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Land Development  
101 West Costilla, Suite 122  
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# STORM DRAINAGE MASTER PLAN HEWLETT-PACKARD AT BRIARGATE COLORADO SPRINGS, COLORADO

December 1983

RETURN WITHIN 2 WEEKS TO:  
CITY OF COLORADO SPRINGS  
STORM WATER & SUBDIVISION  
101 W. COSTILLA, SUITE 113  
COLORADO SPRINGS, CO 80903,  
(719) 578-6212

Prepared for:  
**Hewlett-Packard Corporation**  
1501 Page Mill Road, 29u  
Palo Alto, California 94304

thru:

**Fisher, Reece & Johnson, Architects, P.C.**  
1500 South Pearl Street  
Denver, Colorado 80210

DEC Job 101

STORM DRAINAGE MASTER PLAN  
HEWLETT-PACKARD AT BRIARGATE  
COLORADO SPRINGS, COLORADO

December, 1983

Prepared For:

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1501 Page Mill Road, 29u  
Palo Alto, California 93403

through:

Fisher, Reece & Johnson, Architects, P.C.  
1500 South Pearl Street  
Denver, Colorado 80210

Prepared By:

Denver Engineering Corporation  
1626 Cole Boulevard  
Building 7, Suite 300  
Golden, Colorado 80401  
(303) 233-0533

DEC Job No. 101

ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by the negligent acts, errors or omissions on my part in preparing this report.

Prepared by:

*Bruce Prommersberger*

Bruce Prommersberger, P.E.  
Project Manager

Reviewed by:

*David E. Moothart*

David E. Moothart, P.E.  
Vice-President  
Colorado Professional Engineer No. 18183



DEVELOPER'S STATEMENT

The Developer and/or his representative has read and will comply with all the requirements specified in this drainage report and plan.

Hewlett-Packard Corporation

By: \_\_\_\_\_

Title: \_\_\_\_\_

Address: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

ORIGINAL SET  
SIGNED BY  
DEVELOPER

CITY OF COLORADO SPRINGS

Filed in accordance with Section 15-3-906 of the Code of the City of Colorado Springs, 1980, as amended.

*Gary Haynes*

Gary Haynes  
City Engineer

Date: 1/19/84

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STORM DRAINAGE MASTER PLAN  
HEWLETT-PACKARD AT BRIARGATE  
COLORADO SPRINGS, COLORADO

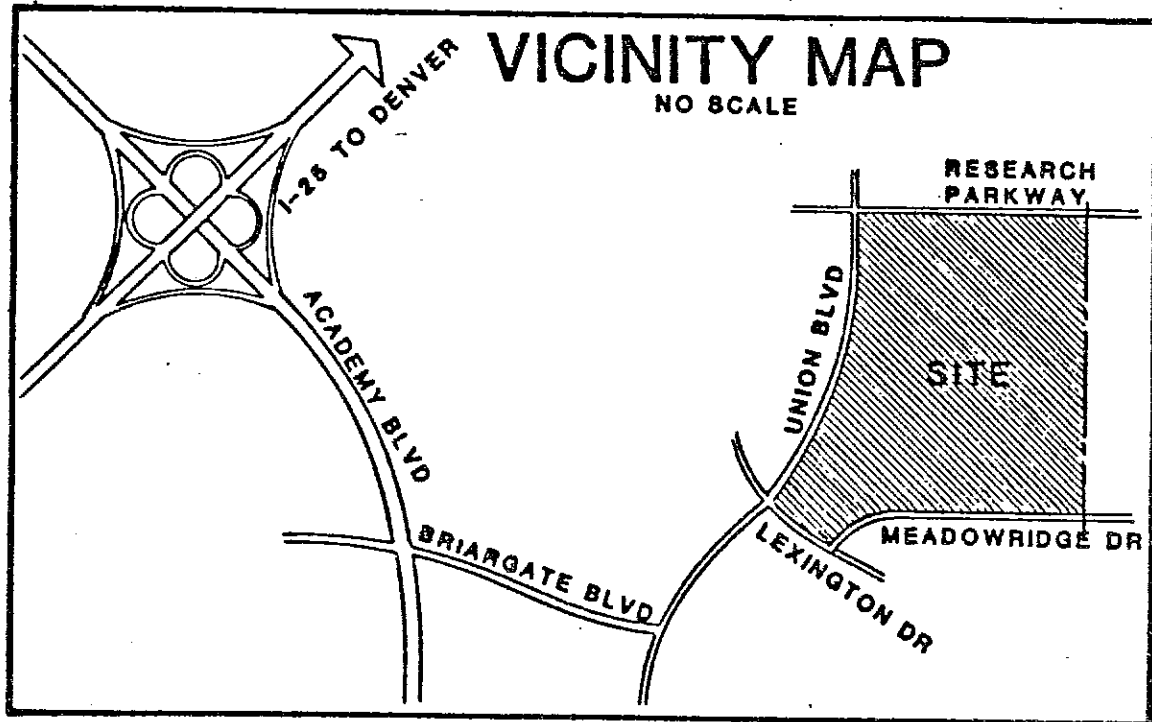
Objective

This report presents results of a storm drainage study for Hewlett-Packard at Briargate in Colorado Springs, Colorado. This report is intended to be a master plan to define the drainage facilities required for this site. The plan will assure continuity of drainage design as the site progresses through its planned phased development. The master plan describes drainage facilities to safely handle stormwater runoff when the site is fully developed as presently planned. A detailed design will be required as each phase is developed.

Location

The vicinity map and drainage basin map included in this report show the location of the Hewlett-Packard site. The site is located in the southeast quarter of Section 34, Township 12 South, Range 66 West, and the northeast, northwest and southwest quarters of Section 3, Township 13 South, Range 66 West, of the Sixth Principal Meridian, El Paso County, Colorado.

The 206-acre site is tributary to Cottonwood Creek. Approximately 307 acres upstream contribute additional runoff onto the site. The site is currently undeveloped and has a cover of native grasses. The soil for the entire site is Blakeland loamy sand. This is a deep, somewhat excessively drained soil formed in alluvial and eolian material derived from arkosic sedimentary rock on uplands. Blakeland loamy sand belongs to hydrologic soil group A.



### Drainage Considerations

The site generally drains from the northeast to southwest. Stormwater runoff from the north will be intercepted by Research Parkway and carried to the east where it will be conveyed through drainage facilities provided for the subdivision to the east. Offsite flows enter the site from the east at two points shown on the drainage plan as design points 23 and 27. No runoff enters the site from either the west or the south.

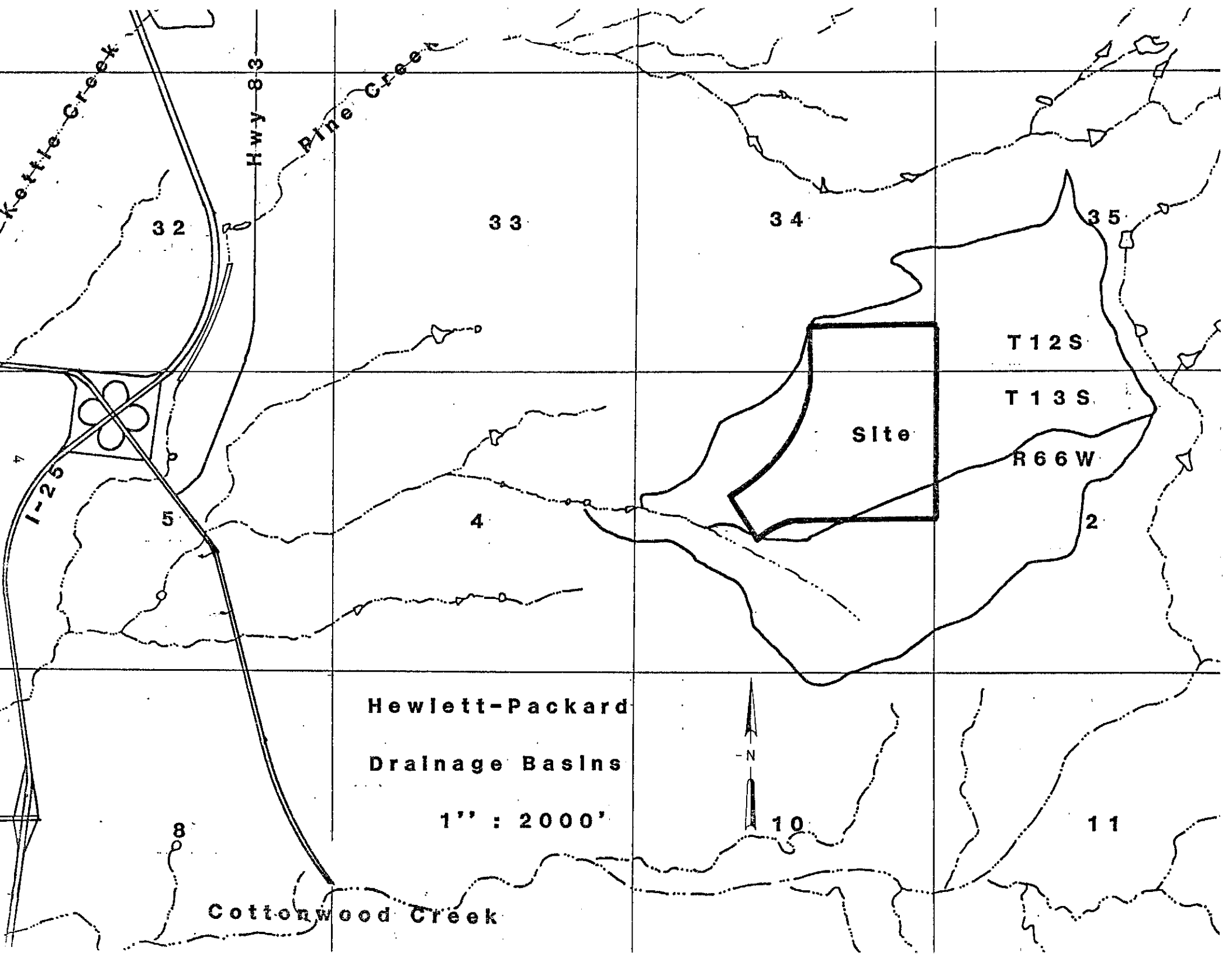
The site is generally divided into five drainage zones.

1. Runoff from the northwest portion of the site is conveyed south along the perimeter road and Union Boulevard to the existing manhole at the driveway across from Brigantine Drive and then to the existing storm sewer which continues down Union.

2. Runoff from a small strip from Brigantine to Lexington Drive along Union is collected in existing inlets to the storm sewer in Union Boulevard.
3. The finished grades cause runoff in the central part of the site to drain to the middle of the site, often to low points on the north side of the proposed buildings. The runoff in this portion of the site is collected and conveyed by a series of pipes south to the major collection facilities along Meadow Ridge Drive. This system is sized for the 100-year storm.
4. Runoff from the east side of the site and from offsite sources to the east are collected and conveyed by pipe and concrete channel south along the east property line and west along the south property line. Flows in the channel will be supercritical. This channel terminates at the driveway off Meadow Ridge Drive. From here, flow continues in a reinforced concrete box culvert. Approximately 230 feet downstream from the entrance to the box culvert, runoff from the central portion of the site joins with the runoff from the east side of the site and the offsite flows.
5. Runoff from the southwest portion of the site is collected and conveyed to the box culvert.

#### Hydrology

Hydrology is computed by SCS TR55, Urban Hydrology for Small Watersheds, as required by City of Colorado Springs Determination of Storm Runoff Criteria, March 1977. Information regarding offsite flows is taken from a September 29, 1983 letter from Donell Jeffries to Gary Haynes, City Engineer. A copy of this letter is included in the Appendix. Soil information is taken from Soil Survey of El Paso





County Area, Colorado, Soil Conservation Service, June, 1981.  
Hydrologic computations are included in the Appendix.

### Drainage Facilities

Drainage facilities are sized for the 5-year or 100-year storms as appropriate. The majority of the inlets and storm sewers are sized for the 100-year storm due to site grading constraints. These constraints exist due to natural topography and the need to maintain certain building elevations to conform with the overall architectural plan. Where drainage facilities are sized to collect the 5-year storm, runoff in excess of the 5-year storm will travel in the streets and will eventually flow to the existing concrete channel at Lexington and Meadow Ridge. Computations for sizing the drainage facilities are included in the Appendix.

### Storm Sewers

The storm sewer system, as planned, is a system of inlets, reinforced concrete pipe, reinforced concrete box culverts and concrete channel. Hydraulic computations and preliminary design data are included in the Appendix.

A minor constraint to the system is the two existing 66-inch culverts at Lexington and Meadow Ridge. These culverts are sized to handle 675 cfs. Calculations in this study indicate that 732 cfs will reach this point. Three alternatives are available to solve this problem.

1. Leave the crossing as it is now. Pressurize the box culvert to develop sufficient head to pass 732 cfs.

2. Install a third culvert and reconstruct one branch of the concrete channel from the discharge end of the three culverts to the main channel.
3. Remove the two existing culverts, lower the water main, and continue the box culverts across Lexington to the channel.

For all three alternatives, an energy dissipator will be required at the discharge end of the culverts. The current plan and cost estimate shows Alternative 1, which is the least expensive. Alternative 3, however, would function the best.

#### Cost Estimate

The construction cost estimate for the Hewlett-Packard storm drainage facilities is \$2,285,680. The portion of this cost to be reimbursed by the City of Colorado Springs is \$1,104,265. The reimbursable cost is computed assuming a concrete channel from the first point of interception of offsite flows near the northeast corner of the site at design point 23, along the east and south property line, terminating at the existing culvert crossing at Lexington and Meadow Ridge at design point 35.

These estimated costs of construction are intended to provide Hewlett-Packard and the City of Colorado Springs an indication of the costs involved and are considered to be a preliminary estimate only. Final design has not yet been performed. We, as engineers, have no control over the cost of labor and materials, or competitive bidding, and cannot guarantee the accuracy of the construction costs. The unit prices used in the estimate reflect estimated current costs and do not provide for inflation. Although this is a planned phased development,

no exact buildout schedule is available, so inflationary costs cannot be estimated.

#### Erosion and Sedimentation Control

Blakeland loamy sand requires good erosion control to minimize soil losses and sedimentation downstream. When protective cover is removed, soil blowing is a hazard. An erosion control plan must be developed with the storm sewer design as each phase of the site is constructed.

**APPENDIX I**  
**HYDROLOGY**





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# DESIGN CALCULATIONS

Project HEWLETT-PACKARD REARBASE  
 Feature DRAINAGE HYDROLOGY  
 Designed BDP Date: 5-23-81 2 of 15  
 Checked Date Job No. 101

BASIN	AREA (ACRES)	AREA (SQ. MI.)	SOIL TYPE	LAND USE	CURVE NO.	BASIN HT. (FT.)	BASIN LENGTH (FT.)	TIME CONC. (HR.)	CSM IN	5 YEAR RUNOFF (IN.)	5 YEAR PEAK Q (CFS)	100 YEAR RUNOFF (IN.)	100 YEAR PEAK Q (CFS)
R	6.00	0.009	A	BLDG, PARKING & LAWN	86	12	850	0.098	1290	0.93	10.7	2.10	24.4
S	5.10	0.008	A	BLDG, PARKING & LAWN	86	4	330	0.042	1430	0.93	10.6	2.10	24.0
T	3.82	0.006	A	BLDG, PARKING & LAWN	81	4	380	0.058	1415	0.67	5.7	1.71	14.5
U	2.30	0.004	A	ROAD & LAWN	74	16	860	0.085	1320	0.40	2.1	1.24	6.5
V	0.58	0.001	A	ROAD & LAWN	66	8	360	0.033	1460	0.18	0.3	0.80	1.2
W	2.95	0.005	A	BLDG, ROAD & LAWN	71	8	720	0.095	1300	0.31	2.0	1.06	6.9
X	12.93	0.020	A	BLDG, ROAD & LAWN	81	23	1130	0.174	1120	0.67	15.0	1.71	38.3
Y	7.24	0.011	A	BLDG, PARKING & LAWN	76	14	780	0.080	1330	0.47	6.8	1.37	20.0
Z	3.76	0.006	A	BLDG, PARKING & LAWN	85	10	560	0.058	1400	0.87	7.3	2.02	16.9
AA	1.63	0.003	A	ROAD	69	42	2230	0.221	1040	0.25	0.8	0.95	3.0
BB	5.96	0.009	A	LAWN & CHANNEL	60		2230	0.031	1465	0.08	1.0	0.53	7.0
CC	OFFSITE												CUMULATIVE 509
DD	3.00	0.005	A	PARKING & LAWN	82	10	750	0.091	1305	0.72	4.7	1.78	11.6
EE	0.94	0.001	A	PARKING & LAWN	45	13	520	0.045	1425	—	—	0.08	0.1
FF	2.90	0.005	A	PARKING & LAWN	84	10	540	0.054	1405	0.82	5.7	1.94	13.6
GG	7.30	0.011	A	BLDG, PARKING & LAWN	83	9	800	0.106	1260	0.76	10.6	1.86	25.8
HH	4.19	0.007	A	BLDG, PARKING & LAWN	89	7	470	0.054	1405	1.11	10.9	2.36	23.2
													237.0 398.2





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## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE  
Detail DRAINAGE HYDROLOGY  
Designer BDP Date 2-5-83  
Checker \_\_\_\_\_ Date \_\_\_\_\_

COMPUTATION OF RUNOFF CURVE NUMBERS

USE TABLE 2-2 PAGE 2-5, SES TR-55

ENTIRE SITE IS BLAKELAND LOAMY SAND :: SOIL TYPE A

PARKING LOTS, STREETS, DRIVEWAYS, ROOFS CN = 98

LAWNS, GOOD CONDITION CN = 39

COMPUTE COMPOSITE CN FOR SITE

COMPARE WITH PLANNING DATA





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Sheet 5 of 15  
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# DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE HYDROLOGY

Designer BDP Date 12-5-83

Checker \_\_\_\_\_ Date \_\_\_\_\_

BASIN	AREA (ACRES)	AREA (SQ. MI)	% CN=39	% CN=98	CN
A	3.85	0.006	47	53	70
B	1.22	0.002	53	47	67
C	7.26	0.011	85	15	48
D	5.96	0.009	78	22	52
E	2.40	0.004	78	22	52
F	1.65	0.003	60	40	63
G	4.43	0.007	100	0	39
H	OFFSITE	OFFSITE	OFFSITE	OFFSITE	OFFSITE
I	2.15	0.003	45	55	71
J	1.69	0.003	73	27	55
K	3.31	0.005	46	54	71
L	6.44	0.010	25	75	83
M	8.70	0.014	27	73	82
N	3.84	0.006	5	95	95
O	3.85	0.006	24	76	84
P	1.15	0.002	19	81	87
Q	12.16	0.019	35	65	77
R	6.00	0.009	20	80	86
S	5.10	0.008	20	80	86
T	3.82	0.006	29	71	81
U	2.30	0.004	40	60	74
V	0.58	0.001	53	47	66
W	2.95	0.005	45	55	71
X	12.95	0.020	29	71	81
Y	7.24	0.011	37	63	76
Z	3.76	0.006	22	78	85
AA	1.63	0.003	50	50	69
BB	5.96	0.009	65	35	60
CC	OFFSITE	OFFSITE	OFFSITE	OFFSITE	OFFSITE
DD	3.00	0.005	27	73	82
EE	0.94	0.001	90	10	45
FF	2.90	0.005	23	77	84
GG	7.30	0.011	25	75	83
HH	4.19	0.007	15	85	89
II	5.04	0.008	20	80	86
JJ	2.92	0.005	20	80	86



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Sheet 6 of 15  
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# DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE HYDROLOGY

Designer BDP Date 12-5-83

Checker \_\_\_\_\_ Date \_\_\_\_\_

BASIN	AREA (ACRES)	AREA (SQ. MI.)	% CN = 39	% CN = 98	CN
KK	3.43	0.005	55	45	66
LL	2.05	0.003	54	46	66
MM	8.14	0.013	97	31	41
NN	1.08	0.002	36	64	77
OO	9.90	0.015	25	75	83
PP	7.70	0.012	46	54	71
QQ	3.10	0.005	15	85	89
RR	8.00	0.013	27	73	82
SS	7.20	0.011	18	82	87
TT	7.32	0.011	89	11	45
UU	2.43	0.004	86	14	47
VV	2.30	0.004	75	25	54
	211.27	0.331			



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## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE HYDROLOGY

Designer BDP Date 2-5-83

Checker \_\_\_\_\_ Date \_\_\_\_\_

DETERMINING CUMULATIVE CN FOR SITE

$$\sum CN = \frac{\sum (A \times CN)}{\sum A} = \frac{15,401.81}{211.27} = 72.90 \approx \underline{\underline{73}}$$

CHECK VS. PLANNING DATA

BUILDINGS & SUPPORT	18.1%
PARKING & DRIVES	40.2%
OPEN SPACE	41.7%
	<u>100.0%</u>

$$CN = (0.181)(98) + (0.402)(98) + (0.417)(39) = 73.40 \approx \underline{\underline{73}}$$



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## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE HYDROLOGY

Designer BDP Date 12-5-83

Checker \_\_\_\_\_ Date \_\_\_\_\_

### COMPUTATION OF TIME OF CONCENTRATION

DETERMINE CHANGE IN ELEVATION FOR EACH SUBBASIN

DETERMINE BASIN LENGTH

DETERMINE BASIN SLOPE,  $\Delta EL / LENGTH$

USE FIGURE 3-1, PAGE 3-2 SCS TR-55,  
MARCH 1980, TO FIND VELOCITY

$$t_c \text{ (HR)} = \frac{1}{\text{VELOCITY (FPS)}} \times \frac{\text{LENGTH (FT)}}{3600 \text{ (SEC/HR)}}$$

HEWLETT-PACKARD @ BRIARGATE  
 DRAINAGE HYDROLOGY  
 BDP 12-5-83

3-2

then computed by dividing the total overland flow length by the average velocity.

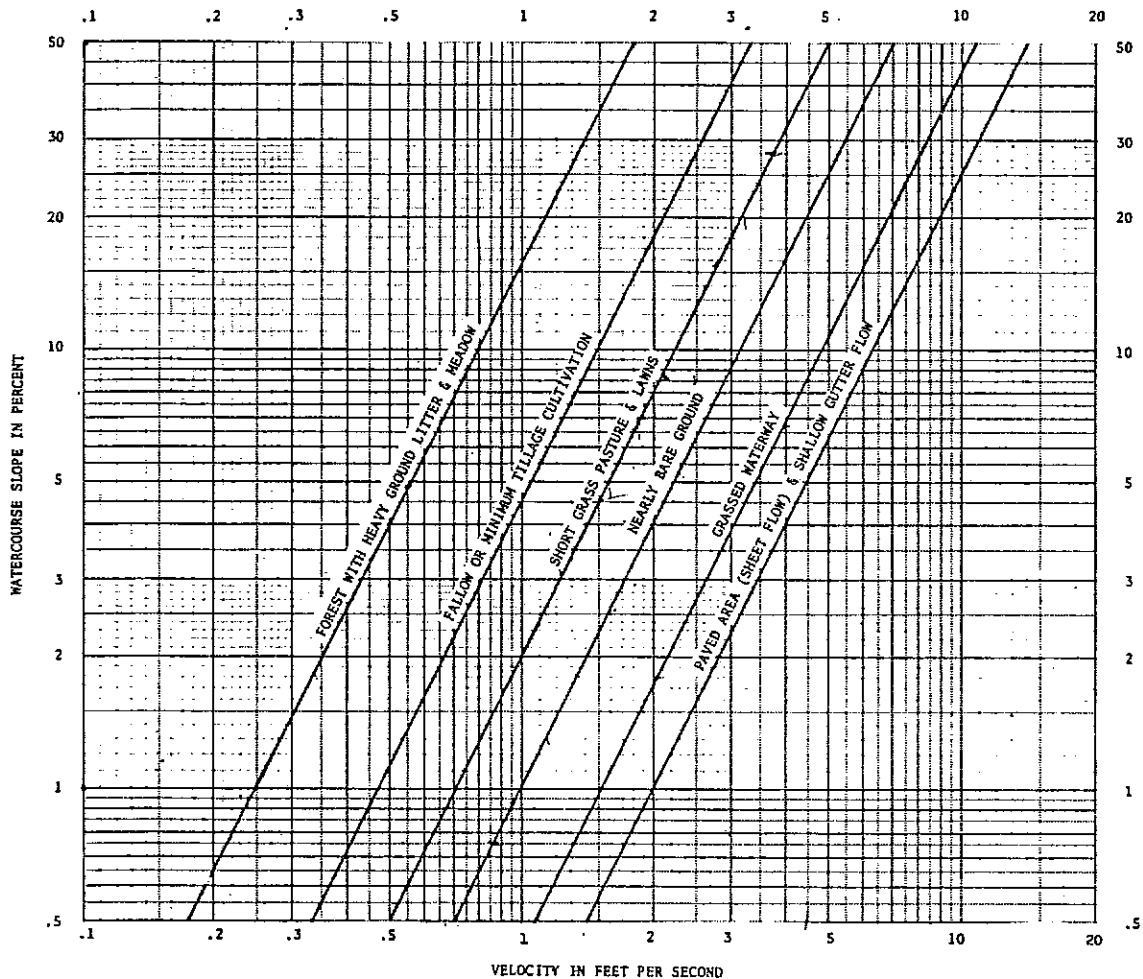


Figure 3-1.--Average velocities for estimating travel time for overland flow.

Storm sewer or road gutter flow

Travel time through the storm sewer or road gutter system to the main open channel is the sum of travel times in each individual component of the system between the uppermost inlet and the outlet. In most cases average velocities can be used without a significant loss of accuracy. During major storm events, the sewer system may be fully taxed and additional overland flow may occur, generally at a significantly lower velocity than the flow in the storm sewers. By using average conduit sizes and an average slope (excluding any vertical drops in the system), the average velocity can be estimated using Manning's formula.

Since the hydraulic radius of a pipe flowing half full is the same as when flowing full, the respective velocities are equal. Travel time may



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# DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BIRMGATE

Detail DRAINAGE HYDROLOGY

Designer BDP Date 12-5-83

Checker \_\_\_\_\_ Date \_\_\_\_\_

BASIN	DEL (FT)	LENGTH (FT)	SLOPE (%)	VELOCITY (FPS)	$t_c$ (HR)	$\Sigma t_c$ (IF READ)
A	81	1820	4.6	4.3	.118	
B	49	880	5.6	4.7	.052	
C	83	300	27.7	3.7	.023	
	13	1250	1.0	2.0	.174	.197
D	87	300	29.0	3.8	.022	
	14	810	1.7	2.6	.087	.109
E	55	700	7.9	2.0	.097	
F	57	2000	2.8	3.4	.167	
G	46	1280	3.6	1.3	.274	
	10	580	1.7	2.0 (EST)	.008	.282
H						OFFSITE
I	36	850	4.2	4.1	.058	
J	31	870	3.6	3.7	.064	
K	14	720	1.9	2.8	.071	
L	14	620	2.3	3.0	.057	
M	8	875	1.0	2.0	.122	
N	4	120	3.3	1.3	.026	
	15	430	3.5	3.7	.032	.058
O	4	170	2.4	1.1	.043	
	17	680	2.5	3.2	.059	.102
P	9	240	3.8	4.0	.017	
Q	7 (EST)	400	1.8	1.0	.111	
	9	850	1.1	2.1	.112	.223
R	12	850	1.4	2.4	.098	
S	4	330	1.2	2.2	.042	
T	4	380	1.1	2.1	.050	
U	16	860	1.9	2.8	.085	
V	8	360	2.2	3.0	.033	
W	8	720	1.1	2.1	.095	
X	7 (EST)	350	2.0	1.0	.097	
	16	780	2.1	2.8	.077	.174
Y	14	780	1.8	2.7	.080	
Z	10	500	1.8	2.7	.058	



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## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE HYDROLOGY

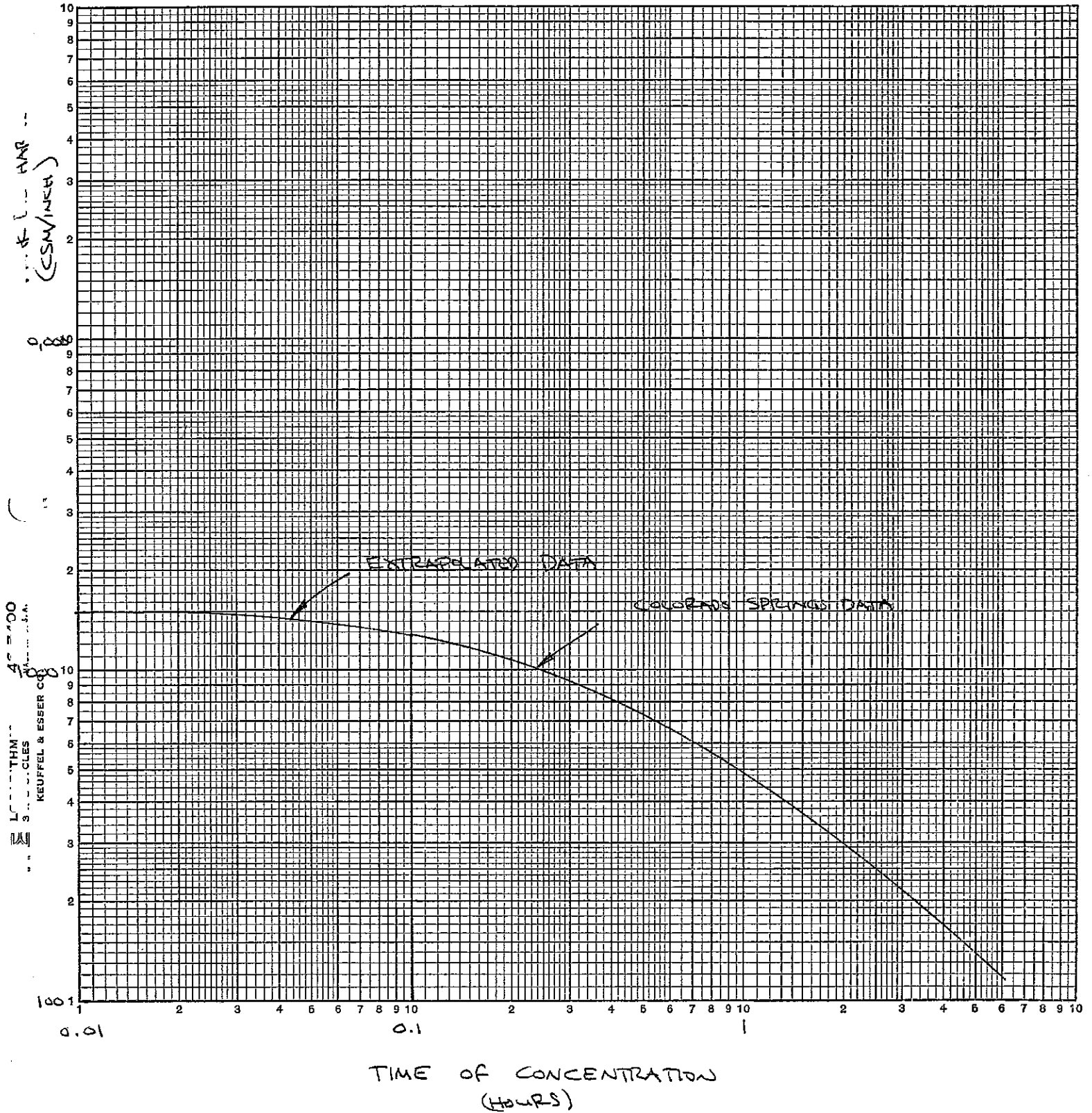
Designer BDP Date 12-5-83

Checker \_\_\_\_\_ Date \_\_\_\_\_

BASIN	AREA (FT)	LENGTH (FT)	SLOPE (%)	VELOCITY (FPS)	C <sub>c</sub> (HR)	E C <sub>c</sub> (IF REQD)
AA	42	2230	1.9	2.8	.221	
BB		2230		2.0 (EST)	.031	
CC						OFFSITE
DD	10	750	1.3	2.3	.091	
EE	13	520	2.5	3.2	.045	
FF	10	540	1.9	2.8	.054	
GG	9	800	1.1	2.1	.106	
HH	7	470	1.5	2.4	.054	
II	5	470	1.1	2.1	.062	
JJ	5	500	1.0	2.0	.069	
KK	38	1300	2.9	3.4	.106	
LL	4	200	2.0	1.0	.056	
	6	550	1.1	2.1	.073	.129
MM	44	1070	4.1	1.4	.212	
	10	570	1.8	2.7	.059	.271
NN	16	910	1.8	2.7	.094	
OO	2	100	2.0	1.0	.028	
	17	450	3.8	3.8	.033	.061
PP	10	470	2.1	2.9	.045	
QQ	8	480	1.7	2.5	.051	
RR	2	130	1.5	0.9	.040	
	7	700	1.0	2.0	.097	.137
SS	17	700	2.4	3.1	.063	
TT	44	680	6.5	1.8	.105	
UU	15	1500	1.0	2.0	.208	
VV	15 (EST)	300	5.0	1.6	.052	
	260	1350	1.9	2.8	.134	.186

$t_c$  0.01 - 0.1 EXTRAPOLATED FROM  
 $t_c$  0.1 - 5.8 DATA 6HR TYPE IIA  
 COLORADO SPRINGS DRAINAGE  
 CRITERIA FIGURE I

HEWLETT-PACKARD @ BRIARGATE  
 DRAINAGE HYDROLOGY  
 BDP 12-5-83





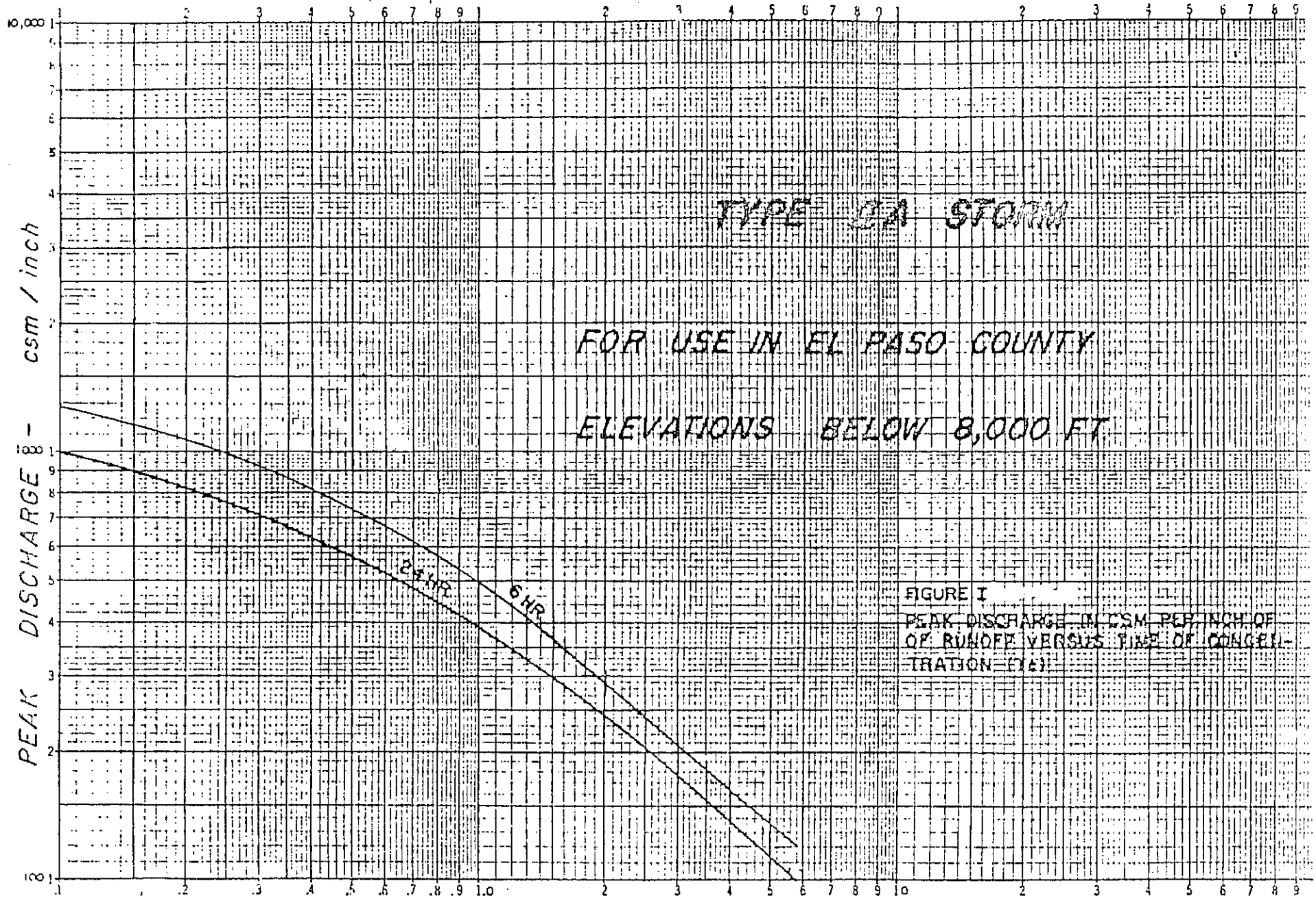


FIGURE I  
 PEAK DISCHARGE IN CSM PER INCH OF  
 OF RUNOFF VERSUS TIME OF CONCENTRATION (T<sub>C</sub>)

TIME OF CONCENTRATION - HOURS  
 Revised 7-13-77 CA

FIGURE I

SHEET 13/15  
 Job No. 101  
 HYDROLOGICAL  
 DRAINAGE  
 HYDROLOGY  
 BOR 12-5-83



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## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE HYDROLOGY

Designer BDP Date 12-5-83

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DETERMINE RUNOFF IN INCHES BY

$$Q = \frac{(P - 0.2S)^2}{P + 0.8S}$$

$$S = \frac{1000 - 10}{CN}$$

FIND POINT OF ZERO RUNOFF FOR 5 YEAR STORM

$$Q = P - 0.2S$$

$$Q = 2.1 - 0.2 \left( \frac{1000 - 10}{CN} \right)$$

$$CN = 48.78$$

FIND POINT OF ZERO RUNOFF FOR 100 YEAR STORM

$$Q = P - 0.2S$$

$$Q = 3.5 - 0.2 \left( \frac{1000 - 10}{CN} \right)$$

$$CN = 36.36$$



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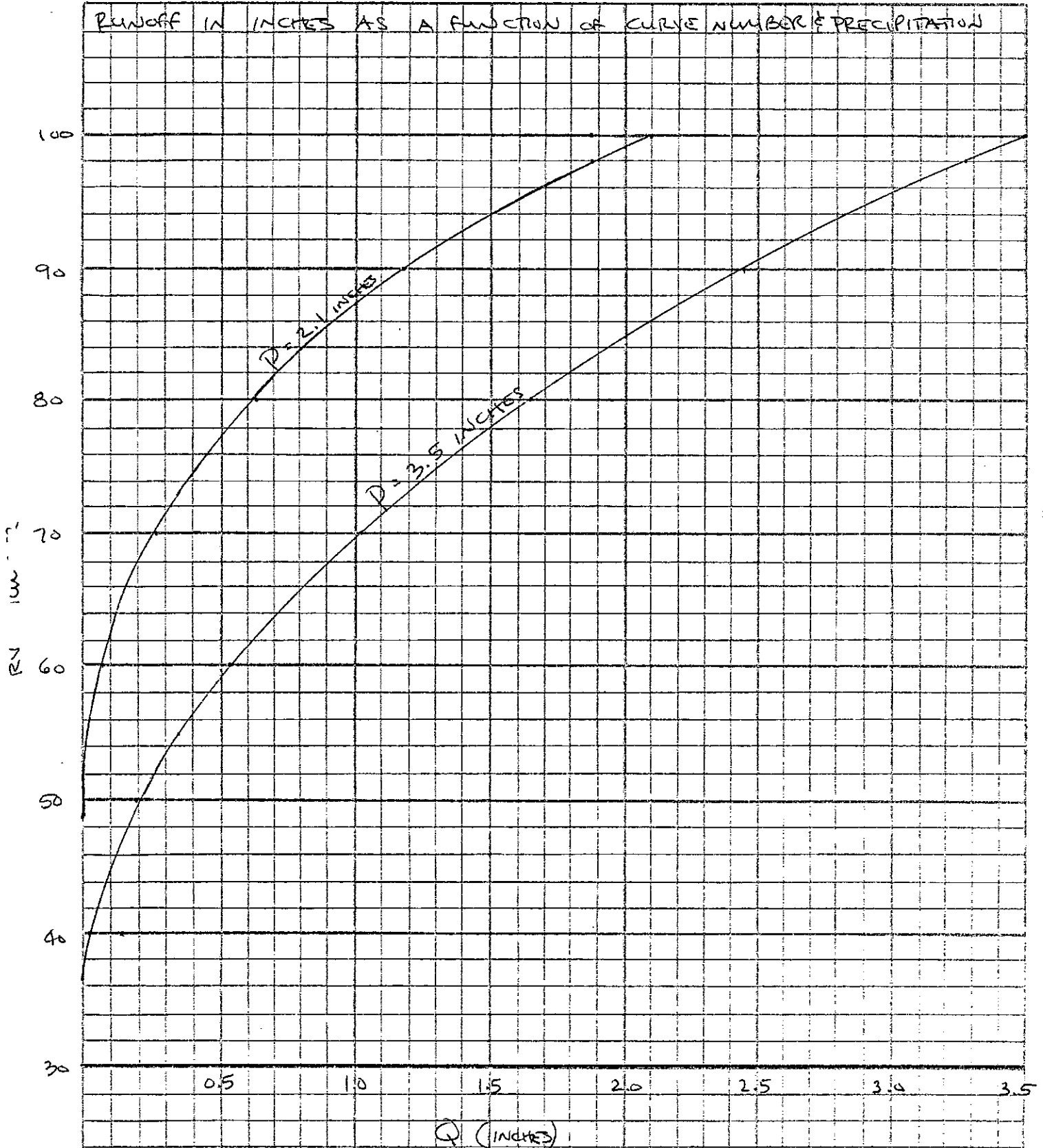
## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE HYDROLOGY

Designer BDP Date 12-5-83

Checker \_\_\_\_\_ Date \_\_\_\_\_

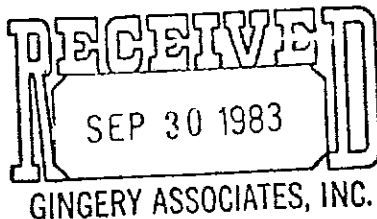


DONIELL JEFFRIES  
PROFESSIONAL ENGINEER  
REGISTERED LAND SURVEYOR  
SUBDIVISION LAYOUT AND DESIGN



3315 Springridge Circle  
Colorado Springs, Colorado 80906  
(303) 576-5576

September 29, 1983



Mr. Gary Haynes  
City Engineer  
Colorado Springs, Colorado

Re: Peak Drainage Flows Affecting the Hewlett Packard Briargate Site

Dear Gary:

Mr. Bruce Prommersberger, Project Manager for Gingery Associates Inc., recently contacted me regarding a discrepancy in the peak flow computations at the southwest corner of their site. His calculations show 1,080 c.f.s. at that point, while my 1980 computations show 675 c.f.s., and the existing twin 66" RCP culverts were designed for the smaller amount. The reason for the predicted difference in peak flows is two-fold.

1. At the time of my calculations in 1980, I assumed that a larger portion (about 50 acres) of the finished Hewlett Packard tract would flow into the Union Boulevard sub-basin, rather than to the south line of the property. The current design features a central system running north to south, which has increased the area draining to the southwest corner.

2. In computing the 1,080 c.f.s. flow, Mr. Prommersberger used my peak runoff quantities of 463 c.f.s. and 309 c.f.s. entering the Hewlett Packard site from the two basins east of their property. These quantities were shown in the drainage reports for Kambridge Point and Contrails No. 2 Subdivisions. However, my computations for the peak flows from those two basins were somewhat conservative as to the times of concentration.

As a safety factor, I generally use an average velocity of 10 feet per second for upstream flows. A more detailed analysis of the velocities indicates that the runoff will take considerably longer than shown to reach the Hewlett Packard tract, thus resulting in a reduction of the predicted storm water peak flows.

The following pages show the results of my re-computations. The times of concentration were taken from Figure 3-1, SCS Technical Release 55.

NORTHERLY BASIN INFLOW INTO HEWLETT PACKARD TRACT

Acres	Square Miles	Curve Number	Basin Length	Time of Concen.	CSM/ Inch	100 Year Runoff	100 Year Peak c.f.s.
1,000	lf of concrete channel @ 2 %				Use 18 feet per second	= 55 seconds	
1,200	lf of street flow @ 1 %				Use 2 " " "	= 600 "	
2,500	lf of street & overland flow @ 3%				Use 3.5 " " "	= 714 "	
						<u>1369</u> seconds =	
						0.38 hours.	
190	.2969	75	4,700'	0.38	830	1.30"	320

SOUTHERLY BASIN INFLOW INTO HEWLETT PACKARD TRACT

Acres	Square Miles	Curve Number	Basin Length	Time of Concen.	CSM/ Inch	100 Year Runoff	100 Year Peak c.f.s.
1,500	lf of grassed swale @ 1 %				Use 2 feet per second	= 750 seconds	
1,800	lf of streets @ 2%				Use 3 " " "	= 600 "	
1,500	lf of streets @ 5 %				Use 5 " " "	= 300 "	
						<u>1650</u> seconds =	
						0.46 hours	
151	.2359	72	4,800'	0.46	770	1.12"	203

COMBINED BASINS INFLOW INTO HEWLETT PACKARD TRACT

Acres	Square Miles	Curve Number	Basin Length	Time of Concen.	CSM/ Inch	100 Year Runoff	100 Year Peak c.f.s.
341*	.5328	74	6,100	0.46	770	1.24"	509

\* Does not include any Hewlett Packard area.

Following are comparisons of these revised quantities with those shown on drainage studies of Kambridge Point, Contrails No. 2, and Phase III Master Plan.

	Previous	This Computation	Difference
Northerly Basin	463 c.f.s.	320 c.f.s.	143 c.f.s.
Southerly Basin	309 c.f.s.	203 c.f.s.	106 c.f.s.
Combined Basins	541 c.f.s.	509 c.f.s.	32 c.f.s.

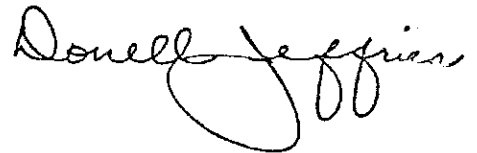
The effect of the predicted reduction in 100 Year peak flows will not be significant on the already constructed drainage facilities in Contrails No. 1 and Kambridge Point Subdivisions. Those structures were sized for the 5 Year Storm, and the 100 Year Storm will flow overland along the linear park.

In Contrails No. 2 Subdivision the storm sewer designed in Research Parkway was sized to carry the 5 Year Storm flows, and again the 100 Year Storm will flow westerly in the street. The proposed 54" RCP culvert which crosses Research Parkway will carry the entire 100 Year Storm flow, although the total predicted is less than 500 c.f.s..

The concrete channel which has been designed between Research Parkway and the Hewlett Packard site will be constructed as presently approved. The channel as designed will carry 512 c.f.s. when full, or 320 c.f.s. with a freeboard of seven inches.

Please contact me if additional information is desired regarding the afore-mentioned discrepancy in peak flows.

Sincerely,

A handwritten signature in cursive script that reads "Donnell Jeffries". The signature is written in dark ink and is positioned to the right of the word "Sincerely,".

cc: Bruce Pommersberger  
Jerry Novak

**APPENDIX 2**  
**DRAINAGE FACILITIES**



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## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE FACILITIES

Designer BDP Date 12-6-83

Checker \_\_\_\_\_ Date \_\_\_\_\_

DESIGN SYSTEM ASSUMING  $n = 0.015$  FOR RCP &

NO LOSSES. WORK FROM U/S TO D/S.

AT FINAL DESIGN WORK FROM D/S TO U/S

USING  $n = 0.013$  & APPROPRIATE LOSSES.

PERIMETER ROAD IS 6" VERTICAL CURB &

30'  $\# - \#$ .

USE COLORADO SPRINGS DIOR INLETS ALONG  
CURB.

USE CDOT TYPE 13 WHERE DESIGNATED

IN PARKING LOTS. CDOT TYPE 13 TO BE

PLACED IN 1" SCUMPS.





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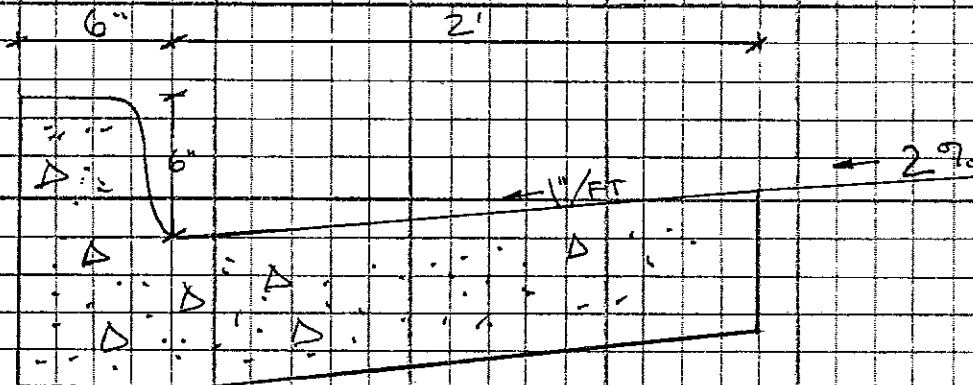
Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE FACILITIES

Designer BDP Date 12-6-83

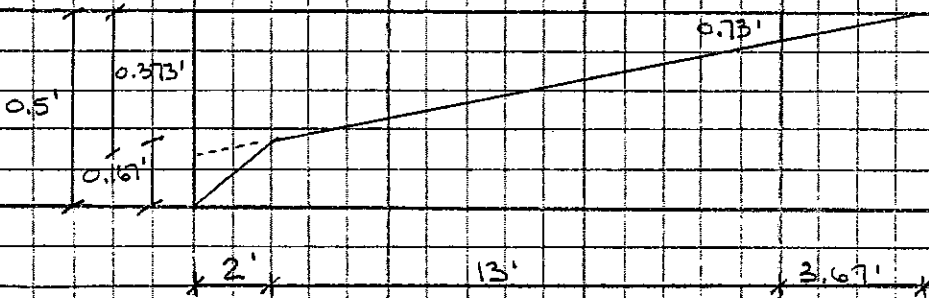
Checker \_\_\_\_\_ Date \_\_\_\_\_

## DETERMINE GUTTER CAPACITY



STREET IS 30' F-F

$$\Delta EL \text{ F-F CROWN} = 2' (1''/\text{FT}) + 13 (0.02 \text{ FT}/\text{FT}) (12''/\text{FT}) = 5.12''$$





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## DESIGN CALCULATIONS

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Detail DRAINAGE FACILITIES

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$$Q = 0.56 \frac{Z}{n} y^{8/3} S^{1/2}$$

Z = RECIPROCAL OF CROSS SLOPE

$$n = 0.016$$

y = DEPTH OF FLOW

S = SLOPE OF STREET

$$Q = 0.56 \left[ \frac{1/0.02 (0.373)^{8/3}}{0.016} + \frac{1/0.02 (0.073)^{8/3}}{0.016} + \frac{1/0.083 (0.167)^{8/3}}{0.016} - \frac{1/0.02 (0.040)^{8/3}}{0.016} \right] \sqrt{S}$$

$$Q = 127.77 \sqrt{S} \quad \text{FOR 6" VERTICAL CURB FLOWING FULL ON 30' A-A STREET}$$



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## DESIGN CALCULATIONS

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TYPE 13 INLET COOH STANDARD M-604-AB

24 OPENINGS x  $(7\frac{5}{16}'' \times 1\frac{1}{4}'')$  = 2.13 SF/GRATING

REDUCE BY 50% TO ALLOW FOR CLOGGING = 1.06 SF

SAY 1 SF/INLET

$$Q = CA \sqrt{2gh}$$

USE 1 FT. SWP

$$Q = (0.5)(1.0) \sqrt{2g(1)'} = 4 \text{ CFS}$$

$$Q = 4 \text{ CFS}$$

DIOR INLET CAPACITIES FROM COLORADO SPRINGS  
"DETERMINATION OF STORM RUNOFF CRITERIA"

(SEE TABLE 6)



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## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE FACILITIES

Designer BDP Date 12-6-83

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①

PART OF BASIN C << 1 CFS 5YR 1.7 CFS 100YR

STREET SLOPE  $\pm 1\%$   $Q_{ALLOW} = 12.78$  CFS

DESIGN FOR 5YR STORM

USE PAN ACROSS DRIVEWAY

②

BASIN A 2.1 CFS 5YR 9.2 CFS 100YR

STREET SLOPE = 5%  $Q_{ALLOW} = 28.6$  CFS

4' DIOR  $Q_{ALLOW} = 8.6$  CFS

DESIGN FOR 5YR STORM

$E Q = 0.1 + 2.1 = 2.2$  CFS

③

BASIN K 2.1 CFS 5YR 7.3 CFS 100YR

STREET SLOPE = 2%  $Q_{ALLOW} = 18.1$  CFS

4' DIOR  $Q_{ALLOW} = 6.5$  CFS

DESIGN FOR 100YR DUE TO LOW POINT

$E Q = 2.2 + 7.3 = 9.5$  CFS

④

$\frac{1}{2}$  BASIN Q 4.9 CFS 5YR 13.9 CFS 100YR

SLOPE ACROSS LOT = 3.6% USE 2%

USE 2GA DIOR INLETS - DESIGN FOR 5YR STORM

4' DIOR  $Q_{ALLOW} = 6.5$  CFS

$E Q = 9.5 + 4.9 = 14.4$  CFS



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## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE FACILITIES

Designer BDP Date 12-6-83

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5

BASIN P 2.9 CFS 5YR 6.5 CFS 100 YR

SLOPE ACROSS LOT = 3% USE 1.5%

DESIGN FOR 5YR STORM

4' DIOR  $Q_{ALLOW} = 7.7$  CFS

$EQ = 14.4 + 2.9 = 17.3$  CFS

6

BASIN I 1.3 CFS 5YR 4.5 CFS 100 YR

BASIN J 0.1 CFS 5YR 1.4 CFS 100 YR

1.4 CFS

5.9 CFS

STREET SLOPE = 4%  $Q_{ALLOW} = 25.55$  CFS

DESIGN FOR 5YR STORM

4' DIOR  $Q_{ALLOW} = 4.4$  CFS

$EQ = 17.3 + 1.4 = 18.7$  CFS

7

BASIN W 2.0 CFS 5YR 6.9 CFS 100 YR

STREET SLOPE = 1%  $Q_{ALLOW} = 12.77$  CFS

DESIGN FOR 5YR

4' DIOR  $Q_{ALLOW} = 8.6$  CFS

$EQ = 18.7 + 2.0 = 20.7$  CFS



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## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE  
 Detail DRAINAGE FACILITIES  
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 Checker \_\_\_\_\_ Date \_\_\_\_\_

8	70% BASIN X	10.5 CFS 5YR	26.8 CFS 100YR
	BASIN Y	0.3 CFS 5YR	1.2 CFS 100YR
		<u>10.8 CFS</u>	<u>28.0 CFS</u>
	SLOPE ACROSS LOT = 4% USE 2%		
	SLOPE ALONG CURB = 1.3% Q <sub>ALLOW</sub> = 14.57 CFS		
	DESIGN FOR 5YR STORM		
	10" DIOR Q <sub>ALLOW</sub> = 10.9 CFS		
	EQ = 10.8 CFS		
9	1/2 BASIN FF	0.2 CFS 5YR	2.2 CFS 100YR
	SLOPE ACROSS LOT = 1.5% USE 0.75%		
	4" DIOR Q <sub>ALLOW</sub> = 7.5 CFS		
	DESIGN FOR 5YR STORM		
	EQ = 10.8 + 0.2 = 11.0 CFS		
10	1/2 BASIN FF	0.2 CFS 5YR	2.2 CFS 100YR
	SLOPE ACROSS LOT = 1.5% USE 0.75%		
	4" DIOR Q <sub>ALLOW</sub> = 7.5 CFS		
	DESIGN FOR 5YR STORM		
	EQ = 11.0 + 0.2 = 11.2 CFS		



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# DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE FACILITIES

Designer BDP Date 12-6-83

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△  
11

BASIN U  
 BASIN EE

2.1 CFS 5YR  
 0.1 CFS 5YR  
 2.2 CFS

6.5 CFS 100YR  
 0.1 CFS 100YR  
 6.6 CFS

STREET SLOPE = 2.5% Q ALLOW = 20.2 CFS

DESIGN FOR 5YR STORM

Q DIOR Q ALLOW = 5.7 CFS

EQ = 11.2 + 2.2 = 13.4 CFS

△  
12

COLLECT △ F △ 11 AT EXISTING MANHOLE

EQ = 20.7 + 13.4 = 34.1 CFS

SEE △ 26 FOR ADDITIONAL RUNOFF TO UNION



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## DESIGN CALCULATIONS

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Detail DRAINAGE FACILITIES

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13

PART OF BASIN C	<< 1 CFS 5YR	1.7 CFS	100 YR
BASIN D	0.1 CFS 5YR	2.8 CFS	100 YR
	0.2 CFS	4.5	

RUNOFF COLLECTS @ LOW POINT

STREET SLOPE = 2%  $Q_{ALLOW} = 18.1$  CFS

DESIGN FOR 100 YR STORM

4' DIOR  $Q_{ALLOW} = 6.5$  CFS

$E Q = 4.5$  CFS

14

BASIN L 10.7 CFS 5YR 26.0 CFS 100 YR

PARKING LOT SLOPE 3% N-S  $\mp$  2% E-W

CURB CAPACITY = 22.1 CFS  $\mp$  18.1 CFS

DESIGN FOR 100 YR

4' DIOR @ 2%  $Q_{ALLOW} = 6.5$  CFS

4' DIOR @ 3%  $Q_{ALLOW} = 5.2$  CFS

8' DIOR @ 3%  $Q_{ALLOW} = 14.8$  CFS

8' DIOR @ 2%  $Q_{ALLOW} = 12.5$

$\Sigma Q = 4.5 + 26.0 = 30.5$  CFS

15

BASIN S 10.5 CFS 5YR 24.0 CFS 100 YR

SLOPE ACROSS LOT = 4% USE 2%

DESIGN FOR 100 YR

6' DIOR  $Q_{ALLOW} = 12.2$  CFS USE 3EA.

$E Q = 30.5 + 24.0 = 54.5$  CFS





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## DESIGN CALCULATIONS

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16

$\frac{1}{2}$  BASIN Q (SEE 14) 4.9 CFS 5YR 13.9 CFS 100YR

SLOPE ACROSS LOT = 3.6% USE 1.8%

DESIGN FOR 100YR

4' DIOR Q ALLOW = 7.0 CFS USE 2EA

$$\Sigma Q = 54.5 + 13.9 = 68.4 \text{ CFS}$$

17

BASIN R 10.7 CFS 5YR 24.4 CFS 100YR

SLOPE ALONG CURB = 2% Q ALLOW = 18.07 CFS

NEED DIOR TO PICK UP 7.5 CFS

6' DIOR Q ALLOW = 12.2 CFS

$$24.4 - 7.5 = 16.9 \text{ CFS}$$

USE 1EA TYPE 13 @ LOW POINT

$$\Sigma Q = 68.4 + 24.4 = 92.8 \text{ CFS}$$

18

BASIN Y 6.8 CFS 5YR 20.0 CFS 100YR

DESIGN FOR 100YR

LOW POINT COLLECTS  $\pm$  30% OF BASIN  $\rightarrow$  6 CFS

SLOPE ALONG CURB = 2% SLOPE @ LOW POINT = 0.5% USE 0.5%

4' DIOR Q ALLOW = 6.3 CFS

REMAINDER OF BASIN  $\pm$  70%  $\rightarrow$  14 CFS

STREET SLOPE = 2% , 6' DIOR Q ALLOW = 12.2 CFS , USE 2EA

$$\Sigma Q = 92.8 + 20.0 = 112.8 \text{ CFS}$$



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## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE FACILITIES

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19

•  $\frac{1}{2}$  BASIN DD 2.4 CFS 5YR 5.8 CFS 100YR

DESIGN FOR 100 YR

SLOPE ACROSS LOT TO LOW POINT = 2.5% USE 1.25%

4' DIOR Q ALLOW = 8.2 CFS

SUB EQ = 5.8 CFS

• BASIN JJ 6.3 CFS 5YR 14.3 CFS 100YR

DESIGN FOR 100YR @ LOW POINT @ LOADING DOCK

TYPE B Q ALLOW = 4 CFS USE 4 GA

SUB EQ = 5.8 + 14.3 = 20.1 CFS

• BASIN II 10.3 CFS 5YR 23.3 CFS 100YR

DESIGN FOR 100YR SIZE DIOR @ 2%

6' DIOR Q ALLOW = 12.2 CFS USE 3 GA

SUB EQ = 20.1 + 23.3 = 43.4

• EQ = 112.8 + 43.4 = 156.2 CFS

20

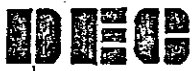
30% BASIN X (SEE 8) 4.5 CFS 5YR 11.5 CFS 100YR

DESIGN FOR 100YR

SLOPE ACROSS LOT = 2.6% CURB SLOPE = 0.9% USE 1%

6' DIOR Q ALLOW = 8.8 CFS USE 2 GA

EQ = 156.2 + 11.5 = 167.7 CFS



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## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE FACILITIES

Designer BDD Date 12-6-83

Checker \_\_\_\_\_ Date \_\_\_\_\_

21

BASIN HH 10.9 cfs 5YR 23.2 cfs 100YR

SLOPE ACROSS LOT  $\pm 2.5\%$  USE  $1\%$

DESIGN FOR 100 YR

4' DIOR Q ALLOW = 8.6 cfs - USE 20A

TYPE 1B Q ALLOW = 8.0 cfs - USE 20A

$$EQ = 167.7 + 23.2 = 190.9 \text{ cfs}$$

22

• BASIN RR 11.1 cfs 5YR 27.7 cfs 100 YR

DESIGN FOR 5YR

STREET SLOPE =  $1.6\%$  Q ALLOW = 16.2 cfs

DESIGN @  $1.5\%$  4' DIOR Q ALLOW = 7.7 cfs USE 20A

$$SUB EQ = 11.1 \text{ cfs}$$

• BASIN QQ 7.8 cfs 5YR 16.6 cfs 100YR

DESIGN FOR 5YR

STREET SLOPE =  $1.8\%$  Q ALLOW = 17.2 cfs

MOST OF BASIN ON W. SIDE

6' DIOR Q ALLOW = 11.6 cfs USE 10A W. SIDE

4' DIOR Q ALLOW = 7.0 cfs USE 10A E. SIDE IN CONJUNCTION W/ BASIN RR

$$SUB EQ = 11.1 + 7.8 = 18.9 \text{ cfs}$$

• EQ =  $190.9 + 18.9 = 209.8 \text{ cfs}$



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Detail DRAINAGE FACILITIES

Designer BDP Date 12-6-83

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23

BASIN H 320 CFS 100 YR

PER SEPTEMBER 29, 1983 LETTER FROM  
 DONELL JEFFRIES TO GARY HANNES,  
 CITY OF COLORADO SPRINGS

EQ = 320 CFS

24

• BASIN M 12.2 CFS 5 YR 30.4 CFS 100 YR

DESIGN FOR 100 YR

45% DRAINS TO N SIDE BLDG = 13.7 CFS

SLOPE ACROSS LOT = 4% USE 2%

6" DIOR ALLOW = 12.2 CFS USE 2EA

E SIDE BLDG & PARKING LOT @ 3/4%

20% BASIN = 6.1 CFS

USE 2EA 4" DIOR

35% BASIN = 10.6 CFS REMAINING

@ 4% 6" DIOR ALLOW = 10.6 CFS USE 2EA

SUB EQ = 30.4 CFS

• BASIN N 13.3 CFS 5 YR 24.7 CFS 100 YR

DESIGN FOR 100 YR

SLOPE ACROSS LOT = ± 4% USE 2%

6" DIOR ALLOW = 12.2 CFS USE 2EA

SUB EQ = 30.4 + 24.7 = 55.1 CFS

• EQ = 320 + 55.1 = 375.1 CFS

## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE FACILITIES

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25

• BASIN T 5.7 CFS 5YR 14.5 CFS 100 YR

DESIGN FOR 100 YR @ LOW POINT

TYPE 13  $Q_{ALLOW} = 4$  CFS USE 4' DIA.

SUB EQ = 14.5 CFS

• BASIN O 6.2 CFS 5YR 14.8 CFS 100 YR

DESIGN FOR 100 YR

CURB SLOPE =  $\pm 1\%$   $Q_{ALLOW} = 12.8$  CFS

4' DIA R  $Q_{ALLOW} = 8.6$  CFS USE 2' DIA

SUB EQ =  $14.5 + 14.8 = 29.3$  CFS

• EQ =  $375.1 + 29.3 = 404.4$  CFS

Flows from this point generally drain away from building. Colorado Springs requires design for 100 YR storm if  $EQ > 500$  CFS. This will occur once basin CC is reached. Design for 100 YR storm from this point.

26

• BASIN G 0.1 CFS 5YR 0.1 CFS 100 YR

DISCHARGES DIRECTLY TO CHANNEL

SUB EQ = 0.1 CFS

• 60% BASIN Z 4.4 CFS 5YR 10.1 CFS 100 YR

PARKING LOT SLOPE 2% 6' DIA R  $Q_{ALLOW} = 12.2$  CFS

• BASIN E 0.1 CFS 5YR 1.3 CFS 100 YR

BASIN F 0.4 CFS 5YR 2.2 CFS 100 YR

0.5 CFS 3.5 CFS

STREET SLOPE 2% 4' DIA R  $Q_{ALLOW} = 6.5$  CFS

• EQ =  $404.4 + 10.1 + 3.5 = 418.0$  CFS



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Project HEWLETT-PACKARD @ BRYARGATE

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127

BASIN CC

509 CFS 5YR 607.0 CFS 100YR (CUMULATIVE)

PER SEPTEMBER 29, 1983 LETTER FROM  
 DONALD JEFFRIES TO CARL HANDES,  
 CITY OF COLORADO SPRINGS

$$EQ = 509 - 320 + 418.0 = 607.0 \text{ CFS}$$

128

40% BASIN F

2.9 CFS 5YR 6.8 CFS 100YR

STREET SLOPE 2% 4' DIOR ALLOW = 6.5 CFS OR

$$EQ = 607.0 + 6.8 = 615.8 \text{ CFS}$$

129

1/2 BASIN DD (SEE 127)

2.4 CFS 5YR 5.8 CFS 100YR

STREET SLOPE = 2% 4' DIOR ALLOW = 6.5 CFS

$$EQ = 615.8 + 5.8 = 621.6 \text{ CFS}$$

130

• BASIN SS

15.0 CFS 5YR 33.2 CFS 100YR

STREET SLOPE = 2% 6' DIOR ALLOW = 12.2 CFS : 30%  
 SUB EQ = 33.2 CFS

• 75% BASIN AA

0.6 CFS 5YR 2.3 CFS 100YR

STREET SLOPE = 2% 4' DIOR ALLOW = 6.5 CFS

$$\text{SUB EQ} = 33.2 + 2.3 = 35.5 \text{ CFS}$$

$$EQ = 621.6 + 35.5 = 657.1 \text{ CFS}$$



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 Suite 300 Building 7  
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Sheet 16 of 18  
 Job No. 101

## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BIRMGATE  
 Detail DRAINAGE FACILITIES  
 Designer BDP Date 12-6-83  
 Checker \_\_\_\_\_ Date \_\_\_\_\_

31

• BASIN BB 1.0 CFS 5YR 7.0 CFS 100YR

DRAINS DIRECTLY TO CHANNEL

SUB EQ = 7.0 CFS

• 25% BASIN AA 0.2 CFS 5YR 0.8 CFS 100YR

RUN TO COMMON POINT w/ BASIN VV

• BASIN VV 0.1 CFS 5YR 1.4 CFS 100YR

STREET SLOPE = 2% 4' DIOR Q ALLOW = 6.5 CFS

SUB SUB EQ = 1.4 + 0.8 = 2.2 CFS

SUB EQ = 2.2 + 7.0 = 9.2 CFS

• EQ = 657.1 + 9.2 = 666.3 CFS

32

COLLECTION POINT

DESIGN FOR EQ FROM 22 & 31

EQ = 209.8 + 666.3 = 876.1 CFS



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# DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail DRAINAGE FACILITIES

Designer BDP Date 12-6-83

Checker \_\_\_\_\_ Date \_\_\_\_\_

33

• BASIN GG 10.6 CFS 5YR 25.8 CFS 100YR

30% (7.7 CFS) COLLECTS @ N. SIDE PLANTER

CURB SLOPE = 0.8% PARKING LOT SLOPE = 2.5%

4' DIOR @ 1% Q ALLOW = 8.6 CFS

20% (18.1 CFS) COLLECTS @ LOW POINT

TYRE 13 Q ALLOW = 0 CFS USE SPA.

• BASIN PP 5.2 CFS 5YR 18.2 CFS 100YR

STREET SLOPE = 0.4% SPA 0.5%

STREET CAPACITY = 9 CFS

12' DIOR Q ALLOW = 8.8 CFS

USE 2 SPA = 17.6 CFS ∴ 0.6 CFS CONTINUES TO L.P.

SUB EQ = 25.8 + 18.2 = 44.0 CFS

• EQ = 876.1 + 44.0 = 920.1 CFS

34

BASIN LL 0.7 CFS 5YR 2.9 CFS 100YR

BASIN NN 2.6 CFS 5YR 7.4 CFS 100YR

BASIN UU 0.0 CFS 5YR 0.5 CFS 100YR

BASIN OO 15.9 CFS 5YR 38.8 CFS 100YR

19.2 CFS

49.6 CFS

STREET SLOPE = ± 1.75%

4' DIOR Q ALLOW = 7.1 CFS - USE ON S. SIDE

6' DIOR Q ALLOW = 11.4 CFS - USE 4' DIA

EQ = 920.1 + 49.6 = 969.7 CFS





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Sheet 18 of 18  
 Job No. 101

# DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE  
 Detail DRAINAGE FACILITIES  
 Designer BDP Date 12-6-83  
 Checker \_\_\_\_\_ Date \_\_\_\_\_

35

BASIN MM  
 BASIN TT

0.0 cfs 5YR  
 0.0 cfs 5YR  
 0.0 cfs

0.1 cfs 100YR  
 1.2 cfs 100YR  
 1.3 cfs

COLLECT @ EXISTING 8' DIOR @ LEXINGTON/MENARD RIDGE

$$EQ = 969.7 + 1.3 = 971.0 \text{ cfs}$$

36

BASIN KK

1.2 cfs 5YR

5.0 cfs 100YR

COLLECT @ EXISTING FACILITIES ON UNION

**APPENDIX 3**  
**HYDRAULICS**



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# DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE  
 Detail HYDRAULICS  
 Designer BDP Date 12-15-83  
 Checker \_\_\_\_\_ Date \_\_\_\_\_

## PIPE DESIGN

PRELIMINARY SIZE OF PIPE BASED ON MANNING EQUATION.  $n = 0.015$  USED TO ACCOUNT FOR HEAD LOSSES. FINAL DESIGN TO BE BASED ON  $n = 0.013$  & WILL CONSIDER HEAD LOSSES.

## CHANNEL DESIGN

CHANNEL WILL BE DESIGNED FOR SUPERCRITICAL FLOW. CHANNEL CAPACITY VARIES FROM 320 CFS TO 732 CFS. AT MAXIMUM  $Q$ ,  $S = 0.017$  FT/FT,  $B = 6$  FT,  $Z = 1.5:1$ ,  $y = 2.86$  FT. FREEBOARD = 1.0' OR  $0.25y$ , WHICHEVER IS GREATER. USE 1.0' FREEBOARD. SPECIAL DESIGN CONSIDERATIONS FOR COLORADO SPRINGS CRITERIA WILL BE MADE FOR SUPERCRITICAL CHANNEL.

## CULVERT SIZING @ $\Delta$

SEE BUREAU OF PUBLIC ROADS CHARTS 1 & 8.  
 USE 8' x 4' RCBC (8' WIDTH & 4' HEIGHT).

## D/S FROM CULVERT

USE MANNING FOR CAPACITY OF 8' x 4' RCBC.  
 $n = 0.015$  &  $S = 0.025$  FT/FT

## EXISTING 66" Ø CULVERTS @ LEXINGTON

121.5 LF @ 1/2", 20".  
 $Q_{ALLOW} = 672$  CFS  
 PIPES WILL FLOW UNDER PRESSURE

@ CULVERT ENTRANCE REQUIRED HEADWATER DEPTH = 13.5 FT  
 SEE BUREAU OF PUBLIC ROADS CHART 2

## CHECK EXISTING CHANNEL

$S = 0.005$  FT/FT  $B = 6$  FT  $Z = 1.5:1$   $n = 0.015$   $y = 5.5$  FT  $Q = 1,150$  CFS  
 USING THIS PUN,  $CO = 1150 - 675 + 732 = 1207$   
 $y = 5.63$  FT.  $\therefore 0.87$  FT FREEBOARD AVAILABLE.

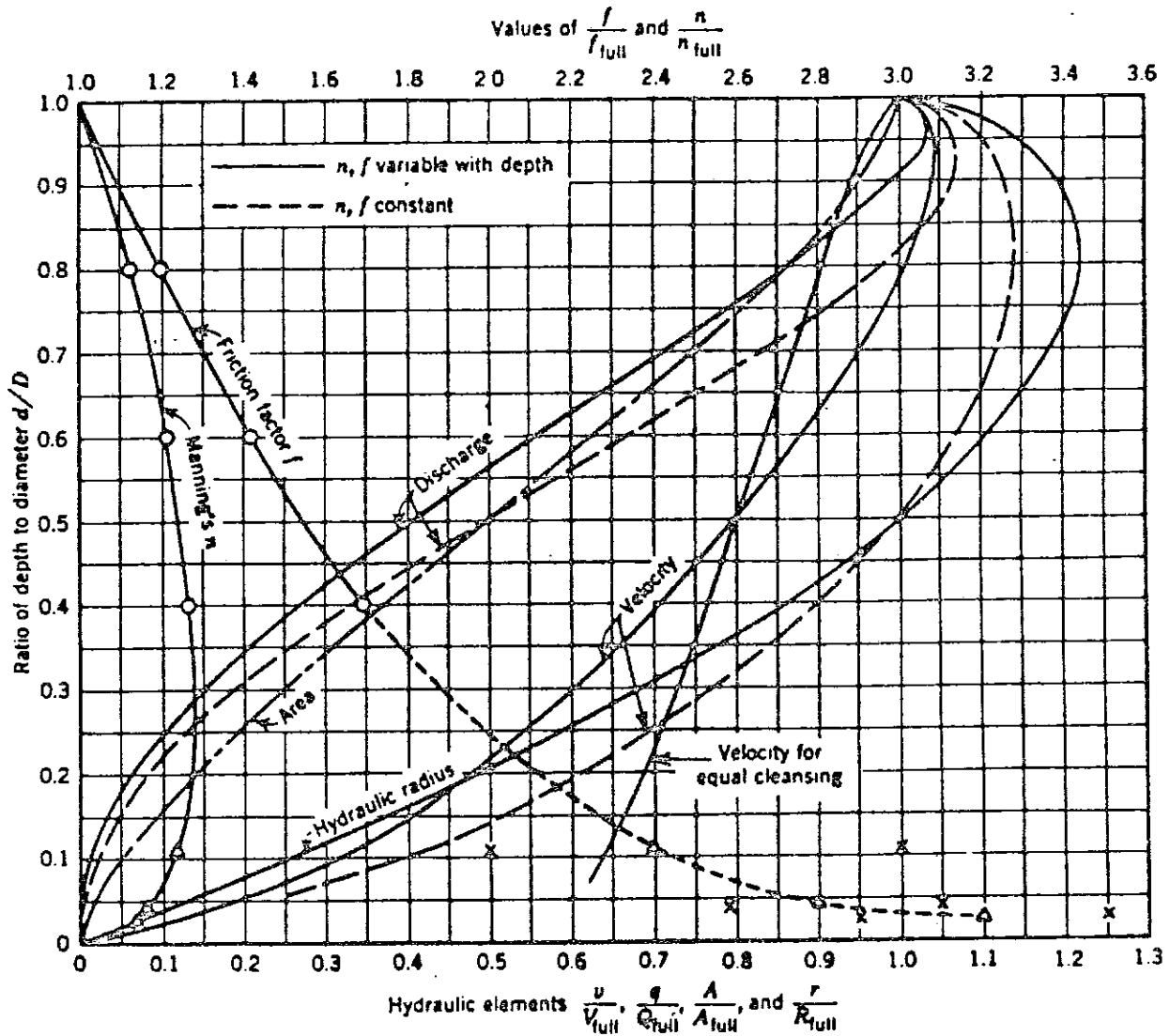
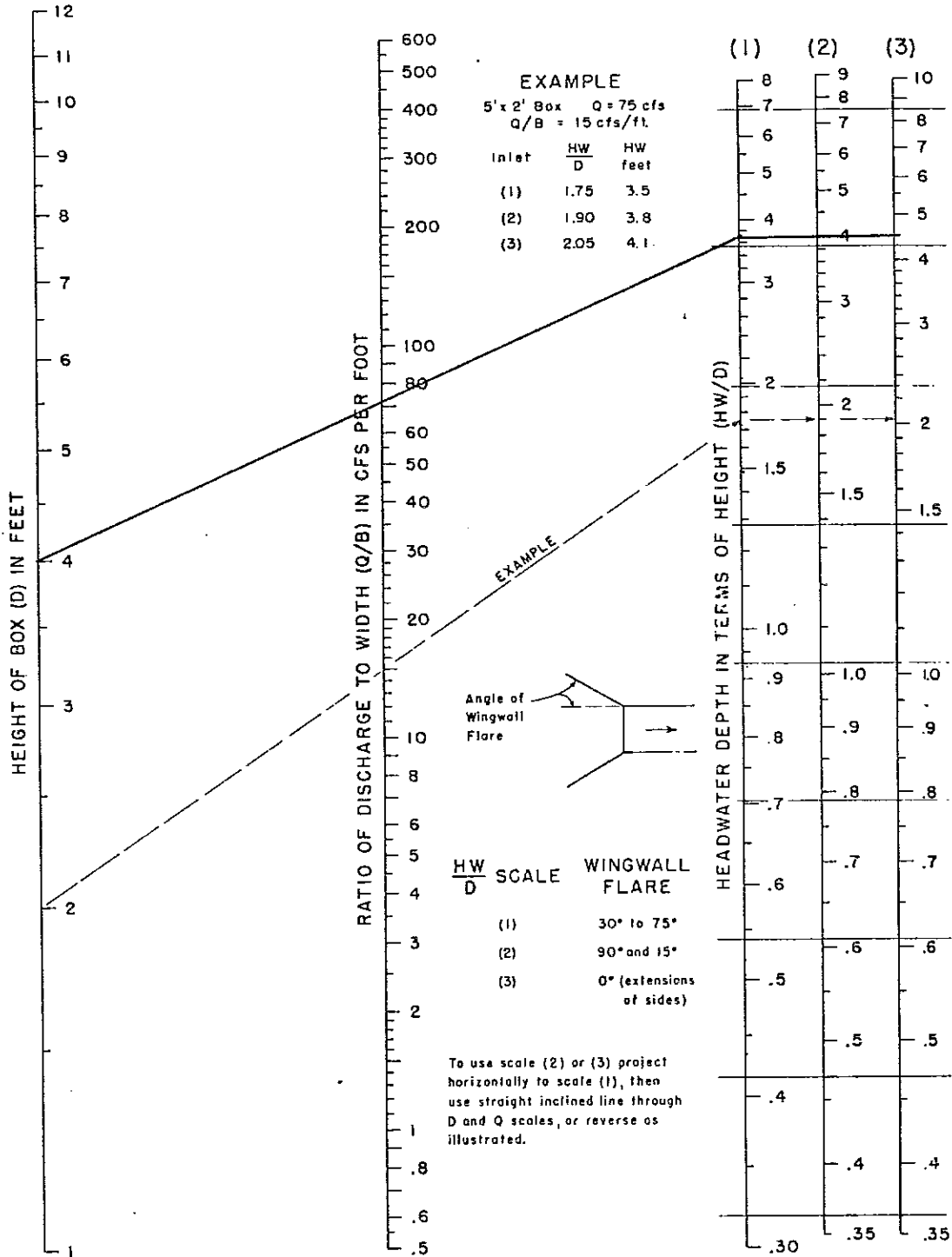


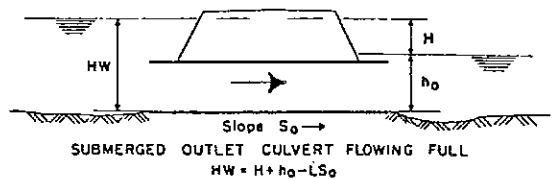
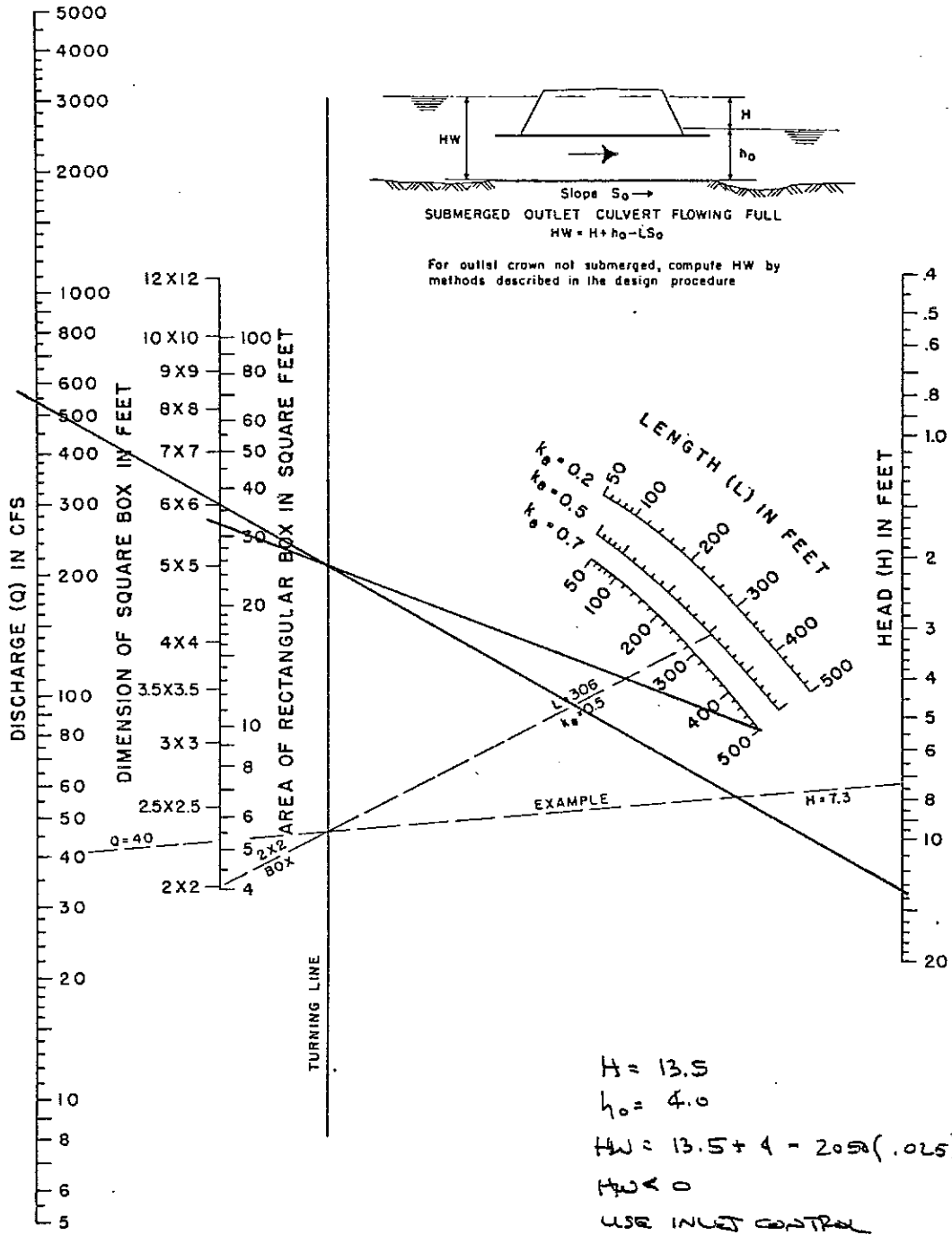
FIGURE 8-1. HYDRAULIC ELEMENTS OF CIRCULAR CONDUITS (2)

# CHART I



HEADWATER DEPTH FOR BOX CULVERTS WITH INLET CONTROL

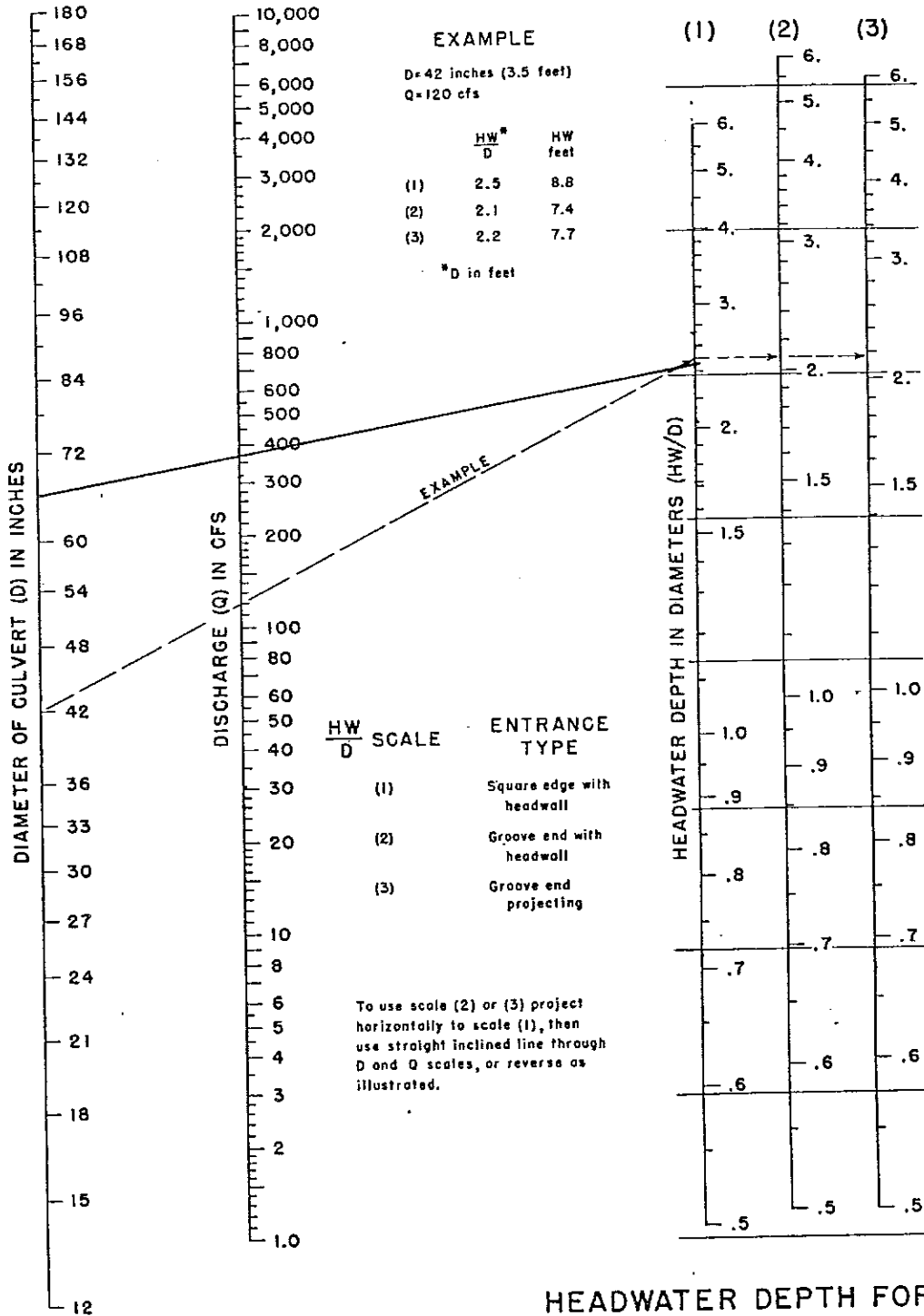
# CHART 8



For outlet crown not submerged, compute HW by methods described in the design procedure

HEAD FOR  
 CONCRETE BOX CULVERTS  
 FLOWING FULL  
 $n = 0.012$

# CHART 2



HEADWATER DEPTH FOR  
 CONCRETE PIPE CULVERTS  
 WITH INLET CONTROL

**APPENDIX 4**  
**PRELIMINARY DESIGN DATA**



# STORM DRAINAGE SYSTEM PRELIMINARY DESIGN DATA

HEWLETT-PACKARD @ BIRMGATE BDP 12-12-83 101

1/1

DESIGN POINT	BASIN	AREA (SQ. MI.)	% AREA (SQ. MI.)	CN	CN	BASIN HEIGHT (FT)	BASIN LENGTH (FT)	BASIN $t_c$ (HR)	BASIN $t_c$ (HR)	Σ TIME (HR)	CSM INCH	5YR RUNOFF (IN)	5YR PEAK (CFS)	100YR RUNOFF (IN)	100YR PEAK (CFS)	PIPE DIAMETER (IN)	PIPE SLOPE (FT/FT)	PIPE VELOCITY (FPS)
	POINT											<<1						
1												<<1				PAN		
	A											2.1						
2												2.2				18	.038	
	K											2.1		7.3				
3												9.5				18	.040	
	50% D											4.9						
4												14.4				18	.033	
	P											2.9						
5												17.3				18	.038	
	H											1.3						
	J											0.1						
6												18.7				21	.024	



# STORM DRAINAGE SYSTEM PRELIMINARY DESIGN DATA

HEWLETT-PACKARD @ BRIARGATE

BDP

12-12-83

101

2/7

DESIGN POINT	BASIN	AREA (SQ. MI.)	Σ AREA (SQ. MI.)	Σ	CN	W	BASIN HEIGHT (FT)	BASIN LENGTH (FT)	BASIN $t_c$ (HR)	BASIN $t_e$ (HR)	Σ TIME (HR)	CSM INCH	5YR RUNOFF (IN)	5YR PEAK (CFS)	100YR RUNOFF (IN)	100YR PEAK (CFS)	PIPE DIAMETER (IN)	PIPE SLOPE (FT/FT)	PIPE VELOCITY (CFS)
	W												2.0						
△													20.7				24	.015	
	70% X												10.5						
	V												0.3						
△													10.8				18	.025	
	50% FF												0.2						
△													11.0				18	.020	
	50% FF												0.2						
△													11.2				18	.018	
	U4												2.1						
	EE												0.1						
△													13.4				21	.019	
	△												20.7						
	△												13.4						
△													34.1						

EXISTING  
36

# STORM DRAINAGE SYSTEM PRELIMINARY DESIGN DATA

HEWLETT-PACKARD @ BIRMGATE BDP 12-12-83 101

3/7

DESIGN POINT	BASIN	AREA (SQ. MI.)	W	L	BASIN HEIGHT (FT)	BASIN LENGTH (FT)	BASIN $t_c$ (HR)	BASIN $t_c$ (HR)	Σ TIME (HR)	CSM INCH	5YR RUNOFF (IN)	5YR PEAK (CFS)	100YR RUNOFF (IN)	100YR PEAK (CFS)	PIPE DIAMETER (IN)	PIPE SLOPE (FT/FT)	PIPE VELOCITY (FPS)
	PART C	.007	48		80	280	.021										
	D	.009	52		101	1,110	.109										
13		.016	50						.109	1250			0.20	3.9	18	0.010	4.27
	L	.010	83		14	620	.057										
14		.026	63				.026		.135	1200			0.66	20.6	24	0.013	7.27
	S	.008	86		4	330	.042	.005						24.0	24	0.025	9.67
15		.034	68				.025		.160	1150			0.90	35.2	24	0.040	12.73
	50% Q	.010	89		5	670	.169	.011							18	0.019	6.15
16		.044	73				.002		.169	1130			1.18	58.7	33	0.026	12.19
	R	.009	86		12	850	.098								21	0.030	
17		.053	75				.006		.175	1120			1.30	77.2	36	0.025	12.93
	Y	.011	76		14	780	.080	.027							24	0.020	8.38
18		.064	75				.005		.180	1105			1.30	92.1	42	0.018	11.92



# STORM DRAINAGE SYSTEM PRELIMINARY DESIGN DATA

HEWLETT-PACKARD @ BLYARGATE

BDP

12-12-83

101

4/7

DESIGN POINT	BASIN	AREA (SQ. MI.)	E AREA (SQ. MI.)	N	NW	BASIN LENGTH (FT)	BASIN $t_c$ (HR)	BASIN $t_e$ (HR)	$\Sigma$ TIME (HR)	CSM INCH	5YR RUNOFF (IN)	5YR PEAK (CFS)	100YR RUNOFF (IN)	100YR PEAK (CFS)	PIPE DIAMETER (IN)	PIPE SLOPE (FT/FT)	PIPE VELOCITY (FPS)
	50% DD	.002		82		8	420	.042	.009						18	0.017	5.86
	JJ	.005		86		5	500	.069	.014						24	0.014	7.44
	11	.008		86		5	470	.062	.009						30	0.025	11.11
19			.079		77			<u>.009</u>	.189	1095			1.43	123.7	42	0.030	15.38
	30% X	.006		81		9	970	<u>.224</u>	<u>.019</u>					11.5	18	0.020	7.45
20			.085		78				.243	1005			1.50	127.9	54	0.010	10.39
	HH	.007		89		7	470	.054	.003					23.2	24	0.020	8.82
21			.092		78			<u>.008</u>	.251	995			1.50	137.3	60	0.006	8.72
	RR	.013		82		9	830	.137									
	QQ	.005		89		8	480	.051									
22			.110		79			<u>.019</u>	.270	970			1.57	167.5	60	.009	10.69



# STORM DRAINAGE SYSTEM PRELIMINARY DESIGN DATA

HEWLETT-PACKARD @ BIRMGATE BDP

12-12-83

101

51

DESIGN POINT	BASIN	AREA (SQ. MI.)	% AREA (SQ. MI.)	Z	CN	BASIN HEIGHT (FT)	BASIN LENGTH (FT)	BASIN $t_c$ (HR)	BASIN $t_e$ (HR)	$\Sigma$ TIME (HR)	CSM INCH	5YR RUNOFF (IN)	5YR PEAK (CFS)	100YR RUNOFF (IN)	100YR PEAK (CFS)	PIPE DIAMETER (IN)	PIPE SLOPE (FT/FT)	PIPE VELOCITY (FPS)
	H*	.297		75			4,700	0.38										
23			.297		75					0.38	830			1.30	320	66	0.018	16.42
	M	.014		82		8	875	.122	.004							36	0.005	5.61
	N	.006		95		19	550	.058	.026							42	0.005	6.41
24			.37		76				0.13	.393	825			1.37	358	72	0.013	14.93
																		15.36
	T	.004		81		12	850	.098	.010							21	0.013	6.72
	O	.006		84		21	850	.102	.014							30	0.007	6.29
25			.329		76				0.005	.398	820			1.37	370		0.014	15.88
	G	.007		39		56	1800	.282										
	60% Z	.004		85		10	560	.058										
	E	.003		52		55	700	.097										
	F	.004		63		57	2040	.167										
26			.347		75				0.006	.404	815			1.30	368		0.014	15.88
	CC*	.533		74			6,100	0.46										
27			.583		74					0.46	770			1.24	557		0.017	19.12

\* PER 9-29-83 DONELL JEFFRIES LETTER



Denver Engineering Corporation

# STORM DRAINAGE SYSTEM PRELIMINARY DESIGN DATA

HEWLETT-PACKARD @ BPIARGATE BDP

12-12-83 101

6/7

DESIGN POINT	BASIN	AREA (SQ. MI.)	Σ AREA (SQ. MI.)	N	N W	BASIN HEIGHT (FT)	BASIN LENGTH (FT)	BASIN $t_c$ (HR)	BASIN $t_c$ (HR)	Σ TIME (HR)	CSM INCH	5YR RUNOFF (IN)	5YR PEAK (CFS)	100YR RUNOFF (IN)	100YR PEAK (CFS)	PIPE DIAMETER (IN)	PIPE SLOPE (FT/FT)	PIPE VELOCITY (FPS)	
	40% B	.002		85		10	560	.058											
28			.585		74				.000	.460	770			1.24	559			$B=6$ $Z=1.5$ $y=2.85$	19.09
	50% DD	.002		82		10	750	.091											
29			.587		74				.007	.467	765			1.24	557			$B=6$ $Z=1.5$ $y=2.84$	19.12
	SS	.011		87		17	700	.063											
	75% AA	.002		69		31	1530	.152											
30			.600		74				.010	.477	760			1.24	565			$B=6$ $Z=1.5$ $y=2.86$	19.20
	BB	.009		60			2230	.031											
	25% AA	.001		69		11	700	.069											
	VV	.004		54		41	1650	.186											
31			.614		74				.010	.487	750			1.24	571	8x4	0.025	22.80	
	22	.110		79				.270											
	31	.614		74				.487											
32			.724		75				.003	.490	745			1.30	701	8x4	0.025	24.07	



# STORM DRAINAGE SYSTEM PRELIMINARY DESIGN DATA

HEWLETT-PACKARD @ BIRMGARRE

BDP

12-12-83

101

7/7

DESIGN POINT	BASIN	AREA (SQ. MI.)	% AREA (SQ. MI.)	N	W	BASIN PERMIT (FT)	BASIN LENGTH (FT)	BASIN $t_c$ (HR)	BASIN $t_c$ (HR)	$\Sigma$ TIME (HR)	CSM INCH	5YR RUNOFF (IN)	5YR PEAK (CFS)	100YR RUNOFF (IN)	100YR PEAK (CFS)	PIPE DIAMETER (IN)	PIPE SLOPE (FT/FT)	PIPE VELOCITY (FPS)
	GG	.011		83		9	800	.106	.028						25.8	27	0.010	7.02
	PP	.012		71		10	470	.045	.003						44.0	33	0.015	9.26
33			.747		75			.006		.496	740			1.30	719	8x4	0.025	24.23
	LL	.003		66		10	750	.129										
	NN	.007		77		16	910	.094										
	UU	.004		47		15	1500	.208										
	OO	.015		83		19	550	.061							49.6	30	0.020	
34			.771		75			.008		.504	730			1.30	732	8x4	0.025	24.34
35															732	8x4	0.025	24.34



**APPENDIX 5**  
**COST ESTIMATE**



<b>DEES</b> Denver Engineering Corporation 1626 Cole Boulevard Suite 300 Building 7 Golden, Colorado 80401	<b>QUANTITY TAKE-OFF SHEET</b>	SHEET <u>1</u> OF <u>19</u> JOB NO. <u>101</u> DATE <u>12-13-83</u> PREPARED BY <u>BDP</u> CHECKED BY
PROJECT NAME <u>HEWLETT-PACKARD @ BRIA GATE</u> LOCATION <u>COLORADO SPRINGS, COLORADO</u>		PROJECT DESCRIPTION <p style="text-align: center; font-weight: bold;">STORM DRAINAGE</p>

ITEM NO.	DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST
1					
2	4' DIOR * 0'-10'	1	EA		
3	18" $\phi$ RCP *	250	LF		
	5' $\phi$ MH *	1	EA		
	18" $\phi$ RCP	260	LF		
	4' DIOR	1	EA		
4	18" $\phi$ RCP *	210	LF		
	4' $\phi$ MH *	1	EA		
	18" $\phi$ RCP	50	LF		
	4' DIOR	1	EA		
	18" $\phi$ RCP	170	LF		
	4' DIOR	1	EA		
5	18" $\phi$ RCP *	280	LF		
	4' $\phi$ MH *	1	EA		
	18" $\phi$ RCP	55	LF		
	4' DIOR	1	EA		
6	18" $\phi$ RCP *	180	LF		
	5' $\phi$ MH *	1	EA		
	18" $\phi$ RCP *	55	LF		
	4' DIOR *	1	EA		
7	21" $\phi$ RCP *	160	LF		
	5' $\phi$ MH *	1	EA		
	18" $\phi$ RCP	70	LF		
	4' DIOR	1	EA		
8	5' $\phi$ MH	1	EA		
	18" $\phi$ RCP	70	LF		
	10' DIOR	1	EA		
9	18" $\phi$ RCP	240	LF		
	5' $\phi$ MH	1	EA		
	18" $\phi$ RCP	70	LF		
	4' DIOR	1	EA		

V. DEES - BDP

<b>DEEC</b>	<b>QUANTITY TAKE-OFF SHEET</b>	SHEET 2 OF 19
Denver Engineering Corporation	PROJECT NAME HEWLETT-PACKARD@BRIARGATE	JOB NO. 101
1626 Cole Boulevard Suite 300 Building 7 Golden, Colorado 80401	LOCATION COLORADO SPRINGS, COLORADO	DATE 12-13-83
PROJECT DESCRIPTION  STORM DRAINAGE		PREPARED BY BDP
		CHECKED BY

ITEM NO.	DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST
△10	18" ∅ RCP 0'-10'	280	LF		
	5' ∅ MH	1	EA		
	18" ∅ RCP	55	LF		
	4' DIOR	1	EA		
△11	18" ∅ RCP	70	LF		
	4' DIOR *	1	EA		
△12	21" ∅ RCP *	50	LF		
	24" ∅ RCP *	345	LF		
	5' ∅ MH *	1	EA		
	24" ∅ RCP *	395	LF		
	5' ∅ MH *	1	EA		
	24" ∅ RCP * v	135	LF		
	<b>SUBTOTAL ①</b>				
	4' DIOR 0'-10'	10	EA		
	10' DIOR	1	EA		
	4' ∅ MH	2	EA		
	5' ∅ MH	8	EA		
	18" ∅ RCP	2,365	LF		
	21" ∅ RCP	210	LF		
	24" ∅ RCP v	875	LF		

**DEES**

## QUANTITY TAKE-OFF SHEET

SHEET 3 OF 19

Denver Engineering Corporation


1626 Cole Boulevard  
Suite 300 Building 7  
Golden, Colorado 80401PROJECT NAME  
HEWLETT-PACKARD @ BRIA GATE  
LOCATION  
COLORADO SPRINGS, COLORADOJOB NO.  
101  
DATE  
12-13-83

PROJECT DESCRIPTION

PREPARED BY  
BDP  
CHECKED BY

## STORM DRAINAGE

ITEM NO.	DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST
13	4' DIOR 10'-15'	1	EA		
14	18" $\phi$ RCP 10'-15'	400	LF		
	4' DIOR 10'-15'	1	EA		
	18" $\phi$ RCP 10'-15'	45	LF		
	8' DIOR 10'-15'	1	EA		
	24" $\phi$ RCP 10'-15'	160	LF		
	8' DIOR 10'-15'	1	EA		
15	24" $\phi$ RCP 15'-20'	380	LF		
	5' $\phi$ MH 15'-20'	1	EA		
	24" $\phi$ RCP 15'-20'	270	LF		
	5' $\phi$ MH 15'-20'	1	EA		
	24" $\phi$ RCP 0'-10'	170	LF		
	18" $\phi$ RCP 0'-10'	70	LF		
	6' DIOR 0'-10'	1	EA		
	6' DIOR 0'-10'	1	EA		
	18" $\phi$ RCP 0'-10'	10	LF		
	6' DIOR 0'-10'	1	EA		
16	24" $\phi$ RCP 15'-20'	95	LF		
	5' $\phi$ MH 30'-35'	1	EA		
	24" $\phi$ RCP 15'-20'	50	LF		
	4' DIOR 15'-20'	1	EA		
	18" $\phi$ RCP 15'-20'	210	LF		
	4' DIOR 15'-20'	1	EA		
17	33" $\phi$ RCP 30'-35'	30	LF		
	33" $\phi$ RCP 15'-20'	190	LF		
	33" $\phi$ RCP 10'-15'	40	LF		
	6' $\phi$ MH 15'-20'	1	EA		
	21" $\phi$ RCP 10'-15'	100	LF		
	TYPE 13 10'-15'	4	EA		
	18" $\phi$ RCP 10'-15'	270	LF		
	6' DIOR 10'-15'	1	EA		

 <b>Denver Engineering Corporation</b> 1626 Cole Boulevard Suite 300 Building 7 Golden, Colorado 80401	<h2 style="margin:0;">QUANTITY TAKE-OFF SHEET</h2>	SHEET <span style="font-size: 2em;">4</span> OF <span style="font-size: 2em;">19</span>
PROJECT NAME <b>HEWLETT-PACKARD @ BIRMGATE</b>	JOB NO. 101	
LOCATION <b>COLORADO SPRINGS, COLORADO</b>	DATE 12-13-83	
PROJECT DESCRIPTION <h3 style="text-align: center; margin-top: 10px;">STORM DRAINAGE</h3>	PREPARED BY <b>BDP</b>	
	CHECKED BY	

ITEM NO.	DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST
18	36" $\phi$ RCP 20'-25'	250	LF		
	6' $\phi$ MH 20'-25'	1	EA		
	24" $\phi$ RCP 20'-25'	145	LF		
	5' $\phi$ MH 15'-20'	1	EA		
	24" $\phi$ RCP 15'-20'	225	LF		
	5' $\phi$ MH 15'-20'	1	EA		
	24" $\phi$ RCP 10'-15'	50	LF		
	5' $\phi$ MH 10'-15'	1	EA		
	24" $\phi$ RCP 10'-15'	150	LF		
	5' $\phi$ MH 10'-15'	1	EA		
	24" $\phi$ RCP 0'-10'	210	LF		
	4' DIOR 0'-10'	1	EA		
	24" $\phi$ RCP 0'-10'	10	LF		
	6' DIOR 0'-10'	1	EA		
	18" $\phi$ RCP 0'-10'	25	LF		
	6' DIOR 0'-10'	1	EA		
19	42" $\phi$ RCP 25'-30'	200	LF		
	42" $\phi$ RCP 30'-35'	190	LF		
	6' $\phi$ MH 30'-35'	1	EA		
	30" $\phi$ RCP 10'-15'	270	LF		
	6' DIOR 10'-15'	1	EA		
	18" $\phi$ RCP 10'-15'	20	LF		
	6' DIOR 10'-15'	1	EA		
	30" $\phi$ RCP 10'-15'	55	LF		
	6' DIOR 10'-15'	1	EA		
	24" $\phi$ RCP 10'-15'	120	LF		
	5' $\phi$ MH 0'-10'	1	EA		
	24" $\phi$ RCP 0'-10'	120	LF		
	5' $\phi$ MH 0'-10'	1	EA		
	24" $\phi$ RCP 0'-10'	50	LF		
	5' $\phi$ MH 0'-10'	1	EA		
	24" $\phi$ RCP 0'-10'	75	LF		
	TYPE 13 0'-10'	4	EA		



QUANTITY TAKE-OFF SHEET

SHEET 5 OF 19

Denver Engineering Corporation

1626 Cole Boulevard  
Suite 300 Building 7  
Golden, Colorado 80401

PROJECT NAME  
HEWLETT-PACKARD @ BRIAARGATE  
LOCATION  
COLORADO SPRINGS, COLORADO

JOB NO.  
101  
DATE  
12-13-83

PROJECT DESCRIPTION

PREPARED BY  
BDP  
CHECKED BY

STORM DRAINAGE

ITEM NO.	DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST
	18" Ø RCP 0'-10'	180	LF		
	4' DIOR 0'-10'	1	EA		
20	42" Ø RCP 30'-35'	100	LF		
	6' Ø MH 30'-35'	1	EA		
	18" Ø RCP 10'-15'	260	LF		
	6' DIOR 10'-15'	1	EA		
	18" Ø RCP 0'-10'	250	LF		
	6' DIOR 0'-10'	1	EA		
21	54" Ø RCP 30'-35'	60	LF		
	54" Ø RCP 15'-20'	240	LF		
	SPECIAL MH 15'-20'	1	EA		
	24" Ø RCP 10'-15'	100	LF		
	4' DIOR 10'-15'	1	EA		
	18" Ø RCP 0'-10'	45	LF		
	4' DIOR 0'-10'	1	EA		
	18" Ø RCP 0'-10'	30	LF		
	TYPE 13 0'-10'	2	EA		
22	60" Ø RCP 15'-20'	340	LF		
	60" Ø RCP 10'-15'	20	LF		
	SPECIAL MH 10'-15'	1	EA		
	60" Ø RCP 10'-15'	255	LF		
	SPECIAL MH 10'-15'	1	EA		
	18" Ø RCP 10'-15'	15	LF		
	6' DIOR 10'-15'	1	EA		
	24" Ø RCP 0'-10'	90	LF		
	4' DIOR 0'-10'	1	EA		
	24" Ø RCP 0'-10'	175	LF		
	4' DIOR 0'-10'	1	EA		





Denver Engineering Corporation

1626 Cole Boulevard  
Suite 300 Building 7  
Golden, Colorado 80401

QUANTITY TAKE-OFF SHEET

SHEET 7 OF 19


PROJECT NAME  
HEWLETT-PACKARD @ BRIARGATE  
LOCATION  
COLORADO SPRINGS, COLORADO

JOB NO.  
101  
DATE  
12-13-83

PROJECT DESCRIPTION  
STORM DRAINAGE

PREPARED BY  
BDP  
CHECKED BY

ITEM NO.	DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST
	SUBTOTAL ② (CONT)				
	18" Ø RCP 0'-10'	610	LF		
	10'-15'	1,010	LF		
	15'-20'	210	LF		
	21" Ø RCP 10'-15'	100	LF		
	24" Ø RCP 0'-10'	900	LF		
	10'-15'	580	LF		
	15'-20'	1,020	LF		
	20'-25'	145	LF		
	30" Ø RCP 10'-15'	325	LF		
	33" Ø RCP 10'-15'	40	LF		
	15'-20'	190	LF		
	30'-35'	30	LF		
	36" Ø RCP 20'-25'	250	LF		
	42" Ø RCP 25'-30'	200	LF		
	30'-35'	290	LF		
	54" Ø RCP 15'-20'	240	LF		
	30'-35'	60	LF		
	60" Ø RCP 10'-15'	275	LF		
	15'-20'	340	LF		

 <b>Denver Engineering Corporation</b> 1626 Cole Boulevard Suite 300 Building 7 Golden, Colorado 80401	<b>QUANTITY TAKE-OFF SHEET</b>	SHEET 8 OF 19 JOB NO. 101 DATE 12-13-83 PREPARED BY BDP CHECKED BY
PROJECT NAME HEWLETT-PACKARD @BRIARSGATE LOCATION COLORADO SPRINGS, COLORADO		
PROJECT DESCRIPTION <b>STORM DRAINAGE</b>		

ITEM NO.	DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST
23	66" φ RCP ** 10'-15'	90	LF		
	SPECIAL MH ** 10'-15'	1	EA		
24	66" φ RCP ** 10'-15'	400	LF		
	SPECIAL MH ** 10'-15'	1	EA		
	66" φ RCP ** 10'-15'	365	LF		
	SPECIAL MH ** 10'-15'	1	EA		
	42" φ RCP 10'-15'	220	LF		
	5' φ MH 10'-15'	1	EA		
	42" φ RCP 10'-15'	200	LF		
	42" φ RCP 0'-10'	200	LF		
	18" φ RCP 0'-10'	20	LF		
	6' Dia R 0'-10'	1	EA		
	18" φ RCP 0'-10'	20	LF		
	6' Dia R 0'-10'	1	EA		
	5' φ MH 0'-10'	1	EA		
	36" φ RCP 0'-10'	100	LF		
	5' φ MH 0'-10'	1	EA		
	18" φ RCP 0'-10'	15	LF		
	6' Dia R 0'-10'	1	EA		
	18" φ RCP 0'-10'	15	LF		
	6' Dia R 0'-10'	1	EA		
	30" φ RCP 0'-10'	130	LF		
	5' φ MH 0'-10'	1	EA		
	30" φ RCP 0'-10'	55	LF		
	5' φ MH 0'-10'	1	EA		
	18" φ RCP 0'-10'	10	LF		
	4' Dia R 0'-10'	1	EA		
	18" φ RCP 0'-10'	10	LF		
	4' Dia R 0'-10'	1	EA		
	24" φ RCP 0'-10'	120	LF		
	5' φ MH 0'-10'	1	EA		
	24" φ RCP 0'-10'	60	LF		
	6' Dia R 0'-10'	1	EA		

XX = BE REIMBURSED AS CONCRETE CHAIRS



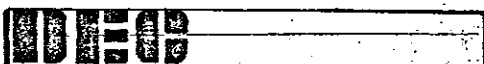
ITEM NO.		DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST
<b>DEEG</b> Denver Engineering Corporation 1626 Cole Boulevard Suite 300 Building 7 Golden, Colorado 80401						
PROJECT NAME			HEWLETT-PACKARD @ BRIARGATE		JOB NO. 101	
LOCATION			COLORADO SPRINGS, COLORADO		DATE 12-13-83	
PROJECT DESCRIPTION					PREPARED BY BDP	
STORM DRAINAGE					CHECKED BY	
		21" $\phi$ RCP 0'-10'	180	LF		
		6" DIOR 0'-10'	1	EA		
$\triangle$ 25		72" $\phi$ RCP * 10'-15'	70	LF		
		CONC. CHWL *	200	LF		
		30" $\phi$ RCP 0'-10'	320	LF		
		4' DIOR 0'-10'	1	EA		
		18" $\phi$ RCP 0'-10'	70	LF		
		4' DIOR 0'-10'	1	EA		
		21" $\phi$ RCP 0'-10'	220	LF		
		TYPE 13 0'-10'	4	EA		
$\triangle$ 26		CONC. CHWL. *	320	LF		
		18" $\phi$ RCP 0'-10'	50	LF		
		4' DIOR 0'-10'	1	EA		
		18" $\phi$ RCP 0'-10'	20	LF		
		6' DIOR 0'-10'	1	EA		
$\triangle$ 27		CONC. CHWL. *	125	LF		
$\triangle$ 28		CONC. CHWL. *	30	LF		
		18" $\phi$ RCP 0'-10'	70	LF		
		4' DIOR 0'-10'	1	EA		
$\triangle$ 29		CONC. CHWL. *	495	LF		
		18" $\phi$ RCP 0'-10'	70	LF		
		4' DIOR 0'-10'	1	EA		
$\triangle$ 30		CONC. CHWL. *	950	LF		
		18" $\phi$ RCP 0'-10'	50	LF		
		6' DIOR 0'-10'	1	EA		
		18" $\phi$ RCP 0'-10'	50	LF		
		6' DIOR 0'-10'	1	EA		
		18" $\phi$ RCP 0'-10'	70	LF		
		4' DIOR 0'-10'	1	EA		
		18" $\phi$ RCP 0'-10'	30	LF		
		6' DIOR 0'-10'	1	EA		

ITEM NO.		QUANTITY TAKE-OFF SHEET			SHEET 10 OF 19	
Denver Engineering Corporation		PROJECT NAME			JOB NO.	
1626 Cole Boulevard		HEWLETT-PACKARD @ BRIARGATE			101	
Suite 300 Building 7		LOCATION			DATE	
Golden, Colorado 80401		COLORADO SPRINGS, COLORADO			12-13-83	
PROJECT DESCRIPTION				PREPARED BY		
STORM DRAINAGE				BDP		
				CHECKED BY		
ITEM NO.	DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST	
31	CONCRETE *	700	LF			
	18" $\phi$ RCP 0'-10'	50	LF			
	4' DIOR 0'-10'	1	EA			
32	8'x4' RCBC * 15'-20'	230	LF			
	RCBC MH RISER *	13	LF			
	60" $\phi$ RCP 10'-15'	110	LF			
33	8'x4' RCBC * 15'-20'	435	LF			
	8'x4' RCBC * 20'-25'	120	LF			
	RCBC MH RISER *	18	LF			
	33" $\phi$ RCP 0'-10'	85	LF			
	12' DIOR 0'-10'	1	EA			
	21" $\phi$ RCP 0'-10'	270	LF			
	12' DIOR 0'-10'	1	EA			
	27" $\phi$ RCP 10'-15'	200	LF			
	5' $\phi$ MH 10'-15'	1	EA			
	27" $\phi$ RCP 10'-15'	235	LF			
	5' $\phi$ MH 10'-15'	1	EA			
	27" $\phi$ RCP 10'-15'	275	LF			
	TYPE B 0'-10'	5	EA			
	18" $\phi$ RCP 0'-10'	180	LF			
	4' DIOR 0'-10'	1	EA			
34	8'x4' RCBC * 20'-25'	335	LF			
	RCBC MH RISER *	22	LF			
	8'x4' RCBC * 20'-25'	400	LF			
	RCBC MH RISER *	18	LF			
	30" $\phi$ RCP 0'-10'	70	LF			
	5' $\phi$ MH 10'-15'	1	EA			
	30" $\phi$ RCP 0'-10'	80	LF			
	5' $\phi$ MH 10'-15'	1	EA			
	30" $\phi$ RCP 0'-10'	50	LF			
	4' DIOR 0'-10'	1	EA			
	30" $\phi$ RCP 0'-10'	25	LF			
	6' DIOR 0'-10'	1	EA			

<b>DEEP</b>		<b>QUANTITY TAKE-OFF SHEET</b>	SHEET 11 OF 19
Denver Engineering Corporation		PROJECT NAME	JOB NO.
1626 Cole Boulevard		HEWLETT-PACKARD @ BRIA GATE	101
Suite 300 Building 7		LOCATION	DATE
Golden, Colorado 80401		COLORADO SPRINGS, COLORADO	12-13-83

PROJECT DESCRIPTION	PREPARED BY
STORM DRAINAGE	BDP
	CHECKED BY

ITEM NO.	DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST
	18" $\phi$ RCP 0'-10'	150	LF		
	6' DIOR 0'-10'	1	EA		
	18" $\phi$ RCP 0'-10'	120	LF		
	6' DIOR 0'-10'	1	EA		
	18" $\phi$ RCP 0'-10'	120	LF		
	6' DIOR 0'-10'	1	EA		
35	8'x4' RCBC * 20'-25'	130	LF		
	RCBC MH. RISER *	16	LF		
	8'x4' RCBC * 15'-20'	400	LF		
	TRANSITION STRUCTURE *	1	EA		
	ENERGY DISSIPATION STRUCTURE *	1	EA		
	18" $\phi$ RCP * 0'-10'	75	LF		



QUANTITY TAKE-OFF SHEET

SHEET 12 OF 19

Denver Engineering Corporation  
 1626 Cole Boulevard  
 Suite 300 Building 7  
 Golden, Colorado 80401

PROJECT NAME  
 HEWLETT-PACKARD @ BRIARGATE  
 LOCATION  
 COLORADO SPRINGS, COLORADO

JOB NO.  
 101  
 DATE  
 12-13-83

PREPARED BY  
 BDP  
 CHECKED BY

PROJECT DESCRIPTION

STORM DRAINAGE

ITEM NO.	DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST
	SUBTOTAL (3)				
	4' DIOR 0'-10'	11	EA		
	6' DIOR 0'-10'	14	EA		
	12' DIOR 0'-10'	2	EA		
	TYPE 13 0'-10'	9	EA		
	5' Ø MH 0'-10'	5	EA		
	10'-15'	5	EA		
	SPECIAL MH 10'-15'	3	EA		
	18" Ø RCP 0'-10'	1,215	LF		
	21" Ø RCP 0'-10'	670	LF		
	24" Ø RCP 0'-10'	180	LF		
	27" Ø RCP 10'-15'	710	LF		
	30" Ø RCP 0'-10'	730	LF		
	33" Ø RCP 0'-10'	85	LF		
	36" Ø RCP 0'-10'	100	LF		
	42" Ø RCP 0'-10'	200	LF		
	10'-15'	420	LF		
	60" Ø RCP 10'-15'	110	LF		
	66" Ø RCP 10'-15'	855	LF		
	72" Ø RCP 10'-15'	70	LF		
	8'x4' RCBC 15'-20'	1,065	LF		
	20'-25'	985	LF		
	RCBC MH RISER	87	LF		
	CONCRETE CHANNEL	2,820	LF		
	TRANSITION STRUCTURE	1	EA		
	ENERGY DISSIPATION STRUCTURE	1	EA		
		1			

<b>DEEC</b>	<b>QUANTITY TAKE-OFF SHEET</b>	SHEET <u>13</u> OF <u>19</u>
Denver Engineering Corporation	PROJECT NAME HEWLETT-PACKARD @ BRIARGATE	JOB NO. 101
1626 Cole Boulevard Suite 300 Building 7 Golden, Colorado 80401	LOCATION COLORADO SPRINGS, COLORADO	DATE 12-13-83
PROJECT DESCRIPTION  STORM DRAINAGE		PREPARED BY BDP
		CHECKED BY

ITEM NO.	DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST
	TOTAL				
	4' DIOR      0'-10'	26	EA	1,000	26,000
	10'-15'	3	EA	1,250	3,750
	15'-20'	2	EA	1,750	3,500
	6' DIOR      0'-10'	20	EA	1,200	24,000
	10'-15'	6	EA	1,450	8,700
	8' DIOR      10'-15'	2	EA	1,650	3,300
	10' DIOR     0'-10'	1	EA	1,500	1,500
	12' DIOR     0'-10'	2	EA	1,600	3,200
	TYPE 13     0'-10'	15	EA	1,000	15,000
	10'-15'	4	EA	1,250	5,000
	4' Ø MH      0'-10'	2	EA	1,000	2,000
	5' Ø MH      0'-10'	16	EA	1,200	19,200
	10'-15'	7	EA	1,450	10,150
	15'-20'	4	EA	1,950	7,800
	30'-35'	1	EA	4,000	4,000
	6' Ø MH      15'-20'	1	EA	2,250	2,250
	20'-25'	1	EA	2,750	2,750
	30'-35'	2	EA	4,500	9,000
	SPECIAL MH   10'-15'	5	EA	2,500	12,500
	15'-20'	1	EA	3,500	3,500
	TRANSITION STRUCTURE	1	EA	15,000	15,000
	ENERGY DISSIPATION STRUCTURE	1	EA	15,000	15,000
	CONCRETE CHANNEL	2,820	LF	150	423,000

ITEM		QUANTITY TAKE-OFF SHEET			SHEET 14 OF 19	
Denver Engineering Corporation		PROJECT NAME			JOB NO.	
1626 Cole Boulevard		HEWLETT-PACKARD @ BRIARGATE			101	
Suite 300 Building 7		LOCATION			DATE	
Golden, Colorado 80401		COLORADO SPRINGS, COLORADO			12-13-83	
PROJECT DESCRIPTION					PREPARED BY	
STORM DRAINAGE					BDP	
					CHECKED BY	
ITEM NO.	DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST	
	TOTAL (CONT)					
	18" $\phi$ RCP	0'-10'	4,190	LF	21	87,990
		10'-15'	1,010	LF	30	30,300
		15'-20'	210	LF	43	9,030
	21" $\phi$ RCP	0'-10'	880	LF	26	22,880
		10'-15'	100	LF	34	3,400
	24" $\phi$ RCP	0'-10'	1,955	LF	31	60,605
		10'-15'	580	LF	40	23,200
		15'-20'	1,020	LF	52	53,040
		20'-25'	145	LF	65	9,425
	27" $\phi$ RCP	10'-15'	710	LF	37	26,270
	30" $\phi$ RCP	0'-10'	730	LF	46	33,580
		10'-15'	325	LF	57	18,525
	33" $\phi$ RCP	0'-10'	85	LF	52	4,420
		10'-15'	40	LF	62	2,480
		15'-20'	190	LF	76	14,440
		30'-35'	30	LF	146	4,380
	36" $\phi$ RCP	0'-10'	100	LF	60	6,000
		20'-25'	250	LF	104	26,000
	42" $\phi$ RCP	0'-10'	200	LF	72	14,400
		10'-15'	420	LF	82	34,440
		25'-30'	200	LF	141	28,200
		30'-35'	290	LF	171	49,590
	54" $\phi$ RCP	15'-20'	240	LF	129	30,960
		30'-35'	60	LF	210	12,600
	60" $\phi$ RCP	10'-15'	385	LF	135	51,975
		15'-20'	340	LF	151	51,340
	66" $\phi$ RCP	10'-15'	855	LF	175	149,625
	72" $\phi$ RCP	10'-15'	70	LF	187	13,090
	8' x 4' REBC	15'-20'	1,065	LF	270	287,550
		20'-25'	985	LF	295	290,575
	REBC MH RISER		87	LF	86	7,480





Denver Engineering Corporation  
 1626 Cole Boulevard  
 Suite 300 Building 7  
 Golden, Colorado 80401  
 (303) 232 6262

Sheet 16 of 19  
 Job No. 101

## DESIGN CALCULATIONS

Project HEWLETT-PACKARD @ BRIARGATE

Detail COST ESTIMATE

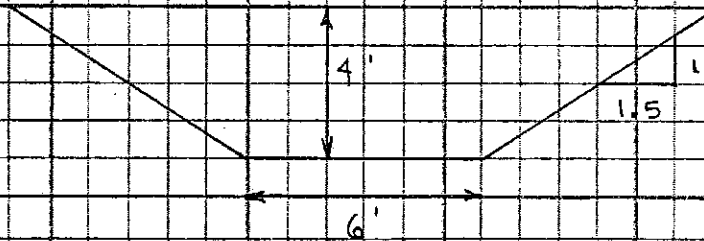
Designer BDP Date 12-13-83

Checker \_\_\_\_\_ Date \_\_\_\_\_

### CHANNEL QUANTITIES

MAX. CHANNEL DEPTH OF FLOW = 2.86 FT

FRSD = 1.0' OR 0.25 D<sub>w</sub> WHICHEVER GREATER  
 USE 1.0' FRSD



6" CONCRETE ON SLOPE PAVING @ \$170/CY  
 TO ALLOW FOR SPECIAL DESIGN ON SUPERIOR FLOW CHANNEL,  
 USE \$215 / CY

$$P = 6 + 2 \times 4 + [1.5(4)]^2 = 20.42 \text{ SF/LF}$$

$$\text{@ 9"}, V = 20.42 \frac{\text{SF}}{\text{LF}} \times \frac{9 \text{ IN}}{12 \text{ IN/FT}} = 15.32 \frac{\text{CF}}{\text{LF}}$$

$$\text{CONCRETE COST} = \frac{15.32 \text{ CF/LF}}{27 \text{ CF/CY}} \times \$215/\text{CY} = \$122/\text{LF}$$

USE 6" Ø PVC UNDERDRAIN @ \$6/LF

$$\text{FILTER MATERIAL} = \frac{1' \times 6' \times 1'}{27 \text{ CF/CY}} \times \frac{\$18}{\text{CY}} = \$4/\text{LF}$$

$$\text{ACCESS ROAD} = \frac{12' \times 0.5' \times 1'}{27} \times \frac{\$18}{\text{CY}} = \$4/\text{LF}$$

$$\text{SUBTOTAL} = \$122 + 6 + 4 + 4 = \$136/\text{LF}$$

$$+ \text{CONTINGENCY @ 10\%} = \$150/\text{LF}$$

(COST OF EXCAVATION INCLUDED IN GRADING)





Denver Engineering Corporation

1626 Cole Boulevard  
Suite 300 Building 7  
Golden, Colorado 80401

QUANTITY TAKE-OFF SHEET

SHEET 17 OF 19

PROJECT NAME  
HEWLETT-PACKARD @ BRIARGATE  
LOCATION  
COLORADO SPRINGS, COLORADO

JOB NO.  
101  
DATE  
12-13-83

PROJECT DESCRIPTION

\*REIMBURSABLE  
STORM DRAINAGE

PREPARED BY  
BDP  
CHECKED BY

ITEM NO.	DESCRIPTION	ESTIMATED QUANTITY	UNIT	UNIT COST	TOTAL COST
2	4' DIOR 0'-10'	1	EA	1,000	1,000
3	18" Ø RCP 0'-10'	250	LF	21	5,250
	5' Ø MH 0'-10'	1	EA	1,200	1,200
4	18" Ø RCP 0'-10'	210	LF	21	4,410
	4' Ø MH 0'-10'	1	EA	1,000	1,000
5	18" Ø RCP 0'-10'	280	LF	21	5,880
	4' Ø MH 0'-10'	1	EA	1,000	1,000
6	18" Ø RCP 0'-10'	180	LF	21	3,780
	5' Ø MH 0'-10'	1	EA	1,200	1,200
	18" Ø RCP 0'-10'	55	LF	21	1,155
	4' DIOR 0'-10'	1	EA	1,000	1,000
7	21" Ø RCP 0'-10'	160	LF	26	4,160
	5' Ø MH 0'-10'	1	EA	1,200	1,200
11	4' DIOR 0'-10'	1	EA	1,000	1,000
12	21" Ø RCP 0'-10'	50	LF	26	1,300
	24" Ø RCP 0'-10'	345	LF	31	10,695
	5' Ø MH 0'-10'	1	EA	1,200	1,200
	24" Ø RCP 0'-10'	395	LF	31	12,245
	5' Ø MH 0'-10'	1	EA	1,200	1,200
	24" Ø RCP 0'-10'	135	LF	31	4,185
23	CONC. CHNL.	90	LF	157	14,130
24	CONC. CHNL.	765	LF	157	120,105
25	CONC. CHNL.	270	LF	157	42,390
26	CONC. CHNL.	320	LF	157	50,240
27	CONC. CHNL.	125	LF	157	19,625
28	CONC. CHNL.	30	LF	157	4,710
29	CONC. CHNL.	495	LF	157	77,715
30	CONC. CHNL.	950	LF	157	149,150
31	CONC. CHNL.	700	LF	157	109,900
32	CONC. CHNL.	230	LF	157	36,110
33	CONC. CHNL.	555	LF	157	87,135
34	CONC. CHNL.	735	LF	157	115,395



**DEEG**

Denver Engineering Corporation  
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Sheet 19 of 19  
 Job No. 101

**DESIGN CALCULATIONS**Project HEWLETT-PACKARD @ BRIARGATEDetail REIMBURSABLE COST ESTIMATEDesigner BDP Date 12-13-83

Checker \_\_\_\_\_ Date \_\_\_\_\_

CHANNEL VOLUME FOR EARTHWORK

$$V = \left( \frac{18+6}{2} \right) 4 + 15.32 + 6 = 69.32 \text{ CF} = 2.57 \text{ CF/LF}$$

DOUBLE THIS FIGURE TO ACCOUNT FOR NECESSARY  
 EXCAVATION OTHER THAN CHANNEL CROSS SECTION: 5.13 CF/LF

USE \$1.25 / CY  $\therefore$  \$6.02 / CF SAY \$7 / CF

$$\therefore \text{CHANNEL COST} = \$150 + \$7 = \$157 / \text{LF}$$

**APPENDIX 6**  
**DRAINAGE PLAN**