# MASTER DEVELOPMENT DRAINAGE PLAN

FOR

# **FALCON TRUCKING FILING NO.1**

June 2023

Prepared for:

Falcon Trucking Co. 8800 Dix Street Detroit, MI 48209 (719) 475-7621

Prepared by:



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Project #29-007

#### MASTER DEVELOPMENT DRAINAGE PLAN FOR FALCON TRUCKING FILING NO. 1

#### **DRAINAGE REPORT STATEMENTS**

#### ENGINEER'S STATEMENT

This report and plan for the drainage design of Falcon Trucking Filing No. 1 was prepared under my supervision and is correct to the best of my knowledge and belief. Said drainage report and plan has been prepared in accordance with the City of Colorado Springs Drainage Criteria Manual and is in conformity with the master plan of the drainage basin. I understand that the City of Colorado Springs does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.



Virgil A. Sanchez, P.E. #37160 For and on Behalf of M&S Civil Consultants, Inc

#### **DEVELOPER'S STATEMENT**

Falcon Trucking Co. hereby certifies that the drainage facilities for Falcon Trucking Filing No. 1, shall be constructed according to the design presented in this report. I understand that the City of Colorado Springs does not and will not assume liability for the drainage facilities designed and/or certified by my engineer and that are submitted to the City of Colorado Springs pursuant to Section 7.7.906 of the City Code; and cannot, on behalf of the Falcon Trucking Filing No. 1, guarantee that final drainage design review will absolve Falcon Trucking Co. and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the final plat does not imply approval of my engineer's drainage design.

DATE: /

TITLE: VICE PRESIDENT

ADDRESS: Falcon Trucking Co. 8800 Dix Street Detroit, MI 48209

CITY OF COLORADO SPRINGS

Filed in accordance with Section 7.7.906 of the Code of the City of Colorado Springs} 2001, as amended,

BY:

alua l'ellacter

DATE: 06/12/2023

For the City Engineer Heidi McMacken

CONDITIONS: "The City of Colorado Springs approves these plans based upon the non-jurisdictional status of the facility. If upon State review the classification changes to jurisdictional, additional City review and approval will be necessary."

A final drainage report shall be required with a submittal of the final plat and an amendment to this document is likely upon determination of a site specific development plan.

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# MASTER DEVELOPMENT DRAINAGE PLAN FOR FALCON TRUCKING FILING NO. 1

#### PURPOSE

This document is intended to serve as the Master Development Drainage Plan for Falcon Trucking Filing No. 1. A Zone Change, Master Plan Amendment and Concept Plan were approved in February 2022 to rezone the Falcon Trucking property from light industrial uses (PIP-1) to Planned Unit Development (PUD) to accommodate Medium-High Density Residential (3.5-7.99 du/ac) on 16.078 acres, Commercial/ High Density Residential (12-24.99 du/ac) on 14.309 acres, and Commercial uses on 5.34 acres.

The currently proposed Zone Change, Master Plan Amendment and Concept Plan will retain the PUD zoning but proposes to remove the Commercial uses and reallocate the residential uses/ densities. The revised plans will allow High Density Residential (12-24.99 du/ac) on the western 19.65 acres of the site and Residential Medium-High Density (8-11.99 du/ac) on the eastern 16.08 acres. The primary purpose of this report at this time is provide ample information of the support of the rezone and to ensure that post development runoff is routed through the site safely and in a manner that satisfies the requirements set forth by the El Paso County and City of Colorado Springs Drainage Criteria Manual. A final drainage report shall be required with a submittal of the final plat and an amendment to this document is likely upon determination of a site specific development plan.

It is important to note that at the time of the writing of this report, the preliminary designs for both Marksheffel Roadway and Barnes Roads were being evaluated by other consultants. As such the given the nature of this project being to seek a rezone the drainage analysis provided seeks only to match historic discharge at the boundary lines and determine that there is ample room for detention and water quality treatment.

#### **GENERAL LOCATION AND DESCRIPTION**

Falcon Trucking Filing No.1 is located northeast of the intersection of Marksheffel Road and Graphite Drive, in a portion of the southwest quarter of the southwest quarter (SW1/4, SW1/4) of Section 21, and a portion of the northwest quarter of the northwest quarter (NW1/4, NW1/4) of Township 13 South, Range 65 West of the 6<sup>th</sup> Principal Meridian, Colorado Springs, El Paso County, Colorado. The site is bound on the south by Graphite Drive, to the north by unplatted land owned by the City of Colorado Springs – Rec. No. 96020361 and by a track of land owned by BLH No. 2 LLC that was set aside for Barnes Roadway extension and to the west by Marksheffel Road Right of Way, and to the east by Enclaves at Mountain Vista Ranch, Filing No's 5 and 6 (Rec. No's – 220714464 and 220714464). The parcel is located within the Sand Creek Drainage Basin. Drainage flows from this site are tributary to Sand Creek.

Falcon Trucking Filing No. 1 consists of 35.731 acres and is presently undeveloped. Vegetation is sparse, consisting of native grasses. Existing site terrain generally slopes from north to south. More specifically, the west half of the site drains southwest, while the east half drains southeast. Grade rates across the site vary between 1 and 10%.

There are existing large overhead electric lines and an existing water line located along the northern boundary of the site. Existing underground gas lines are located within an easements and a right of way

that run north to south through the center of the parcel Existing gas, water and fiber optic water lines run along the west side of the site adjacent to existing Marksheffel Road. Existing sanitary sewer and water lines run under existing graphite drive along the west boundary of the site. Existing sanitary and waterline stubs are provided within the street terminus of the adjacent Enclaves at Mountain Vista Ranch Filings No. 5 and 6.

There are no irrigation facilities on site.

Anticipated concept plan improvements proposed for the site include paved streets, parking lots, sidewalks, townhomes, commercial buildings, full spectrum detention ponds, and wet/dry utilities as normally constructed for those developments.

Two (2) full spectrum detention ponds are anticipated to be necessary to provide water quality treatment and detention for the proposed development. The outlet structures from the western pond will discharge to the existing swale/ditch located along the west side of Marksheffel road, while the FSD planned for the east half of the development will tie into an existing storm sewer system along the north side of Graphite Drive that was constructed with Enclaves at MVR Filing No.3.

#### WETLANDS

There are no apparent wetlands within the boundary of this project.

#### **CHANNEL IMPROVEMENTS**

The proposed project is not adjacent to Sand Creek or any other significant drainageway. In accordance with the Sand Creek Drainage Basin Planning Study (DBPS) no channel improvements are required as a part of this project.

#### SOILS

Soils for this project are delineated by the map in the appendix as Truckton Sandy Loam (97) and have been characterized as Hydrologic Soil Types "A". Soils in the study area are shown as mapped by S.C.S. in the "Soils Survey of El Paso County Area". See Appendix for soils report.

#### HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the City of Colorado Springs Storm Drainage Design Criteria manual and where applicable the Urban Storm Drainage Criteria Manual. The Rational Method was used to estimate storm water runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

#### HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the City of Colorado Springs Storm Drainage Design Criteria manual. The relevant data sheets are included in the Appendix of this report.

#### FLOODPLAIN STATEMENT

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0543G, revised December 7, 2018, the subject site is <u>NOT</u> located within the 100 year floodplain. However, the subject site is located within the Other Areas Zone 'X' which is defined as an area determined to be outside the 0.2 annual chance floodplain and/or Other Areas Zone 'D' in which flood hazards are undetermined but possible. See Appendix.

#### **DRAINAGE CRITERIA**

This drainage analysis has been prepared in accordance with the current City of Colorado Springs Drainage Criteria Manual. Calculations were performed to determine runoff quantities for the 5-year and 100-year frequency storms for developed conditions using the Rational Method as required for basins having areas less than 100 acres. See Appendix for calculations.

#### **EXISTING DRAINAGE CONDITIONS**

The existing undeveloped parcel consists of sparsely vegetated native grassland consistent with common agricultural grazing land. The site is bisected by a ridgeline (which contains two private gas lines) that splits the parcel into an east and west halves. The western half of the parcel slopes to the west/southwest at grades that range between 2 and 10%. Runoff produced within the northern half of the west half of the site combines with sheet flows from a small undeveloped offsite area located north of the site at a localized depression along the west edge of existing Marksheffel Road some 600 feet to the south of Barnes Road. It is at this location, where an existing public 18" RCP culvert directs the drainage under the roadway to an existing earthen swale that parallels the west side of Marksheffel Road.

Runoff produced within majority of the south half of the western side of the parcel drains as sheet flow the existing roadside swale located along the eastern side of existing Marksheffel Road. At Granite Drive an existing public 24" RCP culvert conveys runoff, north to south, under the roadway.

Runoff produced along the southwestern boundary of the site, are collected within the curb and gutter of Graphite drive which drains to existing Marksheffel Road. This runoff combines with flows conveyed by the public 18" culvert south of the subject site within the eastern roadside ditch of Marksheffel road. A cross culvert located south 550' below the site at a low point collects and conveys drainage to the west half of existing Marksheffel Road.

The eastern half of the existing undeveloped parcel consists also consists of sparsely vegetated native grassland commonly associated with agricultural grazing land. The eastern half of the subject site slopes to the west/southwest at grades that range between 2 and 10%. Runoff produced within the eastern half of the site combines with sheet flows from undeveloped offsite areas located north of the subject site. In the existing condition runoff reaching the eastern boundary of the subject site is intersected and conveyed south within a temporary earthen swale and temporary grading and drainage easement constructed with Enclaves at Mountain Vista Ranch (Filings 5 and 6). The conveyed runoff is collected by a existing CDOT Type D inlet and which discharges via a private 30" RCP storm sewer into an existing Full Spectrum Detention Pond (Pond 1) within EMV Filing 5 located north of Granite Drive, see Existing Drainage Map in the appendix.

#### **Existing Conditions Detailed Drainage Discussion**

**Basin A** consists of approximately 2.37 acres of undeveloped offsite land with sparse, native grasses and vegetation located to the north of the western half of the subject site. Runoff from the basin (Q5=0.6 cfs, Q100=4.4 cfs) drains northeast to southwest and enters the northern boundary of the site as sheet flow.

**Basin B** consists of approximately 8.42 acres of undeveloped land with sparse, native grasses and vegetation. Runoff from the basin (Q5=2.2 cfs, Q100=16.1 cfs) combines with flows from **Basin A** at **Design Point 1** where it is discharged into to the existing right of way adjacent to the existing 18" RCP at the low point of Marksheffel Road. The existing combined peak flow calculated to cross the western property totals Q5=2.7 cfs, Q100=19.6 cfs.

**Basin C** consists of approximately 7.53 acres of undeveloped offsite land with sparse, native grasses and vegetation located along the southwestern side of the subject site. Runoff from the basin (Q5=1.8 cfs, Q100=13.2 cfs) is conveyed west as sheet flow to the western boundary just up-gradient from the cross culvert at Graphite Drive near **Design Point 2** (Q5=1.8 cfs, Q100=13.2 cfs).

**Basin D** consists of approximately 2.23 acres of undeveloped offsite land with sparse, native grasses and vegetation located adjacent to existing Graphite Drive. Runoff from the basin (Q5=0.6 cfs, Q100=4.1 cfs) continues west within the curb and gutter to Marksheffel Road (**Design Point 3**).

**Basin E** consists of approximately 12.97 acres of undeveloped offsite land with sparse, native grasses and vegetation located to the north of the eastern half of the subject site. Runoff from the basin (Q5=3.1 cfs, Q100=22.5 cfs) drains north to south/southeast and enters the northern boundary of the site as sheet flow.

**Basin F** consists of approximately 8.97 acres of undeveloped land with sparse, native grasses and vegetation located along the eastern half of the site. Runoff from the basin (Q5=2.0 cfs, Q100=15.0 cfs) combines with flows from **Basin E** at **Design Point 4**. The existing combined peak flow calculated to within the existing earthen swale totals Q5=4.0 cfs, Q100=29.6 cfs.

**Basin G** consists of approximately 7.78 acres of undeveloped land with sparse, native grasses and vegetation located along the southeastern portion of the site. Runoff from the basin (Q5=1.5 cfs, Q100=11.3 cfs) combines with flows from **DP4** at **Design Point 5**. The existing combined peak flow calculated to within the existing earthen swale totals Q5=4.6 cfs, Q100=33.6 cfs. Runoff conveyed by the swale is currently being conveyed to the FSD Pond 1 within Enclaves Filing No.5.

**Basin H** consists of approximately 0.79 acres of undeveloped offsite land with sparse, native grasses and vegetation located adjacent to existing Graphite Drive (**Design Point 6**). Runoff from the basin (Q5=0.2 cfs, Q100=1.5 cfs) continues east within the curb and gutter to inlets located within Graphite Drive.

#### FOUR STEP PROCESS

**Step 1 Employ Runoff Reduction Practices**. Whenever possible roof drains will be directed to vegetated landscaping buffer areas and islands prior to release to streets aiding in minimizing direct connection of impervious surfaces. The new Runoff Reduction criteria will need to be met with the submittal with future FDR's. This includes compliance with the Green Infrastructure Manual and Policy Clarification on

Green Infrastructure and corresponding calculations (UD-BMP v 3.07) and Runoff Reduction Exhibit showing that a10% reduction in the WQCV is being met.

**Step 2 Implement BMPs that provide a water quality capture volume with slow release.** – A Full Spectrum Detention basin is being proposed at the south end of the site to collect and treated developed runoff. This facility will restrict discharge rates to predevelopment rates and slowly release the Water Quality volume over 40 hours and the EURV storm event over 72 hours. Future FDR submittals will need to evaluate the area (in acres) and percent of the total disturbed area that will receive water quality treatment. A minimum of 95% of the total disturbed area must receive water quality treatment and the remaining 5% must not exceed 1 acre.

**Step 3 Stabilize streams.** – The runoff from the site will be directed to an existing stable underground storm sewer system that discharges into subsequent downstream conveys systems before discharge into the East Fork Sand Creek Sub-tributary and East Fork of the Sand Creek. All new and re-development projects are required to construct or participate in the funding of channel stabilization measures. Drainage basin fees paid, at the time of platting, go towards channel stabilization within the drainage basin.

**Step 4 Implement site specific and other source control BMPs.** – The proposed development will implement a Stormwater Management Plan including property housekeeping practices and spill containment procedures. Material storage (such as backfill stockpiles or landscape materials), during construction are to be located away from drainage facilities. Designated Fueling areas and trash enclosures are to be placed in locations where they can be easily source.

## PROPOSED DRAINAGE CHARACTERISTICS

#### **General Concept Drainage Discussion**

The proposed drainage plan evaluates proposed flow patterns and recommends infrastructure and facility sizing for the parcel based upon conceptual grading and layouts for high and medium density residential development. The parcel upon development is anticipated to include asphalt and curb and guttered roadways, parking lots, retaining walls, and building structures consistent with higher density residential development. Water, wastewater and other subsurface utilities will be extended into the site as necessary to provides services. In addition to open space and landscaping two full spectrum detention and water quality ponds are anticipated to be constructed.

The proposed site will continue to mimic existing general drainage patterns with proposed drainage being directed to the southeast and southwest corners of the site. The ridgeline which holds the gas lines will remain intact coordination and concurrence from the utility companies will be required. Conceptual storm sewer main lines have been extended to areas for collection of runoff and directed to the aforementioned FSD ponds. Basins F, G, H and J will remain undeveloped and fully pervious, therefore, water quality is not required. This is a conceptual layout to accurately size the detention facilities for future knowledge and planning. Therefore, the following calculations for pipe sizes, inlets, and detention pond sizing are irrelevant until a Development Plan is submitted to the City."

#### **Proposed Conditions Detailed Drainage Discussion**

**Basin A** consists of approximately 0.95 acres offsite land located adjacent planned Barnes Road north of the subject site. The basin is a mixture of proposed roadway, landscaping and native grasses. Runoff from

the basin (Q5=1.1 cfs, Q100=3.7 cfs) drains northeast to southwest and enters the northern boundary of the site as sheet flow.

**Basin B** consists of approximately 4.50 acres of future medium density residential development and access roadways. Runoff from basin (Q5=8.9 cfs, Q100=19.0 cfs) flows toward the southwestern corner of the site after combining with flows from **Basin A**. A proposed private 36" storm sewer main (**PR1**) has been extended into the area to collect the flow at **Design Point 1** (Q5=11.0 cfs, Q100=24.6 cfs).

**Basin C** consists of approximately 5.07 acres of future medium density residential development and access roadways. Runoff from basin (Q5=9.0 cfs, Q100=19.1 cfs) is anticipated to be directed to the street side and conveyed to a low point. A proposed private 30" storm sewer main (**PR2**) has been extended into the area to collect the flow at **Design Point 2** (Q5=9.0 cfs, Q100=19.1 cfs).

**Basin D** consists of approximately 2.80 acres of future medium density residential development and access roadways. Runoff from basin (Q5=5.2 cfs, Q100=11.1 cfs) is anticipated to be directed to the street side and conveyed to a low point. A proposed private 24" storm sewer main (**PR3**) has been extended into the area to collect the flow at **Design Point 3** (Q5=5.2 cfs, Q100=11.1 cfs).

**Basin D1** consists of approximately 0.46 acres of future medium density residential development and open space. Runoff from the basin (Q5=0.6 cfs, Q100=1.6 cfs) is anticipated to be directed overland to the adjacent tract **Design Point 4** (Q5=0.6 cfs, Q100=1.6 cfs).

**Basin E** is located at the southwest corner of the property and consists 3.41 acres of a Tract dedicated to house a Full Spectrum Detention and Water Quality Pond (**FSD Pond1**). Runoff from this basin (Q5=1.6 cfs, Q100=9.0 cfs) is captured within the pond and combines with the flows conveyed by **PR1**, **PR2**, **PR3** and sheet flow from **DP4**. The total peak runoff anticipated to reach **FSD Pond 1** at **Design Point 5** is Q5 = 23.3 cfs, Q100 = 50.9 cfs. The total peak acres contributing to **FSD Pond 1** is 16.73 acres. The private full spectrum detention pond will discharge to predevelopment flow rates and drain the water quality volume and excess urban runoff volume over 40 hours and 72 hours respectively. A private 24" storm sewer will be constructed at the southwest corner of the pond which will discharge to the westside of Marksheffel Road. The peak flows calculated to be released from the pond (**PR4**) total 2.3 cfs and 12.0 cfs in the 5-year and 100-year events respectively. Refer to drainage facility design section of the report for additional information regarding the facility.

**Basin F** consists of approximately 0.37 acres of offsite land likely a mixture of landscaping and native grasses located adjacent to planned Barnes Road. Runoff from the basin (Q5=0.2 cfs, Q100=1.0 cfs) drains northeast to southwest and enters the northern boundary of the site as sheet flow.

**Basin G** consists of approximately 1.44 acres of undeveloped offsite land with sparse, native grasses and vegetation. The area houses three easements for two underground waterlines and a gas line. Runoff from the basin (Q5=0.5 cfs, Q100=3.7 cfs) combines with flows from **Basin F** at **Design Point 6** where it is discharged into to the existing right of way adjacent to the existing public 18" RCP at the low point of Marksheffel Road. The combined peak flow calculated to cross the western property totals Q5=0.7 cfs, Q100=4.5 cfs.

**Basin H** consists of approximately 1.22 acres of undeveloped offsite land with sparse, native grasses and vegetation. The area houses three easements for two underground waterlines and a gas line. Runoff from the basin (Q5=0.4 cfs, Q100=3.0 cfs) combines with flows from **Basin F** at **Design Point 6** where it is discharged into to the existing right of way, up-gradient from the cross culvert at Graphite Drive near **Design Point 7** (Q5=0.4 cfs, Q100=3.0 cfs). The cumulative flows from DP6, DP7 and the **Pond 1** 

**Outfall** at **DP9** are (Q5=2.9 cfs, Q100=16.5 cfs), outfall into an existing swale on the westside of Marksheffel Road.

**Basin I** consists of approximately 0.30 acres of development directly adjacent to existing Graphite Drive, which will consist likely a mixture of landscaping and native grasses. Runoff from the basin (Q5=0.3 cfs, Q100=1.2 cfs) drains south to the roadway.

**Basin J** consists of approximately 0.17 acres of development directly adjacent to existing Graphite Drive, which will consist likely a mixture of landscaping and native grasses. Runoff from the basin (Q5=0.1 cfs, Q100=0.4 cfs) drains south to the roadway. The combined flow from **Basin I** and **Basin J** reaching the west sloping portion of Graphite Drive is Q5=0.4 cfs, Q100=1.5 cfs (**Design Point 8**).

**Basin K** consists of approximately 0.97 acres offsite land located adjacent planned Barnes Road north of the subject site. The basin is a mixture of landscaping and native grasses. Runoff from the basin (Q5=0.5 cfs, Q100=2.7 cfs) drains northeast to southwest and enters the northern boundary of the site as sheet flow.

**Basin L** consists of approximately 4.76 acres of future high density residential development and roadways. Runoff from basin (Q5=8.6 cfs, Q100=18.2 cfs) combines with flows from **Basin K** at a low point located within the future residential streets. A proposed 30" storm sewer main (**PR5**) has been extended into the area to collect the flow at **Design Point 10** (Q5=9.0 cfs, Q100=20.6 cfs).

**Basin M** consists of approximately 5.84 acres of future high density residential development, open space and roadways. Runoff from basin (Q5=11.0 cfs, Q100=25.1 cfs) is collected within a low point located within the future residential streets. A proposed private 36" storm sewer main (**PR6**) will collect the flow at **Design Point 11** (Q5=11.0 cfs, Q100=25.1 cfs). A private proposed 42" sewer (**PR7**) will collect the combined runoff carried within **Pipes Runs 5** and **6**.

**Basin N** consists of approximately 2.49 acres of future high density residential development and roadways. Runoff from basin (Q5=5.0 cfs, Q100=10.7 cfs) is collected within a low point located within the future residential streets. A proposed 36" storm sewer main (**PR8**) has been extended into the area to collect the combined flow from **PR7** and **DP 12** (Q5=5.0 cfs, Q100=10.7 cfs).

**Basin O** is located at the southeast corner of the property and consists 0.9 acres of a Tract dedicated to house a Full Spectrum Detention and Water Quality Pond (**FSD Pond2**). Runoff from this basin (Q5=0.5 cfs, Q100=2.8 cfs) is captured within the pond and combines with the flows conveyed by **PR8**. The total peak runoff anticipated to reach **FSD Pond 2** at **Design Point 13** is Q5 = 23.0 cfs, Q100 = 53.2 cfs. The total peak acres contributing to **FSD Pond 2** is 15.37 acres. The private full spectrum detention pond will discharge to predevelopment flow rates and drain the water quality volume and excess urban runoff volume over 40 hours and 72 hours respectively. A private 18" storm sewer will be constructed at the southeast corner of the pond which will discharge an existing 24" stub provided within the rights of way of Granite Drive (Filing No. 5). The peak flows calculated to be released from the pond (**PR9**) total 0.6 cfs and 11.7 cfs in the 5-year and 100-year events respectively. Refer to drainage facility design section of the report for additional information regarding the facility.

**Basin P** consists of approximately 0.41 acres offsite land located adjacent planned Barnes Road north of the subject site. The basin is a mixture of landscaping and native grasses. Runoff from the basin (Q5=0.2 cfs, Q100=1.1 cfs) drains north to south and enters the northern boundary of the site as sheet flow.

**Basin Q** consists of approximately 0.08 acres of future high density residential development and roadway. Runoff from basin (Q5=0.7 cfs, Q100=1.6 cfs) combines with flows from **Basin P** within the proposed residential roadway connection with existing Talc Drive at **Design Point 14**. The cumulative flows from **DP14** are Q5=0.7 cfs, Q100=1.6 cfs.

**Basin Q2** consists of approximately 0.08 acres of future high density residential development and roadway. Runoff from the basin (Q5=0.2 cfs, Q100=0.4 cfs) is carried within the curb and gutter of the future connection with Talc Drive where it enters existing Enclaves at Mountain Vista at Filing 6 at **Design Point 14A**. The cumulative flows from **DP14A** are Q5=0.2 cfs, Q100=0.4 cfs.

**Basin R** consists of approximately 0.40 acres of the rear lots of future high density residential development along the eastern boundary of the subject site. Runoff from the basin (Q5=0.8 cfs, Q100=2.0 cfs) will enter Enclaves at Mountain Vista Filing 6 and shall be distributed and conveyed down the adjacent lines. The total flow represented by **Design Point 15** totals Q5=0.8 cfs, Q100=2.0 cfs, which is less than 0.25 cfs/ lot line.

**Basin R2** consists of approximately 0.22 acres of the rear lots of future high density residential development along the eastern boundary of the subject site. Runoff from the basin (Q5=0.5 cfs, Q100=1.1 cfs) will enter Enclaves at Mountain Vista Filing 6 and shall be distributed and conveyed down the adjacent lot lines. The total flow represented by **Design Point 15A** totals Q5=0.5 cfs, Q100=1.1 cfs which is less than 0.25 cfs/ lot line.

**Basin S** consists of approximately 0.11 acres of future high density residential development and roadway. Runoff from basin (Q5=0.5 cfs, Q100=0.9 cfs) is carried within the curb and gutter of the future connection with Basaltic Drive where it enters Enclaves at Mountain Vista Filling No. 5 at **Design Point 16**. The cumulative flows from **DP16** are Q5=0.5 cfs, Q100=0.9 cfs.

**Basin S2** consists of approximately 0.08 acres of future high density residential development and roadway. Runoff from basin (Q5=0.4 cfs, Q100=0.6 cfs) is carried within the curb and gutter of the future connection with Basaltic Drive where it enters Enclaves at Mountain Vista Filling No. 5 at **Design Point 16A**. The cumulative flows from **DP16A** are Q5=0.4 cfs, Q100=0.6 cfs.

**Basin T** consists of approximately 0.33 acres of the rear lots of future high density residential development along the eastern boundary of the subject site. Runoff from the basin (Q5=0.7 cfs, Q100=1.6 cfs) will enter Enclaves at Mountain Vista Ranch Filing 5 and shall be distributed and conveyed down the adjacent lot lines at an average of less than 0.2 cfs per lot line. The cumulative flows from at **DP17** are (Q5=0.7 cfs, Q100=1.6 cfs).

It should be noted, that in previously approved drainage reports (EMVR Filing 5 and 6) the runoff reaching the western boundary of Enclaves at Mountain Vista Ranch Filing No. 5 and 6 from the subject site was to be conveyed south via swales located along the shared property line (Filing 5 FDR Map in appendix). This was largely done to protect the lots from the large undeveloped offsite watershed that naturally reached the property until upstream development could occur and the quantity of runoff and impact from drainage could be greatly reduced and controlled.

With the development of the subject site, the swale is no longer necessary and will be largely removed. A very limited amount of rear lot drainage from the Falcon Trucking site is now anticipated to enter the existing lots (within Filings 5 and 6) from the west as represented on the enclosed proposed drainage map.

To ensure that drainage would cause no negative effects to downstream property and existing downstream systems within Filing 5 and 6 the drainage analysis (hydrologic worksheets and inlet calculations, etc) for EMVR Filing 5/6 were re-evaluted to incorporate the additional runoff from **Basins P-T.** A second drainage map (sheet DM2) has been provided within the appendix which outlines the revised flow rates for these downstream systems.

In addition to the rational drainage calculations showing that the minor addition flow to the existing lots can be conveyed by the downstream storm systems without negative impacts, calculations showing that the exiting side lot property line swales are also adequate to convey this minor runoff to the streets, which contain the existing storm systems. Please refer to the hydraulic calculations provided in the appendix for additional details.

The existing 30" RCP (Pipe 12) leaving EMV Filing 6 (north of Basaltic Drive) was anticipated to convey 11.2 cfs and 20.1 cfs in the minor and major storm events per the approved Filling No. 6 FDR, based upon the current analysis the same 30" Pipe (12\*) is anticipated to carry 11.3 cfs and 20.4 cfs in the relative events. These increases of 0.9% and 1.05% in the two storm events are considered negligible and are anticipated to have no notable effects on conveyance or water quality.

Similarly the existing 36" RCP (Pipe 12) entering the north east side of existing Pond 303 within Filing 5 was (per the approved Filing 5 FDR) anticipated to convey 24.7 cfs and 58.1 cfs in the minor and major storm events. Based upon the current analysis the same 36" Pipe (12\*\*) is anticipated to carry 19.4 cfs and 46.9 cfs in the relative events. These decreases of 27.3% and 23.9% in the two storm events are not anticipated to have a negative impact to the existing system or to water quality. The primary cause for the decrease in actual flow rates vs. planned flow lies within the utilization of a shortened planned time of concentration, utilized as a measure of conservatism, within the Filing 5 FDR.

Therefore a concept design of similar density and grading patterns to the one shown within this MDDP does not negatively affect the existing downstream storm sewer facilities.

## DRAINAGE FACILITY DESIGN

Based upon a concept layout a minimum of two new Full Spectrum Detention (FSD) will be required in order to reduce the fully developed flows from the site to pre-development levels and address water quality. The ponds have been sized utilizing MHFD v4.04 from Urban Drainage and Flood Control District (UDFCD).

The ponds are being modeled with an outlet control structure which limits the release rate of the pond through the use of orifices, weirs, and a restrictor plates placed before a proposed outlet pipes to store the WQCV, EURV, and the flood control volumes for the 2, 5, 10, 25, 50, and 100 year storm events. The WQCV will be slowly released over 40 hours. The 100 year will drain in less than 120 hours. Maintenance to the proposed private FSD Pond 1 and private FSD Pond 2 is by the Falcon Trucking Metro District.

A private Full Spectrum Detention Extended Detention Basin (FSD Pond 1) is being proposed for the west half of the site to address water quality from 16.73 acres at 54.0% imperviousness. FSD Pond 1 is being constructed with an outlet control structure and a proposed 24" RCP outlet pipe. An overflow emergency weir is proposed along the southwest embankment to safely convey flows to Marksheffel corridor in the event of outlet clogging. The 0.0' height (lowest orifice) stage was based upon an elevation of 6630.00.

FSD Pond 1	WQCV	EURV	5 Year	<u> 100 Year</u>
Maximum Volume Stored (acre-ft)	0.337	1.109	1.236	2.081
Maximum WS Elevation	6632.47	6633.53	6633.68	6634.47
Peak Inflow (cfs)(calc)			21.7	47.7
Peak Outflow (cfs)	0.2	0.3	2.3	12.0

A second private Full Spectrum Detention Extended Detention Basin (**FSD Pond 2**) is being proposed for the east half of the site to address water quality from 15.37 acres at 60.0% imperviousness. . **FSD Pond 2** is being constructed with an outlet control structure and a proposed 18" RCP outlet pipe. An overflow emergency weir is proposed along the southern embankment to safely convey flows to Graphite Drive corridor in the event of outlet clogging. The 0.0' height (lowest orifice) stage was based upon an elevation of 6634.67.

FSD Pond 2	WQCV	EURV	5 Year	<u> 100 Year</u>
Maximum Volume Stored (acre-ft)	0.304	1.004	1.085	1.766
Maximum WS Elevation	6637.09	6639.13	6639.33	6640.74
Peak Inflow (cfs)(calc)			21.1	44.6
Peak Outflow (cfs)	0.1	0.4	2.6	11.7

Some of the proposed runoff from Falcon Trucking site is planned to be directed to the existing streets and storm sewer systems located within EMVR Filings 5 and 6, ultimately outfalling into the existing Extended Detention Basin (FSD Pond 303). See Appendix for a letter from the Mountain Vista Metropolitan District (MVMD), which permits Falcon Trucking, to access and allow for modifications to the existing facility (FSD Pond 303), as required by future Final Drainage Reports and analysis. Based upon the concept layout and proposed drainage patterns the existing facility will now conceptually function to address water quality from 18.52 acres (east edge of proposed Falcon Trucking Filing No.1, Enclaves at Mountain Vista Ranch Filing No.6 and Enclaves at Mountain Vista Ranch Filing No.5) at approximately 53.3% imperviousness. Based upon the current concept design and discharge, the pond as constructed appears to be able to accept the runoff. In order to meet the various release rates it is anticipated that the outlet structure and north forebay will need to be modified. This may or may not include raising the outlet box elevation by approximately 24 inches and removal, resizing and replacement of the trash screen and orifice plate. The forebay may or may not include raising the forebay walls an additional foot. The modifications should be addressed as with the Final Drainage Report. With this improvement a concept design of similar density and grading patterns to the one shown within this MDDP does not negatively affect the existing downstream storm sewer facilities or water quality. It should be noted that for all basins that will remain fully landscaped and are not directed to one of the three ponds, the basin will remain fully pervious, therefore, water quality treatment is not required.

#### **EROSION CONTROL**

It is the policy of the City of Colorado Springs that we submit an erosion control plan with the drainage report. At this time we respectfully request that the erosion control plan be submitted in conjunction with the final grading plan. Proposed straw bale check dams, silt fence, inlet protection, sediment basin, vehicle traffic control, and reseeding are proposed as erosion control measures.

#### DRAINAGE, BRIDGE, AND POND FEES

The project is located within the Sand Creek Drainage Basin. The "2023 Drainage, Bridge, and Pond Fees-City of Colorado Springs", table identifies the following fees associated with the basin. These fees have been applied and summarized here for this 35.731 acre site. Drainage fees are due prior to plat recordation.

Basin Fees 2023	Total area (acres)	Basin Fee (per acre)	Total Cost Basin Fee
Drainage Fee	35.731	\$22,015	\$786,617.97
Bridge Fee	35.731	\$0.00	\$0.00
Pond Fee – Land	35.731	\$0.00	\$0.00
<b>Pond Fee - Facility</b>	35.731	\$0.00	\$0.00
Surcharge	35.731	\$0.00	\$0.00
Total			\$786,617.97

#### CONSTRUCTION COST ESTIMATE

(Private Storm Sewer System, Non-Reimbursable)

(1110	the Storin Sewer System, 140	n Kennouisuolej			
Item	Description	Quantity	Unit Cost	С	ost
1.	18" RCP Storm Drain	220 LF	\$75/LF	\$	16,500.00
2.	24" RCP Storm Drain	696 LF	\$85/LF	\$	59,160.00
3.	30" RCP Storm Drain	332 LF	\$105/LF	\$	34,860.00
4.	36" RCP Storm Drain	270 LF	\$145/LF	\$	39,150.00
5.	42" RCP Storm Drain	410 LF	\$190/LF	\$	77,900.00
			Subtotal	\$	227,570.00
			Contingency/(25%)	\$	56,892.50
			Total =	\$	284,462.50
·	te, Non-Reimbursable Ponds)				
	1 (Private facilities to be m	•	<b>e</b> ,		
1.	Forebay	LS	\$6976/LS	\$	6,976.00
2.	FSD Pond Outlet Struc	LS	\$11779/LS	\$	11,779.00
3.	2' Wide Trickle Channel	765 LF	\$30/LF	\$	22,950.00
4.	11' Wide Access Rd. Cl 2	574 Ton	\$20/Ton	\$	11,480.00
5.	Soil Riprap Type M	151 CY	\$65/CY	\$	9,815.00
6.	Concrete Cutoff Wall	LS	\$3410/LS	\$	3,410.00
7.	Signage	LS	\$1000/LS	\$	1,000.00
			Total:	\$	67,410.00
	2 (Private facilities to be m	•		<b>.</b>	<
1.	Forebay	LS	\$6976/LS	\$	6,976.00
2.	FSD Pond Outlet Struc	LS	\$11779/LS	\$	11,779.00
3.	2' Wide Trickle Channel	262 LF	\$30/LF	\$	7,860.00
4.	11' Wide Access Rd. Cl 2	269 Ton	\$20/Ton	\$	5,380.00
5.	Soil Riprap Type M	85 CY	\$65/CY	\$	5,525.00

		\$1740/LS		\$	1,740.00
ignage	LS	\$1000/LS		\$	1,000.00
			Total:	\$	35,260.00
(Private facility maintain	ed by the Mou	ıntain Vista Ranch Metro Distr	ict)		
eplace Orifice Plate	LS	\$800/LS	,	\$	800.00
eplace Filter Screen	LS	\$1000/LS		\$	1,000.00
utlet Box Modification	LS	\$4500/LS\$		\$	4,500.00
			Total:	\$	6,300.00
		Subtotal (Dands 1	7 8-3)	¢	108,970.00
			,		16,345.50
		0,	· /	<u> </u>	<u>10,345.50</u> 125,315.50
(	( <b>Private facility maintain</b> eplace Orifice Plate eplace Filter Screen	(Private facility maintained by the Mou eplace Orifice Plate LS eplace Filter Screen LS	(Private facility maintained by the Mountain Vista Ranch Metro Distri eplace Orifice Plate LS \$800/LS eplace Filter Screen LS \$1000/LS utlet Box Modification LS \$4500/LS\$ Subtotal (Ponds 1, Contingency	Total:         (Private facility maintained by the Mountain Vista Ranch Metro District)         eplace Orifice Plate       LS       \$800/LS         eplace Filter Screen       LS       \$1000/LS         utlet Box Modification       LS       \$4500/LS\$	Total:       \$         Total:       \$         (Private facility maintained by the Mountain Vista Ranch Metro District)         eplace Orifice Plate       LS       \$800/LS       \$         eplace Filter Screen       LS       \$1000/LS       \$         utlet Box Modification       LS       \$4500/LS\$       \$         Total:       \$         Subtotal (Ponds 1, 2 &3)       \$         Contingency (15%)       \$

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above is only an estimate of the facility cost in 2021.

#### SUMMARY

Development of Falcon Trucking Filing No.1 will not adversely affect the surrounding development. The proposed concept drainage facilities will adequately convey, detain and route runoff from the onsite & offsite flows to existing facilities, as well as provide water quality treatment. Runoff and storm drain and appurtenances will not adversely affect the existing downstream infrastructure and surrounding developments. This MDDP is in general compliance with prior hydrologic studies affecting the site. All drainage facilities described herein and shown on the included Proposed Drainage Map (See Appendix) are subject to change being dependent upon individual lot development. However, this MDDP should be used as a guideline for release of flows offsite, and final Full Spectrum & Water Quality Detention Pond sizing. Care will be taken to accommodate overland emergency flow routes on site and temporary drainage conditions.

#### REFERENCES

- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manual".
- 2.) "Urban Storm Drainage Criteria Manual"
- 3.) Web Soil Survey, USDA NRCS Soils Map <u>https://websoilsurvey.sc.egov.usda.gov/App/HomePage.htm</u>
- 4.) FEMA flood Map Service Center, Federal Emergency Management Agency https://msc.fema.gov/portal/home
- 5.) "Master Development Drainage Plan for Enclaves at Mountain Vista", last revised May 12<sup>th</sup>, 2016, by Galloway and Company, Inc.
- 6.) "Sand Creek Drainage Basin Planning Study Preliminary Design Report" dated January 1993, Revised March 1996, by Kiowa Engineering Corporation.
- 7.) "Preliminary/Final Drainage Report for Enclaves at Mountain Vista Ranch Filing No. 6" dated June 2020 by M&S Civil Consultants, Inc.
- 8.) "Preliminary/Final Drainage Report for Enclaves at Mountain Vista Ranch Filing No. 5" dated October 2019 by M&S Civil Consultants, Inc.
- 9.) "Preliminary/Final Drainage Report Enclaves at Mountain Vista Filing No. 2" dated March 2016, Revised April 2017 by Galloway & Company, Inc.

APPENDIX

VICINITY MAP

SOILS MAP

FIRM PANELS

# HYDROLOGIC CALCULATIONS

HYDRAULIC CALCULATIONS / POND CALCULATIONS

MARKSEFFEL ROAD FINAL DRAINAGE REPORT EXCERPTS

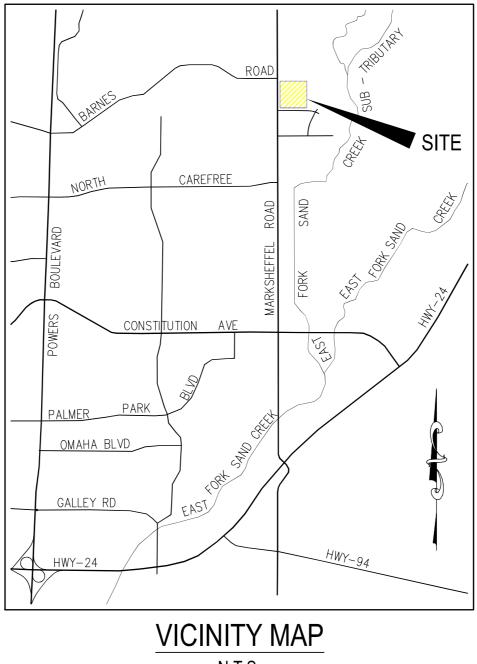
JIMMY CAMP CREEK DRAINAGE REPORT EXCERPTS

**DRAINAGE MAPS** 

# **BACKGROUND INFORMATION**

APPENDIX

VICINITY MAP



N.T.S.

# MOUNTAIN VISTA METROPOLITAN DISTRICT ACCESS LETTER AGREEMENT

# Mountain Vista Metropolitan District

February 7, 2022

City of Colorado Springs Stormwater Enterprise 30 S. Nevada, Suite 401 Colorado Springs, CO 80903

# RE: Falcon Trucking Drainage & Enclaves at Mountain Vista Ranch Pond Modification

The Falcon Trucking project is located northeast of the intersection of Marksheffel Road and Graphite Drive, in a portion of the southwest quarter of the southwest quarter (SW1/4, SW1/4) of Section 21, and a portion of the northwest quarter of the northwest quarter (NW1/4, NW1/4) of Township 13 South, Range 65 West of the 6<sup>th</sup> Principal Meridian, Colorado Springs, El Paso County, Colorado. The site is bound on the south by Graphite Drive, to the north by unplatted land owned by the City of Colorado Springs – Rec. No. 96020361 and by a tract of land owned by BLH No. 2 LLC that was set aside for Barnes Roadway extension and to the west by Marksheffel Road Right of Way, and to the east by Enclaves at Mountain Vista Ranch, Filing No's 5 and 6 (Rec. No's – 220714464 and 220714464). The site is approximately 35.7 acres.

The Falcon Trucking project will require the construction, ownership and maintenance of a full spectrum, water quality detention pond at its southeast corner. This pond will discharge into an existing pond (Pond 303) inside of Enclaves at Mountain Vista Ranch Filings 5. Pond 303 is currently owned and maintained by the Mountain Vista Metropolitan District. In order to meet the City's design criteria, minor modifications to Pond 303 will be required. These modifications are necessary to comply with the City's criteria for storm water discharge rates. The cost of the pond modifications, a two year warranty on the construction, any costs for fees for review or inspection, etc. will be 100% borne upon the owner/developer of the Falcon Trucking project. The maintenance of Pond 303 will remain the responsibility of the Mountain Vista Metropolitan District. The maintenance of the Falcon Trucking pond will remain the responsibility of the owner/developer of the Falcon Trucking project.

The below signature, by the representative of the district, agrees to permit access and allow for modification to the existing facility that are necessary to account for drainage as outlined within the approved drainage report for the Falcon Trucking site

KWall.

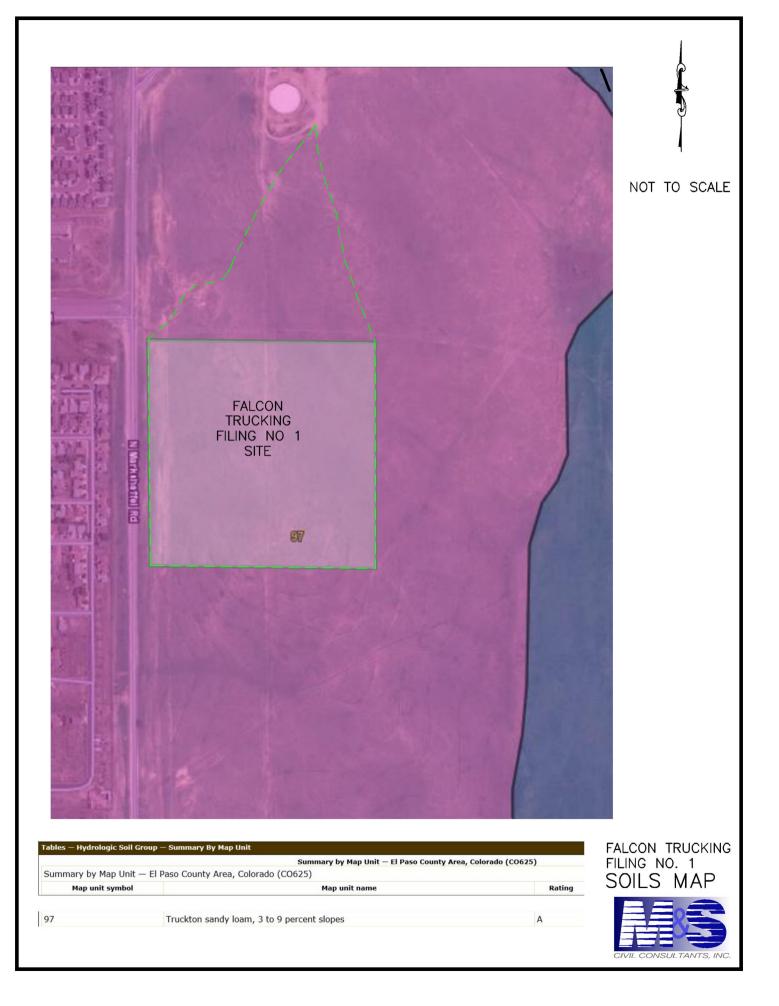
By:

Kevin Walker, District Manager

614 N. Tejon St.

Colorado Springs, CO 80903

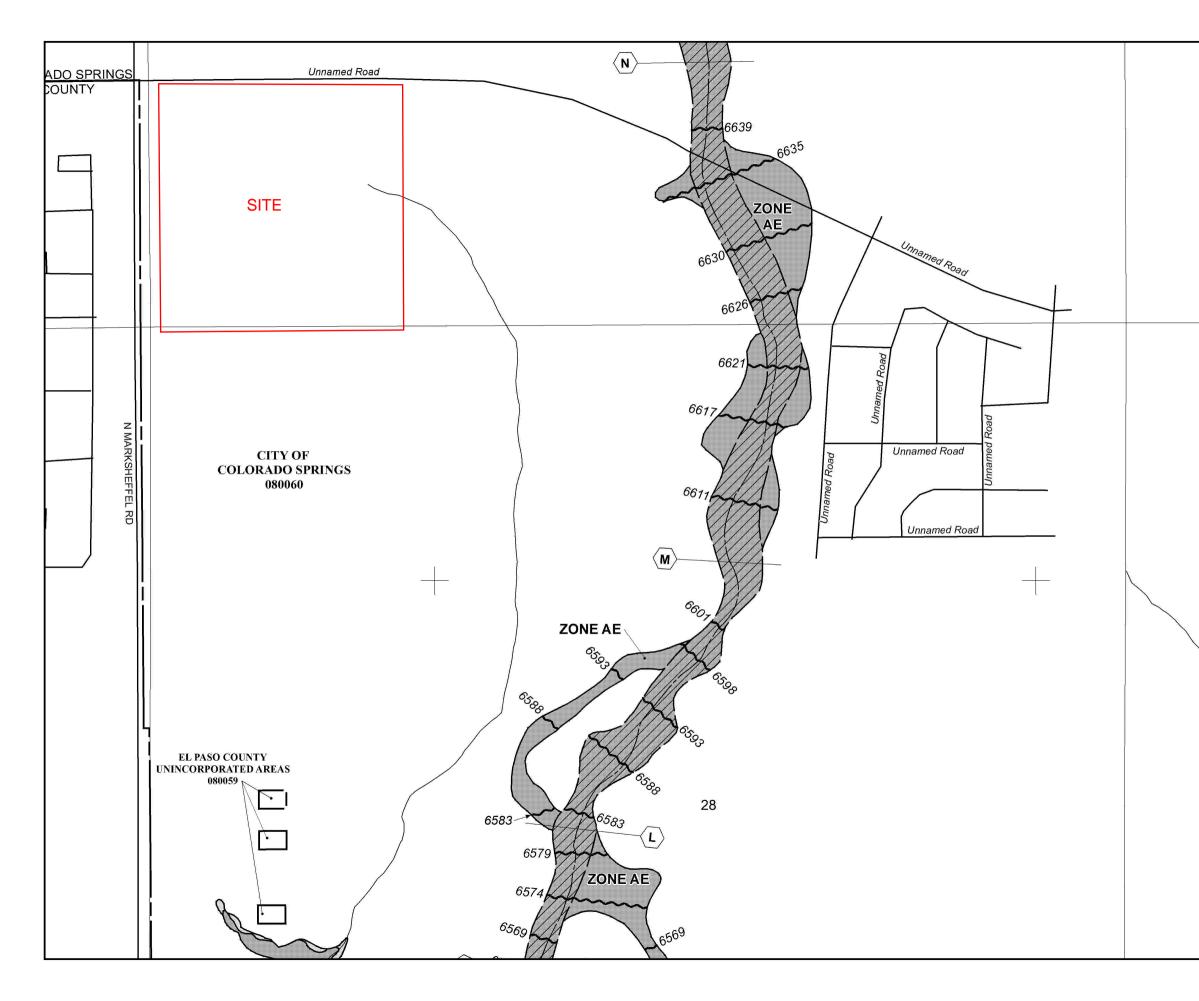
SOILS MAP

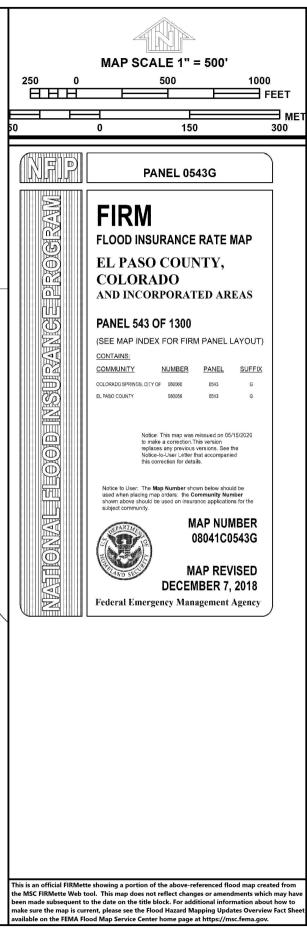


#### Hydrologic Soil Group—El Paso County Area, Colorado (29007 Soils Map)

	MAP INFORMATION
Area of Interest (AOI) C   Area of Interest (AOI) C/D   Soils D   Soil Ratiny Polygons D   A D   A/D Not rated or not available   B/D Streams and Canals   B/D Streams and Canals   B/D Transportation   C/D Interstate Highways   C/D US Routes   D US Routes   D Local Roads   Soil Ratiny Lines A/D   A/D A/D   A/D A/D   A/D A/D   D US Routes   D Local Roads   D Arial Photography   A/D Arial Photography	<ul> <li>MAP INFORMATION</li> <li>The soil surveys that comprise your AOI were mapped at 1:24,000.</li> <li>Warning: Soil Map may not be valid at this scale.</li> <li>Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of so line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detail scale.</li> <li>Please rely on the bar scale on each map sheet for map measurements.</li> <li>Source of Map: Natural Resources Conservation Service Web Soil Survey URL:</li> <li>Coordinate System: Web Mercator (EPSG:3857)</li> <li>Maps from the Web Soil Survey are based on the Web Merca projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.</li> <li>This product is generated from the USDA-NRCS certified dat of the version date(s) listed below.</li> <li>Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 18, Jun 5, 2020</li> <li>Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.</li> <li>Date(s) aerial images were photographed: Aug 19, 2018—\$23, 2018</li> <li>The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.</li> </ul>

USDA Natural Resources Conservation Service FIRM PANELS





### HYDROLOGIC CALCULATIONS

# FALCON TRUCKING EXISTING CONDITIONS DRAINAGE CALCULATIONS (Area Runoff Coefficient Summary)

			STRE	ETS/DEVEL	LOPED		NATURAL		RUNOFF C	OEFFICIENT
BASIN	TOTAL AREA (SF)	TOTAL AREA (Acres)	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	C <sub>5</sub>	C <sub>100</sub>
A	103422.537	2.37	0.00	0.90	0.96	2.37	0.08	0.35	0.08	0.35
В	366973.3818	8.42	0.00	0.90	0.96	8.42	0.08	0.35	0.08	0.35
С	328181.7374	7.53	0.00	0.90	0.96	7.53	0.08	0.35	0.08	0.35
D	97021.0981	2.23	0.00	0.90	0.96	2.23	0.08	0.35	0.08	0.35
Ε	565052.7368	12.97	0.00	0.90	0.96	12.97	0.08	0.35	0.08	0.35
F	390740.069	8.97	0.00	0.90	0.96	8.97	0.08	0.35	0.08	0.35
G	338690.3842	7.78	0.00	0.90	0.96	7.78	0.08	0.35	0.08	0.35
Н	34387.7952	0.79	0.00	0.90	0.96	0.79	0.08	0.35	0.08	0.35

Date: 5/28/2021	Calculated by:	DLM
	Date:	5/28/2021
Checked by: VAS	Checked by:	VAS

## FALCON TRUCKING FILING NO. 1 PROPOSED DRAINAGE CALCULATIONS

# (Area Drainage Summary)

From	Area Runoff Coej	ficient Summary			OVERLA	1ND		S7	REET / CH	ANNEL FLO	DW	Time of T	ravel (T <sub>t</sub> )	INTEN	SITY *	TOTAL	FLOWS
BASIN	AREA TOTAL	C <sub>5</sub>	C <sub>100</sub>	C5	Length	Height	T <sub>c</sub>	Length	Slope	Velocity	T <sub>t</sub>	TOTAL	CHECK	I <sub>5</sub>	I <sub>100</sub>	Q5	Q <sub>100</sub>
	(Acres)	From DCM	1 Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
A	0.95	0.23	0.47	0.23	75	8	6.2	0	0.0%	0.0	0.0	6.2	10.4	4.8	8.1	1.1	3.7
В	4.50	0.81	0.88	0.81	75	1.5	3.6	460	1.7%	2.6	2.9	6.5	13.0	4.8	8.0	17.4	31.7
С	5.07	0.49	0.62	0.49	140	1.7	12.2	575	1.4%	2.4	4.1	16.3	14.0	3.6	6.1	9.0	19.1
D	2.80	0.49	0.62	0.49	140	1.7	12.2	280	3.9%	4.0	1.2	13.4	12.3	3.8	6.4	5.2	11.1
D1	0.46	0.31	0.51	0.31	75	1.5	9.9	160	8.8%	5.9	0.5	10.3	11.3	4.1	6.8	0.6	1.6
Ε	3.41	0.12	0.39	0.12	50	16	4.0	570	0.5%	1.4	6.7	10.7	13.4	4.0	6.8	1.6	9.0
F	0.37	0.12	0.39	0.12	100	6	9.8	130	10.0%	6.3	0.3	10.1	11.3	4.1	6.9	0.2	1.0
G	1.44	0.08	0.35	0.08	100	10	8.6	0	0.0%	0.0	0.0	8.6	10.6	4.4	7.3	0.5	3.7
Н	1.22	0.08	0.35	0.08	100	7.5	9.4	0	0.0%	0.0	0.0	9.4	10.6	4.2	7.1	0.4	3.0
Ι	0.30	0.20	0.45	0.20	20	0.6	5.1	0	0.0%	0.0	0.0	5.1	10.1	5.1	8.6	0.3	1.2
J	0.17	0.09	0.36	0.09	100	9	8.8	0	0.0%	0.0	0.0	8.8	10.6	4.3	7.2	0.1	0.4
K	0.97	0.12	0.39	0.12	100	8	8.9	0	0.0%	0.0	0.0	8.9	10.6	4.3	7.2	0.5	2.7
L	4.76	0.49	0.62	0.49	100	2	8.8	850	2.2%	3.0	4.7	13.5	15.3	3.7	6.2	8.6	18.2
М	5.84	0.42	0.58	0.42	100	18	4.7	650	2.3%	3.0	3.6	8.3	14.2	4.4	7.4	11.0	25.1
N	2.49	0.49	0.62	0.49	100	2	8.8	230	2.2%	2.9	1.3	10.1	11.8	4.1	6.9	5.0	10.7
0	0.90	0.12	0.39	0.12	50	16	4.0	250	0.5%	1.4	2.9	6.9	11.7	4.7	7.9	0.5	2.8
Р	0.41	0.10	0.37	0.10	100	8	9.1	0	0.0%	0.0	0.0	9.1	10.6	4.3	7.2	0.2	1.1
Q	0.43	0.49	0.62	0.49	100	2	8.8	90	1.0%	2.0	0.8	9.5	11.1	4.2	7.1	0.9	1.9
R	0.63	0.40	0.56	0.40	50	3	4.9	0	0.0%	0.0	0.0	5.0	10.3	5.2	8.7	1.3	3.0
S	0.18	0.63	0.76	0.63	50	1	4.8	0	0.0%	0.0	0.0	5.0	10.3	5.2	8.7	0.6	1.2
Т	0.33	0.40	0.56	0.40	50	3	4.9	0	0.0%	0.0	0.0	5.0	10.3	5.2	8.7	0.7	1.6

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: DLM

Date: 5/28/2021

Checked by:

## FALCON TRUCKING EXISTING CONDITIONS DRAINAGE CALCULATIONS

### (Basin Routing Summary)

	From Area Runoff Coefficient Summary	2			OVE	RLAND		PIPE	/ CHA	NNEL FLO	W	Time of Travel $(T_i)$	INTEN	SITY *	TOTAL	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS/PIPES	CA5	CA <sub>100</sub>	C <sub>5</sub>	Length	Height	T <sub>c</sub>	Length	Slope	Velocity	T,	TOTAL	I <sub>5</sub>	I <sub>100</sub>	Q5	Q <sub>100</sub>	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
1	A, B	0.86	3.78	19.0		19.0	135	9.6%	2.2	1.0	20.0	3.1	5.2	2.7	19.6	TO WEST SIDE OF MARKSHEFFEL	
					Basin A Tc was used											(CULVERT UNDER MS)	
2	С	0.60	2.64		22.3						22.3	2.9	4.9	1.8	13.0	TO EAST MARKSHEFFEL ROW	
					Basin B Tc was used											(VIA CULVERT AT GRAPHITE)	
3	D	0.18	0.78				19.3					19.3	3.1	5.3	0.6	4.1	TO EAST MARKSHEFFEL ROW
																	(VIA GRAPHITE DRIVE)
					Basin D	Tc was use	d										
4	E, F	1.76	7.68				22.0	900	3.2%	1.3	11.9	33.9	2.3	3.9	4.0	29.6	3' BOTTOM EARTHEN SWALE
					Basin E	Tc was use	d										
5	DP4, G	2.38	10.40				33.9	400	1.0%	0.7	9.5	43.4	1.9	3.2	4.6	33.6	EX TYPE D INLET
				DP4 Tc was used													
6	Н	0.06	0.28		5141	e mus used	18.3					18.3	3.2	5.4	0.2	1.5	TO ENCLAVES
0							1010								0.2		(VIA GRAPHITE DRIVE ROW)
					Basin H	Tc was use	d										

# FALCON TRUCKING FILING NO. 1 PROPOSED DRAINAGE CALCULATIONS (Area Runoff Coefficient Summary)

		STREETS / DEVELOPED			DE	VELOPED L	OTS	DEVEL	OPED LAND	SCAPING	RUNOFF C	DEFFICIENT
AREA	TOTAL AREA (Acres)	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	AREA (Acres)	C <sub>5</sub>	C <sub>100</sub>	С5	C <sub>100</sub>
41412.9359	0.95	0.14	0.90	0.96	0.00	0.41	0.59	0.81	0.12	0.39	0.23	0.47
196037.5092	4.50	0.00	0.90	0.96	4.50	0.49	0.62	0.00	0.12	0.39	0.49	0.62
220884.164	5.07	0.00	0.90	0.96	5.07	0.49	0.62	0.00	0.12	0.39	0.49	0.62
121982.6078	2.80	0.00	0.90	0.96	2.80	0.49	0.62	0.00	0.12	0.39	0.49	0.62
19904.6983	0.46	0.00	0.90	0.96	0.23	0.49	0.62	0.23	0.12	0.39	0.31	0.51
148540.714	3.41	0.00	0.90	0.96	0.00	0.41	0.59	3.41	0.12	0.39	0.12	0.39
15980.5358	0.37	0.00	0.90	0.96	0.00	0.41	0.59	0.37	0.12	0.39	0.12	0.39
62573.1761	1.44	0.00	0.90	0.96	0.00	0.41	0.59	1.44	0.08	0.35	0.08	0.35
52997.6828	1.22	0.00	0.90	0.96	0.12	0.12	0.39	1.09	0.08	0.35	0.08	0.35
13240.8606	0.30	0.03	0.90	0.96	0.00	0.41	0.59	0.27	0.12	0.39	0.20	0.45
7253.9384	0.17	0.00	0.90	0.96	0.04	0.12	0.39	0.12	0.08	0.35	0.09	0.36
42071.6429	0.97	0.00	0.90	0.96	0.00	0.41	0.59	0.97	0.12	0.39	0.12	0.39
207398.1901	4.76	0.00	0.90	0.96	4.76	0.49	0.62	0.00	0.12	0.39	0.49	0.62
254291.867	5.84	0.00	0.90	0.96	4.81	0.49	0.62	1.03	0.12	0.39	0.42	0.58
108513.4307	2.49	0.00	0.90	0.96	2.49	0.49	0.62	0.00	0.12	0.39	0.49	0.62
77225.004	0.90	0.00	0.90	0.96	0.00	0.81	0.88	0.90	0.12	0.39	0.12	0.39
17954.8589	0.41	0.00	0.90	0.96	0.00	0.41	0.59	0.41	0.10	0.37	0.10	0.37
15514.9657	0.36	0.00	0.90	0.96	0.36	0.49	0.62	0.00	0.12	0.39	0.49	0.62
3385.1025	0.08	0.00	0.90	0.96	0.08	0.49	0.62	0.00	0.12	0.39	0.49	0.62
17612.2726	0.40	0.00	0.90	0.96	0.40	0.40	0.56	0.00	0.12	0.39	0.40	0.56
9575.7189	0.22	0.00	0.90	0.96	0.22	0.40	0.56	0.00	0.12	0.39	0.40	0.56
4812.5786	0.11	0.11	0.90	0.96	0.00	0.41	0.59	0.00	0.12	0.39	0.90	0.96
3391.6752	0.08	0.08	0.90	0.96	0.00	0.41	0.59	0.00	0.12	0.39	0.90	0.96
14241.6721	0.33	0.00	0.90	0.96	0.33	0.40	0.56	0.00	0.12	0.39	0.40	0.56
	1.00	0.00	0.90	0.96	0.00	0.38	0.57	1.00	0.12	0.39	0.12	0.39
	1.40	0.00	0.90	0.96	0.00	0.38	0.57	1.40	0.09	0.36	0.09	0.36
	2.00	0.00	0.90	0.96	2.00	0.38	0.57	0.00	0.09	0.36	0.38	0.57
	0.40	0.00	0.90	0.96	0.40	0.38	0.57	0.00	0.09	0.36	0.38	0.57
	2.00	0.00	0.90	0.96	1.60	0.38	0.57	0.40	0.09	0.36	0.32	0.53
	1.30	0.00	0.90	0.96	1.30	0.38	0.57	0.00	0.09	0.36	0.38	0.57
	0.80	0.00	0.90	0.96	0.80	0.38	0.57	0.00	0.09	0.36	0.38	0.57
	0.70	0.00	0.90	0.96	0.70	0.38	0.57	0.00	0.09	0.36	0.38	0.57
	0.20	0.00	0.90	0.96	0.20	0.38	0.57	0.00	0.09	0.36	0.38	0.57
	1.10	0.00	0.90	0.96	1.10	0.38	0.57	0.00	0.09	0.36	0.38	0.57
	0.20	0.00	0.90	0.90	0.20	0.38	0.57	0.00	0.09	0.36	0.38	0.57
	0.40	0.00	0.90	0.96	0.40	0.38	0.57	0.00	0.09	0.36	0.38	0.57
	1.23	0.00	0.90	0.96	1.23	0.45	0.59	0.00	0.09	0.36	0.45	0.59
	0.93	0.00	0.90	0.96	0.93	0.45	0.59	0.00	0.09	0.36	0.45	0.59
	0.82	0.00	0.90	0.96	0.82	0.45	0.59	0.00	0.09	0.36	0.45	0.59
	41412.9359 196037.5092 220884.164 121982.6078 19904.6983 148540.714 15980.5358 62573.1761 52997.6828 13240.8606 7253.9384 42071.6429 207398.1901 254291.867 108513.4307 77225.004 17954.8589 15514.9657 3385.1025 17612.2726 9575.7189 4812.5786 3391.6752	AREA         AREA (Acres)           41412.9359         0.95           196037.5092         4.50           220884.164         5.07           121982.6078         2.80           19904.6983         0.46           148540.714         3.41           15980.5358         0.37           62573.1761         1.44           52997.6828         1.22           13240.8606         0.03           7253.9384         0.17           42071.6429         0.97           207398.1901         4.76           254291.867         5.84           108513.4307         2.49           77225.004         0.90           17954.8589         0.41           15514.9657         0.36           3385.1025         0.08           17612.2726         0.40           9575.7189         0.22           4812.5786         0.11           3391.6752         0.08           14241.6721         0.33           100         1.40           2.00         1.30           0.40         2.00           1.30         0.80           0.70         0.20      <	AREA         TOTAL (Acres)         AREA (Acres)           41412.9359         0.95         0.14           196037.5092         4.50         0.00           220884.164         5.07         0.00           121982.6078         2.80         0.00           19904.6983         0.46         0.00           19904.6983         0.46         0.00           1980.5358         0.37         0.00           15980.5358         0.37         0.00           62573.1761         1.44         0.00           13240.8606         0.30         0.03           7253.9384         0.17         0.00           207398.1901         4.76         0.00           254291.867         5.84         0.00           77225.004         0.90         0.00           17954.8589         0.41         0.00           17612.2726         0.40         0.00           17612.5786         0.11         0.11           3391.6752         0.08         0.08           1421.5786         0.11         0.11           3391.6752         0.08         0.00           1.40         0.00         0.00           2.00         <	AREA         TOTAL (Acres)         AREA (Acres)         Cs           41412.9359         0.95         0.14         0.90           196037.5092         4.50         0.00         0.90           220884.164         5.07         0.00         0.90           121982.6078         2.80         0.00         0.90           121982.6078         2.80         0.00         0.90           148540.714         3.41         0.00         0.90           15980.5358         0.37         0.00         0.90           62573.1761         1.44         0.00         0.90           13240.8606         0.30         0.03         0.90           7253.9384         0.17         0.00         0.90           207398.1901         4.76         0.00         0.90           207398.1901         4.76         0.00         0.90           207398.1901         4.76         0.00         0.90           17255.004         0.90         0.00         0.90           17954.8589         0.41         0.00         0.90           17612.2726         0.40         0.00         0.90           17612.2726         0.40         0.00         0.90 <td>AREA         TOTAL AREA (Acres)         AREA (Acres)         C5         C100           41412.9359         0.95         0.14         0.90         0.96           120884.164         5.07         0.00         0.90         0.96           121982.6078         2.80         0.00         0.90         0.96           121982.6078         2.80         0.00         0.90         0.96           15980.5358         0.37         0.00         0.90         0.96           15980.5358         0.37         0.00         0.90         0.96           15980.5358         0.37         0.00         0.90         0.96           15980.5358         0.37         0.00         0.90         0.96           15980.5358         0.37         0.00         0.90         0.96           15980.5358         0.37         0.00         0.90         0.96           15249.8606         0.30         0.03         0.90         0.96           15249.8606         0.30         0.00         0.90         0.96           1534.3607         2.49         0.00         0.90         0.96           17954.8589         0.41         0.00         0.90         0.96</td> <td>AREA         TOTAL (Acres)         AREA (Acres)         C3         C100         AREA (Acres)           41412.9359         0.95         0.14         0.90         0.96         0.00           196037.5092         4.50         0.00         0.90         0.96         4.50           220884.164         5.07         0.00         0.90         0.96         2.80           12982.6078         2.80         0.00         0.90         0.96         2.80           19904.6983         0.46         0.00         0.90         0.96         0.00           15980.5358         0.37         0.00         0.90         0.96         0.00           62573.1761         1.44         0.00         0.90         0.96         0.00           7235.9384         0.17         0.00         0.90         0.96         0.00           273.1761         4.76         0.00         0.90         0.96         0.00           273.1761         1.44         0.00         0.90         0.96         0.00           273.1761         1.47         0.00         0.90         0.96         0.00           273.1761         1.47         0.00         0.90         0.96         0.00</td> <td>AREA         TOTAL (Acres)         AREA (Acres)         C5         C100         AREA (Acres)         C5           41412.9359         0.95         0.14         0.90         0.96         0.00         0.41           196037.5092         4.50         0.00         0.90         0.96         4.50         0.49           220884.164         5.07         0.00         0.90         0.96         5.07         0.49           19904.6983         0.46         0.00         0.90         0.96         0.23         0.49           18905.358         0.37         0.00         0.90         0.96         0.00         0.41           62573.1761         1.44         0.00         0.90         0.96         0.00         0.41           52997.6828         1.22         0.00         0.90         0.96         0.00         0.41           7253.9384         0.17         0.00         0.90         0.96         0.04         0.12           42071.6429         0.97         0.00         0.90         0.96         4.76         0.49           7253.9384         0.17         0.00         0.90         0.96         4.76         0.49           7252.90.4         0.90</td> <td>AREA         AREA (Acres)         AREA (Acres)         AREA (Acres)         C5         C100         AREA (Acres)         C5         C100           41412.9359         0.95         0.14         0.90         0.96         0.00         0.41         0.59           196037.5092         4.50         0.00         0.90         0.96         5.07         0.49         0.62           121982.6078         2.80         0.00         0.90         0.96         2.33         0.49         0.62           15980.5358         0.37         0.00         0.90         0.96         0.00         0.41         0.59           15880.5358         0.37         0.00         0.90         0.96         0.00         0.41         0.59           15880.5358         0.37         0.00         0.90         0.96         0.00         0.41         0.59           15980.5358         0.37         0.00         0.90         0.96         0.00         0.41         0.59           15240.8060         0.30         0.33         0.90         0.96         0.00         0.41         0.59           20738.901         4.76         0.00         0.90         0.96         0.00         0.41         0.59</td> <td>AREA         TOTAL (Ares)         AREA (Ares)         C5         C100         AREA (Ares)           4112.9359         0.95         0.14         0.90         0.96         0.50         0.49         0.62         0.00           220884.164         5.07         0.00         0.90         0.96         2.80         0.49         0.62         0.00           19906.6983         0.46         0.00         0.90         0.96         0.00         0.41         0.59         3.41           18848.711         3.41         0.00         0.90         0.96         0.00         0.41         0.59         0.37           18348.711         3.41         0.00         0.90         0.96         0.00         0.41         0.59         0.37           18348.711         3.41         0.00         0.90         0.96         0.00         0.41         0.59         0.37           25373.163         0.37         0.00         0.90         0.96         0.00         0.41         0.59</td> <td>AREA         TOTAL (Acres)         AREA (Acres)         Cs (Acres)         AREA (Acres)         Cs (Acres)           19607.5092         4.50         0.00         0.90         0.96         5.07         0.49         0.62         0.00         0.12           120884.164         5.07         0.00         0.90         0.96         2.30         0.49         0.62         0.00         0.12           19904.6983         0.46         0.00         0.90         0.96         0.00         0.41         0.59         0.31         0.12           19904.6983         0.37         0.00         0.90         0.96         0.00         0.41         0.59         1.44         0.08           2573.17c1         1.44         0.00         0.90         0.96         0.00         0.41         0.59         0.27         0.12           2573.17c1         1.44         0.00         0.90         0.96         0.00         0.41         0.59         0.27         0.12           2738.9384         0.17</td> <td><math display="block"> \begin{array}{ c c c c c c c c c c c c c c c c c c c</math></td> <td>AREA         TOTAL (Acres)         REA (Acres)         C<sub>5</sub>         C<sub>100</sub>         AREA (Acres)         C<sub>5</sub>         C<sub>100</sub>         AREA (Acres)         C<sub>5</sub>         C<sub>100</sub>         C<sub>5</sub>         C<sub>100</sub>         C<sub>5</sub>         C<sub>100</sub>         C<sub>5</sub>         C<sub>100</sub>         C<sub>5</sub>         C<sub>100</sub>         C<sub>5</sub>         C<sub>100</sub>         C<sub>5</sub>           111292507         9.50         0.40         0.090         0.96         4.50         0.49         0.62         0.00         0.12         0.39         0.49           121992.607         2.80         0.000         0.90         0.96         2.80         0.49         0.62         0.00         0.12         0.39         0.49           121992.607         2.80         0.000         0.90         0.96         0.23         0.49         0.62         0.00         0.12         0.39         0.47           1341         0.00         0.90         0.96         0.00         0.41         0.59         1.44         0.08         0.35         0.08           13240.806         0.30         0.03         0.90         0.96         0.00         0.41         0.59         0.77         0.12         0.39         0.20           13240.806         0.30         0.30&lt;</td>	AREA         TOTAL AREA (Acres)         AREA (Acres)         C5         C100           41412.9359         0.95         0.14         0.90         0.96           120884.164         5.07         0.00         0.90         0.96           121982.6078         2.80         0.00         0.90         0.96           121982.6078         2.80         0.00         0.90         0.96           15980.5358         0.37         0.00         0.90         0.96           15980.5358         0.37         0.00         0.90         0.96           15980.5358         0.37         0.00         0.90         0.96           15980.5358         0.37         0.00         0.90         0.96           15980.5358         0.37         0.00         0.90         0.96           15980.5358         0.37         0.00         0.90         0.96           15249.8606         0.30         0.03         0.90         0.96           15249.8606         0.30         0.00         0.90         0.96           1534.3607         2.49         0.00         0.90         0.96           17954.8589         0.41         0.00         0.90         0.96	AREA         TOTAL (Acres)         AREA (Acres)         C3         C100         AREA (Acres)           41412.9359         0.95         0.14         0.90         0.96         0.00           196037.5092         4.50         0.00         0.90         0.96         4.50           220884.164         5.07         0.00         0.90         0.96         2.80           12982.6078         2.80         0.00         0.90         0.96         2.80           19904.6983         0.46         0.00         0.90         0.96         0.00           15980.5358         0.37         0.00         0.90         0.96         0.00           62573.1761         1.44         0.00         0.90         0.96         0.00           7235.9384         0.17         0.00         0.90         0.96         0.00           273.1761         4.76         0.00         0.90         0.96         0.00           273.1761         1.44         0.00         0.90         0.96         0.00           273.1761         1.47         0.00         0.90         0.96         0.00           273.1761         1.47         0.00         0.90         0.96         0.00	AREA         TOTAL (Acres)         AREA (Acres)         C5         C100         AREA (Acres)         C5           41412.9359         0.95         0.14         0.90         0.96         0.00         0.41           196037.5092         4.50         0.00         0.90         0.96         4.50         0.49           220884.164         5.07         0.00         0.90         0.96         5.07         0.49           19904.6983         0.46         0.00         0.90         0.96         0.23         0.49           18905.358         0.37         0.00         0.90         0.96         0.00         0.41           62573.1761         1.44         0.00         0.90         0.96         0.00         0.41           52997.6828         1.22         0.00         0.90         0.96         0.00         0.41           7253.9384         0.17         0.00         0.90         0.96         0.04         0.12           42071.6429         0.97         0.00         0.90         0.96         4.76         0.49           7253.9384         0.17         0.00         0.90         0.96         4.76         0.49           7252.90.4         0.90	AREA         AREA (Acres)         AREA (Acres)         AREA (Acres)         C5         C100         AREA (Acres)         C5         C100           41412.9359         0.95         0.14         0.90         0.96         0.00         0.41         0.59           196037.5092         4.50         0.00         0.90         0.96         5.07         0.49         0.62           121982.6078         2.80         0.00         0.90         0.96         2.33         0.49         0.62           15980.5358         0.37         0.00         0.90         0.96         0.00         0.41         0.59           15880.5358         0.37         0.00         0.90         0.96         0.00         0.41         0.59           15880.5358         0.37         0.00         0.90         0.96         0.00         0.41         0.59           15980.5358         0.37         0.00         0.90         0.96         0.00         0.41         0.59           15240.8060         0.30         0.33         0.90         0.96         0.00         0.41         0.59           20738.901         4.76         0.00         0.90         0.96         0.00         0.41         0.59	AREA         TOTAL (Ares)         AREA (Ares)         C5         C100         AREA (Ares)           4112.9359         0.95         0.14         0.90         0.96         0.50         0.49         0.62         0.00           220884.164         5.07         0.00         0.90         0.96         2.80         0.49         0.62         0.00           19906.6983         0.46         0.00         0.90         0.96         0.00         0.41         0.59         3.41           18848.711         3.41         0.00         0.90         0.96         0.00         0.41         0.59         0.37           18348.711         3.41         0.00         0.90         0.96         0.00         0.41         0.59         0.37           18348.711         3.41         0.00         0.90         0.96         0.00         0.41         0.59         0.37           25373.163         0.37         0.00         0.90         0.96         0.00         0.41         0.59	AREA         TOTAL (Acres)         AREA (Acres)         Cs (Acres)         AREA (Acres)         Cs (Acres)           19607.5092         4.50         0.00         0.90         0.96         5.07         0.49         0.62         0.00         0.12           120884.164         5.07         0.00         0.90         0.96         2.30         0.49         0.62         0.00         0.12           19904.6983         0.46         0.00         0.90         0.96         0.00         0.41         0.59         0.31         0.12           19904.6983         0.37         0.00         0.90         0.96         0.00         0.41         0.59         1.44         0.08           2573.17c1         1.44         0.00         0.90         0.96         0.00         0.41         0.59         0.27         0.12           2573.17c1         1.44         0.00         0.90         0.96         0.00         0.41         0.59         0.27         0.12           2738.9384         0.17	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	AREA         TOTAL (Acres)         REA (Acres)         C <sub>5</sub> C <sub>100</sub> AREA (Acres)         C <sub>5</sub> C <sub>100</sub> AREA (Acres)         C <sub>5</sub> C <sub>100</sub> C <sub>5</sub> 111292507         9.50         0.40         0.090         0.96         4.50         0.49         0.62         0.00         0.12         0.39         0.49           121992.607         2.80         0.000         0.90         0.96         2.80         0.49         0.62         0.00         0.12         0.39         0.49           121992.607         2.80         0.000         0.90         0.96         0.23         0.49         0.62         0.00         0.12         0.39         0.47           1341         0.00         0.90         0.96         0.00         0.41         0.59         1.44         0.08         0.35         0.08           13240.806         0.30         0.03         0.90         0.96         0.00         0.41         0.59         0.77         0.12         0.39         0.20           13240.806         0.30         0.30<

Date: 12/11/2021 Checked by:

## FALCON TRUCKING FILING NO. 1 PROPOSED DRAINAGE CALCULATIONS (Area Drainage Summary)

From	Area Runoff Coef	fficient Summary			OVERLA	IND		57	REET / CH	ANNEL FLO	)W	Time of T	ravel (T <sub>t</sub> )	INTEN	SITY *	TOTAL	FLOWS
	AREA												1				
BASIN	TOTAL	C5	C100	C5	Length	Height	T <sub>C</sub>	Length	Slope	Velocity	Tt	TOTAL	CHECK	I <sub>5</sub>	I <sub>100</sub>	Q5	Q100
	(Acres)		d Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
A	0.95	0.23	0.47	0.23	75	8	6.2	0	0.0%	0.0	0.0	6.2	10.4	4.8	8.1	1.1	3.7
<u> </u>	4.50	0.49	0.62	0.49	75	1.5	7.6	460	1.7%	2.6	2.9	10.5	13.0	4.1	6.8	8.9	19.0
С	5.07	0.49	0.62	0.49	140	1.7	12.2	575	1.4%	2.4	4.1	16.3	14.0	3.6	6.1	9.0	19.1
D	2.80	0.49	0.62	0.49	140	1.7	12.2	280	3.9%	4.0	1.2	13.4	12.3	3.8	6.4	5.2	11.1
D1	0.46	0.31	0.51	0.31	75	1.5	9.9	160	8.8%	5.9	0.5	10.3	11.3	4.1	6.8	0.6	1.6
E	3.41	0.12	0.39	0.12	50	16	4.0	570	0.5%	1.4	6.7	10.7	13.4	4.0	6.8	1.6	9.0
F	0.37	0.12	0.39	0.12	100	6	9.8	130	10.0%	6.3	0.3	10.1	11.3	4.1	6.9	0.2	1.0
G	1.44	0.08	0.35	0.08	100	10	8.6	0	0.0%	0.0	0.0	8.6	10.6	4.4	7.3	0.5	3.7
Н	1.22	0.08	0.35	0.08	100	7.5	9.4	0	0.0%	0.0	0.0	9.4	10.6	4.2	7.1	0.4	3.0
Ι	0.30	0.20	0.45	0.20	20	0.6	5.1	0	0.0%	0.0	0.0	5.1	10.1	5.1	8.6	0.3	1.2
J	0.17	0.09	0.36	0.09	100	9	8.8	0	0.0%	0.0	0.0	8.8	10.6	4.3	7.2	0.1	0.4
K	0.97	0.12	0.39	0.12	100	8	8.9	0	0.0%	0.0	0.0	8.9	10.6	4.3	7.2	0.5	2.7
L	4.76	0.49	0.62	0.49	100	2	8.8	850	2.2%	3.0	4.7	13.5	15.3	3.7	6.2	8.6	18.2
М	5.84	0.42	0.58	0.42	100	18	4.7	650	2.3%	3.0	3.6	8.3	14.2	4.4	7.4	11.0	25.1
N	2.49	0.49	0.62	0.49	100	2	8.8	230	2.2%	2.9	1.3	10.1	11.8	4.1	6.9	5.0	10.7
0	0.90	0.12	0.39	0.12	50	16	4.0	250	0.5%	1.4	2.9	6.9	11.7	4.7	7.9	0.5	2.8
Р	0.41	0.10	0.37	0.10	100	8	9.1	0	0.0%	0.0	0.0	9.1	10.6	4.3	7.2	0.2	1.1
0	0.36	0.49	0.62	0.49	100	2	8.8	90	1.0%	2.0	0.8	9.5	11.1	4.2	7.1	0.7	1.6
02	0.08	0.49	0.62	0.49	25	1	3.5	0	0.0%	0.0	0.0	5.0	10.1	5.2	8.7	0.2	0.4
R	0.40	0.40	0.56	0.40	50	3	4.9	0	0.0%	0.0	0.0	5.0	10.3	5.2	8.7	0.8	2.0
R2	0.22	0.40	0.56	0.40	50	3	4.9	0	0.0%	0.0	0.0	5.0	10.3	5.2	8.7	0.5	1.1
S	0.11	0.90	0.96	0.90	25	1	1.1	0	0.0%	0.0	0.0	5.0	10.1	5.2	8.7	0.5	0.9
S2	0.08	0.90	0.96	0.90	25	1	1.1	0	0.0%	0.0	0.0	5.0	10.1	5.2	8.7	0.4	0.6
Т	0.33	0.40	0.56	0.40	50	3	4.9	0	0.0%	0.0	0.0	5.0	10.3	5.2	8.7	0.7	1.6
OS6	1.00	0.12	0.39	0.12	50	2	7.9	5	4.0%	1.4	0.1	8.0	10.3	4.1	6.9	0.5	2.7
Al	1.40	0.09	0.36	0.09	75	4	9.1	0	1.4%	0.8	0.0	9.1	10.4	4.3	7.2	0.5	3.6
A2	2.00	0.38	0.57	0.38	110	3	9.8	500	1.4%	2.4	3.5	13.3	13.4	3.7	6.2	2.8	7.1
A3	0.40	0.38	0.57	0.38	70	2	7.7	370	1.4%	2.4	2.6	10.3	12.4	4.1	6.9	0.6	1.6
A4	2.00	0.32	0.53	0.32	100	5	8.3	250	2.9%	3.4	1.2	9.5	11.9	4.2	7.1	2.7	7.5
A5	1.30	0.38	0.57	0.38	70	3	6.7	340	3.6%	3.8	1.5	8.2	12.3	4.4	7.4	2.2	5.5
A6	0.80	0.38	0.57	0.38	120	4	9.6	170	3.5%	3.7	0.8	10.3	11.6	4.1	6.9	1.2	3.1
A7	0.70	0.38	0.57	0.38	100	4	8.2	250	3.5%	3.7	1.1	9.3	11.9	4.2	7.1	1.1	2.8
A8	0.20	0.38	0.57	0.38	35	1	5.4	60	4.0%	4.0	0.3	5.7	10.5	5.0	8.4	0.4	1.0
A9	1.10	0.38	0.57	0.38	70	3	6.7	520	2.9%	3.4	2.5	9.3	13.3	4.2	7.1	1.8	4.5
A12	0.20	0.38	0.57	0.38	70	2	7.7	520	4.0%	4.0	2.2	9.9	13.3	4.2	7.0	0.3	0.8
A13	0.40	0.38	0.57	0.38	70	2	7.7	300	4.0%	4.0	1.3	8.9	12.1	4.3	7.2	0.7	1.6
A7*	1.23	0.45	0.59	0.45	100	6	6.5	443	3.0%	3.5	2.1	8.6	13.0	4.4	7.3	2.4	5.3
A8*	0.93	0.45	0.59	0.45	60	1.2	7.2	329	2.5%	3.2	1.7	9.0	12.2	4.3	7.2	1.8	4.0
A9*	0.82	0.45	0.59	0.45	80	1.6	8.4	200	2.0%	2.8	1.2	9.5	11.6	4.2	7.1	1.6	3.4

\* Intensity equations assume a minimum travel time of 5 minutes.

Calculated by: DLM Date: 12/11/2021 Checked by:

### FALCON TRUCKING FILING NO. 1 PROPOSED DRAINAGE CALCULATIONS

(Basin Routing Summary)

	L FLOWS	TOTA	SITY *	INTEN	Time of Travel (T <sub>t</sub> )	W	NNEL FLO	/ CHA	PIPE		ERLAND	OVE			From Area Runoff Coefficient Summary	
COMMENTS	Q <sub>100</sub>	Q5	I <sub>100</sub>	I <sub>5</sub>	TOTAL	T <sub>t</sub>	Velocity	Slope	Length	T <sub>C</sub>	Height	Length	CA <sub>100</sub>	CA <sub>5</sub>	CONTRIBUTING BASINS	ESIGN POINT
	(c.f.s.)	(c.f.s.)	(in/hr) 7.6	(in/hr) 4.5	(min) 7.7	(min) 1.5	(fps) 3.3	(%) 2.7%	(ft) 300	(min) 6.2	(ft)	(ft)	3.24	2.43	4 B	
Prop 36" Storm Sewer	24.6	11.0	7.6	4.5	1.1	1.5	5.5	2.7%	300	6.2			3.24	2.43	А, В	1
										sed	Tc Was Use	Basin A	-			
Prop 36" Storm Sewer	19.1	9.0	6.1	3.6	14.0					14.0			3.14	2.48	С	2
																-
											Tc Was Use	Basin C				
Prop 24" Storm Sewer	11.1	5.2	6.4	3.8	12.3					12.3			1.74	1.37	D	3
											Tc Was Use	Pasia D	-			
	1.6	0.6	6.8	4.1	10.3					10.3	Te was Use	Basin D	0.23	0.14	D1	4
	1.0	0.0	0.0	4.1	10.5					10.5			0.25	0.14	Ы	7
									1	sed	Tc Was Us	Basin D1				
FSD Pond 1	50.9	23.3	6.1	3.6	14.0					14.0			8.35	6.42	PR1, PR2, PR3, DP4, E	5
											nt 2 Tc Was	Design Poir				
	4.5	0.7	6.9	4.1	10.1					10.1			0.65	0.16	F, G	6
										ed	Tc Was Use	Rasin F	-			
	3.0	0.4	7.1	4.2	9.4					9.4	10 11 43 0 30	Dasani	0.43	0.10	Н	7
	5.5			-											21	1
									1	ed	Tc Was Use	Basin H				
Grafite Drive	1.5	0.4	7.8	4.7	6.9					6.9			0.20	0.08	I, J	8
											c Was Used	Avg T				-
West Side of Marksheffel	4.5 12.0	0.7 2.3	6.9	4.1	10.1					10.1			0.65 1.74	0.16 0.55	DP6 POND OUTFALL	9
	16.5	2.3									5 Tc Used	DP	2.39	0.71	(POND 1)	
Prop 30" Storm Sewer	20.6	9.0	6.2	3.7	13.5					13.5			3.33	2.45	K, L	10
											Tc Was Use	Basin L				
Prop 36" Storm Sewer	25.1	11.0	7.4	4.4	8.3					8.3			3.38	2.48	М	11
										ead	Tc Was Use	Bacin M				
Prop 42" Storm Sewer	10.7	5.0	6.9	4.1	10.1					10.1	Te mus est	Dubiniti	1.54	1.22	N	12
110p 42 Storin Sewer	10.7	5.0	0.7		10.1					10.1						12
									1	ed	Tc Was Use	Basin N	-			
FSD Pond 2	53.2	23.0	6.2	3.7	13.5					13.5			8.61	6.26	PR8, O	13
											c Was Used	PR8 T				
Discharges to Talc Drive	2.6	0.9	7.1	4.2	9.5					9.5			0.37	0.22	P, Q	14
									1		T . W /	Duri O	-			
	0.4	0.2	8.7	5.2	5.0					5.0	Tc Was Use	Basin Q	0.05	0.04	Q2	14A
Discharges to Talc Drive	0.4	0.2	ð./	3.2	5.0					5.0			0.05	0.04	Q2	14A
									1	sed	Tc Was Us	Basin O?	ŀ			
Discharges to EMVR Filing	2.0	0.8	8.7	5.2	5.0					5.0			0.23	0.16	R	15
											Tc Was Use	Basin R				
Discharges to EMVR Filing	1.1	0.5	8.7	5.2	5.0					5.0			0.12	0.09	R2	15A
									1		T. W	Duris D2				
Distance D. M. D.	0.9	0.5	8.7	5.2	5.0					sed 5.0	Tc Was Us	Basın R2	0.11	0.10	S	16
Discharges to Basaltic Driv	0.9	0.5	8.7	5.2	5.0					5.0			0.11	0.10	3	10
										ed	Tc Was Use	Basin S	F			
Discharges to Basaltic Driv	0.6	0.4	8.7	5.2	5.0					5.0			0.07	0.07	82	16A
~																
											Te Was Us	Basin S2				
Discharges to EMVR Filing	1.6	0.7	8.7	5.2	5.0					5.0			0.18	0.13	Т	17

Date: 12/11/2021 Checked by: VAS

# FALCON TRUCKING FILING NO. 1 FINAL DRAINAGE REPORT (Surface Routing Summary- surface runoff)

	From Area Runoff Coefficient Summary				OVE	ERLAND		PIPE	/ CHA	NNEL FLO	W	Time of Travel $(T_t)$	INTEN	SITY *	TOTAL .	FLOWS	
DESIGN POINT	CONTRIBUTING BASINS	CA5	CA100	C <sub>5</sub>	Length	Height	T <sub>C</sub>	Length	Slope	Velocity	Tt	TOTAL	I <sub>5</sub>	I <sub>100</sub>	Q5	Q <sub>100</sub>	COMMENTS
					(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)	
2*	DP14, A1, A2, OS6	1.22	2.41									13.3	3.7	6.2	4.5	15.0	EX CROSS PAN
				See	e Area Drai	nage Sheet	for Input										
3*	DP2, A3	1.37	2.64									13.3	3.7	6.2	5.1	16.4	EX 4' AT GRADE INLET
																	2.3/3.7 intercepted
				See	e Area Drai	nage Sheet	for Input										2.8/12.7 flowby
4*	DP14A, DP15, A5	0.69	1.02									8.2	4.4	7.4	3.1	7.5	EX 4' AT GRADE INLET
																	1.9/2.7 intercepted
				See	e Area Drai	nage Sheet	for Input										1.2/4.8 flowby
5*	FB DP3, A4	1.40	3.10									14.8	3.5	5.9	4.9	18.4	EX 4' AT GRADE INLET
																	2.2/3.7 intercepted
				See	e Area Drai	nage Sheet	for Input										2.4/13.7 flowby
6*	A6	0.30	0.46									10.3	4.1	6.9	1.2	3.1	EX 4' AT GRADE INLET
																	1.1/1.9 intercepted
				See	e Area Drai	nage Sheet	for Input										0.1/1.2 flowby
7*	FB DP4, A7, 15A	0.62	1.17									9.4	4.2	7.1	2.6	8.3	EX 4' AT GRADE INLET
																	1.7/2.8 intercepted
				See	e Area Drai	nage Sheet	for Input										0.9/5.5 flowby
8*	FB DP5, FB DP6, FB DP7, A8, A12	1.10	3.55									9.5	4.2	7.1	4.6	25.0	EX 8' AT GRADE INLET
																	3.8/8.7 intercepted
				See	e Area Drai	nage Sheet	for Input										0.5/15.1 flowby
9*	DP16, A9, A13, FB DP8	0.87	3.27									15.5	3.5	5.8	3.0	19.1	EX 16' AT GRADE INLET
																	2.7/14.5 intercepted
				See	e Area Drai	nage Sheet	for Input										0.0/3.6 flowby
7**	A8*	0.42	0.55									9.0	4.3	7.2	1.8	4.0	EX 8' SUMP INLET
																	1.8/4.0 intercepted
				See	e Area Drai	nage Sheet	for Input										
8**	DP16A, DP17, A7*, A9*	1.12	1.47									9.5	4.2	7.1	4.7	10.4	EX 10' SUMP INLET
																	4.7/10.4 intercepted
				See	e Area Drai	nage Sheet	for Input										

## FALCON TRUCKING FILING NO. 1 **PROPOSED DRAINAGE CALCULATIONS**

(Storm Sewer Routing Summary)

					Inter	isity*	Fl	low	PIPE S
PIPE RUN	Contributing Pipes/Design Points	Equivalent CA 5	Equivalent CA <sub>100</sub>	Maximum T <sub>C</sub>	$I_5$	I 100	Q 5	Q 100	
1	DP1	2.43	3.24	7.7	4.5	7.6	11.0	24.6	36" RC
2	DP2	2.48	3.14	14.0	3.6	6.1	9.0	19.1	30" RC
3	DP3	1.37	1.74	12.3	3.8	6.4	5.2	11.1	24" R0
4	POND 1 OUTFALL	0.55	1.74	10.1	4.1	6.9	2.3	12.0	24" RC
5	DP10	2.45	3.33	13.5	3.7	6.2	9.0	20.6	30" RC
6	DP11	2.48	3.38	8.3	4.4	7.4	11.0	25.1	36" RC
7	PR5, PR6	4.93	6.71	13.5	3.7	6.2	18.1	41.5	42" RC
8	PR7, DP12	6.15	8.26	13.5	3.7	6.2	22.6	51.0	42" RC
9	POND 2 OUTFALL	0.15	1.90	13.5	3.7	6.2	0.6	11.7	18" RC
1*	INLET 4*	0.43	0.36	8.2	4.4	7.4	1.9	2.7	18" RC
2*	PR1*	0.43	0.36	8.2	4.4	7.4	1.9	2.7	18" RC
3*	PR2*	0.43	0.36	8.2	4.4	7.4	1.9	2.7	18" RC
4*	INLET 7*	0.40	0.40	9.4	4.2	7.1	1.7	2.8	18" RC
4A*	INLET 6*	0.27	0.28	10.3	4.1	6.9	1.1	1.9	18" RC
5*	PR3*, PR4*, PR4A*	1.10	1.04	10.3	4.1	6.9	4.5	7.1	18" RC
5A*	INLET 3*	0.62	0.60	13.3	3.7	6.2	2.3	3.7	18" RC
6*	PR5A*	0.62	0.60	13.3	3.7	6.2	2.3	3.7	18" RC
7*	PR6*	0.62	0.60	13.3	3.7	6.2	2.3	3.7	18" RC
8*	INLET 5*	0.62	0.62	14.8	3.5	5.9	2.2	3.7	18" RC
9*	PR7*, PR8*	1.24	1.22	14.8	3.5	5.9	4.4	7.2	18" RC
10*	PR5*, PR9*	2.34	2.25	14.8	3.5	5.9	8.3	13.4	24" RC
11*	INLET 8*	0.90	1.23	9.5	4.2	7.1	3.8	8.7	18" RC
12*	PR10*, PR11*	3.25	3.49	14.8	3.5	5.9	11.5	20.7	30" RC
13*	INLET 9	0.78	2.49	15.5	3.5	5.8	2.7	14.5	18" RC
9**	PR12*, PR13*	4.02	5.97	14.8	3.5	5.9	14.3	35.5	36" RC
10**	INLET 7**	0.42	0.55	9.0	4.3	7.2	1.8	4.0	18" RG
11**	PR9**, PR10**	4.44	6.52	15.0	3.5	5.9	15.6	38.5	36" R0
12**	PR11, INLET 8**	5.57	7.99	15.0	3.5	5.9	19.6	47.2	36" RC

FB- Flow By from Design Point DP - Design Point EX - Existing Design Point

INT- Intercepted Flow from Design Point

Date: 12/11/2021 Checked by: VAS

HYDRAULIC CALCULATIONS / POND CALCULATIONS

	Weighted P	Percent Imp	erviousness (Pond	1)
Contributing Basins	Area (Acres)	<i>C</i> <sub>5</sub>	Impervious % (I)	(Acres)*(I)
A	0.95	0.23	0.13	0.12
В	4.50	0.49	0.70	3.15
С	5.07	0.49	0.70	3.55
D	2.80	0.49	0.70	1.96
E	3.41	0.12	0.07	0.24
Totals	16.73			9.02
Total Imperviousness			54%	

Contributing Basins	Area (Acres)	<i>C</i> <sub>5</sub>	Impervious % (I)	(Acres)*(I)
Column1	Column2	Column3	Column4	Column5
K	0.97	0.12	0.07	0.07
L	4.76	0.49	0.70	3.33
М	5.84	0.42	0.60	3.50
N	2.49	0.49	0.70	1.74
0	0.41	0.10	0.04	0.02
Totals	15.37			9.25
Total mperviousness			60%	

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

Project:	Falcon Truc	king Filing	No. 1	MHFD-D	etention, Version	4.04 (Febi	ruary 2021,	)						
Basin ID:	FSD Pond 1													
ZONE	2 ONE 1													
							_							
	1.410.2	100-YE ORIFIC	AR E		Depth Increment =		ft							
PERMANENT ORIFIC	1 AND 2 CES e Configura	tion (Reter	ntion Pond)		Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
			,		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft <sup>2</sup> )	Area (ft <sup>2</sup> )	(acre)	(ft 3)	(ac-ft)
Watershed Information Selected BMP Type =	EDB	1		6630	Top of Micropool		0.00				0 40	0.000	7	0.000
Watershed Area =	16.73	acres					1.00				500	0.001	187	0.004
Watershed Length =	1,375	ft					2.00				11,458	0.263	6,166	0.142
Watershed Length to Centroid =	740	ft					4.00				43,369	0.996	60,993	1.400
Watershed Slope = Watershed Imperviousness =	0.043 54.00%	ft/ft percent					6.00				57,403	1.318	161,765	3.714
Percentage Hydrologic Soil Group A =	0.0%	percent												
Percentage Hydrologic Soil Group B =	100.0%	percent												
Percentage Hydrologic Soil Groups C/D =	0.0%	percent												
Target WQCV Drain Time = Location for 1-hr Rainfall Depths =	40.0	hours												
After providing required inputs above inc		rainfall												
depths, click 'Run CUHP' to generate run	off hydrograpł	hs using												
the embedded Colorado Urban Hydro Water Quality Capture Volume (WQCV) =	0.303	acre-feet	Optional Use	er Overrides acre-feet										
Excess Urban Runoff Volume (EURV) =	0.972	acre-feet		acre-feet										
2-yr Runoff Volume (P1 = 1.19 in.) =	0.902	acre-feet	1.19	inches										
5-yr Runoff Volume (P1 = 1.5 in.) =	1.270	acre-feet	1.50	inches										
10-yr Runoff Volume (P1 = 1.75 in.) = 25-yr Runoff Volume (P1 = 2 in.) =	1.591 2.011	acre-feet acre-feet	1.75 2.00	inches inches										
50-yr Runoff Volume (P1 = 2.25 in.) =	2.356	acre-feet	2.25	inches										
100-yr Runoff Volume (P1 = 2.52 in.) =	2.791	acre-feet	2.52	inches										
500-yr Runoff Volume (P1 = 3.14 in.) =	3.680	acre-feet		inches										
Approximate 2-yr Detention Volume = Approximate 5-yr Detention Volume =	0.739	acre-feet acre-feet												
Approximate 10-yr Detention Volume =	1.317	acre-feet				-								
Approximate 25-yr Detention Volume =	1.434	acre-feet												
Approximate 50-yr Detention Volume = Approximate 100-yr Detention Volume =	1.497 1.656	acre-feet acre-feet												
Approximate 100-yr Detention Volume -	1.050	acterieet												
Define Zones and Basin Geometry		_												
Zone 1 Volume (WQCV) =	0.303	acre-feet												
Zone 2 Volume (EURV - Zone 1) = Zone 3 Volume (100-year - Zones 1 & 2) =	0.669	acre-feet acre-feet												
Total Detention Basin Volume =	1.656	acre-feet												
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>												
Initial Surcharge Depth (ISD) =	user	ft												
Total Available Detention Depth $(H_{total}) =$ Depth of Trickle Channel $(H_{TC}) =$	user	ft ft												
Slope of Trickle Channel $(S_{TC}) =$	user	ft/ft												
Slopes of Main Basin Sides ( $S_{main}$ ) =	user	H:V				1								
Basin Length-to-Width Ratio $(R_{L/W}) =$	user													
Initial Surcharge Area (A <sub>ISV</sub> ) =	user	ft²												
Surcharge Volume Length $(L_{ISV}) =$	user	ft												
Surcharge Volume Width ( $W_{ISV}$ ) =	user	ft												
Depth of Basin Floor $(H_{FLOOR})$ = Length of Basin Floor $(L_{FLOOR})$ =	user	ft ft												
Width of Basin Floor (W <sub>FLOOR</sub> ) =	user	ft												
Area of Basin Floor $(A_{FLOOR}) =$	user	ft <sup>2</sup>												
Volume of Basin Floor (V <sub>FLOOR</sub> ) = Depth of Main Basin (H <sub>MAIN</sub> ) =	user	ft <sup>3</sup>												
Length of Main Basin (L <sub>MAIN</sub> ) =	user	ft												
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft												
Area of Main Basin (A <sub>MAIN</sub> ) =	user	ft <sup>2</sup>												
Volume of Main Basin ( $V_{MAIN}$ ) = Calculated Total Basin Volume ( $V_{total}$ ) =	user user	ft <sup>3</sup> acre-feet												
( utal)														
						-								
						-								
						-								
												-	-	
							1							

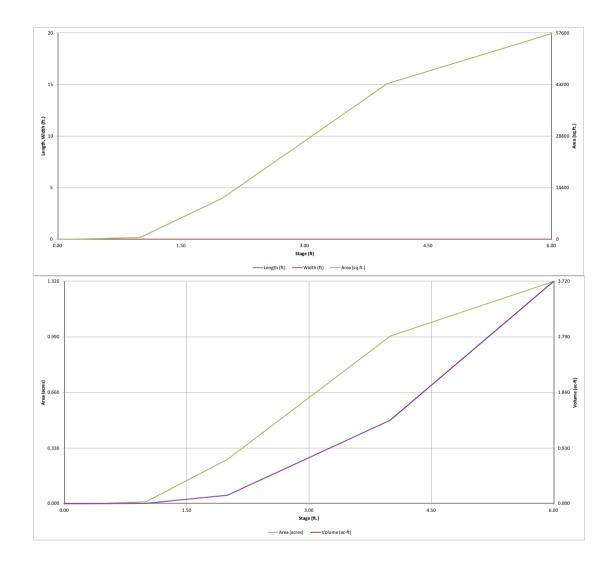
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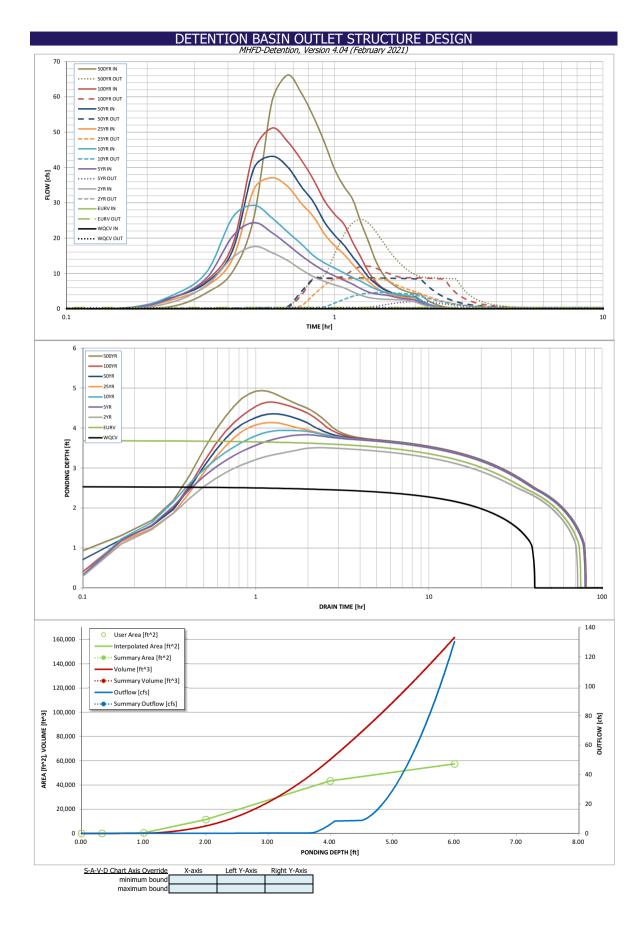
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# DETENTION BASIN STAGE-STORAGE TABLE BUILDER MHFD-Detention, Version 4.04 (February 2021)



DETENTION BASIN OUTLET STRUCTURE DESIGN								
Devised	Falses Touching F		FD-Detention, Vers	sion 4.04 (Februar	ry 2021)			
-	Falcon Trucking Fi FSD Pond 1	lling No. 1						
ZONE 3				Estimated	Estimated			
				Stage (ft)	Volume (ac-ft)	Outlet Type		
100-YR VOLUME EURV WQCV			Zone 1 (WQCV)	2.47	0.303	Orifice Plate	1	
			,				-	
ZONE 1 AND 2	100-YEAR ORIFICE		Zone 2 (EURV)	3.53	0.669	Orifice Plate		
PERMANENT ORIFICES	Configuration (Re	tontion Bond)	Zone 3 (100-year)	4.26	0.684	Weir&Pipe (Restrict)		
•		•		Total (all zones)	1.656			
User Input: Orifice at Underdrain Outlet (typical	y used to drain WQ		_				Calculated Parame	ters for Underdrain
Underdrain Orifice Invert Depth =	:		the filtration media	surface)		drain Orifice Area =		ft <sup>2</sup>
Underdrain Orifice Diameter =	:	inches			Underdrai	n Orifice Centroid =		feet
User Input: Orifice Plate with one or more orific							Calculated Parame	
Invert of Lowest Orifice =	0.00	· ·	bottom at Stage =	,		ice Area per Row =	N/A	ft <sup>2</sup>
Depth at top of Zone using Orifice Plate =			bottom at Stage =	0 ft)		iptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =		inches				ical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	N/A	inches			t	Elliptical Slot Area =	N/A	ft <sup>2</sup>
Here Transfer Charge and Tabel Area of Fach Orific	- Davis (assessible and 6							
User Input: Stage and Total Area of Each Orific	· · · ·	Row 2 (optional)	Row 3 (optional)	Dow 4 (antianal)	Row 5 (optional)	Dow 6 (optional)	Row 7 (optional)	Dow 9 (optional)
Change of Outling Combusid (P)	Row 1 (required)	,		Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft) Orifice Area (sq. inches)		1.18	2.35 4.00					
Offlice Area (sq. flictes)	1.20	1.29	4.00					
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)		Row 10 (optional)	Row II (optional)		Row 15 (optional)	Row 14 (optional)	Row 15 (optional)	Now 10 (optional)
Orifice Area (sq. inches)								
office Area (sq. incles)								
User Input: Vertical Orifice (Circular or Rectang	ular)						Calculated Parame	ters for Vertical Orif
	Not Selected	Not Selected	]				Not Selected	Not Selected
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	= 0 ft) Ve	rtical Orifice Area =	N/A	N/A
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	= 0 ft) Vertica	I Orifice Centroid =	N/A	N/A
Vertical Orifice Diameter =	N/A	N/A	inches					
			-					
User Input: Overflow Weir (Dropbox with Flat o	r Sloped Grate and	Outlet Pipe OR Rec	tangular/Trapezoida	al Weir (and No Out	tlet Pipe)		Calculated Parame	ters for Overflow W
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected
Overflow Weir Front Edge Height, Ho =	3.54	N/A	ft (relative to basin b	oottom at Stage = 0 f		e Upper Edge, $H_t =$	3.54	N/A
Overflow Weir Front Edge Length =	6.50	N/A	feet			/eir Slope Length =	5.00	N/A
Overflow Weir Grate Slope =	0.00	N/A	H:V		rate Open Area / 10		18.75	N/A
Horiz. Length of Weir Sides =	5.00	N/A	feet		verflow Grate Open		22.62	N/A
Overflow Grate Type =	Type C Grate	N/A		(	Overflow Grate Ope	n Area w/ Debris =	11.31	N/A
Debris Clogging % =	50%	N/A	%					
	(C)   0   C   D				6		( 0.11 × 15)	EL D
User Input: Outlet Pipe w/ Flow Restriction Plate			ectangular Orifice)		<u>Ca</u>	alculated Parameter	· · · ·	Flow Restriction Pla
Death to Jacob of Outlet Dise	Zone 3 Restrictor						Zone 3 Restrictor	Not Selected
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below ba	asin bottom at Stage	,	utlet Orifice Area =	1.21	N/A
Outlet Pipe Diameter =		N/A	inches	Half Con		t Orifice Centroid =	0.47	N/A
Restrictor Plate Height Above Pipe Invert =	9.80	1	inches	ndii-Celi	trai Angle of Restric	tor Plate on Pipe =	1.39	N/A
User Input: Emergency Spillway (Rectangular or	Transozoidal)						Calculated Barama	tors for Spillwov
	<u> </u>	ft (rolativo to bacir	n bottom at Stage =	0.00	Spillwov F	ocian Flow Donth-	Calculated Parame 0.71	feet
Spillway Invert Stage= Spillway Crest Length =		feet	- Solitoni at Staye =			esign Flow Depth= Top of Freeboard =	6.21	feet
. , _	24.00 4.00				-		1.32	
Spillway End Slopes = Freeboard above Max Water Surface =		H:V feet				Top of Freeboard = Top of Freeboard =	3.71	acres acre-ft
Treeboard above max water sullate -	1.00	, cou			Dubin volume dl	- op of Freeboard -	5./1	
Routed Hydrograph Results								lumns W through Al
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52

Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52
CUHP Runoff Volume (acre-ft) =	0.303	0.972	0.902	1.270	1.591	2.011	2.356	2.791
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.902	1.270	1.591	2.011	2.356	2.791
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	1.8	5.2	7.9	13.9	17.4	22.2
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A						
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.11	0.31	0.47	0.83	1.04	1.33
Peak Inflow Q (cfs) =	N/A	N/A	15.2	21.7	26.4	34.2	40.1	47.7
Peak Outflow Q (cfs) =	0.2	0.3	0.3	2.3	5.2	11.0	11.5	12.0
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	0.4	0.7	0.8	0.7	0.5
Structure Controlling Flow =	Plate	Plate	Plate	Overflow Weir 1	Overflow Weir 1	Outlet Plate 1	Outlet Plate 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	0.1	0.2	0.5	0.5	0.5
Max Velocity through Grate 2 (fps) =		N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	38	69	67	72	70	68	67	65
Time to Drain 99% of Inflow Volume (hours) =	40	73	71	77	76	75	75	74
Maximum Ponding Depth (ft) =	2.47	3.53	3.38	3.68	3.80	3.98	4.15	4.47
Area at Maximum Ponding Depth (acres) =	0.44	0.82	0.77	0.88	0.92	0.98	1.02	1.07
Maximum Volume Stored (acre-ft) =	0.306	0.973	0.853	1.100	1.199	1.371	1.541	1.875
E							-	



# DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can override the calculated	inflow hydrographs from this workboo	k with inflow hydrographs developed	I in a separate program.

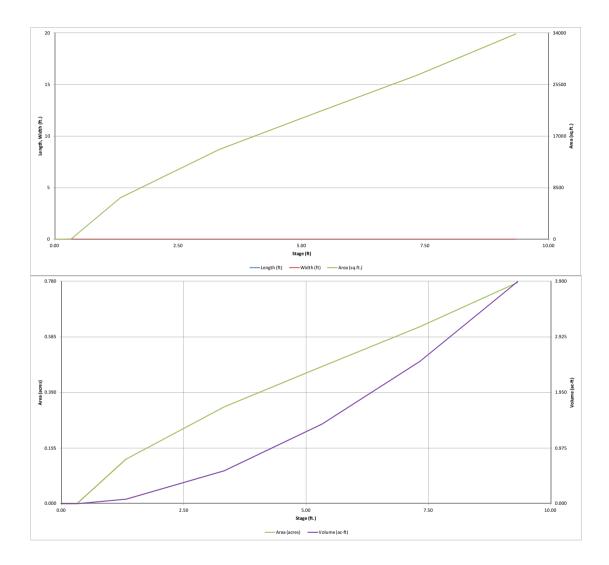
	The user can or	Perride the calcu	lated inflow hyd	rographs from tr	is workdook wit	h inflow hydrogr	apris developed	in a separate pro	gram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3.00 11111	0:05:00									
		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.22	0.02	0.70
	0:15:00	0.00	0.00	1.94	3.16	3.91	2.62	3.25	3.19	4.52
	0:20:00	0.00	0.00	6.71	8.76	10.45	6.45	7.49	8.05	10.53
	0:25:00	0.00	0.00	14.51	20.59	25.90	14.22	16.65	18.22	25.97
	0:30:00	0.00	0.00	17.60	24.40	29.29	33.89	39.82	44.67	58.61
	0:35:00	0.00	0.00	15.86	21.55	25.71	37.10	43.18	51.16	66.18
	0:40:00	0.00	0.00	13.66	18.19	21.76	34.67	40.21	47.37	61.13
		0.00	0.00	11.08	15.08	18.34	29.87	34.64	42.16	54.36
	0:50:00	0.00	0.00	9.04	12.59	15.02	26.06	30.19	36.52	47.01
	0:55:00 1:00:00		0.00	7.67	10.66	12.95	21.09	24.47	30.52	39.41
		0.00	0.00	6.73	9.29	11.47	17.85	20.77	26.70	34.55
	1:05:00	0.00	0.00	5.88	8.06	10.11	15.40	17.96	23.89	30.94
	1:10:00	0.00	0.00	4.76	6.94	8.84 7.77	12.58	14.69	18.87	24.56
	1:15:00 1:20:00	0.00	0.00	3.82	5.71		10.12	11.84	14.62	19.16
		0.00	0.00	3.19	4.75	6.63	7.73	9.03	10.54	13.82
	1:25:00	0.00	0.00	2.86	4.24	5.61	6.14	7.17	7.74	10.18
	1:30:00	0.00	0.00	2.69	3.95	4.94	4.97	5.78	6.03	7.95
	1:35:00	0.00	0.00	2.60	3.76	4.47	4.23	4.90	5.00	6.58
	1:40:00 1:45:00	0.00	0.00	2.55	3.34	4.14	3.74	4.30	4.28	5.61
	1:45:00	0.00	0.00	2.50 2.47	3.03	3.91 3.75	3.42 3.21	3.91 3.64	3.80 3.46	4.98 4.52
	1:55:00				2.81					
	2:00:00	0.00	0.00	2.13	2.64	3.52 3.16	3.06 2.97	3.47	3.24	4.23 4.10
	2:05:00	0.00	0.00	1.87	1.77	2.27	2.97	3.36 2.43	3.15	2.96
	2:10:00	0.00	0.00	0.96	1.77	1.60	1.52	2.43	1.62	2.96
	2:15:00	0.00	0.00	0.90	0.87	1.12	1.07	1.71	1.02	1.49
	2:20:00	0.00	0.00	0.07	0.87	0.77	0.74	0.83	0.79	1.49
	2:25:00	0.00	0.00	0.31	0.39	0.52	0.50	0.56	0.53	0.69
	2:30:00	0.00	0.00	0.20	0.26	0.35	0.34	0.38	0.36	0.47
	2:35:00	0.00	0.00	0.12	0.16	0.33	0.21	0.30	0.23	0.29
	2:40:00	0.00	0.00	0.06	0.09	0.11	0.12	0.13	0.12	0.16
	2:45:00	0.00	0.00	0.00	0.03	0.04	0.05	0.15	0.05	0.07
	2:50:00	0.00	0.00	0.02	0.01	0.01	0.03	0.03	0.03	0.01
	2:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00 4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00 4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00 5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0.00.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

Project: Falcon Trucking Filing No. 1

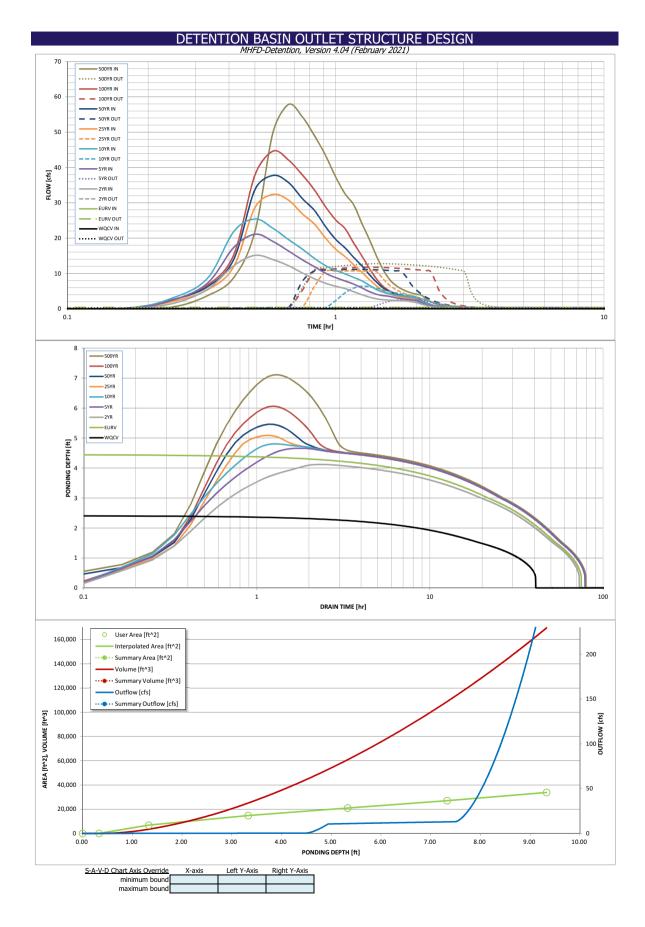
MHFD-Detention, Version 4.04 (February 2021)

$ \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c}$	Volume (ac-ft) 0.000 0.575 1.396 2.497 3.894
$ \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c}$	(ac-ft) 0.000 0.079 0.575 1.396 2.497
Depth Increment =       Depth Increment =       Depth Increment =         Watershed Information       Selected BMP Type =       EDB         Selected BMP Type =       EDB         Watershed Information       5634.67         Watershed Information       564.67         Watershed Length =       1,320         Watershed Imperviousness =       60.0%         600.0%       percent         Percentage Hydrologic Soll Group A =       0.0%         Percentage Hydrologic Soll Group A =       0.0%         Percentage Hydrologic Soll Group A =       0.0%         Location for 1-kr Rainfall Deptrs = User Input	(ac-ft) 0.000 0.079 0.575 1.396 2.497
Parameter         Display Zone Configuration (Retention Pond) Example Zone Configuration (Retention Pond)           Watershed Information         Selected BMP Type = 15.37         EDB         Stage - Storage         Stage - Micropool         -         -         -         -         0         0.00         7           Watershed Length         13.37         acres         6634.57         Ope of Micropool         -         0.00         -         -         -         0         0.00         7           Watershed Length         1.320         ft         6635         -         0.33          -         -         6,840         0.01         7           Watershed Length         1.320         ft         6635         -         1.33          -         -         6,840         0.017         3,446           Watershed Length         1.320         ft         6635         -         1.33           -         14,772         0.339         25,058           Watershed Imperiousness         60.00%         percent         6642         -         7.33           -         27,071         0.620         100,78           Percentage Hydrologic Soli Group A = 10.0%         percent	(ac-ft) 0.000 0.079 0.575 1.396 2.497
Description         Character (http:///////////////////////////////////	(ac-ft) 0.000 0.079 0.575 1.396 2.497
Watershed Information         FOB         FOD	0.000 0.079 0.575 1.396 2.497
Selected BMP Type =       EDB       6635       -       0.33          40       0.001       7         Watershed Length =       15.37       acres       15.37       acres       6635        1.33         6,840       0.157       3,446         Watershed Length =       1,280       ft       6636        3.33         6,840       0.157       3,446         Watershed Length =       1,280       ft       6640        5.33         14,772       0.399       25,058         Watershed Impervousness =       60.0%       percent       6640        5.33          20,969       0.481       160,799         Percentage Hydrologic Soll Group A =       60.0%       percent        7.33          22,017       0.620       108,785         Percentage Hydrologic Soll Group A =       0.0%       percent	0.079 0.575 1.396 2.497
Watershed Area =       15.37       acres       6636       -       1.33         6,840       0.157       3,446         Watershed Length -       1,380       ft       6638       -       3.33         -       44,772       0.399       25,058         Watershed Ingerivousness       60.00%       percent       6640        5.33         -       20,969       0.481       60,799         Watershed Imperivousness       60.00%       percent       6642        7,33         22,969       0.481       60,799         Percentage Hydrologic Soll Group A =       100.0%       percent       6644        9,33          22,017       0.620       108,785         Percentage Hydrologic Soll Group A =       100.0%       percent	0.079 0.575 1.396 2.497
Watershed Length 0 Certroid       1,380       ft       6638       -       3.33       -       -       14,772       0.339       25,058         Watershed Length 10 Certroid       680       ft       6640       -       5.33       -       -       -       20,969       0.481       60,799         Watershed Ingentvourses       60,00%       percent       6642       -       7,33       -       -       -       20,969       0.481       60,799         Watershed Ingentvourses       60,00%       percent       0.0%       percent       6644       -       9,33       -       -       -       -       -       -       -       -       0.0%       percent       0.0%       percent       -       -       -       -       -       -       0.0%       percent       0.0%       percent       -       -       -       -       -       -       -       -       -       -       -       0.0       -       <	0.575 1.396 2.497
Watershed Length to Certroid         6690         n         5.33           20,969         0.481         60,799           Watershed Stope         0.030         ft/ft         6642          7.33           27,070         0.620         168,785           Watershed Inpreviousness         60.00%         percent         6642          7.33           27,070         0.620         168,785           Percentage Hydrologic Soll Group A         0.0%         percent <td>2.497</td>	2.497
Watershed Imperviousess =         60.00%         percent         6644          9.33           33,813         0.776         169,615           Percentage Hydrologic Sol Group & =         0.0%         percent              33,813         0.776         169,615           Percentage Hydrologic Sol Group & E         0.0%         percent <td></td>	
Percentage Hydrologic Soll Group A =       0.0%       percent	3.894
Percentage Hydrologic Soll Groups (2) =       100.0%       percent	
Percentage Hydrologic Soll Groups C/D =       0.0%       percent	
Target WQCV Drain Time       40.0       hours	
After providing required inputs above including 1-hour rainfall depths, click Run CUHP to generate runoff hydrograph Procedure.         Optional User Overrides   <	
After providing request inputs above including 1-hour rainarial depths, click and CJMP to generate rundif Mydorgaphs using the embedded Colorado Urban Hydorgaphs Procedure.	
the embedded cloarado Urban Hydorgaph Procedure.         Optional User Overrides   <	
Water Quality Capture Volume (WQCV) =         0.302         acre-feet         acre-feet   -	
Excess Urban Runoff Volume (FLRV) =     1.000     acre-feet     acre-feet	
5-yr Runoff Volume (P1 = 1.5 in.) =         1.269         acre-feet         1.50         Inches	
10-yr Runoff Volume (P1 = 1.75 in.) = 1.570 arc-feet 1.75 inches	
25-yr Punoff Volume (P1 = 2 in ) = 1.051 acre-feet 2.00 inches	
	$\square$
50-yr Rundf Volume (P1 = 225 in ) = 2.273 a ora-feet 2.25 inches	┝──┤
100-yr Runoff Volume (P1 = 2.52 in.) = 2.669 acre-feet 2.52 inches	┣───┦
Subsystation volume (r) = 5.491         actretet         incres               Approximate 2vp Determinate 2vp D	┢──┤
Approximate Syn Declaradin Volume 1.038 acrefect	
Approximate 10-yr Detention Volume = 1.338 acre-feet	
Approximate 25-yr Detention Volume = 1.447 acre-feet	
Approximate 50-yr Detention Volume = 1.509 acre-feet	
Approximate 100-yr Detention Volume = 1.647 acre-feet	
Define Zones and Basin Geometry	
Zone zvolume (vrocu) – 0.592 acrefect – – – – – – – – – – – – – – – – – – –	
Zone 3 Volume (100-year - Zones 1 & 2) = 0.647 acre-feet	
Total Detention Basin Volume = 1.647 acre-feet	
Initial Surcharge Volume (ISV) = user ft <sup>3</sup>	
Initial Surcharge Depth (ISD) = user ft	
Total Available Detention Depth (H <sub>lobal</sub> ) = user ft	
Depth of Trickle Channel ( $H_{TC}$ ) = user It	
Slope of Trickle Channel ( $S_{TC}$ ) = user ft/ft Slope of Trickle Channel ( $S_{TC}$ ) = user ft/ft	
Slopes of Main Basin Sides (S <sub>main</sub> ) =         user         H:V </td <td></td>	
Initial Surcharge Area (A <sub>ISV</sub> ) = user ft <sup>2</sup>	
Surcharge Volume Length (Lisv) = user ft tr	
Surcharge Volume Width (W <sub>EV</sub> ) = user ft	
Depth of Basin Floor (H <sub>FLOOR</sub> ) = user ft	
Length of Basin Floor (L <sub>ELOOR</sub> )         user         ft	
Width of Basin Floor (WFLOOR)         user         ft	
Volume of Basin Floro (Vrucos) = user It <sup>2</sup>	
Depth of Main Basin (H <sub>MAR</sub> ) = user ft	
Length of Main Basin (LMAR) = user ft	
Width of Main Basin (W <sub>MAR</sub> )         user         ft	
Area of Main Basin (Ayan) = user tt -	$\parallel$
Volume of Main Basin (V <sub>MUN</sub> )         user         ft <sup>3</sup>	┣──┤
Calculated Total Basin Volume (V <sub>total</sub> ) = user acre-feet	┣───┦
	$\square$
	┣───┦
interface     interface     interface     interface     interface       interface     interface     interface     interface     interface       interface     interface     interface     interface     interface	
n     n     n     n     n     n       1     1     1     1     1     1       1     1     1     1     1     1       1     1     1     1     1     1       1     1     1     1     1     1	
iii       iiii       iii       iiii       iii       iii       iii       iii       iiii       iiii       iiii       iiii       iiii       iiii       iiii       iiii       iiii       iiiiii       iiiiiii       iiiiii       iiiiiiii       iiiiiiiiii       iiiiiiiiiiiiiii       iiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiii	
in     in     in     in     in     in	
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	
n $n$	
n $n$	



### DETENTION BASIN OUTLET STRUCTURE DESIGN

Project:	Falcon Trucking Fi		FD-Detention, Vers	sion 4.04 (Februar	y 2021)			
	FSD Pond 2							
ZONE 3				Estimated	Estimated			
				Stage (ft)	Volume (ac-ft)	Outlet Type	_	
			Zone 1 (WQCV)	2.42	0.302	Orifice Plate		
	100-YEAR ORIFICE		Zone 2 (EURV)	4.46	0.698	Orifice Plate		
PERMANENT ORIFICES			Zone 3 (100-year)	5.84	0.647	Weir&Pipe (Restrict)		
POOL Example Zone	Configuration (Re	tention Pond)		Total (all zones)	1.647		1	
User Input: Orifice at Underdrain Outlet (typically	v used to drain WQ	CV in a Filtration BN	1P)	· · · ·		1	Calculated Parame	ters for Underdrain
Underdrain Orifice Invert Depth =	N/A	ft (distance below	the filtration media	surface)	Underc	drain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Diameter =	N/A	inches			Underdrair	Orifice Centroid =	N/A	feet
		-						
User Input: Orifice Plate with one or more orific	es or Elliptical Slot				mentation BMP)		Calculated Parame	
Invert of Lowest Orifice =	0.00	•	bottom at Stage =	,	-	ice Area per Row =	N/A	ft <sup>2</sup>
Depth at top of Zone using Orifice Plate =	4.46		bottom at Stage =	0 ft)		ptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	17.80	inches				ical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	N/A	inches			E	Iliptical Slot Area =	N/A	ft²
User Input: Stage and Total Area of Each Orifice	Dow (numbered f	rom lowort to high	vct)					
User Input. Stage and Total Area of Each Office	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)		1.49	2.97				(optional)	
Orifice Area (sq. inches)		1.49	3.50					
	1.70	1.70	5.50					
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)		Tow To (optional)	Now II (optional)	Row 12 (optional)	Kow 15 (optional)	now in (optional)	Tow 15 (optional)	now to (optional)
Orifice Area (sq. inches)								
						1	1	1
User Input: Vertical Orifice (Circular or Rectangu	<u>ılar)</u>						Calculated Parame	ters for Vertical Orif
	Not Selected	Not Selected					Not Selected	Not Selected
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	0 ft) Ver	tical Orifice Area =	N/A	N/A
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	0 ft) Vertica	I Orifice Centroid =	N/A	N/A
Vertical Orifice Diameter =	N/A	N/A	inches					
User Input: Overflow Weir (Dropbox with Flat or			tangular/Trapezoida 1	I Weir (and No Out	let Pipe)			ters for Overflow W
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected
Overflow Weir Front Edge Height, Ho =	4.50	N/A	-	ottom at Stage = 0 f	, -	e Upper Edge, $H_t =$	4.50	N/A
Overflow Weir Front Edge Length =	8.00	N/A	feet			/eir Slope Length =	2.91	N/A
Overflow Weir Grate Slope =	0.00	N/A	H:V		rate Open Area / 10		16.07	N/A
Horiz. Length of Weir Sides =	2.91	N/A	feet		verflow Grate Open		16.20	N/A
Overflow Grate Type = Debris Clogging % =	Type C Grate 50%	N/A N/A	%	(	Overflow Grate Ope	n Area w/ Debris =	8.10	N/A
Debris clogging % -	50%	N/A	70					
User Input: Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice R	estrictor Plate or R	ectangular Orifice)		Ca	lculated Parameter	s for Outlet Pine w/	Flow Restriction Pla
oser input. Outer tipe wy now restriction nate	Zone 3 Restrictor	Not Selected			<u></u>		Zone 3 Restrictor	Not Selected
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below ba	sin bottom at Stage :	= 0 ft) O	utlet Orifice Area =	1.01	N/A
Outlet Pipe Diameter =	18.00	N/A	inches	· · · · · · · · · · · · · · · · · · ·	-	t Orifice Centroid =	0.48	N/A
Restrictor Plate Height Above Pipe Invert =	10.00	,	inches	Half-Cent	ral Angle of Restric		1.68	N/A
		1					•	
User Input: Emergency Spillway (Rectangular or	<u>Trapezoidal)</u>						Calculated Parame	ters for Spillway
Spillway Invert Stage=	6.07	ft (relative to basir	bottom at Stage =	0 ft)	Spillway D	esign Flow Depth=	0.60	feet
Spillway Crest Length =	30.00	feet			Stage at 7	Fop of Freeboard =	7.67	feet
Spillway End Slopes =	4.00	H:V			Basin Area at 7	Fop of Freeboard =	0.65	acres
Freeboard above Max Water Surface =	1.00	feet			Basin Volume at 1	Fop of Freeboard =	2.71	acre-ft
Routed Hydrograph Results	The user can over	ride the default CLI	- D hydrographs and	runoff volumes by	entering new value	as in the Inflow Hvo	Irographs table (Co	lumns W through Ai
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52
CUHP Runoff Volume (acre-ft) =	0.302	1.000	0.919	1.269	1.570	1.951	2.273	2.669
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.919	1.269	1.570	1.951	2.273	2.669
CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A N/A	N/A N/A	1.6	4.4	6.7	12.0	15.0	19.2
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.10	0.29	0.43	0.78	0.98	1.25
Peak Inflow Q (cfs) =	N/A	N/A	15.1	21.1	25.4	32.4	37.7	44.6
Peak Outflow Q (cfs) =	0.1	0.4	0.3	2.6	6.4	10.7	11.1	11.7
Ratio Peak Outflow to Predevelopment Q =	N/A Plate	N/A Plate	N/A Plate	0.6 Overflow Weir 1	1.0 Overflow Weir 1	0.9 Outlet Plate 1	0.7 Outlet Plate 1	0.6 Outlet Plate 1
Structure Controlling Flow = Max Velocity through Grate 1 (fps) =	Plate N/A	Plate N/A	Plate N/A	Overflow Weir 1 0.1	Overflow Weir 1 0.4	Outlet Plate 1 0.6	Outlet Plate 1 0.7	Outlet Plate 1 0.7
Max Velocity through Grate 2 (fps) =	N/A	N/A N/A	N/A N/A	N/A	N/A	N/A	N/A	0.7 N/A
Time to Drain 97% of Inflow Volume (hours) =	38	68	66	70	68	66	64	62
Time to Drain 99% of Inflow Volume (hours) =	40	72	70	75	75	74	73	73
Maximum Ponding Depth (ft) = Area at Maximum Ponding Depth (acres) =	2.42 0.26	4.46 0.42	4.12 0.40	4.66 0.43	4.81 0.44	5.09 0.46	5.46 0.49	6.06 0.53
Maximum Volume Stored (acre-ft) =	0.304	1.004	0.865	1.085	1.151	1.282	1.459	1.766



# DETENTION BASIN OUTLET STRUCTURE DESIGN Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

The user can ov	verride the calcu	lated inflow hyd	rographs from th	nis workbook wit	h inflow hydrogr	aphs developed	in a separate pro	gram.

	The user can ov	verride the calcu	lated inflow hyd	rographs from th	nis workbook wit	h inflow hydrogi	aphs developed	in a separate pro	gram.	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.18	0.00	0.58
	0:15:00	0.00	0.00	1.58	2.59	3.20	2.15	2.67	2.62	3.73
	0:20:00	0.00	0.00	5.57	7.30	8.71	5.39	6.27	6.72	8.81
	0:25:00	0.00	0.00	12.18	17.33	21.84	11.94	14.00	15.33	21.91
	0:30:00	0.00	0.00	15.12	21.08	25.41	28.71	33.78	37.91	49.92
	0:35:00	0.00	0.00	13.92	19.03	22.78	32.37	37.75	44.63	57.88
	0:40:00	0.00	0.00	12.20	16.35	19.59	30.76	35.72	42.10	54.41
	0:45:00	0.00	0.00	10.16	13.87	16.89	26.91	31.24	37.93	49.01
	0:50:00	0.00	0.00	8.48	11.87	14.24	23.97	27.82	33.60	43.39
	0:55:00	0.00	0.00	7.20	10.03	12.17	19.99	23.23	28.83	37.27
	1:00:00	0.00	0.00	6.35	8.79	10.87	16.85	19.63	25.12	32.56
	1:05:00	0.00	0.00	5.70	7.85	9.84	14.75	17.22	22.68	29.44
	1:10:00	0.00	0.00	4.81	6.97	8.85	12.44	14.54	18.60	24.26
	1:15:00	0.00	0.00	4.00	5.91	7.91	10.40	12.18	15.03	19.72
	1:20:00	0.00	0.00	3.30	4.86	6.64	8.29	9.69	11.47	15.02
	1:25:00	0.00	0.00	2.81	4.12	5.42	6.52	7.61	8.51	11.13
	1:30:00	0.00	0.00	2.54	3.72	4.69	5.07	5.90	6.39	8.39
	1:35:00	0.00	0.00	2.42	3.51	4.23	4.20	4.87	5.12	6.74
	1:40:00 1:45:00	0.00	0.00	2.35	3.13	3.90	3.65	4.21	4.33	5.69
	1:45:00	0.00	0.00	2.31 2.27	2.84	3.67 3.50	3.29 3.05	3.77 3.48	3.78 3.40	4.96 4.45
	1:55:00	0.00	0.00	1.98	2.63	3.30	2.88	3.48	3.13	4.45
	2:00:00	0.00	0.00	1.96	2.47	2.97	2.88	3.14	2.95	3.85
	2:05:00	0.00	0.00	1.74	1.71	2.97	2.07	2.34	2.95	2.85
	2:10:00	0.00	0.00	0.96	1.24	1.59	1.50	1.69	1.59	2.05
	2:15:00	0.00	0.00	0.70	0.90	1.15	1.09	1.22	1.16	1.50
	2:20:00	0.00	0.00	0.50	0.64	0.82	0.78	0.88	0.84	1.09
	2:25:00	0.00	0.00	0.35	0.45	0.58	0.55	0.62	0.59	0.77
	2:30:00	0.00	0.00	0.24	0.30	0.40	0.39	0.43	0.41	0.54
	2:35:00	0.00	0.00	0.16	0.21	0.28	0.27	0.30	0.29	0.37
	2:40:00	0.00	0.00	0.10	0.13	0.17	0.17	0.19	0.18	0.24
	2:45:00	0.00	0.00	0.05	0.07	0.09	0.10	0.11	0.10	0.13
	2:50:00	0.00	0.00	0.02	0.03	0.04	0.04	0.05	0.05	0.06
	2:55:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01
	3:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:15:00 3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00 4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:45:00 4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00 5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00 5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00			0.00	0.00	0.00	0.00	0.00	0.00

# Final Drainage Report Falcon Trucking Filing No.1 (Pond Volume Calculation)

## FSD POND 1

			Storage			
_	Elevation	SF	CF	AF	Sum	
6630	0.00	0.00			0	
6630.33	0.33	40.00	6.60	0.00	0.00	
6631	1.00	500.00	180.90	0.00	0.00	
6632	2.00	11,458.00	5,979.00	0.14	0.14	
6634	4.00	43,369.00	54,827.00	1.26	1.40	
6636	6.00	57,403.00	100,772.00	2.31	3.71	
	Pro	ovided Total =	$\frac{161,766}{\text{Total}} =$	CF <u>3.7</u> 4	Ac-ft	
	t Elevation 1.5, the	-				
А	At Elevation 3.5, the	Storage is 1.09 A	c-ft.			

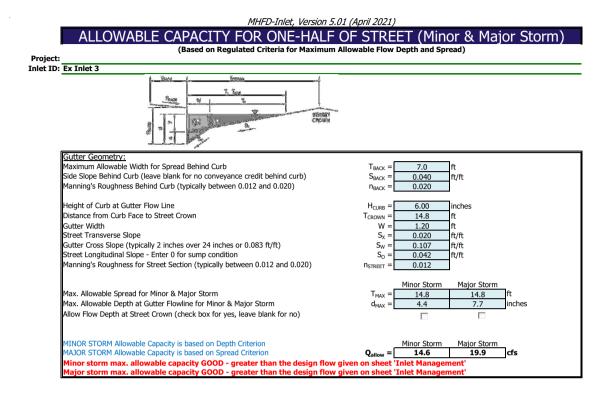
Calculated by: GT Date: 10/7/2019 Checked by:

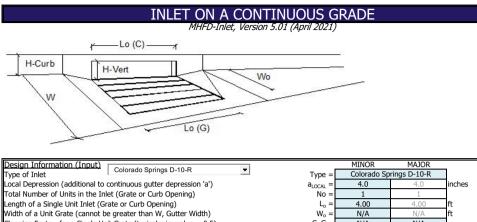
# Final Drainage Report Falcon Trucking Filing No.1 (Pond Volume Calculation)

## FSD POND 2

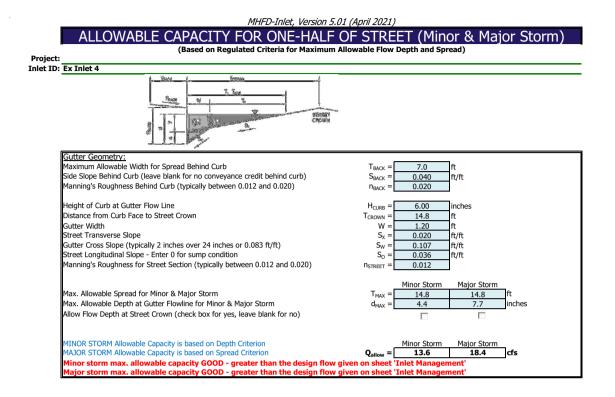
				Stora	age
	Elevation	SF	CF	AF	Sum
6634.67	0.00	0.00			0
6635	0.33	40.00	6.60	0.00	0.00
6636	1.33	6,840.00	3,440.00	0.08	0.08
6638	3.33	14,772.00	21,612.00	0.50	0.58
6640	5.33	20,696.00	35,468.00	0.81	1.39
6642	7.33	27,017.00	47,713.00	1.10	2.48
6644	9.33	33,813.00	60,830.00	1.40	3.88
		Total =	<u>169,070</u> C Total =		Ac-ft
	t Elevation 3, the St t Elevation 4, the St	-			

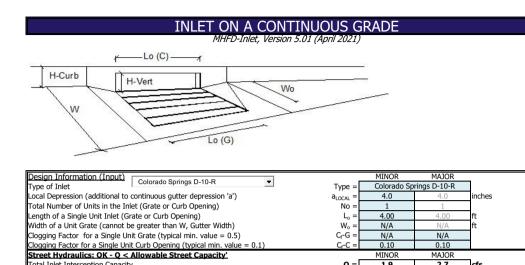
Calculated by:	DLM
Date:	6/21/2016
Checked by:	





Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}-G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	2.3	3.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	2.8	12.7	cfs
Capture Percentage = $0/0$ =	C0/a -	46	22	9/6





MINOR

1.9

1.2

61

Q =

Q<sub>b</sub> = <u>C% =</u>

MAJOR

2.7

4.8

36

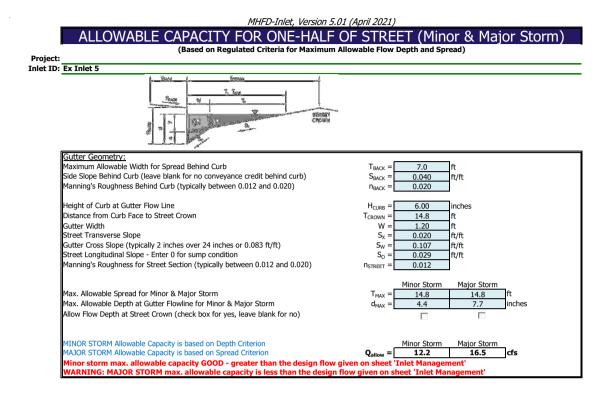
cfs

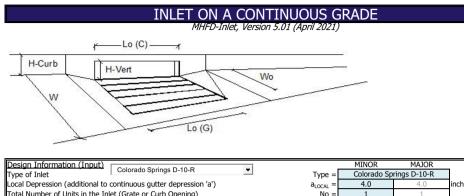
cfs

%

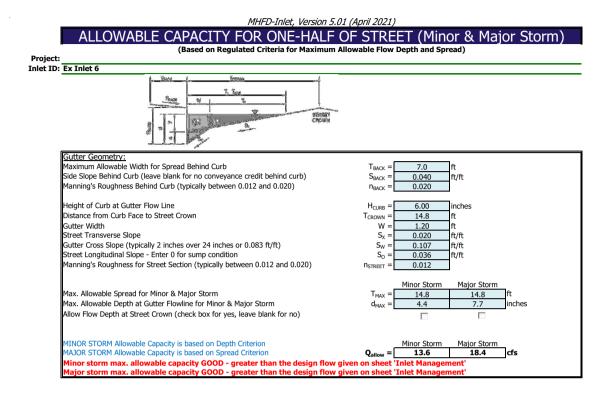
Total Inlet Interception Capacity Total Inlet Carry-Over Flow (flow bypassing inlet)

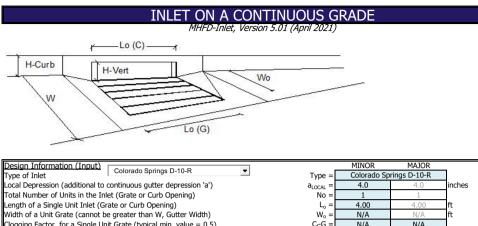
Capture Percentage =  $Q_a/Q_o =$ 



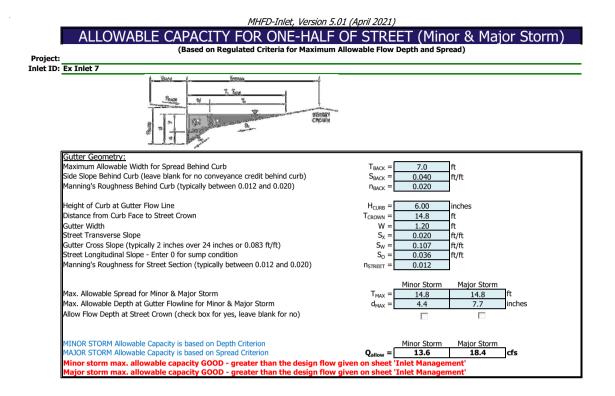


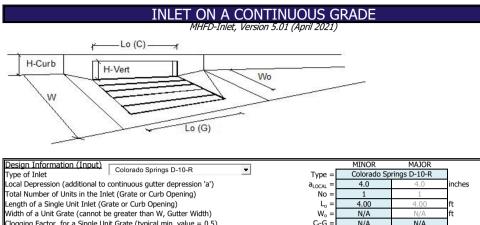
Colorado Springs D-10-R		MINOR	MAJOR	
Type of Inlet	Type =	Colorado Sp	rings D-10-R	
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	4.0	4.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_o =$	4.00	4.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}-G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MAJOR STORM		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.2	3.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	<b>Q</b> <sub>b</sub> =	2.4	13.7	cfs
Capture Percentage = $Q_a/Q_a$ =	C% =	48	21	%



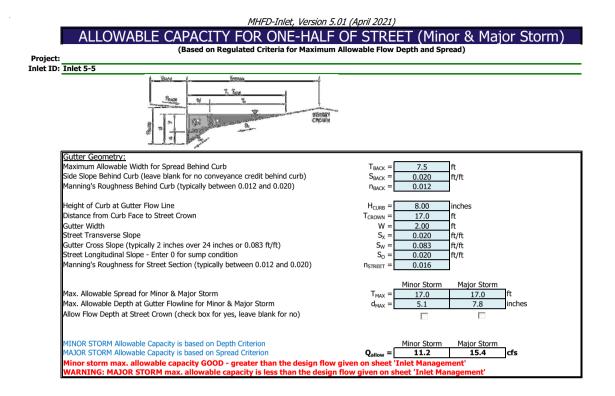


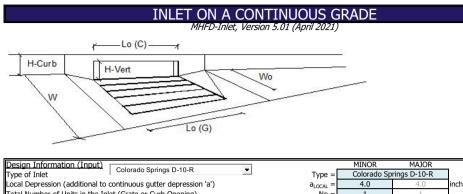
Total Number of Units in the Inlet (Grate of Curb Opening)	NO =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	4.00	4.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}-G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.1	1.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.1	1.2	cfs
Capture Percentage = $Q_a/Q_o$ =	C% =	93	61	%



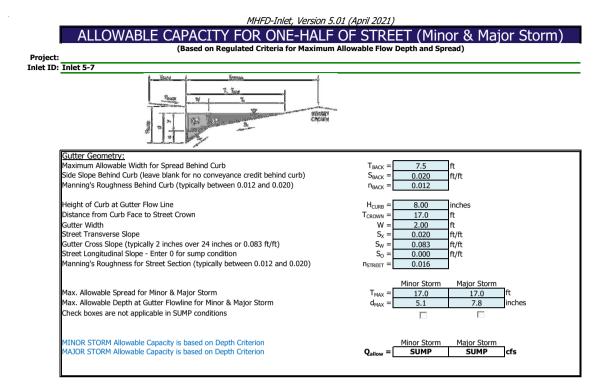


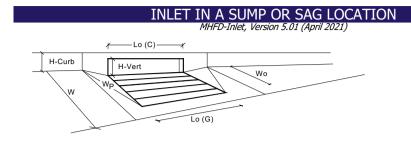
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	4.00	4.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}-G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.7	2.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.9	5.5	cfs



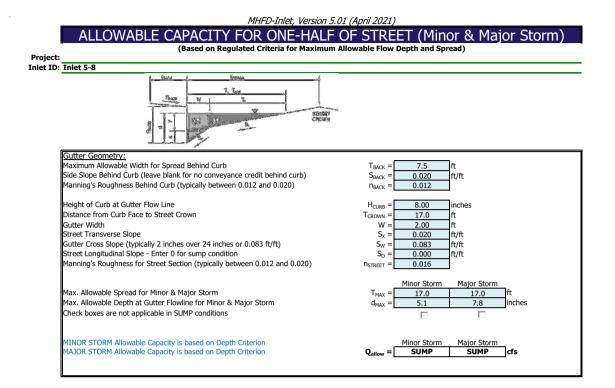


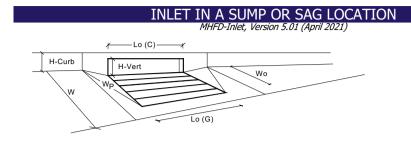
Local Depression (additional to continuous gutter depression 'a')	a <sub>LOCAL</sub> =	4.0	4.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L <sub>o</sub> =	16.00	16.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	$C_{f}-G =$	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10	
Street Hydraulics: WARNING: Q > ALLOWABLE Q FOR MAJOR STORM		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.7	14.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	3.6	cfs
Capture Percentage = $Q_a/Q_a$ =	C% =	100	80	%



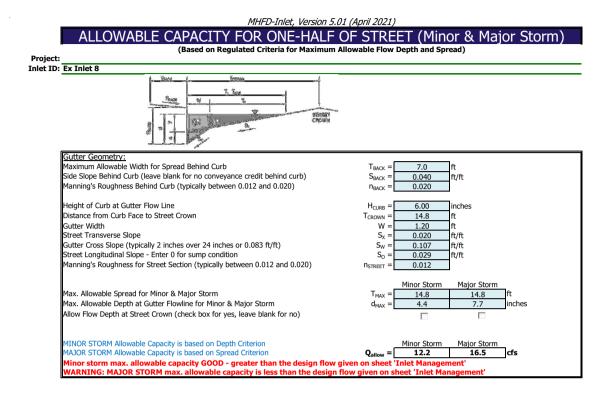


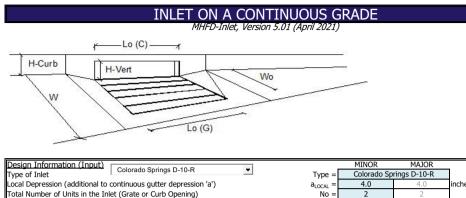
Colorado Springs D-10-R	_	MINOR	MAJOR	
Type of Inlet	Type =	Colorado Sp	rings D-10-R	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	4.00	4.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.7	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_{w}$ (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	4.00	4.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	8.00	8.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	8.00	8.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	81.00	81.00	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.72	1.00	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
		MINOD	MAIOD	
Total Inlat Interception Canacity (accumes closed condition)	<b>0</b> <sub>2</sub> =	MINOR 3.2	MAJOR 7.9	cfs
Total Inlet Interception Capacity (assumes clogged condition)	$Q_a = Q_{PEAK REQUIRED} =$	1.8	4.0	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	✓ PEAK REQUIRED —	1.0	U.F	C13





Design Information (Input)	_	MINOR	MAJOR	
lype of Inlet	Type =	Colorado Sp	rings D-10-R	
Local Depression (additional to continuous gutter depression 'a' from above)	a <sub>local</sub> =	4.00	4.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.1	7.7	inches
Grate Information	_	MINOR	MAJOR	Override Depths
Length of a Unit Grate	$L_{o}(G) =$	N/A	N/A	feet
Width of a Unit Grate	W <sub>o</sub> =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A <sub>ratio</sub> =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	$C_{f}(G) =$	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	$C_w$ (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	$C_{0}(G) =$	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	$L_{o}(C) =$	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H <sub>vert</sub> =	8.00	8.00	inches
Height of Curb Orifice Throat in Inches	H <sub>throat</sub> =	8.00	8.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	81.00	81.00	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W <sub>p</sub> =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	$C_w(C) =$	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	$C_{o}(C) =$	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d <sub>Grate</sub> =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d <sub>Curb</sub> =	0.26	0.48	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF <sub>Combination</sub> =	0.48	0.73	
Curb Opening Performance Reduction Factor for Long Inlets	RF <sub>Curb</sub> =	0.88	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF <sub>Grate</sub> =	N/A	N/A	
		MINOD	MAJOD	
Tatal Jalat Jatawashing Consults (converse alassed condition)	o - [	MINOR	MAJOR 15.1	cfs
Total Inlet Interception Capacity (assumes clogged condition)	<b>Q</b> <sub>a</sub> =	<b>5.3</b> 4.7	10.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	$Q_{PEAK REQUIRED} =$	4./	10.4	us





Type of Inlet	Colorado Springs D-10-R	Type =	Colorado Sp	rings D-10-R					
	al Depression (additional to continuous gutter depression 'a') aLCCAL = 4.0 4.0								
Total Number of Units in the In	let (Grate or Curb Opening)	No =	2	2					
Length of a Single Unit Inlet (G	rate or Curb Opening)	L <sub>o</sub> =	4.00	4.00	ft				
Width of a Unit Grate (cannot b	e greater than W, Gutter Width)	W <sub>o</sub> =	N/A	N/A	ft				
Clogging Factor for a Single Ur	it Grate (typical min. value = 0.5)	$C_{f}-G =$	N/A	N/A					
Clogging Factor for a Single Un	t Curb Opening (typical min. value = 0.1)	$C_{f}-C =$	0.10	0.10					
Street Hydraulics: WARNIN	<u>G: Q &gt; ALLOWABLE Q FOR MAJOR STORM</u>		MINOR	MAJOR					
Total Inlet Interception Capacit	y .	Q =	3.8	8.7	cfs				
Total Inlet Carry-Over Flow (flo	w bypassing inlet)	$Q_b =$	0.5	15.1	cfs				
Capture Percentage = $Q_a/Q_o$ =		C% =	89	36	%				

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Falcon Trucking/Enclaves Filing No. 5									
Drainage Report Drainage Plan									
Water Quality Control Volu		/orksheet							
Ex Pond A (303)	0								
CONTRUBUTING			CORRESPONDING						
BASINS	AC	C100	<b>IMPERVIOUS %</b>						
P~	0.41	0.37	3						
Q~	0.36	0.62	70						
Q2~	0.08	0.62	70						
R~	0.40	0.56	57						
R2~	0.22	0.56	57						
S~	0.11	0.96	100						
S2~	0.08	0.96	100						
T~	0.33	0.56	57						
OS6#	1.00	0.39	7						
A1#	1.40	0.36	2						
A2#	2.00	0.57	59						
A3#	0.40	0.57	59						
A4#	2.00	0.53	48						
A5#	1.30	0.57	59						
A6#	0.80	0.57	59						
A7#	0.70	0.57	59						
A8#	0.20	0.57	59						
A9#	1.10	0.57	59						
A12#	0.20	0.57	59						
A13#	0.40	0.57	59						
A7*	1.23	0.59	65						
A8*	0.93	0.59	65						
A9*	0.82	0.59	65						
B*	2.05	0.42	15						
			from COS DCM						
			Table 6-6						
COMBINED ACREAGE	18.52								
COMB. % IMPERVIOUS			53.3%						

~ Falcon Trucking Fil 1

# Enclaves at Mountain Vista Fil 6

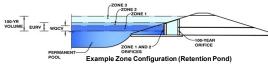
\* Enclaves at Mountain Vista Fil 5

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)

Project: Falcon Trucking

#### Basin ID: EX Pond 303 w/proposed Falcon Trucking drainage basins (revised acreage and imperviousness) and existing outlet structure height.



#### Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	18.52	acres
Watershed Length =	1,750	ft
Watershed Length to Centroid =	925	ft
Watershed Slope =	0.031	ft/ft
Watershed Imperviousness =	53.30%	percent
Percentage Hydrologic Soil Group A =	100.0%	percent
Percentage Hydrologic Soil Group B =	0.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

## After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

Water Quality Capture Volume (WQCV) =	0.333	acre-feet
Excess Urban Runoff Volume (EURV) =	1.159	acre-feet
2-yr Runoff Volume (P1 = 1.19 in.) =	0.865	acre-feet
5-yr Runoff Volume (P1 = 1.5 in.) =	1.145	acre-feet
10-yr Runoff Volume (P1 = 1.75 in.) =	1.370	acre-feet
25-yr Runoff Volume (P1 = 2 in.) =	1.709	acre-feet
50-yr Runoff Volume (P1 = 2.25 in.) =	2.040	acre-feet
100-yr Runoff Volume (P1 = 2.52 in.) =	2.456	acre-feet
500-yr Runoff Volume (P1 = 3.14 in.) =	3.359	acre-feet
Approximate 2-yr Detention Volume =	0.747	acre-feet
Approximate 5-yr Detention Volume =	0.982	acre-feet
Approximate 10-yr Detention Volume =	1.195	acre-feet
Approximate 25-yr Detention Volume =	1.456	acre-feet
Approximate 50-yr Detention Volume =	1.619	acre-feet
Approximate 100-yr Detention Volume =	1.811	acre-feet

#### Define Zones and Basin Geometry

ine zones and basin Geometry		
Zone 1 Volume (WQCV) =	0.333	acre-feet
Zone 2 Volume (EURV - Zone 1) =	0.826	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	0.652	acre-feet
Total Detention Basin Volume =	1.811	acre-feet
Initial Surcharge Volume (ISV) =	user	ft <sup>3</sup>
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth $(H_{total}) =$	user	ft
Depth of Trickle Channel $(H_{TC}) =$	user	ft
Slope of Trickle Channel (S <sub>TC</sub> ) =	user	ft/ft
Slopes of Main Basin Sides (S <sub>main</sub> ) =	user	H:V
Basin Length-to-Width Ratio $(R_{L/W}) =$	user	
Initial Surcharge Area $(A_{ISV}) =$	user	ft <sup>2</sup>
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width $(W_{ISV}) =$	user	ft
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor $(W_{FLOOR}) =$	user	ft
Area of Basin Floor $(A_{FLOOR}) =$	user	ft <sup>2</sup>
Volume of Basin Floor ( $V_{FLOOR}$ ) =	user	ft <sup>3</sup>
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin ( $W_{MAIN}$ ) =	user	ft
Area of Main Basin $(A_{MAIN}) =$	user	ft <sup>2</sup>
Volume of Main Basin ( $V_{MAIN}$ ) =	user	ft <sup>3</sup>
Calculated Total Basin Volume ( $V_{total}$ ) =	user	acre-feet

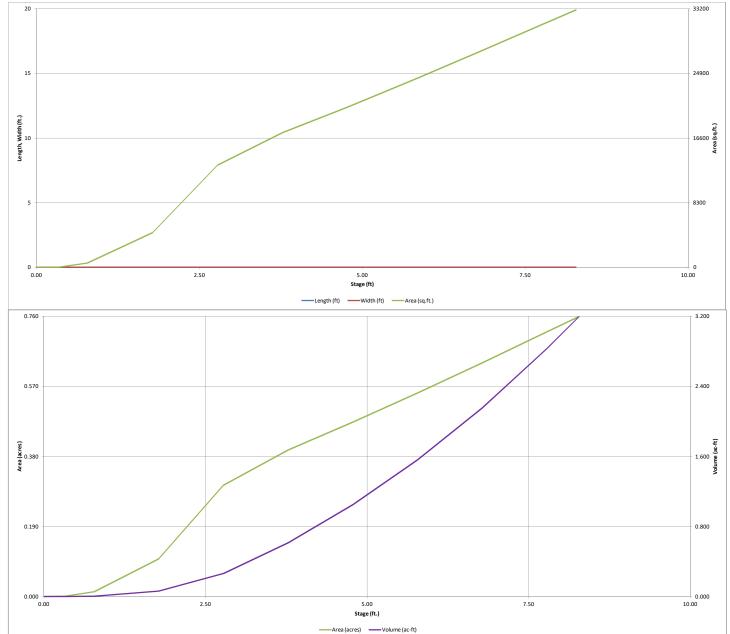
EA	R		Depth Increment =		ft							
	Pond)		Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
			Description	(ft)	Stage (ft)	(ft)	(ft)	(ft <sup>2</sup> )	Area (ft <sup>2</sup> )	(acre)	(ft 3)	(ac-ft)
		6618.22	Top of Micropool		0.00				0	0.000		
					0.33				32	0.001	5	0.000
					0.78				557	0.013	138	0.003
					1.78	-			4,458	0.102	2,645	0.061
					2.78				13,151	0.302	11,450	0.263
					3.78				17,337	0.398	26,694	0.613
					4.78				20,620	0.473	45,672	1.048
					5.78				24,045	0.552	68,005	1.561
					6.78				27,624	0.634	93,839	2.154
					7.78				31,256	0.718	123,279	2.830
					8.28				33,072	0.759	139,361	3.199
						-	-					
	Optional User	Overrides				-	-					
		acre-feet										
		acre-feet					-					
	1.19	inches										
	1.50	inches										
	1.75	inches										
	2.00	inches										
	2.25	inches										
	2.52	inches										
	2.52											
		inches										
						-	-					
						-						
						-						
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...

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

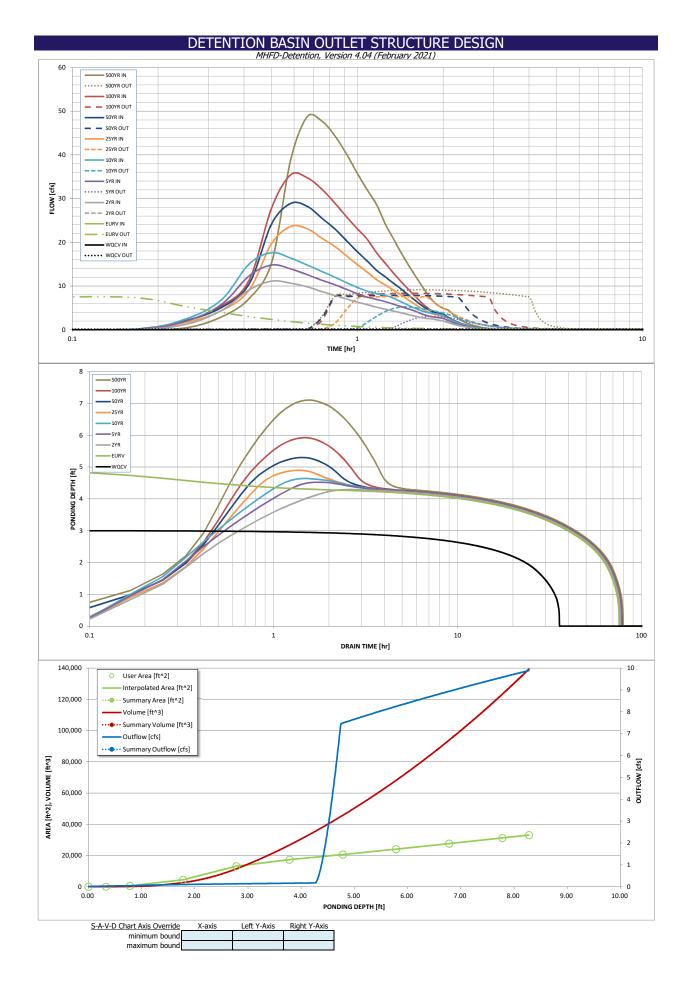
MHFD-Detention, Version 4.04 (February 2021)



## DETENTION BASIN OUTLET STRUCTURE DESIGN

Project:	Falcon Trucking	וחוייו	FD-Delenlion, ver	SION 4.04 (Februar	ry 2021)			
Basin ID:	EX Pond 303 w/pr	oposed Falcon True	cking drainage bas	ins (revised acreag	e and imperviousn	ess) and existing o	utlet structure heig	jht.
ZONE 3 ZONE 2 ZONE 2				Estimated	Estimated			
100-YR				Stage (ft)	Volume (ac-ft)	Outlet Type	-	
			Zone 1 (WQCV)	3.01	0.333	Orifice Plate		
ZONE 1 AND 2	100-YEAR ORIFICE		Zone 2 (EURV)	5.01	0.826	Orifice Plate		
PERMANENT ORIFICES	Configuration (Do	tention Dand)	Zone 3 (100-year)	6.22	0.652	Weir&Pipe (Restrict)		
•	Configuration (Re			Total (all zones)	1.811			
User Input: Orifice at Underdrain Outlet (typically	-			<i>c</i>				ters for Underdrain
Underdrain Orifice Invert Depth = Underdrain Orifice Diameter =	N/A N/A	inches	the filtration media	surface)		drain Orifice Area = n Orifice Centroid =		ft <sup>2</sup> feet
	N/A	inches			Underdrai		N/A	leet
User Input: Orifice Plate with one or more orifice	es or Elliptical Slot \	Neir (typically used	to drain WQCV and	d/or EURV in a sedii	mentation BMP)		Calculated Paramet	ters for Plate
Invert of Lowest Orifice =	0.00	ft (relative to basin	n bottom at Stage =	= 0 ft)	WQ Orit	ice Area per Row =	N/A	ft <sup>2</sup>
Depth at top of Zone using Orifice Plate =	4.27	ft (relative to basir	n bottom at Stage =	= 0 ft)		iptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	N/A	inches				tical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	N/A	inches			1	Elliptical Slot Area =	N/A	ft <sup>2</sup>
User Input: Stage and Total Area of Each Orifice	e Row (numbered fi	rom lowest to highe	est)					
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.92	3.60					
Orifice Area (sq. inches)	1.63	0.94	0.12					
	David ( 11 11	D 10 (	David La Carta a D	David 2 ( attach	Day 12 ( 111 - 11	David 4 ( 11 11 11	David E (contraction	Den 16 (
Stage of Orifice Centroid (ft)	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Orifice Area (sq. inches)								
User Input: Vertical Orifice (Circular or Rectangu	<u>ılar)</u>		-				Calculated Paramet	ters for Vertical Orif
	Not Selected	Not Selected					Not Selected	Not Selected
Invert of Vertical Orifice =	N/A	N/A		n bottom at Stage =		rtical Orifice Area =	N/A	N/A
Depth at top of Zone using Vertical Orifice = Vertical Orifice Diameter =	N/A N/A	N/A N/A	rt (relative to basil inches	n bottom at Stage =	= 0 ft) Vertica	al Orifice Centroid =	N/A	N/A
	N/A	N/A	inches					
User Input: Overflow Weir (Dropbox with Flat or	Sloped Grate and	Outlet Pipe OR Rec	tangular/Trapezoid	al Weir (and No Out	tlet Pipe)		Calculated Parame	ters for Overflow W
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected
Overflow Weir Front Edge Height, Ho =	4.27	N/A		bottom at Stage = 0 f	-	e Upper Edge, H <sub>t</sub> =		N/A
Overflow Weir Front Edge Length =	4.00	N/A N/A	feet H:V	6		Veir Slope Length =	2.91	N/A N/A
Overflow Weir Grate Slope = Horiz. Length of Weir Sides =	0.00 2.91	N/A	feet			00-yr Orifice Area = Area w/o Debris =	11.30 8.10	N/A N/A
Overflow Grate Type =	Type C Grate	N/A			•	en Area w/ Debris =	4.05	N/A
Debris Clogging % =	50%	N/A			·			
				xisting structure	-			
User Input: Outlet Pipe w/ Flow Restriction Plate			ectangular Orifice)		<u>C</u>	alculated Parameter		
Depth to Invert of Outlet Pipe =	Zone 3 Restrictor 0.25	Not Selected N/A	ft (distance below b	asin bottom at Stage	- 0 <del>ft</del> ) C	outlet Orifice Area =	Zone 3 Restrictor 0.72	Not Selected N/A
Outlet Pipe Diameter =	24.00	N/A	inches	asin bottom at stage	,	t Orifice Centroid =	0.33	N/A N/A
Restrictor Plate Height Above Pipe Invert =	6.70		inches	Half-Cen		ctor Plate on Pipe =	1.11	N/A
								•
User Input: Emergency Spillway (Rectangular or		1					Calculated Paramet	
Spillway Invert Stage=	8.28		n bottom at Stage =	= 0 ft)		Design Flow Depth=	0.31	feet
Spillway Crest Length = Spillway End Slopes =	65.00 10.00	feet H:V			-	Top of Freeboard = Top of Freeboard =	9.09 0.76	feet acres
Freeboard above Max Water Surface =	0.50	feet				Top of Freeboard =	3.20	acre-ft
						· · · · · · · · · · · · · · · · · · ·		]
Douted Hydrograph Desylte	The user	vida tha d-f- it all	UD budeaconte	d www.off.u-lines.l	contoxing 1	as in the I-flow !!	dragraphs t-t-1- 12	humana 14/ thereas a
Routed Hydrograph Results Design Storm Return Period =	WOCV	EURV	2 Year	5 Year	10 Year	<i>es in the Inflow Hyd</i> 25 Year	50 Year	100 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.50	1.75	2.00	2.25	2.52
CUHP Runoff Volume (acre-ft) =	0.333	1.159	0.865	1.145	1.370	1.709	2.040	2.456
Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) =	N/A N/A	N/A N/A	0.865	1.145 0.2	1.370 0.3	1.709 2.7	2.040 5.5	2.456 9.1
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A						
Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) =	N/A N/A	N/A N/A	0.01 11.1	0.01 14.8	0.02	0.15 23.6	0.30 28.9	0.49 35.4
Peak Inflow Q (cfs) = Peak Outflow Q (cfs) =	0.1	7.6	0.3	3.0	5.2	7.6	7.9	8.3
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	14.1	17.3	2.8	1.4	0.9
Structure Controlling Flow = Max Velocity through Grate 1 (fps) =	Plate N/A	Outlet Plate 1 0.92	Overflow Weir 1 0.01	Overflow Weir 1 0.3	Overflow Weir 1 0.6	Outlet Plate 1 0.9	0 diflet Plate 1 0.9	Outlet Plate 1 1.0
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Time to Drain 97% of Inflow Volume (hours) =	34	70 73	72 75	72	71	69 74	68	67
Time to Drain 99% of Inflow Volume (hours) = Maximum Ponding Depth (ft) =	35 3.01	5.01	4.29	75 4.52	75 4.64	<b>4</b> .90	74 5.30	74 5.92
Area at Maximum Ponding Depth (acres) =	0.32	<b>X</b> 49	0.44	0.45	0.46	0.48	0.51	0.56
Maximum Volume Stored (acre-ft) =	0.335	1.150	0.826	0.928	0.983	1.101	1.305	1.639
		$\sim$			/			
			This et	neet provided to	$\neg$			
				provided to				

This sheet provided to demonstrate existing structure height does not work.



#### DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

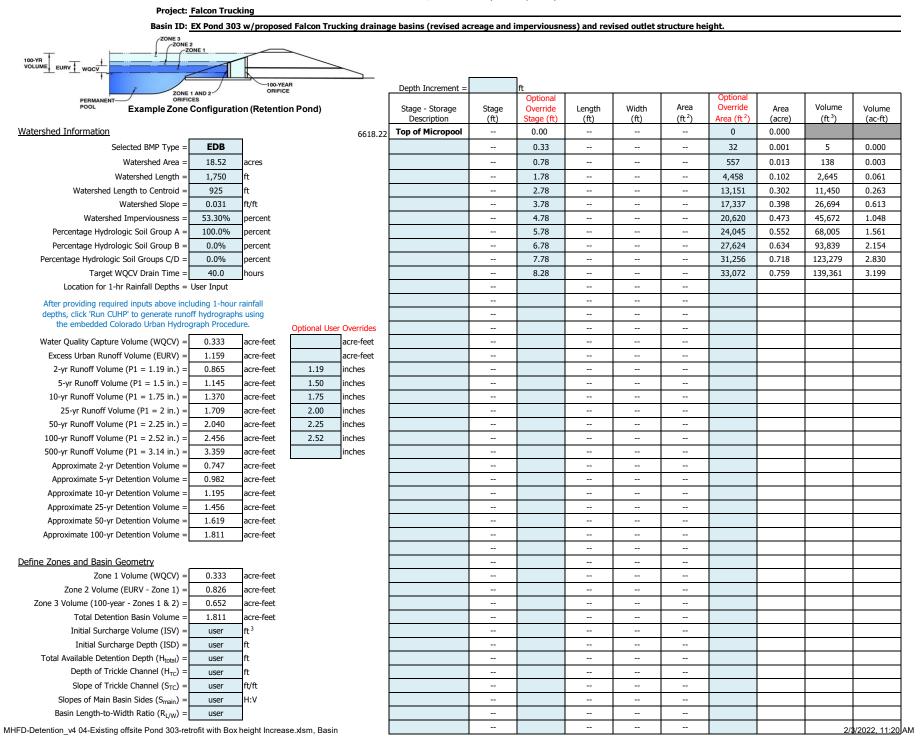
Inflow Hydrographs

The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program.

	The user can o									
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.14	0.01	0.45
	0:15:00	0.00	0.00	1.22	1.98	2.46	1.66	2.08	2.03	2.95
	0:20:00	0.00	0.00	4.41	5.81	6.85	4.34	5.08	5.43	7.12
	0:25:00	0.00	0.00	9.10	12.32	15.03	9.05	10.44	11.32	15.33
	0:30:00	0.00	0.00	11.10	14.82	17.64	19.70	24.22	27.86	38.85
	0:35:00	0.00	0.00	10.64 9.80	13.93	16.41 14.82	23.61 23.10	28.89 28.23	35.43 34.75	48.72 47.72
	0:45:00	0.00	0.00	8.73	12.62 11.34	14.82	20.96	25.52	32.16	44.35
	0:50:00	0.00	0.00	7.82	10.31	12.02	19.05	23.07	28.95	40.13
	0:55:00	0.00	0.00	7.02	9.24	10.79	16.87	20.33	25.79	35.72
	1:00:00	0.00	0.00	6.30	8.25	9.70	14.88	17.83	23.08	31.94
	1:05:00	0.00	0.00	5.74	7.47	8.84	13.15	15.68	20.67	28.67
	1:10:00	0.00	0.00	5.16	6.97	8.31	11.47	13.60	17.62	24.33
	1:15:00	0.00	0.00	4.69	6.46	7.89	10.27	12.13	15.27	20.96
	1:20:00	0.00	0.00	4.27	5.89	7.27	9.11	10.71	13.09	17.86
	1:25:00	0.00	0.00	3.88	5.35	6.47	8.05	9.42	11.15	15.11
	1:30:00	0.00	0.00	3.50	4.83	5.70	6.95	8.09	9.43	12.69
	1:35:00 1:40:00	0.00	0.00	3.13 2.81	4.34 3.73	4.99 4.40	5.92 4.99	6.85 5.73	7.84 6.40	10.45 8.43
	1:40:00	0.00	0.00	2.81	3.73	4.40 3.99	4.99	4.77	5.16	6.71
	1:50:00	0.00	0.00	2.39	2.98	3.99	3.65	4.12	4.33	5.59
	1:55:00	0.00	0.00	2.10	2.79	3.57	3.33	3.75	3.84	4.92
	2:00:00	0.00	0.00	1.99	2.60	3.29	3.14	3.53	3.54	4.49
	2:05:00	0.00	0.00	1.61	2.11	2.67	2.52	2.84	2.80	3.53
	2:10:00	0.00	0.00	1.27	1.66	2.11	1.97	2.21	2.15	2.70
	2:15:00	0.00	0.00	1.00	1.31	1.66	1.54	1.73	1.65	2.05
	2:20:00	0.00	0.00	0.78	1.02	1.29	1.20	1.34	1.26	1.56
	2:25:00	0.00	0.00	0.61	0.80	1.00	0.93	1.04	0.97	1.19
	2:30:00	0.00	0.00	0.47	0.61	0.76	0.71	0.79	0.74	0.91
	2:35:00 2:40:00	0.00	0.00	0.36	0.46	0.57	0.53	0.59 0.45	0.56 0.43	0.69
	2:45:00	0.00	0.00	0.27	0.26	0.33	0.40	0.43	0.43	0.33
	2:50:00	0.00	0.00	0.14	0.18	0.24	0.23	0.25	0.33	0.29
	2:55:00	0.00	0.00	0.10	0.13	0.16	0.16	0.17	0.16	0.20
	3:00:00	0.00	0.00	0.06	0.08	0.10	0.10	0.11	0.10	0.12
	3:05:00	0.00	0.00	0.03	0.05	0.06	0.06	0.06	0.06	0.07
	3:10:00	0.00	0.00	0.01	0.02	0.02	0.02	0.03	0.02	0.03
	3:15:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00 3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00 4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00 4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00 5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00 5:50:00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

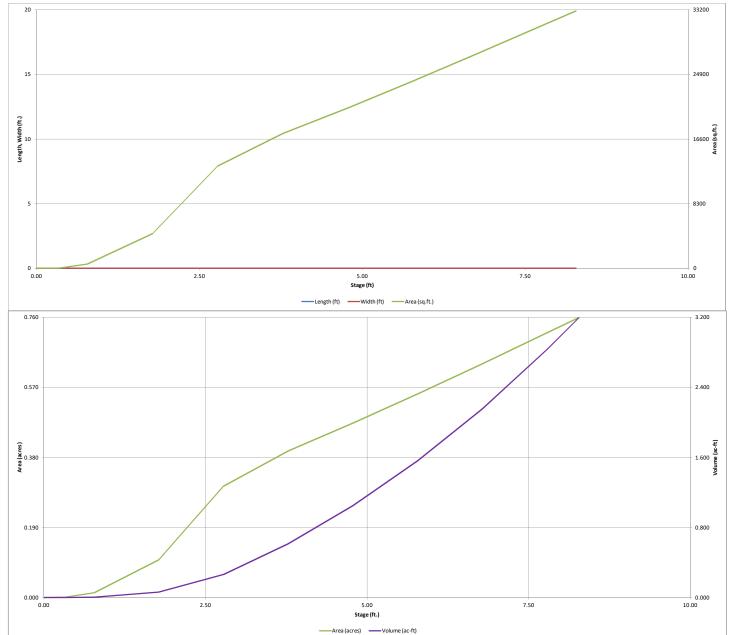
#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



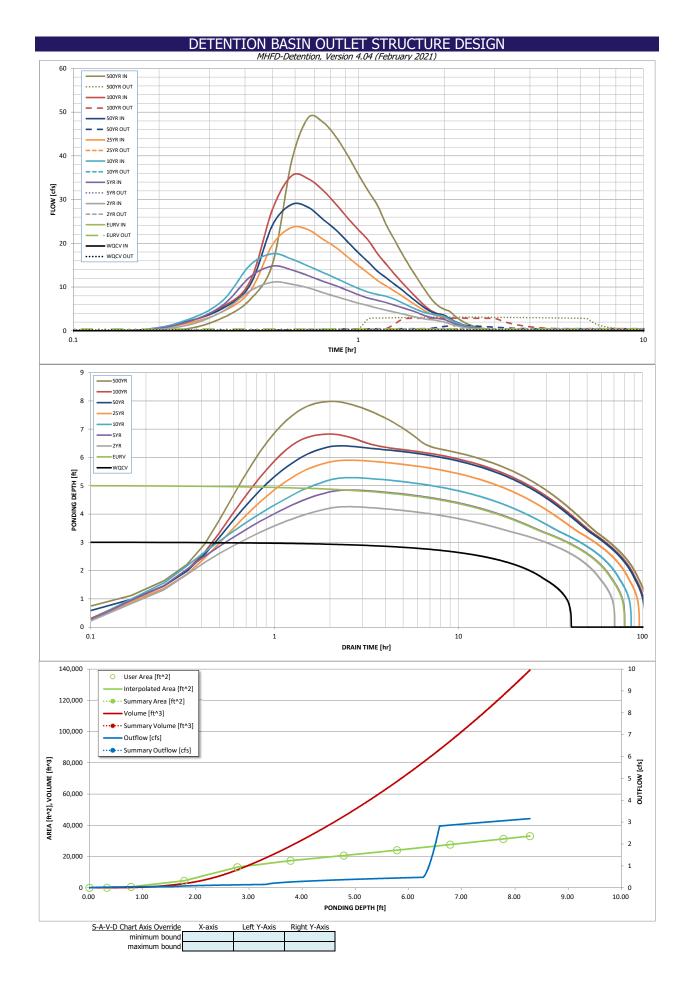
#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



### DETENTION BASIN OUTLET STRUCTURE DESIGN

Project:	Falcon Trucking	МНІ	FD-Detention, Vers	sion 4.04 (Februar	y 2021)			
		oposed Falcon True	cking drainage basi	ns (revised acreag	e and imperviousne	ess) and revised ou	tlet structure heig	nt.
ZONE 3				Estimated	Estimated			
				Stage (ft)	Volume (ac-ft)	Outlet Type		
	<b>1</b>		Zone 1 (WQCV)	3.01	0.333	Orifice Plate		
	100-YEAR		Zone 2 (EURV)	5.01	0.826	Orifice Plate		
PERMANENT ORIFICES	ORIFICE		Zone 3 (100-year)	6.22	0.652	Weir&Pipe (Restrict)		
	Configuration (Re	tention Pond)		Total (all zones)	1.811	frendinge (Reserver)	i -	
User Input: Orifice at Underdrain Outlet (typically	v used to drain WO	CV in a Filtration BN	(P)	rotar (un zones)	1.011	1	Calculated Paramet	ters for Underdrain
Underdrain Orifice Invert Depth =	_		the filtration media	surface)	Underd	drain Orifice Area =	N/A	ft <sup>2</sup>
Underdrain Orifice Diameter =		inches		,		Orifice Centroid =	N/A	feet
						I		
User Input: Orifice Plate with one or more orifice	es or Elliptical Slot V	Neir (typically used	to drain WQCV and	/or EURV in a sedir	mentation BMP)		Calculated Paramet	ters for Plate
Invert of Lowest Orifice =		ft (relative to basin	bottom at Stage =	0 ft)	WQ Orifi	ice Area per Row =	N/A	ft <sup>2</sup>
Depth at top of Zone using Orifice Plate =		•	bottom at Stage =	0 ft)		ptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =		inches			•	ical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	N/A	inches			E	lliptical Slot Area =	N/A	ft <sup>2</sup>
Lloss Innuity, Stage and Total Area of Each Orifice	Daw (numbered fi	om lowest to highe	(at)					
User Input: Stage and Total Area of Each Orifice		-	· ·	Row 4 (optional)	Dow E (optional)	Dow 6 (optional)	Dow 7 (antional)	Dow 9 (optional)
Stage of Orifice Centroid (ft)	Row 1 (required) 0.00	Row 2 (optional) 1.67	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Orifice Area (sq. inches)	1.45	1.45	3.34 4.40					
Office Area (sq. incles)	1.45	1.45						
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)		now to (optional)	Now II (optional)	Row 12 (optional)	now 15 (optional)	now in (optional)	(optional)	
Orifice Area (sq. inches)								
			1		1	1		
User Input: Vertical Orifice (Circular or Rectangu	<u>ılar)</u>						Calculated Paramet	ters for Vertical Orif
	Not Selected	Not Selected					Not Selected	Not Selected
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	0 ft) Ver	tical Orifice Area =	N/A	N/A
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	0 ft) Vertica	I Orifice Centroid =	N/A	N/A
Vertical Orifice Diameter =	N/A	N/A	inches					
		0 H H D' OD D					<u></u>	
User Input: Overflow Weir (Dropbox with Flat or			tangular/Trapezoida 1	a weir (and No Out	let Pipe)	ĺ		ters for Overflow W
Overfley, Weir Frent Edge Height He -	Zone 3 Weir 6.27	Not Selected N/A	A (uslative to basis b		N Hoight of Crat	e Upper Edge, H <sub>t</sub> =	Zone 3 Weir 6.27	Not Selected N/A
Overflow Weir Front Edge Height, Ho = Overflow Weir Front Edge Length =	4.00	N/A N/A	feet	ottom at Stage = 0 fl		/eir Slope Length =	2.91	N/A N/A
Overflow Weir Front Edge Length =	0.00	N/A	H:V	G	rate Open Area / 10		35.74	N/A N/A
Horiz. Length of Weir Sides =	2.91	N/A	feet		verflow Grate Open		8.10	N/A N/A
Overflow Grate Type =	Type C Grate	N/A			Overflow Grate Open	-	2.43	N/A
Debris Clogging % =	70%	N/A	%				2110	.,,,,
		,						
User Input: Outlet Pipe w/ Flow Restriction Plate	(Circular Orifice, Re	estrictor Plate, or Re	<u>ectangular Orifice)</u>		Ca	Iculated Parameters	s for Outlet Pipe w/	Flow Restriction Pla
	Zone 3 Restrictor	Not Selected					Zone 3 Restrictor	Not Selected
Depth to Invert of Outlet Pipe =	0.25	N/A	ft (distance below ba	isin bottom at Stage :	= 0 ft) O	utlet Orifice Area =	0.23	N/A
Outlet Pipe Diameter =	24.00	N/A	inches		Outlet	t Orifice Centroid =	0.15	N/A
Restrictor Plate Height Above Pipe Invert =	3.00		inches	Half-Cent	tral Angle of Restric	tor Plate on Pipe =	0.72	N/A
User Input: Emergency Spillway (Rectangular or							Calculated Paramet	
Spillway Invert Stage=		•	bottom at Stage =	0 ft)	· · ·	esign Flow Depth=	0.31	feet
Spillway Crest Length =		feet			-	Fop of Freeboard =	9.09	feet
Spillway End Slopes =		H:V				Fop of Freeboard =		acres
Freeboard above Max Water Surface =	0.50	feet			Basin volume at	Fop of Freeboard =	3.20	acre-ft
Routed Hydrograph Results	The user can overn	ride the default CUP	HP hydrographs and	runoff volumes by	entering new value	es in the Inflow Hya	rographs table (Co	lumns W through Al
Design Storm Return Period =	WQCV	EURV	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) =	N/A 0.333	N/A 1.159	1.19 0.865	1.50 1.145	1.75 1.370	2.00 1.709	2.25 2.040	2.52 2.456
Inflow Hydrograph Volume (acre-ft) =	N/A	N/A	0.865	1.145	1.370	1.709	2.040	2.456
CUHP Predevelopment Peak Q (cfs) =	N/A	N/A	0.1	0.2	0.3	2.7	5.5	9.1
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A			0.77	0.15	0	
Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) =	N/A N/A	N/A N/A	0.01 11.1	0.01 14.8	0.02 17.6	0.15 23.6	0.30 28.9	0.49 35.4
Peak Innow Q (crs) = Peak Outflow Q (crs) =	0.1	0.4	0.3	0.4	0.4	0.5	1.2	2.9
Ratio Peak Outflow to Predevelopment Q =	N/A	N/A	N/A	1.7	1.4	0.2	0.2	0.3
Structure Controlling Flow =	Plate	Plate	Plate	Plate	Plate	Plate	Overflow Weir 1	Outlet Plate 1
Max Velocity through Grate 1 (fps) =	N/A	N/A	N/A	N/A	N/A N/A	N/A	0.1	0.3
Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	N/A 38	N/A 72	N/A 64	N/A 72	N/A 77	N/A 85	N/A 90	N/A 89
Time to Drain 99% of Inflow Volume (hours) =	40	77	68	77	83	92	98	98
Maximum Ponding Depth (ft) =	3.01	5.01	4.26	4.85	5.29	5.90	6.41	6.83
Area at Maximum Ponding Depth (acres) =	0.32	0.49	0.43	0.48	0.51	0.56	0.60	0.64
Maximum Volume Stored (acre-ft) =	0.335	1.159	0.808	1.077	1.295	1.628	1.925	2.180



#### DETENTION BASIN OUTLET STRUCTURE DESIGN

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

1								in a separate pro	-	
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.14	0.01	0.45
	0:15:00	0.00	0.00	1.22	1.98	2.46	1.66	2.08	2.03	2.95
	0:20:00	0.00	0.00	4.41	5.81	6.85	4.34	5.08	5.43	7.12
	0:25:00	0.00	0.00	9.10	12.32	15.03	9.05	10.44	11.32	15.33
	0:30:00	0.00	0.00	11.10	14.82	17.64	19.70	24.22	27.86	38.85
	0:35:00 0:40:00	0.00	0.00	10.64	13.93	16.41	23.61	28.89	35.43	48.72
	0:45:00	0.00	0.00	9.80 8.73	12.62 11.34	14.82 13.35	23.10 20.96	28.23 25.52	34.75 32.16	47.72 44.35
	0:50:00	0.00	0.00	7.82	10.31	12.02	19.05	23.07	28.95	40.13
	0:55:00	0.00	0.00	7.02	9.24	10.79	16.87	20.33	25.79	35.72
	1:00:00	0.00	0.00	6.30	8.25	9.70	14.88	17.83	23.08	31.94
	1:05:00	0.00	0.00	5.74	7.47	8.84	13.15	15.68	20.67	28.67
	1:10:00	0.00	0.00	5.16	6.97	8.31	11.47	13.60	17.62	24.33
	1:15:00	0.00	0.00	4.69	6.46	7.89	10.27	12.13	15.27	20.96
	1:20:00	0.00	0.00	4.27	5.89	7.27	9.11	10.71	13.09	17.86
	1:25:00	0.00	0.00	3.88	5.35	6.47	8.05	9.42	11.15	15.11
	1:30:00	0.00	0.00	3.50	4.83	5.70	6.95	8.09	9.43	12.69
	1:35:00 1:40:00	0.00	0.00	3.13 2.81	4.34 3.73	4.99 4.40	5.92 4.99	6.85 5.73	7.84 6.40	10.45 8.43
	1:45:00	0.00	0.00	2.81	3.73	3.99	4.99	4.77	5.16	6.71
	1:50:00	0.00	0.00	2.39	2.98	3.99	3.65	4.12	4.33	5.59
	1:55:00	0.00	0.00	2.22	2.79	3.57	3.33	3.75	3.84	4.92
	2:00:00	0.00	0.00	1.99	2.60	3.29	3.14	3.53	3.54	4.49
	2:05:00	0.00	0.00	1.61	2.11	2.67	2.52	2.84	2.80	3.53
	2:10:00	0.00	0.00	1.27	1.66	2.11	1.97	2.21	2.15	2.70
	2:15:00	0.00	0.00	1.00	1.31	1.66	1.54	1.73	1.65	2.05
	2:20:00	0.00	0.00	0.78	1.02	1.29	1.20	1.34	1.26	1.56
	2:25:00	0.00	0.00	0.61	0.80	1.00	0.93	1.04	0.97	1.19
	2:30:00	0.00	0.00	0.47	0.61	0.76	0.71	0.79	0.74	0.91
	2:35:00 2:40:00	0.00	0.00	0.36	0.46	0.57	0.53	0.59 0.45	0.56	0.69 0.53
	2:45:00	0.00	0.00	0.27	0.34	0.44	0.40	0.45	0.43	0.33
	2:50:00	0.00	0.00	0.20	0.20	0.33	0.23	0.25	0.33	0.40
	2:55:00	0.00	0.00	0.10	0.13	0.16	0.16	0.17	0.16	0.20
	3:00:00	0.00	0.00	0.06	0.08	0.10	0.10	0.11	0.10	0.12
	3:05:00	0.00	0.00	0.03	0.05	0.06	0.06	0.06	0.06	0.07
	3:10:00	0.00	0.00	0.01	0.02	0.02	0.02	0.03	0.02	0.03
	3:15:00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01
	3:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:30:00 3:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	3:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:10:00	0.00 0.00	0.00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00 4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00 4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
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	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:00:00 5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00 5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:45:00 5:50:00	0.00 0.00	0.00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00



212 N. Wahsatch Ave., Ste. 305 Colorado Springs, CO **719.955.5485** 

Project: FARCON TRUCKTARE FILING No. 1 Date: 62-04-2022 Volume Power 303 FORE BAN ENTIMES AT MOUNTAIN VESTA FLITNE NOSER (E.MV5) 3% OF WOCV = 3% × 0.335 pc-FT (43560 4FF)=437.8 CUPE = 43800 St WEST FORBAY NON APPLICABLE FLOWS DINSTED TO EMVS. NORTH FREEDAN = 180 SF x 1.5" = 270 CU FT PER EMVS BMP PLANS 180 SF X 2 5' - 450 CU FT 2 438 CUFT DESTEN NORTH FORBBAY WILL HAVE TO BE MODIFIED FORE BAY RELEASE AND CONFIGURA TION 2º16 OF 100YR PEAK DZS HARCE 2% × 47.2 cFS = 0.944 cFs ≤ 3.05 c8s For 3" DATEN OPENIZOG SEE BRODDCRESTED WEIR FOLEBAND NOTCH CALCULATION IN APPENDIX. SEE OPENCILANNEL FLOW CALCULATOR IN APPENDZK. FUL CAPACITY 2'XB" @ 0.5% = 4.39 cfs > 3.05 cfs North SPILLINGY CALC. 47.2055 + BASIN B 5.3 CBS EMVS = 52.5 cfs 52.5 cds £ 73.19 of FMV 5 BMP PLANS \$ FOR

onlinechannel14.php: Discharge over a broad-crested weir				
H The broad-crested w	eir	C = (2/3	<b>nulas:</b> ) <sup>3/2</sup> (g) <sup>1/2</sup> CLH <sup>3/2</sup>	
INPUT DATA:	INTERMEDIATE	CALCS:	OUTPUT:	
Select: SI units (metric) U.S. Customary units	Units selected: Customary	U.S.	Discharge Q: 3.050 cfs	
Hydraulic head 2.5 ft	Gravitational acc g: 32.17 ft s <sup>-2</sup>	eleration		
Weir length L: .25 ft	Discharge coeffic 3.087 ft <sup>1/2</sup> s <sup>-1</sup>	cient C:		
Calcula Your request was processed a 220204 15:03:58 ].			4th, 2022 [	
Thank you for running onlined	channel14.php. P	lease call a	again. [140618]	

### **EX POND 303 FOREBAY NOTCH CALCULATION**

]	The open channel flow calculator					
Select Channel Type: Rectangle ✓	FT  ↓ ↓ Fb  Rectangle	z1 t b t z2 Trapezoid	z1 z2 Iy			
Velocity(V)&Discharge(Q) V	elect unit system: F	eet(ft) V				
Channel slope: 0.005 ft/ft	Water depth(y): 0.	5 ft	Bottom W(b) ft	2		
Flow velocity 4.3926 ft/s	LeftSlope (Z1): 0	to 1 (H:'	RightSlope (2)	Z2): 0		
Flow discharge 4.3926 ft^3/s	Input n value 0.011	5 or select r				
Calculate!	Status: Calculation f	nished	Reset			
Wetted perimeter 3	Flow area 1	ft^2	Top width(T)	)2 [ft		
Specific energy 0.8	Froude number 1.09 Flow status Supercritical flow					
Critical depth 0.53 ft	Critical slope 0.004	2 ft/ft	Velocity head	d 0.3 ft		

Copyright 2000 Dr. Xing Fang, Department of Civil Engineering, Lamar University.

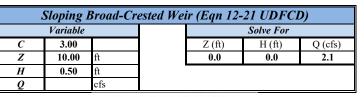
#### **EX POND 303 TRICKLE CHANNEL**

#### **ENCLAVES AT MOUNTAIN VISTA FILING NO.5** EMERGENCY SPILLWAY CALCULATIONS FSD POND A

Ha	Horizontal Broad-Crested Weir (Eqn 12-20 UDFCD)					
Variable				Solve For		
С	3.00			L (ft)	H (ft)	Q (cfs)
L	65.00	ft		0.0	0.0	68.9
Н	0.50	ft				
Q		cfs				

Equation 12-20	

Where:



Equation 12-21  $Q = \left(\frac{2}{5}\right) C_{BCW} Z H^{25}$ 

Q = discharge (cfs)

 $Q = C_{acw} L H^{13}$ 

CBCW = broad-crested weir coefficient (This ranges from 2.6 to 3.0. A value of 3.0 is often used in practice.) See Hydraulic Engineering Circular No. 22 for additional information.

L = broad-crested weir length (ft)

H = head above weir crest (ft)

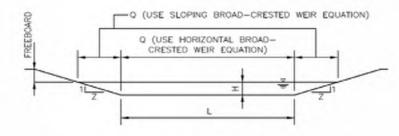
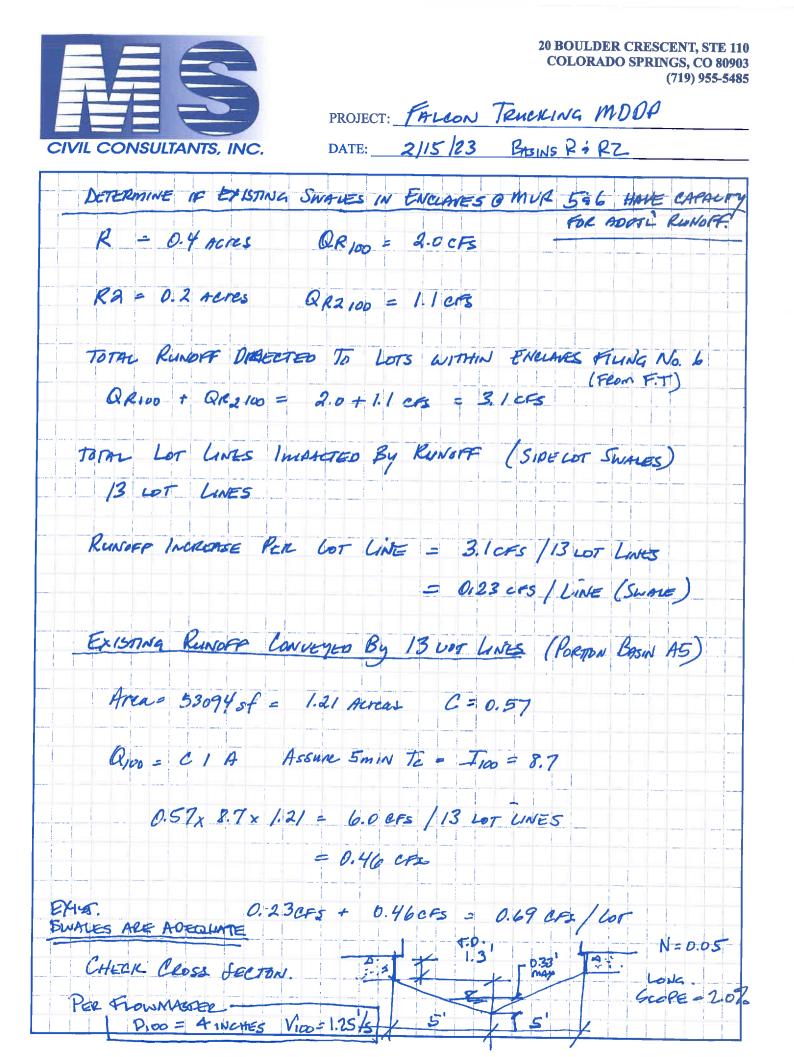
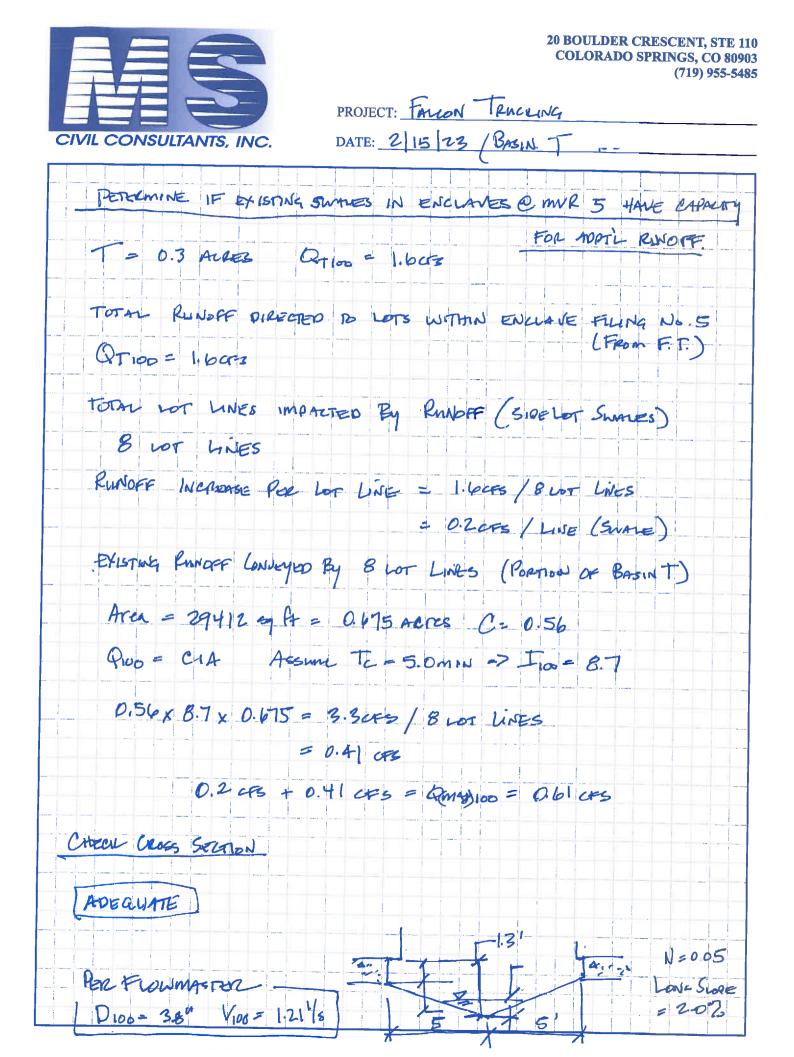
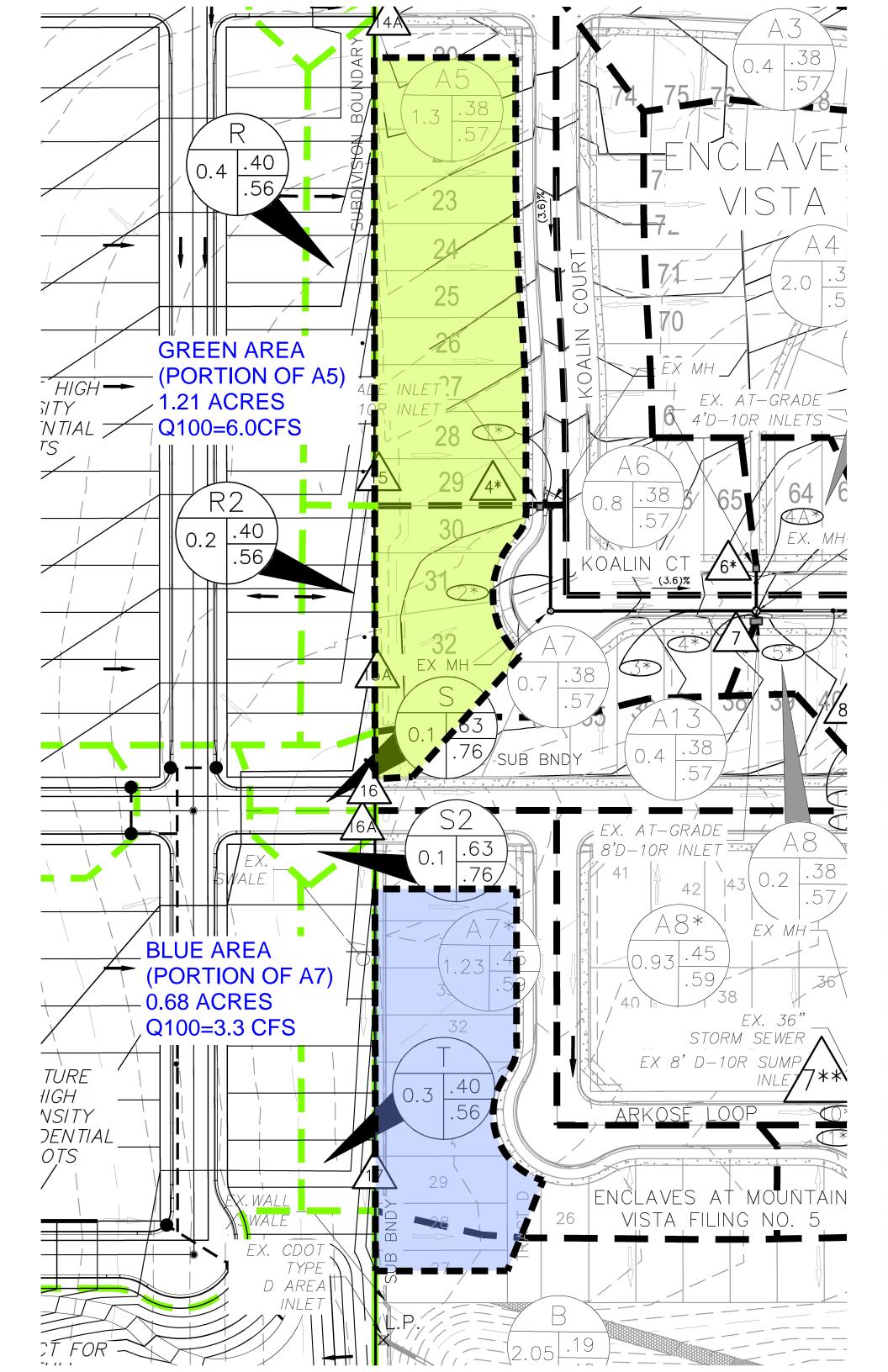


Figure 12-20. Sloping broad-crest weir







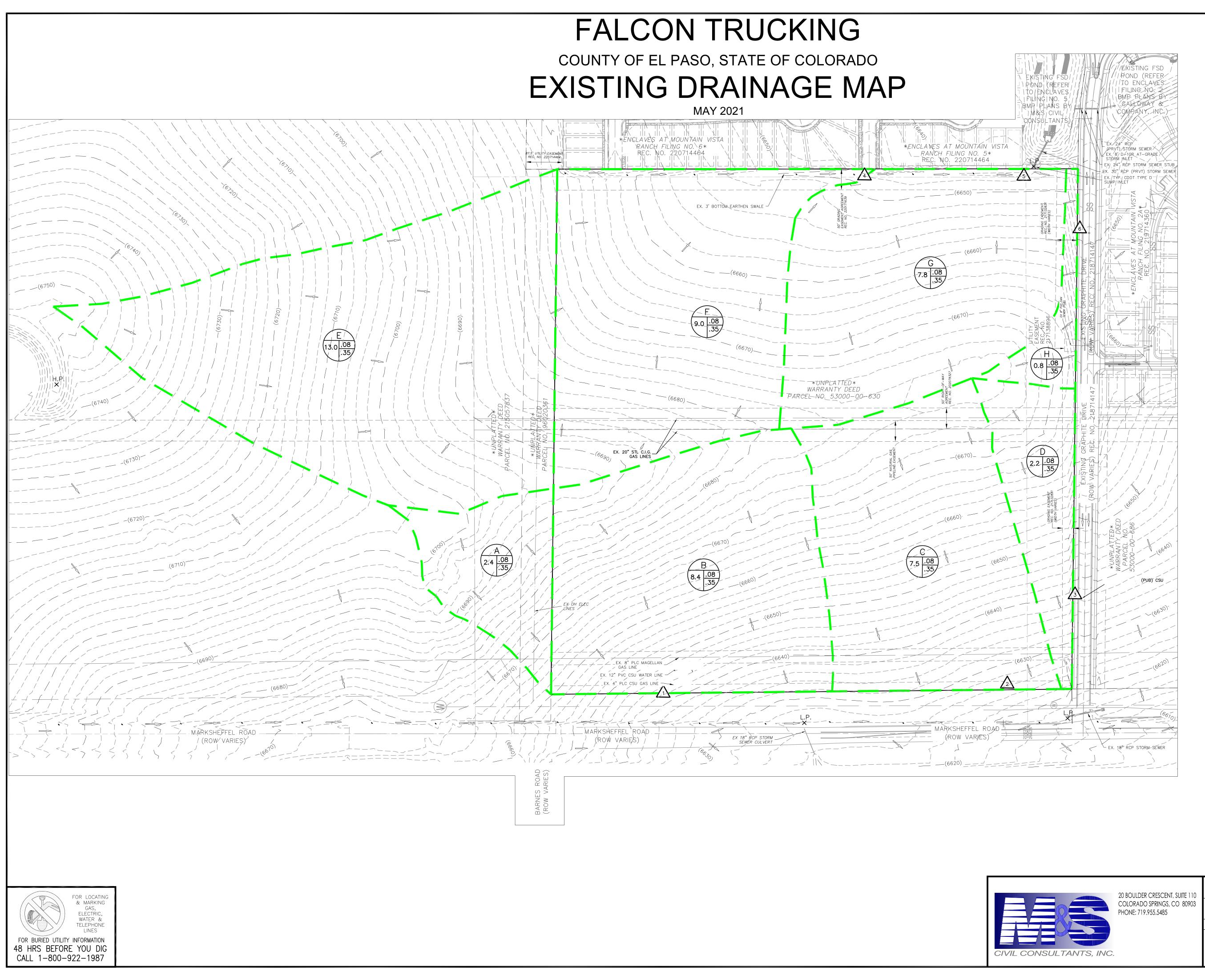
Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.050	
Channel Slope	0.020 ft/ft	
Left Side Slope	5.000 H:V	
Right Side Slope	5.000 H:V	
Discharge	0.69 cfs	
Results		
Normal Depth	4.0 in	
Flow Area	0.6 ft <sup>2</sup>	
Wetted Perimeter	3.4 ft	
Hydraulic Radius	2.0 in	
Top Width	3.32 ft	
Critical Depth	3.1 in	
Critical Slope	0.074 ft/ft	
Velocity	1.25 ft/s	
Velocity Head	0.02 ft	
Specific Energy	0.36 ft	
Froude Number	0.542	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	0.00 ft/s	
Upstream Velocity	0.00 ft/s	
Normal Depth	4.0 in	
Critical Depth	3.1 in	
Channel Slope	0.020 ft/ft	
Critical Slope	0.074 ft/ft	

#### Worksheet for Common Side Lot Swale - Filing 6 - 0.69 cfs

Project Description		
Friction Method	Manning	
	Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.050	
Channel Slope	0.020 ft/ft	
Left Side Slope	5.000 H:V	
Right Side Slope	5.000 H:V	
Discharge	0.61 cfs	
Results		
Normal Depth	3.8 in	
Flow Area	0.5 ft <sup>2</sup>	
Wetted Perimeter	3.2 ft	
Hydraulic Radius	1.9 in	
Top Width	3.17 ft	
Critical Depth	3.0 in	
Critical Slope	0.075 ft/ft	
Velocity	1.21 ft/s	
Velocity Head	0.02 ft	
Specific Energy	0.34 ft	
Froude Number	0.538	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	0.00 ft/s	
Upstream Velocity	0.00 ft/s	
Normal Depth	3.8 in	
Critical Depth	3.0 in	
Channel Slope	0.020 ft/ft	
Critical Slope	0.075 ft/ft	

### Worksheet for Common Side Lot Swale - Filing 5 - 0.61 cfs

**DRAINAGE MAPS** 



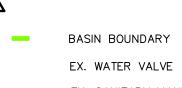
BASIN	BASIN SUMMARY						
AREA AREA BASIN (ACRES) Q <sub>5</sub> Q <sub>10</sub>							
A	2.37	0.6	4.4				
В	8.42	2.2	16.1				
С	7.53	1.8	13.0				
D	2.23	0.6	4.1				
E	12.97	3.1	22.5				
F	8.97	2.0	15.0				
G	7.78	1.5	11.3				
Н	0.79	0.2	1.5				

	DESIGN POINT SUMMARY						
DESIGN POINT	<b>Q</b> <sub>5</sub>	<b>Q</b> <sub>100</sub>	BASIN	STRUCTURE			
1	2.7	19.6	А, В	TO MS ROW (MS CULVERT)			
2	1.8	13.0	С	To MS ROW (GRAPHITE CULVERT)			
3	0.6	4.1	D	to graphite dr row (w)			
4	4.0	29.6	E, F	3' EARTHEN SWALE			
5	4.6	33.6	DP4, G	EX TYPE D INLET			
6	0.2	1.5	Н	to graphite dr row (e)			

<u>LEGEND</u>

# BASIN DESIGNATION

SURFACE DESIGN POINT



/

05

 $\langle ||$ H.P. X

L.P. X

 $< = \bullet$ 

EX. SANITARY MANHOLE

EXIST MAJ CONT

EXIST MIN CONT

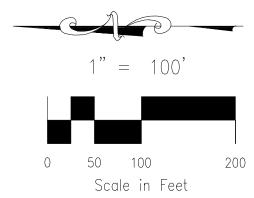
EXISTING FLOW DIRECTION ARROW

HIGH POINT LOW POINT

EXISTING ROADSIDE DITCH

SITE BOUNDARY

- ----- R.O.W./EASEMENT
  - LOT LINE



## FALCON TRUCKING FXISTING DRAINAGE MAP

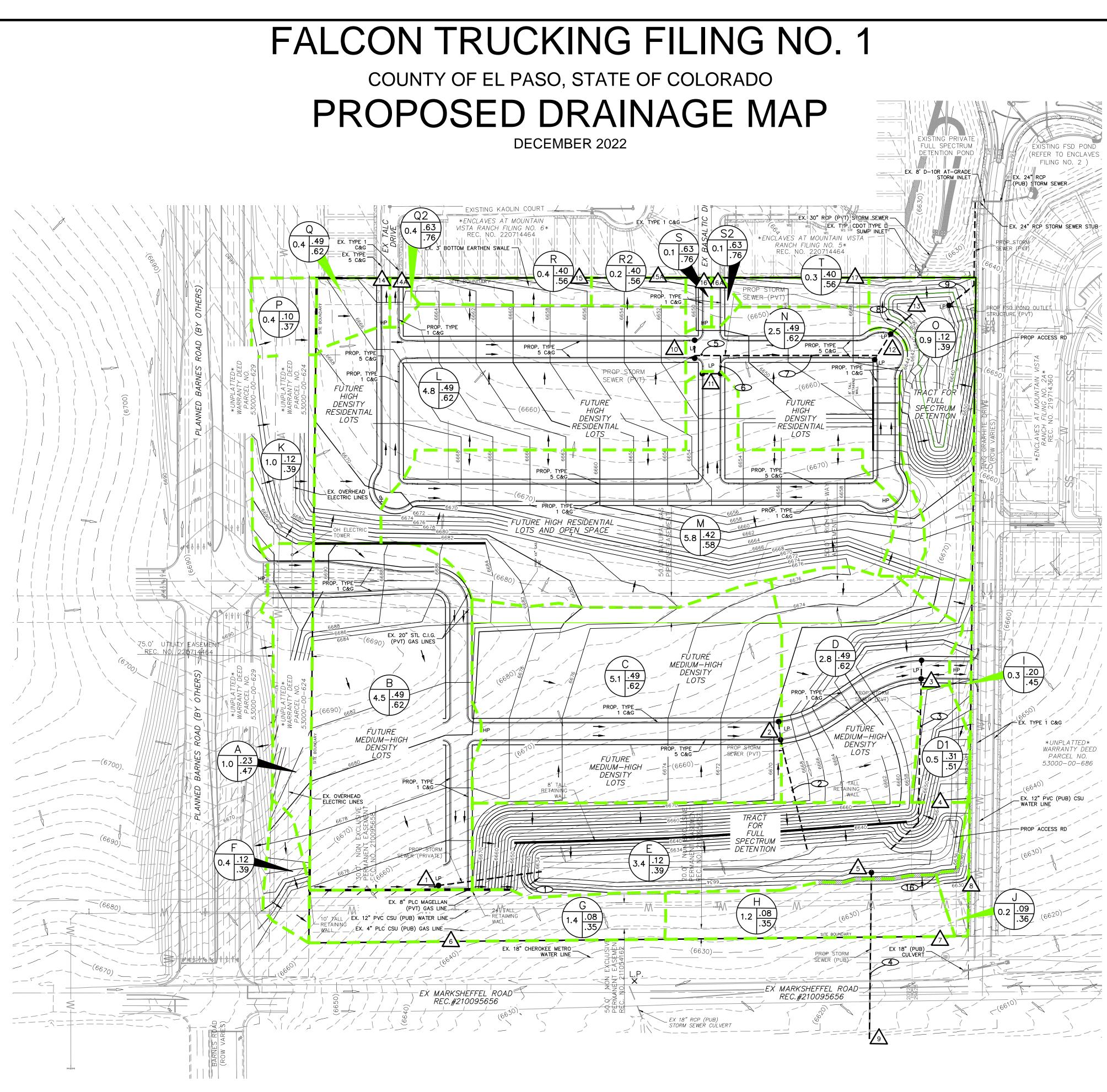
	EXISTING DRAINAGE MAP					
PROJECT NO. 2	9-007A	SCALE:	DATE: 05/20/21			
DESIGNED BY: DRAWN BY: CHECKED BY:	DLM DLM VAS	HORIZONTAL: 1"=100' VERTICAL: N/A	SHEET 1 OF 1	PDM		

BASIN SUMMARY						
BASIN	AREA (ACRES)	$Q_5$	<b>Q</b> 100			
А	0.95	1.1	3.7			
В	4.50	8.9	19.0			
С	5.07	9.0	19.1			
D	2.80	5.2	11.1			
D1	0.46	0.6	1.6			
E	3.41	1.6	9.0			
F	0.37	0.2	1.0			
G	1.44	0.5	3.7			
Н	1.22	0.4	3.0			
	0.30	0.3	1.2			
J	0.17	0.1	0.4			
K	0.97	0.5	2.7			
L	4.76	8.6	18.2			
М	5.84	11.0	25.1			
Ν	2.49	5.0	10.7			
0	0.90	0.5	2.8			
Ρ	0.41	0.2	1.1			
Q	0.36	0.7	1.6			
Q2	0.08	0.2	0.4			
R	0.40	0.8	2.0			
R2	0.22	0.5	1.1			
S	0.11	0.5	0.9			
S2	0.08	0.4	0.6			
Т	0.33	0.7	1.6			

DESIGN POINT SUMMARY					
DESIGN POINT	<b>Q</b> <sub>5</sub>	Q <sub>100</sub>	BASIN	STRUCTURE	
1	11.0	24.6	А, В	PROP 36" RCP*	
2	9.0	19.1	С	PROP 30" RCP*	
3	5.2	11.1	D	PROP 24" RCP*	
4	0.6	1.6	D1		
5	28.5	58.0	PR1-PR3, DP4, E	FSD POND 1	
6	0.7	4.5	F, G		
7	0.4	3.0	Н		
8	0.4	1.5	I, J	graphite drive	
9	2.7	16.5	DP6, POND 1	EARTHEN SWALE	
10	9.0	20.6	K, L	PROP 30" RCP*	
11	11.0	25.1	М	PROP 36" RCP*	
12	5.0	10.7	Ν	PROP 42" RCP*	
13	23.0	53.2	PR8, O	FSD POND 2	
14	0.9	2.6	P, Q	EX TALC DRIVE	
14A	0.2	0.4	Q2	EX TALC DRIVE	
15	0.8	2.0	R	FILING 6 BOUNDARY	
15A	0.5	1.1	R2	FILING 6 BOUNDARY	
16	0.5	0.9	S	EX BASALTIC DRIVE	
16A	0.4	0.6	S2	EX BASALTIC DRIVE	
17	0.7	1.6	Т	FILING 5 BOUNDARY	

STORM SEWER SUMMARY					
PIPE RUN	$Q_5$	<b>Q</b> <sub>100</sub>	PIPE SIZE	CONTRIBUTING PIPES & DESIGN POINTS	
1	11.0	24.6	36" RCP*	DP1	
2	9.0	19.1	30" RCP*	DP2	
3	5.2	11.1	24" RCP*	DP3	
4	2.1	12.0	24" RCP*	FSD POND 1 OUTFALL	
5	9.0	20.6	30" RCP*	DP10	
6	11.0	25.1	36"RCP*	DP11	
7	18.1	41.5	42" RCP*	PR5, PR6	
8	22.6	51.0	42" RCP*	PR7, DP12	
9	0.6	11.7	18" RCP*	FSD POND 2 OUTFALL	





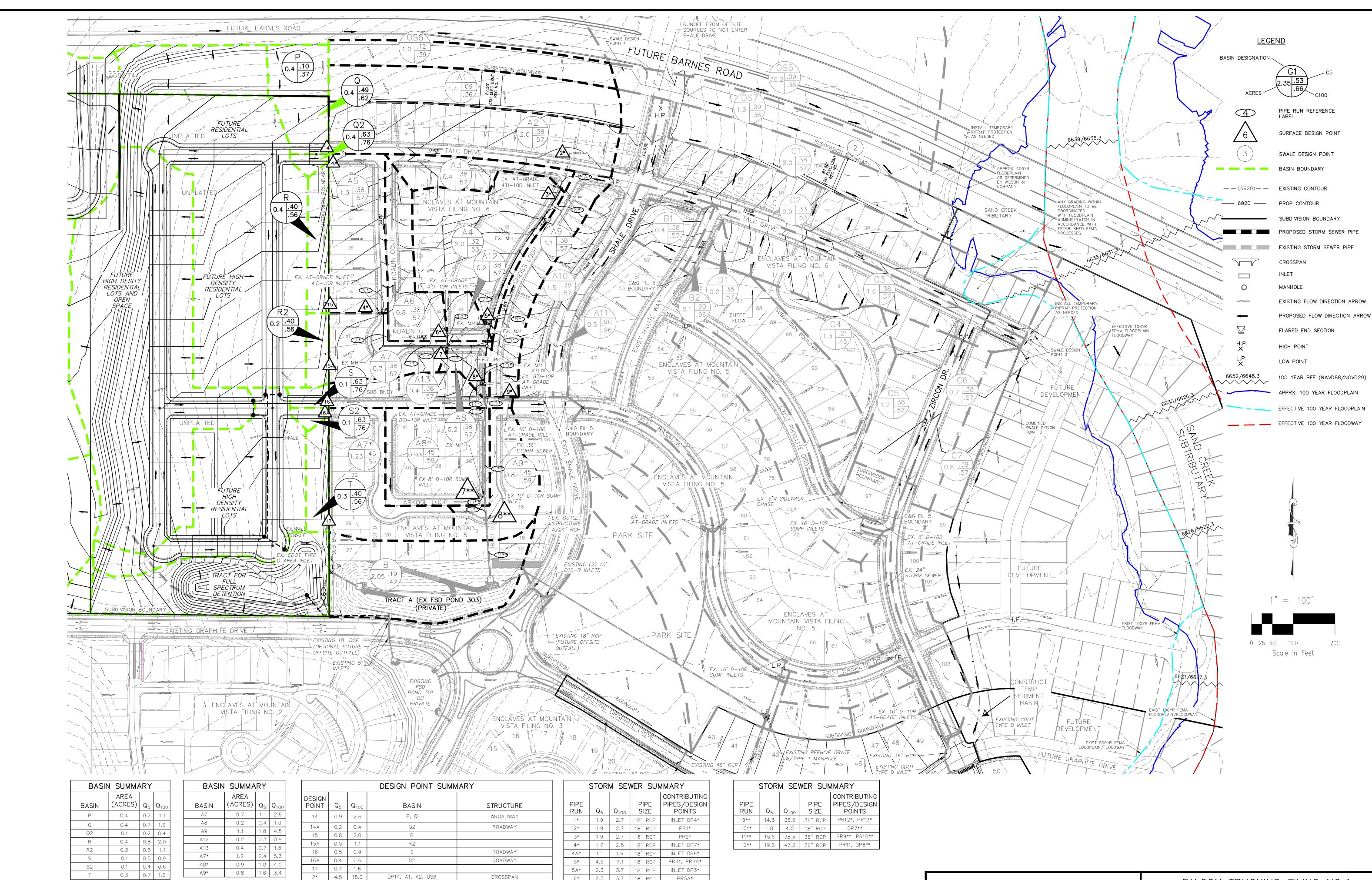
# <u>LEGEND</u> BASIN DESIGNATION SURFACE DESIGN POINT BASIN BOUNDARY EX. WATER VALVE (\$\$ EX. SANITARY MANHOLE EXIST MAJ CONT EXIST MIN CONT EXISTING FLOW DIRECTION ARROW Н.Р. **Х** HIGH POINT L.P. LOW POINT PROP STORM SEWER 1" = 100' 200 0 50 100 Scale in Feet FALCON TRUCKING FILING NO. PROPOSED DRAINAGE MAP

# CIVIL CONSULTANTS, INC.

212 n. Wahsatch ave., ste 305 Colorado springs, co 80903 Phone: 719.955.5485

PROJECT NO. 29-007A SCALE: DATE: **12/02/22** HORIZONTAL DESIGNED BY: CVW 1"=100' DRAWN BY: CVW SHEET 1 OF 2 VERTICAL: CHECKED BY: VAS N/A

PDM





OS6

A1

A2

A3

1.0 0.5 2.7

1.40.53.62.02.87.1

0.4 0.6 1.6

A4 2.0 2.7 7.5

A5 1.3 2.2 5.5

A6 0.8 1.2 3.1

DESIGN POINT SUMMARY							
DESIGN POINT	$Q_5$	Q <sub>100</sub>	BASIN	STRUCTURE			
14	0.9	2.6	P, Q	WROADWAY			
14A	0.2	0.4	Q2	ROADWAY			
15	0.8	2.0	R				
15A	0.5	1.1	R2				
16	0.5	0.9	S	ROADWAY			
16A	0.4	0.6	S2	ROADWAY			
17	0.7	1.6	Т				
2*	4.5	15.0	DP14, A1, A2, OS6	CROSSPAN			
3*	5.1	16.4	DP2, A3	EX 4'D10-R AT-GRADE INLET			
4*	3.1	7.5	DP14A, DP15, A5	EX 4' D10-R AT-GRADE INLET			
5*	4.9	18.4	FB DP3, A4	EX 4' D10-R AT-GRADE INLET			
6*	1.2	3.1	A6	EX 4' D10-R AT-GRADE INLET			
7*	2.6	8.3	FB DP4, A7, 15A	EX 4' D10-R AT-GRADE INLET			
8*	4.6	25.0	FB DP5, FB DP6, FB DP7, A8, A12	EX 8' D10-R AT-GRADE INLET			
9*	3.0	19.1	DP16, A9, A13, FB DP8	EX 16' D10-R AT-GRADE INLET			
7**	1.8	4.0	A8*	EX 8' D10-R SUMP INLET			
8**	4.7	10.4	DP16A, DP17, A7*, A9*	EX 10' D10-R SUMP INLET			

STORM SEWER SUMMARY							
PIPE RUN	<b>Q</b> <sub>5</sub>	Q <sub>100</sub>	PIPE SIZE	CONTRIBUTING PIPES/DESIGN POINTS			
1*	1.9	2.7	18" RCP	INLET DP4*			
2*	1.9	2.7	18" RCP	PR1*			
3*	1.9	2.7	18" RCP	PR2*			
4*	1.7	2.8	18" RCP	INLET DP7*			
4A*	1.1	1.9	18" RCP	INLET DP6*			
5*	4.5	7.1	18" RCP	PR4*, PR4A*			
5A*	2.3	3.7	18" RCP	INLET DP3*			
6*	2.3	3.7	18" RCP	PR5A*			
7*	2.3	3.7	18" RCP	PR6*			
8*	2.2	3.7	18" RCP	INLET DP5*			
9*	4.4	7.2	18" RCP	PR7*, PR8*			
10*	8.3	13.4	24" RCP	PR5*, PR9*			
11*	3.8	8.7	18" RCP	INLET DP8*			
12*	11.5	20.7	30" RCP	PR10*, PR11*			
13*	2.7	14.5	18" RCP	PR12*, PR13*			

STORM SEWER SUMMARY								
PIPE RUN	$Q_5$	<b>Q</b> <sub>100</sub>	PIPE SIZE	CONTRIBUTING PIPES/DESIGN POINTS				
9**	14.3	35.5	36" RCP	PR12*, PR13*				
10**	1.8	4.0	18"RCP	DP7**				
11**	15.6	38.5	36" RCP	PR9**, PR10**				
12**	19.6	47.2	36" RCP	PR11, DP8**				



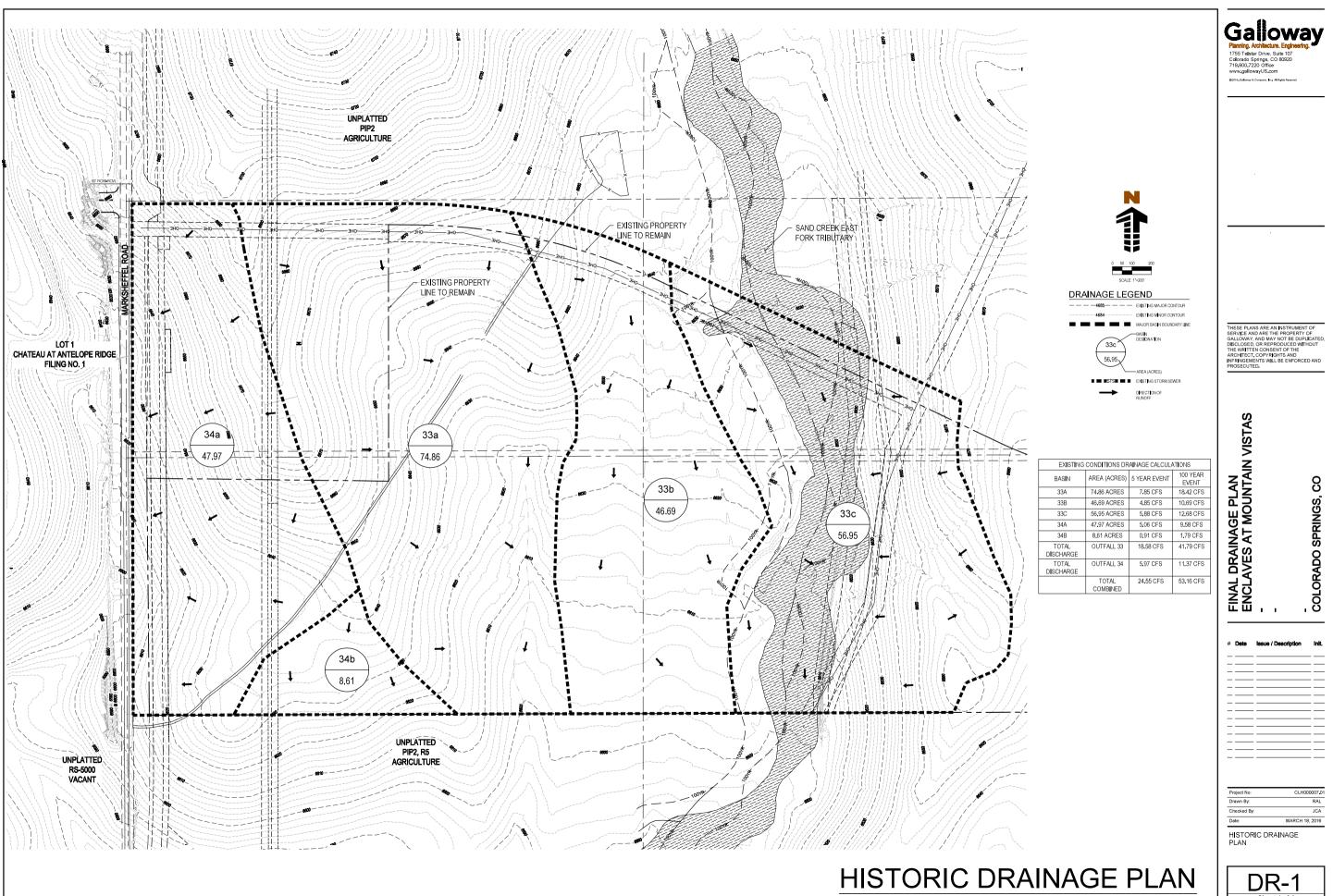
IL CONSULTANTS, INC.

102 E. PIKES PEAK AVE., 5TH FLOOR COLORADO SPRINGS, CO 80903 PHONE: 719.955.5485

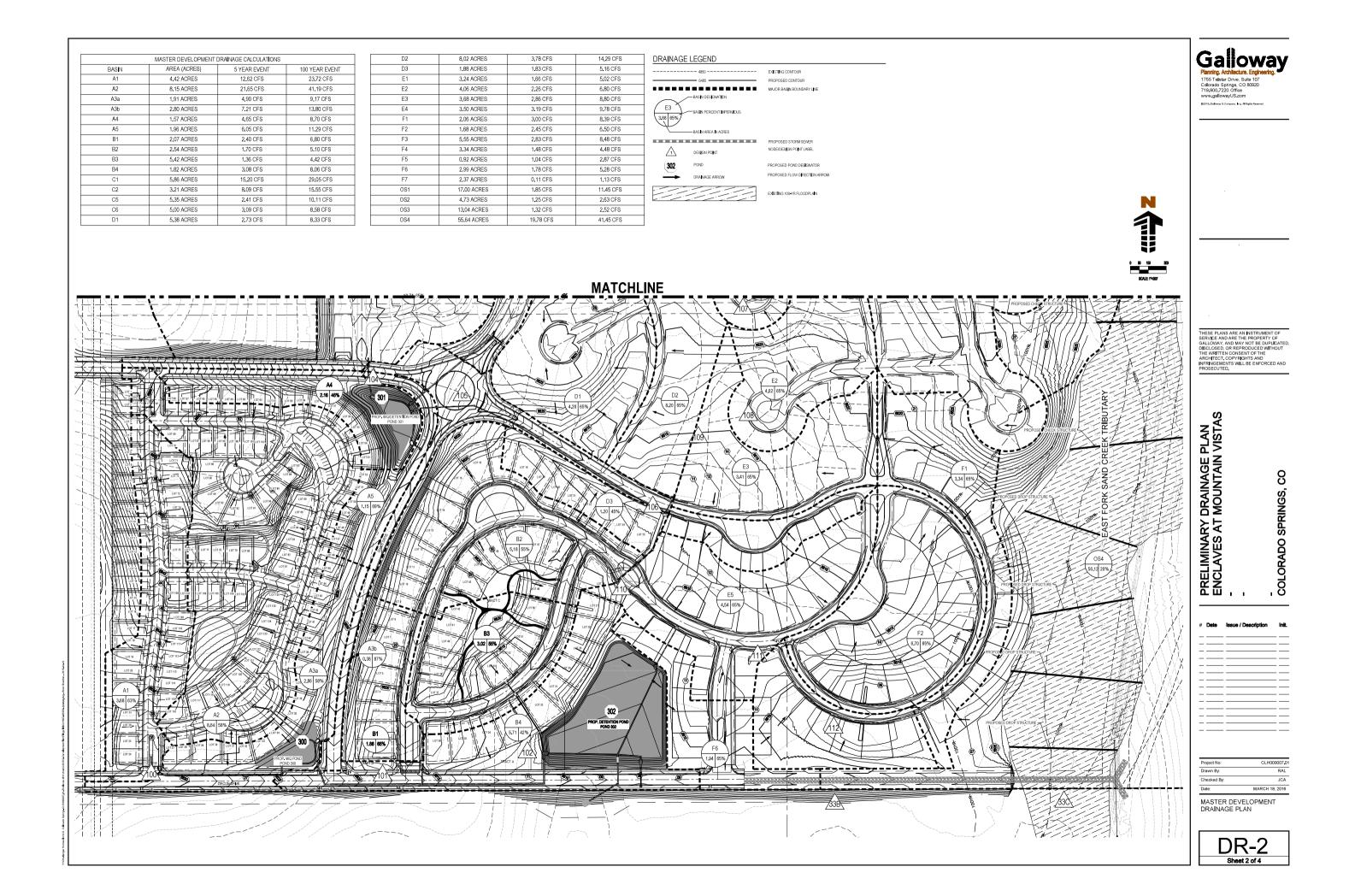
## FALCON TRUCKING FILING NO.1 EINIAL DOAINIACE MAD

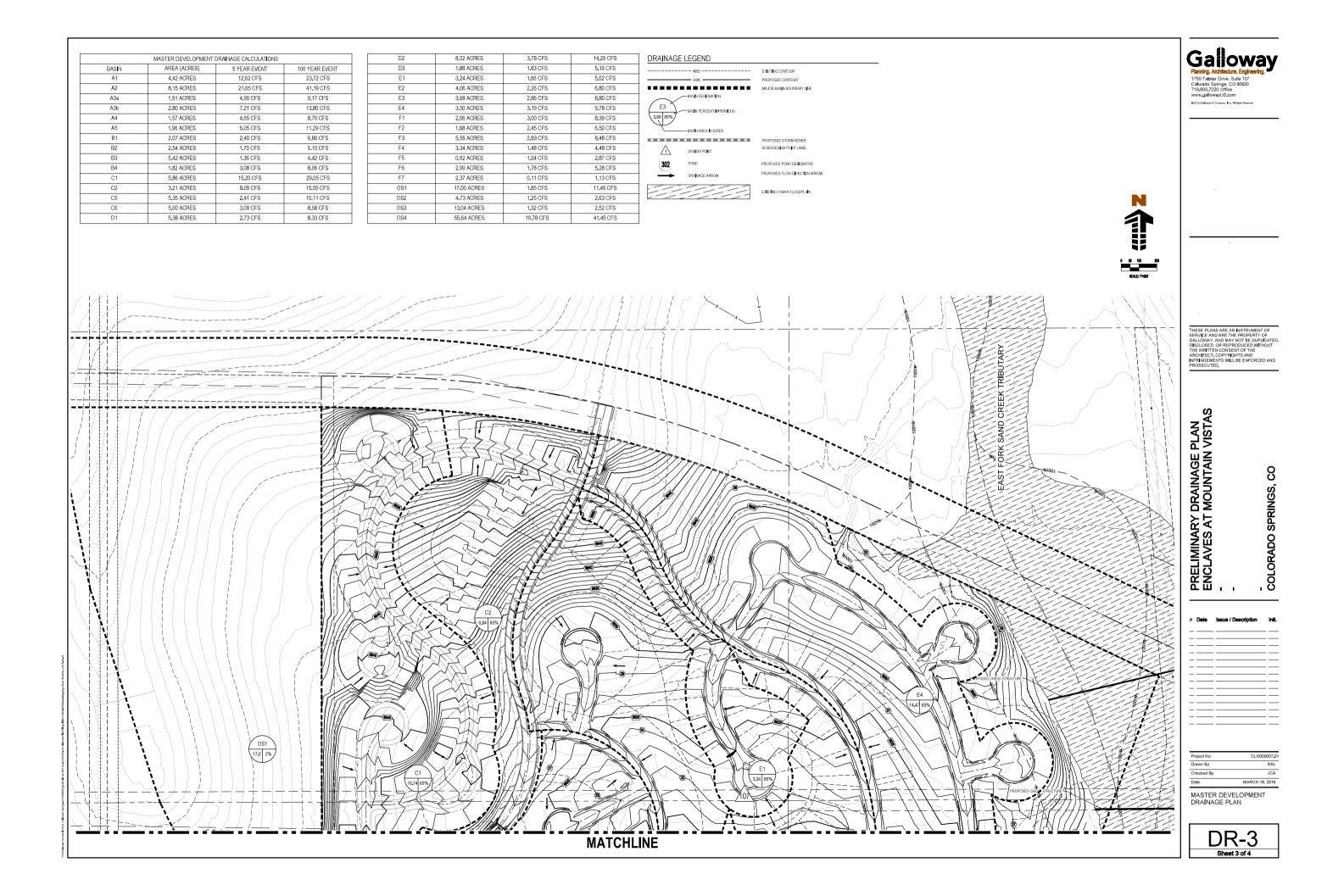
FINAL DRAINAGE MAP					
PROJECT NO. 29-0	D7 SCALE:	DATE: 12-02-202	22		
DESIGNED BY: VA Drawn by: CLP Checked by: VA	DCV VERTICAL:	SHEET 2 OF 2	DM2		

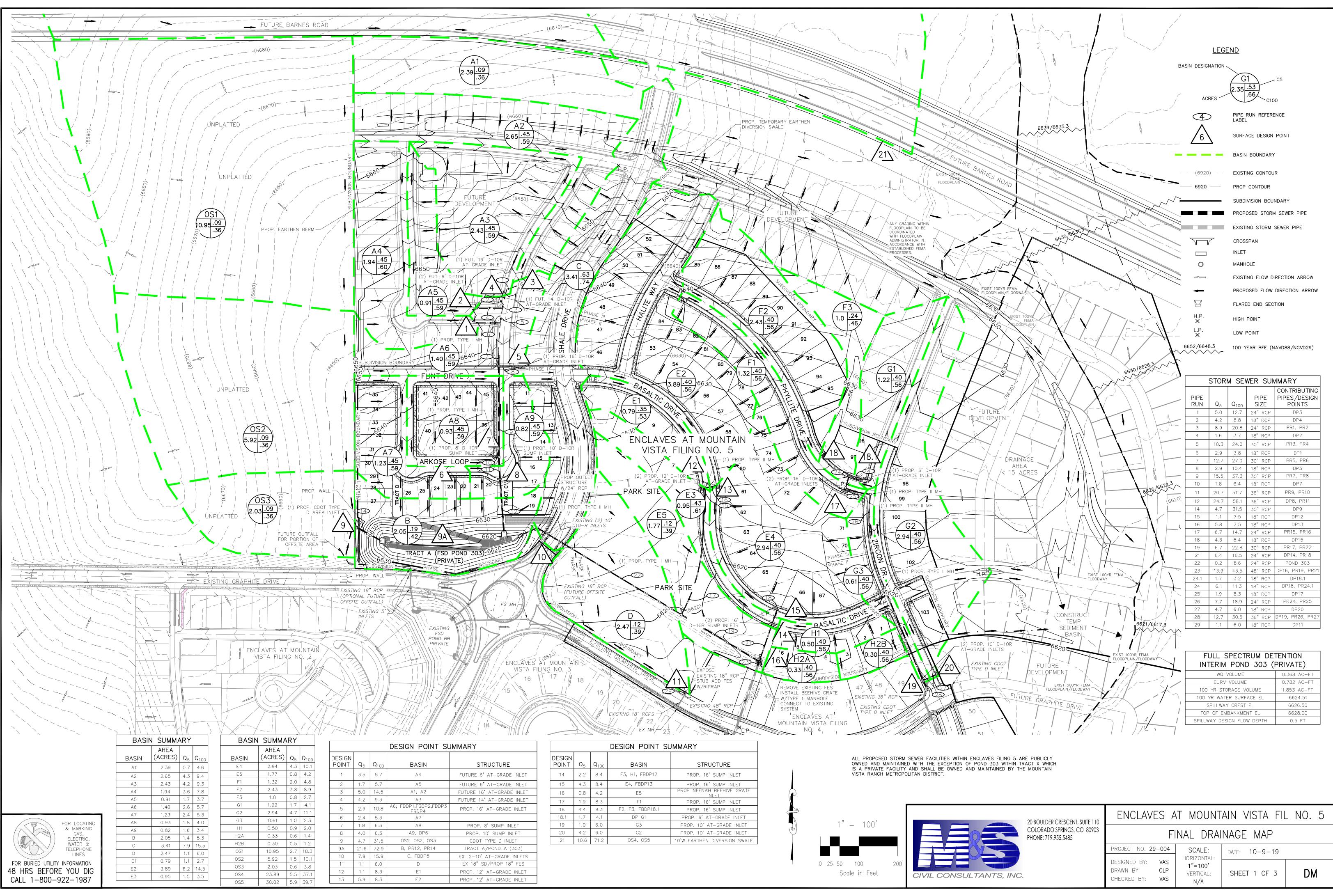
#### **BACKGROUND INFORMATION**



Sheet 1 of 4



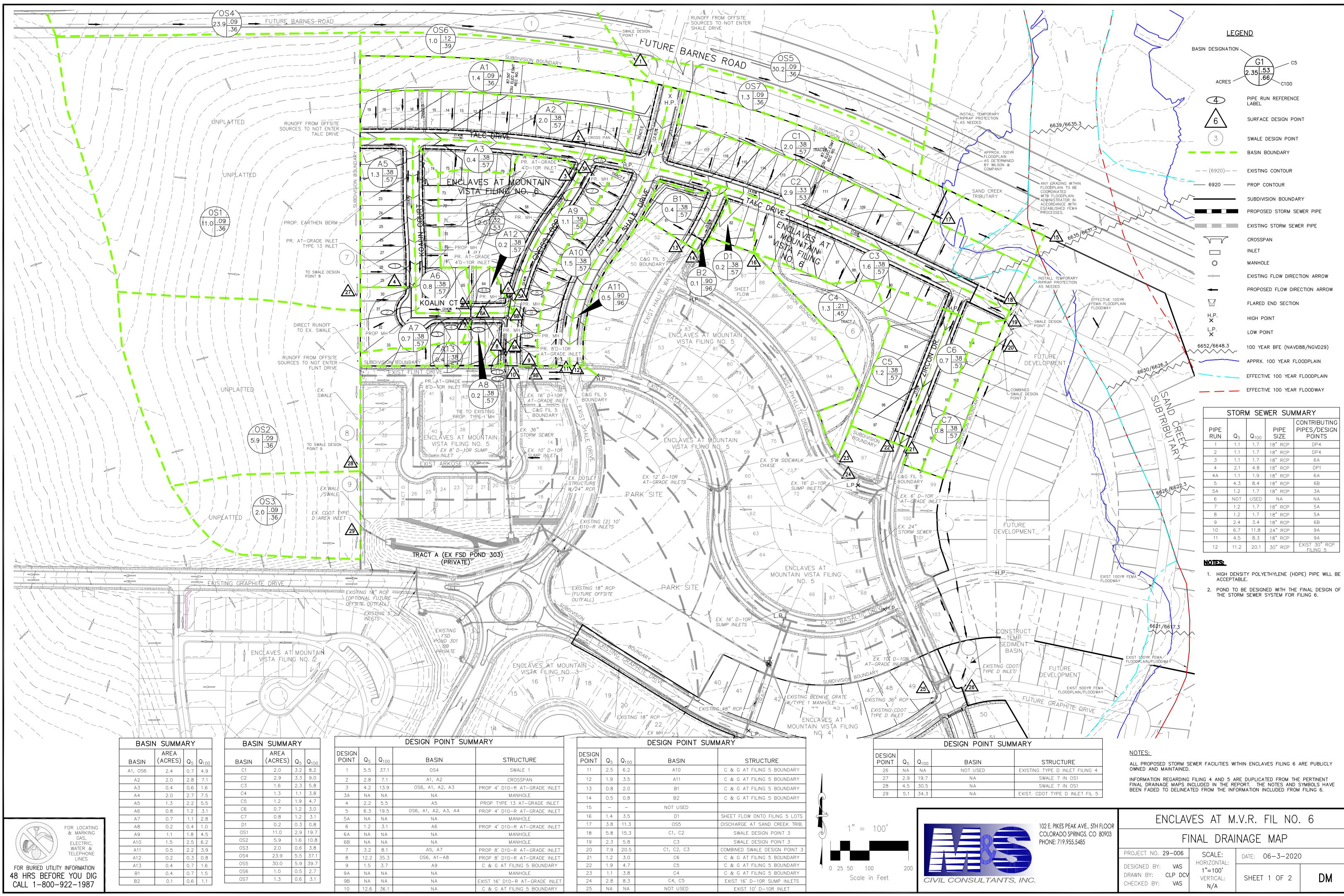




	STRUCTURE
	FUTURE 6' AT-GRADE INLET
	FUTURE 6' AT-GRADE INLET
	FUTURE 16' AT-GRADE INLET
	FUTURE 14' AT-GRADE INLET
3	PROP. 16' AT-GRADE INLET
	PROP. 8' SUMP INLET
	PROP. 10' SUMP INLET
	CDOT TYPE D INLET
	TRACT A/POND A (303)
	EX. 2-10' AT-GRADE INLETS
	EX 18"SD/PROP 18"FES
	PROP. 12' AT-GRADE INLET
	PROP. 12' AT-GRADE INLET

SIGN OINT	$Q_5$	<b>Q</b> <sub>100</sub>	BASIN	STRUCTURE
14	2.2	8.4	E3, H1, FBDP12	PROP. 16' SUMP INLET
15	4.3	8.4	E4, FBDP13	PROP. 16' SUMP INLET
16	0.8	4.2	E5	PROP NEENAH BEEHIVE GRATE INLET
17	1.9	8.3	F1	PROP. 16' SUMP INLET
18	4.4	8.3	F2, F3, FBDP18.1	PROP. 16' SUMP INLET
18.1	1.7	4.1	DP G1	PROP. 6' AT-GRADE INLET
19	1.0	6.0	G3	PROP. 10' AT-GRADE INLET
20	4.2	6.0	G2	PROP. 10' AT-GRADE INLET
21	10.6	71.2	OS4, OS5	10'W EARTHEN DIVERSION SWALE

	20 BOULDER CRESCENT, SUITE 110	ENCLAVES AT MOUNTAIN VISTA FIL NO. 5				
	Colorado Springs, Co 80903 Phone: 719.955.5485		FI	INAL DRAI	NAGE MAP	
		PROJECT NO. 2	9-004	SCALE: HORIZONTAL:	DATE: 10-9-19	
L CONSULTANTS, INC.		DESIGNED BY: DRAWN BY: CHECKED BY:	VAS CLP VAS	1"=100' VERTICAL: N/A	SHEET 1 OF 3	DM



•			
PROJECT NO. <b>29-006</b>	SCALE:	DATE: 06-3-2020	)
DESIGNED BY: VAS DRAWN BY: CLP DC CHECKED BY: VAS	HORIZONTAL: 1"=100' VERTICAL: N/A	SHEET 1 OF 2	DM

BEEN FADED TO DELINEATED FROM THE INFORMATION INCLUDED FROM FILING 6.

CONTRIBUTING

PIPES/DESIGN

POINTS

DP4

DP4

6 A

6A

6B

3A

ΝA

5A

5A

6B

9A

9A

EXIST 30" RCF FILING 5

ALL PROPOSED STORM SEWER FACILITIES WITHIN ENCLAVES FILING 6 ARE PUBLICLY

INFORMATION REGARDING FILING 4 AND 5 ARE DUPLICATED FROM THE PERTINENT FINAL DRAINAGE MAPS INCLUDED IN THE REPORT. THE NOTES AND SYMBOLS HAVE