MASTER DEVELOPMENT DRAINAGE PLAN FOR THE GOLD HILL MESA

Prepared for:
City of Colorado Springs
Department of Public Works
Engineering Division

On Behalf of: Gold Hill Mesa Township

Prepared by:



2925 Professional Place, #200 Colorado Springs, Colorado 80904 (719) 575-0100 fax (719) 575-0208

July 2004

ENGINEER'S STATEMENT:

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City / County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Jorathan Moore, P.E. #34944

DEVELOPER'S STATEMENT:

I, the developer, have read and will comply with all of the requirements specified in this report and plan.

Business Name

 $\mathbf{R}\mathbf{w}$

Title

Address:

GHMT Go Spr. Mga

1040 South 8th St, Suit 101

Filed in accordance with Section 15-3-906 of the Code of the City of Colorado Springs, 1980, as amended.

Circle

City Engineer

Conditions:



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Vicinity Map

FEMA Map 728 & Soils Map

Water Quality Pond – Extended Detention Basin (EDB)



A. INTRODUCTION

The following Master Development Drainage Plan (MDDP) has been prepared for Gold Hill Mesa Township to evaluate existing drainage conditions and conceptually size stormwater management facilities serving the 210-acre site situated within the City of Colorado Springs. The Gold Hill Mesa development is located along and south of Fountain Creek at the southeast corner of 21st Street and Highway 24, approximately 0.25 miles west of Interstate Highway 25 (See Figure 1 – Existing Topography / Drainage Basins). Gold Hill Mesa currently has residential development immediately to the south (Crown Hill Subdivision) and east (Portland Heights Subdivision). Villa de Mesa subdivision is accessed through 21st Street and is surrounded by the Gold Hill Mesa property. At the northwest corner of the site are existing retail buildings in the K&J, Golden Cycle, and Moore's Subdivisions.

The current Gold Hill Mesa development plan looks to transform the highly visible property to a range of mixed uses including commercial, residential, and open space. The redevelopment of Gold Hill Mesa is planned to have 1,699 residential dwelling units, 458,000 square feet of commercial buildings, and 107,000 square feet of office and government buildings (See Figure 4 - Gold Hill Mesa Development Plan).

Soil Conditions

Soils within the Gold Hill Mesa property consist primarily of the soil group "Badland" which originated from gold ore tailings. These tailings were deposited during the operation of the Golden Cycle Mill from 1905-1949. The hillside has severe slopes and is prone to very rapid runoff and has a high potential for erosion. A small percentage of the site consists of the soil group Chaseville-Midway complex. The permeability of this soil group is rapid, but because of the steep slopes of the area, the surface runoff is medium and the erosion potential is moderate to high. The Razor-Midway complex has gently to moderate sloping soils with moderate hazard of erosion. The Ustic Torrifluvents soil group is located adjacent to Fountain Creek and has a moderate to high hazard of erosion.

The soil groups located within the Gold Hill Mesa property are summarized below in Table 1. The information was taken from the El Paso County Soil Survey prepared by the National Resource Conservation Service.

Table 1
Current Hydrologic Soil Groups
(Source: NCRS Soil Survey for El Paso County)

| Map Symbol | Name | Hydrologic Soil Group |
|------------|--|-----------------------|
| 4 | Badland, 0 to 100% slopes | D |
| 18 | Chaseville-Midway complex, 5% to 50% slopes | A/D |
| 75 | Razor-Midway complex, gently sloping to moderately steep | C/D |
| 101 | Ustic Torrifluvents, loamy, 0% to 3% slopes | В |

An excerpt of the soil survey map is provided in the appendices and shows the presence of D soil across 90% of the site and C soils across the remainder.



Topography

The topography of the Gold Hill Mesa property is dominated by the deposition of the gold tailings on the site between 1905 and 1949. Large channels have been formed through the erosion of the hillside toward Fountain Creek. The site drains from the southwest to the northeast with elevations varying from 6000 to 6250 feet above sea level. The top of the hill is relatively flat with slopes varying from 0.5% to 5.0%. The hill slopes steeply towards Fountain Creek at slopes varying from 10.0% to 25.0%. Approximately 85% of the property outfalls directly to Fountain Creek through several drainage basins. The majority of the remainder of the site on the southeast corner drains off the property through a natural channel to Fountain Creek downstream of the Gold Hill Mesa property. A fraction of the southwest corner of the site is part of the Bear Creek Drainage Basin.

As described above, the development will be phased and consist of a mix between commercial, residential, and open space. A Voluntary Cleanup Application (VCUP) was made on June 6, 2000 and appended on June 12, 2002. This document describes the actions that will be taken to reduce the impact of development in the area. The VCUP has been approved by the State of Colorado on December 20, 2002, and this approval letter is included in the appendix.

A *Preliminary Geological Hazards Evaluation and Preliminary Geotechnical Investigation* dated October 9, 2002, was generated by CTL/Thompson. This drainage report agrees with its basic assessment with regard to drainage. It is the intent of this development to convey stormwater to Fountain Creek via underground conduits and to minimize ponding areas and as a result, limit infiltration.

The steep slopes and soil properties have contributed to a large amount of erosion on the face of the hill. Deep cuts into the hillside are readily visible from Highway 24 and will be addressed as part of the development. The material management program will be established by others and is outside the scope of this report. However, it is our understanding that non-paved areas will be topped with 2.5 feet of clean fill to allow for vegetation and help to mitigate the erosion problems. Any detention ponds will be located outside the limits of the gold tailings. Detailed grading plans will be provided for the hillside development at a later stage.

B. HISTORIC DRAINAGE

The site has historically drained to Fountain Creek, either directly or indirectly across an adjacent property. A small section (2.6 acres) of the property is within the Bear Creek Drainage Basin and drains to the south into 21st Street into an existing storm sewer. The remainder of the site is broken into several drainage basins that outfall into Fountain Creek. The existing drainage basins are delineated on Figure 1 – Gold Hill Mesa: Existing Topography / Drainage Basins.

The Villa de Mesa Subdivision drains to the northeast corner of the property and outfalls onto the Gold Hill Mesa Property. The only drainage report available at the City of Colorado Springs for this area is the **Drainage Report: Villa de Mesa** prepared by R. Keith Hook & Assoc. on December 29, 1966. This report covers 328 acres including Gold Hill Mesa and Crown Hill Mesa Subdivision. Currently, the development encompasses 9.6 acres. Because of lack of information on the flows for the developed area, the contributing flows were calculated using the same criteria as the proposed area.

The majority of the site is not located within a 100-year floodplain as delineated by the Federal Emergency Management Agency's (FEMA) Flood Insurance Rate Map Panel Number 08041C0728 F,



dated March 17, 1997. Because of the property's location adjacent to Fountain Creek, the area along the creek is located within the floodplain. The floodplain is shown on Figure 2 – Gold Hill Mesa: 100 / 500 - Yr Floodplain Delineated.

Improvements to Fountain Creek are currently under construction immediately downstream of the Gold Hill Mesa property. The improvements include the acquisition of property along the south side of Fountain Creek and are planned to alleviate the historical flooding problems in the Portland Heights Subdivision. Our understanding of City policy, is that no improvements will be required of Fountain Creek with the development of Gold Hill Mesa. However, improvements to Fountain Creek will be done to protect structures such as homes or commercial buildings built as part of the development. Any development along Fountain Creek within Gold Hill Mesa will be done outside the 100-Yr floodplain and floodway and any alteration of the floodplain will require consulting the City's Flood Plain Administrator and following the appropriate procedures for revising the FEMA map.

| Table 2 |
|--|
| Existing Basin Hydrology: 100-Year Storm Event (Rational Method) |

| Basin | Imperviousness | C | C | Area | Q ₁₀₀ |
|--------|----------------|------|------|-------|------------------|
| | (%) | 10 | 100 | (Ac) | (cfs) |
| 101 | 0 | 0.30 | 0.45 | 17.60 | 49.10 |
| 102 | 0 | 0.30 | 0.45 | 6.80 | 27.54 |
| 103 | 0 | 0.30 | 0.45 | 27.70 | 56.09 |
| 104 | 0 | 0.30 | 0.45 | 84.80 | 137.38 |
| 105 | 0 | 0.30 | 0.45 | 49.80 | 84.04 |
| 106 | 0 | 0.30 | 0.45 | 27.20 | 47.74 |
| 107 | 0 | 0.30 | 0.45 | 2.06 | 6.49 |
| E1 | 95 | 0.90 | 0.95 | 9.90 | 66.00 |
| Totals | - 4 - | · | | | |

C. DESIGN CRITERIA

The City of Colorado Springs recommends the use of the Rational Formula for basins smaller than 100 acres. This methodology was used to analyze the hydrology on the Gold Hill Mesa property. The rainfall data and other design information were taken from the City of Colorado Springs Drainage Criteria Manual. The following tables / figures are included in the Appendix:

- 1. Intensity-Duration-Frequency Curves
- 2. Recommended Average Runoff Coefficients and Percent Impervious
- 3. Overland Flow Curves
- 4. Estimate of Average Flow Velocity for Use with the Rational Formula

For existing conditions, the runoff coefficient was taken from Table 5-1 of the Colorado Springs Drainage Criteria Manual for "Undeveloped Area-Greenbelts, Agricultural" and soil group C&D. As shown in Table 2, the coefficients used for the 5-year and 100-year event were 0.30 and 0.45. Times of concentrations were based on tables from the City of Colorado Springs for Overland Flow Curves for a maximum of 1000 foot run. The remainder of the time of concentration was calculated using a defined waterway.



The runoff coefficients were determined based on the proposed land uses. While there are large concentrations of open space on the high end of the site, a composite coefficient of 0.80 and 0.70 was used for the 100-year and 5-year storm, respectively. A percent impervious of 80% was used for the commercial / office areas and 70% for the residential areas.

The report analyzes the hydrological impacts of the development to determine the effects of the 5-year (Minor) and the 100-year (Major) storm events and the infrastructure required to convey the storm runoff.

Table 3 5-Year & 100-Year Storm Runoff (Proposed)

| Basin | Area (Ac) | C ₅ | C ₁₀₀ | Tc (min) | l ₅ | I ₁₀₀ | Q_5 | Q ₁₀₀ |
|-------|-----------|----------------|------------------|----------|----------------|------------------|-------|------------------|
| А | 162.92 | 0.73 | 0.80 | 15.42 | 3.5 | 6.1 | 416.3 | 795.1 |
| В | 55.68 | 0.70 | 0.76 | 12.5 | 3.7 | 6.7 | 144.2 | 283.5 |

D. DRAINAGE PLAN

The drainage plan for Gold Hill Mesa addresses the current erosion problems that exist at the proposed site. As mentioned earlier, the VCUP discusses to some degree the material management program that includes the placement of a "viable barrier between residual tailings and the end user of the site." This plan will help to reduce the amount of surface runoff by directing runoff on surface streets and underground conveyance systems. Fountain Creek will be protected from further erosion caused by runoff from Gold Hill Mesa by using several locations to outfall the developed flows. Structures will be designed so as to dissipate the high velocities of runoff prior to entering Fountain Creek. The proposed hydrology including basins, outfall locations, and trunk storm sewer size and locations are shown on Figure 3. Details of outfalls and energy dissipaters will be done as the design of the development progresses.

Basin A consists of 162.92 acres along the western side of the over-all development. This basin includes flows from Villa de Mesa Subdivision and the future commercial area. Based on this basin information, the Water Quality Pond (WQP) #1 needs to be 1.07 acres, see appendix for calculation. A diversion box will be placed outside the WQP to limit the amount of storm water that enters the pond to the 5-Year storm event threshold. All remaining storm water will be routed around the pond and will discharge into Fountain Creek.

Basin B consists of 55.68 acres along the eastern side of the over-all development. This basin will only include flows from this site. Based on this basin information, the Water Quality Pond (WQP) #2 needs to be 0.31 acres, see appendix for calculation. A diversion box will be placed out side the WQP to limit the amount of storm water that enters the pond to the 5-Year storm event threshold. All remaining storm water will be routed around the pond and will discharge into Fountain Creek.

E. STORMWATER MANAGEMENT

The two goals at the Gold Hill Mesa development are to provide safe conveyance of runoff and to protect the water quality. The first item is accomplished by properly sizing the conveyance elements to protect the existing and proposed development. The second goal is generally accomplished through a multi-level, multi element approach of what is termed best management practices (BMPs).



Traditionally, BMP's include detention ponds, elements of detention ponds such as the outlet works systems, smaller storage ponds known as water quality ponds, and grass swales. These elements and others will be incorporated into the Gold Hill Mesa drainage plan. A recent concept will also be employed to the extent practicable: Minimization of Directly Connected Impervious Areas (DCIA). This is a simple concept, which is to direct runoff through vegetated areas in order to provide for natural filtering and treatment of containments in the runoff. Implementation of DCIA has only a negligible affect on major storm runoff peaks, but can provide significant improvements of water quality from urban areas.

The majority of the Gold Hill Mesa development does not lend itself to the most common type of BMP. The presence of gold tailings prevents the use of water quality and detention ponds to provide treatment of water prior to outfall. In areas where the gold tailings are present, the Stormceptor product that treats water by separating the stormwater from oil, sediment, and other pollutants from urban runoff will be widely used on this development. Where possible, typical water quality ponds will be constructed to treat the runoff prior to outfall to Fountain Creek.

F. CONCLUSION

In summary, the Gold Hill Mesa development will convey the 100-yr flows within proposed roadways and underground drainage facilities on the southern, high end of the development. Due to steep slopes and erosion potential, the 100-yr flows will be conveyed down the steep slopes completely underground. Several outfall structures will release directly to Fountain Creek with a total flow of 1081 cfs. This concept will have to be examined further to determine possible impacts to the existing subdivision. All outfall structures will also serve as energy dissipaters so as to reduce to the erosion problems within Fountain Creek. As further refinement of the grading and development plan take place, the method of conveyance may be adjusted to provide more surface drainage.

The Extended Detention Basin Pond #1 will be built with the first Filing and no development will occur in Basin B until the Extended Detention Basin Pond #2 is built. No development in the vicinity of Fountain Creek will be allowed until improvements or prudent line/build to line has been established.

This report attempts to address comments made to the MDDP dated April 2004. It represents the ongoing effort in the redevelopment of the Gold Hill Mesa property. We welcome any additional comments the City of Colorado Springs may have with regards to the drainage issues of this area.

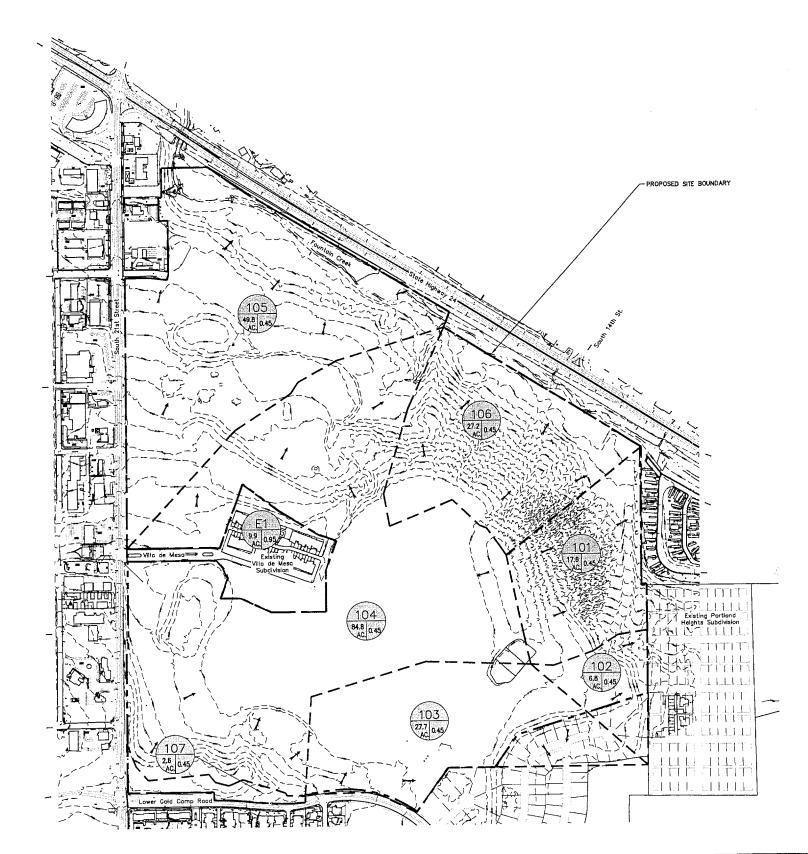


G. REFERENCES

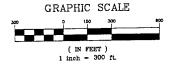
- 1. <u>Soil Survey of El Paso County Area, Colorado</u>, United States Department of Agriculture Soil Conservation Service, June 1981.
- 2. <u>Master Development Drainage Plan for Crown Hill Mesa Subdivision</u>, Associated Design Professionals, Inc., November 15, 1995.
- 3. Voluntary Cleanup Application (VCUP), Spectrum Services, June 6, 2000, and June 12, 2002.
- 4. <u>Villa de Mesa: Preliminary Drainage Report</u>, R. Keith Hook & Assoc., December 29, 1966.
- 5. <u>Fountain Creek Drainage Basin Planning Study</u>, Volume 1, Muller Engineering Company, Inc., July 1994.
- 6. <u>Drainage Study of the Bear Creek Basin</u>, Lincoln DeVore Engineers, December 1980.
- 7. Federal Emergency Management Agency's (FEMA) Flood Insurance Rate Map Panel Number 08041C0728 F, dated March 17, 1997

H. APPENDIX









LEGEND

- EXISITING BASIN BOUNDARY PROPOSED PROPERTY LINE EXISTING FLOW DIRECTION ARROW

> - BASIN DESIGNATION $\langle xx-x \rangle$

- "C" COEFFICIENT (100 YR) - BASIN AREA (ACRES)

REFERENCE DRAWINGS X-EX-TOPO X-TITLE X-EX-FEAT BENCHMARK DATA(ELEV.)_ NAME: S:\03.028.007(Phase1)\dwg\DEVELOP\STRM\MODP\EXTP1.dwg
PCP: Matrix.ctb
PLOT DATE: Wed Apr 28, 2004 11:34cm (DATUM)_ (DESCRIPTION/LOCATION)_



FOR AND ON BEHALF OF MATRIX DESIGN GROUP, INC.

Matrix Design Group, Inc.
Integrated Design Solutions

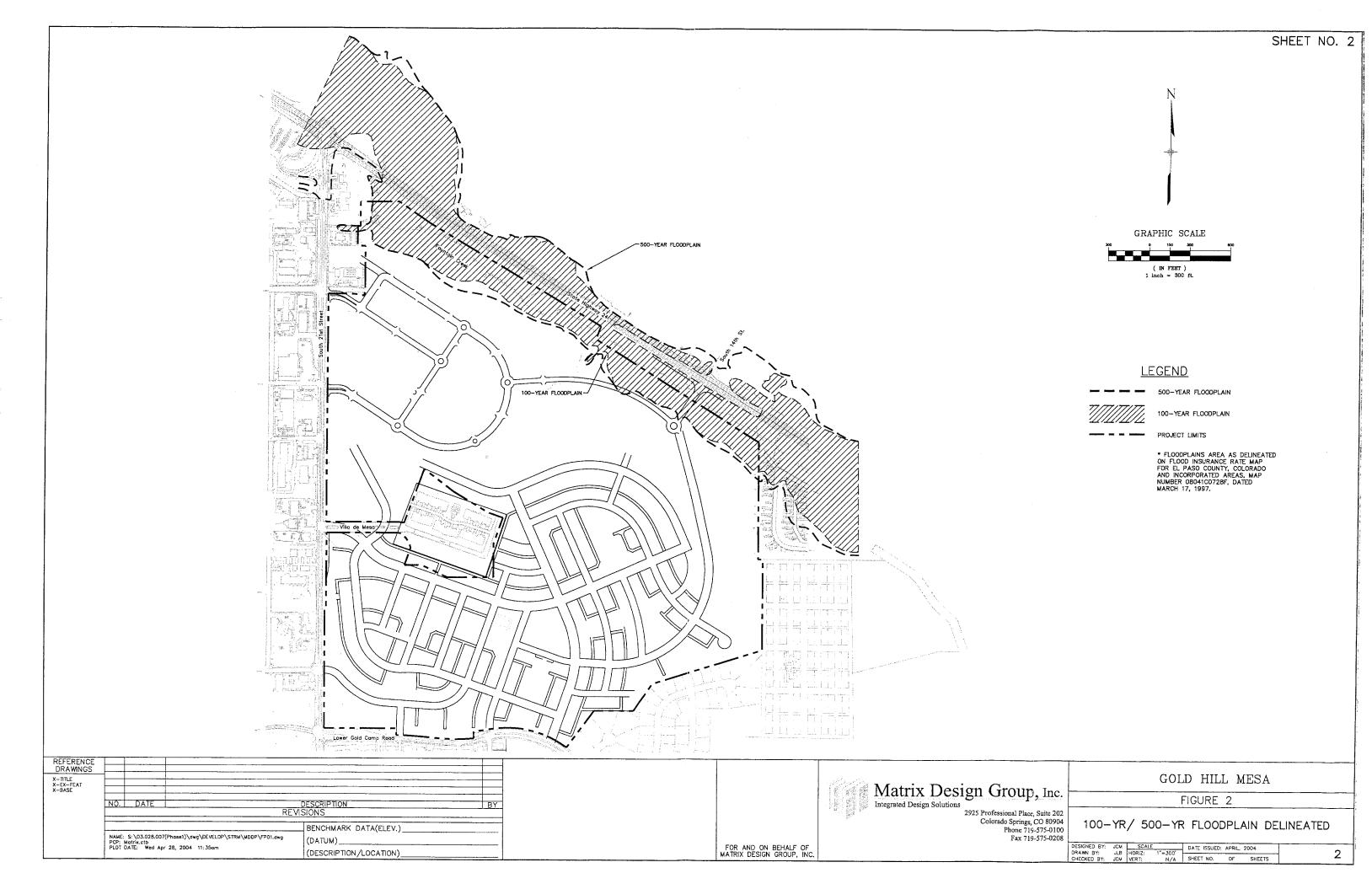
2925 Professional Place, Suite 202 Colorado Springs, CO 80904 Phone 719-575-0100 Fax 719-575-0208

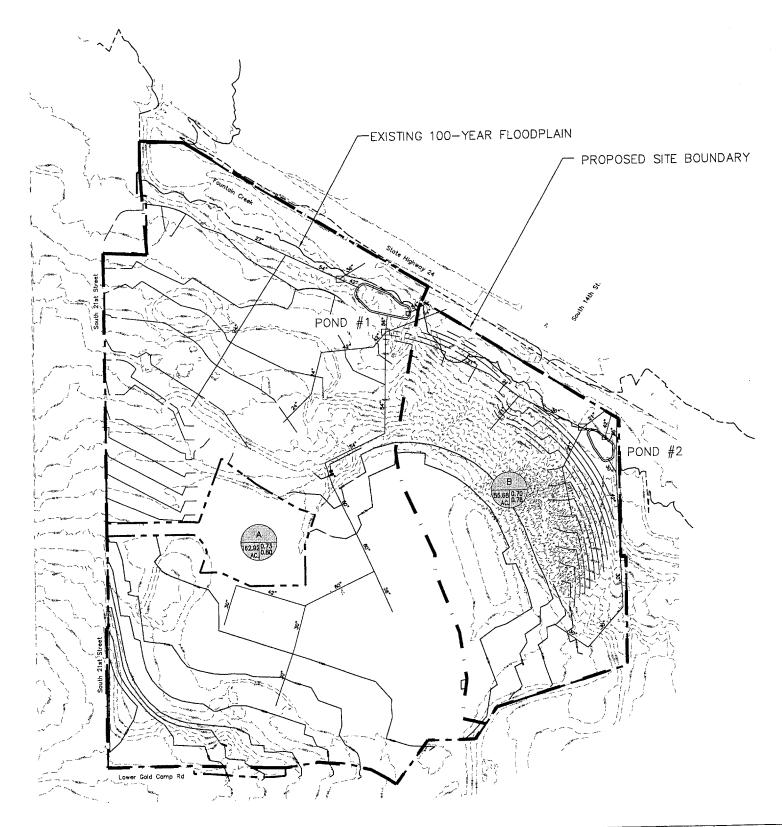
GOLD HILL MESA

FIGURE 1

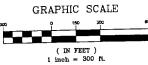
EXISTING TOPOGRAPHY/ DRAINAGE BASINS

| SIGNED BY: | JCM | SCALE | 45 700' | DATE | ISSUED: | APRIL, | 2004 | |
|------------|-----|--------|---------|-------|---------|--------|---------|---|
| RAWN BY: | | HORIZ: | 1"=300" | 0.155 | | 05 | SHEETS | l |
| ECKED BY: | JCM | VERT: | N/A | SHEE. | I NO. | OF | SUEE 12 | i |

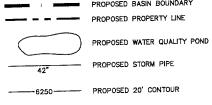


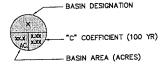






LEGEND





| REFERENCE DRAWINGS | | |
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| X-EX-TOPO X-TITLE X-EX-FEAT X-BASE X-PP-TOPO | NO. DATE RE | DESCRIPTION BY VISIONS |
| | NAME: S:\03.028.007(Phose1)\dwg\0EVELOP\STRM\M0DP\P801.dwg PCP: Matrix.ctb PLOT DATE: Mon Jul 12, 2004 10:31am | BENCHMARK DATA(ELEV.) (DATUM) (DESCRIPTION/LOCATION) |



FOR AND ON BEHALF OF MATRIX DESIGN GROUP, INC.

Matrix Design Group, Inc.
Integrated Design Solutions
2925 Professional Place, Suite 202

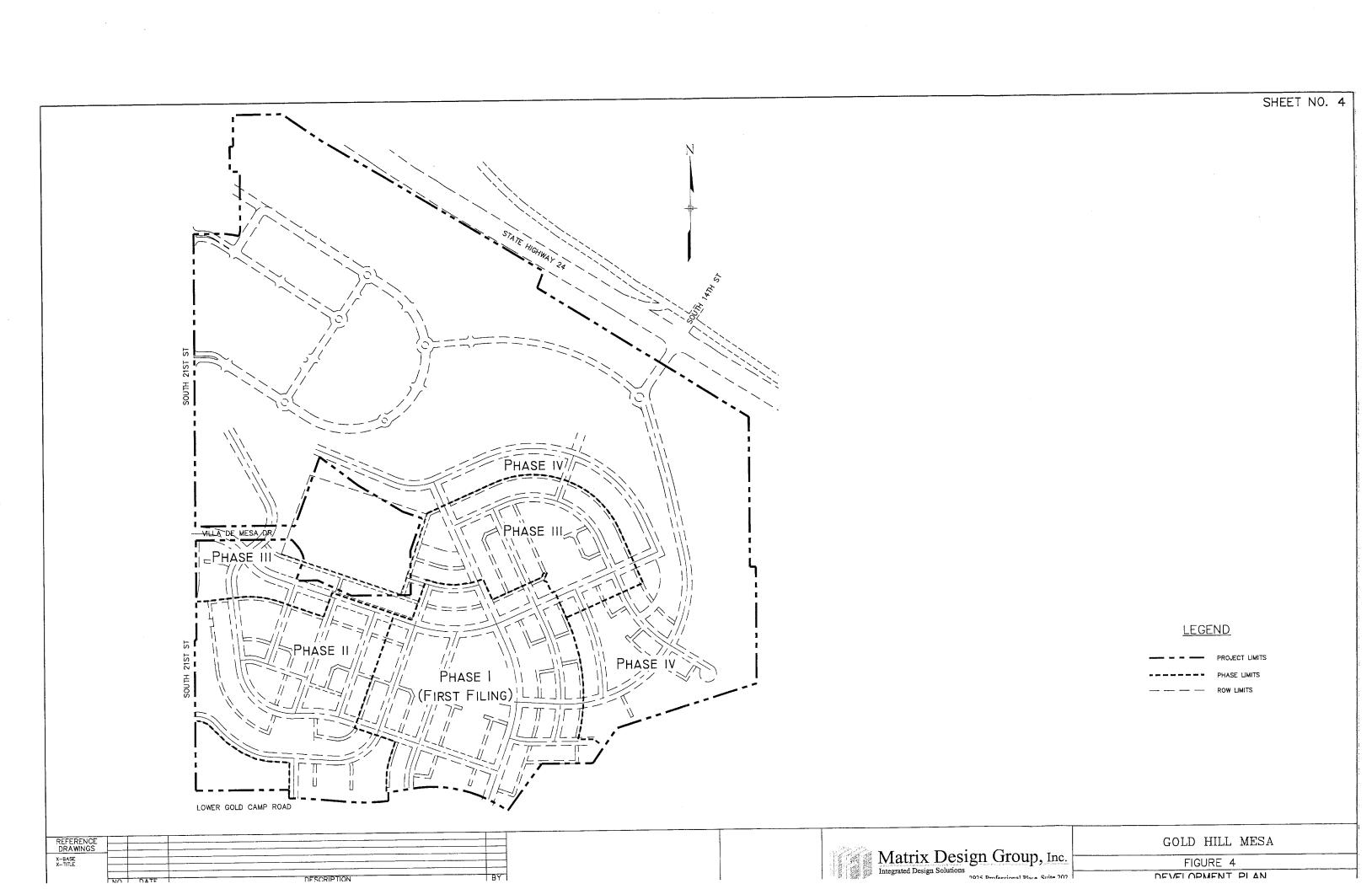
2925 Professional Place, Suite 202 Colorado Springs, CO 80904 Phone 719-575-0100 Fax 719-575-0208

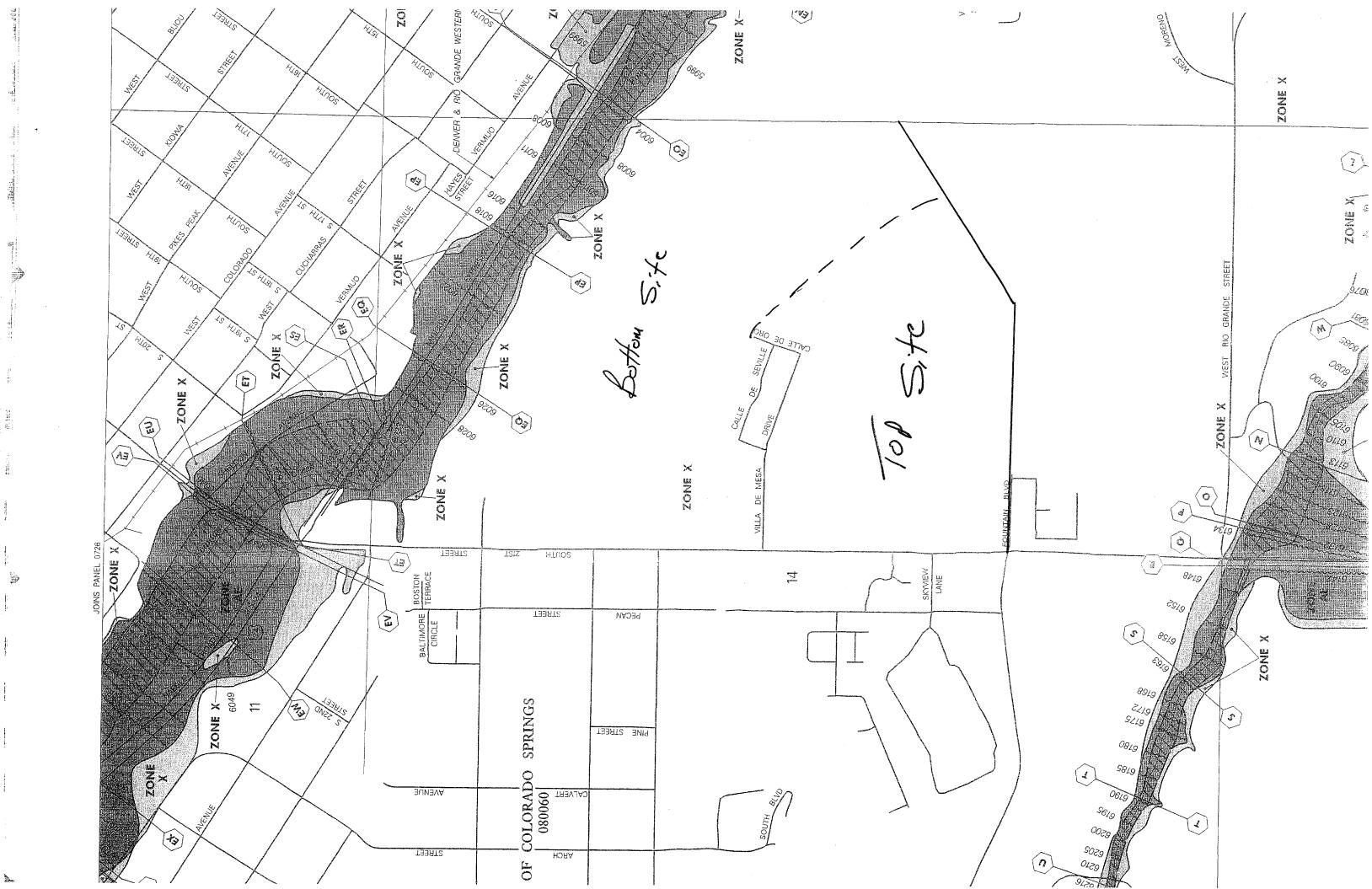
| GOLD | HILL | MESA |
|------|-------|------|
| FIG | URE 3 | 5 |

PROPOSED BASINS

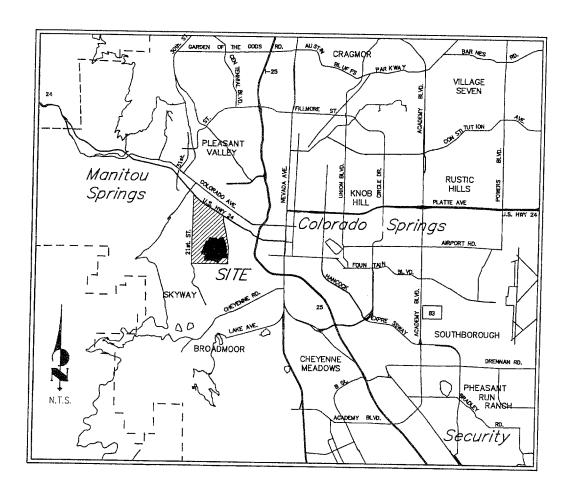
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| | JCM | SCALE | | DATE | ISSUED: | APRIL, | 2004 |] |
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| | | | | | | | | |





GOLD HILL MESA VICINITY MAP



Bill Owens, Governor Douglas H. Benevento, Acting Executive Director

Dedicated to protecting and improving the health and environment of the people of Colorado

7195750208

4300 Cherry Creek Dr. 5. Denver, Colorado 80246-1530 Phone (303) 692-2000 TDD Line (303) 691-7700 Located in Glendale, Colorado

Laboratory and Radiation Services Division 8100 Lowry Blvd. Denver, Colorado 80230-6928 (303) 692-3090

http://www.cdphe.state.co.us

Colorado Department of Public Health and Environment

December 20, 2002

Mr. Robert Willard ERSH, L.L.C. 1040 S 8th ST Suite 101 Colorado Springs, CO 80906

Re: Voluntary Cleanup Plan Approval, Gold Hill Tailing Pile, 21st ST and Highway 24, Colorado Springs, Colorado.

Dear Mr. Willard:

The Colorado Department of Public Health and Environment (the "Department") has reviewed the voluntary cleanup plan submitted on behalf of ERSH, L.L.C. (the Applicant) concerning the property identified in the application and known as the Gold Hill Tailing Pile, 21" ST and Highway 24, Colorado Springs, Colorado (the site). This review was limited to the materials submitted by the Applicant, as well as those materials required by 25-16-304(2) C.R.S.

Based on this review the Department has concluded that, if fully and properly implemented, the plan will attain a degree of cleanup and control of hazardous substances and petroleum products, such that the property does not present an unacceptable risk to human health or the environment based on the property's proposed future use which is mixed use, substantially similar to Figure 2 of the application (Conceptual Master Plan I).

In accordance with the Voluntary Cleanup and Redevelopment Act 25-16-301 to 311, C.R.S., the Department hereby approves the voluntary cleanup plan submitted by the Applicant for the property identified in the application and located near 21" ST and Highway 24 in Colorado Springs, Colorado. It is the opinion of the Colorado Department of Public Health and Environment that upon completion of the voluntary cleanup plan no further action is required to assure that this property, when used for the purposes identified in the voluntary cleanup plan (mixed use, substantially similar to Figure 2 of the application [Conceptual Master Plan II), is protective of existing and proposed uses and does not pose an unacceptable risk to human health or the environment at the site.

The approval of the voluntary cleanup plan by the Department, and the Department's conclusions and opinions relating thereto, apply only to conditions on the property and state standards that exist at the time of submission of, and which were addressed in the voluntary cleanup plan application. The submission of any materially misleading information by the Applicant in the context of a voluntary cleanup plan shall render the Department's approval of the plan void. Also, failure of the Applicant to materially comply with the voluntary cleanup plan shall render the Department's approval of the plan void.

Mr. Robert Willard December 20, 2002 Page 2

Further, if the voluntary cleanup plan is not initiated within twelve months after approval by the Department, or completed within twenty-four months after approval or within a Department approved extension for completion of the voluntary cleanup plan, the approval shall lapse, and reapplication and Department approval pursuant to 25-16-306(4), C.R.S. is required prior to implementation of the lapsed voluntary cleanup plan.

Within forty-five days after completion of the voluntary cleanup described in the plan approved by the Department, the Applicant shall provide to the Department a certification from a qualified environmental professional that the voluntary cleanup plan has been fully implemented. Any person who fails after initiation of an approved voluntary cleanup plan, to fully and properly implement the plan, may be required by the Department to take further action, provided such action is authorized or required under applicable state laws and regulations.

The Applicant shall comply with all applicable federal, state, and local laws or regulations and shall obtain all necessary approvals or permits to conduct the activities required by the voluntary cleanup plan. The Department makes no representation with respect to approvals or permits required by federal or local laws or regulations or state laws or regulations other than the Voluntary Cleanup and Redevelopment Act.

Further, the Department shall not be liable for any injuries or damages to persons or property resulting from acts or omissions of the Applicant or those acting for or on behalf of the Applicant, including its officers, employees, agents, successors, representatives, contractors, or consultants in carrying out the activities required by the voluntary cleanup plan. Nothing in the Department's approval of the voluntary cleanup plan, or the Department's conclusions or opinions relating thereto, shall constitute an express or implied waiver of sovereign immunity otherwise applicable to the Department, its employees, agents, or representatives.

Nothing in this letter shall be construed to limit the Department's authority, and the Department reserves all rights and authorities to bring any action pursuant to applicable state laws or regulations.

If you have any questions, please call me at (303) 692-3449.

F Walley

7195750208

Sincerely.

Mark E. Walker

Voluntary Cleanup Program

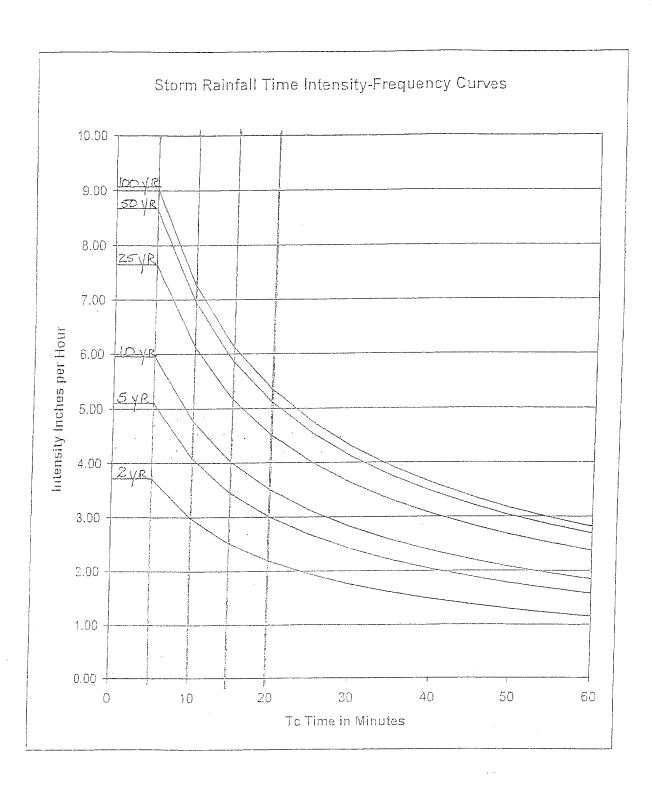
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Sandy Friedman, El Paso County Health Dept. James Mayerl, City of Colorado Springs Planning Dept.

TABLE 5-1
RECOMMENDED AVERAGE RUNOFF COEFFICIENTS AND PERCENT IMPERVIOUS

| | | | | "C" | |
|---|------------|------|--------------|--------------|-----------------|
| | | | FRE | QUENCY | |
| LAND USE OR | PERCENT | | 10 | | 00 |
| SURFACE CHARACTERISTICS | IMPERVIOUS | A&B* | C&D* | A&B* | <u>C&D*</u> |
| Business | | | - | | |
| Commercial Areas | 95 | 0.90 | 0.90 | 0.90 | 0.90 |
| Neighborhood Areas | 70 | 0.75 | 0.75 | 0.80 | 0.80 |
| Residential | | 0.50 | 0 70 | 0.70 | 0.80 |
| 1/8 Acre or less | 65 | 0.60 | | | |
| 1/4 Acre | 40 | | | 0.60 0.55 | |
| 1/3 Acre | 30 | | 0.50 0.45 | | 0.55 |
| 1/2 Acre | 25 | | 0.40 | | 0.50 |
| 1 Acre | 20 | 0.30 | U . 4: U | U. ** U | .0.50 |
| Industrial | 2.0 | 0.70 | 0.70 | 0.80 | 0.80 |
| Light Areas | 80 90 | 0.80 | 0.80 | 0.90 | 0.90 |
| Heavy Areas | 30 | U.OU | 0.00 | | |
| Parks and Cemeteries | 7 | 0.30 | 0.35 | | 0.60 |
| Playgrounds | 13 | 0.30 | | | 0.65 |
| Railroad Yard Areas | 4 O | 0.50 | 0.55 | 0.60 | 0.65 |
| Undeveloped Areas | | | | | |
| Historic Flow Analysis- Greenbelts, Agricultural | 2 | 0.15 | 0.25 | 0.20 | 0.30 |
| Pasture/Meadow | O | 0.25 | 0.30 | 0.35 | 0.45 |
| Forest | ŏ | 0.10 | | 0.15 | 0.20 |
| Exposed Rock | 1.00 | 0.90 | 0.90 | 0.95 | 0.95 |
| Offsite Flow Analysis | 4.5 | 0.55 | 0.60 | 0.65 | 0.70 |
| (when land use not define | eđ) | | | | |
| Streets | | | | | |
| Paved | 100 | 0.90 | 0.90 | 0.95 | 0.95 |
| Gravel | 80 | 0.80 | 0.80 | 0.85 | 0.85 |
| Drive and Walks | 100 | 0.90 | 0.90 | 0.95 | |
| Roofs | 90 | 0.90 | 0.90 | 0,95 | |
| Lawns | 0 | 0.25 | 0.30 | 0.35 | 0.45 |

^{*} Hydrologic Soil Group



Rainfall Depth - Duration - Frequency Table derived from Rainfall Atlas III for Colorado Resource: Guo, James C.Y., (2001) "Urban Storm Water Modeling", Chapter 5: Runoff Prediction for Small Catchment, published by Auraria Campus Book Company, University of Colorado at Denver, Denver, Colorado.

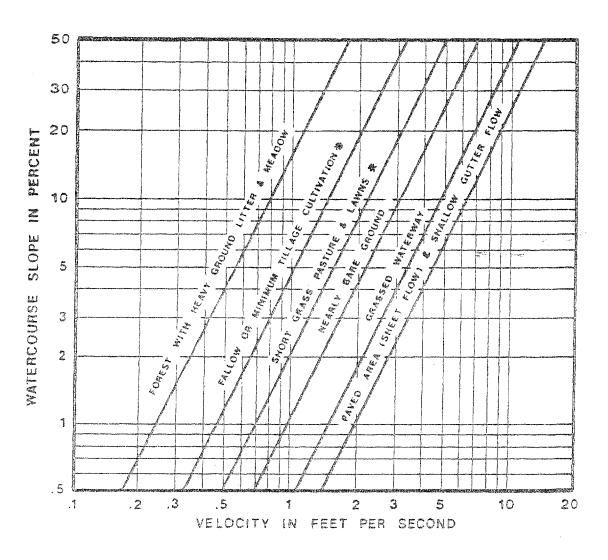
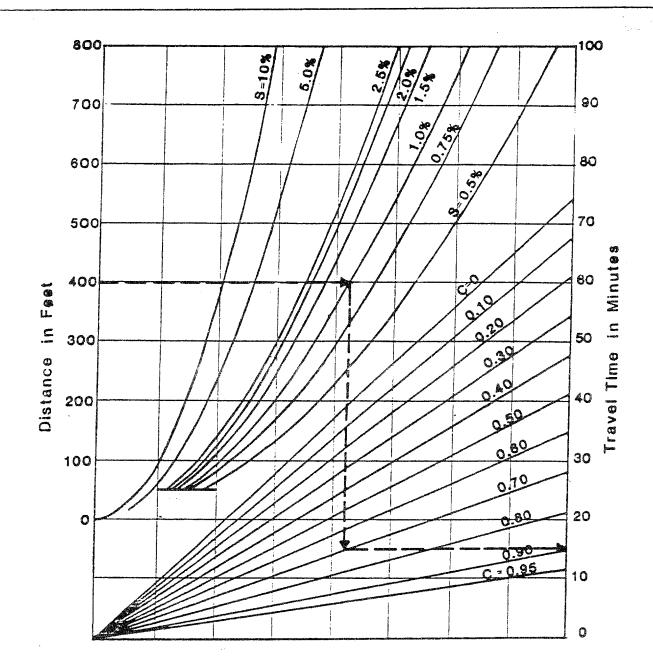


FIGURE RO-1
Estimate of Average Overland Flow Velocity for Use With the Rational Formula.



REFERENCE: Wright - McLaughlin Engineers, Urban Storm Drainage Criteria Manuai, Vol. 1,

Denver Regional Council of Governments, Denver, Co. 1977



The City of Colorado Springs / El Paso County
Drainage Criteria Manual

OCT. 1987

Figure

Overland Flow Curves

5-2

5

5-10

NATIONAL FLOOD INSURANCE PROGRAM

FRM

FLOOD INSURANCE RATE MAP

EL PASO COUNTY, COLORADO AND INCORPORATED AREAS

PANEL 728 OF 1300

(SEE MAP INDEX FOR PANELS NOT PRINTED)

CONTAINS: COMMUNITY

NUMBER PANEL SUFFIX

COLORADO SPRINGS, CITY OF EL PASO COUNTY, UNINCORPORATED AREAS

080059

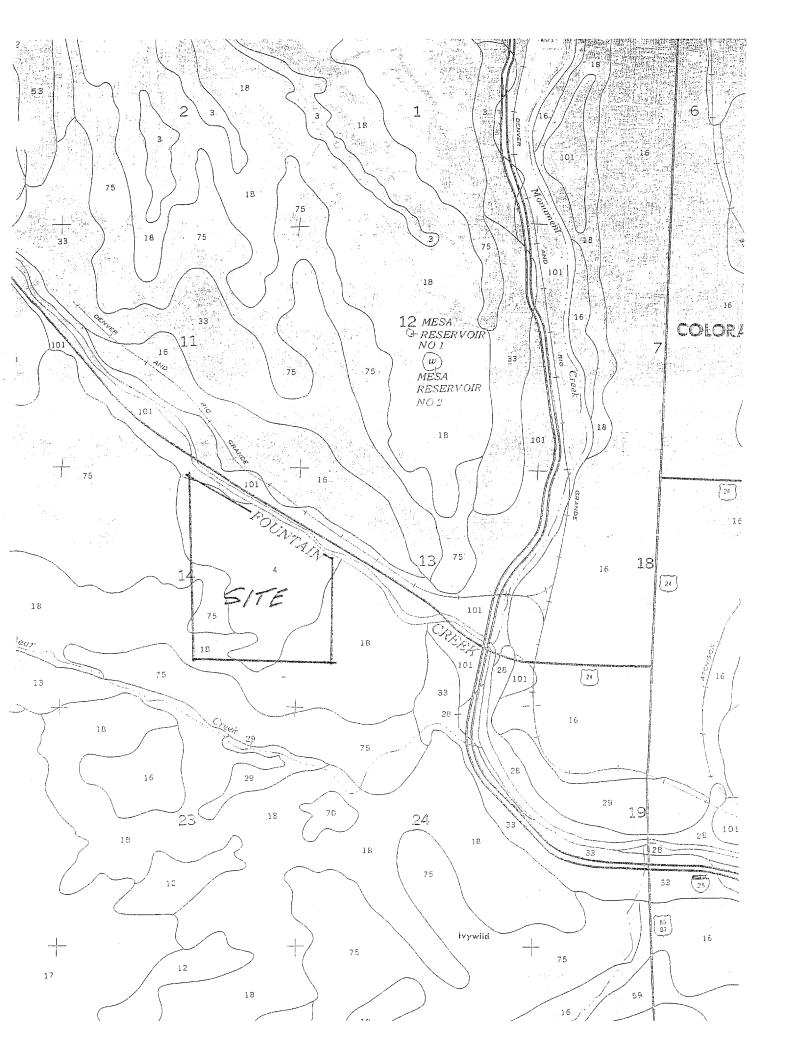
0728

MAP NUMBER 08041C0728 F

EFFECTIVE DATE: MARCH 17, 1997



Federal Emergency Management Agency





BASIN A

Water Quality Volume - Extended Detention Basin (EDB)

| Total Imperv. Ratio (I) WQCV (inches) Site Area (Acres) Vwq (Ac-Ft) | 0.80 0.33 162.92 5.35 | WQCV = 1.0*(0.91* ^3-1.19* ^2+0.78*) (40-hour Drain Time) Vwq=WQCV*Acres*1.2 |
|---|---------------------------------------|---|
| Dwq (feet) Dbs (feet) Dmp (feet) | 5.0 6.5 2.5 | |
| 15% Bottom Stage (Ac-Ft) Bottom Stage Area (Ac) Total WQP Area (Ac) | 0.80 0.09 1.0 7 | |

BASIN B

Water Quality Volume - Extended Detention Basin (EDB)

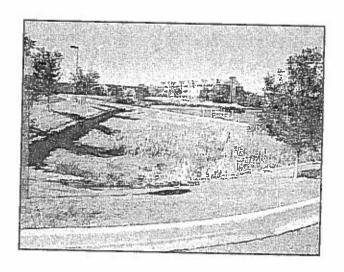
| 0.70 | |
|-------|---|
| 0.28 | $WQCV = 1.0*(0.91*1^3-1.19*1^2+0.78*1)$ |
| 55.68 | (40-hour Drain Time) |
| 1.53 | Vwq=WQCV*Acres*1.2 |
| 5.0 | |
| 6.5 | |
| 2.5 | |
| 0.23 | |
| 0.03 | |
| 0.31 | |
| | 0.28 55.68 1.53 5.0 6.5 2.5 0.23 0.03 |

 $S: \verb|\03.028.007| Phase 1| \verb|\Drainage Study| \verb|\MDDP| [WQP's.xls]| Sheet 1| \\$

By: Jonathan Moore 7/6/2004 14:57

Project: Gold Hill Mesa

Extended Detention Basin (EDB)— Sedimentation Facility



Description

An extended detention basin (EDB) is a sedimentation basin designed to totally drain dry sometime after stormwater runoff ends. It is an adaptation of a detention basin used for flood control. The primary difference is in the outlet design. The EDB uses a much smaller outlet that extends the emptying time of the more frequently occurring runoff events to facilitate pollutant removal. The EDB's drain time for the brim-full water quality capture volume (i.e., time to fully evacuate the design capture volume) of 40 hours is recommended to remove a significant portion of fine particulate pollutants found in urban stormwater runoff. Soluble pollutant removal can be somewhat enhanced by providing a small wetland marsh or ponding area in the basin's bottom to promote biological uptake. The basins are considered to be "dry" because they are designed not to have a significant permanent pool of water remaining between storm runoff events. However, EDB may develop wetland vegetation and sometimes shallow pools in the bottom portions of the facilities.

General Application

An EDB can be used to enhance stormwater runoff quality and reduce peak stormwater runoff rates. If these basins are constructed early in the development cycle, they can also be used to trap sediment from construction activities within the tributary drainage area. The accumulated sediment, however, will need to be removed after upstream land disturbances cease and before the basin is placed into final long-term use. Also, an EDB can sometimes be retrofitted into existing flood control detention basins.

EDBs can be used to improve the quality of urban runoff from roads, parking lots, residential neighborhoods, commercial areas, and industrial sites and are generally used for regional or

follow-up treatment. They can also be used as an onsite BMP and work well in conjunction with other BMPs, such as upstream onsite source controls and downstream infiltration/filtration basins or wetland channels. If desired, a flood routing detention volume can be provided above the water quality capture volume (WQCV) of the basin.

Advantages/Disadvantages

General

An EDB can be designed to provide other benefits such as recreation and open space opportunities in addition to reducing peak runoff rates and improving water quality. They are effective in removing particulate matter and the associated heavy metals and other pollutants. As with other BMPs, safety issues need to be addressed through proper design.

Physical Site Suitability

Normally, the land required for an EDB is approximately 0.5 to 2.0 percent of the total tributary development area. In high groundwater areas, consider the use of retention ponds (RP) instead in order to avoid many of the problems that can occur when the EDB's bottom is located below the seasonal high water table. Soil maps should be consulted, and soil borings may be needed to establish design geotechnical parameters.

Pollutant Removal

The pollutant removal range of an EDB was presented in section 4.1, Table ND-2. Removal of suspended solids and metals can be moderate to high, and removal of nutrients is low to moderate. The removal of nutrients can be improved when a small shallow pool or wetland is included as part of the basin's bottom or the basin is followed by BMPs more efficient at removing soluble pollutants, such as a filtration system, constructed wetlands or wetland channels.

The major factor controlling the degree of pollutant removal is the emptying time provided by the outlet. The rate and degree of removal will also depend on influent particle sizes. Metals, oil and grease, and some nutrients have a close affinity for suspended sediment and will be removed partially through sedimentation.

Aesthetics and Multiple Uses

Since an EDB is designed to drain very slowly, its bottom and lower portions will be inundated frequently for extended periods of time. Grasses in this frequently inundated zone will tend to die off, with only the species that can survive the specific environment at each site eventually prevailing. In addition, the bottom will be the depository of all the sediment that settles out in the basin. As a result, the bottom can be muddy and may have an undesirable appearance to some. To reduce this problem and to improve the basin's availability for other uses (such as open space, habitat or passive recreation), it is suggested that the designer provide a lower-stage basin as suggested in the Two Stage Design procedure. As an alternative, a retention pond (RP) could be used, in which the settling occurs primarily within the permanent pool.

Design Considerations

Whenever desirable and feasible, incorporate the EDB within a larger flood control basin. Also, whenever possible try to provide within the basin for other urban uses such as passive recreation, and wildlife habitat. If multiple uses are being contemplated, consider the multiple-stage detention basin to limit inundation of passive recreational areas to one or two occurrences a year. Generally, the area within the WQCV is not well suited for active recreation facilities such as ballparks, playing fields, and picnic areas. These are best located above the WQCV pool level.

Figure EDB-1 shows a representative layout of an EDB. Although flood control storage can be accomplished by providing a storage volume above the water quality storage, how best to accomplish this is not included in this discussion. Whether or not flood storage is provided, all embankments should be protected from catastrophic failure when runoff exceeds the design event. The State Engineer's regulatory requirements for larger dam embankments and storage volumes must be followed whenever regulatory height and/or volume thresholds are exceeded. Below those thresholds, the engineer should design the embankment-spillway-outlet system so that catastrophic failure will not occur.

Perforated outlet and trash rack configurations are illustrated in section 4.3, *Typical Structural Details*. Figure EDB-3 equates the WQCV that needs to be emptied over 40 hours, to the total required area of perforations per row for the standard configurations shown in that section. The chart is based on the rows being equally spaced vertically at 4-inch centers. This total area of perforations per row is then used to determine the number of uniformly sized holes per row (see detail in the *Structural Details* section). One or more perforated columns on a perforated orifice plate integrated into the front of the outlet can be used. Other types of outlets may also be used, provided they control the release of the WQCV in a manner consistent with the drain time requirements and are approved in advance.

Although the soil types beneath the pond seldom prevent the use of this BMP, they should be considered during design. Any potential exfiltration capacity should be considered a short-term characteristic and ignored in the design of the WQCV because exfiltration will decrease over time as the soils clog with fine sediment and as the groundwater beneath the basin develops a mound that surfaces into the basin.

High groundwater should not preclude the use of an EDB. Groundwater, however, should be considered during design and construction, and the outlet design must account for any upstream base flows that enter the basin or that may result from groundwater surfacing within the basin itself.

Stable, all weather access to critical elements of the pond, such as the inlet, outlet, spillway, and sediment collection areas must be provided for maintenance purposes.

Design Procedure and Criteria

The following steps outline the design procedure and criteria for an EDB.

1. Basin Storage Volume

Provide a storage volume equal to 120 percent of the WQCV based on a 40-hour drain time, above the lowest outlet (i.e., perforation) in the basin. The additional 20 percent of storage volume provides for sediment accumulation and the resultant loss in storage volume.

- A. Determine the WQCV tributary catchment's percent imperviousness. Account for the effects of DCIA, if any, on Effective Imperviousness. Using Figure ND-1, determine the reduction in impervious area to use with WQCV calculations.
- B. Find the required storage volume (watershed inches of runoff):

Determine the required WQCV (watershed inches of runoff) using Figure EDB-2, based on the EDB's 40-hour drain time.

Calculate the Design Volume in acre-feet as follows:

Design Volume =
$$\left(\frac{WQCV}{12}\right) * Area * 1.2$$

In which:

Area

= The watershed area tributary to the extended detention pond.

1.2 factor

 Multiplier of 1.2 to account for the additional 20 percent of required storage for sediment accumulation.

2. Outlet Works

The Outlet Works are to be designed to release the WQCV (i.e., not the "Design Volume") over a 40-hour period, with no more than 50 percent of the WQCV being released in 12 hours. Refer to the Structural Details section for schematics pertaining to structure geometry; grates, trash racks, and screens; outlet type: orifice plate or perforated riser pipe; cutoff collar size and location; and all other necessary components.

For a perforated outlet, use Figure EDB-3 to calculate the required area per row based on WQCV and the depth of perforations at the outlet. See the *Structural Details* section to determine the appropriate perforation geometry and number of rows. (The lowest perforations should be set at the water surface elevation of the outlet micropool.) The total outlet area can then be calculated by multiplying the area per row by the number of rows.

3. Trash Rack

Provide a trash rack of sufficient size to prevent clogging of the primary water quality outlet. Size the rack so as not to interfere with the hydraulic capacity of the outlet. Using the total outlet area and the selected perforation diameter (or height), Figures 6, 6a or 7 in the Structural Details section will help to determine the minimum open area required for the trash rack. If a perforated vertical plate or riser is used as suggested in this manual, use one-half of the total outlet area to calculate the trash rack's size. This accounts for the variable inundation of the outlet orifices. Figures 6 and 6a were developed as suggested standardized outlet designs for smaller sites.

4. Basin Shape

Shape the pond whenever possible with a gradual expansion from the inlet and a gradual contraction toward the outlet, thereby minimizing short circuiting. The basin length to width ratio between the inlet and the outlet should be between 2:1 to 3:1, with the larger being preferred. It may be necessary to modify the inlet and outlet points through the use of pipes, swales, or channels to accomplish this.

5. Two-Stage Design

A two-stage design with a pool that fills often with frequently occurring runoff minimizes standing water and sediment deposition in the remainder of the basin. The two stages are as follows:

- A. Top Stage: The top stage should be 2 or more feet deep with its bottom sloped at 2 percent toward the low flow channel.
- B. Bottom Stage: The active storage basin of the bottom stage should be 1.5 to 3 feet deeper than the top stage and store 5 to 15 percent of the WQCV. Provide a micro-pool below the bottom active storage volume of the lower stage at the outlet point. The pool should be ½ the depth of the upper WQCV depth or 2.5 feet, whichever is the larger.

6. Low-Flow Channel

Conveys low flows from the forebay to the bottom stage. Erosion protection should be provided where the low-flow channel enters bottom stage. Lining the low flow channel with concrete is recommended. Otherwise line its sides with VL Type riprap and bottom with concrete. Make it at least 9 inches deep; at a minimum provide capacity equal to twice the release capacity at the upstream forebay outlet.

7. Basin Side Slopes

Basin side slopes should be stable and gentle to facilitate maintenance and access. Side slopes should be no steeper than 3:1, the flatter, the better and safer.

8. Dam Embankment

The embankment should be designed not to fail during a 100-year and larger storms. Embankment slopes should be no steeper than 3:1, preferably 4:1 or flatter, and planted with turf forming grasses. Poorly compacted native soils should be excavated, and replaced. Embankment soils should be compacted to at least 95 percent of their maximum density according to ASTM D 698-70 (Modified Proctor). Spillway structures and overflows should be designed in accordance with the City of Colorado Springs and El Paso County Drainage Criteria Manual and should consider UDFCD drop-structure design guidelines.

9. Vegetation

Bottom vegetation provides erosion control and sediment entrapment. Pond bottom, berms, and side sloping areas may be planted with native grasses or with irrigated turf, depending on the local setting.

10. Access

All weather stable access to the bottom, forebay, and outlet works area shall be provided for maintenance vehicles. Maximum grades should be 10 percent with a solid driving surface of gravel, rock, or concrete.

11. Inlet

Dissipate flow energy at pond's inflow point(s) to limit erosion and promote particle sedimentation. Inlets should be designed in accordance with the City of Colorado Springs and El Paso County Drainage Criteria Manual's drop structure criteria or another type of energy dissipating structure.

12. Forebay Design

Provide the opportunity for larger particles to settle out in the inlet in an area that has a solid surface bottom to facilitate mechanical sediment removal. A rock berm should be constructed between the forebay and the main EDB. The forebay volume of the permanent pool should be 5 to 10 percent of the design water quality capture volume. A pipe throughout the berm to convey water the EDB should be offset from the inflow streamline to prevent short circuiting and should be sized to drain the forebay volume in 5 minutes.

13. Flood Storage

Combining the water quality facility with a flood control facility is recommended. The 10-year, 100-year, or other floods may be detained above the WQCV. See the *New Development Planning* section of this chapter for further guidance.

14. Multiple Uses

Whenever desirable and feasible, incorporate the EDB within a larger flood control basin. Also, whenever possible try to provide for other urban uses such as active or passive recreation, and wildlife habitat. If multiple uses are being contemplated, use the multiple-stage detention basin to limit inundation of passive recreational areas to one or two occurrences a year. Generally, the

area within the WQCV is not well suited for active recreation facilities such as ballparks, playing fields, and picnic areas. These are best located above the EDB level.

Design Example

Design forms that provide a means of documenting the design procedure are included in the *Design Forms* section. A completed form follows as a design example.

Maintenance Recommendations

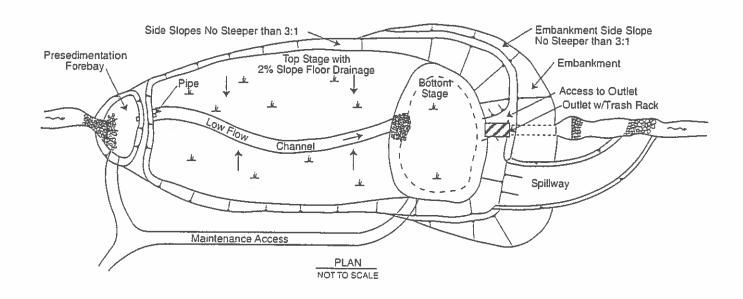
Extended detention basins have low to moderate maintenance requirements. Routine and nonroutine maintenance is necessary to assure performance, enhance aesthetics, and protect structural integrity. The dry basins can result in nuisance complaints if not properly designed or maintained. Bio-degradable pesticides may be required to limit insect problems. Frequent debris removal and grass-mowing can reduce aesthetic complaints. If a shallow wetland or marshy area is included, mosquito breeding and nuisance odors could occur if the water becomes stagnant. Access to critical elements of the pond (inlet, outlet, spillway, and sediment collection areas) must be provided. The basic elements of the maintenance requirements are presented in Table EDB-1.

TABLE EDB-1
Extended Detention Basin Maintenance Considerations

| Required Action | Maintenance Objective | Frequency of Action |
|------------------------------|---|--|
| Lawn mowing and lawn care | Occasional mowing to limit unwanted vegetation. Maintain irrigated turf grass as 2 to 4 inches tall and nonirrigated native turf grasses at 4 to 6 inches. | Routine – Depending on aesthetic requirements. |
| Debris and litter removal | Remove debris and litter from the entire pond to minimize outlet clogging and improve aesthetics. | Routine – Including just before annual storm seasons (that is, April and May) and following significant rainfall events. |
| Erosion and sediment control | Repair and revegetate eroded areas in the basin and channels. | Nonroutine – Periodic and repair as necessary based on inspection. |
| Structural | Repair pond inlets, outlets, forebays, low flow channel liners, and energy dissipators whenever damage is discovered. | Nonroutine – Repair as needed based on regular inspections. |
| Inspections | Inspect basins to insure that the basin continues to function as initially intended. Examine the outlet for clogging, erosion, slumping, excessive sedimentation levels, overgrowth, embankment and spillway integrity, and damage to any structural element. | Routine - Annual inspection of hydraulic and structural facilities. Also check for obvious problems during routine maintenance visits, especially for plugging of outlets. |
| Nuisance control | Address odor, insects, and overgrowth issues associated with stagnant or standing water in the bottom zone. | Nonroutine – Handle as necessary per inspection or local complaints. |

TABLE EDB-1
Extended Detention Basin Maintenance Considerations

| Required Action | Maintenance Objective | Frequency of Action |
|------------------|--|--|
| Sediment removal | Remove accumulated sediment from the forebay, micro-pool, and the bottom of the basin. | Nonroutine – Performed when sediment accumulation occupies 20 percent of the WQCV. This may vary considerably, but expect to do this every 10 to 20 years, as necessary per inspection if no construction activities take place in the tributary watershed. More often it they do. The forebay and the micro-pool will require more frequent cleanout than other areas of the basin, say every 1 or 2 years. |



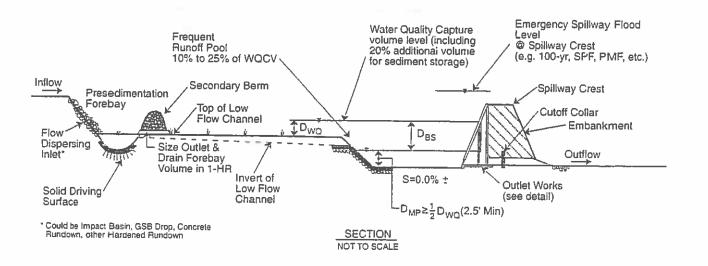


FIGURE EDB-1
Plan and Section of an Extended Detention Basin Sedimentation Facility

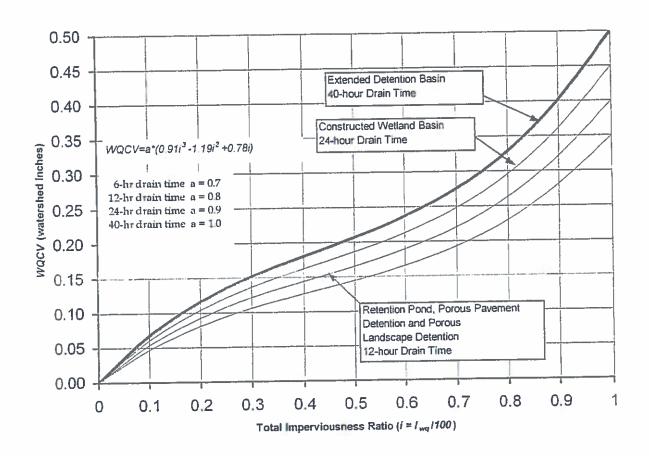


FIGURE EDB-2
Water Quality Capture Volume (WQCV), 80th Percentile Runoff Event

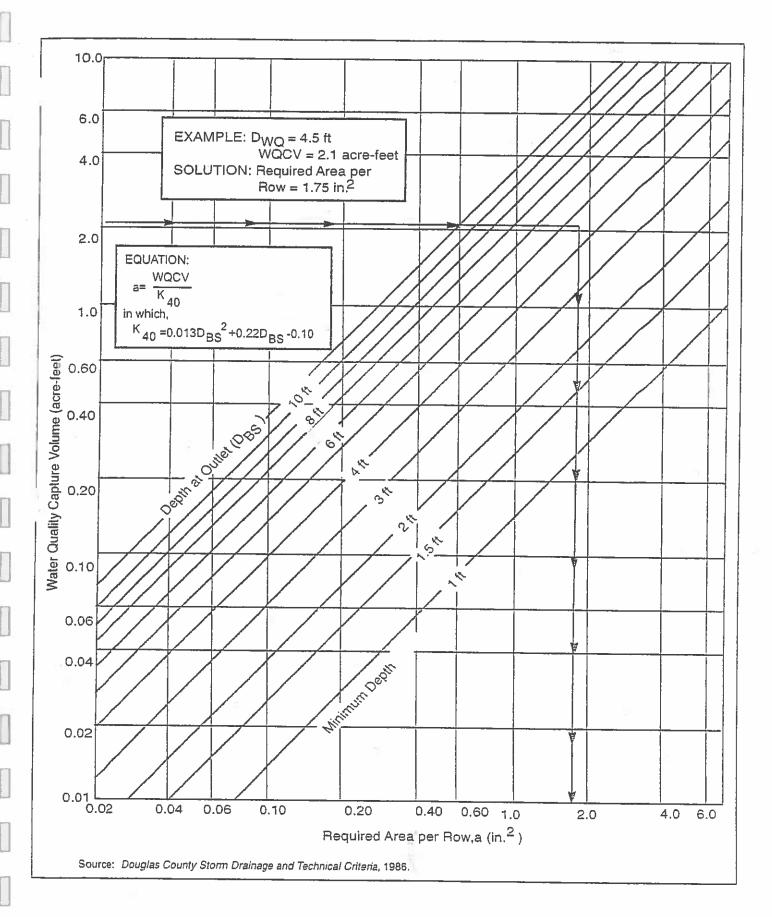


FIGURE EDB-3
Water Quality Outlet Sizing: Dry Extended Detention Basin with a 40-Hour Drain
Time of the Capture Volume

| Designer: Company: Date: September 22, 1999 Project; Location: | |
|---|---|
| 1. Basin Storage Volume A) Tributary Area's Imperviousness Ratio (i = I / 100) | l _a =50.00 % =50.50 % |
| B) Contributing Watershed Area (Area) | Area = 100.00 acres |
| C) Water Quality Capture Volume (WQCV) (WQCV = 1.0 ° (0.91 ° 1³ - 1.19 ° 1² + 0.78 ° 1)) D) Design Volume: Vol = (WQCV / 12) * Area * 1.2 | WQCV = 0.21 watershed inches Vol = 2.063 acre-feet |
| 2. Outlet Works | |
| A) Outlet Type (Check One) | X Orlice Plate Perforated Riser Pipe Other: |
| B) Depth at Outlet Above Lowest Perforation (H) | H =feet |
| C) Required Maximum Outlet Area per Row, (A _o) | A _o = 1.74 square inches |
| D) Perforation Dimensions (enter one only): i) Circular Perforation Diameter OR ii) 2" Height Rectangular Perforation Width | D = 1.5000 inches, OR W = inches |
| E) Number of Columns (nc. See Table 6a-1 For Maximum) | nc =number |
| F) Actual Design Outlet Area per Row (A _n) | A _o = <u>1.77</u> square inches |
| G) Number of Rows (nr) | nr = number |
| H) Total Outlet Area (A _{ol}) | A _{pt} = 27.21 square inches |
| 3. Trash Rack | |
| A) Needed Open Area: A = 0.5 * (Figure 7 Value) * A_{o1} | A _e = 678 square inches |
| B) Type of Outlet Opening (Check One) | X < 2" Diameter Round 2" High Rectangular Other: |
| C) For 2", or Smaller, Round Opening (Ref.: Figure 6s): | |
| Width of Trash Rack and Concrete Opening (W_{conc}) from Table 6a-1 | W _{senc} = 18 inches |
| ii) Height of Trash Rack Screen (Htm) | H _{TR} = 72 inches |

0 100 200

RIO-GRANDE STREET -

400

NORTH

SCALE 1"=200"

URBAN DESIGN
LAND PLANNING
& LANDSCAPE
ARCHITECTURE
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Colorado Springs, CO 80903
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COMMENTS: DATE: BY: COMMENTS:

DRAWN: ADT

DATE: BY: COMMEN

CPC CP 04-127 PLANNER: MAYERL

NORTH

800

SCALE 1"=400'

0 200 400