm sewer system and ultimately discharges at the southeast outfall of W2 ( $Q_5 = 19.7$  cfs,  $Q_{100} = 52.3$  cfs).

**BASIN W2h** is a 3.49 acre watershed located at the north end of the site which is comprised of open space and a portion of a private roadway. Runoff generated within the basin enters the existing storm sewer system and ultimately discharges at the southwest outfall of W2 ( $Q_5 = 3.39$  cfs,  $Q_{100} = 10.3$  cfs).

**BASIN W2i** is a 5.28 acre watershed on the northwest side of the site which is comprised of open space and a portion of the existing parking lot. Stormwater from this basin enters the existing storm sewer system and ultimately discharges at the southwest outfall of W2 ( $Q_5 = 11.8$  cfs,  $Q_{100} = 29.4$  cfs).

**BASIN W2j** is a 0.74 acre watershed which is made up of a portion of an existing building on the west side of the site. Runoff from this basin enters the existing storm sewer system and ultimately discharges at the southwest outfall of W2 ( $Q_5 = 3.2$  cfs,  $Q_{100} = 5.8$  cfs).

**BASIN W2k** is a 0.55 acre watershed which is made up of a portion of an existing building on the west side of the site. Runoff from this basin enters the existing storm sewer system and ultimately discharges at the southwest outfall of W2 ( $Q_5 = 2.4$  cfs,  $Q_{100} = 4.3$  cfs).

**BASIN W2l** is a 6.01 acre watershed which is made up of a portion of an existing building in the center of the site. Runoff from this basin enters the existing storm sewer system and ultimately discharges at the southwest outfall of W2 ( $Q_5 = 26.1$  cfs,  $Q_{100} = 47.0$  cfs).

**BASIN W2m** is a 10.49 acre watershed in the southwest corner of the site, and is comprised of open space, private roadways, and parking lot. Runoff generated from this basin enters the existing storm sewer system and ultimately discharges at the southwest outfall of W2 ( $Q_5 = 9.7$  cfs,  $Q_{100} = 42.1$  cfs).

**BASIN W2n** is a 10.27 acre watershed along the southern edge of the site, and is comprised of open space, private roadways, and parking lot. Runoff generated from this basin sheet flows and discharges at the southwest outfall of W2 ( $Q_5 = 9.0$  cfs,  $Q_{100} = 35.8$  cfs).

**BASIN W2o** is a 4.09 acre watershed is comprised of open space along the western edge of the site. Runoff from this basin sheet flows south and is collected in the existing storm sewer system and discharges at the southwest outfall of W2 ( $Q_5 = 0.8$  cfs,  $Q_{100} = 12.8$  cfs).

**BASIN OS3** is a 2.12 acre watershed which sheet flows and is routed to an existing storm sewer inlet and outfalls into Basin W2m before ultimately discharging at the southwest outfall of W2 ( $Q_5 = 2.9$  cfs,  $Q_{100} = 9.6$  cfs).

**BASIN OS4** is a 0.80 acre watershed located on the northwest side of Vincent Drive (northwest corner of the site). Runoff from this basin enters the existing storm sewer system and ultimately discharges at the southwest outfall of W2 ( $Q_5 = 3.2$  cfs,  $Q_{100} = 6.0$  cfs).

#### IV. DRAINAGE DESIGN CRITERIA

The analysis and design of the stormwater management system for this project was prepared in accordance with the criteria set forth in the City of Colorado Springs Drainage Criteria Manual (DCM) Volumes 1 & 2, dated May 2014.

The rational method was used to calculate peak flows as the tributary areas are less than 100 acres. The rational method has been proven to be accurate for basins of this size and is based on the following formula:

$$Q = CIA$$

Where:

Q = Peak Discharge (cfs)

C = Runoff Coefficient

I = Runoff intensity (inches/hour)

A = Drainage area (acres)

The rainfall intensity calculations are based on the DCM Figure 6-5 and IDF equations. The one hour point rainfall data for the design are listed in Table 1 below.

**Table 1 - Precipitation Data**

Return Period	One Hour Depth (in.)	Intensity (in/hr)
5-year	1.50	5.17
100-year	2.52	8.68



Time of concentrations have been adapted from the equation 6-7 of The City of Colorado Springs Drainage Criteria Manual, Volume 1 which are as follows:

$$T_c = T_i + T_t$$

Where:

$T_c$  = time of concentration (min)

$T_i$  = overland (initial) flow time (min)

$T_t$  = travel time in the ditch, channel, gutter, storm sewer, etc. (min)

**Overland (Initial) Flow Time:** from equations 6-8 from the City of Colorado Springs Drainage Criteria Manual, Volume 1.

$$t_t = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$$

Where:

$T_i$  = overland (initial) flow

$C_5$  = runoff coefficient for 5-year frequency

$L$  = length of overland flow (300 ft maximum for non-urban land uses, 100 ft maximum for urban land uses)

$S$  = average basin slope

### Travel Time

$$V = C_v * S_w^{0.5}$$

Where:

$V$  = Velocity (ft/s)

$C_v$  = conveyance coefficient

$S_w$  = watercourse slope (ft/ft)

The runoff coefficients are calculated based on land use, percent imperviousness, and design storm for each basin, as shown in the DCM, (Table 6-6). The runoff coefficient for commercial impervious basins was 0.88 (100-year) and 0.81 (5-year) per the DCM. The appendix contains runoff coefficient calculations for basins that were not 100% impervious.

The 100-year event was used as the major storm event to show where inlets are necessary based on the capacity of the street and to estimate storm drain pipe sizes based on Mannings equation. Inlets will be sized at the Final Drainage Report stage.

The full spectrum detention method (FSD) was used to size both of the proposed water quality/detention ponds. This method attributes two design volumes; one being the Excess Urban Runoff Volume (EURV) and the other being the 100-year detention volume. This approach includes the Water Quality Capture Volume (WQCV) with the EURV; therefore, no additional volume for the WQCV is required. The equations contained within the DCM were utilized to

calculate the required EURV and WQCV values. The latest UD-Detention spreadsheet from UDFCD was not utilized as it contains different C values and allowable release rates than those contained within the DCM.

As will be discussed later in the report the hydraulics of the ponds is quite complex due to the accounting of water quality for offsite basins, but not EURV or 100-year flood volume for those basins. Additionally, Pond A will overdetain to allow a larger release from Pond B. To accurately account for the complex hydraulics of the ponds EPA SWMM 5.1.010 was utilized to both create hydrographs for the tributary basins and to route runoff through the ponds. EPA SWMM was also utilized to verify that the ponds WQ/EURV volume will drain in 72 hours while the straight WQCV for the pond does not drain faster than 40 hours. The UDFCD spreadsheet UD-Detention 2.34 was utilized to calculate the stage discharge curves for the ponds.

## **V. PROPOSED DRAINAGE PLAN**

### **A. General Description**

Historically, there are two outfall locations from the site; at the southeast corner of the site and the southwest corner of the site. The southwest outfall location will remain and an outfall will be provided at the southern portion of the site. There are two proposed detention ponds on the site. The purpose of the ponds is to provide water quality and detain developed runoff to at or below historic rates. The ponds will be discussed in more depth later in the report.

A future roadway has been designed to bisect the property, Campus Drive. A Preliminary/Final Drainage Report has been approved by the City for Campus Drive titled *Preliminary/Final Drainage Plan and Report for Crest at Woodmen Campus Drive Looart Subdivision Filing No. 6* (Campus FDR) by Galloway & Company approved 5/15/18. The detention pond shown in the Campus FDR for Campus Drive will be modified and enlarged and is now referenced as “Pond B” (see section V-D and the Proposed Drainage Map in Appendix D).

### **B. Four Step Process**

The Four Step Process to minimize the adverse impacts of urbanization is vital component of developing a balanced, sustainable project. Below identifies the approach to the four step process:

#### **1. Employ Runoff Reduction Practices**

This step uses low impact development (LID) practices to reduce runoff at the source. Generally rather than creating point discharged that are directly connected to impervious areas runoff is routed through pervious areas to promote infiltration. Due to the existing site constraints and topography this is a difficult task. Grass buffers and swales are encouraged and used where practical. Runoff reduction plays a large role in the overall system design as detention volume and water quality control volume is minimized.

#### **2. Implement BMPs That Provide a Water Quality Capture Volume with Slow Release**

This step utilizes formalized water quality capture volume to slow the release of runoff from the site. Both proposed ponds (Pond A & Pond B) will provide EURV volume for

the new development which incorporates a 72 hour release. These ponds will also provide WQCV for the offsite tributary areas which will release in no less than 40 hours.

### 3. Stabilize Drainageways

This step implements stabilization to channels to accommodate developed flows while protecting infrastructure and controlling sediment loading from erosion in the drainageways. Improvements to Cottonwood Creek have recently been made. These improvements have already taken into account developed flows from the site (as the site was currently developed). With this project, these rates will be reduced back to pre-redevelopment values. Therefore, the recently completed channel improvements will be adequate for this development as they take into account the existing undetained site conditions.

### 4. Implement Site Specific and Other Source Control BMPs

This step is typically implemented at a detailed level when the site develops. Source control BMPs protect the release of pollutants from outdoor storage areas. Trash enclosures will be provided for the lots as they develop which will reduce trash from leaving the lots. This will be identified and implemented within future Final Drainage reports for the site.

## C. Proposed Basins

The original DBPS prepared by URS identified one Basin for our project site, W2, as described previously. For the proposed drainage design, new basin designations were required as a result of the proposed improvements. The basin size and locations shown in the FDR for Campus Drive will stay the same.

The basins and their proposed size, shape and orientation can be seen on the proposed drainage map found in Appendix C.

**Basin A1** (2.47 AC,  $Q_5 = 10.2$  cfs,  $Q_{100} = 18.6$  cfs): a basin defining the area of future commercial development. With future development, a storm sewer system will collect runoff from this basin and tie into the proposed storm inlet at DP 50. Flow will be routed to proposed Pond A.

**Basin A2** (2.48 AC,  $Q_5 = 3.4$  cfs,  $Q_{100} = 8.4$  cfs): a basin defining the area of future private roadway and future commercial for the Phase 2 development. A proposed storm sewer system will collect runoff from this basin and tie into the proposed inlet at DP 54A. Flow will be routed to proposed Pond A. Any bypassed flow will enter Basin A7 and will enter the storm system at the inlet at DP 60A.

**Basin A3** (3.81 AC,  $Q_5 = 10.1$  cfs,  $Q_{100} = 19.8$  cfs): a basin defining the area of future commercial for the Phase 2 development. Flow will enter the system at the proposed inlet at DP 58 and will be routed to proposed Pond A.

**Basin A4** (3.44 AC,  $Q_5 = 14.6$  cfs,  $Q_{100} = 26.6$  cfs): a basin defining the area of building rooftop and future commercial lot for the Phase 2 development. The proposed storm sewer storm sewer system will collect runoff from this basin and tie into the proposed inlet at DP 59A. Flow will be

routed to proposed Pond A.

**Basin A5** (0.33 AC,  $Q_5 = 1.6$  cfs,  $Q_{100} = 2.8$  cfs): a basin defining the area of a future private roadway. The storm sewer system will collect runoff from this basin and tie into the proposed storm inlet at DP 54B. Flow will be routed to proposed Pond A.

**Basin A6** (3.33 AC,  $Q_5 = 14.0$  cfs,  $Q_{100} = 25.4$  cfs): a basin defining the area of a future commercial lot. With future development, a storm sewer system will collect runoff from this basin and tie into the proposed storm system at DP 51A. Flow will be routed to proposed Pond A.

**Basin A7** (2.86 AC,  $Q_5 = 11.7$  cfs,  $Q_{100} = 21.4$  cfs): a basin comprised of building rooftop and future commercial area for the Phase 3 development. An existing trench drain will remain in place and collect some of the runoff, with the rest entering the system at the inlet located at DP 60A. The proposed storm system will replace the existing storm sewer system and will collect runoff which will then be routed to Pond A.

**Basin A8** (0.60 AC,  $Q_5 = 2.8$  cfs,  $Q_{100} = 5.0$  cfs): a basin comprised of future commercial for the Phase 3 development. A proposed inlet will collect runoff at DP 61A and tie into the proposed storm sewer system that is replacing the existing system. Flow will be routed to proposed Pond A.

**Basin A9** (1.33 AC,  $Q_5 = 5.9$  cfs,  $Q_{100} = 10.6$  cfs): a basin comprised of a future commercial area for the Phase 3 development. With future development, a storm sewer system will collect runoff from this basin and tie into a future storm inlet at DP 55A. Flow will be routed to proposed Pond A.

**Basin A10** (2.75 AC,  $Q_5 = 11.4$  cfs,  $Q_{100} = 20.7$  cfs): a basin comprised of building rooftop and future commercial area for the Phase 3 development. An existing trench drain will remain in place and collect some of the runoff, with the rest entering the system at the inlet located at DP 62A. The proposed storm system will replace the existing storm sewer system and will collect runoff which will then be routed to Pond A.

**Basin A11** (3.80 AC,  $Q_5 = 15.7$  cfs,  $Q_{100} = 29.0$  cfs): a basin comprised of building rooftop and future commercial area for the Phase 3 development. Runoff will flow through the parking lot and enter the storm sewer system at the inlet at DP 56A. Flow will be routed to proposed Pond A.

**Basin A12** (0.24 AC,  $Q_5 = 1.0$  cfs,  $Q_{100} = 1.8$  cfs): a basin defining the area of future private roadway. The storm sewer system will collect runoff from this basin and tie into the proposed storm inlet at DP 56B. Flow will be routed to proposed Pond A.

**Basin A13** (5.00 AC,  $Q_5 = 17.3$  cfs,  $Q_{100} = 31.5$  cfs): a basin defining the area of a future commercial development. With future development, a storm sewer system will collect runoff from this basin and tie into the proposed storm inlet at DP 58C. Flow will be routed to proposed Pond A.

**Basin A14** (0.05 AC,  $Q_5 = 0.2$  cfs,  $Q_{100} = 0.4$  cfs): a basin defining a small area of future commercial for the Phase 3 development. The inlets will tie into the storm sewer system at DP 63

and will be routed to Pond A.

**Basin A15** (1.09 AC,  $Q_5 = 5.1$  cfs,  $Q_{100} = 9.1$  cfs): a basin defining future commercial area for the Phase 3 development. Runoff will be collected at DP 65A with an inlet and tied into the storm sewer system. Flow will be routed to proposed Pond A.

**Basin A16** (1.21 AC,  $Q_5 = 5.6$  cfs,  $Q_{100} = 10.1$  cfs): a basin defining the private roadway along the south side of the Phase 3 development. The storm sewer system will collect runoff from this basin at DP 57A. Flow will be routed to proposed Pond A.

**Basin A17** (5.24 AC,  $Q_5 = 19.8$  cfs,  $Q_{100} = 36.1$  cfs): a basin defining the area of future commercial development. With future development, a storm sewer system will collect runoff from this basin and tie into the proposed storm inlet at DP 66A. Flow will be routed to proposed Pond A.

**Basin A18** (4.12 AC,  $Q_5 = 16.9$  cfs,  $Q_{100} = 30.9$  cfs): a basin defining the area of future commercial development. With future development, a storm sewer system will collect runoff from this basin and tie into the proposed storm inlet at DP 66B. Flow will be routed to proposed Pond A.

**Basin A19** (0.69 AC,  $Q_5 = 3.2$  cfs,  $Q_{100} = 5.7$  cfs): a basin defining a future commercial area for the Phase 3 development. An inlet will collect runoff at DP 68A and into the storm sewer system to route the flow to Pond A.

**Basin A20** (1.06 AC,  $Q_5 = 4.9$  cfs,  $Q_{100} = 8.9$  cfs): a basin defining future commercial area. An inlet will collect runoff at DP 67A and into the storm sewer system to route the flow to Pond A.

**Basin A21** (0.45 AC,  $Q_5 = 2.1$  cfs,  $Q_{100} = 3.7$  cfs): a basin defining future commercial area. An inlet will collect runoff at DP 69A and into the storm sewer system to route the flow to Pond A.

**Basin A22** (3.45 AC,  $Q_5 = 1.8$  cfs,  $Q_{100} = 10.6$  cfs): a basin defining the area of Pond A. Pond A is the confluence point for all 'A' basins. Released flow from Pond A will outfall into Cottonwood Creek.

**Basin OSE** is a 33.90 acre watershed ( $Q_5 = 151.1$  cfs,  $Q_{100} = 259.4$  cfs). This watershed covers the existing Yorkshire Estates Subdivision, portions of Woodmen Road, the existing Home Depot, REI, and other portions of the commercial development at the northwest corner of the Woodmen & Academy intersection. This basin is based upon information contained within the Woodmen Road Phase 1 improvements drainage report. The existing pipe will be extended through the proposed site to the proposed Pond A. An excerpt from the Woodmen Road Phase 1 improvements Drainage Report can be found in Appendix B.

**Basin B1-1** (1.32 AC,  $Q_5 = 1.0$  cfs,  $Q_{100} = 5.0$  cfs): a basin consisting of steep terrain with shallow bedrock, has abundant vegetation and will remain undeveloped. Storm runoff will sheet flow to a proposed inlet west of Campus Drive at DP 1. This inlet is the start of the storm sewer system and will collect the flows and convey them to proposed Pond B.

**Basin B1-2** (0.38 AC,  $Q_5 = 1.2$  cfs,  $Q_{100} = 2.1$  cfs): a basin comprised of building rooftop for the Phase 1 development. Flow will enter a roof drain which will tie into the proposed system at DP 1. Flow will be routed to Pond B.

**Basin B2** (1.15 AC,  $Q_5 = 2.4$  cfs,  $Q_{100} = 5.3$  cfs): a basin consisting of Campus Drive half-street and walk areas. Runoff sheets flows from the street and walk areas and is conveyed in the proposed curb & gutter to the inlet at DP 7 and conveys the flow within the Campus Drive storm sewer system to proposed Pond B.

**Basin B3-1** (7.34 AC,  $Q_5 = 17.7$  cfs,  $Q_{100} = 34.7$  cfs): a basin defining the area of future commercial for the Phase 1 development. With future development, a storm sewer system will collect runoff from this basin and tie into the proposed storm inlet at DP 16. The storm sewer system will tie into the Campus Drive storm sewer system and flows will be routed to proposed Pond B.

**Basin B3-2** (1.31 AC,  $Q_5 = 4.8$  cfs,  $Q_{100} = 8.9$  cfs): a basin defining the area of future commercial for the Phase 1 development. With future development, a storm sewer system will collect runoff from this basin and tie into the proposed storm inlet at DP 8A. The storm sewer system will tie into the Campus Drive storm sewer system and flows will be routed to proposed Pond B.

**Basin B3-3** (0.64 AC,  $Q_5 = 2.2$  cfs,  $Q_{100} = 4.2$  cfs): a basin defining the area of future commercial for the Phase 1 development. With future development, a storm sewer system will collect runoff from this basin and tie into the proposed storm inlet at DP 8B. The storm sewer system will tie into the Campus Drive storm sewer system and flows will be routed to proposed Pond B.

**Basin B3-4** (0.92 AC,  $Q_5 = 2.8$  cfs,  $Q_{100} = 5.2$  cfs): a basin comprised of building rooftop for the Phase 1 development. Flow will enter a roof drain which will tie into the proposed system at DP 8A. Flow will be routed to Pond B.

**Basin B4-1** (1.69 AC,  $Q_5 = 6.9$  cfs,  $Q_{100} = 12.6$  cfs): a basin defining the area of future commercial development. With future development, a storm sewer system will collect runoff from this basin and tie into the proposed storm inlet at DP 13. The storm sewer system will tie into the Campus Drive storm sewer system and flows will be routed to proposed Pond B.

**Basin B4-2** (0.87 AC,  $Q_5 = 3.6$  cfs,  $Q_{100} = 6.7$  cfs): a basin defining the area of future commercial development. With future development, a storm sewer system will collect runoff from this basin and tie into the proposed storm inlet at DP 18. The storm sewer system will tie into the Campus Drive storm sewer system and flows will be routed to proposed Pond B.

**Basin B5-1** (0.51 AC,  $Q_5 = 1.8$  cfs,  $Q_{100} = 3.3$  cfs): a basin consisting of Campus Drive half-street and walk areas. Runoff sheet flows from the street and walk areas and is conveyed in the proposed curb & gutter to the inlet at DP 11 and conveys the flow within the Campus Drive storm sewer system to proposed Pond B.

**Basin B5-2** (0.55 AC,  $Q_5 = 1.9$  cfs,  $Q_{100} = 3.6$  cfs): a basin containing a portion of Campus Drive half-street, the roundabout and existing Vincent Drive half-street. Runoff from this basin will be collected in an existing storm inlet at DP 24 and will be routed to Cottonwood Creek in an existing storm sewer system. This basin flows to existing inlets within Vincent Dr. which discharges into Cottonwood Creek.

**Basin B5-3** (0.16 AC,  $Q_5 = 0.6$  cfs,  $Q_{100} = 1.1$  cfs): a basin containing a portion of Campus Drive half-street, the roundabout and existing Vincent Drive half-street. Runoff from this basin will be collected at DP 25 and continue to flow southeasterly towards an existing inlet in Vincent Drive which will be routed to Cottonwood Creek in an existing storm sewer system. This basin flows to existing inlets within Vincent Dr. which discharges into Cottonwood Creek.

**Basin B6** (3.03 AC,  $Q_5 = 11.4$  cfs,  $Q_{100} = 21.3$  cfs): a basin comprised of building rooftop for the Phase 3 development. Runoff will flow into Basin 7-1 and will enter the storm sewer system to be routed to Pond B.

**Basin B7-1** (0.55 AC,  $Q_5 = 0.3$  cfs,  $Q_{100} = 1.5$  cfs): a basin comprised of commercial area for the Phase 3 development. Flow will enter the storm system at DP 27A and will be routed to Pond B.

**Basin B7** (2.51 AC,  $Q_5 = 3.3$  cfs,  $Q_{100} = 9.4$  cfs): a basin comprised of a private drive that connects to Campus Drive. Flow will enter the storm system at DP 27 and will be routed to Pond B.

**Basin B8** (0.90 AC,  $Q_5 = 2.5$  cfs,  $Q_{100} = 5.0$  cfs): a basin consisting of Campus Drive half-street and walk areas as well as a portion of a new local street and adjacent landscaping. Runoff sheet flows from the street and walk areas and is conveyed in the proposed curb & gutter to the inlet at DP 12 and conveys the flow within the Campus Drive storm sewer system to proposed Pond B

**Basin B9-1** (0.72 AC,  $Q_5 = 2.7$  cfs,  $Q_{100} = 5.0$  cfs): a basin comprised of building rooftop for the Phase 3 development. Flow will enter a roof drain at DP 9A which will be routed to the Campus Drive storm sewer system to proposed Pond B.

**Basin B9** (0.96 AC,  $Q_5 = 1.6$  cfs,  $Q_{100} = 3.4$  cfs): a basin comprised of future commercial area for the Phase 3 development. Runoff will enter the system at DP 9 which will tie into the Campus Drive storm system. Flow will be routed to Pond B.

**Basin B10** (1.05 AC,  $Q_5 = 3.7$  cfs,  $Q_{100} = 7.1$  cfs): a basin consisting of Campus Drive half-street and walk areas. Runoff sheet flows from the street and walk areas and is conveyed in the proposed curb & gutter to the inlet at DP 4 and conveys the flow within the Campus Drive storm sewer system to proposed Pond B.

**Basin B11-1** (2.00 AC,  $Q_5 = 0.8$  cfs,  $Q_{100} = 5.4$  cfs): a basin defining an open space area. Flow will enter the system at DP 2A and will be routed to proposed Pond B.

**Basin B11** (1.65 AC,  $Q_5 = 4.3$  cfs,  $Q_{100} = 8.7$  cfs): a basin comprised of a future building rooftop and future commercial area for the Phase 2 development. Runoff will enter the system at DP 2B which will tie into the storm sewer system. Flow will be routed to Pond B through the Campus Drive storm system.

**Basin B12-1** (0.69 AC,  $Q_5 = 2.6$  cfs,  $Q_{100} = 4.9$  cfs): a basin comprised of building rooftop for the Phase 3 development. Flow will enter a roof drain which will tie into the proposed system at DP 2. Flow will be routed to Pond B through the Campus Drive storm system.

**Basin B12** (0.77 AC,  $Q_5 = 2.8$  cfs,  $Q_{100} = 5.4$  cfs): a basin comprised of a future building rooftop and future commercial area for the Phase 2 development. Runoff will enter the system at DP 2C

which will tie into the storm sewer system. Flow will be routed to Pond B through the Campus Drive storm system.

**Basin OS1** (1.29 AC,  $Q_5 = 5.2$  cfs,  $Q_{100} = 9.6$  cfs): a basin comprised of proposed roadway and open space area. Runoff from this basin will be collected in a storm inlet at DP 21 and will be routed to the existing storm sewer system within Woodmen Road.

**Basin OS2** (0.54 AC,  $Q_5 = 0.9$  cfs,  $Q_{100} = 2.6$  cfs): a basin comprised of reconstructed Vincent Drive southern half-street and adjacent area. Runoff from this basin will be collected in a storm inlet at DP 22 and will be routed to a new storm sewer system which ties into the existing storm sewer system as part of the Campus Drive Roadway improvements. The existing storm sewer system ties into an existing storm sewer system within Woodmen Road.

**BASIN OS3** (0.76 AC,  $Q_5 = 1.7$  cfs,  $Q_{100} = 3.9$  cfs): a basin comprised of reconstructed Vincent Drive northern half-street and adjacent area. Runoff from this basin will be collected in a storm inlet at DP 23 and will be routed to a new storm sewer system which ties into the existing storm sewer system as part of the Campus Drive Roadway improvements. The existing storm sewer system ties into an existing storm sewer system within Woodmen Road.

**BASIN OS4** (2.05 AC,  $Q_5 = 2.9$  cfs,  $Q_{100} = 8.9$  cfs): a basin consisting of a portion of existing Vincent Drive and steep terrain with shallow bedrock, has abundant vegetation and will remain undeveloped. Storm runoff will sheet flow to Vincent Drive to an existing inlet at DP 14. This inlet ties into an 60" existing storm sewer system which will tie into a new storm sewer system on the Phase 1 property. A portion of the existing 60" storm sewer system will be abandoned once the proposed storm sewer system is constructed along the west side of the Phase 1 property and conveys flows to proposed Pond B.

**BASIN OS5** (0.80 AC,  $Q_5 = 3.3$  cfs,  $Q_{100} = 6.1$  cfs): an offsite basin from the Nissan Dealership property to the west consisting of parking lot and landscaping (Refer to the excerpts of the *Final Drainage Report and Plan for I-2 Nissan* dated February 2003 in Appendix B). This area flows into an inlet on the Nissan Dealership which ties into an existing 60" storm sewer which runs across Vincent Drive and into the Crest at Woodmen property. The flows will combine with basin OS4 flows at inlet along Vincent Drive at DP 14. This inlet ties into an 60" existing storm sewer system which will tie into a new storm sewer system on the Phase 1 property. A portion of the existing 60" storm sewer system will be abandoned once the proposed storm sewer system is constructed along the west side of the Phase 1 property and conveys flows to proposed Pond B.

#### D. Detention and Water Quality

There are two ponds on the proposed site: Pond A, located at the southeast corner of the site and Pond B, located at the southwest corner of the site. The proposed basins delineated with the letter A are tributary to Pond A while the basins delineated with the letter B are tributary to Pond B. Pond A will be sized to overdetain and allow Pond B to release at a higher than existing flow rates. The total release from the site will be at or below existing values.



Per section 6.4.2 of the DCM the redevelopment of sites larger than 1 acre may require on-site detention to be provided if the downstream drainage system is shown to be inadequate to convey storm runoff for the entire site. The DBPS takes into account that the site is in a developed condition and has sized the downstream infrastructure as such. With the redevelopment of the site EURV will be provided for the full redeveloped site. This will reduce the higher probability storm runoff from the site which will improve the conditions on the downstream infrastructure and will fulfill the requirement of providing water quality for all redevelopment disturbing 1 acre or more. Historically basins OS3, OS4, and OSE drain through the site undetained. This developed flow rate has been accounted for in the allowable release from the site. The proposed detention ponds are sized such that the redeveloped release from the site will be at or below the existing rate. SWMM models for both the existing and proposed conditions have been prepared to show that this accomplished utilizing the proposed ponds.

In the existing conditions Basin OSE outfalls into the site through an existing 48" storm sewer. The pipe outfalls into an existing water quality pond. The pond at best has been sized for small portions of Woodmen Road as part of the widening project from 2009. This pond does not provide water quality for the entire tributary basin. The proposed Pond A has been sized to provide water quality for the entire Basin OS-E. This is a major improvement from the existing conditions.

In the existing conditions Basins OS-3 and OS-4 flow through the site without water quality being provided for them. The proposed Pond B has been sized to provide water quality for both basins. This is a major improvement from the existing conditions.

## **Pond A**

This pond has approximately 49.80 acres of on-site basins tributary to it (Basins A1-A22). The pond is private and will provide full spectrum, EURV, detention for the proposed development. This volume was added to the required WQCV for the offsite basin to obtain a total first stage volume of 5.74 ac-ft. This first stage was designed to drain in 72 hours. A check was done utilizing SWMM to ensure that the total WQCV in Pond A does not drain in less than 40 hours. A check was also done to ensure that the pond releases within 72 hours. The latest Urban Drainage UD-Detention spreadsheets were not utilized in these calculations due to the fact that Pond A overdetains and Pond B underdetains. All EURV and WQCV volume calculations were completed using the equations provided in the DCM. The sizing of the EURV holes was done on a preliminary level using the UD-Detention spreadsheet (with some tweaking to obtain the correct volumes), but was then checked and finalized using EPA SWMM. The orifice sizing was completed in SWMM using a pond node that was given an initial volume equal to either the EURV + WQCV for the offsite basin or the total WQCV for the total tributary area and in both cases no inflow (it assumes the storm has completed). It was then allowed to be routed through the orifices and the depth of the pond was checked at either 40 (WQCV) or 72 (EURV) hours depending on the scenario to verify the holes are correctly sized. Assumptions made in the SWMM model are as follows:

- Kinematic Wave Method
- Horton's Infiltration Method
- Manning's n for impervious areas – 0.011

- Manning's n for pervious areas – 0.024
- Depression storage for impervious areas – 0.1”
- Depression storage for pervious areas – 0.35”

These results are all contained within Appendix C.

As was mentioned previously Pond A will overdetain to allow Pond B to discharge at a higher rate. The SWMM model prepared generalizes the basins identified on the Proposed Drainage Map into single basins for onsite and offsite, for Pond A the basins are Basin A and OS-East. A predevelopment model was also prepared for the basin to identify what the release from the site would have been prior to any development on site. Both offsite basins were maintained as developed in this model since detention is not provided for them. They will be allowed to directly pass through the ponds. Discussion on total volume and release will be provided after Pond B.

### **Pond B**

This pond has approximately 31.7 acres of on-site basins tributary to it (Basins B1-B12). The pond is private and will provide full spectrum, EURV, detention for the proposed development. In addition, the small offsite basins OS-4 and OS-5 are tributary to this pond. The orifices for the first stage were sized in the same manner that was discussed with Pond A.

As was previously mentioned Pond B will release at a rate higher than historic in an effort to shrink its footprint and create a useable area in this portion of the site. To compensate for that Pond A will overdetain. No detention has been planned for the offsite runoff coming through the site. It will be allowed to pass through the pond.

### **Detention Sizing**

To ensure that detention is being adequately provided for the site a predevelopment SWMM model was prepared for the entire 81.4 acres of onsite basins. The offsite basins were left as a developed condition as no detention will be provided for them. The historic model was run for both the 5-year and the 100-year events. There are two historic outfalls from the site, the east and the west. The east outfall has historic rates of 141.83 cfs and 279.90 cfs in the minor and major storms respectively. The west outfall has historic rates of 10.40 cfs and 27.14 cfs in the minor and major storms respectively. The total release from both outfalls in the historic condition is 152.23 cfs and 307.04 cfs in the minor and major storms respectively.

Pond A was sized to have a release of 107.8 cfs and 219.8 cfs in the minor and major events respectively. Pond B was sized to have a release of 8.9 cfs and 79.8 cfs in the minor and major events respectively. This gives a total release of 109.0 cfs in the minor storm, which is less than the historic rate and 299.7 cfs in the major storm which is also less than the historic rate. These flow rates are derived from the Historic SWMM model for the area prior to the existing development. This includes Basin A, Basin B, and the offsite tributary area. The required volumes for the ponds are 7.36 ac-ft in Pond A and 3.10 ac-ft in Pond B. The ponds will have the required freeboard per the DCM. At the time of final design, any variances will be requested with the final drainage report.

It should be noted that in its current condition there is no detention provided for the site and that runoff release from the site will significantly exceed the historic rates designed to. The improvements provided with this development will reduce direct runoff into Cottonwood Creek and will not have negative effects on the channel system.

## **VI. DRAINAGE AND BRIDGE FEES**

The project is located within the Cottonwood Creek Drainage Basin. This site was previously platted; therefore no drainage and bridge fees are due at this time.

## **VII. CONCLUSIONS**

This report for The Crest at Woodmen has been prepared using the criteria and methods as described in the City of Colorado Springs Drainage Criteria Manual Volumes 1 & 2. The proposed ponds will adequately provide water quality for all tributary areas. They will also provide full spectrum detention for the onsite areas and ensure that the 100-year discharge from the site does not exceed the pre developed conditions in accordance with the DCM. The downstream facilities within Cottonwood Creek are adequate to protect the runoff proposed from the site. The site runoff will not adversely affect the downstream and surrounding developments.

## **VIII. REFERENCES**

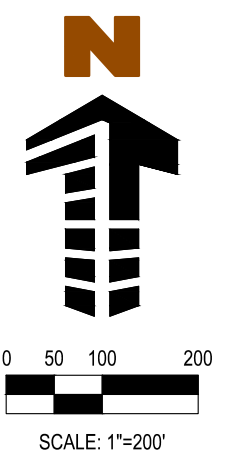
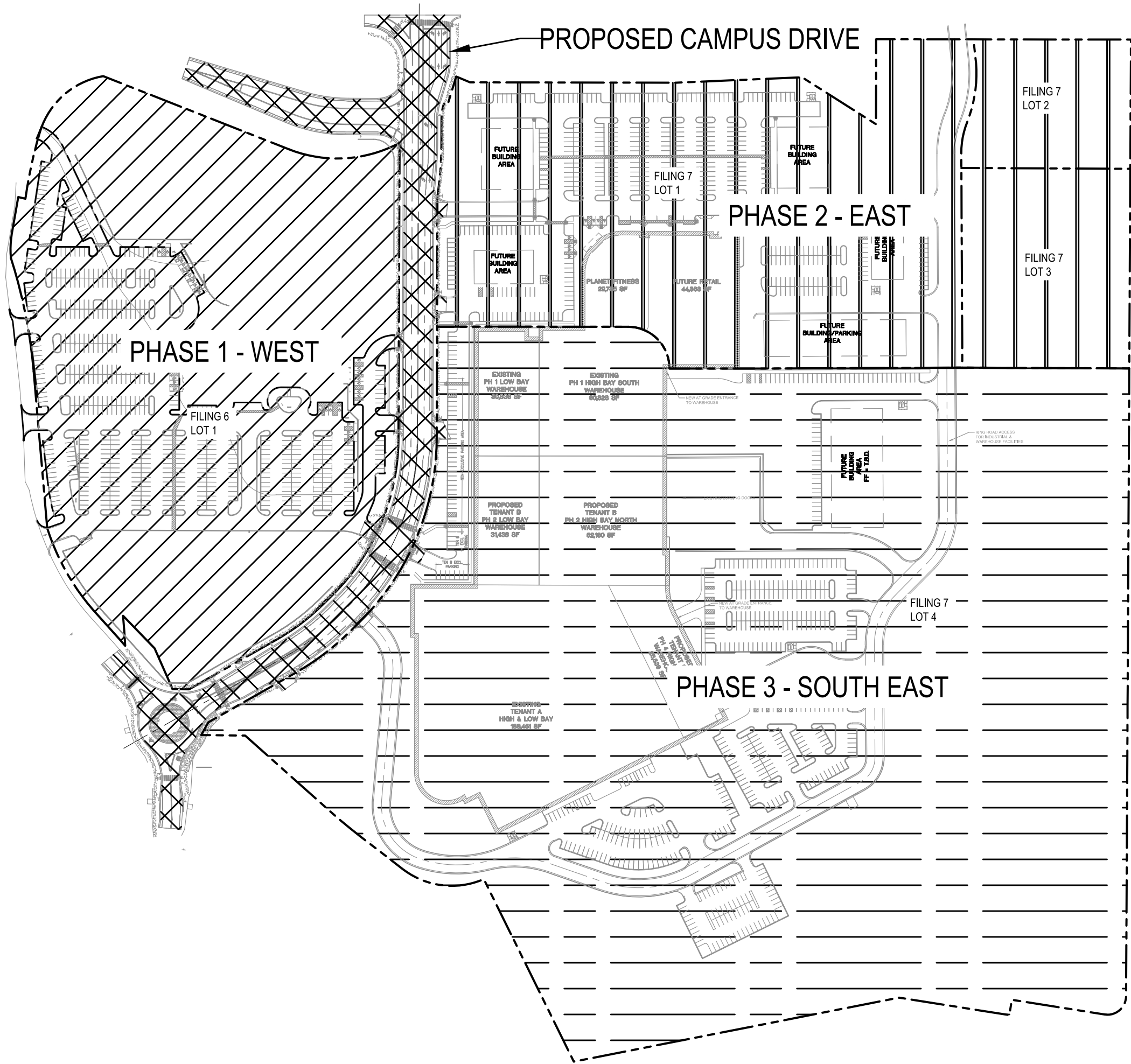
1. *Drainage Criteria Manual Volumes 1 & 2*, City of Colorado Springs, dated May 2014.
2. *Urban Storm Drainage Criteria Manual*, Urban Drainage and Flood Control District, latest revision.
3. Flood Insurance Rate Map (FIRM), El Paso County, Colorado and Incorporated Areas. Map Number 08041C0516F, March 17, 1997 (Federal Emergency Management Agency)
4. Soil Survey of El Paso County, Colorado, Natural Resource Conservation Service, Sept 22, 2015
5. "Cottonwood Creek Drainage Basin Planning Study (DBPS)", June 9, 1994, URS Consultants.
6. "Cottonwood Creek Drainage Basin Planning Study (DBPS)", June 2000, Ayres Associates.
7. "Looart Master Drainage Report and Looart Subdivision No. 2 Drainage Report", April 1978, R. Keith Hook & Associates, Inc.
8. "Looart Subdivision No. 5 Drainage Plan and Report", April 1985, R. Keith Hook & Associates, Inc.
9. "Final Drainage Report and Plan for 1-25 Nissan Pre-Owned Car Dealership American Furniture at Woodman Rd. Fil. No. 1", February 2003, Leigh & Whitehead Associates, Inc.

10. "Woodmen Road Corridor Improvement Project – Phase 1: Campus Drive to Stinson Road Drainage Report -100%", February 17, 2009, URS.
11. "Master Development Drainage Plan for The Crest At Woodmen", April, 2018, Galloway & Company, Inc.
12. "Preliminary/Final Drainage Report for the Crest at Woodmen Campus Drive – Looart Subdivision Filing 6", May 2018, Galloway & Company, Inc.




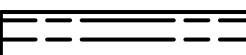
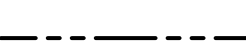
**Appendix A**  
**Figure and Exhibits**

# VICINITY MAP

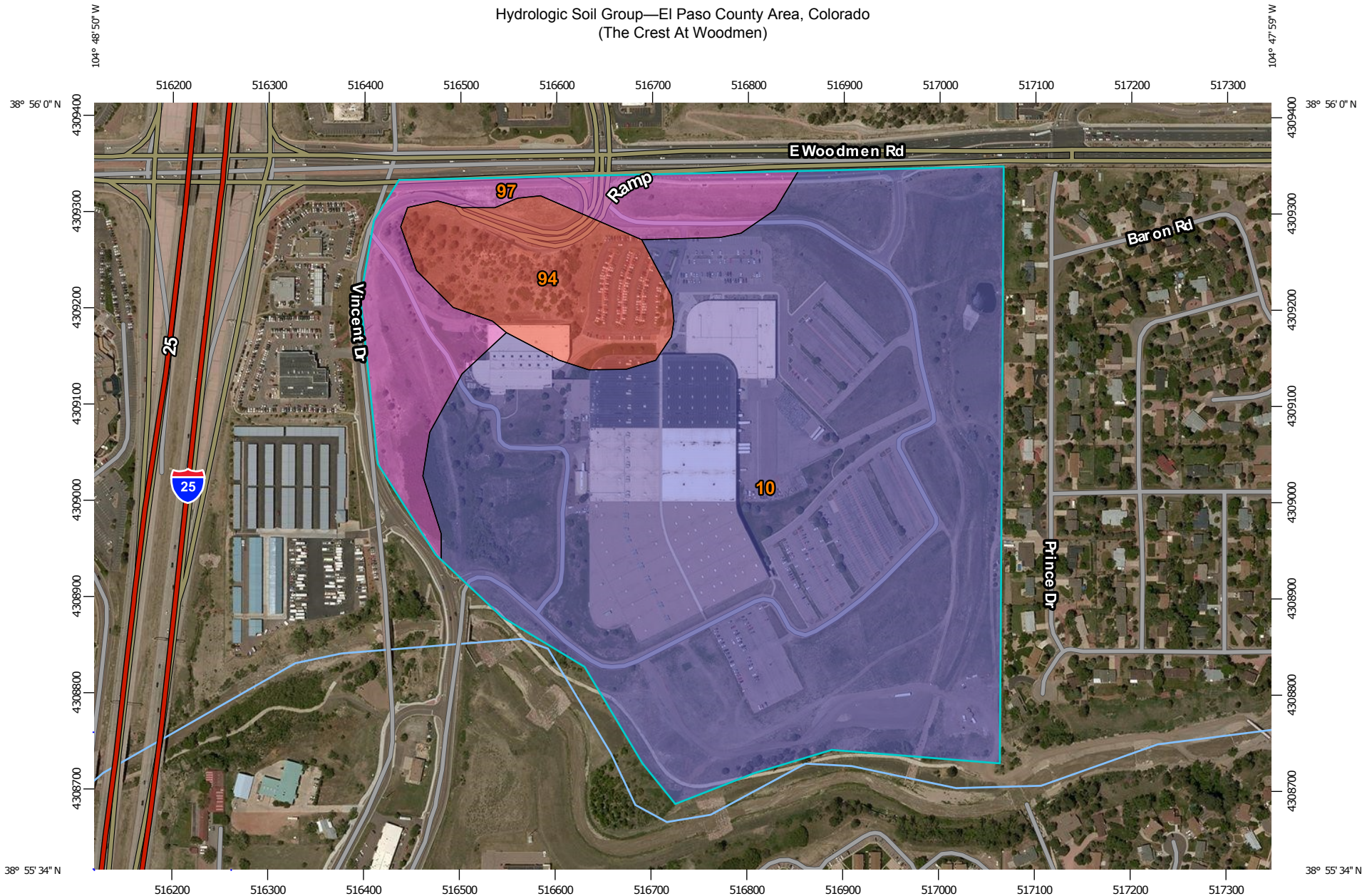




**LOCATION MAP LEGEND**

-  PROPOSED CAMPUS DRIVE
-  PHASE 1 WEST
-  PHASE 2 EAST
-  PHASE 3 SOUTH EAST
-  PROPERTY BOUNDARY

Hydrologic Soil Group—El Paso County Area, Colorado  
(The Crest At Woodmen)



Map Scale: 1:5,620 if printed on A landscape (11" x 8.5") sheet.

0 50 100 200 300 Meters

0 250 500 1000 1500 Feet

Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 13N WGS84






Hydrologic Soil Group—El Paso County Area, Colorado  
(The Crest At Woodmen)

### MAP LEGEND

**Area of Interest (AOI)**









 Area of Interest (AOI)

**Soils**

**Soil Rating Polygons**





-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Lines**

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available

**Soil Rating Points**






-  A
-  A/D
-  B
-  B/D

-  C
-  C/D
-  D
-  Not rated or not available


**Water Features**

 Streams and Canals

**Transportation**

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

**Background**

 Aerial Photography

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
Web Soil Survey URL: <http://websoilsurvey.nrcs.usda.gov>  
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado  
Survey Area Data: Version 13, Sep 22, 2015

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 3, 2014—Jun 17, 2014

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

Hydrologic Soil Group— Summary by Map Unit — El Paso County Area, Colorado (CO625)				
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
10	Blendon sandy loam, 0 to 3 percent slopes	B	70.5	78.9%
94	Travessilla-Rock outcrop complex, 8 to 90 percent slopes	D	8.6	9.7%
97	Truckton sandy loam, 3 to 9 percent slopes	A	10.2	11.4%
<b>Totals for Area of Interest</b>			<b>89.4</b>	<b>100.0%</b>

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## Rating Options

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff:* None Specified

*Tie-break Rule:* Higher

**NOTES TO USERS**

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **Floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be used in conjunction with the FIRM for purposes of construction and/or floodplain management.

**Coastal Base Flood Elevations** shown on this map apply only to landward of 0' North American Vertical Datum of 1988 (NAVD88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations tables in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD83, GRS80 spheroid. Elevations in datum, and the projection or UTM zone codes are provided in the production of FIRMs for adjacent jurisdictions may result in slight positional differences on map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the **North American Vertical Datum of 1988 (NAVD88)**. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov/> or contact the National Geodetic Survey at the following address:

NGS Information Services  
NOAA NNGS12  
National Geodetic Survey  
SSMC-3, #9002  
1315 East-West Highway  
Silver Spring, MD 20910-3282

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at <http://www.ngs.noaa.gov/>.

**Base Map** information shown on this FIRM was provided in digital format by El Paso County, Colorado Springs Utilities, City of Fountain, Bureau of Land Management, National Oceanic and Atmospheric Administration, United States Geological Survey, and Anderson Consulting Engineers, Inc. These data are current as of 2004.

This map reflects more detailed and up-to-date stream channel configurations and floodplain delineations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map. The profile baselines depicted on this map represent the hydraulic modeling baselines that match the flood profiles and Floodway Data Tables if applicable, in the FIS report. As a result, the profile baselines may deviate significantly from the new base map channel representation and may appear outside of the floodplain.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact **FEMA Map Service Center (MSC)** via the FEMA Map Information eXchange (FMIX) 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The MSC may also be reached by Fax at 1-800-336-9620 and its website at <http://www.msc.fema.gov/>.

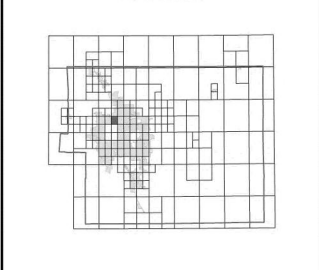
If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/>.

**El Paso County Vertical Datum Offset Table**

Flooding Source	Vertical Datum Offset (ft)

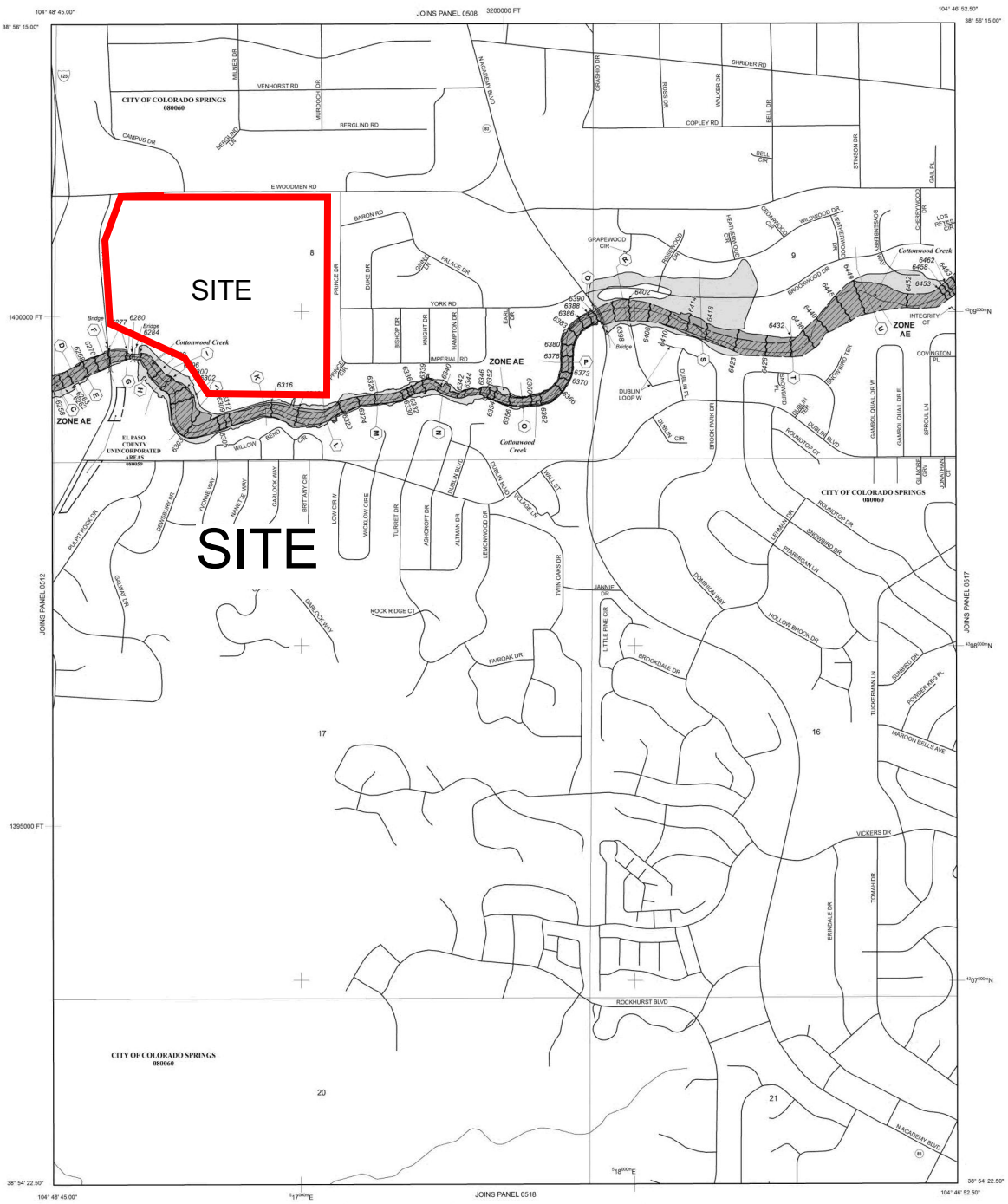
REFER TO SECTION 3.3 OF THE EL PASO COUNTY FLOOD INSURANCE STUDY FOR STREAM-BY-STREAM VERTICAL DATUM CONVERSION INFORMATION

**Panel Location Map**



This Digital Flood Insurance Rate Map (DFIRM) was produced through a Cooperating Technical Partner (CTP) agreement between the State of Colorado Water Conservation Board (CWCB) and the Federal Emergency Management Agency (FEMA).

Additional Flood Hazard information and resources are available from local communities and the Colorado Water Conservation Board.



**LEGEND**

**SPECIAL FLOOD HAZARD AREAS (SFHAS) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD**

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zone A, AE, AH, AO, AV, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

**ZONE A:** No Base Flood Elevations determined.  
**ZONE AE:** Base Flood Elevations determined.  
**ZONE AH:** Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined.  
**ZONE AO:** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.  
**ZONE AR:** Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently abandoned. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.  
**ZONE AR9:** Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations determined.  
**ZONE V:** Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.  
**ZONE VE:** Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

**FLOODWAY AREAS IN ZONE AE**

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachments or use that would increase the 1% annual chance flood up to current velocities. Substantial increases in flood heights.

**OTHER FLOOD AREAS**

**ZONE X:** Areas of 0.2% annual chance flood; areas of 1% annual chance flood with an average flood depth of 1 foot or less; drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.  
**OTHER AREAS:**  
**ZONE X:** Areas determined to be outside the 0.2% annual chance floodplain.  
**ZONE D:** Areas in which flood hazards are undetermined, but possible.  
**COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS**  
**OTHERWISE PROTECTED AREAS (OPAs)**

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

- Floodplain boundary
- Floodway boundary
- Zone D boundary
- CBRS and OPA boundary

Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations; flood depths or flood velocities.  
 Base Flood Elevation line and value; elevation in feet\*  
 Base Flood Elevation value where uniform within zone; elevation in feet\*  
 \* Referenced to the North American Vertical Datum of 1988 (NAVD 88)

—○—○—○— Cross section line  
 —(E 887)—(E 887)—(E 887)— Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)  
 1000-meter Universal Transverse Mercator grid ticks, zone 13  
 5000-foot grid ticks: Colorado State Plane coordinate system, central zone one (PSPROJ 005), Lambert Conformal Conic Projection  
 Bench mark (see explanation in Notes to Users section of this FIRM panel)  
 M 1.5 River Mile

**MAP REPOSITORIES**  
 Refer to Map Repositories list on Map Index  
**EFFECTIVE DATE OF COUNTRYWIDE FLOOD INSURANCE RATE MAP**  
 MARCH 17, 1997  
**EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL**  
 AUGUST 21, 1999  
**DECEMBER 7, 2018** - to update corporate limits, to change Base Flood Elevations and Special Flood Hazard Areas, to update map format, to add water feature names, and to incorporate previously issued Letters of Map Revision.  
 For community map revision history prior to countywide mapping, refer to the Community Map History Tables located in the Flood Insurance Study report for this jurisdiction.  
 To determine if flood insurance is available in this community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6633.

**MAP SCALE 1" = 500'**

250 0 250 500 1000  
 FEET  
 150 0 150 300  
 METERS

**NFIP PANEL 0516G**

**FIRM FLOOD INSURANCE RATE MAP EL PASO COUNTY, COLORADO AND INCORPORATED AREAS**

**PANEL 516 OF 1300**  
 (SEE MAP INDEX FOR FIRM PANEL LAYOUT)

**CONTAINS:**

COMMUNITY	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS CITY OF	8000	001	0
EL PASO COUNTY	9000	001	0

Notice to User: The Map Number shown in brackets should be used when citing map titles. The Community Number shown above should be used on insurance applications for the subject community.

**MAP NUMBER 08041C0516G**

**MAP REVISED DECEMBER 7, 2018**

Federal Emergency Management Agency

NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 13 SOUTH, RANGE 66 WEST.

## **Appendix B**

### **Previous Drainage Report Excerpts**

- 1) Cottonwood Creek DBPS**
- 2) Woodmen Rd**
- 3) Nissan/American Furniture**

LIBRARY COPY  
DO NOT REMOVE

**URS**  
**CONSULTANTS**  
**MAKING**  
**TECHNOLOGY**  
**WORK™**



**Cottonwood Creek**  
**Drainage Basin Planning Study**

City of Colorado Springs and El Paso County

**JUNE 9, 1994**

# CITY ENGR. — CHECK OUT SET #4



APPROXIMATE LIMITS OF AREA BOUNDING BY AND TERTIARY TO MAJOR DEVELOPMENT DRAINAGE PLAN FOR PASSAGE AT BRIARGATE. SEE THAT PLAN FOR ALTERNATIVE DETENTION POND AND MAJOR FACILITIES PRELIMINARY DESIGN.

### RECOMMENDED IMPROVEMENTS FOR DRAINAGE REACHES IN EL PASO COUNTY OUTSIDE (UPSTREAM) OF THE DETAILED AERIAL TOPOGRAPHIC STUDY MAPPING.

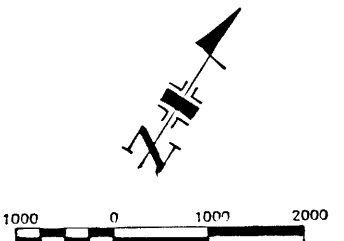
REACH	REC-1 FLOW w/det. (CFS)	CHANNEL LENGTH (FT)	EXISTING IMPROVEMENT	TOTAL		RECOMMENDED IMPROVEMENT
				WIDTH (FT)	DEPTH (FT)	
7 TO DESIGN POINT 8	2,332	3,000	NATURAL	80	4.5	NATURAL BOTTOM WITH GRAVEL/SAND DAMS & BRIDGE CONTROL, DETER 12 (SHRIMP)
8 TO DESIGN POINT 7	1,715	3,500	NATURAL	80	5.0	NATURAL BOTTOM WITH GRAVEL/SAND DAMS & BRIDGE CONTROL, DETER 12 (SHRIMP)
7 TO DESIGN POINT 6	854	3,500	NATURAL	50	4.5	NATURAL BOTTOM WITH GRAVEL/SAND DAMS & BRIDGE CONTROL, DETER 12 (SHRIMP)
6 TO DESIGN POINT 5	673	3,000	NATURAL	50	4.0	NATURAL BOTTOM WITH GRAVEL/SAND DAMS & BRIDGE CONTROL, DETER 12 (SHRIMP)
5 TO DESIGN POINT 4	870	3,000	VEG. LINING	50	4.0	GRADE CONTROL, 111 (SHRIMP)
4 TO DESIGN POINT 3	467	3,500	VEG. LINING	20	4.0	GRADE CONTROL, 111 (SHRIMP)
3 TO DESIGN POINT 2	335	3,500	VEG. LINING	20	4.5	NATURAL BOTTOM WITH GRAVEL/SAND DAMS & BRIDGE CONTROL, DETER 12 (SHRIMP)
2 TO DESIGN POINT 1	114	2,300	NATURAL	20	3.0	NATURAL BOTTOM WITH GRAVEL/SAND DAMS & BRIDGE CONTROL, DETER 12 (SHRIMP)
C14 TO DESIGN POINT 9A	577	8,800	NATURAL	48"	RCP	STORM DRAIN
9A TO DESIGN POINT 9B	255	2,500	NATURAL	48"	RCP	STORM DRAIN
9B TO DESIGN POINT 8	592	4,800	NATURAL	48"	RCP	NATURAL BOTTOM WITH GRAVEL/SAND DAMS & BRIDGE CONTROL, DETER 12 (SHRIMP)
8 TO DESIGN POINT 7F	594	4,000	NATURAL	60"	RCP	NATURAL BOTTOM WITH BRUSH MATS/ROCKDAMS DAMS & BRIDGE CONTROL, DETER 12 (SHRIMP)
7F TO DESIGN POINT 7E	973	3,000	NATURAL	60"	RCP	NATURAL BOTTOM WITH GRAVEL/SAND DAMS & BRIDGE CONTROL, DETER 12 (SHRIMP)
7E TO DESIGN POINT 7D	330	4,100	NATURAL	60"	RCP	STORM DRAIN
7D TO DESIGN POINT 7C	552	4,000	NATURAL	60"	RCP	NATURAL BOTTOM WITH GRAVEL/SAND DAMS & BRIDGE CONTROL, DETER 12 (SHRIMP)
7C TO DESIGN POINT 7B	179	3,000	NATURAL	48"	RCP	STORM DRAIN
7B TO DESIGN POINT 7A	412	3,000	NATURAL	48"	RCP	NATURAL BOTTOM WITH GRAVEL/SAND DAMS & BRIDGE CONTROL, DETER 12 (SHRIMP)
7A TO DESIGN POINT 5	138	3,900	NATURAL	20	3.0	NATURAL BOTTOM WITH GRAVEL/SAND DAMS & BRIDGE CONTROL, DETER 12 (SHRIMP)

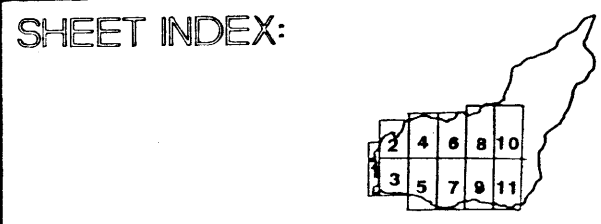
LOCATION	REC-1 FLOW w/det. (CFS)	BRIDGE LENGTH (FT)	EXISTING IMPROVEMENT	TOTAL		RECOMMENDED IMPROVEMENT
				WIDTH (FT)	DEPTH (FT)	
BRIARGATE PKWY (DP 8E)	861	180	N/A	12'	9"	12" x 4' CONCRETE PIPE CULVERT
RESEARCH PKWY (DP 5)	673	180	N/A	10'	8"	12" x 4' CONCRETE PIPE CULVERT
BRIARGATE PKWY (DP 5)	870	180	N/A	12'	9"	12" x 4' CONCRETE PIPE CULVERT
TOBIAS ROAD (LANE DP 1)	60	60	HP - 5' x 48"	12'	9"	12" x 4' CONCRETE PIPE CULVERT
HUNTERS ROAD (DP 3)	335	60	CRP - 36" 2872' RCP	N/A	N/A	1.5' x 12' REINFORCED CONCRETE PIPE
HUNTERS ROAD (DP 5)	235	60	CRP - 48" 2872' RCP	N/A	N/A	1.5' x 12' REINFORCED CONCRETE PIPE
HUNTERS ROAD (DP 7)	114	70	N/A	48"	RCP	48" REINFORCED CONCRETE PIPE
HUNTERS ROAD (DP 1)	81	60	N/A	42"	RCP	42" REINFORCED CONCRETE PIPE

BASED ON THE REACHES/CULVERTS LISTED ON THIS SHEET, APPROXIMATELY 13.3 ACRES OF ENVIRONMENTALLY CLASSIFIED AREAS WILL BE DISTURBED OR DESTROYED AND REQUIRE MITIGATION.

LOCATION	REC-1 FLOW w/det. (CFS)	EXISTING IMPROVEMENT	PROPOSED IMPROVEMENT
CITY BRIDGES			
RESEARCH PKWY (DP 8E)	1,632	N/A	TRIPLE 18" x 4' CMC
BLAKE FOREST ROAD (DP 7)	854	BRIDGE, 7-45, 8-24, 8-17	REPLACE FOR 3 LANE ARCHITECTURAL, 70' x 110'



**LEGEND:**  
 A1 SUB-BASIN DESIGNATION  
 ▲ DESIGN POINT  
 --- MAJOR BASIN BOUNDARY  
 --- SUB-BASIN BOUNDARY



**MAPPING:**  
 LANDMARK MAPPING

**ENGINEER:**  
 URS CONSULTANTS  
 MAKING TECHNOLOGY WORK  
 1040 SOUTH EIGHTH STREET  
 COLORADO SPRINGS, CO 80906  
 (719)634-6899

**PROJECT:**  
 COTTONWOOD CREEK DRAINAGE BASIN PLANNING STUDY  
 OVERALL BASIN MAP  
 SCALE 1"=1000' CONTOUR INTERVAL=2'  
 FIGURE 2 SHEET OF



# **Phase 1: Campus Drive to Stinson Road Drainage Report – 100%**

February 17, 2009



30 S. Nevada Avenue  
Colorado Springs, CO 80903  
(719) 385-2489





Scenario: Five Year

Table A - Catchment Report

Label	Description	Area (acres)	Inlet C	Local Tc (min)	Local Intensity (in/hr)	Local Rational Flow (cfs)	Carryover CA (acres)	Carryover Tc (min)	Carryover Rational Flow (cfs)	Carryover Additional Flow (cfs)	Total Inlet CA (acres)	Total Inlet Time of Concentration (min)	Total Flow To Inlet (cfs)
13-1	Existing On-Grade Curb Inlet	0.15099	0.90	5.00	5.10	0.70	0.34577	5.00	1.78	0.00	0.48166	5.00	2.48
13-2	On-Grade Curb Inlet	1.58000	0.90	5.00	5.10	7.32	0.00000	0.00	0.00	0.00	1.42200	5.00	7.32
13-3	On-Grade Curb Inlet	3.70000	0.40	11.41	3.90	5.81	0.00000	0.00	0.00	0.00	1.48000	11.41	5.81
38-2	On-Grade Curb Inlet	1.57000	0.90	5.37	5.01	7.14	0.00000	0.00	0.00	0.00	1.41300	5.37	7.14
35-2	Stinson Det Pond Outlet Low Flow	0.00000	0.00	41.99	0.00	0.00	0.00000	0.00	0.00	18.89	0.00000	41.99	18.89
36-2	Stinson Det Pond Outlet High Flow	0.00000	0.00	41.99	0.00	0.00	0.00000	0.00	0.00	0.00	0.00000	41.99	0.00
25-1A	Existing Inlet flow adjusted for time	0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	1.50	0.00000	5.00	1.50
25-2	Existing Inlet flow adjusted for time	0.00000	0.00	23.38	0.00	0.00	0.00000	0.00	0.00	51.00	0.00000	23.38	51.00
DP-7B	Existing 5' Combination Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	5.00	0.00	0.75	0.00000	5.00	0.75
DP-7C	Existing 5' Combination Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	5.00	0.00	0.80	0.00000	5.00	0.80
06-2	On-Grade Curb Inlet	0.07000	0.90	5.00	5.10	0.32	0.00000	5.00	0.00	0.00	0.06300	5.00	0.32
06-3	Special On-Grade Curb Inlet	0.05000	0.90	5.00	5.10	0.23	0.00109	5.00	0.01	0.00	0.04609	5.00	0.24
37-1	On-Grade Curb Inlet	0.50000	0.90	5.00	5.10	2.32	0.00000	5.00	0.00	0.00	0.45000	5.00	2.32
07-1	On-Grade Curb Inlet	1.16276	0.90	5.00	5.10	5.38	0.00000	0.00	0.00	0.00	1.04649	5.00	5.38
08-1	Special On-Grade Curb Inlet	0.06357	0.90	5.00	5.10	0.29	0.00000	0.00	0.00	0.00	0.05721	5.00	0.29
WV-SW	Woodmen Valley Storm System	0.32160	0.50	7.06	4.63	0.75	0.00000	0.00	0.00	0.00	0.16080	7.06	0.75
WV-SE	Woodmen Valley Storm System	5.68283	0.50	18.80	3.11	8.91	0.00000	0.00	0.00	0.00	2.84141	18.80	8.91
WV-N	Woodmen Valley Storm System	3.15561	0.50	13.65	3.61	5.75	0.00000	0.00	0.00	0.00	1.57831	13.65	5.75
09-2	Special On-Grade Inlet	0.21000	0.90	5.00	5.10	0.97	0.00000	0.00	0.00	0.00	0.18900	5.00	0.97
09-3	On-Grade Curb Inlet	0.08000	0.90	5.00	5.10	0.37	0.00000	0.00	0.00	0.00	0.07200	5.00	0.37
10-1	Special On-Grade Curb Inlet	0.04373	0.90	5.00	5.10	0.20	0.00000	5.00	0.00	0.00	0.03936	5.00	0.20
06-4	On-Grade Curb Inlet	0.16389	0.90	5.00	5.10	0.76	0.00000	0.00	0.00	0.00	0.14750	5.00	0.76
DP-6	Existing 5' Combination Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	2.40	0.00000	5.00	2.40
DP-7A	Existing 5' Combination Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	2.30	0.00000	5.00	2.30
HD-E2	Existing grate Inlet	0.00000	0.00	11.92	0.00	0.00	0.00000	0.00	0.00	1.40	0.00000	11.92	1.40
HD-F1	Existing grate Inlet	0.00000	0.00	11.92	0.00	0.00	0.00000	0.00	0.00	1.40	0.00000	11.92	1.40
HD-D1	Existing Roof Drain	0.00000	0.00	8.07	0.00	0.00	0.00000	0.00	0.00	10.00	0.00000	8.07	10.00
HD-C1	Existing Grate Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	2.10	0.00000	5.00	2.10
HD-C2	Existing Grate Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	2.10	0.00000	5.00	2.10
HD-B1	Existing Grate Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	0.50	0.00000	5.00	0.50
WV-2	Existing No. 13 Grate Inlet	0.00000	0.00	13.00	0.00	0.00	0.00000	0.00	0.00	30.10	0.00000	13.00	30.10
WV-1	Existing 10' D-10-R Inlet	0.00000	0.00	11.00	0.00	0.00	0.00000	0.00	0.00	31.00	0.00000	11.00	31.00
21-3	Home Depot Sump Field FES	1.04203	0.40	7.07	4.63	1.94	0.00000	0.00	0.00	0.00	0.41681	7.07	1.94
02-2	Special Flanking Vane Grate Inlet	0.39164	0.90	5.00	5.10	1.81	0.03857	5.00	0.20	0.00	0.39105	5.00	2.01
02-3	Special Sump Vane Grate Inlet	0.00000	0.00	0.00	0.00	0.00	0.06606	0.00	0.34	0.00	0.06606	0.00	0.34

Scenario: Five Year

Table A - Catchment Report

Label	Description	Area (acres)	Inlet C	Local Tc (min)	Local Intensity (in/hr)	Local Rational Flow (cfs)	Carryover CA (acres)	Carryover Tc (min)	Carryover Rational Flow (cfs)	Carryover Additional Flow (cfs)	Total Inlet CA (acres)	Total Inlet Time of Concentration (min)	Total Flow To Inlet (cfs)
05-1	On-Grade Curb Inlet	0.11000	0.90	5.00	5.10	0.51	0.48566	5.00	2.50	0.00	0.58466	5.00	3.01
05-2	On-Grade Curb Inlet	2.05641	0.90	6.80	4.68	8.74	0.00981	6.80	0.05	0.00	1.86058	6.80	8.78
01-3	Flanking Curb Inlet	0.66000	0.90	5.00	5.10	3.06	0.00000	0.00	0.00	0.00	0.59400	5.00	3.06
01-4	Sump Curb Inlet	0.00000	0.00	5.00	0.00	0.00	0.85446	5.00	4.40	0.00	0.85446	5.00	4.40
01-5	Flanking Curb Inlet	2.68000	0.90	6.39	4.77	11.60	0.00000	6.39	0.00	0.00	2.41200	6.39	11.60
01-7	Special On-Grade Curb Inlet	0.18085	0.90	5.00	5.10	0.84	0.02891	5.00	0.15	0.00	0.19168	5.00	0.99
01-8	On-Grade Curb Inlet	1.37769	0.90	5.00	5.10	6.38	0.00000	5.00	0.00	0.00	1.23992	5.00	6.38
HD-G1	Home Depot Detention Pond	0.00000	0.00	16.50	0.00	0.00	0.00000	16.50	0.00	13.92	0.00000	16.50	13.92
03-1	Existing Type C Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	5.90	0.00000	5.00	5.90
02-4	Special Flanking Vane Grate In	0.68000	0.90	5.00	5.10	3.15	0.00000	0.00	0.00	0.00	0.61200	5.00	3.15
01-3a		1.31000	0.40	7.67	4.51	2.38	0.00000	0.00	0.00	0.00	0.52400	7.67	2.38

Table B - Inlet Report

Label	Inlet	Inlet Type	Ground Elevation (ft)	Sump Elevation (ft)	Curb Opening Length (ft)	Clogging Factor (%)	Road Cross Slope (%)	Depressed Gutter?	Gutter Cross Slope (%)	Gutter Width (ft)	Inlet Location	Bypass Target	Longitudinal Slope (%)	Manning's n	Total Flow To Inlet (cfs)	Total Interceptor Flow (cfs)	Total Bypassed Flow (cfs)	Capture Efficiency (%)	Gutter Spread (ft)	Gutter Ditch Depth (ft)	
13-1	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,354.81	6,349.92	18.00			2.00	true												
13-2	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,356.53	6,352.70	12.00		2.00	true	6.25	2.00	On Grade	O-4	2.00	0.013	2.48	2.48	0.00	100.0	7.32	0.23	
13-3	Grate CDOT Type C	Grate Inlet	6,355.55	6,353.20		50.0	2.00	false	2.00	0.00	In Sag	13-1	2.00	0.013	7.32	5.54	1.78	75.7	11.77	0.32	
38-2	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,355.72	6,349.06	12.00		2.00	true	6.25	2.00	On Grade	O-5	2.00	0.013	5.81	5.81	0.00	100.0	25.32	0.51	
35-2	Generic Default 100%	Generic Inlet	6,468.00	6,467.70			2.00	false	2.00	0.00	In Sag				7.14	5.46	1.68	76.5	11.65	0.32	
36-2	Generic Default 100%	Generic Inlet	6,479.61	6,472.00			2.00	false	2.00	0.00	In Sag				18.89	18.89	0.00	100.0	0.00	0.00	
25-1A	Grate CDOT TYPE D	Grate Inlet	6,482.00	6,471.30			2.00	false	2.00	0.00	In Sag				0.00	0.00	0.00	100.0	0.00	0.00	
25-2	Grate Special Type D Grate Inlet	Grate Inlet	6,478.41	6,471.80		50.0	2.00	false	2.00	0.00	In Sag				1.50	1.50	0.00	100.0	10.41	0.21	
DP-7B	Combination Denver No 16 Single	Combination Inlet	6,400.10	6,394.60	3.33	38.0	2.00	true	6.25	2.00	On Grade	DP-7C	0.00	0.013	51.00	51.00	0.00	100.0	43.64	0.87	
DP-7C	Combination Denver No 16 Single	Combination Inlet	6,400.00	6,393.60	3.33	38.0	2.00	false	2.00	0.00	On Grade	HD-G1	0.01	0.013	0.75	0.75	0.00	100.0	23.05	0.55	
06-2	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,396.37	6,379.70	6.00		2.00	true	6.25	2.00	On Grade				0.80	0.78	0.02	97.3	14.54	0.29	
06-3	Curb CDOT Type R	Curb Inlet	6,397.17	6,380.50	5.00		2.00	true	4.16	1.00	On Grade	05-2	1.33	0.013	0.32	0.32	0.00	100.0	2.12	0.13	
37-1	Curb CDOT Type R	Curb Inlet	6,397.64	6,380.83	15.00		2.00	true	4.16	1.00	On Grade	05-2	1.34	0.013	0.24	0.24	0.00	100.0	3.44	0.09	
07-1	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,397.20	6,392.90	20.00		2.00	true	6.25	2.00	On Grade	05-2	1.35	0.013	2.32	2.26	0.05	97.8	8.65	0.19	
08-1	Curb CDOT Type R	Curb Inlet	6,398.84	6,394.00	5.00		2.00	true	4.16	1.00	On Grade	06-2	1.62	0.013	5.38	5.38	0.00	100.0	10.82	0.30	
VV-SW	Generic Default 100%	Generic Inlet	6,358.31	6,354.90			2.00	false	2.00	0.00	In Sag	06-3	1.90	0.013	0.29	0.29	0.01	98.1	3.51	0.09	
VV-SE	Generic Default 100%	Generic Inlet	6,359.09	6,355.00			2.00	false	2.00	0.00	In Sag				0.75	0.75	0.00	100.0	0.00	0.00	
VV-N	Generic Default 100%	Generic Inlet	6,360.84	6,357.60			2.00	false	2.00	0.00	In Sag				8.91	8.91	0.00	100.0	0.00	0.00	
09-2	Curb CDOT Type R	Curb Inlet	6,403.20	6,396.10	15.00		1.28	true	4.16	1.00	On Grade	10-1	2.03	0.013	5.75	5.75	0.00	100.0	0.00	0.00	
09-3	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,402.77	6,396.70	6.00		2.80	true	6.25	2.00	On Grade	37-1	2.80	0.013	0.97	0.97	0.00	100.0	7.40	0.12	
10-1	Curb CDOT Type R	Curb Inlet	6,402.23	6,396.70	15.00		0.38	true	4.16	1.00	On Grade	37-1	1.84	0.013	0.20	0.20	0.00	100.0	1.86	0.12	
06-4	Curb CDOT Type R	Curb Inlet	6,395.15	6,386.20	15.00		0.71	true	4.16	1.00	On Grade	01-8	1.41	0.013	0.76	0.76	0.00	100.0	8.15	0.07	
DP-6	Combination Denver No 16 Single	Combination Inlet	6,402.50	6,398.70	3.33	20.0	2.00	true	6.25	2.00	In Sag				2.40	2.40	0.00	100.0	10.40	0.11	
DP-7A	Combination Denver No 16 Single	Combination Inlet	6,400.50	6,395.50	3.33	38.0	2.00	true	6.25	2.00	On Grade	DP-7B	0.00	0.013	2.30	2.25	0.05	97.9	29.00	0.66	
HD-E2	Grate CDOT Type C	Grate Inlet	6,400.50	6,397.00		50.0	2.00	false	2.00	0.00	In Sag				1.40	1.40	0.00	100.0	9.93	0.20	
HD-F1	Grate CDOT Type C	Grate Inlet	6,400.50	6,397.00		50.0	2.00	false	2.00	0.00	In Sag				1.40	1.40	0.00	100.0	8.41	0.17	
HD-D1	Generic Default 100%	Generic Inlet	6,400.00	6,394.10			2.00	false	2.00	0.00	In Sag				10.00	10.00	0.00	100.0	0.00	0.00	
HD-C1	Grate CDOT Type C	Grate Inlet	6,398.00	6,393.30		50.0	2.00	false	2.00	0.00	In Sag				2.10	2.10	0.00	100.0	12.31	0.25	
HD-C2	Grate CDOT Type C	Grate Inlet	6,397.10	6,393.60		50.0	2.00	false	2.00	0.00	In Sag				2.10	2.10	0.00	100.0	12.31	0.25	
HD-B1	Generic Default 100%	Generic Inlet	6,400.50	6,397.31			2.00	false	2.00	0.00	In Sag				0.50	0.50	0.00	100.0	0.00	0.00	
VV-2	Generic Default 100%	Generic Inlet	6,386.00	6,382.00			2.00	false	2.00	0.00	In Sag				30.10	30.10	0.00	100.0	0.00	0.00	
VV-1	Generic Default 100%	Generic Inlet	6,386.00	6,382.00			2.00	false	2.00	0.00	In Sag				31.00	31.00	0.00	100.0	0.00	0.00	
21-3	Grate CDOT TYPE D	Grate Inlet	6,391.00	6,385.30		50.0	2.00	false	2.00	0.00	In Sag				1.94	1.94	0.00	100.0	11.80	0.23	
02-2	Combination Denver No 16 Double	Combination Inlet	6,367.67	6,363.89	7.08	38.0	2.00	true	6.25	2.00	On Grade	02-3	0.63	0.013	2.01	1.87	0.15	92.7	8.67	0.26	
02-3	Combination Denver No 16 Double	Combination Inlet	6,367.50	6,364.47	7.08	50.0	2.00	false	2.00	0.00	In Sag				0.34	0.34	0.00	100.0	1.94	0.03	
05-1	Combination Denver No 16 Triple	Combination Inlet	6,369.39	6,365.77	10.92	38.0	2.00	true	6.25	2.00	On Grade	02-2	2.00	0.013	3.01	2.81	0.20	93.4	8.01	0.25	
05-2	Combination Denver Special No 16 Triple	Combination Inlet	6,370.67	6,367.10	10.92	38.0	2.00	true	6.25	2.00	On Grade	05-1	2.57	0.013	8.78	6.49	2.29	73.9	12.05	0.33	
01-3	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,368.39	6,364.31	20.00		2.00	true	6.25	2.00	On Grade	01-4	0.30	0.013	3.06	3.06	0.00	100.0	12.14	0.33	
01-4	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,368.33	6,364.36	16.00		2.00	true	6.25	2.00	On Grade				4.40	4.40	0.00	100.0	9.99	0.28	
01-5	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,368.50	6,364.48	10.00		2.00	true	6.25	2.00	On Grade	01-4	0.63	0.013	11.60	7.49	4.11	64.6	17.85	0.44	
01-7	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,372.50	6,367.01	14.00		2.00	true	6.25	2.00	On Grade	01-5	3.02	0.013	0.99	0.99	0.00	100.0	3.90	0.16	
01-8	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,374.09	6,367.83	20.00		2.00	true	6.25	2.00	On Grade	01-7	3.52	0.013	6.38	6.23	0.15	97.7	9.86	0.28	
HD-G1	Generic Default 100%	Generic Inlet	6,379.56	6,372.79			0.00	false	0.00	0.00	In Sag				13.92	13.92	0.00	100.0	0.00	0.00	
03-1	Grate CDOT Type C	Grate Inlet	6,379.55	6,366.00		50.0	2.00	false	2.00	0.00	In Sag				5.90	5.90	0.00	100.0	25.56	0.51	
02-4	Combination Denver No 16 Double	Combination Inlet	6,367.51	6,364.80	7.08	38.0	2.00	true	6.25	2.00	On Grade	02-3	0.10	0.013	3.15	2.96	0.19	93.9	15.35	0.39	
01-3a	Grate CDOT Type C	Grate Inlet	6,367.38	6,363.38		50.0	2.00	false	2.00	0.00	In Sag				2.38	2.38	0.00	100.0	12.97	0.28	

Table C - Pipe Report

Label	Upstream Node	Downstream Node	Section Shape	Section Size	Material	Manning n	Length (ft)	Bend Angle (degrees)	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Upstream Sump Elevation (ft)	Downstream Sump Elevation (ft)	Upstream Crown Elevation (ft)	Downstream Crown Elevation (ft)	Upstream Cover (ft)	Downstream Cover (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Average Velocity (ft/s)	Full Capacity (cfs)	Total System Flow (cfs)
P-13-2	13-2	13-1	Circular	18 inch	Concrete	0.013	46.70	2.74	6,352.70	6,351.40	6,352.70	6,349.92	6,354.20	6,352.90	2.33	1.91	6,353.92	6,352.25	10.24	17.53	10.01
P-13-1	13-1	O-4	Circular	18 inch	Concrete	0.013	175.96	0.00	6,349.92	6,347.69	6,349.92	6,347.69	6,351.42	6,349.19	3.39	0.81	6,351.23	6,348.92	7.63	11.82	11.86
P-13-3	13-3	13-2	Circular	18 inch	Concrete	0.013	27.86	0.00	6,353.20	6,353.00	6,353.20	6,352.70	6,354.70	6,354.50	0.85	2.03	6,354.13	6,354.03	5.37	8.90	5.81
P-38-2	38-2	38-1	Circular	18 inch	Concrete	0.013	19.62	41.22	6,349.06	6,348.79	6,349.06	6,348.79	6,350.56	6,350.29	5.16	4.10	6,349.96	6,349.70	6.76	12.32	5.46
P-38-1	38-1	O-5	Circular	18 inch	Concrete	0.013	120.44	0.00	6,348.79	6,347.29	6,348.79	6,347.29	6,350.29	6,348.79	4.10	2.71	6,349.69	6,348.01	6.51	11.72	5.44
P-35-2	35-2	35-1	Circular	24 inch	Concrete	0.013	133.95	0.00	6,467.70	6,461.80	6,467.70	6,461.80	6,469.70	6,463.80	-1.70	4.20	6,469.26	6,462.68	14.25	47.48	18.89
P-36-2	36-2	36A	Horizontal El	24x38 inch	Concrete	0.013	12.21	41.25	6,472.00	6,471.72	6,472.00	6,471.72	6,474.00	6,473.72	5.61	0.76	6,472.00	6,471.72	0.00	135.71	0.00
P-36A	36A	36-1	Horizontal El	24x38 inch	Concrete	0.013	218.03	0.00	6,471.72	6,468.01	6,471.72	6,467.71	6,473.72	6,470.01	0.76	9.72	6,471.72	6,468.01	0.00	116.90	0.00
P-25-2	25-1A	25-1	Horizontal El	29x45 inch	Concrete	0.013	52.01	0.00	6,471.30	6,471.05	6,471.30	6,471.05	6,473.70	6,473.45	8.30	0.97	6,472.63	6,472.27	6.75	102.17	52.50
P-25-3	25-2	25-1A	Horizontal El	29x45 inch	Concrete	0.013	108.65	0.00	6,471.30	6,471.30	6,471.30	6,471.30	6,474.20	6,473.70	4.21	6.30	6,473.11	6,472.66	6.59	99.97	51.00
P-01-A	28-A	28-2	Circular	48 inch	Concrete	0.013	15.00	55.38	6,353.58	6,353.51	6,353.58	6,353.51	6,357.58	6,357.51	1.14	1.87	6,359.53	6,359.38	11.30	98.12	142.00
P-06-3	06-3	06-3	Circular	36 inch	Concrete	0.013	19.13	13.54	6,380.83	6,380.80	6,380.83	6,380.50	6,383.83	6,383.80	13.81	13.37	6,382.67	6,382.54	4.25	26.41	25.21
P-06-2	06-2	06-1	Circular	36 inch	Concrete	0.013	41.04	1.84	6,380.50	6,379.70	6,380.50	6,379.70	6,383.50	6,383.00	13.67	13.37	6,382.15	6,381.67	9.52	73.62	26.07
P-07-1	07-1	06-2	Circular	18 inch	Concrete	0.013	38.43	91.16	6,392.90	6,391.90	6,392.90	6,379.70	6,394.40	6,393.40	2.80	2.97	6,393.79	6,392.50	8.51	16.94	5.38
P-08-1	08-1	06-3	Circular	18 inch	Concrete	0.013	95.69	91.21	6,394.00	6,392.90	6,394.00	6,380.50	6,395.50	6,394.40	3.34	2.77	6,394.20	6,393.07	2.72	11.26	0.29
P-WV-3	WV-3	WV-4	Circular	42 inch	Concrete	0.013	63.20	0.88	6,376.02	6,372.91	6,376.02	6,372.91	6,379.52	6,376.41	3.98	11.47	6,377.82	6,375.41	16.73	223.17	33.79
P-06-1	06-1	WV-4	Circular	42 inch	Concrete	0.013	95.55	14.85	6,372.91	6,371.37	6,372.91	6,371.37	6,376.41	6,374.87	11.47	2.63	6,375.41	6,374.60	13.25	127.72	63.35
P-28-2	28-1	28-A	Circular	48 inch	Concrete	0.013	84.20	38.83	6,371.37	6,356.00	6,371.37	6,356.00	6,375.37	6,360.00	2.13	1.91	6,374.30	6,360.80	15.28	193.81	93.42
P-28-2	28-1	WV-SE	Circular	24 inch	Concrete	0.013	148.04	2.20	6,356.00	6,353.58	6,356.00	6,353.58	6,360.00	6,357.58	1.91	1.14	6,360.30	6,359.60	7.84	183.65	98.47
P-WV-SE	WV-SE	WV-SW	Circular	24 inch	Concrete	0.013	40.20	13.13	6,355.00	6,354.90	6,355.00	6,354.90	6,357.00	6,356.90	2.09	1.41	6,358.37	6,358.31	2.83	11.28	8.91
P-WV-SW	WV-SW	28-2	Circular	24 inch	Concrete	0.013	8.60	20.28	6,354.90	6,353.51	6,354.90	6,353.51	6,356.90	6,355.51	1.41	3.87	6,359.09	6,359.07	2.98	90.94	9.35
P-WV-N	WV-N	28-1	Circular	24 inch	Concrete	0.013	47.60	47.61	6,357.60	6,356.00	6,357.60	6,356.00	6,359.60	6,358.00	1.24	3.91	6,360.65	6,360.62	1.83	41.47	5.75
P-09-3	09-3	09-2	Circular	18 inch	Concrete	0.013	31.07	46.51	6,395.70	6,395.40	6,395.70	6,395.40	6,398.70	6,397.90	4.57	5.30	6,396.92	6,396.59	2.76	10.32	3.37
P-09-2	09-2	09-1	Circular	18 inch	Concrete	0.013	19.26	57.63	6,396.10	6,395.80	6,396.10	6,395.80	6,397.60	6,397.30	5.60	5.74	6,396.56	6,396.15	4.96	13.11	1.52
P-10-1	10-1	09-2	Circular	18 inch	Concrete	0.013	36.94	87.32	6,396.70	6,396.40	6,396.70	6,396.10	6,398.20	6,397.90	4.03	5.30	6,396.87	6,396.57	2.16	9.47	0.20
P-09-1	09-1	WV-3	Circular	42 inch	Concrete	0.013	178.20	0.09	6,382.34	6,376.02	6,382.34	6,376.02	6,385.84	6,379.52	17.20	3.98	6,382.88	6,377.83	7.47	189.46	3.29
P-06-4	06-4	06-3	Circular	18 inch	Concrete	0.013	233.21	95.09	6,386.20	6,382.00	6,386.20	6,380.50	6,387.70	6,383.50	7.45	13.67	6,386.52	6,382.51	4.25	14.10	0.76
P-37-2	37-2	37-1	Circular	18 inch	Concrete	0.013	185.16	52.50	6,381.46	6,381.13	6,381.46	6,380.83	6,382.96	6,382.63	16.81	15.01	6,385.26	6,382.89	6.70	8.85	23.68
P-DP-5	DP-5	37-2	Circular	30 inch	Concrete	0.013	325.16	115.80	6,395.70	6,384.11	6,395.70	6,381.46	6,395.10	6,386.61	2.30	13.16	6,395.93	6,385.79	4.44	77.43	0.50
P-DP-8	DP-8	37-2	Circular	24 inch	Concrete	0.013	141.95	26.51	6,393.10	6,384.11	6,393.10	6,381.46	6,395.10	6,386.11	5.60	13.66	6,394.81	6,385.00	17.19	56.93	23.18
P-DP-7C	DP-7C	DP-6	Circular	24 inch	Concrete	0.013	60.88	6.10	6,393.90	6,393.60	6,393.90	6,393.10	6,395.90	6,395.60	4.10	5.10	6,395.75	6,395.17	6.04	15.87	18.98
P-DP-7B	DP-7B	DP-7C	Circular	24 inch	Concrete	0.013	141.26	5.41	6,394.60	6,393.90	6,394.60	6,393.90	6,396.60	6,395.90	3.50	4.10	6,395.99	6,395.88	5.11	15.92	8.20
P-DP-6	DP-6	18 inch	Circular	18 inch	Concrete	0.013	87.91	6.48	6,398.70	6,398.00	6,398.70	6,398.00	6,400.20	6,399.50	2.30	2.20	6,399.29	6,398.52	4.44	9.37	2.40
P-DP-7	DP-7	DP-7A	Circular	24 inch	Concrete	0.013	97.44	6.53	6,396.00	6,395.60	6,396.00	6,395.60	6,398.00	6,397.50	3.70	3.00	6,396.80	6,396.51	4.59	16.20	5.20
P-DP-7A	DP-7A	DP-7B	Circular	24 inch	Concrete	0.013	180.27	0.38	6,395.50	6,394.60	6,395.50	6,394.60	6,397.50	6,396.60	3.00	3.50	6,396.47	6,396.00	5.00	15.98	7.45
P-HD-E2	HD-E2	HD-E1	Circular	15 inch	Concrete	0.013	121.84	0.02	6,397.00	6,396.40	6,397.00	6,396.40	6,398.25	6,397.65	2.25	3.15	6,397.48	6,397.13	3.25	4.53	1.40
P-HD-E1	HD-E1	DP-7	Circular	15 inch	Concrete	0.013	82.41	83.53	6,396.40	6,396.00	6,396.40	6,396.00	6,397.65	6,397.25	3.15	4.45	6,397.12	6,396.94	3.87	4.60	2.80
P-HD-F1	HD-F1	HD-E1	Circular	15 inch	Concrete	0.013	15.85	90.11	6,397.00	6,396.90	6,397.00	6,396.90	6,398.25	6,397.65	2.25	2.65	6,397.47	6,397.35	3.56	5.13	1.40
P-HD-D1	HD-D1	DP-7C	Circular	24 inch	Concrete	0.013	38.48	96.66	6,394.10	6,393.90	6,394.10	6,393.90	6,395.90	6,395.90	3.90	4.10	6,396.01	6,395.94	5.45	16.31	10.00
P-HDC2	HD-C2	HD-C1	Circular	15 inch	Concrete	0.013	48.28	0.44	6,393.60	6,393.30	6,393.60	6,393.30	6,394.55	6,394.55	2.25	3.45	6,395.16	6,395.11	1.71	5.09	2.10
P-HD-C1	HD-C1	DP-6	Circular	15 inch	Concrete	0.013	37.98	89.64	6,393.30	6,393.10	6,393.30	6,393.10	6,394.55	6,394.35	3.45	6.35	6,395.07	6,394.91	3.42	4.69	4.20
P-HD-B	HD-B1	DP-5	Circular	12 inch	Concrete	0.013	2.00	89.40	6,397.31	6,397.30	6,397.31	6,395.70	6,398.31	6,398.30	2.19	2.20	6,397.61	6,397.59	2.50	2.52	0.50
P-WV-2	WV-2	WV-4	Circular	24 inch	Concrete	0.013	073.00	93.47	6,382.00	6,371.37	6,382.00	6,371.37	6,384.00	6,373.37	2.00	4.13	6,383.51	6,374.51	9.58	22.52	30.10
P-WV-1	WV-1	WV-3	Circular	24 inch	Concrete	0.013	381.00	48.83	6,382.00	6,376.02	6,382.00	6,376.02	6,384.00	6,378.02	2.00	5.48	6,385.06	6,377.90	9.87	28.34	31.00
P-21-3	21-3	21-2	Circular	30 inch	Concrete	0.013	56.33	15.83	6,385.30	6,384.70	6,385.30	6,384.40	6,387.80	6,387.20	3.20	16.85	6,385.75	6,385.06	4.38	42.33	1.94
P-30	21-2	21-1	Circular	30 inch	Concrete	0.013	12.48	39.73	6,384.40	6,384.17	6,384.40	6,384.17	6,386.90	6,386.67	17.15	17.26	6,384.85	6,384.62	5.30	55.68	1.93
P-31	21-1	09-1	Circular	30 inch	Concrete	0.013	42.14	0.24	6,384.17	6,382.34	6,384.17	6,382.34	6,386.67	6,384.84	17.26	18.20	6,384.82	6,382.88	7.14	85.47	1.92
P-01	28-2	O-1B	Circular	48 inch	Concrete	0.013	145.00	0.00	6,353.51	6,351.73	6,353.51	6,351.73	6,357.51	6,355.73	1.87	-1.73	6,356.11	6,356.50	12.03	159.14	151.12
P-40	01-00	28-A	Circular	48 inch	Concrete	0.013	23.00	31.52	6,353.77	6,353.69	6,353.77	6,353.69	6,357.77	6,357.69	1.47	1.03	6,359.78	6,359.75	3.54	84.71	44.47
P-02-3	02-3	02-2	Circular	18 inch	Concrete	0.013	49.85	0.91	6,364.47	6,364.19	6,364.47	6,363.83	6,365.97	6,365.69	1.53	1.96	6,365.16	6,364.87	4.26	7.87	3.29

Title: Woodmen Road and Academy Blvd Intersection  
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Table C - Pipe Report

Label	Upstream Node	Downstream Node	Section Shape	Section Size	Material	Manning's n	Length (ft)	Bend Angle (degrees)	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Upstream Sump Elevation (ft)	Downstream Sump Elevation (ft)	Upstream Crown Elevation (ft)	Downstream Crown Elevation (ft)	Upstream Cover (ft)	Downstream Cover (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Average Velocity (ft/s)	Full Capacity (cfs)	Total System Flow (cfs)
P-02-2	02-2	02-1	Circular	18 inch	Concrete	0.013	76.19	91.91	6,363.89	6,362.00	6,363.89	6,361.39	6,365.39	6,363.50	2.28	5.32	6,364.76	6,363.48	8.25	15.54	5.11
P-05-2	05-2	05-1	Circular	18 inch	Concrete	0.013	46.06	0.63	6,367.10	6,366.07	6,367.10	6,365.77	6,368.60	6,367.57	2.07	1.82	6,368.09	6,366.78	8.48	15.70	6.49
P-05-1	05-1	02-1	Circular	18 inch	Concrete	0.013	45.63	88.78	6,365.77	6,364.85	6,365.77	6,361.39	6,367.27	6,366.35	2.12	2.47	6,366.93	6,365.72	8.84	14.91	9.03
P-02-1	02-1	01-1	Horizontal El	19x30 inch	Concrete	0.013	14.46	0.13	6,361.87	6,361.77	6,361.77	6,361.39	6,355.20	6,363.47	5.35	6.26	6,363.47	6,363.42	6.65	20.90	13.69
P-01-8	01-8	01-7	Circular	36 inch	Concrete	0.013	32.99	1.48	6,367.83	6,367.31	6,367.83	6,367.01	6,370.83	6,370.31	3.26	2.19	6,369.19	6,368.34	9.43	83.73	17.95
P-HD-G1	HD-G1	01-9	Circular	36 inch	Concrete	0.013	1.00	22.09	6,372.79	6,372.78	6,372.78	6,372.78	6,375.79	6,375.78	3.77	3.85	6,373.98	6,373.97	7.46	66.69	13.92
P-01-9	01-9	01-8	Circular	36 inch	Concrete	0.013	116.21	5.22	6,372.78	6,368.13	6,372.78	6,367.83	6,375.78	6,371.13	3.85	2.96	6,373.97	6,368.78	12.22	133.41	13.92
P-01-7	01-7	01-6	Circular	36 inch	Concrete	0.013	132.55	4.40	6,367.01	6,364.90	6,367.01	6,364.90	6,370.01	6,367.90	2.49	1.71	6,368.39	6,366.64	9.56	84.15	18.58
P-01-6	01-6	01-5	Circular	36 inch	Concrete	0.013	87.48	4.54	6,364.90	6,364.48	6,364.90	6,364.48	6,367.90	6,367.48	1.71	1.02	6,366.64	6,366.62	6.63	46.21	24.45
P-01-5	01-5	01-4	Circular	36 inch	Concrete	0.013	45.78	0.45	6,364.48	6,364.36	6,364.48	6,364.36	6,367.48	6,367.36	1.02	0.97	6,366.56	6,366.41	5.44	34.15	29.52
P-01-4	01-4	01-3	Circular	36 inch	Concrete	0.013	17.68	97.50	6,364.36	6,364.31	6,364.36	6,364.31	6,367.36	6,367.31	0.97	1.08	6,366.36	6,366.15	5.69	35.47	32.27
P-01-3	01-3	01-2	Horizontal El	19x30 inch	Concrete	0.013	120.04	81.59	6,364.31	6,363.94	6,364.31	6,362.78	6,365.91	6,365.54	2.48	3.13	6,365.44	6,365.02	4.72	41.86	35.89
P-01-2	01-2	01-1	Circular	42 inch	Concrete	0.013	148.06	91.93	6,362.78	6,361.67	6,362.78	6,355.20	6,366.28	6,365.17	2.39	4.46	6,364.83	6,363.59	8.60	87.11	35.71
P-03-1	03-1	01-6	Circular	18 inch	Concrete	0.013	26.87	61.98	6,365.00	6,365.85	6,365.00	6,364.90	6,367.50	6,367.35	12.05	2.26	6,366.97	6,366.79	4.88	7.85	5.90
P-02-4	02-4	02-3	Circular	18 inch	Concrete	0.013	4.67	1.51	6,364.80	6,364.77	6,364.80	6,364.47	6,366.30	6,366.27	1.21	1.23	6,365.45	6,365.39	4.35	8.42	2.96
P-36	01-3a	01-3	Circular	24 inch	Concrete	0.013	23.16	0.00	6,364.50	6,364.38	6,363.38	6,364.31	6,366.50	6,366.38	0.88	2.01	6,365.52	6,365.52	3.70	16.28	2.38
P-37	01-1	01-0	Circular	30 inch	Concrete	0.013	85.00	2.21	6,361.67	6,358.81	6,355.20	6,358.00	6,364.17	6,361.31	5.46	1.32	6,363.28	6,359.79	13.38	150.47	44.93
P-39	01-0	01-00	Circular	30 inch	Concrete	0.013	282.00	0.00	6,358.51	6,356.01	6,356.00	6,352.96	6,361.01	6,358.51	1.62	0.73	6,360.12	6,359.24	8.16	77.24	44.86

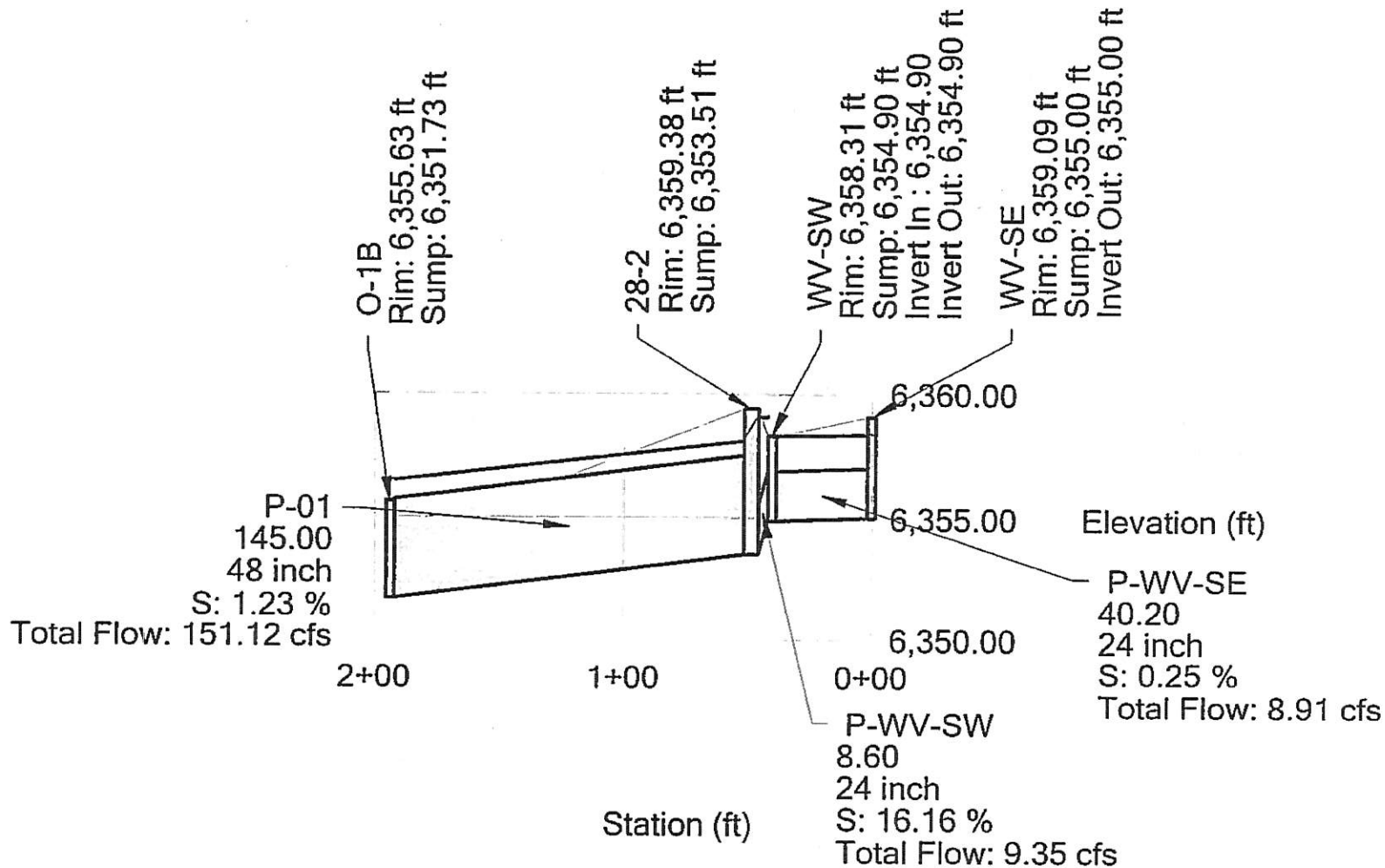
Scenario: Five Year

Table D - Junction Report

Label	Description	Structure Diameter (ft)	Ground Elevation (ft)	Sump Elevation (ft)	Set Rim Equal to Ground Elevation?	Rim Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Total Flow (cfs)
38-1	Proposed Manhole Connection to Exis	6.00	6,354.39	6,348.79	true	6,354.39	6,349.70	6,349.69	5.44
36A		2.00	6,474.48	6,471.72	false	6,474.48	6,471.72	6,471.72	0.00
28-A	Existing Manhole Existing Manhole Existing Junction Existing Wye  Pipe Connection Existing MH           Connection to Existing Home Depot In	6.00	6,358.72	6,353.58	false	6,355.69	6,359.60	6,359.53	142.00
06-1		6.00	6,387.88	6,372.91	true	6,387.88	6,375.41	6,375.41	63.35
28-2		6.00	6,359.38	6,353.51	true	6,359.38	6,359.07	6,358.11	151.12
28-1		7.00	6,361.91	6,356.00	false	6,361.75	6,360.62	6,360.30	98.47
WV-4		4.00	6,377.50	6,371.37	false	6,377.50	6,374.51	6,374.30	93.42
WV-3		6.00	6,383.50	6,376.02	false	6,383.50	6,377.83	6,377.82	33.79
09-1		6.00	6,403.04	6,382.34	true	6,403.04	6,382.88	6,382.88	3.29
DP-7		4.00	6,401.70	6,396.00	false	6,401.70	6,396.83	6,396.80	5.20
DP-8		4.00	6,400.70	6,393.10	false	6,400.70	6,394.91	6,394.81	23.18
HD-E1		1.25	6,400.80	6,396.40	false	6,400.80	6,397.13	6,397.12	2.80
37-2		6.00	6,399.77	6,381.46	true	6,399.77	6,385.59	6,385.26	23.68
DP-5		4.00	6,400.50	6,395.70	false	6,400.50	6,395.94	6,395.93	0.50
21-1		5.00	6,403.93	6,384.17	false	6,403.93	6,384.62	6,384.62	1.92
21-2		5.00	6,404.05	6,384.40	true	6,404.05	6,384.85	6,384.85	1.93
01-00		10.00	6,359.24	6,352.96	true	6,359.24	6,359.25	6,359.24	44.47
01-0		10.00	6,362.63	6,358.00	true	6,362.63	6,360.13	6,360.12	44.86
01-1		7.00	6,369.63	6,355.20	true	6,369.63	6,363.42	6,363.28	44.93
01-2		6.00	6,368.67	6,362.78	true	6,368.67	6,365.02	6,364.63	35.71
01-6		7.00	6,369.61	6,364.90	true	6,369.61	6,366.64	6,366.64	24.45
01-9		5.00	6,379.63	6,372.78	true	6,379.63	6,373.97	6,373.97	13.92
02-1	4.00	6,368.82	6,361.39	true	6,368.82	6,363.48	6,363.47	13.69	

# Profile: Prince Inlets

## Scenario: Five Year



Scenario: One Hundred Year

Table A - Catchment Report

Label	Description	Area (acres)	Inlet C	Local Tc (min)	Local Intensity (in/hr)	Local Rational Flow (cfs)	Carryover CA (acres)	Carryover Tc (min)	Carryover Rational Flow (cfs)	Carryover Additional Flow (cfs)	Total Inlet CA (acres)	Total Inlet Time of Concentration (min)	Total Flow To Inlet (cfs)
13-1	Existing On-Grade Curb Inlet	0.15000	0.95	5.00	9.09	1.31	0.64944	5.00	5.95	0.00	0.79194	5.00	7.25
13-2	On-Grade Curb Inlet	1.58000	0.95	5.00	9.09	13.75	0.00000	0.00	0.00	0.00	1.50100	5.00	13.75
13-3		3.70000	0.50	11.41	6.93	12.93	0.00000	0.00	0.00	0.00	1.85000	11.41	12.93
38-2	On-Grade Curb Inlet	1.57000	0.95	5.37	8.92	13.41	0.00000	0.00	0.00	0.00	1.49150	5.37	13.41
35-2	Stinson Det Pond Outlet Low Flow	0.00000	0.00	41.99	0.00	0.00	0.00000	0.00	0.00	37.82	0.00000	41.99	37.82
36-2	Stinson Det Pond Outlet High Flow	0.00000	0.00	41.99	0.00	0.00	0.00000	0.00	0.00	59.08	0.00000	41.99	59.08
25-1A	Existing Inlet flow adjusted for time	0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	9.60	0.00000	5.00	9.60
25-2		0.00000	0.00	23.83	0.00	0.00	0.00000	0.00	0.00	200.70	0.00000	23.83	200.70
DP-7B	Existing 5' Combination Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	5.00	0.00	1.52	0.00000	5.00	1.52
DP-7C	Existing 5' Combination Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	5.00	0.00	1.60	0.00000	5.00	1.60
06-2	On-Grade Curb Inlet	0.07000	0.95	5.00	9.09	0.61	0.07276	5.00	0.67	0.00	0.13926	5.00	1.28
06-3	Special On-Grade Curb Inlet	0.05000	0.95	5.00	9.09	0.44	0.01064	5.00	0.10	0.00	0.05814	5.00	0.53
37-1	On-Grade Curb Inlet	0.50000	0.95	5.00	9.09	4.35	0.00007	5.00	0.00	0.00	0.47507	5.00	4.35
07-1	On-Grade Curb Inlet	1.16276	0.95	5.00	9.09	10.12	0.00000	0.00	0.00	0.00	1.10463	5.00	10.12
08-1	Special On-Grade Curb Inlet	0.06357	0.95	5.00	9.09	0.55	0.00000	0.00	0.00	0.00	0.06039	5.00	0.55
WV-SW	Woodmen Valley Storm System	0.32160	0.60	7.06	8.24	1.60	0.00000	0.00	0.00	0.00	0.19296	7.06	1.60
WV-SE	Woodmen Valley Storm System	5.68283	0.60	18.80	5.53	19.02	0.00000	0.00	0.00	0.00	3.40970	18.80	19.02
WV-N	Woodmen Valley Storm System	3.15661	0.60	13.65	6.43	12.27	0.00000	0.00	0.00	0.00	1.89397	13.65	12.27
09-2	Special On-Grade Inlet	0.21000	0.95	5.00	9.09	1.83	0.00000	0.00	0.00	0.00	0.19950	5.00	1.83
09-3	On-Grade Curb Inlet	0.08000	0.95	5.00	9.09	0.70	0.00000	0.00	0.00	0.00	0.07600	5.00	0.70
10-1	Special On-Grade Curb Inlet	0.04373	0.95	5.00	9.09	0.38	0.01130	5.00	0.10	0.00	0.05285	5.00	0.48
06-4	On-Grade Curb Inlet	0.16389	0.95	5.00	9.09	1.43	0.00000	0.00	0.00	0.00	0.15569	5.00	1.43
DP-6	Existing 5' Combination Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	3.60	0.00000	5.00	3.60
DP-7A	Existing 5' Combination Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	4.40	0.00000	5.00	4.40
HD-E2	Existing grate inlet	0.00000	0.00	11.92	0.00	0.00	0.00000	0.00	0.00	2.50	0.00000	11.92	2.50
HD-F1	Existing grate inlet	0.00000	0.00	11.92	0.00	0.00	0.00000	0.00	0.00	2.50	0.00000	11.92	2.50
HD-D1	Existing Roof Drain	0.00000	0.00	8.07	0.00	0.00	0.00000	0.00	0.00	16.80	0.00000	8.07	16.80
HD-C1	Existing Grate Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	4.05	0.00000	5.00	4.05
HD-C2	Existing Grate Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	4.05	0.00000	5.00	4.05
HD-B1		0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	1.00	0.00000	5.00	1.00
WV-2	Existing No. 13 Grate Inlet	0.00000	0.00	13.00	0.00	0.00	0.00000	0.00	0.00	30.10	0.00000	13.00	30.10
WV-1	Existing 10' D-10-R Inlet	0.00000	0.00	11.00	0.00	0.00	0.00000	0.00	0.00	31.00	0.00000	11.00	31.00
21-3	Home Depot Sump Field FES	1.04203	0.50	7.07	8.24	4.33	0.00000	0.00	0.00	0.00	0.52102	7.07	4.33
02-2	Special Flanking Vane Grate Inlet	0.39164	0.95	5.00	9.09	3.41	0.20854	5.00	1.91	0.00	0.58060	5.00	5.32
02-3	Special Sump Vane Grate Inlet	0.00000	0.95	5.00	0.00	0.00	0.21858	5.00	2.00	0.00	0.21858	5.00	2.00



Scenario: One Hundred Year

Table A - Catchment Report

Label	Description	Area (acres)	Inlet C	Local Tc (min)	Local Intensity (in/hr)	Local Rational Flow (cfs)	Carryover CA (acres)	Carryover Tc (min)	Carryover Rational Flow (cfs)	Carryover Additional Flow (cfs)	Total Inlet CA (acres)	Total Inlet Time of Concentration (min)	Total Flow To Inlet (cfs)
05-1	On-Grade Curb Inlet	0.11000	0.95	5.00	9.09	0.96	0.79634	5.00	7.29	0.00	0.90084	5.00	8.25
05-2	On-Grade Curb Inlet	2.05641	0.95	6.80	8.34	16.42	0.09649	6.80	0.81	0.00	2.05007	6.80	17.23
01-3	Flanking Curb Inlet	0.66000	0.95	5.00	9.09	5.74	0.00000	0.00	0.00	0.00	0.62700	5.00	5.74
01-4	Sump Curb Inlet	0.00000	0.00	5.00	0.00	0.00	1.34294	5.00	12.30	0.00	1.34294	5.00	12.30
01-5	Flanking Curb Inlet	2.68000	0.95	6.39	8.49	21.80	0.01432	6.39	0.12	0.00	2.56032	6.39	21.92
01-7	Special On-Grade Curb Inlet	0.18085	0.95	5.00	9.09	1.57	0.25654	5.00	2.35	0.00	0.42835	5.00	3.92
01-8	On-Grade Curb Inlet	1.37769	0.95	5.00	9.09	11.99	0.00634	5.00	0.06	0.00	1.31514	5.00	12.05
HD-G1	Home Depot Detention Pond	0.00000	0.00	16.50	0.00	0.00	0.00000	16.50	0.00	22.62	0.00000	16.50	22.62
03-1	Existing Type C Inlet	0.00000	0.00	5.00	0.00	0.00	0.00000	0.00	0.00	10.20	0.00000	5.00	10.20
02-4	Special Flanking Vane Grate In	0.68000	0.95	5.00	9.09	5.92	0.00000	0.00	0.00	0.00	0.64600	5.00	5.92
01-3a		1.31000	0.50	7.67	8.02	5.30	0.00000	0.00	0.00	0.00	0.65500	7.67	5.30

Table B - Inlet Report

Label	Inlet	Inlet Type	Ground Elevation (ft)	Sump Elevation (ft)	Curb Opening Length (ft)	Clogging Factor (%)	Read Cross Slope (%)	Depressed Gutter?	Gutter Cross Slope (%)	Gutter Width (ft)	Inlet Location	Bypass Target	Longitudinal Slope (%)	Manning's n	Total Flow To Inlet (cfs)	Total Intercepted Flow (cfs)	Total Bypassed Flow (cfs)	Capture Efficiency (%)	Gutter Spread (ft)	Gutter Ditch Depth (ft)	
13-1	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,354.81	6,349.92	18.00		2.00	true	6.25	2.00	On Grade										
13-2	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,356.53	6,352.70	12.00		2.00	true	6.25	2.00	On Grade										
13-3	Grate CDOT Type C	Grate Inlet	6,355.55	6,353.20		50.0	2.00	false	2.00	0.00	In Sag	13-1	2.00	0.013	13.75	7.80	5.95	56.7	15.20	0.39	
38-2	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,355.72	6,349.06	12.00		2.00	true	6.25	2.00	On Grade										
35-2	Generic Default 100%	Generic Inlet	6,468.00	6,467.70			2.00	false	2.00	0.00	In Sag										
36-2	Generic Default 100%	Generic Inlet	6,479.61	6,472.00			2.00	false	2.00	0.00	In Sag										
25-1A	Grate CDOT TYPE D	Grate Inlet	6,482.00	6,471.30		50.0	2.00	false	2.00	0.00	In Sag										
25-2	Grate Special Type D	Grate Inlet	6,478.41	6,471.80		50.0	2.00	false	2.00	0.00	In Sag										
DP-7B	Combination Denver No 16 Single	Combination Inlet	6,400.10	6,394.60	3.33		2.00	true	6.25	2.00	On Grade				200.70	200.70	0.00	100.0	141.83	2.84	
DP-7C	Combination Denver No 16 Single	Combination Inlet	6,400.00	6,393.90	3.33	38.0	2.00	false	2.00	0.00	On Grade	DP-7C	0.00	0.013	1.52	1.52	0.00	99.9	30.24	0.69	
06-2	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,398.37	6,379.70	6.00		2.00	true	6.25	2.00	On Grade										
06-3	Curb CDOT Type R	Curb Inlet	6,397.17	6,380.50	5.00		2.00	true	4.16	1.00	On Grade	HD-G1	0.01	0.013	1.60	1.49	0.12	92.8	18.87	0.38	
37-1	Curb CDOT Type R	Curb Inlet	6,397.64	6,380.83	15.00		2.00	true	4.16	1.00	On Grade	05-2	1.33	0.013	1.28	1.23	0.05	95.4	5.82	0.20	
07-1	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,397.20	6,392.90	20.00		2.00	true	4.16	1.00	On Grade	05-2	1.35	0.013	4.35	3.58	0.77	82.3	10.88	0.24	
08-1	Curb CDOT Type R	Curb Inlet	6,398.84	6,394.00	5.00		2.00	true	4.16	1.00	On Grade	06-2	1.62	0.013	10.12	9.45	0.67	93.4	14.02	0.37	
WW-SW	Generic Default 100%	Generic Inlet	6,358.31	6,354.90			2.00	false	2.00	0.00	In Sag	05-3	1.90	0.013	0.55	0.46	0.10	82.4	4.56	0.11	
WW-SE	Generic Default 100%	Generic Inlet	6,359.09	6,355.00			2.00	false	2.00	0.00	In Sag				1.60	1.60	0.00	100.0	0.00	0.00	
WW-N	Generic Default 100%	Generic Inlet	6,360.84	6,357.60			2.00	false	2.00	0.00	In Sag				19.02	19.02	0.00	100.0	0.00	0.00	
09-2	Curb CDOT Type R	Curb Inlet	6,403.20	6,396.10	15.00		1.28	true	4.16	1.00	On Grade				12.27	12.27	0.00	100.0	0.00	0.00	
09-3	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,402.77	6,395.70	6.00		2.80	true	6.25	2.00	On Grade	10-1	2.03	0.013	1.83	1.72	0.10	94.3	9.50	0.15	
10-1	Curb CDOT Type R	Curb Inlet	6,402.23	6,396.70	15.00		0.38	true	4.16	1.00	On Grade	37-1	2.80	0.013	0.70	0.70	0.00	99.9	2.79	0.15	
06-4	Curb CDOT Type R	Curb Inlet	6,395.15	6,386.20	15.00		0.71	true	4.16	1.00	On Grade	37-1	1.84	0.013	0.48	0.48	0.00	100.0	12.09	0.08	
DP-6	Combination Denver No 16 Single	Combination Inlet	6,402.50	6,396.70	3.33	20.0	2.00	true	6.25	2.00	In Sag	01-8	1.41	0.013	1.43	1.37	0.06	95.9	13.37	0.13	
DP-7A	Combination Denver No 16 Single	Combination Inlet	6,400.50	6,395.50	3.33	38.0	2.00	true	6.25	2.00	On Grade				3.60	3.60	0.00	100.0	10.26	0.29	
HD-E2	Grate CDOT Type C	Grate Inlet	6,400.50	6,397.00		50.0	2.00	false	2.00	0.00	In Sag	DP-7B	0.00	0.013	4.40	4.18	0.22	95.0	37.09	0.66	
HD-F1	Grate CDOT Type C	Grate Inlet	6,400.00	6,394.10		50.0	2.00	false	2.00	0.00	In Sag				2.50	2.50	0.00	100.0	13.55	0.27	
HD-D1	Generic Default 100%	Generic Inlet	6,400.00	6,394.10			2.00	false	2.00	0.00	In Sag				16.80	16.80	0.00	100.0	11.41	0.23	
HD-C1	Grate CDOT Type C	Grate Inlet	6,398.00	6,393.30		50.0	2.00	false	2.00	0.00	In Sag				4.05	4.05	0.00	100.0	0.00	0.00	
HD-C2	Grate CDOT Type C	Grate Inlet	6,397.10	6,393.60		50.0	2.00	false	2.00	0.00	In Sag				4.05	4.05	0.00	100.0	17.83	0.36	
HD-B1	Generic Default 100%	Generic Inlet	6,400.50	6,397.31			2.00	false	2.00	0.00	In Sag				1.00	1.00	0.00	100.0	17.83	0.36	
WW-2	Generic Default 100%	Generic Inlet	6,386.00	6,382.00			2.00	false	2.00	0.00	In Sag				30.10	30.10	0.00	100.0	0.00	0.00	
WW-1	Generic Default 100%	Generic Inlet	6,386.00	6,382.00			2.00	false	2.00	0.00	In Sag				31.00	31.00	0.00	100.0	0.00	0.00	
21-3	Grate CDOT TYPE D	Grate Inlet	6,391.00	6,385.30		50.0	2.00	false	2.00	0.00	In Sag				4.33	4.33	0.00	100.0	16.85	0.34	
02-2	Combination Denver No 16 Double	Combination Inlet	6,367.67	6,363.89	7.08		38.0	2.00	true	6.25	2.00	On Grade				5.32	4.06	1.25	76.4	13.09	0.35
02-3	Combination Denver No 16 Double	Combination Inlet	6,367.50	6,364.47	7.08		50.0	2.00	false	2.00	In Sag				2.00	2.00	0.00	100.0	6.07	0.12	
05-1	Combination Denver No 16 Triple	Combination Inlet	6,369.39	6,365.77	10.92	38.0	2.00	true	6.25	2.00	On Grade	02-2	2.00	0.013	8.25	6.34	1.91	76.9	12.37	0.33	
05-2	Combination Denver Special No 16 Triple	Combination Inlet	6,370.67	6,367.10	10.92	38.0	2.00	true	6.25	2.00	On Grade	05-1	2.57	0.013	17.23	10.54	6.69	61.2	15.82	0.40	
01-3	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,368.39	6,364.31	20.00		2.00	true	6.25	2.00	On Grade	01-4	0.30	0.013	5.74	5.74	0.00	100.0	15.66	0.40	
01-4	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,368.33	6,364.36	16.00		2.00	true	6.25	2.00	In Sag				12.30	12.30	0.00	100.0	19.84	0.48	
01-5	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,368.50	6,364.48	10.00		2.00	true	6.25	2.00	On Grade	01-4	0.63	0.013	21.92	10.42	11.50	47.5	22.85	0.54	
01-7	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,372.50	6,367.01	14.00		2.00	true	6.25	2.00	On Grade	01-5	3.02	0.013	3.92	3.79	0.13	95.7	8.23	0.25	
01-8	Curb Colo. Sprgs. D-10-R Inlet	Curb Inlet	6,374.09	6,367.83	20.00		2.00	true	6.25	2.00	On Grade	01-7	3.52	0.013	12.05	9.70	2.35	80.5	12.86	0.34	
HD-G1	Generic Default 100%	Generic Inlet	6,379.56	6,372.79			0.00	false	0.00	0.00	In Sag				22.62	22.62	0.00	100.0	0.00	0.00	
03-1	Grate CDOT Type C	Grate Inlet	6,379.55	6,366.00		50.0	2.00	false	2.00	0.00	In Sag				10.20	10.20	0.00	100.0	35.87	0.72	
02-4	Combination Denver No 16 Double	Combination Inlet	6,367.51	6,364.80	7.08	38.0	2.00	true	6.25	2.00	On Grade	02-3	0.10	0.013	5.92	5.17	0.75	87.3	19.66	0.48	
01-3a	Grate CDOT Type C	Grate Inlet	6,367.38	6,363.36		50.0	2.00	false	2.00	0.00	In Sag				5.30	5.30	0.00	100.0	20.50	0.41	

Scenario: One Hundred Year

Table C - Pipe Report

Label	Upstream Node	Downstream Node	Section Shape	Section Size	Material	Manning's n	Length (ft)	Bend Angle (degrees)	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Upstream Sump Elevation (ft)	Downstream Sump Elevation (ft)	Upstream Crown Elevation (ft)	Downstream Crown Elevation (ft)	Upstream Cover (ft)	Downstream Cover (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Average Velocity (ft/s)	Full Capacity (cfs)	Total System Flow (cfs)
P-13-2	13-2	13-1	Circular	18 inch	Concrete	0.013	46.70	2.74	6,352.70	6,351.40	6,352.70	6,349.92	6,354.20	6,352.90	2.33	1.91	6,356.31	6,354.81	10.66	17.53	18.84
P-13-1	13-1	O-4	Circular	18 inch	Concrete	0.013	175.96	0.00	6,348.92	6,347.69	6,349.92	6,347.69	6,354.50	6,354.50	0.85	2.03	6,356.95	6,349.17	13.61	11.82	24.05
P-13-3	13-3	13-2	Circular	18 inch	Concrete	0.013	27.86	0.00	6,353.20	6,353.00	6,353.20	6,347.69	6,354.50	6,350.29	5.16	4.10	6,350.14	6,349.88	7.36	12.32	7.70
P-38-2	38-2	38-1	Circular	18 inch	Concrete	0.013	19.82	41.22	6,348.06	6,348.79	6,349.06	6,348.79	6,350.56	6,350.29	4.10	2.71	6,349.86	6,348.18	7.08	11.72	7.68
P-38-1	38-1	O-5	Circular	18 inch	Concrete	0.013	120.44	0.00	6,348.79	6,347.29	6,348.79	6,347.29	6,350.29	6,348.79	4.10	2.71	6,349.86	6,348.18	7.08	11.72	7.68
P-35-2	35-2	35-1	Circular	24 inch	Concrete	0.013	133.95	0.00	6,457.70	6,451.80	6,467.70	6,461.80	6,469.70	6,463.80	-1.70	4.20	6,469.64	6,463.16	16.78	47.46	37.82
P-36-2	36-2	36A	Horizontal El	24x38 inch	Concrete	0.013	12.21	41.25	6,472.00	6,471.72	6,472.00	6,471.72	6,474.00	6,473.72	5.61	0.76	6,473.52	6,473.26	12.24	135.71	59.08
P-36A	36A	36-1	Horizontal El	24x38 inch	Concrete	0.013	218.03	0.00	6,471.72	6,468.01	6,471.72	6,467.70	6,473.72	6,470.01	0.76	9.72	6,473.24	6,469.02	11.14	116.90	59.08
P-25-2	25-1A	25-1	Horizontal El	29x45 inch	Concrete	0.013	52.01	0.00	6,471.30	6,471.05	6,471.30	6,471.05	6,473.70	6,473.45	8.30	0.97	6,474.49	6,473.39	14.21	102.17	210.30
P-25-3	25-2	25-1A	Horizontal El	29x45 inch	Concrete	0.013	108.65	0.00	6,471.80	6,471.30	6,471.80	6,471.30	6,474.20	6,473.70	4.21	8.30	6,476.76	6,474.76	13.56	99.97	200.70
P-01-A	28-A	28-2	Circular	48 inch	Concrete	0.013	15.00	55.38	6,353.58	6,353.51	6,353.58	6,353.51	6,357.58	6,357.51	1.14	1.87	6,359.80	6,359.38	19.08	98.12	239.72
P-37-1	37-1	06-3	Circular	36 inch	Concrete	0.013	19.13	13.54	6,380.83	6,380.80	6,380.83	6,380.80	6,383.83	6,383.80	13.81	13.37	6,383.50	6,383.39	6.23	26.41	44.07
P-06-3	06-3	06-2	Circular	36 inch	Concrete	0.013	41.04	1.84	6,380.50	6,380.00	6,380.50	6,380.50	6,383.83	6,383.80	13.67	13.37	6,382.70	6,382.42	10.97	73.62	45.58
P-06-2	06-2	06-1	Circular	36 inch	Concrete	0.013	102.42	60.61	6,379.70	6,378.70	6,379.70	6,372.91	6,382.70	6,381.70	13.67	6.18	6,382.06	6,380.75	10.36	65.90	52.66
P-07-1	07-1	08-2	Circular	18 inch	Concrete	0.013	38.43	91.16	6,392.90	6,391.90	6,392.90	6,379.70	6,394.40	6,393.40	2.80	2.97	6,394.09	6,392.75	9.85	16.94	9.45
P-08-1	08-1	08-3	Circular	18 inch	Concrete	0.013	85.69	91.21	6,394.00	6,392.90	6,394.00	6,380.50	6,395.50	6,394.40	3.34	2.77	6,394.25	6,393.11	3.12	11.26	0.46
P-WV-3	WV-3	06-1	Circular	42 inch	Concrete	0.013	63.20	0.88	6,376.02	6,372.91	6,376.02	6,372.91	6,379.52	6,376.41	3.98	11.47	6,378.60	6,376.92	20.35	223.17	67.87
P-06-1	06-1	WV-4	Circular	42 inch	Concrete	0.013	95.55	14.85	6,372.91	6,371.37	6,372.91	6,371.37	6,376.41	6,374.87	11.47	2.63	6,376.89	6,375.54	12.44	127.72	119.67
P-WV-4	WV-4	28-1	Circular	48 inch	Concrete	0.013	844.20	38.83	6,371.37	6,366.00	6,371.37	6,366.00	6,375.37	6,360.00	2.13	1.91	6,374.96	6,361.91	17.22	193.81	149.71
P-28-2	28-1	28-A	Circular	48 inch	Concrete	0.013	148.04	2.20	6,356.00	6,353.58	6,356.00	6,353.58	6,360.00	6,357.58	1.91	1.14	6,361.90	6,360.05	12.07	183.65	160.47
P-WV-SE	WV-SE	WV-SW	Circular	24 inch	Concrete	0.013	40.20	13.13	6,355.00	6,354.90	6,355.00	6,354.90	6,357.00	6,356.90	2.09	1.41	6,358.59	6,358.31	6.05	11.28	19.02
P-WV-SW	WV-SW	28-2	Circular	24 inch	Concrete	0.013	8.60	20.28	6,354.90	6,353.51	6,354.90	6,353.51	6,356.90	6,355.51	1.41	3.87	6,359.45	6,359.36	6.38	90.94	20.04
P-WV-N	WV-N	28-1	Circular	24 inch	Concrete	0.013	47.60	47.61	6,357.60	6,356.00	6,357.60	6,356.00	6,359.60	6,358.00	1.24	3.91	6,362.05	6,361.91	3.91	41.47	12.27
P-09-3	09-3	09-2	Circular	18 inch	Concrete	0.013	31.07	46.51	6,396.70	6,396.40	6,396.70	6,396.10	6,398.20	6,397.90	4.57	5.30	6,397.01	6,396.81	3.33	10.32	0.70
P-09-2	09-2	09-1	Circular	18 inch	Concrete	0.013	19.26	57.63	6,396.10	6,395.80	6,396.10	6,382.34	6,397.60	6,397.30	5.60	5.74	6,396.74	6,396.30	5.94	13.11	2.87
P-10-1	10-1	09-2	Circular	18 inch	Concrete	0.013	36.94	87.32	6,396.70	6,396.40	6,396.70	6,396.10	6,398.20	6,397.90	4.03	5.30	6,396.96	6,396.76	2.81	9.47	0.48
P-09-1	09-1	WV-3	Circular	42 inch	Concrete	0.013	178.20	0.09	6,382.34	6,376.02	6,382.34	6,376.02	6,385.84	6,379.52	17.20	3.98	6,383.13	6,378.61	9.33	169.46	6.87
P-08-4	08-4	06-3	Circular	18 inch	Concrete	0.013	233.21	95.09	6,386.20	6,382.00	6,386.20	6,380.50	6,387.70	6,383.50	7.45	13.67	6,386.64	6,383.37	5.06	14.10	1.37
P-37-2	37-2	37-1	Circular	18 inch	Concrete	0.013	186.15	52.50	6,381.46	6,381.13	6,381.46	6,380.83	6,382.96	6,382.63	16.81	15.01	6,391.23	6,383.90	11.79	8.85	41.68
P-DP-5	DP-5	37-2	Circular	30 inch	Concrete	0.013	325.16	115.80	6,395.70	6,384.11	6,395.70	6,381.46	6,398.20	6,386.61	2.30	13.16	6,395.02	6,391.79	5.47	77.43	1.00
P-DP-8	DP-8	37-2	Circular	24 inch	Concrete	0.013	141.95	26.51	6,393.10	6,384.11	6,393.10	6,381.46	6,395.10	6,386.11	5.60	13.66	6,395.50	6,391.91	12.95	56.93	40.68
P-DP-7C	DP-7C	DP-8	Circular	24 inch	Concrete	0.013	60.98	6.10	6,393.90	6,393.60	6,393.90	6,393.10	6,395.90	6,395.60	4.10	6.10	6,398.53	6,397.27	10.37	15.87	32.58
P-DP-7B	DP-7B	DP-7C	Circular	24 inch	Concrete	0.013	141.26	5.41	6,394.60	6,393.90	6,394.60	6,393.90	6,396.60	6,395.90	3.50	4.10	6,399.71	6,399.15	4.55	15.92	14.30
P-DP-6	DP-6	DP-7	Circular	18 inch	Concrete	0.013	87.91	6.48	6,398.70	6,398.00	6,398.70	6,396.00	6,400.20	6,399.50	2.30	2.20	6,400.68	6,400.58	2.04	9.37	3.60
P-DP-7	DP-7	DP-7A	Circular	24 inch	Concrete	0.013	97.44	6.53	6,396.00	6,395.50	6,396.00	6,395.50	6,398.00	6,397.50	3.70	3.00	6,400.54	6,400.40	2.74	16.20	8.60
P-DP-7A	DP-7A	DP-7B	Circular	24 inch	Concrete	0.013	180.27	0.38	6,395.50	6,394.60	6,395.50	6,394.60	6,397.50	6,396.60	3.00	3.50	6,400.33	6,399.76	4.07	15.98	12.78
P-HD-E2	HD-E2	HD-E1	Circular	15 inch	Concrete	0.013	121.84	0.02	6,397.00	6,396.40	6,397.00	6,396.40	6,398.25	6,397.65	2.25	3.15	6,400.98	6,400.80	2.04	4.53	2.50
P-HD-E1	HD-E1	DP-7	Circular	15 inch	Concrete	0.013	82.41	83.53	6,396.40	6,395.00	6,396.40	6,396.00	6,397.65	6,397.25	3.15	4.45	6,401.18	6,400.69	4.07	5.00	5.00
P-HD-F1	HD-F1	HD-E1	Circular	15 inch	Concrete	0.013	15.85	90.11	6,397.00	6,396.90	6,397.00	6,396.40	6,398.25	6,397.65	2.25	2.65	6,400.82	6,400.80	2.04	5.13	2.50
P-HD-D1	HD-D1	DP-7C	Circular	24 inch	Concrete	0.013	38.48	96.66	6,394.10	6,393.90	6,394.10	6,393.90	6,395.10	6,395.90	3.90	4.10	6,399.63	6,399.42	5.35	16.31	16.80
P-HD-C2	HD-C2	HD-C1	Circular	15 inch	Concrete	0.013	48.26	0.44	6,393.60	6,393.30	6,393.60	6,393.30	6,394.85	6,394.55	2.25	3.45	6,397.97	6,397.78	3.30	5.09	4.05
P-HD-C1	HD-C1	DP-8	Circular	15 inch	Concrete	0.013	37.98	89.64	6,393.30	6,393.10	6,393.30	6,393.10	6,394.55	6,394.35	3.45	6.35	6,397.53	6,396.93	6.60	4.89	8.10
P-HD-B	HD-B1	DP-5	Circular	12 inch	Concrete	0.013	2.00	89.40	6,397.31	6,397.30	6,397.31	6,395.70	6,398.30	6,398.30	2.19	2.20	6,397.74	6,397.72	3.02	2.52	1.00
P-WV-2	WV-2	WV-4	Circular	24 inch	Concrete	0.013	073.00	93.47	6,392.00	6,371.37	6,392.00	6,371.37	6,384.00	6,373.37	2.00	4.13	6,394.22	6,375.22	9.58	22.52	30.10
P-WV-1	WV-1	WV-3	Circular	24 inch	Concrete	0.013	381.00	48.83	6,382.00	6,376.02	6,382.00	6,376.02	6,384.00	6,378.02	2.00	5.48	6,407.26	6,378.64	19.74	28.34	62.00
P-21-3	21-3	21-2	Circular	30 inch	Concrete	0.013	56.33	15.83	6,385.30	6,384.70	6,385.30	6,384.40	6,387.80	6,387.20	3.20	16.85	6,385.98	6,385.24	5.55	42.33	4.33
P-30	21-2	21-1	Circular	30 inch	Concrete	0.013	12.48	39.73	6,384.40	6,384.17	6,384.40	6,384.17	6,386.90	6,386.67	17.15	17.26	6,385.08	6,384.86	6.72	55.68	4.29
P-31	21-1	09-1	Circular	30 inch	Concrete	0.013	42.14	0.24	6,384.17	6,382.34	6,384.17	6,382.34	6,386.67	6,384.84	17.26	18.20	6,384.85	6,383.13	9.08	85.47	4.29
P-01	28-2	O-1B	Circular	48 inch	Concrete	0.013	145.00	0.00	6,353.51	6,351.73	6,353.51	6,351.73	6,357.51	6,355.73	1.87	-1.73	6,361.22	6,356.50	20.61	159.14	259.04
P-40	01-00	28-A	Circular	48 inch	Concrete	0.013	23.00	31.52	6,353.77	6,353.69	6,353.77	6,353.69	6,357.77	6,357.69	1.47	1.03	6,360.61	6,360.53	6.41	84.71	80.53
P-02-3	02-3	02-2	Circular	18 inch	Concrete	0.013	49.65	0.91	6,364.47	6,364.19	6,364.47	6,363.89	6,365.97	6,365.69	1.53	1.98	6,365.65	6,365.46	5.05	7.87	7.16

Title: Woodmen Road and Academy Blvd Intersection  
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 01/07/09 12:59:19 PM

Table C - Pipe Report

Label	Upstream Node	Downstream Node	Section Shape	Section Size	Material	Manning's n	Length (ft)	Bend Angle (degrees)	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Upstream Sump Elevation (ft)	Downstream Sump Elevation (ft)	Upstream Crown Elevation (ft)	Downstream Crown Elevation (ft)	Upstream Cover (ft)	Downstream Cover (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Average Velocity (ft/s)	Full Capacity (cfs)	Total System Flow (cfs)
P-02-2	02-2	02-1	Circular	18 inch	Concrete	0.013	76.19	91.91	6,363.89	6,362.00	6,363.89	6,361.39	6,365.39	6,363.50	2.28	5.32	6,365.35	6,364.51	10.04	16.54	11.13
P-05-2	05-2	05-1	Circular	18 inch	Concrete	0.013	46.08	0.63	6,367.10	6,366.07	6,367.10	6,365.77	6,368.60	6,367.57	2.07	1.82	6,368.35	6,367.66	9.53	15.70	10.54
P-05-1	05-1	02-1	Circular	18 inch	Concrete	0.013	45.63	88.78	6,365.77	6,364.85	6,365.77	6,361.39	6,367.27	6,366.35	2.12	2.47	6,367.39	6,366.26	9.22	14.91	16.29
P-02-1	02-1	01-1	Horizontal El	19x30 inch	Concrete	0.013	14.46	0.13	6,361.87	6,361.77	6,361.39	6,355.20	6,363.47	6,363.37	5.35	6.26	6,364.28	6,364.12	8.02	20.90	26.46
P-01-6	01-8	01-7	Circular	36 inch	Concrete	0.013	32.99	1.48	6,367.83	6,367.31	6,367.83	6,367.01	6,370.83	6,370.31	3.26	2.19	6,369.57	6,368.67	10.75	83.73	26.88
P-HD-G1	HD-G1	01-9	Circular	36 inch	Concrete	0.013	1.00	22.09	6,372.79	6,372.78	6,372.79	6,372.78	6,375.79	6,375.78	3.77	3.85	6,374.32	6,374.32	8.53	66.69	22.62
P-01-9	01-9	01-8	Circular	36 inch	Concrete	0.013	116.21	5.22	6,372.78	6,368.13	6,372.76	6,367.83	6,375.76	6,371.13	3.85	2.96	6,374.31	6,368.98	14.06	133.41	22.62
P-01-7	01-7	01-6	Circular	36 inch	Concrete	0.013	132.55	4.40	6,367.01	6,364.90	6,367.01	6,364.90	6,370.01	6,367.90	2.49	1.71	6,368.83	6,368.34	11.03	84.15	31.32
P-01-6	01-6	01-5	Circular	36 inch	Concrete	0.013	87.48	4.54	6,364.90	6,364.48	6,364.90	6,364.48	6,367.90	6,367.48	1.71	1.02	6,368.33	6,367.99	5.87	46.21	41.47
P-01-5	01-5	01-4	Circular	36 inch	Concrete	0.013	45.78	0.45	6,364.48	6,364.36	6,364.48	6,364.36	6,367.48	6,367.35	1.02	0.97	6,367.88	6,367.63	6.86	34.15	48.52
P-01-4	01-4	01-3	Circular	36 inch	Concrete	0.013	17.68	97.50	6,364.36	6,364.31	6,364.36	6,364.31	6,367.36	6,367.31	0.97	1.08	6,367.53	6,367.41	7.96	35.47	56.28
P-01-3	01-3	01-2	Horizontal El	19x30 inch	Concrete	0.013	120.04	81.59	6,364.31	6,363.94	6,364.31	6,362.78	6,365.91	6,365.54	2.48	3.13	6,365.85	6,365.99	6.44	41.86	63.71
P-01-2	01-2	01-1	Circular	42 inch	Concrete	0.013	146.06	91.93	6,362.78	6,361.67	6,362.78	6,355.20	6,366.28	6,365.17	2.39	4.46	6,365.28	6,364.46	9.88	87.11	63.44
P-03-1	03-1	01-6	Circular	18 inch	Concrete	0.013	26.87	61.98	6,366.00	6,365.85	6,366.00	6,364.90	6,367.50	6,367.35	12.05	2.26	6,368.64	6,368.38	5.77	7.65	10.20
P-02-4	02-4	02-3	Circular	18 inch	Concrete	0.013	4.67	1.51	6,364.80	6,364.77	6,364.80	6,364.47	6,365.30	6,366.27	1.21	1.23	6,365.70	6,365.71	5.01	8.42	5.17
P-36	01-3a	01-3	Circular	24 inch	Concrete	0.013	23.16	0.00	6,364.50	6,364.38	6,363.38	6,364.31	6,366.50	6,366.38	0.88	2.01	6,367.09	6,367.08	1.69	16.28	5.30
P-37	01-1	01-0	Circular	30 inch	Concrete	0.013	85.00	2.21	6,361.67	6,358.81	6,355.20	6,358.00	6,364.17	6,361.31	5.46	1.32	6,363.81	6,362.07	15.63	150.47	81.39
P-39	01-0	01-00	Circular	30 inch	Concrete	0.013	282.00	0.00	6,358.51	6,356.01	6,358.00	6,352.96	6,361.01	6,358.51	1.62	0.73	6,362.01	6,359.24	6.28	77.24	81.27

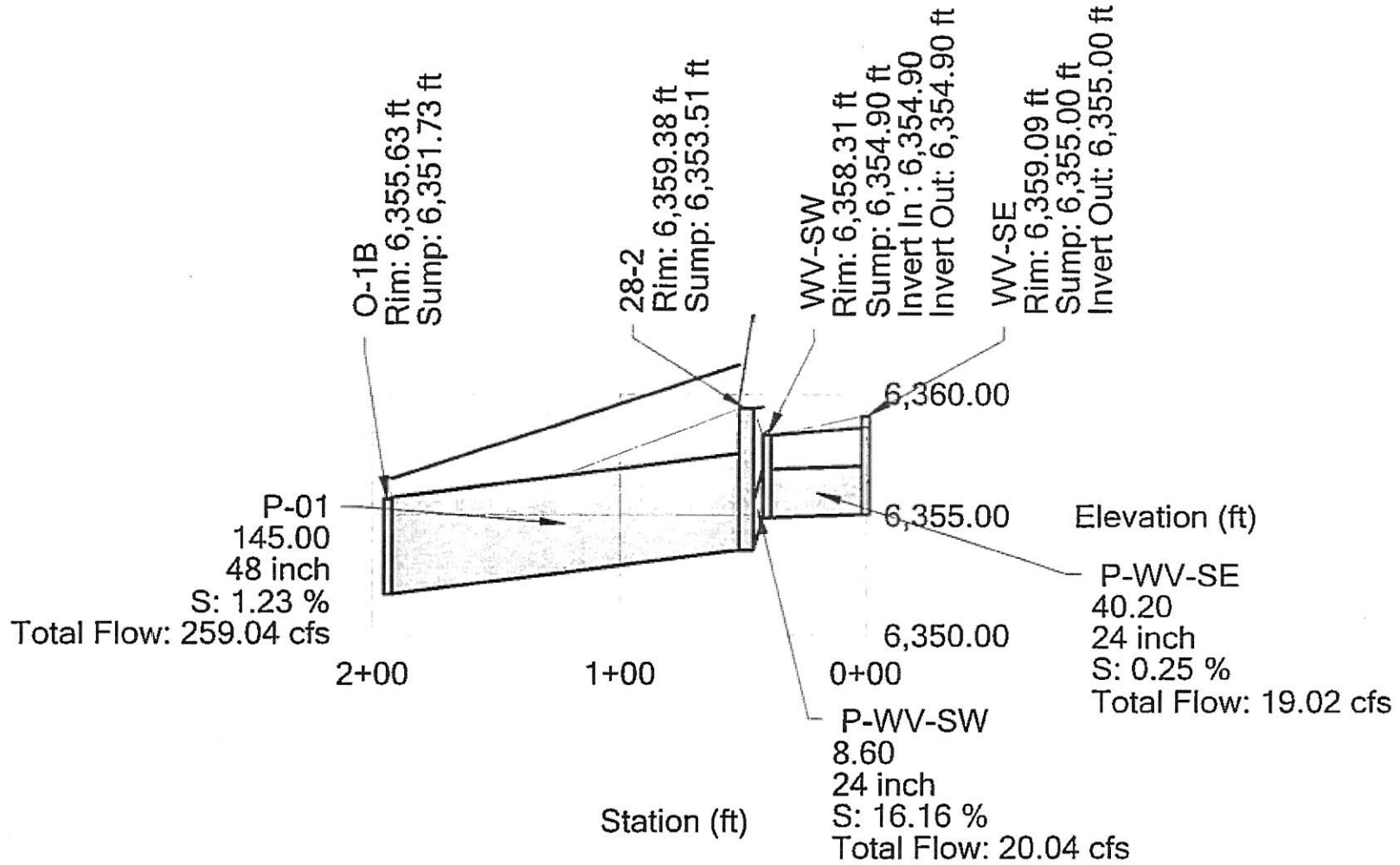
Scenario: One Hundred Year

Table D - Junction Report

Label	Description	Structure Diameter (ft)	Ground Elevation (ft)	Sump Elevation (ft)	Set Rim Equal to Ground Elevation?	Rim Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Total Flow (cfs)
38-1	Proposed Manhole Connection to Exis	6.00	6,354.39	6,348.79	true	6,354.39	6,349.88	6,349.86	7.68
36A		2.00	6,474.48	6,471.72	false	6,474.48	6,473.26	6,473.24	59.08
28-A		6.00	6,358.72	6,353.58	false	6,355.69	6,360.05	6,359.80	239.72
06-1		6.00	6,387.88	6,372.91	true	6,387.88	6,376.92	6,376.89	119.67
28-2	Existing Manhole	6.00	6,359.38	6,353.51	true	6,359.38	6,363.25	6,359.38	259.04
28-1	Existing Manhole	7.00	6,361.91	6,356.00	false	6,361.75	6,362.93	6,361.90	160.47
WV-4	Existing Junction	4.00	6,377.50	6,371.37	false	6,377.50	6,375.22	6,374.96	149.71
WV-3	Existing Wye	6.00	6,383.50	6,376.02	false	6,383.50	6,378.61	6,378.60	67.87
09-1		6.00	6,403.04	6,382.34	true	6,403.04	6,383.13	6,383.13	6.87
DP-7		4.00	6,401.70	6,396.00	false	6,401.70	6,400.58	6,400.54	8.60
DP-8		4.00	6,400.70	6,393.10	false	6,400.70	6,396.93	6,396.50	40.68
HD-E1	Pipe Connection	1.25	6,400.80	6,396.40	false	6,400.80	6,400.84	6,400.80	5.00
37-2	Existing MH	6.00	6,399.77	6,381.46	true	6,399.77	6,391.79	6,391.23	41.68
DP-5		4.00	6,400.50	6,395.70	false	6,400.50	6,396.05	6,396.02	1.00
21-1		5.00	6,403.93	6,384.17	false	6,403.93	6,384.86	6,384.85	4.29
21-2		5.00	6,404.05	6,384.40	true	6,404.05	6,385.08	6,385.08	4.29
01-00		10.00	6,359.24	6,352.96	true	6,359.24	6,359.27	6,359.24	80.53
01-0		10.00	6,362.63	6,358.00	true	6,362.63	6,362.07	6,362.01	81.27
01-1		7.00	6,369.63	6,355.20	true	6,369.63	6,364.12	6,363.81	81.39
01-2		6.00	6,368.67	6,362.78	true	6,368.67	6,365.99	6,365.28	63.44
01-6		7.00	6,369.61	6,364.90	true	6,369.61	6,368.34	6,368.33	41.47
01-9	Connection to Existing Home Depot In	5.00	6,379.63	6,372.78	true	6,379.63	6,374.32	6,374.31	22.62
02-1		4.00	6,368.82	6,361.39	true	6,368.82	6,364.51	6,364.28	26.46

# Profile: Prince Inlets

## Scenario: One Hundred Year



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**FINAL  
DRAINAGE REPORT AND PLAN  
FOR  
I-25 NISSAN PRE-OWNED CAR DEALERSHIP  
AMERICAN FURNITURE AT WOODMAN RD. FIL. NO. 1**

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February, 2003

**Leigh  
& Whitehead  
Associates, Inc.**

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CONSULTING CIVIL ENGINEERS & SURVEYORS  
2720 EAST YAMPA STREET, SUITE 1  
COLORADO SPRINGS, CO 80909-5061

LWA Project No. 03009.64

A

parking for prospective car purchasers along with a display area of pre-owned and some new vehicles. Basic improvements to the I-25 off-ramp and Woodmen Road along the north are currently in the process of being constructed by the Colorado Department of Highways. Anticipated completion is unknown at this time. Vincent Drive on the east, is an existing City of Colorado Springs street, and is currently fully developed. Runoff from the Woodmen Road and I-25 off-ramp will not enter this subdivision. This development will not impact the I-25 Woodmen Road improvements.

This building's roof drains will be routed underground through 8" under drain pipes that will outlet in the appropriate parking and drive area. The location of the underground pipes and release locations are shown on the attached Drainage Plan.

**Basin Characteristics:**

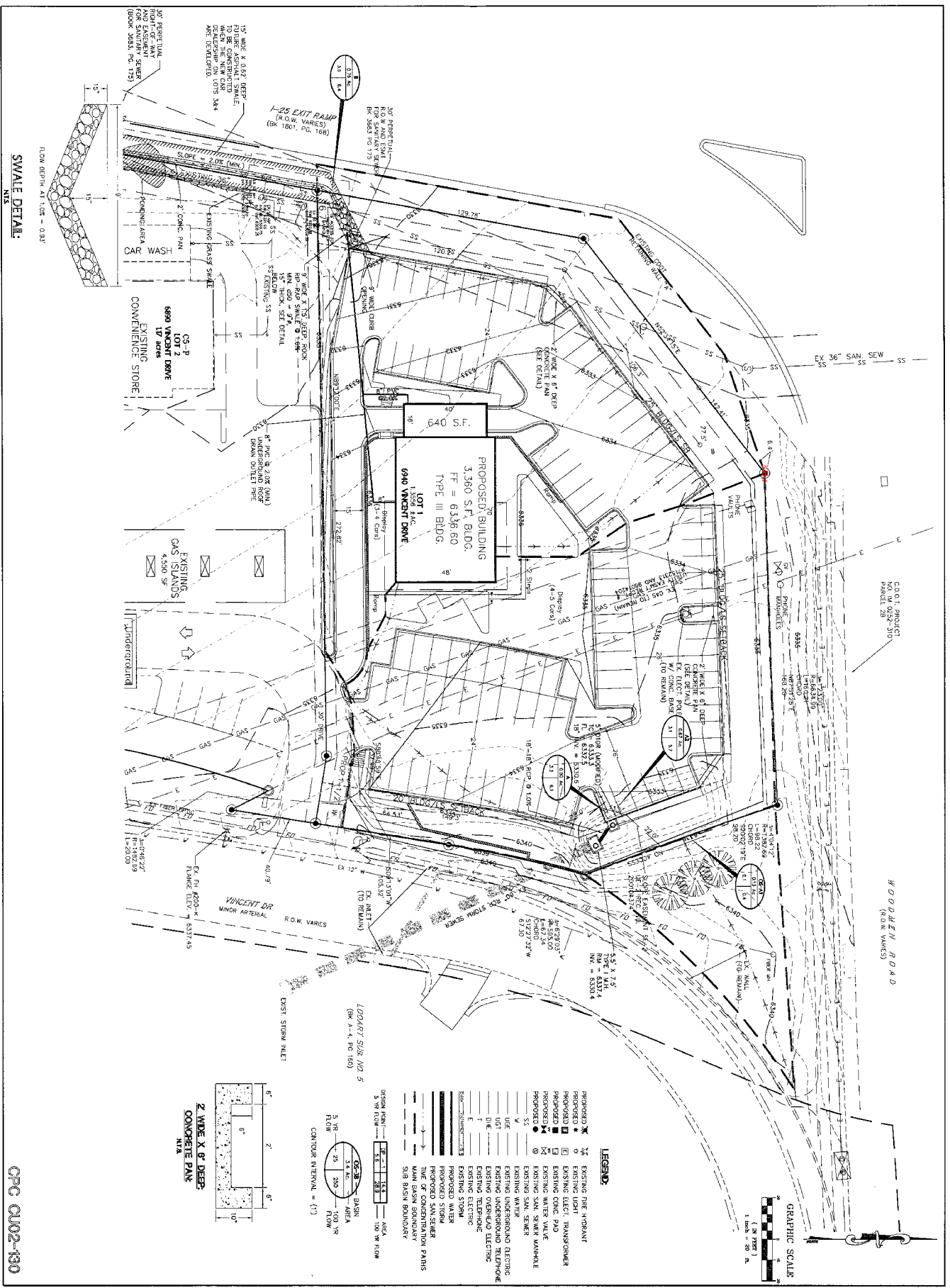
This site was divided into two major basins delineated on the attached Drainage Plan as Basin A and Basin B. Basin A is the easterly half of this site, and was divided into two sub-basins. Sub-basin OS-A-1 located east of this property between Woodmen Road and Vincent Drive is a small, landscaped grass area that directs runoff westerly to this property. Sub-Basin OS A-1 contains 0.13 acres and generates a peak flow of 0.1 cfs for the 5-year event and 0.4 cfs for the 100-year event. These flows are directed to this site via sheetflow to a proposed 5' D10R inlet in a sump condition. The location of this inlet is shown on the attached proposed drainage plan. Sub-Basin A-2 is the easterly half of this property and directs runoff easterly and northerly to the previously mentioned 5' D10R, located in a sump condition along the easterly edge of the parking area. Sub-Basin A-2 contains 0.67 acres and generates a peak flow of 3.1 cfs for the 5-year event and 5.7 cfs for the 100-year event. Basin A has a total area of 0.80 acres and generates a peak flow of 3.3 cfs for the 5-year event, and 6.1 cfs for the 100-year event. Runoff from this inlet is conveyed easterly to the existing 60" RCP via a proposed 18" RCP at a minimum of 1% slope. The end of the existing 60" RCP will have a Type I manhole constructed. This manhole will be 5½' wide by 7½' long. These flows will then be conveyed southeasterly under Vincent Road to an appropriate outlet point, and then to Cottonwood Creek,



located south of this property.

Basin B is the westerly half of this site and contains 0.75 acres. Peak runoff exiting Basin B is 3.5 cfs for the 5-year event and 6.4 cfs for the 100-year event. Runoff is directed westerly and southerly to a curb opening located at the southwest corner of the parking lot. Runoff will be conveyed southwesterly through a 9' wide curb opening to a proposed 9' wide x 1 ½' deep rock rip-rap "V" swale to the previously mentioned undefined existing swale within the I-25 off-ramp right-of-way, and west of the Loaf and Jug. Flows will then be conveyed southerly within this swale to an existing 24" RCP located in the southwesterly portion of Lot 4. Currently, this existing swale is undefined and initial observations indicate that runoff ponds south of this site. Proposed conditions for this swale would be to construct an asphalt swale 15' wide with a 2' wide concrete pan that will be routed southerly to an existing 24" RCP located on the north edge of the American Storage Subdivision. This asphalt swale will be located adjacent to the existing I-25 exit ramp retaining wall. This paved swale will be 15' wide with 12:1 side slopes and a 2' wide concrete pan located in the center of the swale. The swale will be 0.63' deep and peak flow exiting the Nissan site is 6.4 cfs for the 100-year event. This results in a water surface depth of 0.37'. This asphalt swale will be directed southerly to lots 3 and 4 of the American Furniture Subdivision. The exact details of this swale will be shown on the construction documents and drainage plan for the I-25 Nissan New Car Dealership, Lots 3 and 4, American Furniture at Woodmen Road, Filing No. 1. The proposed/existing grass swale along the west side of the Loaf and Jug is part of the requirements as outlined in the preliminary/final drainage report for Loaf and Jug prepared by ADP Inc., and accepted by the City of Colorado Springs in January, 2001. Currently, this swale is not functioning as designed. This could be related to the continued construction of the I-25 exit ramp. A portion of the proposed swale and its location is shown on the attached Proposed Drainage Plan for I-25 Nissan. If the I-25 Nissan New Car Dealership located on Lots 3 and 4 of this subdivision is not developed in a timely manner, and it appears that the runoff from the Pre-Owned Dealership is creating problems adjacent to the I-25 exit ramp, the improvements outlined in this report will be constructed in a timely manner to prevent possible erosion and undercutting of the existing I-25 exit ramp retaining wall. These





SWALE DETAIL:  
FLOW DEPTH AT 10% = 0.33'

CPC CU02-130

<p>PLANNERS <b>LEIGH WHITEHEAD &amp; ASSOCIATES</b> 2728 EAST TAPPA STREET, SUITE 1 DENVER, COLORADO 80231 TEL: 303.733.8888 FAX: 303.733.8889</p>	<p>COPYRIGHT <b>LEIGH WHITEHEAD &amp; ASSOCIATES, INC.</b> ALL RIGHTS RESERVED NO PART OF THIS DRAWING WITHOUT WRITTEN PERMISSION OF ENGINEER</p>	<p>SHEET TITLE: <b>PROPOSED DRAINAGE PLAN WOODMAN RD. &amp; VINCENT DR.</b></p> <p>PROJECT NAME: <b>1-25 NISSAN PRE - OWNED CAR DEALERSHIP</b></p>	<p>BENCHMARK: TOP OF OLD SOUTHWEST CONCRETE LOT MARK = 5527.95</p>	<p>REVISIONS:</p> <table border="1"> <tr> <td>NO.</td> <td>DATE</td> <td>BY</td> <td>DESCRIPTION</td> </tr> <tr> <td>1</td> <td>02/28/03</td> <td>KEM</td> <td>DRYING MARKS</td> </tr> <tr> <td>2</td> <td></td> <td></td> <td>FP - DRAINAGE</td> </tr> </table>	NO.	DATE	BY	DESCRIPTION	1	02/28/03	KEM	DRYING MARKS	2			FP - DRAINAGE	<p>PROJECT NO.: 06009 DRAWING NUMBER: MISSAN SHEET NO.: 1 OF 1</p>
NO.	DATE	BY	DESCRIPTION														
1	02/28/03	KEM	DRYING MARKS														
2			FP - DRAINAGE														

**Appendix C**  
**Hydrologic Calculations**

## Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method

Worksheet Protected

UD-BMP (Version 3.06, November 2016)

User Input		
Calculated cells		
---Design Storm: 1-Hour Rain Depth	WQCV Event	0.60
---Minor Storm: 1-Hour Rain Depth	5-Year Event	1.50
---Major Storm: 1-Hour Rain Depth	100-Year Event	2.52
Optional User Defined Storm	CUHP	
(CUHP) NOAA 1 Hour Rainfall Depth and Frequency for User Defined Storm	100-Year Event	
Max Intensity for Optional User Defined Storm		0

**Designer:** Casey Visscher  
**Company:** Galloway & Co.  
**Date:** December 20, 2018  
**Project:** Crest at Woodmen - MDDP Amendment  
**Location:** Colorado Springs, CO

### SITE INFORMATION (USER-INPUT)

Sub-basin Identifier	A1	A2	A3	A4	A5	A6	A7	A8	A9	A10	A11	A12	A13	A14
Receiving Pervious Area Soil Type	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand
Total Area (ac., Sum of DCIA, UIA, RPA, & SPA)	2.470	2.480	3.810	3.440	0.330	3.330	2.860	0.600	1.330	2.750	3.800	0.240	5.000	0.050
Directly Connected Impervious Area (DCIA, acres)	2.347	1.334	3.139	3.296	0.330	3.164	2.720	0.600	1.305	2.607	3.606	0.240	4.750	0.050
Unconnected Impervious Area (UIA, acres)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Receiving Pervious Area (RPA, acres)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.016	0.016	0.000	0.000
Separate Pervious Area (SPA, acres)	0.124	1.146	0.671	0.144	0.000	0.167	0.140	0.000	0.025	0.143	0.178	(0.016)	0.250	0.000
RPA Treatment Type: Conveyance (C), Volume (V), or Permeable Pavement (PP)	V	V	V	V	V	V	V	V	V	V	V	V	V	V

### CALCULATED RESULTS (OUTPUT)

Total Calculated Area (ac, check against input)	2.470	2.480	3.810	3.440	0.330	3.330	2.860	0.600	1.330	2.750	3.800	0.240	5.000	0.050
Directly Connected Impervious Area (DCIA, %)	95.0%	53.8%	82.4%	95.8%	100.0%	95.0%	95.1%	100.0%	98.1%	94.8%	94.9%	100.0%	95.0%	100.0%
Unconnected Impervious Area (UIA, %)	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
Receiving Pervious Area (RPA, %)	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.4%	6.7%	0.0%	0.0%
Separate Pervious Area (SPA, %)	5.0%	46.2%	17.6%	4.2%	0.0%	5.0%	4.9%	0.0%	1.9%	5.2%	4.7%	-6.7%	5.0%	0.0%
A <sub>s</sub> (RPA / UIA)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
I <sub>s</sub> Check	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
f / I for WQCV Event:	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2
f / I for 5-Year Event:	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
f / I for 100-Year Event:	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4
<b>f / I for Optional User Defined Storm CUHP:</b>														
IRF for WQCV Event:	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
IRF for 5-Year Event:	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
IRF for 100-Year Event:	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
<b>IRF for Optional User Defined Storm CUHP:</b>														
Total Site Imperviousness: I <sub>total</sub>	95.0%	53.8%	82.4%	95.8%	100.0%	95.0%	95.1%	100.0%	98.1%	94.8%	94.9%	100.0%	95.0%	100.0%
Effective Imperviousness for WQCV Event:	95.0%	53.8%	82.4%	95.8%	100.0%	95.0%	95.1%	100.0%	98.1%	94.8%	94.9%	100.0%	95.0%	100.0%
Effective Imperviousness for 5-Year Event:	95.0%	53.8%	82.4%	95.8%	100.0%	95.0%	95.1%	100.0%	98.1%	94.8%	94.9%	100.0%	95.0%	100.0%
Effective Imperviousness for 100-Year Event:	95.0%	53.8%	82.4%	95.8%	100.0%	95.0%	95.1%	100.0%	98.1%	94.8%	94.9%	100.0%	95.0%	100.0%
<b>Effective Imperviousness for Optional User Defined Storm CUHP:</b>														

### LID / EFFECTIVE IMPERVIOUSNESS CREDITS

WQCV Event CREDIT: Reduce Detention By:	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
This line only for 10-Year Event	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
100-Year Event CREDIT**: Reduce Detention By:	0.0%	0.0%	0.0%	0.0%	0.1%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.1%	0.5%
<b>User Defined CUHP CREDIT: Reduce Detention By:</b>														

Total Site Imperviousness:	90.8%
Total Site Effective Imperviousness for WQCV Event:	90.8%
Total Site Effective Imperviousness for 5-Year Event:	90.8%
Total Site Effective Imperviousness for 100-Year Event:	90.8%
Total Site Effective Imperviousness for Optional User Defined Storm CUHP:	

#### Notes:

- \* Use Green-Ampt average infiltration rate values from Table 3-3.
- \*\* Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM.
- \*\*\* Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed

## Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method

UD-BMP (Version 3.06, November 2016)

User Input		
Calculated cells		
---Design Storm: 1-Hour Rain Depth	WQCV Event	0.60 inches
---Minor Storm: 1-Hour Rain Depth	5-Year Event	1.50 inches
---Major Storm: 1-Hour Rain Depth	100-Year Event	2.52 inches
Optional User Defined Storm	CUHP	
(CUHP) NOAA 1 Hour Rainfall Depth and Frequency for User Defined Storm	100-Year Event	
Max Intensity for Optional User Defined Storm		0

**Designer:** Casey Visscher  
**Company:** Galloway & Co.  
**Date:** December 20, 2018  
**Project:** Crest at Woodmen - MDDP Amendment  
**Location:** Colorado Springs, CO

### SITE INFORMATION (USER-INPUT)

Sub-basin Identifier	A15	A16	A17	A18	A19	A20	A21	A22	B1-1	B1-2	B2	B3-1	B3-2	B3-3
Receiving Pervious Area Soil Type	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Sandy Clay Loam	Loamy Sand	Loamy Sand	Sand	Loamy Sand	Loamy Sand
Total Area (ac., Sum of DCIA, UIA, RPA, & SPA)	1.090	1.210	5.240	4.120	0.690	1.060	0.450	3.450	1.320	0.380	1.150	7.340	1.310	0.640
Directly Connected Impervious Area (DCIA, acres)	1.090	1.210	4.978	3.914	0.690	1.060	0.450	0.221	0.066	0.342	0.769	5.711	1.151	0.545
Unconnected Impervious Area (UIA, acres)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Receiving Pervious Area (RPA, acres)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.016	0.016	0.000	0.000
Separate Pervious Area (SPA, acres)	0.000	0.000	0.262	0.206	0.000	0.000	0.000	3.229	1.254	0.038	0.365	1.613	0.159	0.095
RPA Treatment Type: Conveyance (C), Volume (V), or Permeable Pavement (PP)	V	V	V	V	V	V	V	V	V	V	V	V	V	V

### CALCULATED RESULTS (OUTPUT)

Total Calculated Area (ac, check against input)	1.090	1.210	5.240	4.120	0.690	1.060	0.450	3.450	1.320	0.380	1.150	7.340	1.310	0.640
Directly Connected Impervious Area (DCIA, %)	100.0%	100.0%	95.0%	95.0%	100.0%	100.0%	100.0%	6.4%	5.0%	90.0%	66.9%	77.8%	87.9%	85.2%
Unconnected Impervious Area (UIA, %)	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
Receiving Pervious Area (RPA, %)	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	1.4%	0.2%	0.0%	0.0%
Separate Pervious Area (SPA, %)	0.0%	0.0%	5.0%	5.0%	0.0%	0.0%	0.0%	93.6%	95.0%	10.0%	31.7%	22.0%	12.1%	14.8%
A <sub>s</sub> (RPA / UIA)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
I <sub>s</sub> Check	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
f / I for WQCV Event:	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	0.6	3.2	3.2	9.8	3.2	3.2
f / I for 5-Year Event:	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.3	0.5	0.5	0.6	0.5	0.5
f / I for 100-Year Event:	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.2	0.4	0.4	0.6	0.4	0.4
f / I for Optional User Defined Storm CUHP:														
IRF for WQCV Event:	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
IRF for 5-Year Event:	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
IRF for 100-Year Event:	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
IRF for Optional User Defined Storm CUHP:														
Total Site Imperviousness: I <sub>total</sub>	100.0%	100.0%	95.0%	95.0%	100.0%	100.0%	100.0%	6.4%	5.0%	90.0%	66.9%	77.8%	87.9%	85.2%
Effective Imperviousness for WQCV Event:	100.0%	100.0%	95.0%	95.0%	100.0%	100.0%	100.0%	6.4%	5.0%	90.0%	66.9%	77.8%	87.9%	85.2%
Effective Imperviousness for 5-Year Event:	100.0%	100.0%	95.0%	95.0%	100.0%	100.0%	100.0%	6.4%	5.0%	90.0%	66.9%	77.8%	87.9%	85.2%
Effective Imperviousness for 100-Year Event:	100.0%	100.0%	95.0%	95.0%	100.0%	100.0%	100.0%	6.4%	5.0%	90.0%	66.9%	77.8%	87.9%	85.2%
Effective Imperviousness for Optional User Defined Storm CUHP:														

### LID / EFFECTIVE IMPERVIOUSNESS CREDITS

WQCV Event CREDIT: Reduce Detention By:	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
This line only for 10-Year Event	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
100-Year Event CREDIT**: Reduce Detention By:	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.1%	0.2%	0.2%	0.1%	0.0%	0.0%	0.0%	0.0%
User Defined CUHP CREDIT: Reduce Detention By:														

Total Site Imperviousness:	75.4%
Total Site Effective Imperviousness for WQCV Event:	75.4%
Total Site Effective Imperviousness for 5-Year Event:	75.4%
Total Site Effective Imperviousness for 100-Year Event:	75.4%
Total Site Effective Imperviousness for Optional User Defined Storm CUHP:	

**Notes:**  
 \* Use Green-Ampt average infiltration rate values from Table 3-3.  
 \*\* Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM.  
 \*\*\* Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed

## Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method

UD-BMP (Version 3.06, November 2016)

User Input		
Calculated cells		
---Design Storm: 1-Hour Rain Depth	WQCV Event	0.60 inches
---Minor Storm: 1-Hour Rain Depth	5-Year Event	1.50 inches
---Major Storm: 1-Hour Rain Depth	100-Year Event	2.52 inches
Optional User Defined Storm	CUHP	
(CUHP) NOAA 1 Hour Rainfall Depth and Frequency for User Defined Storm	100-Year Event	
Max Intensity for Optional User Defined Storm		0

**Designer:** Scott Brown  
**Company:** Galloway & Co.  
**Date:** December 20, 2018  
**Project:** Crest at Woodmen - MDDP Amendment  
**Location:** Colorado Springs, CO

**SITE INFORMATION (USER-INPUT)**

Sub-basin Identifier	B3-4	B4-1	B4-2	B5-1	B5-2	B5-3	B6	B7	B7-1	B8	B9	B9-1	B10	B11
Receiving Pervious Area Soil Type	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Loamy Sand	Sand	Loamy Sand	Loamy Sand	Loamy Sand
Total Area (ac., Sum of DCIA, UIA, RPA, & SPA)	0.920	1.690	0.870	0.510	0.550	0.160	3.030	2.510	0.550	0.900	0.960	0.720	1.050	1.650
Directly Connected Impervious Area (DCIA, acres)	0.828	1.606	0.827	0.434	0.474	0.141	2.727	0.961	0.028	0.683	0.684	0.648	0.918	1.290
Unconnected Impervious Area (UIA, acres)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Receiving Pervious Area (RPA, acres)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.016	0.016	0.000	0.000
Separate Pervious Area (SPA, acres)	0.092	0.085	0.044	0.076	0.076	0.019	0.303	1.549	0.523	0.217	0.260	0.056	0.132	0.360
RPA Treatment Type: Conveyance (C), Volume (V), or Permeable Pavement (PP)	V	V	V	V	V	V	V	V	V	V	V	V	V	V

**CALCULATED RESULTS (OUTPUT)**

Total Calculated Area (ac, check against input)	0.920	1.690	0.870	0.510	0.550	0.160	3.030	2.510	0.550	0.900	0.960	0.720	1.050	1.650
Directly Connected Impervious Area (DCIA, %)	90.0%	95.0%	95.0%	85.1%	86.2%	88.1%	90.0%	38.3%	5.0%	75.9%	71.3%	90.0%	87.4%	78.2%
Unconnected Impervious Area (UIA, %)	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
Receiving Pervious Area (RPA, %)	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	1.7%	2.2%	0.0%	0.0%
Separate Pervious Area (SPA, %)	10.0%	5.0%	5.0%	14.9%	13.8%	11.9%	10.0%	61.7%	95.0%	24.1%	27.0%	7.8%	12.6%	21.8%
A <sub>s</sub> (RPA / UIA)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
I <sub>s</sub> Check	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
f / I for WQCV Event:	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	9.8	3.2	3.2	3.2
f / I for 5-Year Event:	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.6	0.5	0.5	0.5
f / I for 100-Year Event:	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.6	0.4	0.4	0.4
<b>f / I for Optional User Defined Storm CUHP:</b>														
IRF for WQCV Event:	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
IRF for 5-Year Event:	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
IRF for 100-Year Event:	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
<b>IRF for Optional User Defined Storm CUHP:</b>														
Total Site Imperviousness: I <sub>total</sub>	90.0%	95.0%	95.0%	85.1%	86.2%	88.1%	90.0%	38.3%	5.0%	75.9%	71.3%	90.0%	87.4%	78.2%
Effective Imperviousness for WQCV Event:	90.0%	95.0%	95.0%	85.1%	86.2%	88.1%	90.0%	38.3%	5.0%	75.9%	71.3%	90.0%	87.4%	78.2%
Effective Imperviousness for 5-Year Event:	90.0%	95.0%	95.0%	85.1%	86.2%	88.1%	90.0%	38.3%	5.0%	75.9%	71.3%	90.0%	87.4%	78.2%
Effective Imperviousness for 100-Year Event:	90.0%	95.0%	95.0%	85.1%	86.2%	88.1%	90.0%	38.3%	5.0%	75.9%	71.3%	90.0%	87.4%	78.2%
<b>Effective Imperviousness for Optional User Defined Storm CUHP:</b>														

**LID / EFFECTIVE IMPERVIOUSNESS CREDITS**

WQCV Event CREDIT: Reduce Detention By:	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
This line only for 10-Year Event	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
100-Year Event CREDIT**: Reduce Detention By:	0.0%	0.0%	0.0%	0.1%	0.1%	0.2%	0.0%	0.0%	1.4%	0.0%	0.1%	0.0%	0.0%	0.0%
User Defined CUHP CREDIT: Reduce Detention By:														

Total Site Imperviousness:	76.2%
Total Site Effective Imperviousness for WQCV Event:	76.2%
Total Site Effective Imperviousness for 5-Year Event:	76.2%
Total Site Effective Imperviousness for 100-Year Event:	76.2%
Total Site Effective Imperviousness for Optional User Defined Storm CUHP:	

**Notes:**  
 \* Use Green-Ampt average infiltration rate values from Table 3-3.  
 \*\* Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM.  
 \*\*\* Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed

## Site-Level Low Impact Development (LID) Design Effective Impervious Calculator LID Credit by Impervious Reduction Factor (IRF) Method

UD-BMP (Version 3.06, November 2016)

User Input		
Calculated cells		
---Design Storm: 1-Hour Rain Depth	WQCV Event	0.60 inches
---Minor Storm: 1-Hour Rain Depth	5-Year Event	1.50 inches
---Major Storm: 1-Hour Rain Depth	100-Year Event	2.52 inches
Optional User Defined Storm	CUHP	
(CUHP) NOAA 1 Hour Rainfall Depth and Frequency for User Defined Storm	100-Year Event	
Max Intensity for Optional User Defined Storm		0

**Designer:** Scott Brown  
**Company:** Galloway & Co.  
**Date:** December 20, 2018  
**Project:** Crest at Woodmen - MDDP Amendment  
**Location:** Colorado Springs, CO

**SITE INFORMATION (USER-INPUT)**

Sub-basin Identifier	B11-1	B12	B12-1	OS1	OS2	OS3	OS4								
Receiving Pervious Area Soil Type	Loamy Sand	Loamy Sand	Loamy Sand	Sandy Clay Loam	Sandy Clay Loam	Sandy Clay Loam	Sandy Clay Loam	Loamy Sand	Loamy Sand	Loamy Sand	Sand	Loamy Sand	Loamy Sand	Loamy Sand	
Total Area (ac., Sum of DCIA, UIA, RPA, & SPA)	2.000	0.770	0.690	1.290	0.540	0.760	2.050								
Directly Connected Impervious Area (DCIA, acres)	0.100	0.687	0.621	1.196	0.217	0.447	0.654	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Unconnected Impervious Area (UIA, acres)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Receiving Pervious Area (RPA, acres)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.016	0.016	0.000	0.000	
Separate Pervious Area (SPA, acres)	1.900	0.083	0.069	0.094	0.323	0.313	1.396	0.000	0.000	0.000	(0.016)	(0.016)	0.000	0.000	
RPA Treatment Type: Conveyance (C), Volume (V), or Permeable Pavement (PP)	V	V	V	V	V	V	V	V	V	V	V	V	V	V	V

MISSING INPUT  
 MISSING INPUT  
 MISSING INPUT  
 MISSING INPUT  
 MISSING INPUT  
 MISSING INPUT  
 MISSING INPUT

**CALCULATED RESULTS (OUTPUT)**

Total Calculated Area (ac, check against input)	2.000	0.770	0.690	1.290	0.540	0.760	2.050								
Directly Connected Impervious Area (DCIA, %)	5.0%	89.2%	90.0%	92.7%	40.1%	58.8%	31.9%								
Unconnected Impervious Area (UIA, %)	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%								
Receiving Pervious Area (RPA, %)	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%								
Separate Pervious Area (SPA, %)	95.0%	10.8%	10.0%	7.3%	59.9%	41.2%	68.1%								
A <sub>s</sub> (RPA / UIA)	0.000	0.000	0.000	0.000	0.000	0.000	0.000								
I <sub>s</sub> Check	1.000	1.000	1.000	1.000	1.000	1.000	1.000								
f / I for WQCV Event:	3.2	3.2	3.2	0.6	0.6	0.6	0.6								
f / I for 5-Year Event:	0.5	0.5	0.5	0.3	0.3	0.3	0.3								
f / I for 100-Year Event:	0.4	0.4	0.4	0.2	0.2	0.2	0.2								
<span style="color: red;">f / I for Optional User Defined Storm CUHP:</span>															
IRF for WQCV Event:	0.00	0.00	0.00	0.00	0.00	0.00	0.00								
IRF for 5-Year Event:	1.00	1.00	1.00	1.00	1.00	1.00	1.00								
IRF for 100-Year Event:	1.00	1.00	1.00	1.00	1.00	1.00	1.00								
<span style="color: red;">IRF for Optional User Defined Storm CUHP:</span>															
Total Site Imperviousness: I <sub>total</sub>	5.0%	89.2%	90.0%	92.7%	40.1%	58.8%	31.9%								
Effective Imperviousness for WQCV Event:	5.0%	89.2%	90.0%	92.7%	40.1%	58.8%	31.9%								
Effective Imperviousness for 5-Year Event:	5.0%	89.2%	90.0%	92.7%	40.1%	58.8%	31.9%								
Effective Imperviousness for 100-Year Event:	5.0%	89.2%	90.0%	92.7%	40.1%	58.8%	31.9%								
<span style="color: red;">Effective Imperviousness for Optional User Defined Storm CUHP:</span>															

**LID / EFFECTIVE IMPERVIOUSNESS CREDITS**

WQCV Event CREDIT: Reduce Detention By:	N/A	N/A	N/A	N/A	N/A	N/A	N/A								
This line only for 10-Year Event	N/A	N/A	N/A	N/A	N/A	N/A	N/A								
100-Year Event CREDIT**: Reduce Detention By:	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%								
<span style="color: red;">User Defined CUHP CREDIT: Reduce Detention By:</span>															

Total Site Imperviousness:	48.4%
Total Site Effective Imperviousness for WQCV Event:	48.4%
Total Site Effective Imperviousness for 5-Year Event:	48.4%
Total Site Effective Imperviousness for 100-Year Event:	48.4%
Total Site Effective Imperviousness for Optional User Defined Storm CUHP:	

**Notes:**  
 \* Use Green-Ampt average infiltration rate values from Table 3-3.  
 \*\* Flood control detention volume credits based on empirical equations from Storage Chapter of USDCM.  
 \*\*\* Method assumes that 1-hour rainfall depth is equivalent to 1-hour intensity for calculation purposed



## COMPOSITE % IMPERVIOUS CALCULATIONS - HISTORIC

**Subdivision:** Looart Subdivision No. 6  
**Location:** CO, Colorado Springs

**Project Name:** The Crest at Woodmen - MDDP Amendment  
**Project No.:** RLM02.02  
**Calculated By:** SMB  
**Checked By:** JA  
**Date:** 9/12/18

Basin ID	Total Area (ac)	Paved Roads			Lawns			Roofs/Commercial			Basins Total Weighted % Imp.
		% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	
<b>Historic</b>											
W2a	11.95	100	0.42	3.56	5	11.52	4.80	90	0.00	0.00	8.4
W2b	2.56	100	1.45	56.90	5	1.10	2.20	90	0.00	0.00	59.1
W2c	1.56	100	0.00	0.00	5	0.00	0.00	90	1.56	90.00	90.0
W2d	5.07	100	2.50	49.35	5	2.57	2.50	90	0.00	0.00	51.9
W2e	4.23	100	2.71	64.09	5	1.52	1.80	90	0.00	0.00	65.9
W2f	4.76	100	0.00	0.00	5	0.00	0.00	90	4.76	90.00	90.0
W2g	10.13	100	4.34	42.87	5	5.79	2.90	90	0.00	0.00	45.8
W2h	3.49	100	0.34	9.76	5	3.15	4.50	90	0.00	0.00	14.3
W2i	5.28	100	2.59	49.07	5	2.69	2.50	90	0.00	0.00	51.6
W2j	0.74	100	0.00	0.00	5	0.00	0.00	90	0.74	90.00	90.0
W2k	0.55	100	0.00	0.00	5	0.00	0.00	90	0.55	90.00	90.0
W2l	6.01	100	0.00	0.00	5	0.00	0.00	90	6.01	90.00	90.0
W2m	10.49	100	2.03	19.35	5	8.46	4.00	90	0.00	0.00	23.4
W2n	10.27	100	2.38	23.22	5	7.88	3.80	90	0.00	0.00	27.0
W2o	4.09	100	0.00	0.00	5	4.09	5.00	90	0.00	0.00	5.0
OS3	2.12	100	0.63	29.72	5	1.49	3.50	90	0.00	0.00	33.2

## STANDARD FORM SF-2 TIME OF CONCENTRATION - HISTORIC

**Subdivision:** Looart Subdivion No. 6  
**Location:** CO, Colorado Springs

**Project Name:** The Crest at Woodmen - MDDP Amendment  
**Project No.:** RLM02.02  
**Calculated By:** SMB  
**Checked By:** JA  
**Date:** 9/12/18

SUB-BASIN DATA						INITIAL/OVERLAND (T <sub>i</sub> )			TRAVEL TIME (T <sub>t</sub> )					T <sub>c</sub> CHECK (URBANIZED BASINS)			FINAL T <sub>c</sub> (MIN)
BASIN ID	D.A. (AC)	Hydrologic Soils Group	Impervious (%)	C <sub>100</sub>	C <sub>5</sub>	L (FT)	S (%)	T <sub>i</sub> (MIN)	L (FT)	S (%)	C <sub>v</sub>	VEL. (FPS)	T <sub>t</sub> (MIN)	COMP. T <sub>c</sub> (MIN)	TOTAL LENGTH(FT)	Urbanized T <sub>c</sub> (MIN)	T <sub>c</sub> (MIN)
W2a	11.95	B	8.4	0.40	0.13	240	6.0	15.1	2005	1.8	15.0	2.0	16.8	32.0	2245.0	22.5	22.5
W2b	2.56	B	59.1	0.56	0.41	20	18.0	2.2	465	2.7	20.0	3.3	2.4	4.5	485.0	12.7	5.0
W2c	1.56	B	90.0	0.81	0.73												5.0
W2d	5.07	B	51.9	0.53	0.36	75	6.0	6.5	475	3.4	20.0	3.7	2.1	8.6	550.0	13.1	8.6
W2e	4.23	B	65.9	0.60	0.46	75	5.0	5.9	765	2.8	20.0	3.3	3.8	9.7	840.0	14.7	9.7
W2f	4.76	B	90.0	0.81	0.73												5.0
W2g	10.13	B	45.8	0.51	0.33	25	10.0	3.3	920	2.5	20.0	3.2	4.8	8.1	945.0	15.3	8.1
W2h	3.49	B	14.3	0.42	0.16	165	7.4	11.4	990	2.0	15.0	2.1	7.8	19.1	1155.0	16.4	16.4
W2i	5.28	B	51.6	0.53	0.36	195	24.0	6.6	240	3.3	15.0	2.7	1.5	8.0	435.0	12.4	8.0
W2j	0.74	B	90.0	0.81	0.73												5.0
W2k	0.55	B	90.0	0.81	0.73												5.0
W2l	6.01	B	90.0	0.81	0.73												5.0
W2m	10.49	B	23.4	0.45	0.22	40	14.0	4.2	965	4.0	15.0	3.0	5.4	9.6	1005.0	15.6	9.6
W2n	10.27	B	27.0	0.46	0.23	580	2.7	27.6	320	2.2	15.0	2.2	2.4	30.0	900.0	15.0	15.0
W2o	4.09	B	5.0	0.38	0.10	60	22.0	5.1	1000	3.0	15.0	2.6	6.4	11.5	1060.0	15.9	11.5
OS3	2.12	B	33.2	0.48	0.26	150	25.0	6.4	530	3.0	20.0	3.5	2.5	9.0	680.0	13.8	9.0
OS4	0.80	B	83.8	0.74	0.64												5.0

47.05

**NOTES:**

$T_i = (0.395 * (1.1 - C_5) * (L)^{0.5}) / ((S)^{0.33})$ , S in ft/ft

$T_t = L / 60V$  (Velocity From Fig. 501)

Velocity  $V = C_v * S^{0.5}$ , S in ft/ft

$T_c \text{ Check} = 10 + L / 180$

For Urbanized basins a minimum  $T_c$  of 5.0 minutes is required.

For non-urbanized basins a minimum  $T_c$  of 10.0 minutes is required

**STANDARD FORM SF-3**  
**STORM DRAINAGE SYSTEM DESIGN - HISTORIC**  
(RATIONAL METHOD PROCEDURE)

**Subdivision:** Looart Subdivion No. 6  
**Location:** CO, Colorado Springs  
**Design Storm:** 5-Year

**Project Name:** The Crest at Woodmen - MDDP Amendment  
**Project No.:** RLM02.02  
**Calculated By:** SMB  
**Checked By:** JA  
**Date:** 9/12/18

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET	PIPE			TRAVEL TIME			REMARKS	
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)		Tt (min)
	a	W2a	11.95	0.13	22.5	1.55	2.91	4.5													
	b	W2b	2.56	0.41	5.0	1.05	5.17	5.4													
	c	W2c	1.56	0.73	5.0	1.14	5.17	5.9													
	d	W2d	5.07	0.36	8.6	1.82	4.35	7.9													
	e	W2e	4.23	0.46	9.7	1.95	4.17	8.1													
	f	W2f	4.76	0.73	5.0	3.47	5.17	17.9													
	g	W2g	10.13	0.33	8.1	3.34	4.44	14.8	22.5	14.32	2.91	41.7									Basins W2a-W2g
	h	W2h	3.49	0.16	16.4	0.56	3.39	1.9													
	i	W2i	5.28	0.36	8.0	1.90	4.46	8.5													
	j	W2j	0.74	0.73	5.0	0.54	5.17	2.8													
	k	W2k	0.55	0.73	5.0	0.40	5.17	2.1													
	l	W2l	6.01	0.73	5.0	4.39	5.17	22.7													
		OS3	2.12	0.26	9.0	0.55	4.29	2.4													
		OS4	0.80	0.64	5.0	0.51	5.17	2.6	9.0	1.06	4.29	4.5									Basins OS3-OS4

**STANDARD FORM SF-3**  
**STORM DRAINAGE SYSTEM DESIGN - HISTORIC**  
(RATIONAL METHOD PROCEDURE)

**Subdivision:** Looart Subdivion No. 6  
**Location:** CO, Colorado Springs  
**Design Storm:** 5-Year

**Project Name:** The Crest at Woodmen - MDDP Amendment  
**Project No.:** RLM02.02  
**Calculated By:** SMB  
**Checked By:** JA  
**Date:** 9/12/18

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	
	m	W2m	10.49	0.22	9.6	2.31	4.19	9.7													
	n	W2n	10.27	0.23	15.0	2.36	3.52	8.3	16.4	13.52	3.39	45.8									Basins W2a-W2n, OS3-OS4
	o	W2o	4.09	0.10	11.5	0.41	3.92	1.6													

**STANDARD FORM SF-3**  
**STORM DRAINAGE SYSTEM DESIGN - HISTORIC**  
(RATIONAL METHOD PROCEDURE)

**Subdivision:** Looart Subdivion No. 6  
**Location:** CO, Colorado Springs  
**Design Storm:** 100-Year

**Project Name:** The Crest at Woodmen - MDDP Amendment  
**Project No.:** RLM02.02  
**Calculated By:** SMB  
**Checked By:** JA  
**Date:** 9/12/18

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	
	a	W2a	11.95	0.40	22.5	4.78	4.89	23.4													
	b	W2b	2.56	0.56	5.0	1.43	8.68	12.4													
	c	W2c	1.56	0.81	5.0	1.27	8.68	11.0													
	d	W2d	5.07	0.53	8.6	2.69	7.31	19.7													
	e	W2e	4.23	0.60	9.7	2.54	7.00	17.8													
	f	W2f	4.76	0.81	5.0	3.85	8.68	33.4													
	g	W2g	10.13	0.51	8.1	5.17	7.46	38.6	22.5	21.73	4.89	106.3									Basins W2a-W2g
	h	W2h	3.49	0.42	16.4	1.47	5.68	8.3													
	i	W2i	5.28	0.53	8.0	2.80	7.48	20.9													
	j	W2j	0.74	0.81	5.0	0.60	8.68	5.2													
	k	W2k	0.55	0.81	5.0	0.45	8.68	3.9													
	l	W2l	6.01	0.81	5.0	4.87	8.68	42.3													
		OS3	2.12	0.48	9.0	1.02	7.20	7.3													
		OS4	0.80	0.74	5.0	0.59	8.68	5.1	9.0	1.61	7.20	11.6									Basins OS3-OS4

**STANDARD FORM SF-3**  
**STORM DRAINAGE SYSTEM DESIGN - HISTORIC**  
(RATIONAL METHOD PROCEDURE)

**Subdivision:** Looart Subdivion No. 6  
**Location:** CO, Colorado Springs  
**Design Storm:** 100-Year

**Project Name:** The Crest at Woodmen - MDDP Amendment  
**Project No.:** RLM02.02  
**Calculated By:** SMB  
**Checked By:** JA  
**Date:** 9/12/18

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	
	m	W2m	10.49	0.45	9.6	4.72	7.04	33.2													
	n	W2n	10.27	0.46	15.0	4.72	5.91	27.9	16.4	21.24	5.68	120.6									Basins W2a-W2n, OS3-OS4
	o	W2o	4.09	0.38	11.5	1.55	6.58	10.2													

## COMPOSITE % IMPERVIOUS CALCULATIONS - PROPOSED

**Subdivision:** Realm Realty  
**Location:** CO, Colorado Springs

**Project Name:** Crest at Woodmen - MDDP AMENDMENT  
**Project No.:** RLM 2.02  
**Calculated By:** CMV  
**Checked By:** SMB  
**Date:** 1/11/19

Basin ID	Total Area (ac)	Paved Roads			Lawns			Roofs/Commercial			Basins Total Weighted % Imp.
		% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	
B1-1	1.32	100	0.00	0.0	5	1.32	5.0	90	0.00	0.0	5.0
B1-2	0.38	100	0.00	0.0	5	0.00	0.0	90	0.38	90.0	90.0
B2	1.15	100	0.75	65.2	5	0.40	1.7	90	0.00	0.0	66.9
B3-1	7.34	100	5.62	76.6	5	1.72	1.2	90	0.00	0.0	77.8
B3-2	1.31	100	1.14	87.3	5	0.17	0.6	90	0.00	0.0	87.9
B3-3	0.64	100	0.54	84.4	5	0.10	0.8	90	0.00	0.0	85.2
B3-4	0.92	100	0.00	0.0	5	0.00	0.0	90	0.92	90.0	90.0
B4-1	1.69	100	0.00	0.0	5	0.00	0.0	95	1.69	95.0	95.0
B4-2	0.87	100	0.00	0.0	5	0.00	0.0	95	0.87	95.0	95.0
B5-1	0.51	100	0.43	84.3	5	0.08	0.8	90	0.00	0.0	85.1
B5-2	0.55	100	0.47	85.5	5	0.08	0.7	90	0.00	0.0	86.2
B5-3	0.16	100	0.14	87.5	5	0.02	0.6	90	0.00	0.0	88.1
B6	3.03	100	0.00	0.0	5	0.00	0.0	90	3.03	90.0	90.0
B7	2.51	100	0.88	35.1	5	1.63	3.2	90	0.00	0.0	38.3
B7-1	0.55	100	0.00	0.0	5	0.55	5.0	90	0.00	0.0	5.0
B8	0.90	100	0.67	74.4	6	0.23	1.5	90	0.00	0.0	75.9
B9	0.96	100	0.67	69.8	5	0.29	1.5	90	0.00	0.0	71.3
B9-1	0.72	100	0.00	0.0	5	0.00	0.0	90	0.72	90.0	90.0
B10	1.05	100	0.91	86.7	5	0.14	0.7	90	0.00	0.0	87.4
B11	1.65	100	1.03	62.4	5	0.35	1.1	90	0.27	14.7	78.2
B11-1	2.00	100	0.00	0.0	5	2.00	5.0	90	0.00	0.0	5.0
B12	0.77	100	0.53	68.8	5	0.07	0.5	90	0.17	19.9	89.2
B12-1	0.69	100	0.00	0.0	5	0.00	0.0	90	0.69	90.0	90.0
OS1	1.29	100	1.19	92.3	5	0.10	0.4	90	0.00	0.0	92.7
OS2	0.54	100	0.20	37.0	5	0.34	3.1	90	0.00	0.0	40.1
OS3	0.76	100	0.43	56.6	5	0.33	2.2	90	0.00	0.0	58.8
OS4	2.05	100	0.58	28.3	5	1.47	3.6	90	0.00	0.0	31.9
A1	2.47	100	0.00	0.0	5	0.00	0.0	95	2.47	95.0	95.0

Basin ID	Total Area (ac)	Paved Roads			Lawns			Roofs/Commercial			Basins Total Weighted % Imp.
		% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	% Imp.	Area (ac)	Weighted % Imp.	
A2	2.48	100	1.13	45.6	5	1.19	2.4	90	0.16	5.8	53.8
A3	3.81	100	2.86	75.1	5	0.68	0.9	90	0.27	6.4	82.4
A4	3.44	100	2.01	58.4	5	0.00	0.0	90	1.43	37.4	95.8
A5	0.33	100	0.33	100.0	5	0.00	0.0	90	0.00	0.0	100.0
A6	3.33	100	0.00	0.0	5	0.00	0.0	95	3.33	95.0	95.0
A7	2.86	100	1.44	50.4	5	0.00	0.0	90	1.42	44.7	95.1
A8	0.60	100	0.60	100.0	5	0.00	0.0	90	0.00	0.0	100.0
A9	1.33	100	0.80	60.2	5	0.00	0.0	95	0.53	37.9	98.1
A10	2.75	100	1.32	48.0	5	0.00	0.0	90	1.43	46.8	94.8
A11	3.80	100	1.83	48.2	5	0.00	0.0	90	1.97	46.7	94.9
A12	0.24	100	0.24	100.0	5	0.00	0.0	90	0.00	0.0	100.0
A13	5.00	100	0.00	0.0	5	0.00	0.0	95	5.00	95.0	95.0
A14	0.05	100	0.05	100.0	5	0.00	0.0	90	0.00	0.0	100.0
A15	1.09	100	1.09	100.0	5	0.00	0.0	90	0.00	0.0	100.0
A16	1.21	100	1.21	100.0	5	0.00	0.0	90	0.00	0.0	100.0
A17	5.24	100	0.00	0.0	5	0.00	0.0	95	5.24	95.0	95.0
A18	4.12	100	0.00	0.0	5	0.00	0.0	95	4.12	95.0	95.0
A19	0.69	100	0.69	100.0	5	0.00	0.0	90	0.00	0.0	100.0
A20	1.06	100	1.06	100.0	5	0.00	0.0	90	0.00	0.0	100.0
A21	0.45	100	0.45	100.0	5	0.00	0.0	90	0.00	0.0	100.0
A22	3.45	100	0.05	1.5	5	3.40	4.9	90	0.00	0.0	6.4



## STANDARD FORM SF-2 TIME OF CONCENTRATION - PROPOSED

**Subdivision:** Realm Realty  
**Location:** CO, Colorado Springs

**Project Name:** Crest at Woodmen - MDDP AMENDMENT  
**Project No.:** RLM 2.02  
**Calculated By:** CMV  
**Checked By:** SMB  
**Date:** 1/11/19

SUB-BASIN DATA						INITIAL/OVERLAND (T <sub>i</sub> )			TRAVEL TIME (T <sub>i</sub> )					T <sub>c</sub> CHECK (URBANIZED BASINS)			FINAL
BASIN ID	D.A. (AC)	Hydrologic Soils Group	Impervious (%)	C <sub>100</sub>	C <sub>5</sub>	L (FT)	S (%)	T <sub>i</sub> (MIN)	L (FT)	S (%)	C <sub>v</sub>	VEL. (FPS)	T <sub>i</sub> (MIN)	COMP. T <sub>c</sub> (MIN)	TOTAL LENGTH(FT)	Urbanized T <sub>c</sub> (MIN)	T <sub>c</sub> (MIN)
B1-1	1.32	D	5.0	0.52	0.18	80	8.0	7.5	300	5.0	15.0	3.4	1.5	9.0	380.0	12.1	9.0
B1-2	0.38	B	90.0	0.81	0.73												10.0
B2	1.15	B	66.9	0.60	0.46	50	8.0	4.1	700	3.5	20.0	3.7	3.1	7.3	750.0	14.2	7.3
B3-1	7.34	A	77.8	0.63	0.54	100	25.0	3.5	750	2.0	20.0	2.8	4.4	7.9	850.0	14.7	7.9
B3-2	1.31	B	87.9	0.78	0.70	50	2.0	4.1	200	4.0	20.0	4.0	0.8	4.9	250.0	11.4	5.0
B3-3	0.64	B	85.2	0.75	0.66	50	25.0	1.9	150	4.0	20.0	4.0	0.6	2.6	200.0	11.1	5.0
B3-4	0.92	B	90.0	0.81	0.73												10.0
B4-1	1.69	B	95.0	0.88	0.81	80	2.0	3.8	280	2.0	20.0	2.8	1.6	5.4	360.0	12.0	5.4
B4-2	0.87	B	95.0	0.88	0.81	25	2.0	2.1	475	2.0	20.0	2.8	2.8	4.9	500.0	12.8	5.0
B5-1	0.51	B	85.1	0.75	0.66	20	2.0	2.9	500	4.2	20.0	4.1	2.0	4.9	520.0	12.9	5.0
B5-2	0.55	B	86.2	0.76	0.67	10	2.0	2.0	250	2.0	20.0	2.8	1.5	3.4	260.0	11.4	5.0
B5-3	0.16	B	88.1	0.79	0.70	10	2.0	1.8	140	2.0	20.0	2.8	0.8	2.7	150.0	10.8	5.0
B6	3.03	B	90.0	0.81	0.73												5.0
B7	2.51	B	38.3	0.49	0.29	25	2.0	5.9	360	3.0	20.0	3.5	1.7	7.6	385.0	12.1	7.6
B7-1	0.55	B	5.0	0.38	0.10	90	10.0	8.1	130	2.5	20.0	3.2	0.7	8.8	220.0	11.2	8.8
B8	0.90	B	75.9	0.66	0.55	20	2.0	3.6	500	4.2	20.0	4.1	2.0	5.6	520.0	12.9	5.6
B9	0.96	B	71.3	0.63	0.50	100	1.5	9.6	570	0.5	20.0	1.4	6.7	16.3	670.0	13.7	13.7
B9-1	0.72	B	90.0	0.81	0.73												5.0
B10	1.05	B	87.4	0.78	0.69	15	2.0	2.3	450	3.0	20.0	3.5	2.2	4.5	465.0	12.6	5.0
B11	1.65	B	78.2	0.68	0.57	50	2.0	5.4	380	3.0	20.0	3.5	1.8	7.3	430.0	12.4	7.3
B11-1	2.00	B	5.0	0.38	0.10	85	8.0	8.4	220	3.0	20.0	3.5	1.1	9.5	305.0	11.7	9.5
B12	0.77	B	89.2	0.80	0.72	10	1.0	2.2	325	3.0	20.0	3.5	1.6	3.8	335.0	11.9	5.0
B12-1	0.69	B	90.0	0.81	0.73												5.0
OS1	1.29	D	92.7	0.86	0.78	100	20.0	2.2	300	5.0	20.0	4.5	1.1	3.3	400.0	12.2	5.0
OS2	0.54	D	40.1	0.58	0.35	20	2.0	4.9	280	4.5	20.0	4.2	1.1	6.0	300.0	11.7	6.0
OS3	0.76	D	58.8	0.63	0.45	100	18.0	4.5	400	5.0	20.0	4.5	1.5	6.0	500.0	12.8	6.0
OS4	2.05	D	31.9	0.57	0.31	100	25.0	5.0	560	3.0	20.0	3.5	2.7	7.6	660.0	13.7	7.6
OS5	0.80	B	95.0	0.88	0.81												5.0
A1	2.47	B	95.0	0.88	0.81	100	5.0	3.1	440	3.0	20.0	3.5	2.1	5.2	540.0	13.0	5.2
A2	2.48	B	53.8	0.54	0.37	100	2.0	10.6	660	5.0	20.0	4.5	2.5	13.1	760.0	14.2	13.1
A3	3.81	B	82.4	0.72	0.62	90	6.0	4.6	525	1.0	20.0	2.0	4.4	9.0	615.0	13.4	9.0
A4	3.44	B	95.8	0.89	0.82	60	20.0	1.5	490	4.0	20.0	4.0	2.0	3.5	550.0	13.1	5.0
A5	0.33	B	100.0	0.96	0.90	10	1.0	1.2	700	3.0	20.0	3.5	3.4	4.5	710.0	13.9	5.0
A6	3.33	B	95.0	0.88	0.81	10	2.0	1.3	250	4.0	20.0	4.0	1.0	2.4	260.0	11.4	5.0
A7	2.86	B	95.1	0.88	0.81	10	1.0	1.7	550	1.5	20.0	2.4	3.7	5.4	560.0	13.1	5.4
A8	0.60	B	100.0	0.96	0.90	10	1.0	1.2	300	1.2	20.0	2.2	2.3	3.4	310.0	11.7	5.0
A9	1.33	B	98.1	0.92	0.86	10	1.0	1.4	250	0.5	20.0	1.4	2.9	4.3	260.0	11.4	5.0
A10	2.75	B	94.8	0.87	0.80	10	1.0	1.7	460	2.0	20.0	2.8	2.7	4.4	470.0	12.6	5.0
A11	3.80	B	94.9	0.88	0.80	10	1.0	1.7	350	2.2	20.0	3.0	2.0	3.7	360.0	12.0	5.0
A12	0.24	B	100.0	0.96	0.90	100	1.0	3.7	580	1.5	20.0	2.4	3.9	7.6	680.0	13.8	7.6
A13	5.00	B	95.0	0.88	0.81	100	1.0	5.3	650	2.0	20.0	2.8	3.8	9.1	750.0	14.2	9.1
A14	0.05	B	100.0	0.96	0.90	10	1.0	1.2	20	0.5	20.0	1.4	0.2	1.4	30.0	10.2	5.0
A15	1.09	B	100.0	0.96	0.90	30	1.0	2.0	275	4.0	20.0	4.0	1.1	3.2	305.0	11.7	5.0

**STANDARD FORM SF-2**  
**TIME OF CONCENTRATION - PROPOSED**

**Subdivision:** Realm Realty  
**Location:** CO, Colorado Springs

**Project Name:** Crest at Woodmen - MDDP AMENDMENT  
**Project No.:** RLM 2.02  
**Calculated By:** CMV  
**Checked By:** SMB  
**Date:** 1/11/19

SUB-BASIN						INITIAL/OVERLAND			TRAVEL TIME					Tc CHECK			FINAL
DATA						(T <sub>i</sub> )			(T <sub>p</sub> )					(URBANIZED BASINS)			
BASIN ID	D.A. (AC)	Hydrologic Soils Group	Impervious (%)	C <sub>100</sub>	C <sub>5</sub>	L (FT)	S (%)	T <sub>i</sub> (MIN)	L (FT)	S (%)	C <sub>v</sub>	VEL. (FPS)	T <sub>i</sub> (MIN)	COMP. T <sub>c</sub> (MIN)	TOTAL LENGTH(FT)	Urbanized T <sub>c</sub> (MIN)	
A16	1.21	B	100.0	0.96	0.90	10	1.0	1.2	535	1.5	20.0	2.4	3.6	4.8	545.0	13.0	5.0
A17	5.24	B	95.0	0.88	0.81	100	4.0	3.3	620	2.0	20.0	2.8	3.7	7.0	720.0	14.0	7.0
A18	4.12	B	95.0	0.88	0.81	10	1.0	1.7	625	2.0	20.0	2.8	3.7	5.4	635.0	13.5	5.4
A19	0.69	B	100.0	0.96	0.90	10	1.0	1.2	90	2.0	20.0	2.8	0.5	1.7	100.0	10.6	5.0
A20	1.06	B	100.0	0.96	0.90	10	1.0	1.2	255	2.3	20.0	3.0	1.4	2.6	265.0	11.5	5.0
A21	0.45	B	100.0	0.96	0.90	10	1.0	1.2	180	1.5	20.0	2.4	1.2	2.4	190.0	11.1	5.0
A22	3.45	B	6.35	0.39	0.11	50	25.0	4.4	450	2.0	20.0	2.8	2.7	7.0	500.0	12.8	7.0

**NOTES:**

$T_i = (0.395 * (1.1 - C_5) * (L)^{0.5}) / ((S)^{0.33})$ , S in ft/ft

$T_i = L / 60V$  (Velocity From Fig. 501)

Velocity  $V = C_v * S^{0.5}$ , S in ft/ft

Tc Check =  $10 + L / 180$

For Urbanized basins a minimum T<sub>c</sub> of 5.0 minutes is required.

For non-urbanized basins a minimum T<sub>c</sub> of 10.0 minutes is required

**STANDARD FORM SF-3**  
**STORM DRAINAGE SYSTEM DESIGN - PROPOSED**  
(RATIONAL METHOD PROCEDURE)

Subdivision: Realm Realty  
Location: CO, Colorado Springs  
Design Storm: 5-Year

Project Name: Crest at Woodmen - MDDP AMENDMENT  
Project No.: RLM 2.02  
Calculated By: CMV  
Checked By: SMB  
Date: 1/11/19

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	
	1A	B1-2	0.38	0.73	10.0	0.28	4.13	1.2													Runoff from roof - flows to Campus Dr. Stm inlet #8
	1B	B1-1	1.32	0.18	9.0	0.24	4.28	1.0													Flow to Campus Dr. - Stm inlet #8
									10.0	0.52	4.13	2.1									(DP 1A & 1B)
	2A	B11-1	2.00	0.10	9.5	0.20	4.21	0.8													Flow to Phase 2/3 East - Stm inlet 2A
	2B	B11	1.65	0.57	7.3	0.94	4.61	4.3													Flow to Phase 2/3 East - Stm inlet 2B
East MH-28									9.5	1.14	4.21	4.8									(DP 2A & 2B)
	2C	B12	0.77	0.72	5.0	0.55	5.17	2.8													Flow to Phase 2/3 East - Stm inlet 2C
East MH-25									9.5	1.69	4.21	7.1									DP 2B & 2C
	2	B12-1	0.69	0.73	5.0	0.50	5.17	2.6													Roof drain enters at DP 2
									9.5	2.19	4.21	9.2									DP 2C & 2
Campus - MH 12	3								10.0	2.71	4.13	11.2									(DP 1B & 2)
	4	B10	1.05	0.69	5.0	0.72	5.17	3.7													Campus Dr. - Stm inlet #5
	5	B2	1.15	0.46	7.3	0.53	4.61	2.4													Campus Dr. - Stm inlet #4 (includes DP2 & 3)
Campus - MH 14	6								10.0	3.96	4.13	16.4									(DP 1, 2, 3, 4, 5)
	7A	B9-1	0.72	0.73	5.0	0.53	5.17	2.7													Roof drain
	7B	B9	0.96	0.50	13.7	0.48	3.65	1.8													Flow to Phase 2/3 East - Stm inlet 9
East Stm Inlet 9 total Flow									13.7	1.01	3.65	3.7									(DP 7A & 7B)
Campus MH 38	7								13.7	4.97	3.65	18.1									(DP 6 & 7B)
	8	B3-4	0.92	0.73	10.0	0.67	4.13	2.8													Roof drain
	8A	B3-2	1.31	0.70	5.0	0.92	5.17	4.8													Flows to Phase 1 West - Stm inlet #4A
West Stm Inlet 4A total flow									10.0	1.59	4.13	6.6									(DP 8 & 8A)
	8B	B3-3	0.64	0.66	5.0	0.42	5.17	2.2													Flows to Phase 1 West - Stm inlet #4B
West MH 9	9								10.0	2.01	4.13	8.3									(DP 8A, 8B)
Campus MH 15	10								13.7	6.98	3.65	25.5									(DP 7 & 9)
	14	OS4	2.05	0.31	7.6	0.64	4.53	2.9													Flows to Stm West MH 1
		OS5	0.80	0.81	5.0	0.65	5.17	3.4													In Ex. 60" Storm Pipe coming from Nissan Dealership

**STANDARD FORM SF-3**  
**STORM DRAINAGE SYSTEM DESIGN - PROPOSED**  
(RATIONAL METHOD PROCEDURE)

Subdivision: Realm Realty  
Location: CO, Colorado Springs  
Design Storm: 5-Year

Project Name: Crest at Woodmen - MDDP AMENDMENT  
Project No.: RLM 2.02  
Calculated By: CMV  
Checked By: SMB  
Date: 1/11/19

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	
West MH 1	15								7.6	1.29	4.53	5.8									(DP 14 & OS5)
	16	B3-1	7.34	0.54	7.9	3.96	4.48	17.7													Flows to Phase 1 West - Stm inlet 16
West MH 5	17								7.9	5.25	4.48	23.5									(DP 15 & 16)
	18	B4-2	0.87	0.81	5.0	0.70	5.17	3.6													
West MH 3									7.9	5.95	4.48	26.7									(DP 17 & 18)
	11	B5-1	0.51	0.66	5.0	0.34	5.17	1.8													Flows to Campus Stm inlet 6
Campus Stm Inlet 6 total Flow									7.9	6.29	4.48	28.2									(DP 19 & 11)
	12	B8	0.90	0.55	5.6	0.50	5.00	2.5													Flows to Campus Stm inlet 7
Campus Stm inlet 7 total flow									7.9	6.79	4.48	30.4									(DP 11 & 12)
	13	B4-1	1.69	0.81	5.4	1.37	5.05	6.9													Flows to Campus storm stub
Campus - MH 17	19								13.7	15.14	3.65	55.3									Flows to Pond B (DP 10, 12, 13)
	20	OS1	1.29	0.78	5.0	1.01	5.17	5.2													Flows to ex. Woodmen Rd inlet
	21	OS2	0.54	0.35	6.0	0.19	4.90	0.9													Flows to Campus Stm inlet 3
	22	OS3	0.76	0.45	6.0	0.34	4.89	1.7													Flows to Campus Stm inlet 1
Ex. Stm MH V10									6.0	1.54	4.89	7.5									
	23	B5-2	0.55	0.67	5.0	0.37	5.17	1.9													Flows to Ex. Inlet in Vincent northwest of Campus/Vincent Roundabout
	24	B5-3	0.16	0.70	5.0	0.11	5.17	0.6													Flows to Ex. Inlet in Vincent southeast of Campus/Vincent Roundabout
	25	B6	3.03	0.73	5.0	2.21	5.17	11.4													
	26A	B7-1	0.55	0.10	8.8	0.06	4.33	0.3													Flows to Phase 2/3 East - Stm inlet 27A
East Stm Inlet 27A total Flow									8.8	2.27	4.33	9.8									(DP 26 & 27A)
	26	B7	2.51	0.29	7.6	0.73	4.54	3.3													Flows to Phase 2/3 East - Stm inlet 27
East Stm Inlet 27 total Flow									8.8	3.00	4.33	13.0									Flows to Pond B (DP 27A & 27)

**STANDARD FORM SF-3**  
**STORM DRAINAGE SYSTEM DESIGN - PROPOSED**  
(RATIONAL METHOD PROCEDURE)

Subdivision: Realm Realty  
Location: CO, Colorado Springs  
Design Storm: 5-Year

Project Name: Crest at Woodmen - MDDP AMENDMENT  
Project No.: RLM 2.02  
Calculated By: CMV  
Checked By: SMB  
Date: 1/11/19

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS	
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C* A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C* A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)		
	50	A1	2.47	0.81	5.2	2.00	5.10	10.2													Flows to future Stm inlet	
	51A	A6	3.33	0.81	5.0	2.70	5.17	14.0													Flows to future Stm inlet	
	51								5.2	4.70	5.1	24									(DP 50 & 51A)	
	52											151.1									Offsite Flow of 151.1 cfs	
Stm East MH 4	53								5.2	4.7	5.1	175.1									(DP 51 & 52)	
	54A	A2	2.48	0.37	13.1	0.92	3.73	3.4					1.5	0.1		3.3	0.5	18	550	2.45	3.742	Bypass to DP 60A Flows to inlet 54A
	54B	A5	0.33	0.90	5.0	0.30	5.17	1.6														Flows to inlet 54B
	54								13.1	5.58	3.73	171.9										(DP 53, 54A, 54B)
	55A	A9	1.33	0.86	5.0	1.14	5.17	5.9														Flows to future Stm inlet
	55								13.1	6.72	3.73	176.2										(DP 54 & 55A)
	56A	A11	3.80	0.80	5.0	3.04	5.17	15.7														Flows to inlet 56A
	56B	A12	0.24	0.90	7.6	0.22	4.54	1.0														Flow to inlet 56B
	56C	A13	5.00	0.81	9.1	4.05	4.26	17.3														Flows to future Stm inlet
Stm East MH 7	56								13.1	13.81	3.73	202.6										(DP 55, 56A, 56B, & 56C)
	57A	A16	1.21	0.90	5.0	1.09	5.17	5.6														Flows to inlet 57A
	57								13.1	14.905	3.73	206.7										(DP 56 & 57A)
	58	A3	3.81	0.62	9.0	2.36	4.29	10.1														Flows to inlet 58
	59A	A4	3.44	0.82	5.0	2.82	5.17	14.6														Flows to inlet 59A
	59								9.0	5.18	4.29	22.2										(DP 58 & 59A)
	60A	A7	2.86	0.81	5.4	2.32	5.05	11.7														Flows to inlet 60A
	60								16.8	7.54	3.35	25.2										(DP 59 & 60A)
	61A	A8	0.60	0.90	5.0	0.54	5.17	2.8														Flows to inlet 61A
Stm East MH 11	61								16.8	8.08	3.35	27.1										(DP 60 & 61A)
	62A	A10	2.75	0.80	5.0	2.20	5.17	11.4														Flows to inlet 62A
	62								16.8	10.28	3.35	34.4										(DP 61 & 62A)
	63A	A14	0.05	0.90	5.0	0.04	5.17	0.2														Flows into inlets 63A & 63B

**STANDARD FORM SF-3**  
**STORM DRAINAGE SYSTEM DESIGN - PROPOSED**  
(RATIONAL METHOD PROCEDURE)

Subdivision: Realm Realty  
Location: CO, Colorado Springs  
Design Storm: 5-Year

Project Name: Crest at Woodmen - MDDP AMENDMENT  
Project No.: RLM 2.02  
Calculated By: CMV  
Checked By: SMB  
Date: 1/11/19

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C% A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C% A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	
	63								16.8	10.32	3.35	34.6									(DP 62 & 63A)
	64								16.8	25.22	3.35	235.6									(DP 57 & 63)
	65A	A15	1.09	0.90	5.0	0.98	5.17	5.1													Flows to inlet 65A
	65								16.8	26.20	3.35	238.9									(DP 64 & 65A)
	66A	A17	5.24	0.81	7.0	4.24	4.66	19.8													Flows to future Stm inlet
	66B	A18	4.12	0.81	5.4	3.34	5.06	16.9													Flows to future Stm inlet
Future Stm MH	66C								7.0	7.58	4.66	35.3									(DP 66A & 66B)
Stm East MH 15	66								16.8	33.78	3.35	264.3									(DP 65 & 66C)
	67A	A20	1.06	0.90	5.0	0.95	5.17	4.9													Flows to inlet 67A
	67								16.8	34.73	3.35	267.4									(DP 66 & 67A)
	68A	A19	0.69	0.90	5.0	0.62	5.17	3.2													Flows to inlet 68A
Stm East MH 16	68								16.8	35.35	3.35	269.5									(DP 67, 68A)
	69A	A21	0.45	0.90	5.0	0.40	5.17	2.1													Flows to inlet 69A
Stm East MH 16	69								16.8	35.75	3.35	270.9									(DP 68 & 69A)
	70	A22	3.45	0.11	7.0	0.38	4.66	1.8	16.8	36.13	3.35	272.1									Pond A

**STANDARD FORM SF-3**  
**STORM DRAINAGE SYSTEM DESIGN - PROPOSED**  
(RATIONAL METHOD PROCEDURE)

**Subdivision:** Realm Realty  
**Location:** CO, Colorado Springs  
**Design Storm:** 100-Year

**Project Name:** Crest at Woodmen - MDDP AMENDMENT  
**Project No.:** RLM 2.02  
**Calculated By:** CMV  
**Checked By:** SMB  
**Date:** 1/11/19

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	
	1A	B1-2	0.38	0.81	10.0	0.31	6.93	2.1													Runoff from roof - flows to Campus Dr. Stm inlet #8
	1B	B1-1	1.32	0.52	9.0	0.69	7.19	5.0													Flow to Campus Dr. - Stm inlet #8
									10.0	1.00	6.93	6.9									(DP 1A & 1B)
	2A	B11-1	2.00	0.38	9.5	0.76	7.06	5.4													Flow to Phase 2/3 East - Stm inlet 2A
	2B	B11	1.65	0.68	7.3	1.12	7.73	8.7													Flow to Phase 2/3 East - Stm inlet 2B
Stm MH-28									9.5	1.88	7.06	13.3									(DP 2A & 2B)
	2C	B12	0.77	0.80	5.0	0.62	8.68	5.4													Flow to Phase 2/3 East - Stm inlet 2C
Stm MH-25									9.5	2.50	7.06	17.7									DP 2B & 2C
	2	B12-1	0.69	0.81	5.0	0.56	8.68	4.9													Roof drain enters at DP 2
									9.5	3.06	7.06	21.6									DP 2C & 2
Campus - MH 12	3								10.0	4.06	6.93	28.1									(DP 1B & 2)
	4	B10	1.05	0.78	5.0	0.82	8.68	7.1													Campus Dr. - Stm inlet #5
	5	B2	1.15	0.60	7.3	0.69	7.74	5.3													Campus Dr. - Stm inlet #4 (includes DP2 & 3)
Campus - MH 14	6								10.0	5.57	6.93	38.6									(DP 1, 2, 3, 4, 5)
	7A	B9-1	0.72	0.81	5.0	0.58	8.68	5.0													Roof drain
	7B	B9	0.96	0.63	13.7	0.60	6.14	3.7													Flow to Phase 2/3 East - Stm inlet 9
East Stm Inlet 9 total Flow									13.7	1.18	6.14	7.2									(DP 7A & 7B)
Campus MH 38	7								13.7	6.75	6.14	41.4									(DP 6 & 7B)
	8	B3-4	0.92	0.81	10.0	0.75	6.93	5.2													Roof drain
	8A	B3-2	1.31	0.78	5.0	1.02	8.68	8.9													Flows to Phase 1 West - Stm inlet #4A
									10.0	1.77	6.93	12.3									(DP 8 & 8A)
	8B	B3-3	0.64	0.75	5.0	0.48	8.68	4.2													Flows to Phase 1 West - Stm inlet #4B
West MH 9	9								10.0	2.25	6.93	15.6									(DP 8A, 8B)
Campus MH 15	10								13.7	9.00	6.14	55.3									(DP 7 & 9)

**STANDARD FORM SF-3**  
**STORM DRAINAGE SYSTEM DESIGN - PROPOSED**  
(RATIONAL METHOD PROCEDURE)

**Subdivision:** Realm Realty  
**Location:** CO, Colorado Springs  
**Design Storm:** 100-Year

**Project Name:** Crest at Woodmen - MDDP AMENDMENT  
**Project No.:** RLM 2.02  
**Calculated By:** CMV  
**Checked By:** SMB  
**Date:** 1/11/19

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	
	14	OS4	2.05	0.57	7.6	1.17	7.61	8.9													Flows to Stm West MH 1
		OS5	0.80	0.88	5.0	0.70	8.68	6.1													In Ex. 60" Storm Pipe coming from Nissan Dealership
West MH 1	15								7.6	1.87	7.61	14.2									(DP 14 & OS5)
	16	B3-1	7.34	0.63	7.9	4.62	7.52	34.7													Flows to Phase 1 West - Stm inlet 16
West MH 5	17								7.9	6.49	7.52	48.8									(DP 15 & 16)
	18	B4-2	0.87	0.88	5.0	0.77	8.68	6.7													
West MH 3									7.9	7.26	7.52	54.6									(DP 17 & 18)
	11	B5-1	0.51	0.75	5.0	0.38	8.68	3.3													Flows to Campus Stm inlet 6
Campus Stm Inlet 6 total Flow									7.9	7.64	7.52	57.5									(DP 19 & 11)
	12	B8	0.90	0.66	5.6	0.59	8.39	5.0													Flows to Campus Stm inlet 7
Campus Stm inlet 7 total flow									7.9	8.23	7.52	61.9									(DP 11 & 12)
	13	B4-1	1.69	0.88	5.4	1.49	8.48	12.6													Flows to Campus storm stub
Campus - MH 17	19								13.7	18.72	6.14	114.9									Flows to Pond B (DP 10, 12, 13)
	20	OS1	1.29	0.86	5.0	1.11	8.68	9.6													Flows to ex. Woodmen Rd inlet
	21	OS2	0.54	0.58	6.0	0.31	8.23	2.6													Flows to Campus Stm inlet 3
	22	OS3	0.76	0.63	6.0	0.48	8.20	3.9													Flows to Campus Stm inlet 1
Ex. Stm MH V10									6.0	1.90	8.20	15.6									
	23	B5-2	0.55	0.76	5.0	0.42	8.68	3.6													Flows to Ex. Inlet in Vincent northwest of Campus/Vincent Roundabout
	24	B5-3	0.16	0.79	5.0	0.13	8.68	1.1													Flows to Ex. Inlet in Vincent southeast of Campus/Vincent Roundabout
	25	B6	3.03	0.81	5.0	2.45	8.68	21.3													
	26A	B7-1	0.55	0.38	8.8	0.21	7.27	1.5													Flows to Phase 2/3 East - Stm inlet 27A
East Stm Inlet 27A total Flow									8.8	2.66	7.27	19.3									(DP 26 & 27A)
	26	B7	2.51	0.49	7.6	1.23	7.62	9.4													Flows to Phase 2/3 East - Stm inlet 27
East Stm Inlet 27 total Flow									8.8	3.89	7.27	28.3									Flows to Pond B (DP 27A & 27)



**STANDARD FORM SF-3**  
**STORM DRAINAGE SYSTEM DESIGN - PROPOSED**  
(RATIONAL METHOD PROCEDURE)

**Subdivision:** Realm Realty  
**Location:** CO, Colorado Springs  
**Design Storm:** 100-Year

**Project Name:** Crest at Woodmen - MDDP AMENDMENT  
**Project No.:** RLM 2.02  
**Calculated By:** CMV  
**Checked By:** SMB  
**Date:** 1/11/19

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	
	50	A1	2.47	0.88	5.2	2.17	8.57	18.6													Flows to future Stm inlet
	51A	A6	3.33	0.88	5.0	2.93	8.68	25.4													Flows to future Stm inlet
	51								5.2	5.10	8.57	43.7									(DP 50 & 51A)
	52											259.4									Offsite Flow of 259.4 cfs
	54A	A2	2.48	0.54	13.1	1.34	6.26	8.4					1.5	3.7				550	2.45	3.742	Bypass to DP 60A Flows to inlet 54A
	54B	A5	0.33	0.96	5.0	0.32	8.68	2.8					1.5	0.5	4.7	0.5	18	580	2.45	3.946	Bypass to inlet 56B Flows to inlet 54B
	54								13.1	6.12	6.26	297.7									(DP 53, 54A, 54B)
	55A	A9	1.33	0.92	5.0	1.22	8.68	10.6													Flows to future Stm inlet
	55								13.1	7.34	6.26	305.3									(DP 54 & 55A)
	56A	A11	3.8	0.88	5.0	3.34	8.68	29.0													Flows to inlet 56A
	56B	A12	0.24	0.96	7.6	0.23	7.62	1.8	8.9	0.29	7.21	2.1									Flow to inlet 56B
	56C	A13	5	0.88	9.1	4.4	7.16	31.5													Flows to future Stm inlet
Stm East MH 7	56								13.1	15.36	6.26	355.6									(DP 55, 56A, 56B, & 56C)
	57A	A16	1.21	0.96	5.0	1.16	8.68	10.1													Flows to inlet 57A
	57								13.1	16.52	6.26	362.8									(DP 56 & 57A)
	58	A3	3.81	0.72	9.0	2.74	7.21	19.8													Flows to inlet 58
	59A	A4	3.44	0.89	5.0	3.06	8.68	26.6													Flows to inlet 59A
	59								9.0	5.80	7.21	41.8									(DP 58 & 59A)
	60A	A7	2.86	0.88	5.4	2.52	8.48	21.4													Flows to inlet 60A
	60								16.8	8.91	5.62	50.1									(DP 59 & 60A)
	61A	A8	0.6	0.96	5.0	0.58	8.68	5.0													Flows to inlet 61A
Stm East MH 12	61								16.8	9.49	5.62	53.3									(DP 60 & 61A)
	62A	A10	2.75	0.87	5.0	2.39	8.68	20.7													Flows to inlet 62A
	62								16.8	11.88	5.62	66.8									(DP 61 & 62A)

**STANDARD FORM SF-3**  
**STORM DRAINAGE SYSTEM DESIGN - PROPOSED**  
(RATIONAL METHOD PROCEDURE)

**Subdivision:** Realm Realty  
**Location:** CO, Colorado Springs  
**Design Storm:** 100-Year

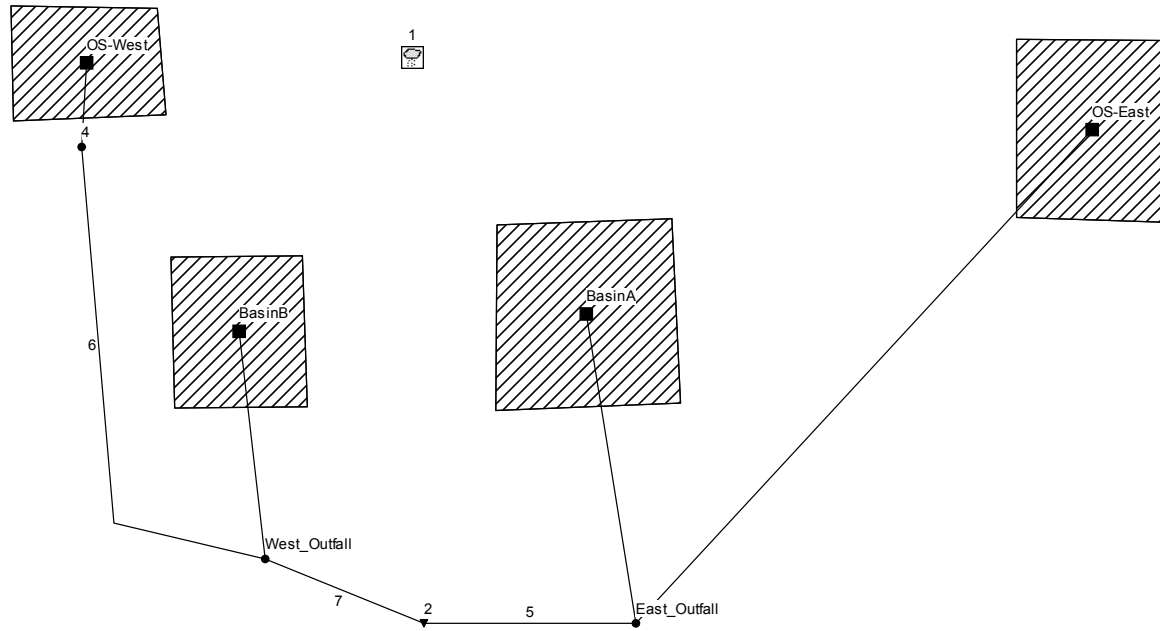
**Project Name:** Crest at Woodmen - MDDP AMENDMENT  
**Project No.:** RLM 2.02  
**Calculated By:** CMV  
**Checked By:** SMB  
**Date:** 1/11/19

STREET	Design Point	DIRECT RUNOFF							TOTAL RUNOFF				STREET		PIPE			TRAVEL TIME			REMARKS
		Basin ID	Area (Ac)	Runoff Coeff.	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Tc (min)	C*A (Ac)	I (in/hr)	Q (cfs)	Slope (%)	Street Flow (cfs)	Design Flow (cfs)	Slope (%)	Pipe Size (inches)	Length (ft)	Velocity (fps)	Tt (min)	
	63A	A14	0.05	0.96	5.0	0.05	8.68	0.4													Flows into inlets 63A & 63B
	63								16.8	11.93	5.62	67									(DP 62 & 63A)
	64								16.8	28.45	5.62	419.3									(DP 57 & 63)
	65A	A15	1.09	0.96	5.0	1.05	8.68	9.1													Flows to inlet 65A
	65								16.8	29.50	5.62	425.2									(DP 64 & 65A)
	66A	A17	5.24	0.88	7.0	4.61	7.83	36.1													Flows to future Stm inlet
	66B	A18	4.12	0.88	5.4	3.63	8.5	30.9													Flows to future Stm inlet
Future Stm MH	66C								7.0	8.24	7.83	64.5									(DP 66A & 66B)
Stm East MH 15	66								16.8	37.74	5.62	471.5									(DP 65 & 66C)
	67A	A20	1.06	0.96	5.0	1.02	8.68	8.9													Flows to inlet 67A
	67								16.8	38.76	5.62	477.2									(DP 66 & 67A)
	68A	A19	0.69	0.96	5.0	0.66	8.68	5.7													Flows to inlet 68A
Stm East MH 16	68								16.8	39.42	5.62	480.9									(DP 67, 68A)
	69A	A21	0.45	0.96	5.0	0.43	8.68	3.7													Flows to inlet 69A
Stm East MH 16	69								16.8	39.85	5.62	483.4									(DP 68 & 69A)
	70	A22	3.45	0.39	7.0	1.35	7.82	10.6	16.8	41.20	5.62	490.9									Pond A

**Appendix D**  
**Pond Calculations**

# **SWMM MODEL – EXISTING CONDITIONS**

Historic Model



Historic Model - Input

[TITLE]  
 ;;Project Title/Notes

[OPTIONS]  
 ;;Option Value  
 FLOW\_UNITS CFS  
 INFILTRATION HORTON  
 FLOW\_ROUTING KINWAVE  
 LINK\_OFFSETS DEPTH  
 MIN\_SLOPE 0  
 ALLOW\_PONDING NO  
 SKIP\_STEADY\_STATE NO  
  
 START\_DATE 08/24/2016  
 START\_TIME 00:00:00  
 REPORT\_START\_DATE 08/24/2016  
 REPORT\_START\_TIME 00:00:00  
 END\_DATE 08/24/2016  
 END\_TIME 02:00:00  
 SWEEP\_START 01/01  
 SWEEP\_END 12/31  
 DRY\_DAYS 0  
 REPORT\_STEP 00:05:00  
 WET\_STEP 00:05:00  
 DRY\_STEP 00:05:00  
 ROUTING\_STEP 0:00:30

INERTIAL\_DAMPING PARTIAL  
 NORMAL\_FLOW\_LIMITED BOTH  
 FORCE\_MAIN\_EQUATION H-W  
 VARIABLE\_STEP 0.75  
 LENGTHENING\_STEP 0  
 MIN\_SURFAREA 12.557  
 MAX\_TRIALS 8  
 HEAD\_TOLERANCE 0.005  
 SYS\_FLOW\_TOL 5  
 LAT\_FLOW\_TOL 5  
 MINIMUM\_STEP 0.5  
 THREADS 1

[EVAPORATION]  
 ;;Data Source Parameters  
 ;;-----  
 CONSTANT 0.0  
 DRY\_ONLY NO

[RAINGAGES]  
 ;;Name Format Interval SCF Source  
 ;;-----  
 1 CUMULATIVE 0:05 1.0 TIMESERIES CS\_100-yr

[SUBCATCHMENTS] ;;Name	Rain Gage	Outlet	Area	%Imperv	width	%Slope	CurbLen
SnowPack	-----						
OS-East	1	East_outfall	33.9	77	6000	2.5	0
BasinA	1	East_outfall	50.88	2	1500	2	0
BasinB	1	west_outfall	29.73	2	800	4	0
OS-West	1	4	2.92	47.05	500	1	0

[SUBAREAS] ;;Subcatchment	N-Imperv	N-Perv	S-Imperv	S-Perv	PctZero	RouteTo	PctRouted
;;	-----						
OS-East	0.011	0.24	0.1	0.35	25	OUTLET	
BasinA	0.011	0.24	0.1	0.35	25	OUTLET	
BasinB	0.011	0.24	0.1	0.35	25	OUTLET	
OS-West	0.011	0.24	0.1	0.35	25	OUTLET	

[INFILTRATION]

Historic Model - Input

Subcatchment	MaxRate	MinRate	Decay	DryTime	MaxInfil
OS-East	4.5	0.6	6.48	7	0
BasinA	4.5	0.6	6.48	7	0
BasinB	4.5	0.6	6.48	7	0
OS-West	4.5	.6	6.48	7	0

[JUNCTIONS]

Name	Elevation	MaxDepth	InitDepth	SurDepth	Aponded
East_outfall	6324	0	0	0	0
4	6327	5	0	0	0
West_outfall	0	0	0	0	0

[OUTFALLS]

Name	Elevation	Type	Stage Data	Gated	Route To
2	6304	FREE		NO	

[CONDUITS]

Name	From Node	To Node	Length	Roughness	InOffset	OutOffset
5	East_outfall	2	400	0.01	0	0
6	4	West_outfall	1320	0.035	0	0
7	West_outfall	2	400	0.01	0	0

[XSECTIONS]

Link	Shape	Geom1	Geom2	Geom3	Geom4	Barrels
5	DUMMY	0	0	0	0	1
6	DUMMY	0	0	0	0	1
7	DUMMY	0	0	0	0	1

[LOSSES]

Link	Kentry	Kexit	Kavg	Flap Gate	Seepage
6	0.5	1	0	NO	0

[CURVES]

Name	Type	X-Value	Y-Value
PondA_Outlet	Rating	0.00	0.00
PondA_Outlet		0.50	0.26
PondA_Outlet		1.00	0.36
PondA_Outlet		1.50	0.44
PondA_Outlet		2.00	0.66
PondA_Outlet		2.50	0.87
PondA_Outlet		3.00	1.02
PondA_Outlet		3.50	1.15
PondA_Outlet		4.00	1.47
PondA_Outlet		4.50	1.69
PondA_Outlet		5.00	1.87
PondA_Outlet		5.50	2.03
PondA_Outlet		6.00	46.67
PondA_Outlet		6.50	132.00
PondA_Outlet	7.00	229.02	
PondB_Outlet	Rating	0.00	0.00
PondB_Outlet		0.50	0.13
PondB_Outlet		1.00	0.18
PondB_Outlet		1.50	0.22
PondB_Outlet		2.00	0.25
PondB_Outlet		2.50	0.28
PondB_Outlet		3.00	0.42

Historic Model - Input

PondB_Outlet		3.50	0.50
PondB_Outlet		4.00	0.57
PondB_Outlet		4.50	0.62
PondB_Outlet		5.00	0.67
PondB_Outlet		5.50	0.82
PondB_Outlet		6.00	0.93
PondB_Outlet		6.50	1.01
PondB_Outlet		7.00	1.08
PondB_Outlet		7.50	1.15
PondB_Outlet		7.75	1.18
PondB_Outlet		8.00	16.50
PondB_Outlet		8.50	85.74
PondB_Outlet		9.00	179.51

;			
PondA_Vol	Storage	0	0
PondA_Vol		1	15014
PondA_Vol		2	30880
PondA_Vol		3	48410
PondA_Vol		4	67605
PondA_Vol		5	88465
PondA_Vol		6	110990
PondA_Vol		7	117516

;			
PondB_Vol	Storage	0.00	0
PondB_Vol		1.00	5422
PondB_Vol		2.00	17888
PondB_Vol		3.00	17888
PondB_Vol		4.00	17888
PondB_Vol		5.00	17888
PondB_Vol		6.00	17888
PondB_Vol		7.00	17888
PondB_Vol		8.00	17888
PondB_Vol		9.00	17888

[TIMESERIES]

;;Name	Date	Time	Value
-----			
;;			
CS_100-yr		0	0
CS_100-yr		0:05	0.03528
CS_100-yr		0:10	0.11592
CS_100-yr		0:15	0.19908
CS_100-yr		0:20	0.3024
CS_100-yr		0:25	0.45108
CS_100-yr		0:30	0.65016
CS_100-yr		0:35	1.06092
CS_100-yr		0:40	1.79424
CS_100-yr		0:45	2.07648
CS_100-yr		0:50	2.24784
CS_100-yr		0:55	2.3562
CS_100-yr		1:00	2.44944
CS_100-yr		1:05	2.53008
CS_100-yr		1:10	2.56536
CS_100-yr		1:15	2.5956
CS_100-yr		1:20	2.62332
CS_100-yr		1:25	2.65104
CS_100-yr		1:30	2.67876
CS_100-yr		1:35	2.70144
CS_100-yr		1:40	2.72664
CS_100-yr		1:45	2.74932
CS_100-yr		1:50	2.772
CS_100-yr		1:55	2.79468
CS_100-yr		2:00	2.81988
;			
CS_5-yr		0	0
CS_5-yr		0:05	0.021
CS_5-yr		0:10	0.069
CS_5-yr		0:15	0.1185
CS_5-yr		0:20	0.18
CS_5-yr		0:25	0.2685
CS_5-yr		0:30	0.387
CS_5-yr		0:35	0.6315
CS_5-yr		0:40	1.068
CS_5-yr		0:45	1.236
CS_5-yr		0:50	1.338



Historic Model - Input

CS_5-yr	0:55	1.4025
CS_5-yr	1:00	1.458
CS_5-yr	1:05	1.506
CS_5-yr	1:10	1.527
CS_5-yr	1:15	1.545
CS_5-yr	1:20	1.5615
CS_5-yr	1:25	1.578
CS_5-yr	1:30	1.5945
CS_5-yr	1:35	1.608
CS_5-yr	1:40	1.623
CS_5-yr	1:45	1.6365
CS_5-yr	1:50	1.65
CS_5-yr	1:55	1.6635
CS_5-yr	2:00	1.6785

[REPORT]

```
;;Reporting Options
INPUT      NO
CONTROLS   NO
SUBCATCHMENTS ALL
NODES ALL
LINKS ALL
```

[TAGS]

[MAP]

```
DIMENSIONS 0.000 0.000 10000.000 10000.000
Units      None
```

[COORDINATES]

```
;;Node      X-Coord      Y-Coord
-----
East_Outfall 2604.626      2929.515
4             -2725.771     7511.013
West_Outfall -954.198      3549.618
2             559.796       2926.209
```

[VERTICES]

```
;;Link      X-Coord      Y-Coord
-----
6             -2406.388     3887.665
```

[Polygons]

```
;;Subcatchment X-Coord      Y-Coord
-----
OS-East        7714.758      8535.242
OS-East        7736.784      6784.141
OS-East        6250.000      6828.194
OS-East        6250.000      8546.256
BasinA         2946.035      6817.181
BasinA         3034.141      5044.053
BasinA         1250.000      4977.974
BasinA         1272.026      6762.115
BasinB         -600.220      6464.758
BasinB         -556.167      5011.013
BasinB         -1822.687     5000.000
BasinB         -1866.740     6453.744
OS-West        -1993.392     8846.366
OS-West        -1916.300     7822.137
OS-West        -3370.044     7767.070
OS-West        -3403.084     8868.392
```

[SYMBOLS]

```
;;Gage      X-Coord      Y-Coord
-----
1             468.062       8359.031
```

[LABELS]

```
;;X-Coord      Y-Coord      Label
82.599         9669.604     "Historic Model" "" "Arial" 10 0 0
```

WARNING 08: elevation drop exceeds length for Conduit 6  
 WARNING 08: elevation drop exceeds length for Conduit 7

\*\*\*\*\*  
 NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
 \*\*\*\*\*

\*\*\*\*\*  
 Analysis Options  
 \*\*\*\*\*

Flow Units ..... CFS  
 Process Models:  
   Rainfall/Runoff ..... YES  
   RDII ..... NO  
   Snowmelt ..... NO  
   Groundwater ..... NO  
   Flow Routing ..... YES  
   Ponding Allowed ..... NO  
   Water Quality ..... NO  
 Infiltration Method ..... HORTON  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... AUG-24-2016 00:00:00  
 Ending Date ..... AUG-24-2016 02:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:05:00  
 Wet Time Step ..... 00:05:00  
 Dry Time Step ..... 00:05:00  
 Routing Time Step ..... 30.00 sec

*****	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
*****	-----	-----
Total Precipitation .....	27.348	2.795
Evaporation Loss .....	0.000	0.000
Infiltration Loss .....	11.691	1.195
Surface Runoff .....	9.890	1.011
Final Storage .....	5.914	0.604
Continuity Error (%) .....	-0.538	

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry weather Inflow .....	0.000	0.000
Wet weather Inflow .....	9.813	3.198
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	0.000	0.000
External Outflow .....	9.813	3.198
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000
Initial stored volume ....	0.000	0.000
Final stored volume .....	0.000	0.000
Continuity Error (%) .....	0.000	

\*\*\*\*\*  
 Highest Flow Instability Indexes  
 \*\*\*\*\*  
 All links are stable.

\*\*\*\*\*  
 Routing Time Step Summary  
 \*\*\*\*\*  
 Minimum Time Step : 30.00 sec

Historic Model - 100-yr

Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.00  
 Percent Not Converging : 0.00

\*\*\*\*\*  
 Subcatchment Runoff Summary  
 \*\*\*\*\*

Peak Runoff	Runoff Coeff	Total Precip	Total Runon	Total Evap	Total Infil	Total Runoff	Total Runoff
Subcatchment		in	in	in	in	in	10^6 gal
CFS							
OS-East		2.79	0.00	0.00	0.37	2.33	2.14
260.74	0.833						
BasinA		2.79	0.00	0.00	1.56	0.41	0.56
20.33	0.146						
BasinB		2.79	0.00	0.00	1.56	0.47	0.38
14.60	0.169						
OS-West		2.79	0.00	0.00	0.84	1.73	0.14
14.27	0.619						

\*\*\*\*\*  
 Node Depth Summary  
 \*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
East_outfall	JUNCTION	0.00	0.00	6324.00	0 00:00	0.00
4	JUNCTION	0.00	0.00	6327.00	0 00:00	0.00
West_outfall	JUNCTION	0.00	0.00	0.00	0 00:00	0.00
2	OUTFALL	0.00	0.00	6304.00	0 00:00	0.00

\*\*\*\*\*  
 Node Inflow Summary  
 \*\*\*\*\*

Flow Balance Error	Node Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr:min	Lateral Inflow volume 10^6 gal	Total Inflow volume 10^6 gal
0.000	East_outfall	279.90	279.90	0 00:45	2.69	2.69
0.000	4	14.27	14.27	0 00:45	0.137	0.137
0.000	West_outfall	14.60	27.14	0 00:45	0.375	0.511
0.000	2	0.00	307.04	0 00:45	0	3.2

\*\*\*\*\*  
Node Surge Summary  
\*\*\*\*\*

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
East_Outfall	JUNCTION	2.00	0.000	0.000
4	JUNCTION	2.00	0.000	5.000
West_Outfall	JUNCTION	2.00	0.000	0.000

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
2	95.42	62.26	307.04	3.197
System	95.42	62.26	307.04	3.197

\*\*\*\*\*  
Link Flow Summary  
\*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
5	DUMMY	279.90	0 00:45			
6	DUMMY	14.27	0 00:45			
7	DUMMY	27.14	0 00:45			

\*\*\*\*\*  
Conduit Surge Summary  
\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Tue Sep 06 15:06:27 2016  
Analysis ended on: Tue Sep 06 15:06:27 2016  
Total elapsed time: < 1 sec

WARNING 08: elevation drop exceeds length for Conduit 6  
 WARNING 08: elevation drop exceeds length for Conduit 7

\*\*\*\*\*  
 NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
 \*\*\*\*\*

\*\*\*\*\*  
 Analysis Options  
 \*\*\*\*\*

Flow Units ..... CFS  
 Process Models:  
   Rainfall/Runoff ..... YES  
   RDII ..... NO  
   Snowmelt ..... NO  
   Groundwater ..... NO  
   Flow Routing ..... YES  
   Ponding Allowed ..... NO  
   Water Quality ..... NO  
 Infiltration Method ..... HORTON  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... AUG-24-2016 00:00:00  
 Ending Date ..... AUG-24-2016 02:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:05:00  
 Wet Time Step ..... 00:05:00  
 Dry Time Step ..... 00:05:00  
 Routing Time Step ..... 30.00 sec

*****	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
*****	-----	-----
Total Precipitation .....	16.279	1.664
Evaporation Loss .....	0.000	0.000
Infiltration Loss .....	11.199	1.144
Surface Runoff .....	3.962	0.405
Final Storage .....	1.167	0.119
Continuity Error (%) .....	-0.305	

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10^6 gal
*****	-----	-----
Dry weather Inflow .....	0.000	0.000
Wet weather Inflow .....	3.943	1.285
Groundwater Inflow .....	0.000	0.000
RDII Inflow .....	0.000	0.000
External Inflow .....	0.000	0.000
External Outflow .....	3.943	1.285
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000
Initial stored volume ....	0.000	0.000
Final stored volume .....	0.000	0.000
Continuity Error (%) .....	0.000	

\*\*\*\*\*  
 Highest Flow Instability Indexes  
 \*\*\*\*\*  
 All links are stable.

\*\*\*\*\*  
 Routing Time Step Summary  
 \*\*\*\*\*  
 Minimum Time Step : 30.00 sec

Historic Model - 5-yr

Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.00  
 Percent Not Converging : 0.00

\*\*\*\*\*  
 Subcatchment Runoff Summary  
 \*\*\*\*\*

Peak Runoff	Runoff Coeff	Total Precip	Total Runon	Total Evap	Total Infil	Total Runoff	Total Runoff
Subcatchment		in	in	in	in	in	10^6 gal
CFS							
OS-East		1.66	0.00	0.00	0.35	1.24	1.14
136.34	0.745						
BasinA		1.66	0.00	0.00	1.49	0.04	0.05
5.49	0.024						
BasinB		1.66	0.00	0.00	1.49	0.04	0.03
3.22	0.025						
OS-West		1.66	0.00	0.00	0.81	0.77	0.06
7.18	0.462						

\*\*\*\*\*  
 Node Depth Summary  
 \*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr:min	Reported Max Depth Feet
East_outfall	JUNCTION	0.00	0.00	6324.00	0 00:00	0.00
4	JUNCTION	0.00	0.00	6327.00	0 00:00	0.00
West_outfall	JUNCTION	0.00	0.00	0.00	0 00:00	0.00
2	OUTFALL	0.00	0.00	6304.00	0 00:00	0.00

\*\*\*\*\*  
 Node Inflow Summary  
 \*\*\*\*\*

Flow Balance Error	Node	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr:min	Lateral Inflow volume 10^6 gal	Total Inflow volume 10^6 gal
0.000	East_outfall	JUNCTION	141.83	141.83	0 00:45	1.19	1.19
0.000	4	JUNCTION	7.18	7.18	0 00:45	0.0606	0.0606
0.000	West_outfall	JUNCTION	3.22	10.40	0 00:45	0.0337	0.0943
0.000	2	OUTFALL	0.00	152.23	0 00:45	0	1.28

\*\*\*\*\*  
Node Surcharge Summary  
\*\*\*\*\*

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Feet	Min. Depth Below Rim Feet
East_Outfall	JUNCTION	2.00	0.000	0.000
4	JUNCTION	2.00	0.000	5.000
West_Outfall	JUNCTION	2.00	0.000	0.000

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
2	95.42	25.01	152.23	1.285
System	95.42	25.01	152.23	1.285

\*\*\*\*\*  
Link Flow Summary  
\*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr:min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
5	DUMMY	141.83	0 00:45			
6	DUMMY	7.18	0 00:45			
7	DUMMY	10.40	0 00:45			

\*\*\*\*\*  
Conduit Surcharge Summary  
\*\*\*\*\*

No conduits were surcharged.

Analysis begun on: Tue Sep 06 15:05:20 2016  
Analysis ended on: Tue Sep 06 15:05:20 2016  
Total elapsed time: < 1 sec

## **POND A DESIGN INFO**

**A) Spreadsheets**

**B) SWMM Model to verify WQCV/EURV Drain Times**



## Detention Pond Tributary Areas

**Subdivision:** Realm Realty  
**Location:** CO, Colorado Springs

**Project Name:** Crest at Woodmen - MDDP AMENDMENT  
**Project No.:** RLM 2.02  
**Calculated By:** CMV  
**Checked By:** SMB  
**Date:** 12/21/18

### Detention Pond #A

Basin	Area	% Imp
A1	2.47	95
A2	2.48	53.76
A3	3.81	82.37
A4	3.44	95.83
A5	0.33	100
A6	3.33	95
A7	2.86	95.05
A8	0.60	100
A9	1.33	98.05
A10	2.75	94.8
A11	3.80	94.86
A12	0.24	100
A13	5.00	95
A14	0.05	100
A15	1.09	100
A16	1.21	100
A17	5.24	95
A18	4.12	95
A19	0.69	100
A20	1.06	100
A21	0.45	100
A22	3.45	6.35
<b>Total</b>	<b>49.80</b>	<b>86.5</b>
Offsite East	33.9	77
<b>Total</b>	<b>83.7</b>	<b>83.0</b>

#### EURV Required For Onsite & Offsite Basins

EURV = 1.17 in From Eqn 13-6  
**EURV = 4.86 ac-ft**

#### WQ Required For Onsite Basins

WQCV = 0.37 in From Eqn. 3-1  
**WQCV = 1.55 ac-ft**

#### WQ Required For Offsite Basins

WQCV = 0.31 in From Eqn. 3-1  
**WQCV = 0.88 ac-ft**

Total Pond A Water Quality = 0.35 in  
**Total Pond A Water Quality = 2.43 ac-ft**

## POND VOLUME CALCULATIONS

Subdivision Realm Realty  
 Location CO, Colorado Springs

Project Name: Crest at Woodmen - Phase 2 East and Phase 3 Southeast  
 Project No. RLM 2.03  
 By: CMV  
 Checked By: SMB  
 Date: 12/21/18

Volume=1/3 x Depth x (A+B+(A\*B)^0.5)  
 A - Upper Surface  
 B - Lower Surface

### Pond A

Stage	Stage Elevation	Stage Surface Area (square feet)	Stage Volume (cubic feet)	Cumulative Volume (cubic feet)	Cumulative Volume (acre feet)
0.00	6310.00	272	0	0	0.00
1.00	6311.00	2,591	1,234	1,234	0.03
2.00	6312.00	10,979	6,301	7,535	0.17
3.00	6313.00	28,075	18,870	26,405	0.61
4.00	6314.00	43,259	35,395	61,800	1.42
5.00	6315.00	48,157	45,686	107,486	2.47
6.00	6316.00	52,238	50,184	157,670	3.62
7.00	6317.00	56,387	54,300	211,970	4.87
8.00	6318.00	60,626	58,494	270,464	6.21
9.00	6319.00	64,959	62,780	333,244	7.65
10.00	6320.00	69,377	67,156	400,400	9.19
11.00	6321.00	73,891	71,622	472,022	10.84
12.00	6322.00	78,503	76,185	548,207	12.59

Volume (acre feet)	Volume	Water Surface Elevation	Stage	
Total WQ	2.43	6314.97	4.97	(Per Pond Tributary spreadsheet)
Onsite EURV + Offsite WQ	5.74	6317.66	7.66	(Per Pond Tributary spreadsheet)
100-Year Detention	7.36	6318.80	8.80	(Per SWMM model)

## STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET

Project: **The Crest at Woodmen**

Basin ID: **Pond A**

**WQCV Design Volume (Input):**

Catchment Imperviousness,  $I_p$  =  percent  
 Catchment Area, A =  acres  
 Depth at WQCV outlet above lowest perforation, H =  feet  
 Vertical distance between rows, h =  inches  
 Number of rows, NL =   
 Orifice discharge coefficient,  $C_d$  =   
 Slope of Basin Trickle Channel, S =  ft / ft  
 Time to Drain the Pond =  hours

Diameter of holes, D =  inches  
 Number of holes per row, N =  **OR**

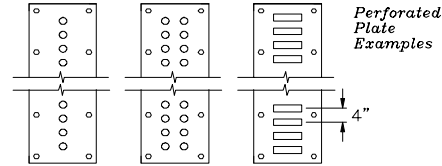
Height of slot, H =  inches  
 Width of slot, W =  inches

**Watershed Design Information (Input):**

Percent Soil Type A =  %  
 Percent Soil Type B =  %  
 Percent Soil Type C/D =  %

**Outlet Design Information (Output):**

Water Quality Capture Volume, WQCV =  watershed inches  
 Water Quality Capture Volume (WQCV) =  acre-feet  
**Design Volume (WQCV / 12 \* Area \* 1.2) Vol =  acre-feet**  
 Outlet area per row,  $A_o$  =  square inches  
 Total opening area at each row based on user-input above,  $A_o$  =  square inches  
 Total opening area at each row based on user-input above,  $A_o$  =  square feet



3

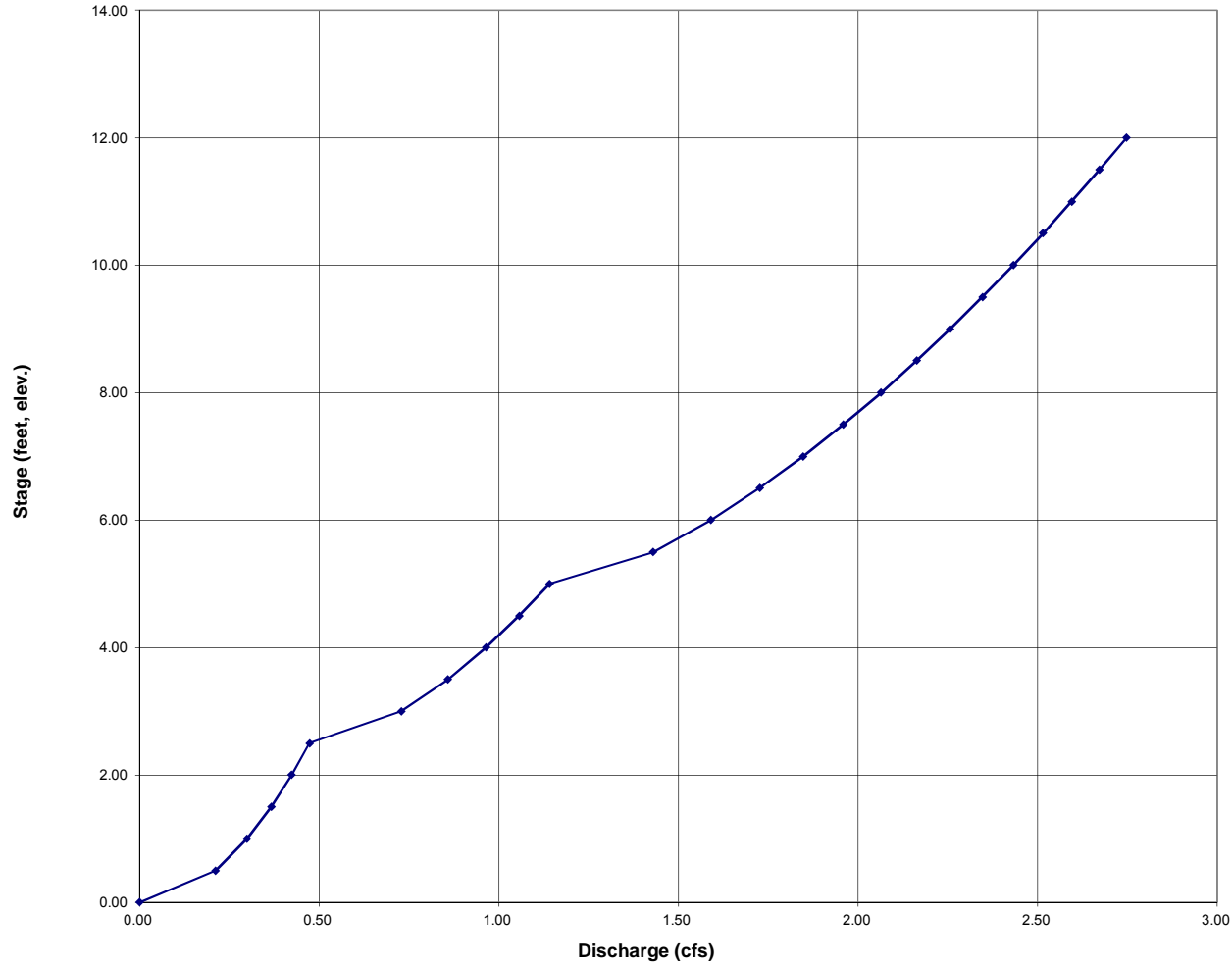
	Central Elevations of Rows of Holes in feet																							$\Sigma$ Flow	
	Row 1	Row 2	Row 3	Row 4	Row 5	Row 6	Row 7	Row 8	Row 9	Row 10	Row 11	Row 12	Row 13	Row 14	Row 15	Row 16	Row 17	Row 18	Row 19	Row 20	Row 21	Row 22	Row 23		Row 23
	0.00		5.00																						
	Collection Capacity for Each Row of Holes in cfs																								
0.00	0.0000	0.0000	0.0000																						0.00
0.50	0.2113	0.0000	0.0000																						0.21
1.00	0.2988	0.0000	0.0000																						0.30
1.50	0.3660	0.0000	0.0000																						0.37
2.00	0.4226	0.0000	0.0000																						0.42
2.50	0.4725	0.0000	0.0000																						0.47
3.00	0.5176	0.2113	0.0000																						0.73
3.50	0.5591	0.2988	0.0000																						0.86
4.00	0.5977	0.3660	0.0000																						0.96
4.50	0.6339	0.4226	0.0000																						1.06
5.00	0.6682	0.4725	0.0000																						1.14
5.50	0.7009	0.5176	0.2113																						1.43
6.00	0.7320	0.5591	0.2988																						1.59
6.50	0.7619	0.5977	0.3660																						1.73
7.00	0.7907	0.6339	0.4226																						1.85
7.50	0.8184	0.6682	0.4725																						1.96
8.00	0.8453	0.7009	0.5176																						2.06
8.50	0.8713	0.7320	0.5591																						2.16
9.00	0.8965	0.7619	0.5977																						2.26
9.50	0.9211	0.7907	0.6339																						2.35
10.00	0.9450	0.8184	0.6682																						2.43
10.50	0.9684	0.8453	0.7009																						2.51
11.00	0.9912	0.8713	0.7320																						2.59
11.50	1.0134	0.8965	0.7619																						2.67
12.00	1.0352	0.9211	0.7907																						2.75
	#N/A	#N/A	#N/A																						#N/A
	#N/A	#N/A	#N/A																						#N/A
	#N/A	#N/A	#N/A																						#N/A
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STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET

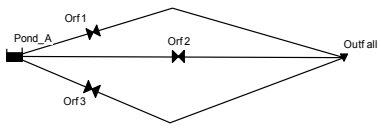
Worksheet Protected

Project: The Crest at Woodmen  
Basin ID: Pond A

STAGE-DISCHARGE CURVE FOR THE WQCV OUTLET STRUCTURE



Pond A Outlet Check



Pond A Outlet Input - Total WQ

[TITLE]

;; Project Title/Notes

[OPTIONS]

```

;; Option      Value
FLOW_UNITS     CFS
INFILTRATION   HORTON
FLOW_ROUTING   KINWAVE
LINK_OFFSETS   DEPTH
MIN_SLOPE      0
ALLOW_PONDING  NO
SKIP_STEADY_STATE NO

START_DATE     09/02/2016
START_TIME     00:00:00
REPORT_START_DATE 09/02/2016
REPORT_START_TIME 00:00:00
END_DATE       09/05/2016
END_TIME       00:00:00
SWEEP_START    01/01
SWEEP_END      12/31
DRY_DAYS       0
REPORT_STEP    00:05:00
WET_STEP       00:05:00
DRY_STEP       00:05:00
ROUTING_STEP   0:00:30
RULE_STEP      00:00:00

INERTIAL_DAMPING PARTIAL
NORMAL_FLOW_LIMITED BOTH
FORCE_MAIN_EQUATION H-W
VARIABLE_STEP   0.75
LENGTHENING_STEP 0
MIN_SURFAREA    12.557
MAX_TRIALS      8
HEAD_TOLERANCE  0.005
SYS_FLOW_TOL    5
LAT_FLOW_TOL    5
MINIMUM_STEP    0.5
THREADS         1
    
```

[EVAPORATION]

```

;; Data Source Parameters
;;-----
CONSTANT      0.0
DRY_ONLY      NO
    
```

[OUTFALLS]

```

;; Name      Elevation  Type      Stage Data  Gated  Route To
;;-----
Outfall     0          FREE      NO          NO
    
```

[STORAGE]

```

;; Name      Elev.  MaxDepth  InitDepth  Shape  Curve Name/Params
N/A      Fevap  Psi      Ksat      IMD
    
```

Pond A Outlet Input - Total WQ

```

;; -----
Pond_A      6310      12      4.97      TABULAR      PondA_Volume      0
  0
  
```

[ORIFICES]

```

;; Name      From Node      To Node      Type      Offset      Qcoeff
Gated      CloseTime
;; -----
Orf1      Pond_A      Outfall      SIDE      0      0.65      NO
  0
Orf2      Pond_A      Outfall      SIDE      2.5      0.65      NO
  0
Orf3      Pond_A      Outfall      SIDE      5      0.65      NO
  0
  
```

[XSECTIONS]

```

;; Link      Shape      Geom1      Geom2      Geom3      Geom4      Barrels
Culvert
;; -----
Orf1      RECT_CLOSED .125      0.458333  0      0
Orf2      RECT_CLOSED .125      .458333  0      0
Orf3      RECT_CLOSED .125      .458333  0      0
  
```

[CURVES]

```

;; Name      Type      X-Value      Y-Value
;; -----
PondA_Volume      Storage      0.00      272
PondA_Volume      1.00      2591
PondA_Volume      2.00      10979
PondA_Volume      3.00      28075
PondA_Volume      4.00      43259
PondA_Volume      5.00      48157
PondA_Volume      6.00      52238
PondA_Volume      7.00      56387
PondA_Volume      8.00      60626
PondA_Volume      9.00      64959
PondA_Volume      10.00     69377
PondA_Volume      11.00     73891
PondA_Volume      12.00     78503
  
```

[REPORT]

```

;; Reporting Options
SUBCATCHMENTS ALL
NODES ALL
LINKS ALL
  
```

[TAGS]

[MAP]

```

DIMENSIONS 0.000 0.000 10000.000 10000.000
Units      None
  
```

Pond A Outlet Input - Total WQ

[COORDINATES]

;; Node	X-Coord	Y-Coord
-----	-----	-----
Outfall	5747.191	5797.753
Pond_A	2455.056	5808.989

[VERTICES]

;; Link	X-Coord	Y-Coord
-----	-----	-----
Orf1	4036.344	6277.533
Orf3	4003.304	5165.198

[LABELS]

;; X-Coord	Y-Coord	Label
2982.143	7690.476	"Pond A Outlet Check" "" "Arial" 10 0 0



Pond A Outlet Check - Total WQ

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.013)

---

\*\*\*\*\*  
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
\*\*\*\*\*

\*\*\*\*\*  
Analysis Options  
\*\*\*\*\*

Flow Units ..... CFS  
Process Models:  
  Rainfall/Runoff ..... NO  
  RDI ..... NO  
  Snowmelt ..... NO  
  Groundwater ..... NO  
  Flow Routing ..... YES  
  Ponding Allowed ..... NO  
  Water Quality ..... NO  
Flow Routing Method ..... KINWAVE  
Starting Date ..... 09/02/2016 00:00:00  
Ending Date ..... 09/05/2016 00:00:00  
Antecedent Dry Days ..... 0.0  
Report Time Step ..... 00:05:00  
Routing Time Step ..... 30.00 sec

\*\*\*\*\*

Flow Routing Continuity	Volume acre-feet	Volume 10 <sup>6</sup> gal
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	0.000	0.000
Groundwater Inflow .....	0.000	0.000
RDI Inflow .....	0.000	0.000
External Inflow .....	0.000	0.000
External Outflow .....	2.471	0.805
Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000
Initial Stored Volume .....	2.472	0.805
Final Stored Volume .....	0.000	0.000
Continuity Error (%) .....	0.016	

\*\*\*\*\*  
Highest Flow Instability Indexes  
\*\*\*\*\*  
All links are stable.

\*\*\*\*\*

Pond A Outlet Check - Total WQ

Routing Time Step Summary

\*\*\*\*\*

Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.00  
 Percent Not Converging : 0.00

\*\*\*\*\*

Node Depth Summary

\*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr: min	Reported Max Depth Feet
Outfall	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
Pond_A	STORAGE	1.80	4.97	6314.97	0 00:00	4.96

\*\*\*\*\*

Node Inflow Summary

\*\*\*\*\*

Flow Balance Error Node Percent	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr: min	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal
Outfall 0.000	OUTFALL	0.00	1.13	0 00:00	0	0.805
Pond_A 0.016	STORAGE	0.00	0.00	0 00:00	0	0.805

\*\*\*\*\*

Node Flooding Summary

\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*

Pond A Outlet Check - Total WQ

Storage Volume Summary

\*\*\*\*\*

Storage Unit	Average Volume	Avg Pcnt Full	Evap Loss	Exfil Loss	Maximum Volume	Max Pcnt Full	Time of Max Occurrence
1000 ft3	1000 ft3				1000 ft3		days hr: min
Pond_A 1.13	24.008	4	0	0	107.659	20	0 00:00

\*\*\*\*\*

Outfall Loading Summary

\*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Outfall	57.99	0.72	1.13	0.805
System	57.99	0.72	1.13	0.805

\*\*\*\*\*

Link Flow Summary

\*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr: min	Maximum  Veloc  ft/sec	Max/Full Flow	Max/Full Depth
Orf1	ORIFICE	0.66	0 00:00			0.00
Orf2	ORIFICE	0.46	0 00:00			0.00
Orf3	ORIFICE	0.00	0 00:00			0.00

\*\*\*\*\*

Conduit Surcharge Summary

\*\*\*\*\*

No conduits were surcharged.

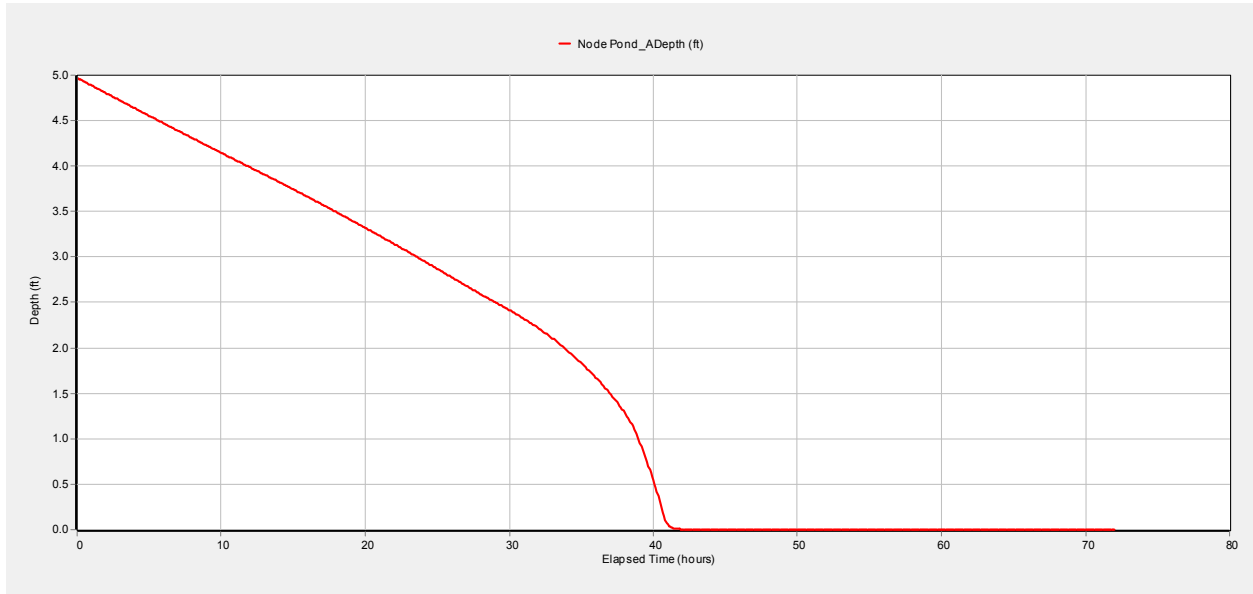
Analysis begun on: Wed Dec 19 12:21:44 2018

Pond A Outlet Check - Total WQ

Analysis ended on: Wed Dec 19 12:21:44 2018

Total elapsed time: < 1 sec

# Total WQ



Pond A Outlet Input - EURV + Offsite WQ

[TITLE]

;; Project Title/Notes

[OPTIONS]

```

;; Option          Value
FLOW_UNITS        CFS
INFILTRATION      HORTON
FLOW_ROUTING      KINWAVE
LINK_OFFSETS      DEPTH
MIN_SLOPE          0
ALLOW_PONDING     NO
SKIP_STEADY_STATE NO

START_DATE        09/02/2016
START_TIME        00:00:00
REPORT_START_DATE 09/02/2016
REPORT_START_TIME 00:00:00
END_DATE          09/05/2016
END_TIME          00:00:00
SWEEP_START       01/01
SWEEP_END         12/31
DRY_DAYS          0
REPORT_STEP       00:05:00
WET_STEP          00:05:00
DRY_STEP          00:05:00
ROUTING_STEP      0:00:30
RULE_STEP         00:00:00

INERTIAL_DAMPING  PARTIAL
NORMAL_FLOW_LIMITED BOTH
FORCE_MAIN_EQUATION H-W
VARIABLE_STEP     0.75
LENGTHENING_STEP 0
MIN_SURFAREA      12.557
MAX_TRIALS        8
HEAD_TOLERANCE    0.005
SYS_FLOW_TOL      5
LAT_FLOW_TOL      5
MINIMUM_STEP      0.5
THREADS           1
    
```

[EVAPORATION]

```

;; Data Source    Parameters
;;-----
CONSTANT          0.0
DRY_ONLY          NO
    
```

[OUTFALLS]

```

;; Name          Elevation  Type          Stage Data    Gated    Route To
;;-----
Outfall         0           FREE          NO            NO
    
```

[STORAGE]

```

;; Name          Elev.    MaxDepth    InitDepth    Shape    Curve Name/Params
N/A            Fevap    Psi         Ksat         IMD
    
```

Pond A Outlet Input - EURV + Offsite WQ

```

;; -----
Pond_A      6310      12      7.66      TABULAR      PondA_Volume      0
  0
  
```

[ORIFICES]

```

;; Name      From Node      To Node      Type      Offset      Qcoeff
Gated      CloseTime
;; -----
Orf1      Pond_A      Outfall      SIDE      0      0.65      NO
  0
Orf2      Pond_A      Outfall      SIDE      2.5      0.65      NO
  0
Orf3      Pond_A      Outfall      SIDE      5      0.65      NO
  0
  
```

[XSECTIONS]

```

;; Link      Shape      Geom1      Geom2      Geom3      Geom4      Barrels
Culvert
;; -----
Orf1      RECT_CLOSED .125      0.458333  0      0
Orf2      RECT_CLOSED .125      .458333  0      0
Orf3      RECT_CLOSED .125      .458333  0      0
  
```

[CURVES]

```

;; Name      Type      X-Value      Y-Value
;; -----
PondA_Volume      Storage      0.00      272
PondA_Volume      1.00      2591
PondA_Volume      2.00      10979
PondA_Volume      3.00      28075
PondA_Volume      4.00      43259
PondA_Volume      5.00      48157
PondA_Volume      6.00      52238
PondA_Volume      7.00      56387
PondA_Volume      8.00      60626
PondA_Volume      9.00      64959
PondA_Volume      10.00      69377
PondA_Volume      11.00      73891
PondA_Volume      12.00      78503
  
```

[REPORT]

```

;; Reporting Options
SUBCATCHMENTS ALL
NODES ALL
LINKS ALL
  
```

[TAGS]

[MAP]

```

DIMENSIONS 0.000 0.000 10000.000 10000.000
Units      None
  
```

Pond A Outlet Input - EURV + Offsite WQ

[COORDINATES]

;; Node	X-Coord	Y-Coord
-----		
Outfall	5747.191	5797.753
Pond_A	2455.056	5808.989

[VERTICES]

;; Link	X-Coord	Y-Coord
-----		
Orf1	4036.344	6277.533
Orf3	4003.304	5165.198

[LABELS]

;; X-Coord	Y-Coord	Label
2982.143	7690.476	"Pond A Outlet Check" "" "Arial" 10 0 0



\*\*\*\*\*
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.
\*\*\*\*\*

\*\*\*\*\*
Analysis Options
\*\*\*\*\*

Flow Units ..... CFS
Process Model s:
Rainfall/Runoff ..... NO
RDI ..... NO
Snowmelt ..... NO
Groundwater ..... NO
Flow Routing ..... YES
Ponding Allowed ..... NO
Water Quality ..... NO
Flow Routing Method ..... KINWAVE
Starting Date ..... 09/02/2016 00:00:00
Ending Date ..... 09/05/2016 00:00:00
Antecedent Dry Days ..... 0.0
Report Time Step ..... 00:05:00
Routing Time Step ..... 30.00 sec

\*\*\*\*\*
Flow Routing Continuity
\*\*\*\*\*
Table with 3 columns: Continuity Item, Volume (acre-feet), Volume (10^6 gal)
Rows include: Dry Weather Inflow, Wet Weather Inflow, Groundwater Inflow, RDI Inflow, External Inflow, External Outflow, Flooding Loss, Evaporation Loss, Exfiltration Loss, Initial Stored Volume, Final Stored Volume, Continuity Error (%)

\*\*\*\*\*
Highest Flow Instability Indexes
\*\*\*\*\*
All links are stable.

\*\*\*\*\*

Pond A Outlet Check - EURV + Offsite WQ

Routing Time Step Summary

\*\*\*\*\*

Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.00  
 Percent Not Converging : 0.00

\*\*\*\*\*

Node Depth Summary

\*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr: min	Reported Max Depth Feet
Outfall	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
Pond_A	STORAGE	3.95	7.66	6317.66	0 00:00	7.65

\*\*\*\*\*

Node Inflow Summary

\*\*\*\*\*

Flow Balance Error Node Percent	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr: min	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal
Outfall 0.000	OUTFALL	0.00	1.98	0 00:00	0	1.88
Pond_A 0.012	STORAGE	0.00	0.00	0 00:00	0	1.88

\*\*\*\*\*

Node Flooding Summary

\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*

Pond A Outlet Check - EURV + Offsite WQ

Storage Volume Summary

\*\*\*\*\*

Maximum Outflow Storage Unit CFS	Average Volume 1000 ft3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of Max Occurrence days hr: min
Pond_A 1.98	83.925	15	0	0	251.737	46	0 00:00

\*\*\*\*\*

Outfall Loading Summary

\*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Outfall	92.50	1.05	1.98	1.883
System	92.50	1.05	1.98	1.883

\*\*\*\*\*

Link Flow Summary

\*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr: min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
Orf1	ORIFICE	0.82	0 00:00			0.00
Orf2	ORIFICE	0.67	0 00:00			0.00
Orf3	ORIFICE	0.48	0 00:00			0.00

\*\*\*\*\*

Conduit Surcharge Summary

\*\*\*\*\*

No conduits were surcharged.

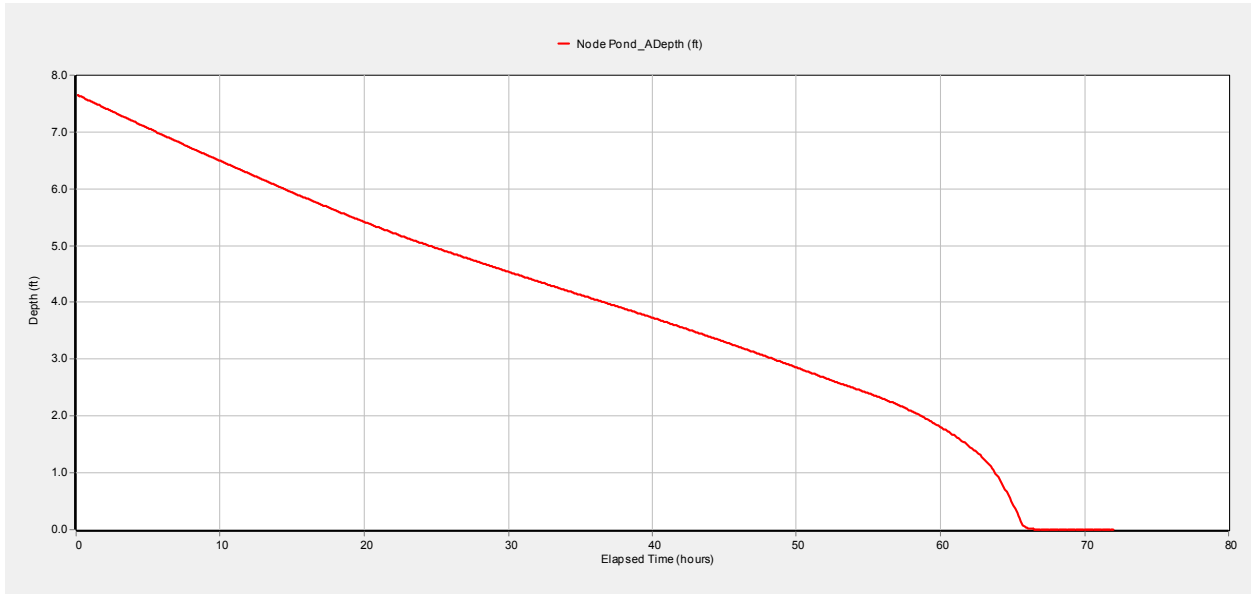
Analysis begun on: Wed Dec 19 12:18:38 2018

Pond A Outlet Check - EURV + Offsite WQ

Analysis ended on: Wed Dec 19 12:18:38 2018

Total elapsed time: < 1 sec

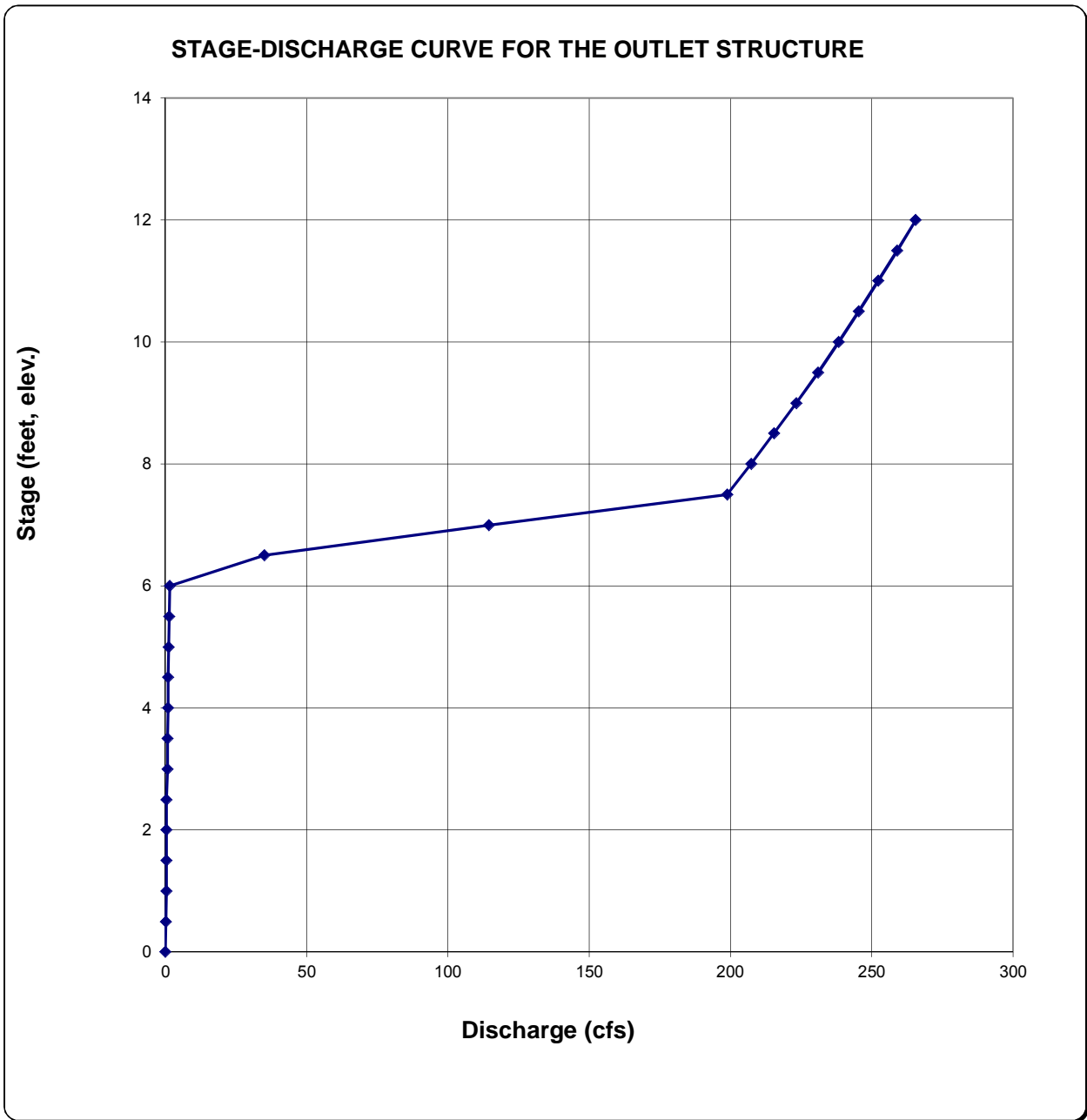
# Onsite EURV + Offsite WQ





STAGE-DISCHARGE SIZING OF THE WEIRS AND ORIFICES (INLET CONTROL)

Project: Crest at Woodmen  
Basin ID: Pond A



## **POND B DESIGN INFO**

**A) Spreadsheets**

**B) SWMM Model to verify WQCV/EURV Drain Times**



**Detention Pond #B**

<b>Basin</b>	<b>Area</b>	<b>% Imp</b>
B1-1	1.32	5
B1-2	0.38	90
B2	1.15	66.92
B3-1	7.34	77.77
B3-2	1.31	87.94
B3-3	0.64	85.18
B3-4	0.92	90
B4-1	1.69	95
B4-2	0.87	95
B5-1	0.51	85.11
B5-2	0.55	86.15
B5-3	0.16	88.1
B6	3.03	90
B7	2.51	38.26
B7-1	0.55	5
B8	0.90	75.94
B9	0.96	71.29
B9-1	0.72	90
B10	1.05	87.37
B11	1.65	78.22
B11-1	2.00	5
B12	0.77	89.23
B12-1	0.69	90
<b>Total Onsite</b>	<b>31.67</b>	<b>70.0</b>
Offsite OS 4	2.05	31.9
Offsite OS 5	0.80	95.0
<b>Offsite West</b>	<b>2.9</b>	<b>50.0</b>
<b>Total</b>	<b>34.52</b>	<b>68.3</b>

From Eqn 13-6

**EURV Required For Onsite Basins**

EURV =	0.94	in	
<b>EURV =</b>	<b>2.48</b>	<b>ac-ft</b>	From Eqn. 3-1

**WQ Required For Onsite Basins**

WQCV =	0.28	in	
<b>WQCV =</b>	<b>0.73</b>	<b>ac-ft</b>	From Eqn. 3-1

**WQ Required For Offsite Basins**

WQCV =	0.21	in	
<b>WQCV =</b>	<b>0.05</b>	<b>ac-ft</b>	

Total Pond B Water Quality =	0.27	in	
<b>Total Pond B Water Quality =</b>	<b>0.77</b>	<b>ac-ft</b>	

Total Pond B EURV+WQ =	1.42	in	
<b>Total Pond B EURV+WQ =</b>	<b>2.53</b>	<b>ac-ft</b>	

## POND VOLUME CALCULATIONS

**Subdivision** Realm Realty  
**Location** CO, Colorado Springs

**Project Name:** Crest at Woodmen - MDDP AMENDMENT  
**Project No.** RLM 2.02  
**By:** CMV  
**Checked By:** SMB  
**Date:** 1/11/19

Volume =  $\frac{1}{3} \times \text{Depth} \times (A+B+(A*B)^{0.5})$   
 A - Upper Surface  
 B - Lower Surface

### Pond B

Stage	Stage Elevation	Stage Surface Area (square feet)	Stage Volume (cubic feet)	Cumulative Volume (cubic feet)	Cumulative Volume (acre feet)
0.00	6303.00	1,722	0	0	0.00
1.00	6304.00	12,437	6,262	6,262	0.14
2.00	6305.00	24,225	18,007	24,269	0.56
3.00	6306.00	26,327	25,269	49,538	1.14
4.00	6307.00	28,436	27,375	76,913	1.77
5.00	6308.00	31,013	29,715	106,628	2.45
6.00	6309.00	33,247	32,123	138,751	3.19
7.00	6310.00	35,432	34,333	173,084	3.97
8.00	6311.00	37,548	36,485	209,569	4.81
9.00	6312.00	39,752	38,645	248,214	5.70

Volume (acre feet)	Volume	Water Surface Elevation	Stage	
<b>Total WQ</b>	0.77	6305.37	2.37	(Per Pond Tributary spreadsheet)
<b>Onsite EURV + Offsite WQ</b>	2.53	6308.12	5.12	(Per Pond Tributary spreadsheet)
<b>100-Year Detention</b>	3.10	6308.89	5.89	(Per SWMM model)

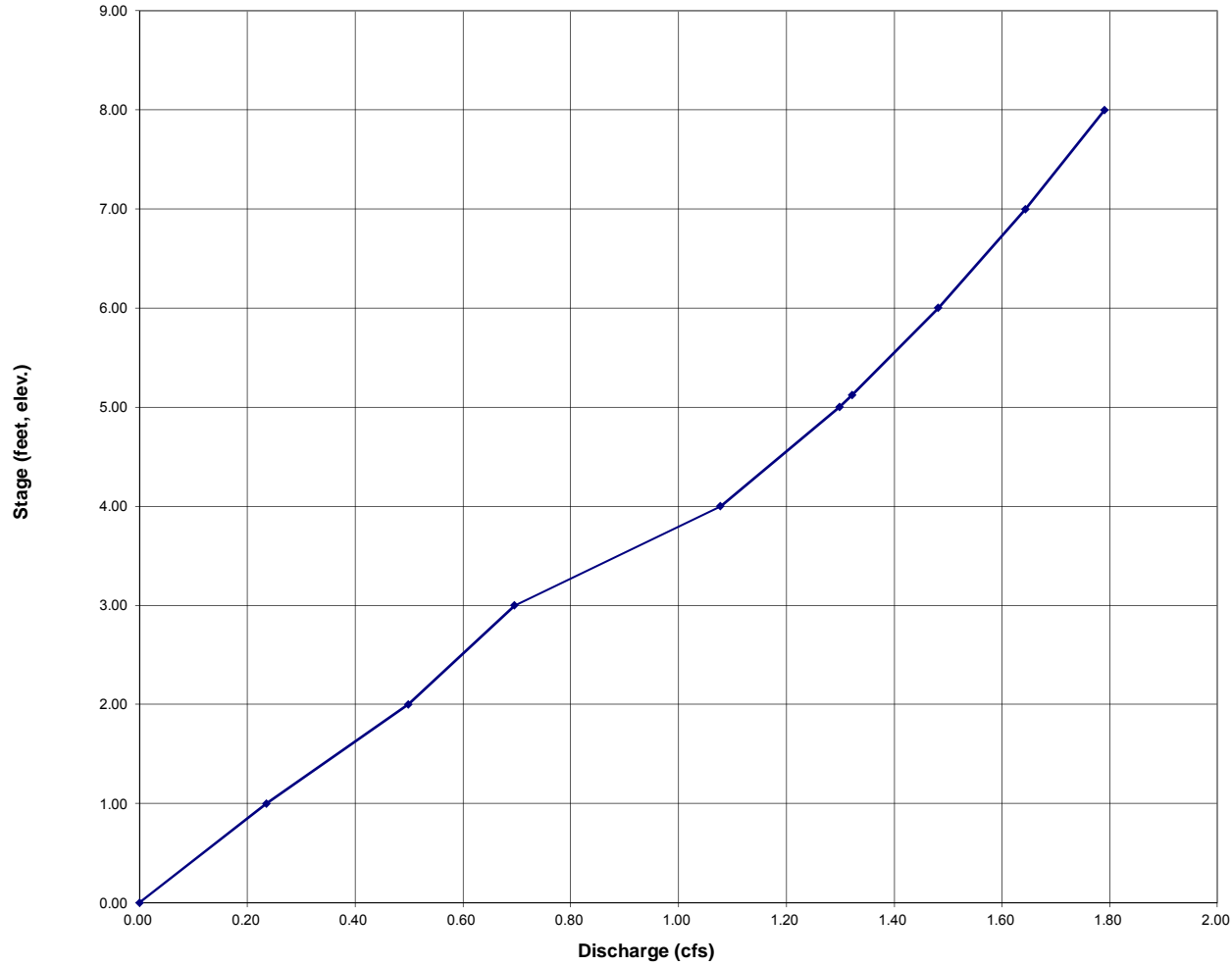


STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET

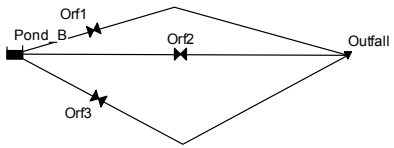
Worksheet Protected

Project: **The Crest At Woodmen**  
Basin ID: **Pond B**

STAGE-DISCHARGE CURVE FOR THE WQCV OUTLET STRUCTURE



Pond B Outlet Check



Pond B Outlet Check Input - Total WQ

[TITLE]

;; Project Title/Notes

[OPTIONS]

```

;; Option      Value
FLOW_UNITS    CFS
INFILTRATION  HORTON
FLOW_ROUTING  KINWAVE
LINK_OFFSETS  DEPTH
MIN_SLOPE     0
ALLOW_PONDING NO
SKIP_STEADY_STATE NO

START_DATE    09/02/2016
START_TIME    00:00:00
REPORT_START_DATE 09/02/2016
REPORT_START_TIME 00:00:00
END_DATE      09/05/2016
END_TIME      00:00:00
SWEEP_START   01/01
SWEEP_END     12/31
DRY_DAYS      0
REPORT_STEP   00:05:00
WET_STEP      00:05:00
DRY_STEP      00:05:00
ROUTING_STEP  0:00:30
RULE_STEP     00:00:00

INERTIAL_DAMPING PARTIAL
NORMAL_FLOW_LIMITED BOTH
FORCE_MAIN_EQUATION H-W
VARIABLE_STEP  0.75
LENGTHENING_STEP 0
MIN_SURFAREA  12.557
MAX_TRIALS     8
HEAD_TOLERANCE 0.005
SYS_FLOW_TOL  5
LAT_FLOW_TOL  5
MINIMUM_STEP  0.5
THREADS        1
    
```

[EVAPORATION]

```

;; Data Source Parameters
;;-----
CONSTANT  0.0
DRY_ONLY  NO
    
```

[OUTFALLS]

```

;; Name      Elevation Type      Stage Data      Gated      Route To
;;-----
Outfall     0          FREE          NO
    
```

[STORAGE]

```

;; Name      Elev.      MaxDepth      InitDepth      Shape      Curve Name/Params
N/A      Fevap      Psi           Ksat           IMD
    
```

Pond B Outlet Input - Total WQ

```

;; -----
Pond_B      6305      5      1.98      TABULAR      PondB_Volume      0
  0
  
```

[ORIFICES]

```

;; Name      From Node      To Node      Type      Offset      Qcoeff
Gated      CloseTime
;; -----
Orf1      Pond_B      Outfall      SIDE      0      0.65      NO
  0
Orf2      Pond_B      Outfall      SIDE      1.5      0.65      NO
  0
Orf3      Pond_B      Outfall      SIDE      3.0      0.65      NO
  0
  
```

[XSECTIONS]

```

;; Link      Shape      Geom1      Geom2      Geom3      Geom4      Barrels
Culvert
;; -----
Orf1      CIRCULAR      .270833      0      0      0
Orf2      CIRCULAR      .270833      0      0      0
Orf3      CIRCULAR      .270833      0      0      0
  
```

[CURVES]

```

;; Name      Type      X-Value      Y-Value
;; -----
PondB_Volume      Storage      0.00      0.00
PondB_Volume      1.00      24217
PondB_Volume      2.00      26279
PondB_Volume      3.00      28406
PondB_Volume      4.00      30812
PondB_Volume      5.00      32909
PondB_Volume      6.00      34926
  
```

[REPORT]

```

;; Reporting Options
SUBCATCHMENTS ALL
NODES ALL
LINKS ALL
  
```

[TAGS]

[MAP]

```

DIMENSIONS 0.000 0.000 10000.000 10000.000
Units      None
  
```

[COORDINATES]

```

;; Node      X-Coord      Y-Coord
;; -----
Outfall      5747.191      5797.753
Pond_B      2455.056      5808.989
  
```

Pond B Outlet Input - Total WQ

[VERTICES]

```
;; Link      X-Coord      Y-Coord
;; -----
Orf1         4036.344     6277.533
Orf3         4003.304     5165.198
```

[LABELS]

```
;; X-Coord      Y-Coord      Label
2779.762        8023.810     "Pond B Outlet Check" "" "Arial" 10 0 0
```



Pond B Outlet Check - Total WQ

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.013)

\*\*\*\*\*
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.
\*\*\*\*\*

\*\*\*\*\*
Analysis Options
\*\*\*\*\*

Flow Units ..... CFS
Process Model s:
Rainfall/Runoff ..... NO
RDI ..... NO
Snowmelt ..... NO
Groundwater ..... NO
Flow Routing ..... YES
Ponding Allowed ..... NO
Water Quality ..... NO
Flow Routing Method ..... KINWAVE
Starting Date ..... 09/02/2016 00:00:00
Ending Date ..... 09/05/2016 00:00:00
Antecedent Dry Days ..... 0.0
Report Time Step ..... 00:05:00
Routing Time Step ..... 30.00 sec

\*\*\*\*\*
Flow Routing Continuity
\*\*\*\*\*
Table with 3 columns: Category, Volume (acre-feet), Volume (10^6 gal)
Rows include: Dry Weather Inflow, Wet Weather Inflow, Groundwater Inflow, RDI Inflow, External Inflow, External Outflow, Flooding Loss, Evaporation Loss, Exfiltration Loss, Initial Stored Volume, Final Stored Volume, Continuity Error (%)

\*\*\*\*\*
Highest Flow Instability Indexes
\*\*\*\*\*
All links are stable.

\*\*\*\*\*

Pond B Outlet Check - Total WQ

Routing Time Step Summary

\*\*\*\*\*

Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.00  
 Percent Not Converging : 0.00

\*\*\*\*\*

Node Depth Summary

\*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr: min	Reported Max Depth Feet
Outfall I	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
Pond_B	STORAGE	0.60	2.37	6305.37	0 00:00	2.36

\*\*\*\*\*

Node Inflow Summary

\*\*\*\*\*

Flow Balance Error Node Percent	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr: min	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal
Outfall I 0.000	OUTFALL	0.00	0.56	0 00:00	0	0.258
Pond_B 0.024	STORAGE	0.00	0.00	0 00:00	0	0.258

\*\*\*\*\*

Node Flooding Summary

\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*

Pond B Outlet Check - Total WQ

Storage Volume Summary

\*\*\*\*\*

Maximum Outflow Storage Unit CFS	Average Volume 1000 ft3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of Max Occurrence days hr: min
Pond_B 0.56	6.039	2	0	0	34.509	14	0 00:00

\*\*\*\*\*

Outfall Loading Summary

\*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Outfall	62.25	0.21	0.56	0.258
System	62.25	0.21	0.56	0.258

\*\*\*\*\*

Link Flow Summary

\*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr: min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
Orf1	ORIFICE	0.35	0 00:00			0.00
Orf2	ORIFICE	0.20	0 00:00			0.00
Orf3	ORIFICE	0.00	0 00:00			0.00

\*\*\*\*\*

Conduit Surcharge Summary

\*\*\*\*\*

No conduits were surcharged.

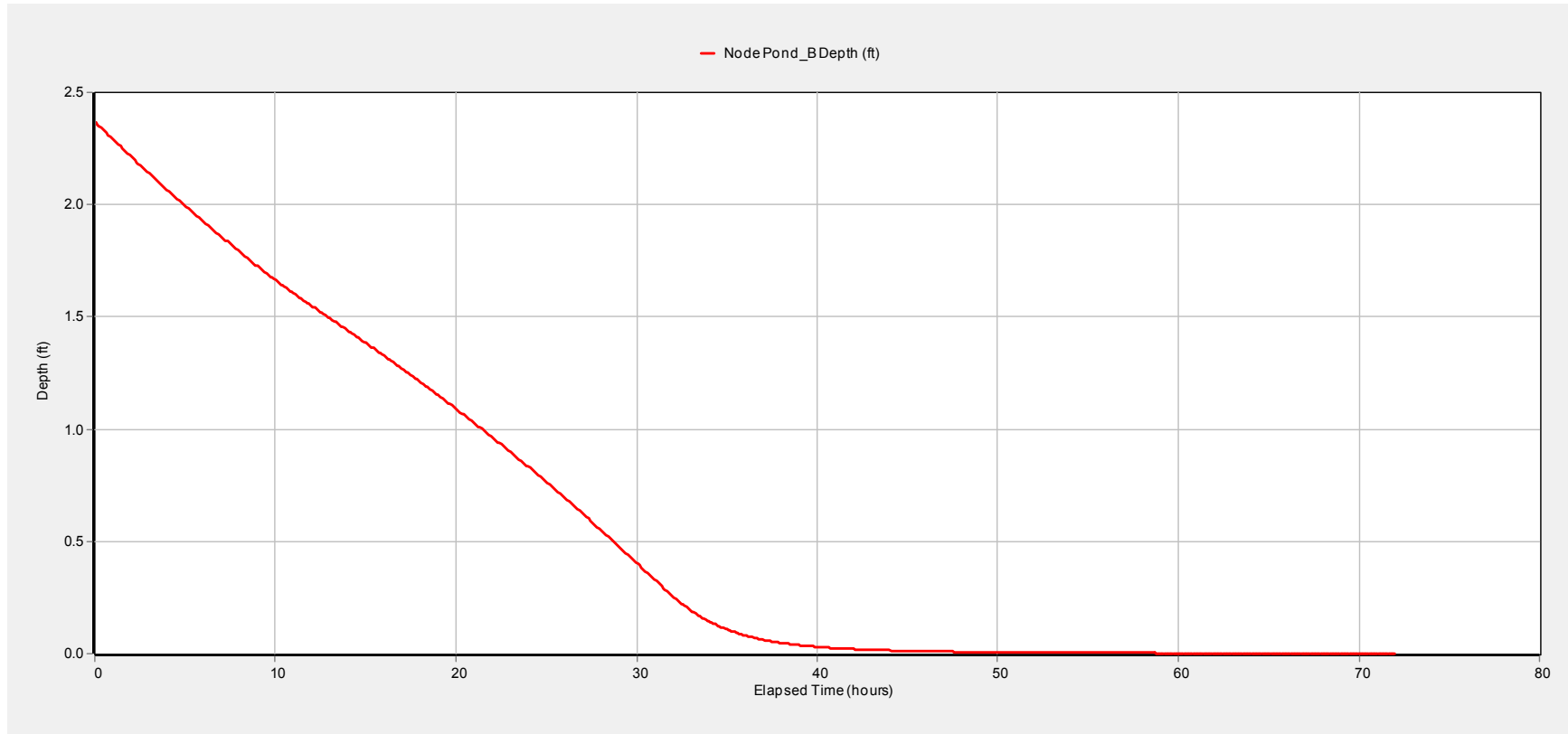
Analysis begun on: Fri Jan 11 10:29:49 2019

Pond B Outlet Check - Total WQ

Analysis ended on: Fri Jan 11 10:29:49 2019

Total elapsed time: < 1 sec

# Total WQ



Pond B Outlet Check Input - EURV

[TITLE]

;; Project Title/Notes

[OPTIONS]

```

;; Option      Value
FLOW_UNITS    CFS
INFILTRATION  HORTON
FLOW_ROUTING  KINWAVE
LINK_OFFSETS  DEPTH
MIN_SLOPE     0
ALLOW_PONDING NO
SKIP_STEADY_STATE NO

START_DATE    09/02/2016
START_TIME    00:00:00
REPORT_START_DATE 09/02/2016
REPORT_START_TIME 00:00:00
END_DATE      09/05/2016
END_TIME      00:00:00
SWEEP_START   01/01
SWEEP_END     12/31
DRY_DAYS      0
REPORT_STEP   00:05:00
WET_STEP      00:05:00
DRY_STEP      00:05:00
ROUTING_STEP  0:00:30
RULE_STEP     00:00:00

INERTIAL_DAMPING PARTIAL
NORMAL_FLOW_LIMITED BOTH
FORCE_MAIN_EQUATION H-W
VARIABLE_STEP   0.75
LENGTHENING_STEP 0
MIN_SURFAREA    12.557
MAX_TRIALS      8
HEAD_TOLERANCE  0.005
SYS_FLOW_TOL    5
LAT_FLOW_TOL    5
MINIMUM_STEP    0.5
THREADS         1
    
```

[EVAPORATION]

```

;; Data Source Parameters
;;-----
CONSTANT      0.0
DRY_ONLY      NO
    
```

[OUTFALLS]

```

;; Name      Elevation Type      Stage Data      Gated      Route To
;;-----
Outfall      0          FREE          NO
    
```

[STORAGE]

```

;; Name      Elev.      MaxDepth      InitDepth      Shape      Curve Name/Params
N/A      Fevap      Psi      Ksat      IMD
    
```

Pond B Outlet Check Input - EURV

```

;;-----
Pond_B      6303      9      5.12      TABULAR      PondB_Vol ume      0
  0
  
```

[ORIFICES]

```

;; Name      From Node      To Node      Type      Offset      Qcoeff
Gated      CloseTime
;;-----
Orf1      Pond_B      Outfall      SIDE      0      0.65      NO
  0
Orf2      Pond_B      Outfall      SIDE      1.5      0.65      NO
  0
Orf3      Pond_B      Outfall      SIDE      3.0      0.65      NO
  0
  
```

[XSECTIONS]

```

;; Link      Shape      Geom1      Geom2      Geom3      Geom4      Barrels
Culvert
;;-----
Orf1      CIRCULAR      0.23958333      0      0      0
Orf2      CIRCULAR      0.23958333      0      0      0
Orf3      CIRCULAR      0.23958333      0      0      0
  
```

[CURVES]

```

;; Name      Type      X-Value      Y-Value
;;-----
PondB_Vol ume      Storage      0.00      1722
PondB_Vol ume      1.00      12437
PondB_Vol ume      2.00      24225
PondB_Vol ume      3.00      26327
PondB_Vol ume      4.00      28436
PondB_Vol ume      5.00      31013
PondB_Vol ume      6.00      33247
PondB_Vol ume      7.00      35432
PondB_Vol ume      8.00      37548
PondB_Vol ume      9.00      39752
  
```

[REPORT]

```

;; Reporting Options
SUBCATCHMENTS ALL
NODES ALL
LINKS ALL
  
```

[TAGS]

[MAP]

```

DIMENSIONS 0.000 0.000 10000.000 10000.000
Units      None
  
```

[COORDINATES]

```

;; Node      X-Coord      Y-Coord
;;-----
  
```

Pond B Outlet Check Input - EURV

Outfall	5747.191	5797.753
Pond_B	2455.056	5808.989

[VERTICES]

;; Link	X-Coord	Y-Coord
Orf1	4036.344	6277.533
Orf3	4003.304	5165.198

[LABELS]

;; X-Coord	Y-Coord	Label
2779.762	8023.810	"Pond B Outlet Check" "" "Arial" 10 0 0



\*\*\*\*\*
NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.
\*\*\*\*\*

\*\*\*\*\*
Analysis Options
\*\*\*\*\*

Flow Units ..... CFS
Process Model s:
Rainfall/Runoff ..... NO
RDI ..... NO
Snowmelt ..... NO
Groundwater ..... NO
Flow Routing ..... YES
Ponding Allowed ..... NO
Water Quality ..... NO
Flow Routing Method ..... KINWAVE
Starting Date ..... 09/02/2016 00:00:00
Ending Date ..... 09/05/2016 00:00:00
Antecedent Dry Days ..... 0.0
Report Time Step ..... 00:05:00
Routing Time Step ..... 30.00 sec

\*\*\*\*\*
Flow Routing Continuity
\*\*\*\*\*
Table with 3 columns: Category, Volume (acre-feet), Volume (10^6 gal)
Rows include: Dry Weather Inflow, Wet Weather Inflow, Groundwater Inflow, RDI Inflow, External Inflow, External Outflow, Flooding Loss, Evaporation Loss, Exfiltration Loss, Initial Stored Volume, Final Stored Volume, Continuity Error (%)

\*\*\*\*\*
Highest Flow Instability Indexes
\*\*\*\*\*
All links are stable.

\*\*\*\*\*

Pond B Outlet Check - EURV + Offsite WQ

Routing Time Step Summary

\*\*\*\*\*

Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.00  
 Percent Not Converging : 0.00

\*\*\*\*\*

Node Depth Summary

\*\*\*\*\*

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr: min	Reported Max Depth Feet
Outfall I	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
Pond_B	STORAGE	1.79	5.12	6308.12	0 00:00	5.11

\*\*\*\*\*

Node Inflow Summary

\*\*\*\*\*

Flow Balance Error Node Percent	Type	Maximum Lateral Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr: min	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal
Outfall I 0.000	OUTFALL	0.00	1.30	0 00:00	0	0.834
Pond_B 0.017	STORAGE	0.00	0.00	0 00:00	0	0.834

\*\*\*\*\*

Node Flooding Summary

\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*

Pond B Outlet Check - EURV + Offsite WQ

Storage Volume Summary

\*\*\*\*\*

Maximum Outflow Storage Unit CFS	Average Volume 1000 ft3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of Max Occurrence days hr: min
Pond_B 1.30	28.328	11	0	0	111.511	45	0 00:00

\*\*\*\*\*

Outfall Loading Summary

\*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Outfall	95.44	0.45	1.30	0.834
System	95.44	0.45	1.30	0.834

\*\*\*\*\*

Link Flow Summary

\*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr: min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
Orf1	ORIFICE	0.53	0 00:00			0.00
Orf2	ORIFICE	0.44	0 00:00			0.00
Orf3	ORIFICE	0.33	0 00:00			0.00

\*\*\*\*\*

Conduit Surcharge Summary

\*\*\*\*\*

No conduits were surcharged.

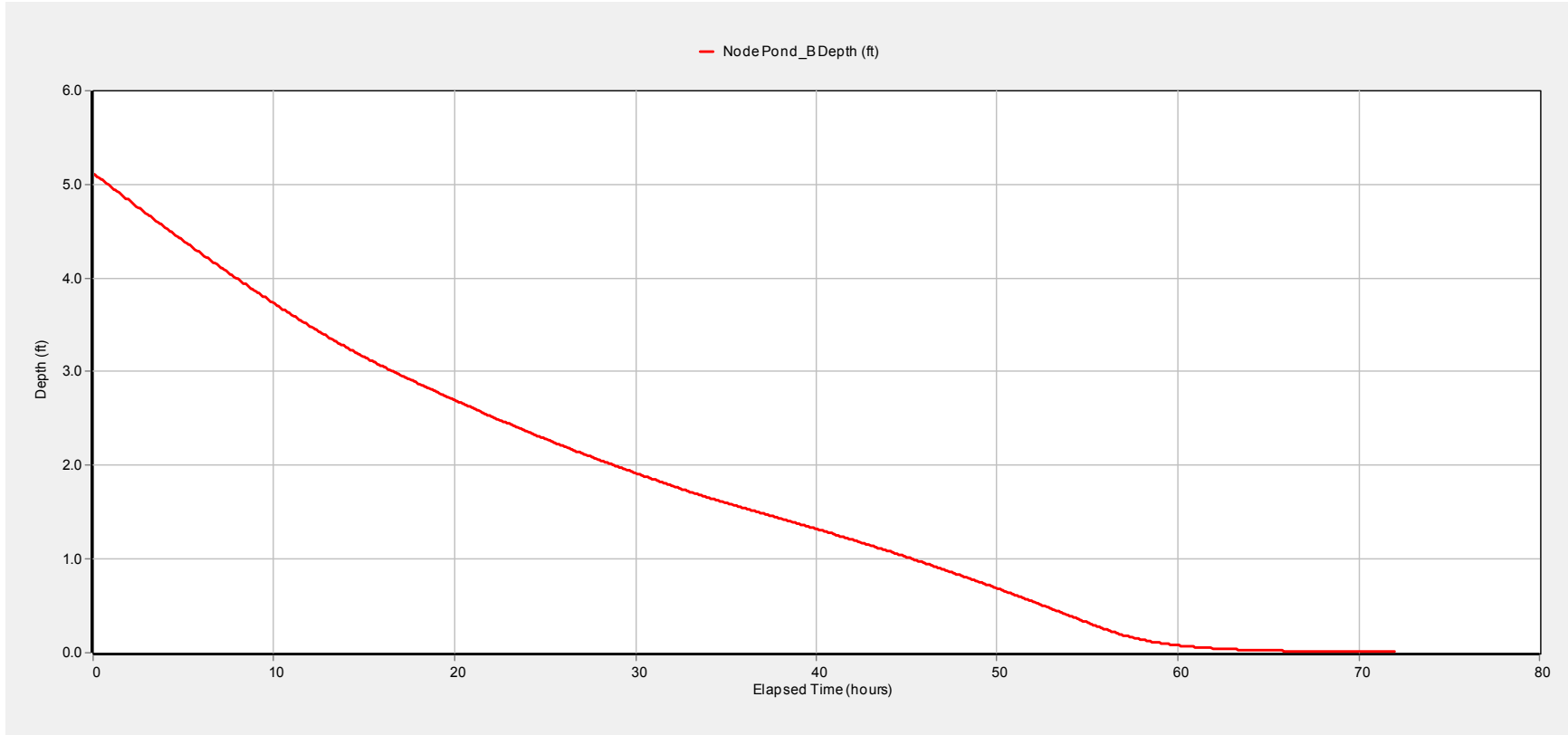
Analysis begun on: Fri Jan 11 10:33:38 2019

Pond B Outlet Check - EURV + Offsite WQ

Analysis ended on: Fri Jan 11 10:33:38 2019

Total elapsed time: < 1 sec

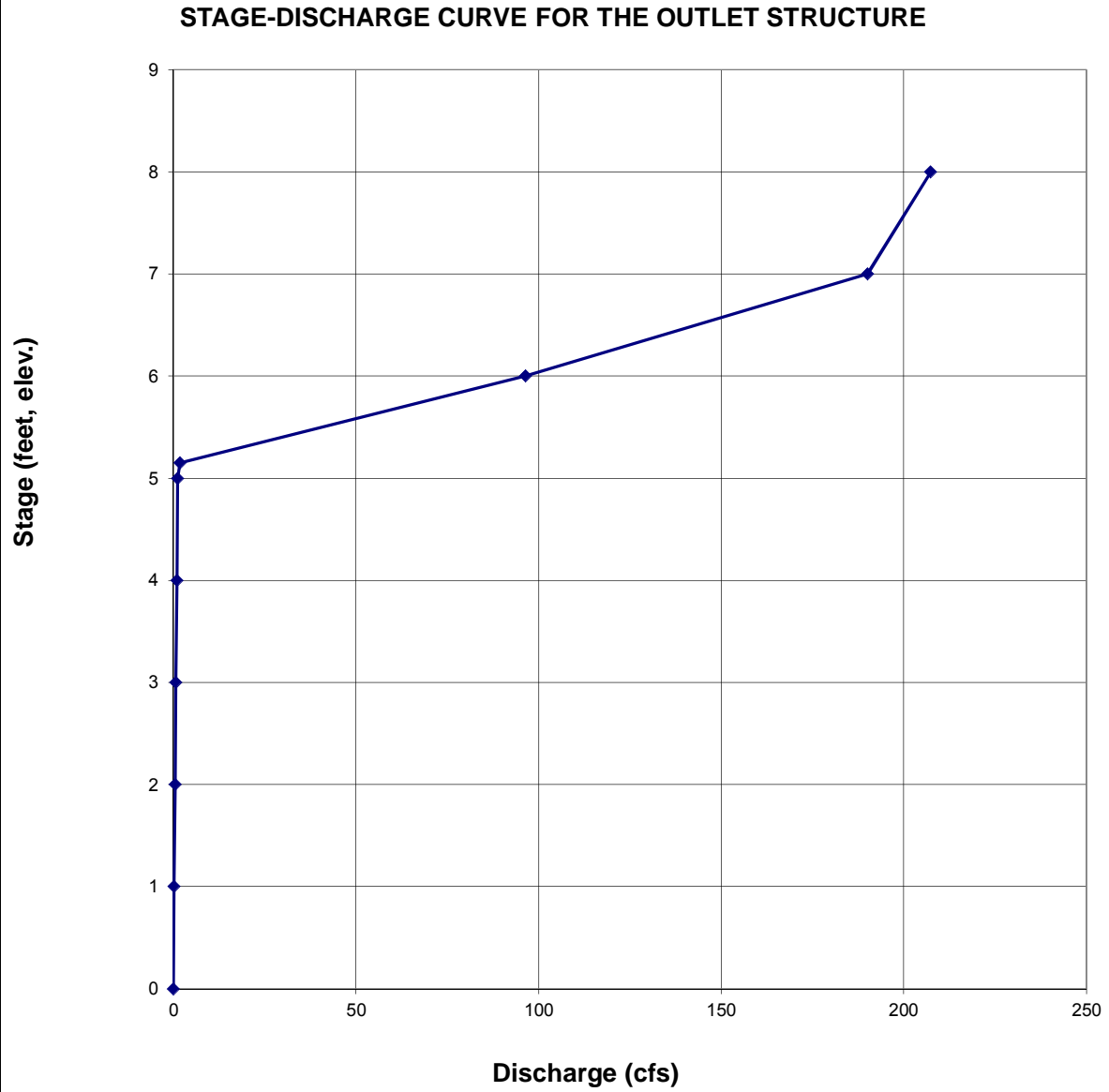
# EURV + OFFSITE WQ





STAGE-DISCHARGE SIZING OF THE WEIRS AND ORIFICES (INLET CONTROL)

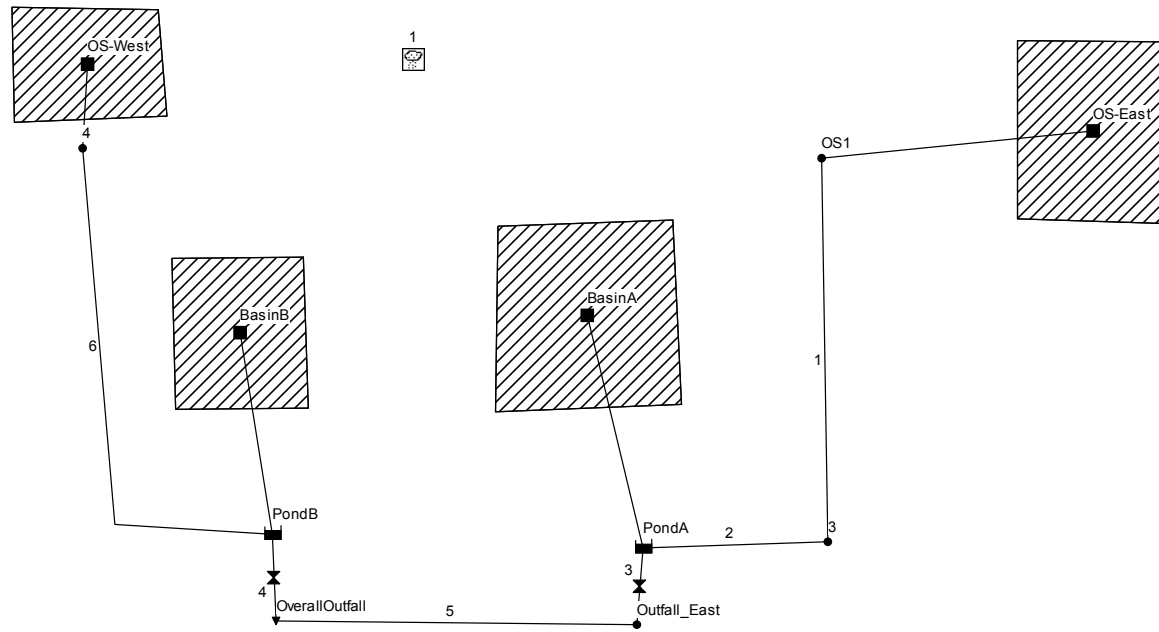
Project: Crest at Woodmen  
Basin ID: Pond B



# **SWMM MODEL – Proposed CONDITIONS**



Proposed Model



Crest at Woodmen MDDP Amend. Input

[TITLE]

;; Project Title/Notes

[OPTIONS]

;; Option Value  
 FLOW\_UNITS CFS  
 INFILTRATION HORTON  
 FLOW\_ROUTING KINWAVE  
 LINK\_OFFSETS DEPTH  
 MIN\_SLOPE 0  
 ALLOW\_PONDING NO  
 SKIP\_STEADY\_STATE NO

START\_DATE 08/24/2016  
 START\_TIME 00:00:00  
 REPORT\_START\_DATE 08/24/2016  
 REPORT\_START\_TIME 00:00:00  
 END\_DATE 08/24/2016  
 END\_TIME 02:00:00  
 SWEEP\_START 01/01  
 SWEEP\_END 12/31  
 DRY\_DAYS 0  
 REPORT\_STEP 00:05:00  
 WET\_STEP 00:05:00  
 DRY\_STEP 00:05:00  
 ROUTING\_STEP 0:00:30  
 RULE\_STEP 00:00:00

INERTIAL\_DAMPING PARTIAL  
 NORMAL\_FLOW\_LIMITED BOTH  
 FORCE\_MAIN\_EQUATION H-W  
 VARIABLE\_STEP 0.75  
 LENGTHENING\_STEP 0  
 MIN\_SURFAREA 12.557  
 MAX\_TRIALS 8  
 HEAD\_TOLERANCE 0.005  
 SYS\_FLOW\_TOL 5  
 LAT\_FLOW\_TOL 5  
 MINIMUM\_STEP 0.5  
 THREADS 1

[EVAPORATION]

;; Data Source Parameters  
 ;;-----  
 CONSTANT 0.0  
 DRY\_ONLY NO

[RAINGAGES]

;; Name Format Interval SCF Source  
 ;;-----  
 1 CUMULATIVE 0:05 1.0 TIMESERIES CS\_100-yr

[SUBCATCHMENTS]

;; Name Rain Gage Outlet Area %Imperv Width %Slope  
 CurbLen SnowPack

Crest at Woodmen MDDP Amend. Input

```

;;-----
OS-East      1          OS1          33.9    77      6000    2.5    0
Basi nA     1          PondA          49.8    86.5    1500    1      0
Basi nB     1          PondB          31.67   70      800     3      0
OS-West     1           4            2.92    50      500     1      0
  
```

[SUBAREAS]

```

;; Subcatchment  N-Imperv  N-Perv  S-Imperv  S-Perv  PctZero  RouteTo
PctRouted
;;-----
  
```

```

OS-East      0.011  0.24  0.1  0.35  25  OUTLET
Basi nA     0.011  0.24  0.1  0.35  25  OUTLET
Basi nB     0.011  0.24  0.1  0.35  25  OUTLET
OS-West     0.011  0.24  0.1  0.35  25  OUTLET
  
```

[INFILTRATION]

```

;; Subcatchment  MaxRate  MinRate  Decay  DryTime  MaxInfil
;;-----
OS-East      4.5      0.6      6.48   7        0
Basi nA     4.5      0.6      6.48   7        0
Basi nB     4.5      0.6      6.48   7        0
OS-West     4.5      .6       6.48   7        0
  
```

[JUNCTIONS]

```

;; Name          El evati on  MaxDepth  Ini tDepth  SurDepth  Aponded
;;-----
OS1              6350        8         0          0         0
Outfall_East    6312        0         0          0         0
4                6324.5     5         0          0         0
  
```

[OUTFALLS]

```

;; Name          El evati on  Type      Stage Data  Gated  Route To
;;-----
OverallOutfall  6303        FREE      NO
  
```

[STORAGE]

```

;; Name          El ev.  MaxDepth  Ini tDepth  Shape  Curve Name/Params
N/A    Fevap  Psi      Ksat      IMD
;;-----
PondA      6310    10       0          TABULAR  PondA_Vol  0
0
PondB      6303    8        0          TABULAR  PondB_Vol  0
0
  
```

[CONDUITS]

```

;; Name          From Node  To Node  Length  Roughness  InOffset
OutOffset  Ini tFlow  MaxFlow
;;-----
  
```

Crest at Woodmen MDDP Amend. Input

1	0	0	OS1	PondA	880	0.035	0	0
5	0	0	Outfall_East	Overall Outfall	400	0.01	0	0
6	0	0	4	PondB	1330	0.013	0	0

[OUTLETS]

;; Name	From Node	To Node	Offset	Type	
QTable/Qcoeff	Qexpon	Gated			
3	PondA	Outfall_East	0	TABULAR/DEPTH	PondA_Outlet
	NO				
4	PondB	Overall Outfall	0	TABULAR/DEPTH	PondB_Outlet
	NO				

[XSECTIONS]

;; Link	Shape	Geom1	Geom2	Geom3	Geom4	Barrels
Culvert						
1	DUMMY	0	0	0	0	1
5	DUMMY	0	0	0	0	1
6	CIRCULAR	1.5	0	0	0	1

[LOSSES]

;; Link	Kentry	Kexit	Kavg	Flap Gate	Seepage
1	0.5	1	0	NO	0
6	0.5	1	0	NO	0

[CURVES]

;; Name	Type	X-Value	Y-Value
PondA_Outlet	Rating	0.00	0.0
PondA_Outlet		0.50	0.2
PondA_Outlet		1.00	0.3
PondA_Outlet		1.50	0.4
PondA_Outlet		2.00	0.4
PondA_Outlet		2.50	0.5
PondA_Outlet		3.00	0.7
PondA_Outlet		3.50	0.9
PondA_Outlet		4.00	1.0
PondA_Outlet		4.50	1.1
PondA_Outlet		5.00	1.1
PondA_Outlet		5.50	1.4
PondA_Outlet		6.00	1.6
PondA_Outlet		6.50	35.1
PondA_Outlet		7.00	114.6
PondA_Outlet		7.5	198.9

Crest at Woodmen MDDP Amend. Input

PondA_Outlet		8	207.4
PondA_Outlet		8.5	215.5
PondA_Outlet		9	223.4
PondA_Outlet		9.5	231.0
PondA_Outlet		10	238.3
PondA_Outlet		10.5	245.4
PondA_Outlet		11	252.3
PondA_Outlet		11.5	259.0
PondA_Outlet		12	265.6

;			
PondB_Outlet	Rating	0.00	0.0
PondB_Outlet		1.00	0.2
PondB_Outlet		2.00	0.5
PondB_Outlet		3.00	0.7
PondB_Outlet		4.00	1.1
PondB_Outlet		5.00	1.3
PondB_Outlet		5.12	1.3
PondB_Outlet		6.00	96.6
PondB_Outlet		7.00	190.1
PondB_Outlet		8.00	207.4

;			
PondA_Vol	Storage	0.00	272
PondA_Vol		1.00	2591
PondA_Vol		2.00	10979
PondA_Vol		3.00	28075
PondA_Vol		4.00	43259
PondA_Vol		5.00	48157
PondA_Vol		6.00	52238
PondA_Vol		7.00	56387
PondA_Vol		8.00	60626
PondA_Vol		9.00	64959
PondA_Vol		10.00	69377
PondA_Vol		11.00	73891
PondA_Vol		12.00	78503

;			
PondB_Vol	Storage	0.00	1722
PondB_Vol		1.00	12437
PondB_Vol		2.00	24225
PondB_Vol		3.00	26327
PondB_Vol		4.00	28436
PondB_Vol		5.00	31013
PondB_Vol		6.00	33247
PondB_Vol		7.00	35432
PondB_Vol		8.00	37548
PondB_Vol		9.00	39752

[TIMESERIES]

;; Name	Date	Time	Value
-----			
CS_100-yr		0	0
CS_100-yr		0:05	0.03528
CS_100-yr		0:10	0.11592
CS_100-yr		0:15	0.19908
CS_100-yr		0:20	0.3024
CS_100-yr		0:25	0.45108

Crest at Woodmen MDDP Amend. Input

CS_100-yr	0: 30	0. 65016
CS_100-yr	0: 35	1. 06092
CS_100-yr	0: 40	1. 79424
CS_100-yr	0: 45	2. 07648
CS_100-yr	0: 50	2. 24784
CS_100-yr	0: 55	2. 3562
CS_100-yr	1: 00	2. 44944
CS_100-yr	1: 05	2. 53008
CS_100-yr	1: 10	2. 56536
CS_100-yr	1: 15	2. 5956
CS_100-yr	1: 20	2. 62332
CS_100-yr	1: 25	2. 65104
CS_100-yr	1: 30	2. 67876
CS_100-yr	1: 35	2. 70144
CS_100-yr	1: 40	2. 72664
CS_100-yr	1: 45	2. 74932
CS_100-yr	1: 50	2. 772
CS_100-yr	1: 55	2. 79468
CS_100-yr	2: 00	2. 81988
;		
CS_5-yr	0	0
CS_5-yr	0: 05	0. 021
CS_5-yr	0: 10	0. 069
CS_5-yr	0: 15	0. 1185
CS_5-yr	0: 20	0. 18
CS_5-yr	0: 25	0. 2685
CS_5-yr	0: 30	0. 387
CS_5-yr	0: 35	0. 6315
CS_5-yr	0: 40	1. 068
CS_5-yr	0: 45	1. 236
CS_5-yr	0: 50	1. 338
CS_5-yr	0: 55	1. 4025
CS_5-yr	1: 00	1. 458
CS_5-yr	1: 05	1. 506
CS_5-yr	1: 10	1. 527
CS_5-yr	1: 15	1. 545
CS_5-yr	1: 20	1. 5615
CS_5-yr	1: 25	1. 578
CS_5-yr	1: 30	1. 5945
CS_5-yr	1: 35	1. 608
CS_5-yr	1: 40	1. 623
CS_5-yr	1: 45	1. 6365
CS_5-yr	1: 50	1. 65
CS_5-yr	1: 55	1. 6635
CS_5-yr	2: 00	1. 6785

[REPORT]

;; Reporting Options  
 SUBCATCHMENTS ALL  
 NODES ALL  
 LINKS ALL

[TAGS]

[MAP]

Crest at Woodmen MDDP Amend. Input

DIMENSIONS 0.000 0.000 10000.000 10000.000

Units None

[COORDINATES]

;; Node	X-Coord	Y-Coord
OS1	4377.753	7411.894
Outfall I_East	2604.626	2929.515
4	-2725.771	7511.013
Overall Outfall	-864.537	2962.555
PondA	2659.692	3667.401
PondB	-897.577	3799.559

[VERTICES]

;; Link	X-Coord	Y-Coord
6	-2406.388	3887.665

[Polygons]

;; Subcatchment	X-Coord	Y-Coord
OS-East	7714.758	8535.242
OS-East	7736.784	6784.141
OS-East	6250.000	6828.194
OS-East	6250.000	8546.256
BasinA	2916.116	6855.457
BasinA	3004.222	5082.329
BasinA	1220.081	5016.250
BasinA	1242.107	6800.391
BasinB	-600.220	6464.758
BasinB	-556.167	5011.013
BasinB	-1822.687	5000.000
BasinB	-1866.740	6453.744
OS-West	-1993.392	8846.366
OS-West	-1916.300	7822.137
OS-West	-3370.044	7767.070
OS-West	-3403.084	8868.392

[SYMBOLS]

;; Gage	X-Coord	Y-Coord
1	468.062	8359.031

[LABELS]

;; X-Coord	Y-Coord	Label
-505.952	9476.190	"Proposed Model" "" "Arial" 10 0 0

WARNING 10: crest elevation is below downstream invert for regulator Link 3

\*\*\*\*\*  
 NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
 \*\*\*\*\*

\*\*\*\*\*  
 Analysis Options  
 \*\*\*\*\*

Flow Units ..... CFS  
 Process Models:  
   Rainfall/Runoff ..... YES  
   RDI ..... NO  
   Snowmelt ..... NO  
   Groundwater ..... NO  
   Flow Routing ..... YES  
   Ponding Allowed ..... NO  
   Water Quality ..... NO  
 Infiltration Method ..... HORTON  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... 08/24/2016 00:00:00  
 Ending Date ..... 08/24/2016 02:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:05:00  
 Wet Time Step ..... 00:05:00  
 Dry Time Step ..... 00:05:00  
 Routing Time Step ..... 30.00 sec

*****	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
*****	-----	-----
Total Precipitation .....	16.398	1.663
Evaporation Loss .....	0.000	0.000
Infiltration Loss .....	3.230	0.328
Surface Runoff .....	11.917	1.209
Final Storage .....	1.398	0.142
Continuity Error (%) .....	-0.899	

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10 <sup>6</sup> gal
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	11.844	3.860
Groundwater Inflow .....	0.000	0.000
RDI Inflow .....	0.000	0.000
External Inflow .....	0.000	0.000
External Outflow .....	5.319	1.733



Crest at Woodmen MDDP Amend. - 5 yr

Flooding Loss .....	0.000	0.000
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000
Initial Stored Volume ....	0.000	0.000
Final Stored Volume .....	6.514	2.123
Continuity Error (%) .....	0.099	

\*\*\*\*\*  
 Highest Flow Instability Indexes  
 \*\*\*\*\*  
 All links are stable.

\*\*\*\*\*  
 Routing Time Step Summary  
 \*\*\*\*\*  
 Minimum Time Step : 30.00 sec  
 Average Time Step : 30.00 sec  
 Maximum Time Step : 30.00 sec  
 Percent in Steady State : 0.00  
 Average Iterations per Step : 1.32  
 Percent Not Converging : 0.00

\*\*\*\*\*  
 Subcatchment Runoff Summary  
 \*\*\*\*\*

Total Runoff		Total Peak Precip Runoff	Total Runoff	Total Evap	Total Infil	Imperv Runoff	Perv Runoff
Subcatchment	in	in	in	in	in	in	in
	10 <sup>6</sup> gal	CFS	in	in	in	in	in
OS-East		1.66	0.00	0.00	0.35	1.22	0.02
1.24	1.14	136.34	0.745				
Basi nA		1.66	0.00	0.00	0.21	1.29	0.00
1.29	1.75	144.64	0.777				
Basi nB		1.66	0.00	0.00	0.46	1.07	0.01
1.08	0.93	91.54	0.649				
OS-West		1.66	0.00	0.00	0.76	0.79	0.02
0.81	0.06	7.61	0.489				

\*\*\*\*\*  
 Node Depth Summary  
 \*\*\*\*\*

Crest at Woodmen MDDP Amend. - 5 yr

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr: mi n	Reported Max Depth Feet
OS1	JUNCTI ON	0. 00	0. 00	6350. 00	0 00: 00	0. 00
Outfall I _East	JUNCTI ON	0. 00	0. 00	6312. 00	0 00: 00	0. 00
4	JUNCTI ON	0. 25	0. 81	6325. 31	0 00: 45	0. 79
Overall I Outfall I	OUTFALL	0. 00	0. 00	6303. 00	0 00: 00	0. 00
PondA	STORAGE	4. 73	6. 96	6316. 96	0 00: 58	6. 94
PondB	STORAGE	3. 24	5. 19	6308. 19	0 01: 24	5. 19

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

Flow Balance Error Node Percent	Type	Maximum Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr: mi n	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal
---------------------------------	------	--------------------	--------------------------	--------------------------------------	--------------------------------	------------------------------

OS1 0. 000	JUNCTI ON	136. 34	136. 34	0 00: 45	1. 14	1. 14
Outfall I _East 0. 000	JUNCTI ON	0. 00	107. 78	0 00: 58	0	1. 59
4 0. 000	JUNCTI ON	7. 61	7. 61	0 00: 45	0. 0642	0. 0642
Overall I Outfall I 0. 000	OUTFALL	0. 00	108. 95	0 00: 58	0	1. 73
PondA 0. 124	STORAGE	144. 64	280. 98	0 00: 45	1. 74	2. 87
PondB -0. 001	STORAGE	91. 54	97. 59	0 00: 45	0. 923	0. 986

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

No nodes were flooded.

\*\*\*\*\*  
Storage Volume Summary  
\*\*\*\*\*

Crest at Woodmen MDDP Amend. - 5 yr

Maximum Outflow Storage Unit CFS	Average Volume 1000 ft3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft3	Max Pcnt Full	Time of Max Occurrence days hr: min
PondA 107.78	123.514	31	0	0	211.270	53	0 00:58
PondB 8.88	66.418	32	0	0	113.730	54	0 01:23

\*\*\*\*\*  
**Outfall Loading Summary**  
 \*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10^6 gal
Overall Outfall	95.00	33.92	108.95	1.733
System	95.00	33.92	108.95	1.733

\*\*\*\*\*  
**Link Flow Summary**  
 \*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr: min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
1	DUMMY	136.34	0 00:45			
5	DUMMY	107.78	0 00:58			
6	CONDUIT	7.07	0 00:47	8.26	0.53	0.51
3	DUMMY	107.78	0 00:58			
4	DUMMY	8.88	0 01:24			

\*\*\*\*\*  
**Conduit Surcharge Summary**  
 \*\*\*\*\*

No conduits were surcharged.

Crest at Woodmen MDDP Amend. - 5 yr

Analysis begun on: Fri Jan 11 10:45:27 2019

Analysis ended on: Fri Jan 11 10:45:27 2019

Total elapsed time: < 1 sec

WARNING 10: crest elevation is below downstream invert for regulator Link 3

\*\*\*\*\*  
 NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.  
 \*\*\*\*\*

\*\*\*\*\*  
 Analysis Options  
 \*\*\*\*\*

Flow Units ..... CFS  
 Process Models:  
   Rainfall/Runoff ..... YES  
   RDI ..... NO  
   Snowmelt ..... NO  
   Groundwater ..... NO  
   Flow Routing ..... YES  
   Ponding Allowed ..... NO  
   Water Quality ..... NO  
 Infiltration Method ..... HORTON  
 Flow Routing Method ..... KINWAVE  
 Starting Date ..... 08/24/2016 00:00:00  
 Ending Date ..... 08/24/2016 02:00:00  
 Antecedent Dry Days ..... 0.0  
 Report Time Step ..... 00:05:00  
 Wet Time Step ..... 00:05:00  
 Dry Time Step ..... 00:05:00  
 Routing Time Step ..... 30.00 sec

*****	Volume	Depth
Runoff Quantity Continuity	acre-feet	inches
*****	-----	-----
Total Precipitation .....	27.549	2.795
Evaporation Loss .....	0.000	0.000
Infiltration Loss .....	3.372	0.342
Surface Runoff .....	22.221	2.254
Final Storage .....	2.233	0.227
Continuity Error (%) .....	-1.007	

*****	Volume	Volume
Flow Routing Continuity	acre-feet	10 <sup>6</sup> gal
*****	-----	-----
Dry Weather Inflow .....	0.000	0.000
Wet Weather Inflow .....	22.101	7.202
Groundwater Inflow .....	0.000	0.000
RDI Inflow .....	0.000	0.000
External Inflow .....	0.000	0.000
External Outflow .....	15.375	5.010

Crest at Woodmen MDDP Amend. - 100 yr

Flooding Loss .....	0.003	0.001
Evaporation Loss .....	0.000	0.000
Exfiltration Loss .....	0.000	0.000
Initial Stored Volume ....	0.000	0.000
Final Stored Volume .....	6.703	2.184
Continuity Error (%) .....	0.095	

\*\*\*\*\*  
 Highest Flow Instability Indexes  
 \*\*\*\*\*

Link 6 (3)  
 Link 1 (2)

\*\*\*\*\*  
 Routing Time Step Summary  
 \*\*\*\*\*

Minimum Time Step	:	30.00 sec
Average Time Step	:	30.00 sec
Maximum Time Step	:	30.00 sec
Percent in Steady State	:	0.00
Average Iterations per Step	:	1.39
Percent Not Converging	:	0.00

\*\*\*\*\*  
 Subcatchment Runoff Summary  
 \*\*\*\*\*

Total Runoff Subcatchment in		Total Runoff 10 <sup>6</sup> gal	Total Peak Runoff Precip in CFS	Total Runoff in	Total Evap in	Total Infil in	Imperv Runoff in	Perv Runoff in
OS-East	2.33	2.14	2.79	0.00	0.00	0.37	2.09	0.24
			0.833					
Basi nA	2.35	3.18	2.79	0.00	0.00	0.21	2.25	0.11
			0.842					
Basi nB	2.06	1.77	2.79	0.00	0.00	0.48	1.86	0.21
			0.738					
OS-West	1.79	0.14	2.79	0.00	0.00	0.79	1.36	0.43
			0.640					

\*\*\*\*\*  
 Node Depth Summary  
 \*\*\*\*\*

Crest at Woodmen MDDP Amend. - 100 yr

Node	Type	Average Depth Feet	Maximum Depth Feet	Maximum HGL Feet	Time of Max Occurrence days hr: mi n	Reported Max Depth Feet
OS1	JUNCTI ON	0. 00	0. 00	6350. 00	0 00: 00	0. 00
Outfall I _East	JUNCTI ON	0. 00	0. 00	6312. 00	0 00: 00	0. 00
4	JUNCTI ON	0. 49	5. 00	6329. 50	0 00: 44	5. 00
Overall Outfall I	OUTFALL	0. 00	0. 00	6303. 00	0 00: 00	0. 00
PondA	STORAGE	5. 45	8. 77	6318. 77	0 00: 56	8. 77
PondB	STORAGE	3. 74	5. 85	6308. 85	0 00: 56	5. 84

\*\*\*\*\*  
Node Inflow Summary  
\*\*\*\*\*

Flow Balance Error Node Percent	Type	Maximum Inflow CFS	Maximum Total Inflow CFS	Time of Max Occurrence days hr: mi n	Lateral Inflow Volume 10^6 gal	Total Inflow Volume 10^6 gal
---------------------------------	------	--------------------	--------------------------	--------------------------------------	--------------------------------	------------------------------

OS1 0. 000	JUNCTI ON	260. 74	260. 74	0 00: 45	2. 13	2. 13
Outfall I _East 0. 000	JUNCTI ON	0. 00	219. 83	0 00: 56	0	3. 96
4 0. 000	JUNCTI ON	15. 00	15. 00	0 00: 45	0. 141	0. 141
Overall Outfall I 0. 000	OUTFALL	0. 00	299. 67	0 00: 56	0	5. 01
PondA 0. 075	STORAGE	285. 86	546. 60	0 00: 45	3. 16	5. 3
PondB 0. 164	STORAGE	173. 76	185. 40	0 00: 45	1. 76	1. 9

\*\*\*\*\*  
Node Flooding Summary  
\*\*\*\*\*

Flooding refers to all water that overflows a node, whether it ponds or not.

Hours	Maximum Rate	Time of Max Occurrence	Total Flood Volume	Maximum Ponded Volume
-------	--------------	------------------------	--------------------	-----------------------

Node	Crest at Woodmen MDDP Amend. - 100 yr Flooded	CFS	days	hr: min	10 <sup>6</sup> gal	1000 ft <sup>3</sup>
4	0.05	1.29	0	00:46	0.001	0.000

\*\*\*\*\*  
Storage Volume Summary  
\*\*\*\*\*

Maximum Outflow Storage Unit CFS	Average Volume 1000 ft <sup>3</sup>	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 ft <sup>3</sup>	Max Pcnt Full	Time of Max Occurrence days hr: min
PondA 219.83	158.339	39	0	0	320.471	80	0 00:55
PondB 79.84	79.699	38	0	0	134.841	64	0 00:55

\*\*\*\*\*  
Outfall Loading Summary  
\*\*\*\*\*

Outfall Node	Flow Freq Pcnt	Avg Flow CFS	Max Flow CFS	Total Volume 10 <sup>6</sup> gal
Overall Outfall	95.42	97.57	299.67	5.010
System	95.42	97.57	299.67	5.010

\*\*\*\*\*  
Link Flow Summary  
\*\*\*\*\*

Link	Type	Maximum  Flow  CFS	Time of Max Occurrence days hr: min	Maximum  Veloc  ft/sec	Max/ Full Flow	Max/ Full Depth
1	DUMMY	260.74	0 00:45			
5	DUMMY	219.83	0 00:56			
6	CONDUIT	14.03	0 00:47	9.50	1.05	0.89
3	DUMMY	219.83	0 00:56			
4	DUMMY	79.84	0 00:56			



\*\*\*\*\*  
 Conduit Surcharge Summary  
 \*\*\*\*\*

Conduit	----- Both Ends	Hours Full Upstream	----- Dnstream	Hours Above Full Normal Flow	Hours Capacity Limited
6	0.04	0.04	0.04	0.03	0.04

Analysis begun on: Fri Jan 11 10:45:13 2019  
 Analysis ended on: Fri Jan 11 10:45:13 2019  
 Total elapsed time: < 1 sec

**Appendix E**  
**Drainage Maps**



