

INNOVATIVE DESIGN. CLASSIC RESULTS.

FINAL DRAINAGE REPORT FOR FOOTHILLS FARM CAMPUS FILING NO. 2 AMENDMENT TO MASTER DEVELOMENT DRAINAGE PLAN FOR MARKETPLACE AT INTERQUEST AND FINAL DRAINAGE REPORT FOR MARKETPLACE AT INTERQUEST FILING NO. 1 AND FILING NO. 2

Prepared for: ALLISON VALLEY DEVELOPMENT COMPANY, LLC 1755 TELSTAR DRIVE, SUITE 211

1755 TELSTAR DRIVE, SUITE 211 COLORADO SPRINGS, CO 80920 (719) 867-2279

Job no. 2399.86



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Conditions:

This report and plan for the drainage design of Foothills Farm Campus Filing No. 2 was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the City of Colorado Springs Drainage Design and Technical Criteria and is in conformity with the master plan of the drainage basin. I understand that the City of Colorado Springs does not caused by any negligent acts, errors or omissions on my part in preparing this report.

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		that the drainage facilities for Foothills Far
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		<u>ling No. 2</u> , guarantee that final drainage desig <u>LC.</u> and/or their successors and/or assigns of
		proval of the final plat does not imply approv
of my engineer's drainage design.		provar of the iniai plat does not imply approv
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Allison Valley Development Co.	, LLC a Colorado Limited Liability	v Company
Name of Developer		
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Authorized Signature	Date	
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Steve Rossoll Printed Name		
Director of Developme	ent	
La Plata Communities, Inc. A Colo		
Title	Stado Corporadon, manager	
1755 Telstar Drive, Suite 211, Colo	orado Springs, CO 80920	
Address:		
City of Colorado Springs States	ment:	
Filed in accordance with Section	7.7.906 of the Code of the City of	of Colorado Springs, 2001, as amended.
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For City Engineer	Date	



GENERAL DESCRIPTION

Foothills Farm Campus Filing No. 2 is a 42.890-acre site located in Sections 17, 18, 19, and 20, Township 12 South, Range 66 West of the Sixth Principal Meridian in the City of Colorado Springs, County of El Paso, State of Colorado. The site is bound on the south by existing Marketplace at Interquest retail development and Federal Drive, to the west by existing USAFA vacant property and Interstate 25, and to the east Black Squirrel Creek. This site includes a platted lot, public street right of way, and tracts to support the proposed Ent Credit Union headquarters office campus development within the previously approved Marketplace at Interquest PUD plan (see Appendix).

The average soil condition reflects Hydrologic Group "B" (Stapleton Sandy Loam) and Hydrologic Group "A" (Blakeland Loamy Sand) as determined by the "Soil Survey of El Paso County Area," prepared by the Web Soil Survey (NRCS). (See map in Appendix).

This site is not impacted by the City Streamside overlay zone.

EXISTING DRAINAGE CONDITIONS

The site is located within the Black Squirrel Drainage Basin, which stretches from the Black Forest, across Hwy. 83 and into the Air Force Academy property. Currently, an existing box culvert conveys flows under Voyager Parkway. This Basin has been previously studied by the URS Corporation in the approved "Black Squirrel Creek Drainage Basin Planning Study" (1989). The historic flows from The Farm currently drain either directly into Black Squirrel Creek or in a westerly direction into Air Force Academy property. The flows are then directed north and south to the existing 1-25 bridge structure.

The overall Farm (including Foothills Farm Campus) property has been previously studied in numerous reports as referenced within the most recent "Allison Valley Master Development Drainage Plan Update," prepared by Kiowa Engineering Corporation, dated December 2011. This MDDP Update was provided to accompany a concurrent Master Plan update at that time.

The Kiowa MDDP update outlines the requirements for The Farm's proposed drainage patterns, outfall locations, and regional detention facility locations as they relate to the existing Black Squirrel Creek and Middle Tributary Basin corridor. Regional Detention and Stormwater Quality Facility outfall locations have been established schematically with the approved MDDP and the USFWS "Biological Assessment and Habitat Mitigation Plan for Allison Valley Project, Colorado Springs, Colorado", prepared by Walsh Environmental Scientists and Engineers, dated May 2007.

The Kiowa MDDP outlines the need to provide Full Spectrum detention pond sizing, which will meet USAFA release rate criteria, will provide for a 72-hour drain time for the public regional stormwater facilities, as well as incorporate Water Quality Capture Volume.

Historically, this site drains in a northerly direction with slopes ranging from 2% to 33%. The site is currently being overlot with the previously approved Drainage Memo for Foothills Farm Campus Filing No. 2 – Overlot Grading. This site has also been previously studied as part of the "Master Development Drainage Plan for Marketplace at Interquest and Final Drainage Report for Marketplace at Interquest Filing No. 1 and Filing No. 2," prepared by Classic Consulting Engineers & Surveyors, approved August 2007.

The subject site was studied as a commercial/retail land use within the previously approved Marketplace at Interquest MDDP, as attached in the Developed Conditions Drainage Map in the Appendix. Please reference this map as the existing conditions map for the subject site. The proposed site development matches the land use, grading configuration, and outfall locations assumed in the Marketplace MDDP, also matching "C" values for developed conditions.

Ultimately, flows from the Marketplace MDDP basins tributary to Black Squirrel Drainage Basin will be conveyed to the proposed BS-3 Full Spectrum Public Regional Facility (Pond G) or to Full Spectrum Public Regional Facility (Pond D). The proposed pond is shown on the approved MDDP developed conditions Drainage Map (see Appendix). In the interim, developed drainage flows tributary to the subject site are being treated in the existing temporary BS-3T pond is still in place as shown on the attached Marketplace interim MDDP Drainage Map.

The Marketplace MDDP Developed Conditions and Interim Conditions drainage map has been included in the Appendix for reference and serves as the "Existing Conditions" map for this site. This map has been marked to show the similar tributary areas for the subject site. While the tributary areas are similar, used commercial "C" land use values, runoff rates and followed very similar outfall routes, this Marketplace MDDP assumed Detention Pond locations in areas slightly different than the proposed condition.

The Marketplace MDDP assumed a BS-2 and a BS-3 Tributary area for each respective Detention Pond. The closely correspond to the proposed subject site in area, land use, and "C" values. See included text in the Appendix of this report for the listing of areas, flows, and basin description of each area tributary to Pond BS-2 and Pond BS-3. These ponds are now being design as Ponds G (in place of BS-3) and Pond D (in place of BS-2). The concept and outfall patterns are similar in intent; however the Ponds will meet current Full Spectrum Detention criteria.



Pond BS-2: Total acreage of 37.2 acres per the Marketplace MDDP is accumulated from Basins BS-2A, BS-2B, BS-2C, BS-2D, BS-2E for a total inflow developed of $Q_5 = 90.18$ cfs, $Q_{100} = 166.54$ cfs. See Map and text in appendix for acreages and flow rates assumed from each basin. As proposed, this tributary area will now be served by proposed Full Spectrum Detention Facility Pond D, total tributary area of 39.60 acres commercial land use with total inflow of $Q_5 = 110$ cfs, $Q_{100} = 203$ cfs.

Pond BS-3 Total acreage of 74.2 acres per the Marketplace MDDP is accumulated from Basins BS-3A, BS-3B, BS-3C, BS-3D, BS-3E, BS-3F, and BS-3G for a total inflow developed of $Q_5 = 197.70$ cfs, $Q_{100} = 366.68$ cfs. See Map and text in appendix for acreages and flow rates assumed from each basin. As proposed, this tributary area will now be served by proposed Full Spectrum Detention Facility Pond G, total tributary area of 69.64 acres commercial land use with total inflow of $Q_5 = 162$ cfs, $Q_{100} = 306$ cfs.

As shown in the enclosed Developed Conditions Drainage Maps, the tributary acre is nearly the same, and the assumed land uses are similar. The split of flows to the proposed Detention facilities has been updated to match the proposed land use and Development Plan. Final flow calculations for these basins follow, along with an updated description of the current detention requirements for the allowable release rates for the full spectrum detention facilities.

The presence of the Preble's Meadow Jumping Mouse and wetlands within the Black Squirrel Tributary adjacent to the subject site have required coordination with the Environmental Protection Agency, the U.S. Army Corps of Engineers, U.S. Fish and Wildlife and the Colorado Division of Wildlife. In addition, due to the proximity of the Air Force Academy, drainage requirements of the Air Force Academy were taken into account.

PROPOSED DRAINAGE CONDITIONS

Developed runoff from Foothills Farm Campus Filing No. 2 development will be conveyed generally to the north in accordance with the previously approved reports, and approved Marketplace at Interquest MDDP. Stormwater will be routed into public and private RCP storm outfall extensions. Proposed development matches the commercial/retail land use and associated "C" values and time of concentration rates previously assumed in the approved Marketplace at Interquest MDDP, therefore proposed drainage conditions described herein closely match developed flowrates and outfall points in conformance with the approved MDDP. Comparison of total developed stormwater rates closely match those anticipated within the approved MDDP. As a function of the PUD site plan layout and stormwater drainage outfall from the subject site to Black Squirrel Creek, the proposed Full Spectrum



Pond D (formerly labeled BS-2 on the MDDP map) has been relocated to the north adjacent to Black Squirrel Creek. For purposes of ensuring adequate tributary basin calculations for the proposed Full Spectrum Ponds G and D, all tributary basins are shown in the calculations and on the Developed Conditions Drainage Map. A detailed description of the developed flows is as follows:

Design Point 1 ($Q_5 = 78$ cfs, $Q_{100} = 143$ cfs) is composed of development area from Basin A and B. Basin A (15.98 acres) is the currently proposed Springs at Foothills Farm Filing No. 1 Apartments site. Basin B (7.42 acres) is unimproved and assumed commercial/retail use per the MDDP. Total flows are routed to the intersection of existing Federal Drive and Summit View Parkway. Stormwater is routed ultimately to the proposed Regional Full Spectrum Facility Pond D.

Design Point 2 ($Q_5 = 23$ cfs, $Q_{100} = 43$ cfs) is composed of asphalt parking and landscaping within Basin C. Basin C (7.73 acres) is the tributary area of Federal Drive at Summit View Parkway. Existing Public storm facilities will combine with stormwater from Design Point 1. A proposed 60" public RCP storm pipe (Pipe Run I) will convey stormwater to proposed Public Full Spectrum Detention (FSD) Pond D.

Design Point 3 (Q₅ = 18 cfs, Q₁₀₀= 34 cfs) is composed of Basins D and E. Basin D (3.18 acres) is the currently proposed Foothills Farm Campus Filing No. 1 office site. Basin E (1.18 acres) is unimproved and assumed commercial/retail use per the MDDP. Total flows are routed in Pipe 2 (30" private storm) to the intersection at Summit View Parkway. Pipe Run 3, a proposed 60" public storm conveys stormwater to the proposed Public Regional FSD Pond D.

<u>Design Point 4</u> ($Q_5 = 8 \text{ cfs}$, $Q_{100} = 15 \text{ cfs}$) is an area of future commercial development from Basin Q. Basin Q (1.99 acres) is unimproved and assumed commercial/retail use per the MIDDP. Total flows are routed in Pipe 4, a proposed 60" public storm that conveys flow to the proposed Public Regional FSD Pond D.

Design Point 5 ($Q_5 = 10 \text{ cfs}$, $Q_{100} = 17 \text{ cfs}$) is an area of future commercial development from Basin K and L. Basin K (1.16 acres) and Basin L (1.12 acres) are unimproved and assumed commercial/retail use per the MDDP. Total flows are routed in Pipe 9, a proposed 24" private storm that conveys flow to the proposed Public Regional FSD Pond G.



Pipe 9 combines with downstream tributary flows from Bains F, G, H, I and J. These basins are shown on the attached Developed Drainage Map and are part of the approved Marketplace at Interquest commercial /retail area as accounted for in the approved MDDP. The stormwater was assumed in the MDDP as commercial/retail land use, and had adequately assumed "C" values and runoff rates appropriate for the currently developed land use. These basins have been shown for reference to substantiate the sizing and tributary area calculations of the proposed Public Full Spectrum Detention Pond G (listed in the MDDP as Pond BS-3). Total flow from these areas are reflected at Pipe Run 8, $Q_5 = 92$ cfs, $Q_{100} = 168$ cfs at the exit at Existing Great Wolf Lodge. A proposed public 54" storm pipe has been extended at this location and will combine with Pipe 9. Pipe 10, a proposed 60" public storm pipe, conveys stormwater to the north, directing drainage to the proposed Public Regional FSD Pond G.

<u>Design Point 6</u> ($Q_5 = 12 \text{ cfs}$, $Q_{100} = 22 \text{ cfs}$) is an area of future commercial development from Basin M. Basin M (3.07 acres) is unimproved and assumed commercial/retail use per the MDDP. Total flows are routed in Pipe 11, a proposed 30" private storm stub that combines with downstream public storm main. Flows are routed in Pipe 12, a proposed public 60" storm pipe, ultimately directing drainage to the proposed Public Regional FSD Pond G.

Design Point 7 ($Q_5 = 12 \text{ cfs}$, $Q_{100} = 21 \text{ cfs}$) consists of developed drainage from Basins N, P3, P4 and half of Basin O. Basin N (1.23 acres) is the proposed private Ent Parkway drive aisle, Basin P3 (0.72 acres) and P4 (0.32 acres) are parking and landscaping areas supporting the Ent office use. Basin O (1.91 acres total) is the public Summit View Parkway right of way. Total flows are routed to Design Point 7, a proposed 8' private D10R inlet. Intercepted flows are conveyed in Pipe 16, a proposed 30" private storm pipe. Flows are ultimately routed to the proposed Public Regional FSD Pond G.

Design Point 8 ($Q_5 = 5$ cfs, $Q_{100} = 9$ cfs) consists of developed drainage from Basins P5 and half of Basin O. Basin P5 (0.39 acres) is the proposed parking and landscaping areas supporting the Ent office use. Basin O (1.91 acres total) is the public Summit View Parkway right of way. Total flows are routed to Design Point 8, a proposed 6' private D10R inlet. Intercepted flows are conveyed in Pipe 17, a proposed 30" private storm pipe. Flows are ultimately routed to the proposed Public Regional FSD Pond G.

Design Point 9 ($Q_5 = 4$ cfs, $Q_{100} = 7$ cfs) consists of developed drainage from Basin P1. Basin P1(0.88 acres) is the proposed parking and landscaping areas supporting the Ent office use. Flows are routed to Design Point 9, a proposed 4' private D10R inlet. Intercepted flows are conveyed in Pipe 13, a proposed 24" private storm pipe. Flows are ultimately routed to the proposed Public Regional FSD Pond G.



Design Point 10 ($Q_5 = 3$ cfs, $Q_{100} = 5$ cfs) consists of developed drainage from Basin P2. Basin P2 (0.66 acres) is the proposed parking and landscaping areas supporting the Ent office use. Flows are routed to Design Point 10, a proposed 4' private D10R inlet. Intercepted flows are conveyed in Pipe 14, a proposed 18" private storm pipe. Flows are ultimately routed to the proposed Public Regional FSD Pond G.

Design Point 11 (Q₅ = 4 cfs, Q₁₀₀= 8 cfs) consists of developed drainage from Basin P6. Basin P6 (1.03 acres) is the proposed parking and landscaping areas supporting the Ent office use. Flows are routed to Design Point 11, a proposed 4' private D10R inlet. Intercepted flows are conveyed in Pipe 18, a proposed 18" private storm pipe. Pipe 18 along with downstream Pipes 13, 14, 15, 16, and 17 and Basin R (1.31 acres of parking garage Roof Drain) combine in Pipe 19, a proposed 36" private storm pipe. Pipe 19 combines with Pipe 12, in a proposed 66" public storm outfall (Pipe 20) and are ultimately routed to the proposed Public Regional FSD Pond G.

Design Point 12 $Q_5 = 3$ cfs, $Q_{100} = 5$ cfs) consists of developed drainage from Basin S1. Basin S1 (0.72 acres) is the proposed landscaping areas supporting the Ent office use, as well as a portion of Ent Parkway private drive. Flows are routed to Design Point 12, a proposed 4' private D10R inlet. Intercepted flows are conveyed in Pipe 21, a proposed 18" public storm pipe. Pipe 21 is ultimately routed to the proposed Public Regional FSD Pond G.

Design Point 13 $Q_5 = 2$ cfs, $Q_{100} = 3$ cfs) consists of developed drainage from Basin S2. Basin S2 (0.47 acres) is the proposed landscaping areas adjunct to and including a portion of Ent Parkway private drive. Flows are routed to Design Point 13, a proposed 4' private D10R inlet. Intercepted flows are conveyed in Pipe 22, a proposed 18" public storm pipe. Pipe 22 combines with Pipe 20, in the proposed 66" public storm outfall (Pipe 23), and is ultimately routed to the proposed Public Regional FSD Pond G.

Design Point 14 $Q_5 = 2$ cfs, $Q_{100} = 8$ cfs) consists of developed drainage from Basin U1. Basin U1 (3.11 acres) is the proposed landscaping areas supporting the Ent office use. It is assumed the building roof drainage will be included in the pipe outfall (see Pipe Run 24) and half the flows included in Design Point 14 are from surface landscaping. Flows are routed to Design Point 14 along the proposed grass paver fire access roadway that is parallel to the west boundary. This access includes a 6" curb along the west edge to ensure routing of stormwater to a collection location (design Point 14). A proposed 4' private D10R inlet will intercept stormwater at Design Point 14. Intercepted flows are conveyed in Pipe 25, a proposed 24" private storm pipe. Pipe 25 is ultimately routed to the proposed Public Regional FSD Pond G.



Design Point 15 $Q_5 = 3$ cfs, $Q_{100} = 7$ cfs) consists of developed drainage from Basin U2. Basin U2 (1.21 acres) is the proposed landscaping areas supporting the Ent office use. Flows are routed to Design Point 15 along the proposed grass paver and asphalt paved fire access roadway. This access includes a 6' curb along the west edge to ensure routing of stormwater to a collection location (design Point 15). A proposed 4' private D10R inlet will intercept stormwater at Design Point 15. It is assumed the building roof drainage from Basin V will be included in the pipe outfall (see Pipe Run 26). Intercepted flows are combined with downstream Pipe 25 in a proposed 30" private storm pipe (Pipe 27). Pipe 27 is ultimately routed to the proposed Public Regional FSD Pond G.

Design Point 16 ($Q_5 = 34$ cfs, $Q_{100} = 62$ cfs) is an area of future commercial development from Basins W (7.04 acres), X (0.91 acres), and Y (1.16 acres). These basins are unimproved and assumed commercial/retail use for the expansion of the Ent office campus building, parking, and landscaping as shown on the Drainage Map. Drainage from this area will be defined in future reports for final routing and facilities. Flows are routed along with downstream Pipe 28 to Pipe 29, a proposed private 36" storm pipe, ultimately directing drainage to the proposed Public Regional FSD Pond G.

Design Point 17 ($Q_5 = 8$ cfs, $Q_{100} = 16$ cfs) is an area of future commercial development from Basin Z, 2.01 acres. This basin is unimproved and assumed commercial/retail use for the expansion of the Ent office campus building, parking, and landscaping as shown on the Drainage Map. Drainage from this area will be defined in future reports for final routing and detention and water quality treatment facilities.

Overflow routing for the private storm system is designed with a maximum ponding depth before overtopping the adjacent high point to the next available downstream inlet. Overflow routing for area inlets adjacent to improvements (including Building foundations or structures) is provided within Detailed Grading Plans to ensure that a limited ponding depth is allowed prior to overtopping to the next inlet and therefor preventing stormwater from impacting proposed improvements. Ponding at these inlets will be provided at a maximum elevation with an additional depth of safety so ensure that the stormwater will be routed to an available inlet prior to stormwater entering the building.

REGIONAL DETENTION AND STORMWATER QUALITY

The City of Colorado Springs Drainage Criteria Manual specifies that this site is required to provide full spectrum detention. The proposed public Pond G and Pond D Full Spectrum Detention facilities will be designed and fully



constructed with pre-sedimentation forebays, low flow trickle channels, a micropool, and an orifice plate to provide for WQCV, EURV and full spectrum detention requirements.

<u>Full Spectrum Detention Requirement:</u> The UD-Detention spreadsheet has been provided in the Appendix of this report to provide sizing based upon UDFCD requirements for EURV, with a minimum drain time of 72 hours.

Detention Summary:

Proposed Detention Facility D is a 5.5 ac-ft Public Full Spectrum Detention facility. A 42" public storm pipe will outlet the stormwater from the pond and will convey flows to the designated outfall location at Black Squirrel Creek. Total inflow to this facility is Q₅ =110 cfs, Q₁₀₀= 203 cfs. The total acreage tributary to Pond D is combined from Basins A, B, C, D, E, Q, and AA. Total acreage is 39.60 acres with 85% imperviousness, as calculated by the attached IRF form in the Appendix of the report. This pond will store and treat developed stormwater from Foothills Farm and the surrounding tributary properties described in this report. Appropriate energy dissipation measures will be included in the construction drawings at the outlet pipe connection to existing Black Squirrel Creek to provide for permanent erosion protection. The proposed outlet structure is a 6'x4' inlet riser with the UDFCD required 3- hole orifice plate. Reference worksheets in Appendix for details. Overflow weir routing for this facility is shown on the Drainage Map and sized in the attached UD-Detention worksheet. A 165 lf overflow weir with a concrete wall will be installed to route the stormwater flows in an emergency event. Overflow routing is directed to existing Black Squirrel Creek. This facility and outlet structure will be constructed with Foothills Farm Campus Filing No. 2 drainage improvements. Final pond design, outlet structure sizing, trickle channel and forebay details will be included with final construction drawings for review and approval by City Engineering prior to construction approval.

Proposed Detention Facility G is an 8.80 ac-ft Public Full Spectrum Detention facility. A 48" public storm pipe will outlet the stormwater from the pond and will convey flows to the designated outfall location at Black Squirrel Creek. Total inflow to this facility is $Q_5 = 162$ cfs, $Q_{100} = 306$ cfs. The total acreage tributary to Pond G is combined from Basins K, L, M, N, O, P3, P4, P5, P1, P2, P6, S1, S2, U1, U2, W, X, Y, R and BB. Offsite basins from Marketplace at Interquest total and additional 38.34 tributary acres. Total acreage is 69.64 acres with 72° imperviousness, as calculated by the attached IRF form in the Appendix of the report. This pond will store and treat developed stormwater from Foothills Farm and the surrounding tributary properties described in this report. Appropriate energy dissipation measures will be included in the construction drawings at the outlet pipe connection to existing Black Squirrel Creek to provide for permanent erosion protection. The proposed outlet structure is an 8'x4' inlet riser with the UDFCD required 3-hole orifice plate. Reference worksheets in Appendix for details. Overflow weir routing for this facility is shown on the Drainage Map and sized in the attached UD-Detention worksheet. A 200 lf overflow weir with a concrete wall will be



installed to route the stormwater flows in an emergency event. Overflow routing is directed to existing Black Squirrel Creek. This facility and outlet structure will be constructed with Foothills Farm Campus Filing No. 2 drainage improvements. Final pond design, outlet structure sizing, trickle channel and forebay details will be included with final construction drawings for review and approval by City Engineering prior to construction approval.

Detention Maintenance, Ownership and Access: The proposed FSD Pond G and Pond D will be owned and maintained by the City of Colorado Springs as pubic facilities. These facilities are located within Tract B per the Foothills Farm Campus Filing No. 2 plat. Access to the pond will be provided per the current City Engineer Criteria and UDFCD criteria as shown on the Drainage Map. A City of Colorado Springs Inspection and Maintenance (IM) plan will be required indicating these Facilities to be ultimately owned and maintained by the City of Colorado Springs.

EURV and Stormwater Quality Capture Volume: The standard UD- Detention spreadsheet has been provided in the Appendix of this report to provide sizing based upon UDFCD requirements for EURV, with a minimum drain time of 72 hours. This spreadsheet includes minimum sizing for the required areas of micropool, forebays and the outlet structure orifice sizing.

WATER QUALITY SUMMARY

The City of Colorado Springs has required the Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainage ways, and implementing long-term source controls. The Four Step Process pertains to management of smaller, frequently occurring storm events, as opposed to larger storms for which drainage and flood control infrastructure are sized. Implementation of these four steps helps to achieve stormwater permit requirements. This site adheres to this Four Step Process as follows:

- 1. This site is an approved PUD zoned commercial/retail site. In general, most roof drains are intended to drains across landscaping where feasible, and parking areas contain landscaping to minimize directly connected impervious areas. These areas are identified in the IRF spreadsheet in the Appendix of this report.
- 2. Permanent BMPs for the overall master planned site have been implemented in initial development of the property in the form of Full Spectrum Detention and Stormwater Quality ponds located within the site in accordance with the approved MDDP.



- 3. Stormwater drainage from the subject property is being routed through stormwater detention /stormwater quality treatment facilities prior to being released to the historic drainage path as described in the previously approved reports. Developed flows will be required to adhere to release rates established within the previously approved reports and all stormwater discharge to downstream facilities will be required to employ energy dissipation measures to ensure no adverse effect to downstream facilities. As discussed in the report, the developed drainage is being routed to the north to proposed public Full Spectrum Detention Ponds G and D. Upon release stormwater enters Black Squirrel Creek. Per the "Allison Valley Master Development Drainage Plan Update", prepared by Kiowa Engineering Corporation, Dated December 2011, channel improvements along Black Squirrel Creek have been identified. These improvements are scheduled for phased construction and their timing and installation have been identified with development adjacent to the Black Squirrel Creek, as approved by the City of Colorado Springs. See Appendix for timing anticipated for all improvements required, along with a map showing the obligation for improvements tied to land development areas. For the subject site, the channel embankment work downstream of Pond #5 is required to take place with Foothills Farm Campus Filing No. 2 work (or assurances posted prior to CO.)
- 4. A site-specific stormwater quality and erosion control plan and narrative has been submitted and approved by City Engineering prior to any disturbance within the project area. Details such as site specific source control construction BMP's as well as permanent BMP's will be detailed in the Grading and Erosion Control plan and in the Stormwater Management Narrative to protect receiving waters. Upon construction of the proposed development, temporary BMP's will be installed and maintained as required. After final stabilization and site improvement completion, any disturbance to the site will need to be evaluated at that time for temporary and permeant BMP provisions.

EROSION CONTROL PLAN

The City of Colorado Springs Drainage Criteria Manual specifies an Erosion Control Plan and associated cost estimate be submitted with the Final Drainage Report. A Grading and Erosion Control Plan for this site has been approved and assurances have been posted.

DRAINAGE CRITERIA

Hydrologic calculations were performed using the City of Colorado Springs Drainage Criteria Manual, as revised in 2014. The Rational Method was used to estimate stormwater runoff anticipated from design storms for the 2 year, 5 year, 10 year, 25 year, 50 year and 100 year recurrence intervals.



factor of 2.63) to a new total of \$870,936.20 for storm pipe and \$236,700.00 for detention pond. See Cost Index (next page).

Per the Allison Ranch Addition Annexation Agreement recorded 4/5/2006 (Reception No.206049309) Section A. Platting "Owner's will not be required to pay drainage, pond or bridge fees for land to be dedicated for park, open space or trail purposes......"

A summary of the area exempt from fees are:

Tract B pond area (not included) 13.107 Ac. 6.544 ac

Total 6.563 ac. excluded from fees – net fee acreage 36.327 Ac.

FEE CALCULTIONS:

\$14,302/acre x 36.327 acres (Drainage 2019)	\$519,548.75
\$1,603/acre x 36.327 acres (Bridge 2019)	\$ 58,232.18
\$789/acre x 36.327 acres (Pond Land 2019)	\$ 28,662.00
	\$606,422.94

CREDITS:

A. Pond land credits will be used for Detention Facility D and G located within Tract B using the current \$76,602/acre.

Tract B <u>Pond area only</u> = 6.544 acres @ 76,602.00 acres = \$501,283.49 credit

Note: This amount is in addition to the existing Pond Land Credits remaining (Previously utilized by The Farm Filing No. 1A, 1B, 1C, 2, 3, 4, 4A, and 5).

B. A current credit remaining after the most recent Farm Filing No. 4A plat leaves \$292,710.53 available to offset drainage fees for Black Squirrel Creek.

Total offsets available at the time of Foothills Farm Campus (FFC) Filing No. 2 plat are:

\$292,710.53 Credits available after Farm 4Aplat

Total fees available for offset after FFC Fil. No. 2: -\$606,422.94 Drainage fees calculated FFC Fil. 2

\$313,732.41 fees remaining to be offset with \$1,107636.20 reimbursable facilities.



FINAL FEE CALCULTIONS:

Black Squirrel Fees Foothills Farm Campus Fi	ling No. 2 - due at platting	\$ 58,232.18
\$789/acre x 36.327 acres (Pond Land 2019)	POND LAND CREDIT	\$ 28,662.00
\$1,603/acre x 36.327 acres (Bridge 2019)		\$ 58,232.18
\$14,302/acre x 36.327 acres (Drainage 2019)	FEES OFFSET	\$519,549.75

NON-REIMBURSABLE CONSTRUCTION COST OPINION

PRIVATE DRAINAGE FACILITIES

ITEM	QUANTITY	UNIT	UNIT COST	TOTAL
18" RCP	322	LF	\$ 45.00	\$ 14,490.00
24" RCP	1307	LF	\$ 55.00	\$ 71,885.00
30" RCP	569	LF	\$ 60.00	\$ 34,140.00
36" RCP	1242	LF	\$ 75.00	\$ 93,150.00
STORM INLET D-10-R (4')	6	EA	\$ 4,500.00	\$ 27,000.00
STORM INLET D-10-R (6')	2	EA	\$ 6,500.00	\$ 13,000.00
STORM INLET D-10-R (8')	1	EA	\$ 8,500.00	\$ 8,500.00
STORM MANHOLE	12	EA	\$ 6,200.00	\$ 74,400.00
SUBTOTAL				\$ 336,565.00
15% ENGINEERING & CONTINGENCY				\$ 50,484.75
TOTAL				\$ 387,049.75

PUBLIC DRAINAGE FACILITES

ITEM	QUANTITY	UNIT	UN	IT COST	TOTAL
54" RCP	281	LF	\$	80.00	\$ 22,480.00
60" RCP	1723	LF	\$	110.00	\$ 189,530.00
66" RCP	980	LF	\$	130.00	\$ 127,400.00
STORM MANHOLE	11	EA	\$	7,000.00	\$ 77,000.00
SUBTOTAL					\$ 416,410.00
15% ENGINEERING & CONTINGENCY					\$ 62,461.50
TOTAL			•		\$ 478,871.50



Hydraulic grade line calculations have been provided for the Public storm outfall mains tributary to Public Pond G and Public Pond D along with their stubs. On-site private storm system HGL calculations supporting the Ent Development in particular will be supplied for review and approval along with the submittal of the private storm design drawings.

FLOODPLAIN STATEMENT

No portion of this site is located within a floodplain as determined by the Flood Insurance Rate Maps (F.I.R.M.) Map Number 08041C 0506G effective date, December 7, 2018 (See Appendix).

DRAINAGE AND BRIDGE FEES

This site has lies within the Black Squirrel Drainage Basin boundaries. The total platted area of Foothills Farm Campus Filing No. 2 is 42.890 acres.

Per the Black Squirrel Creek Drainage Basin Planning Study initial system (urban and rural) conveyance facilities are reimbursable (down to 15" RCP pipe), collection facilities (including inlets) are not. Reference DBPS Table 10, See Appendix.

Public Drainage Facilities (Reimbursable) <u>FOOTHILLS FARM CAMPUS FILING NO. 2</u>- Black Squirrel Creek Basin per DBPS

1.	36" Storm RCP	2,000 LF	\$87/LF	\$174,000.00
2.	48" Storm RCP	1500 LF	\$116/LF	\$174,000.00

TOTAL \$ 348,000.00

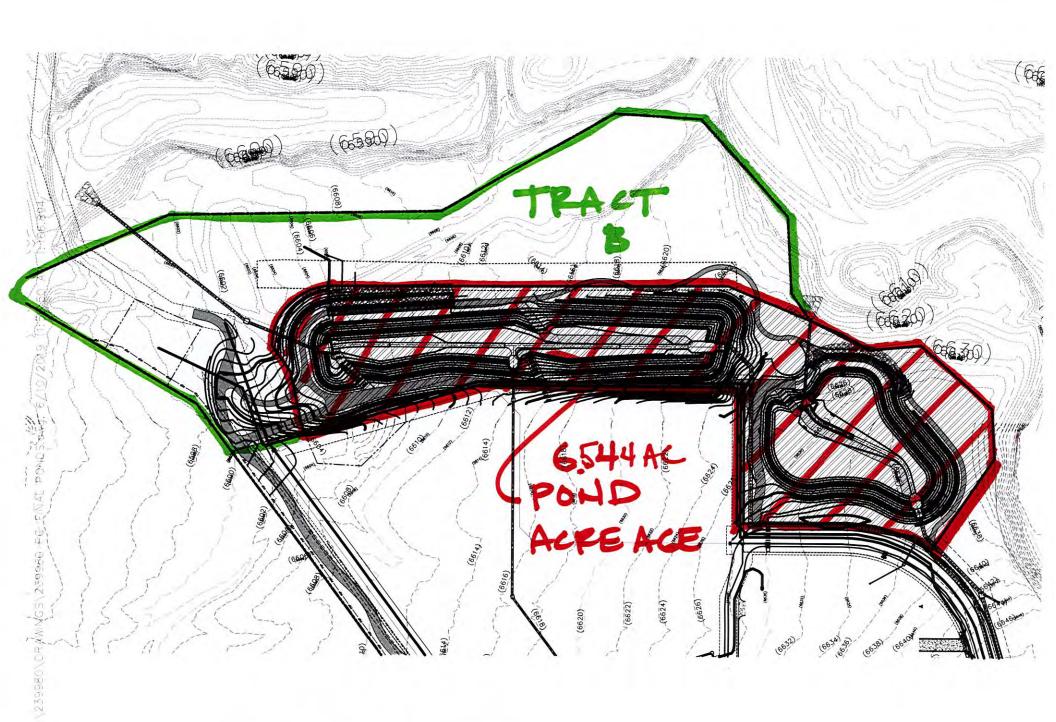
Squirrel Creek Basin per DBPS (Pond #9)

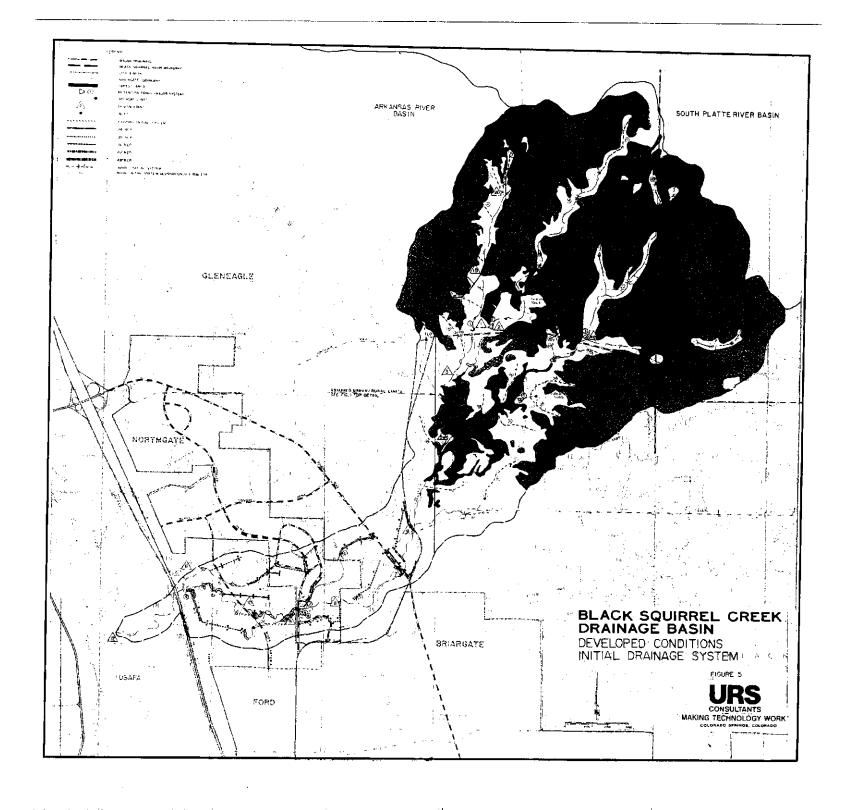
3. Detention Pond 1 EA \$90,000/EA \$90,000.00

TOTAL \$ 90,000.00

Cost of these facilities has been escalated from the original DBPS estimate 1982 to current year based upon the Drainage Basin rate increases. As such, the estimate has been updated at escalated cost (using a









DBPS · BLACK SQUIPPEL
PEIMBURSABLE FACILITIES

TABLE 11

BLACK SQUIRREL CREEK DRAINAGE BASIN ESTIMATED UNIT CONSTRUCTION COSTS

ITEM	UNIT	UNIT COST
RIP-RAP	CY	\$25.00
RIP-RAP (GROUTED EMBANKMENT)	SY	30.00
DAM EMBANKMENT EXCAVATION & EMBANKMENT	CY CY	3.00
GRANULAR BEDDING FOR RIP-RAP	CA	1.50 12.00
BEND PROTECTION	EA	10,000.00
REVEGETATION (Non-reimbursable	AC	2,500.00
when placed over riprap only) DROP STRUCTURES -		,
MAJOR URBAN	EA	60,000.00
MAJOR RURAL	EA	10,000.00
INITIAL RURAL (Q >150 cfs)	EA	3,000.00
INITIAL RURAL (Q <150 cfs)	EA	1,500.00
REINFORCED CONCRETE BOXES -		
CONCRETE	CY	180,00
STEEL	LB	0.50
TRANSITIONS & HEADWALL	EA	12,000.00
REINFORCED CONCRETE PIPE -		
(Including all appurtenances)		
15" Dia	$\mathbf{L}\mathbf{F}$	40.00
18" Dia 24" Dia	LF	48.00
30" Dia	LF LF	61.00
36" Dia	LF	76.00 87.00¥-
42" Dia	LF	104.00
48 " Dia	ĹF	116.00 \
54" Dia	LF	124.00
60" Dia	LF	131.00

BLACE SQUIRREL CREEK DRAIBAGE BASIN ESTIMATED CONCEPTUAL DESIGN IMPROVEMENT COSTS & FEES

ESTIMATED 1988 CONSTRUCTION COSTS DESIGN REACH DESIGN IMPROVEMENT COMMENT QTT. DEIT BHIT DEATHAGE : POINT FLOW COESTRUCTION (\$) LAND COST COST (\$) COST (\$) (cfs) (\$) RUPAL -----. 1-19,21 See Fig. 10 DROPS \$1,260,000 140 BA \$9.000 1-19,21 See Fig. 8 BEED PROTECTION 40 IA 10.000 400,000 S.B. 83 14 563 8. 1 8. CBC 290 120 LF 34,800 18 848 10'x 10' CBC S.I. 83 120 LF 410 49,200 See Thl. 7 DETENTION POND \$1 34 ac-ft 1 LS 256.800 256,800 \$60.840 10'x 10' CBC 906 BORTEGATE ROAD 120 LF 410 49,200 364 7'x 7' CBC S.I. 83 120 LF 240 28.800 See Thl. T DETENTION POND 82 34 ac-ft 1 LS 259,200 259,200 63,960 740 10'x 9' CBC MORTEGATE ROAD 120 LF 390 46,800 MORTEGATE ROAD 120 LF 141 6'x 4' CBC 165 19,800 281 6'x 7' CBC S.I. 43 120 LF 200 24.000 12 497 8'x 8' CBC HILAH ROAD 120 LF 290 34,800 DETENTION POND \$3 13 See Tbl. 7 44 ac-ft 1 LS 396,000 396,000 82,680 574 14 8. x 8. CBC HILAH ROAD 120 LF 290 34,800 7'x 7' CBC 382 15 MILAN ROAD 120 LY 28.890 1641 (10'-10') x 10' CBC BORTEGATE ROAD 150 LF 795 \$119,250 DETERTION PORD #4 18 See Tbl. 7 14 ac-ft 1 LS 125.000 126,000 42,120 20 3536 25'x 8' FLC 4500 LF 855,000 190 1150 (11'-14'-11') x 10' CBC FOTORE ARTERIAL 120 LF 15 (See Fig. 5) 1,280 3536 (11'-14'-11') x 10' CBC S.H. 83 210 LF 1.280 268.800 MAJOR SYSTEM SUBTOTAL \$3,904,000 \$249.600 \$541.650 INITIAL SYSTEM SUBTOTAL 1,163,440 (SEE TABLE 10) RURAL TOTAL \$5,067,440 \$249,600 \$541,650 PRBAN 3577 22 25's 8' FLC 2250 LF 170 382,500 (11'x 14'x 11') x 10' CBC POWERS BLVD. 3577 210 LF 1,220 256.200 23 3597 25'1 8' FLC 2250 LF 382,500 -170 See Tol. 7 DETENTION POND 85 1 LS 63,000 7 ac-ft 63,000 17.160 24 150'-250' 1 4'-5' PLC • 3779 2900 90 261.000 6 EA DROPS 40.000 240,000 DETERTION PORD SE See Thl. 7 12 ac-ft 1 LS 108,000 108,000 26,520 25 358 8'x 3' FLC 3000 LF 75 225,000 DETERTION PORD \$7 See Thl. 7 I ac-ft 1 LS 1 LS 72,000 72,000 24,960 See 761. 7 DETENTION PORD SE 1 ac-ft 81.000 \$1,000 18,720 9 3779 (14'x 14') x 10' CBC TOTAGER PENT 220 LF 1,345 295.900 26 3803 30. T 1. ATC 3200 LF 170 544,000 (11' : 14' : 11') : 10' CBC MINOR APTERIAL 120 LF 10 3803 1,390 166,800 27 1800 LF 3953 30' 1 7' FLC 170 145 10's 5' FLC 1000 LF 28 85 85.000 10.1 8. CBC 28 745 BIBOR ARTERIAL 120 LF 390 46.800 See Thi. 7 DETERTION PORD 89 10 ac-ft 1 LS 90.000 90,400 24,960 MAJOR SYSTEM SUBTOTAL \$2,886,800 \$112,320 \$718,900 INITIAL SYSTEM SUBTOTAL 2.713.000 (SEE TABLE 10) URBAN TOTAL \$5,599,800 \$112,320 \$718,900 URBAN & RURAL SUBTOTALS \$10.667.240 2361.220 21.260.550 COESTRUCTION CONTINGENCY 51 533,362 63.028 REGIETERIEG 101 1,120,060 132,358 MASTER PLAN COST 115,000 BORAL TOTAL ASSESSED ACREAGE: 4970/5 = 494 CRAID TOTALS \$12,435,662 \$361,920 \$1,455,935 URBAN TOTAL ASSESSED ACREAGE = 1256 FEE/ACRE \$5.527 \$161 TOTAL ASSESSED

DETERTION LAND AREA COST/ACRE:
(* SEE TABLE 7 FOR DETERTION POWD ACREAGES)
COUNTY \$15,600
CITY \$15,600

ACREAGE =

2250

COLORADO SPRINGS ANNUAL CONSTRUCTION INDEX

(Per City Code Section 7.7.108)

2019 6.7% 2017 3.5% 2016 4.8% 2015 0% 2014 4.3% 2013 0% 2012 0% 2011 0% 2010 0% 2009 5% 2008 1% 2007 10% 2006 4% 2005 5% 2004 3% 2003 3% 2001 5% 2000 3% 1999 4% 1998 6%		
2017 3.5% 2016 4.8% 2015 0% 2014 4.3% 2013 0% 2012 0% 2011 0% 2010 0% 2009 5% 2008 1% 2007 10% 2006 4% 2005 5% 2004 3% 2003 3% 2001 5% 2000 3% 1999 4%	2019	6.7%
2016 4.8% 2015 0% 2014 4.3% 2013 0% 2012 0% 2011 0% 2010 0% 2010 0% 2009 5% 2008 1% 2007 10% 2006 4% 2005 5% 2004 3% 2003 3% 2001 5% 2000 3% 1999 4%	2018	5.7%
2015 0% 2014 4.3% 2013 0% 2012 0% 2011 0% 2010 0% 2010 0% 2009 5% 2008 1% 2007 10% 2006 4% 2005 5% 2004 3% 2002 3% 2001 5% 2000 3% 1999 4%	2017	3.5%
2014 4.3% 2013 0% 2012 0% 2011 0% 2010 0% 2009 5% 2008 1% 2007 10% 2006 4% 2005 5% 2004 3% 2002 3% 2001 5% 2000 3% 1999 4%	2016	4.8%
2013 0% 2012 0% 2011 0% 2010 0% 2009 5% 2008 1% 2007 10% 2006 4% 2005 5% 2004 3% 2003 3% 2001 5% 2000 3% 1999 4%	2015	0%
2012 0% 2011 0% 2010 0% 2009 5% 2008 1% 2007 10% 2006 4% 2005 5% 2004 3% 2003 3% 2001 5% 2000 3% 1999 4%	2014	4.3%
2011 0% 2010 0% 2009 5% 2008 1% 2007 10% 2006 4% 2005 5% 2004 3% 2002 3% 2001 5% 2000 3% 1999 4%	2013	0%
2010 0% 2009 5% 2008 1% 2007 10% 2006 4% 2005 5% 2004 3% 2003 3% 2002 3% 2001 5% 2000 3% 1999 4%	2012	0%
2009 5% 2008 1% 2007 10% 2006 4% 2005 5% 2004 3% 2003 3% 2002 3% 2001 5% 2000 3% 1999 4%	2011	0%
2008 1% 2007 10% 2006 4% 2005 5% 2004 3% 2003 3% 2002 3% 2001 5% 2000 3% 1999 4%	2010	0%
2007 10% 2006 4% 2005 5% 2004 3% 2003 3% 2002 3% 2001 5% 2000 3% 1999 4%	2009	5%
2006 4% 2005 5% 2004 3% 2003 3% 2002 3% 2001 5% 2000 3% 1999 4%	2008	1%
2005 5% 2004 3% 2003 3% 2002 3% 2001 5% 2000 3% 1999 4%	2007	10%
2004 3% 2003 3% 2002 3% 2001 5% 2000 3% 1999 4%	2006	4%
2003 3% 2002 3% 2001 5% 2000 3% 1999 4%	2005	5%
2002 3% 2001 5% 2000 3% 1999 4%	2004	3%
2001 5% 2000 3% 1999 4%	2003	3%
2000 3% 1999 4%	2002	3%
1999 4%	2001	5%
	2000	3%
1998 6%	1999	4%
	1998	6%
1997 4%	1997	4%

For further information, contact Engineering Development Review at 385-5056

PUBLIC DRAINAGE FACILITIES POND D

ITEM	QUANTITY	UNIT	UN	IIT COST	TOTAL	-
42" RCP	150	LF	\$	170.00	\$	25,500.00
OUTLET BOX W/ MICROPOOL	1	EA	\$	30,000.00	\$	30,000.00
60" IMPACT STRUCTURE	1	EA	\$	105,000.00	\$	105,000.00
TRICKLE CHANNEL (REINFORCED)	256	LF	\$	80.00	\$	20,480.00
RIP RAP SPIILLWAY	214	CY	\$	40.00	\$	8,560.00
OVERFLOW WALL -SPILLWAY	184	LF	\$	170.00	\$	31,280.00
SUBTOTAL					\$	220,820.00
15% ENGINEERING & CONTINGENCY					\$	33,123.00
TOTAL					\$	253,943.00

PUBLIC DRAINAGE FACILITIES POND G

ITEM	QUANTITY	UNIT	UNIT COST	TOTAL	
48" RCP	460	LF	\$ 200.00	\$	92,000.00
OUTLET BOX W/ MICROPOOL	1	EA	\$ 30,000.00	\$	30,000.00
66" IMPACT STRUCTURE	1	EA	\$ 105,000.00	\$	105,000.00
TRICKLE CHANNEL (REINFORCED)	1415	LF	\$ 80.00	\$	113,200.00
RIP RAP SPIILLWAY	380	CY	\$ 40.00	\$	15,200.00
OVERFLOW WALL -SPILLWAY	220	LF	\$ 170.00	\$	37,400.00
SUBTOTAL				\$	392,800.00
15% ENGINEERING & CONTINGENCY				\$	58,920.00
TOTAL				\$	451,720.00

SUMMARY

The proposed Foothills Farm Campus Filing No. 2 site is proposed to drain to onsite proposed public and private storm facilities. Since the MDDP anticipated the same land use, "C" runoff coefficients, and time of concentration rates, the total stormwater from this development generally is equal to what was anticipated in the previously approved Marketplace at Interquest MDDP. Full Spectrum Detention is handled in proposed public Pond D and Pond G Facilities as proposed with Foothills Farm Campus Filing No. 2 development. All drainage facilities were sized using the current City of Colorado Springs Drainage Criteria and will safely discharge storm water runoff to adequate outfalls.

PREPARED BY:

Classic Consulting Engineers & Surveyors, LLC

Cathy M. Tessin, P.E. Project Manager



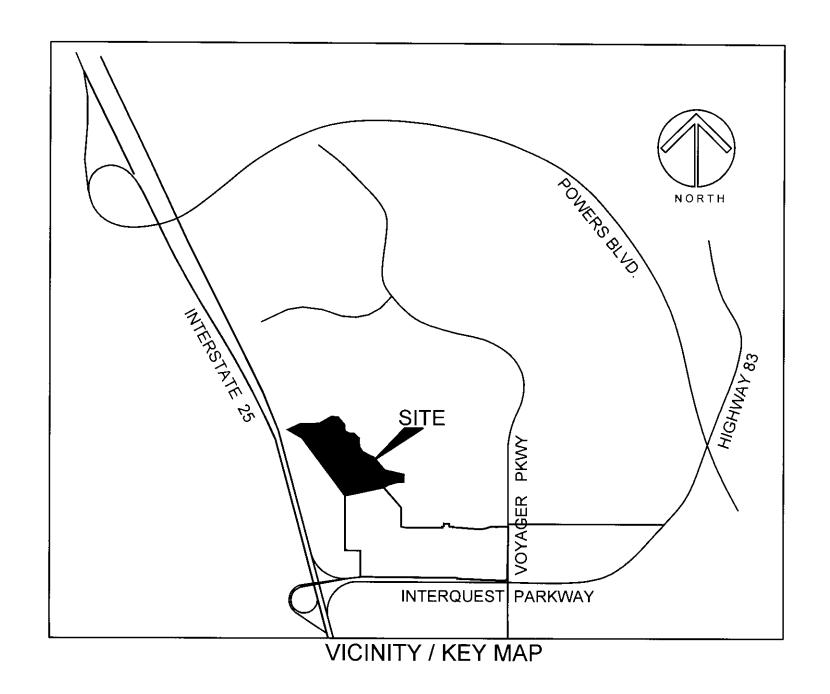
REFERENCES

- 1. City of Colorado Springs/County of El Paso Drainage Criteria Manual dated October 1991.
- 2. "Black Squirrel Creek Drainage Basin Planning Study," prepared by URS Corporation, dated January 1989.
- 3. "Master Development Drainage Plan for Allison Valley," prepared by Classic Consulting Engineers and Surveyors, dated February 2006.
- 4. "Allison Valley Master Development Drainage Plan Update," prepared by Kiowa Engineering Corporation., dated December 2011.
- 5. "2007 Addendum to Biological Assessment and Habitat Mitigation Plan for Allison Valley Project, Colorado Springs, Colorado," prepared by Walsh Environmental Scientists and Engineers, dated May 2007.
- 6. "Master Development Drainage Plan for Trailridge South at Northgate," JR Engineering, dated May 2000, revised September 2000 and January 2001.
- 7. "Final Drainage Report for Northgate Retail Filing No. 1," prepared by WestWorks Engineering, dated March 2007.
- 8. "Final Drainage Report for The Farm Filing No. 1A, 1B, and 1C and Preliminary Drainage Report for The Farm Filing No. 2," dated June 2014.
- 9. "Supplemental Drainage Letter for The Farm Filings 1A, 1B, and 1C," dated October 2015.
- 10. "Final Design Report for Allison Valley On-Site Reaches of Black Squirrel Creek and Middle Tributary Creek Channel Improvements," prepared by Classic Consulting Engineers and Surveyors, dated September 2008.
- 11. "Final Drainage Report for The Farm Filing No. 4," prepared by Classic Consulting Engineers and Surveyors, dated April 2017.
- 12. "The Farm Filing No. 4 Final Drainage Report Addendum," prepared by Classic Consulting Engineers and Surveyors, dated September 2017.
- 13. "The Farm Filing No. 4 Final Drainage Report Addendum Middle Tributary Box Culvert Detention/SWQ Ponds," prepared by Classic Consulting Engineers and Surveyors, pending approval.
- 14. "Master Development Drainage Plan for Marketplace at Interquest and Final Drainage Report for Marketplace at Interquest Filing No. 1 and Filing No. 2," prepared by Classic Consulting Engineers and Surveyors, approved August 2007

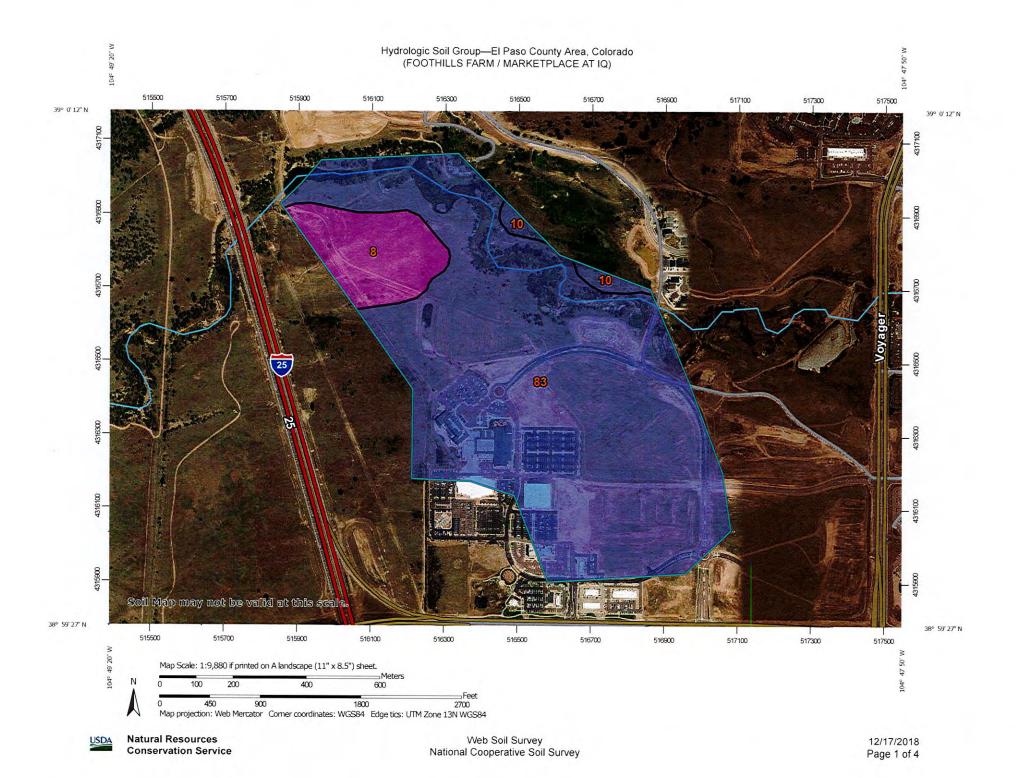


APPENDIX

VICINITY MAP



SOILS MAP (Web Soil Survey)



MAP LEGEND MAP INFORMATION Area of Interest (AOI) C The soil surveys that comprise your AOI were mapped at 1:24,000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale, D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available misunderstanding of the detail of mapping and accuracy of soil Water Features line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed В Transportation B/D Rails Please rely on the bar scale on each map sheet for map C measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available Local Roads Maps from the Web Soil Survey are based on the Web Mercator Soil Rating Lines projection, which preserves direction and shape but distorts Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more A/D accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 16, Sep 10, 2018 Soil map units are labeled (as space allows) for map scales D 1:50,000 or larger. Not rated or not available Date(s) aerial images were photographed: Jul 4, 2010—Oct 16, Soil Rating Points The orthophoto or other base map on which the soil lines were 100 compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	20.3	10.5%
10	Blendon sandy loam, 0 to 3 percent slopes	В	3.4	1.8%
83	Stapleton sandy loam, 3 to 8 percent slopes	В	169.9	87.8%
Totals for Area of Inter	rest		193.6	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified

Tie-break Rule: Higher

F.E.M.A. MAP

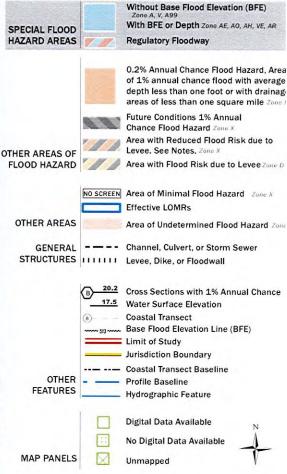
National Flood Hazard Layer FIRMette





Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The pin displayed on the map is an approximate point selected by the user and does not represe

an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 4/11/2019 at 7:01-06 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

HYDROLOGIC/HYDRAULIC CALCULATIONS



JOB NAME:	FOOTHILLS FARM - MARKETPLACE MDDP UPDATE
JOB NUMBER:	2399.86
DATE:	06/27/19
CALCULATED B	YCMT

FINAL DRAINAGE REPORT ~ BASIN RUNOFF COEFFICIENT SUMMARY

BASIN	TOTAL AREA (AC)	IMPERVIOUS AREA / STREETS				LANDSCAPE/UNDEVELOPED AREAS				WEIGHTED			WEIGHTED CA		
		AREA (AC)	C(2)	C(5)	C(100)	AREA (AC)	C(2)	C(5)	C(100)	C(2)	C(5)	C(100)	CA(2)	CA(5)	CA(100)
A	15.98	14.38	0.89	0.90	0.96	1.60	0.02	0.08	0.35	0.80	0.82	0.90	12.83	13.07	14.37
В	7.42	6.68	0.89	0.90	0.96	0.74	0.02	0.08	0.35	0.80	0.82	0.90	5.96	6.07	6.67
C	7.73	6.57	0.89	0.90	0.96	1.16	0.02	0.08	0.35	0.76	0.78	0.87	5.87	6.01	6.71
D	3.18	2.86	0.89	0.90	0.96	0.32	0.02	0.08	0.35	0.80	0.82	0.90	2.55	2.60	2.86
E	1.18	1.06	0.89	0.90	0.96	0.12	0.02	0.08	0.35	0.80	0.82	0.90	0.95	0.97	1.06
F	12.02	12.02	0.89	0.90	0.96	0.00	0.02	0.08	0.35	0.89	0.90	0.96	10.70	10.82	11.54
G	2.40	2.40	0.89	0.90	0.96	0.00	0.02	0.08	0.35	0.89	0.90	0.96	2.14	2.16	
Н	7.04	7.04	0.89	0.90	0.96	0.00	0.02	0.08	0.35	0.89	0.90	0.96	6.27	6.34	2.30
1	4.11	3.49	0.89	0.90	0.96	0.62	0.02	0.08	0.35	0.03	0.78	0.96	3.12	3.19	6.76 3.57
J	7.79	7.01	0.89	0.90	0.96	0.78	0.02	0.08	0.35	0.80	0.76	0.90	6.26	6.37	7.00
K	1.16	0.99	0.89	0.90	0.96	0.17	0.02	0.08	0.35	0.76	0.78	0.90	0.20		
L	1.21	1.03	0.89	0.90	0.96	0.18	0.02	0.08	0.35	0.76	0.78	0.87	0.00	0.90	1.01
M	3.07	2.61	0.89	0.90	0.96	0.46	0.02	0.08	0.35	0.76	0.78	0.87		0.94	1.05
N	1.23	1.11	0.89	0.90	0.96	0.40	0.02	0.08	0.35	0.76	0.76	0.87	2.33	2.39	2.67
0	1.91	1.91	0.89	0.90	0.96	0.00	0.02	0.08	0.35	0.89	0.82	E PE E	0.99	1.01	1.11
P1	0.88	0.75	0.89	0.90	0.96	0.00	0.02	0.08	0.35	0.89	0.90	0.96 0.87	1.70	1.72	1.83
P2	0.66	0.56	0.89	0.90	0.96	0.10	0.02	0.08	0.35	0.76	0.78	0.87	0.67	0.69	0.77
P3	0.72	0.61	0.89	0.90	0.96	0.10	0.02	0.08	0.35	0.76	0.78	0.87	0.50	0.51	0.57
P4	0.32	0.27	0.89	0.90	0.96	0.05	0.02	0.08	0.35	0.76	0.78	0.87	0.55 0.24	0.56	0.63
P5	0.39	0.33	0.89	0.90	0.96	0.06	0.02	0.08	0.35	0.76	0.78	0.87	0.24	0.25	0.28
P6	1.03	0.88	0.89	0.90	0.96	0.15	0.02	0.08	0.35	0.76	0.78	0.87	0.29	0.30 0.80	0.34
Q	1.99	1.79	0.89	0.90	0.96	0.20	0.02	0.08	0.35	0.80	0.76	0.90	1.60	1.63	0.89
R	1.34	1.34	0.89	0.90	0.96	0.00	0.02	0.08	0.35	0.89	0.90	0.96	1.19	1.03	1.79
S1	0.72	0.58	0.89	0.90	0.96	0.14	0.02	0.08	0.35	0.72	0.74	0.84	0.52	0.53	0.60
S2	0.47	0.38	0.89	0.90	0.96	0.09	0.02	0.08	0.35	0.72	0.74	0.84	0.34	0.35	0.39
T	3.75	3.00	0.89	0.90	0.96	0.75	0.02	0.08	0.35	0.72	0.74	0.84	2.69	2.76	3.14
U1	3.11	0.47	0.89	0.90	0.96	2.64	0.02	0.08	0.35	0.15	0.20	0.44	0.47	0.63	1.37
U2	1.21	0.60	0.89	0.90	0.96	0.60	0.02	0.08	0.35	0.46	0.49	0.66	0.55	0.59	0.79
V	1.24	1.24	0.89	0.90	0.96	0.00	0.02	0.08	0.35	0.89	0.90	0.96	1.10	1.12	1.19
W	7.04	5.98	0.89	0.90	0.96	1.06	0.02	0.08	0.35	0.76	0.78	0.87	5.35	5.47	6.11
X	0.91	0.91	0.89	0.90	0.96	0.00	0.02	0.08	0.35	0.89	0.90	0.96	0.81	0.82	0.11
Υ	1.16	1.16	0.89	0.90	0.96	0.00	0.02	0.08	0.35	0.89	0.90	0.96	1.03	1.04	1.11
Z	2.01	1.81	0.89	0.90	0.96	0.20	0.02	0.08	0.35	0.80	0.82	0.90	1.61	1.64	1.81
AA	2.12	0.21	0.89	0.90	0.96	1.90	0.02	0.08	0.35	0.11	0.16	0.41	0.23	0.34	0.87
BB	2.75	0.27	0.89	0.90	0.96	2.47	0.02	0.08	0.35	0.11	0.16	0.41	0.29	0.44	1.13

JOB NAME: FOOTHILLS FARM - MARKETPLACE MDDP UPDATE

JOB NUMBER: DATE:

2399.86

CALC'D BY:

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 $t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$ $V = C_v S_w^{-0.5}$ Tc=L/V

Table 6-7. Conveyance Coefficient, C.

Type of Land Surface	C,
Heavy meadow	2.5
Tillage/field L	5
Riprap (not buried)* $t_c = \frac{1}{180} + 10$	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

For buried riprap, select C_v value based on type of vegetative cover.

FINAL DRAINAGE REPORT ~ BASIN RUNOFF SUMMARY

		WEIGHTE	D		OVER	LAND		STRE	ET / CH	IANNEL	FLOW	Tc	11	NTENSIT	Y	TOT	AL FLO	ows
BASIN	CA(2)	CA(5)	CA(100)	C(5)	Length (ft)	Height (ft)	Tc (min)	Length (ft)	Slope (%)	Velocity (fps)	Tc (min)	TOTAL (min)	l(2) (in/hr)	l(5) (in/hr)	I(100) (in/hr)	Q(2) (cfs)	Q(5) (cfs)	Q(100 (cfs)
A	12.83	13.07	14.37	0.08	25	1	5.8	800	2.0%	2.8	4.7	10.5	3.23	4.05	6.80	41	53	98
В	5.96	6.07	6.67	0.08	25	1	5.8	600	2.0%	2.8	3.5	9.4	3.37	4.23	7.10	20	26	47
C	5.87	6.01	6.71	0.08	15	2	3.0	2000	3.0%	3.5	9.6	12.7	3.01	3.78	6.34	18	23	43
D	2.55	2.60	2.86	0.08	12	2	2.5	200	3.0%	3.5	1.0	5.0	4.12	5.17	8.68	11	13	25
E	0.95	0.97	1.06	0.08	10	2	2.2	200	3.0%	3.5	0.0	5.0	4,12	5.17	8.68	4	5	9
F	10.70	10.82	11.54	0.08	15	2	3.0	1200	2.0%	2.8	7.1	10.1	3.28	4.11	6.91	35	44	80
G	2.14	2.16	2.30	0.08	60	1	12.1	600	1.0%	2.0	5.0	17.1	2.66	3.33	5.59	6	7	13
Н	6.27	6.34	6.76	0.08	5	1	1.5	200	4.0%	4.0	0.8	5.0	4.12	5.17	8.68	26	33	59
1	3.12	3.19	3.57	0.08	20	1	4.8	300	1.0%	2.0	2.5	7.3	3.66	4.59	7.71	11	15	28
J	6.26	6.37	7.00	0.08	25	4	3.7	600	2.0%	2.8	3.5	7.2	3.68	4.62	7.75	23	29	54
К	0.88	0.90	1.01	0.08	20	1	4.8	150	3.0%	3.5	0.7	5.6	3.99	5.01	8.41	4	5	8
L	0.92	0.94	1.05	0.08	20	1	4.8	150	3.0%	3.5	0.7	5.6	3.99	5.01	8.41	4	5	9
M	2.33	2.39	2.67	0.08	20	1	4.8	300	3.0%	3.5	1.4	6.3	3.85	4.83	8.10	9	12	22
N	0.99	1.01	1.11	0.08	10	0.5	3.4	150	2.0%	2.8	0.9	5.0	4.12	5.17	8.68	4	5	10
0	1.70	1.72	1.83	0.08	15	0.3	5.7	500	2.0%	2.8	2.9	8.6	3.47	4.35	7.31	6	7	13
P1	0.67	0.69	0.77	0.08	10	1	2.7	200	2.0%	2.8	1.2	5.0	4.12	5.17	8.68	3	4	7

JOB NAME: FOOTHILLS FARM - MARKETPLACE MDDP UPDATE

JOB NUMBER: 2399.86
DATE: 07/26/06

CALC'D BY: CMT

 $t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$ $V = C_v S_w^{-0.5}$ Tc=L/V

Table 6-7. Conveyance Coefficient, C.

Type of Land Surface	C,
Heavy meadow	2.5
Tillage/field $t = \frac{L}{L} + 10$	5
Riprap (not buried)* $I_c = \frac{1}{180} + 10$	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

For buried riprap, select C_v value based on type of vegetative cover.

FINAL DRAINAGE REPORT ~ BASIN RUNOFF SUMMARY

7		WEIGHTE	D		OVER	LAND		STRE	ET / CH	ANNEL	FLOW	Tc	- 1	NTENSIT	Υ	TOT	AL FLO	ows
BASIN	CA(2)	CA(5)	CA(100)	C(5)	Length (ft)	Height (ft)	Tc (min)	Length (ft)	Slope (%)	Velocity (fps)	Tc (min)	TOTAL (min)	l(2) (in/hr)	l(5) (in/hr)	I(100) (in/hr)	Q(2) (cfs)	Q(5) (cfs)	Q(100) (cfs)
P2	0.50	0.51	0.57	0.08	10	1	2.7	100	2.0%	2.8	0.6	5.0	4.12	5.17	8.68	2	3	5
P3	0.55	0.56	0.63	0.08	20	1_	4.8	100	1.5%	2.4	0.7	5.5	4.00	5.02	8.43	2	3	5
P4	0.24	0.25	0.28	0.08	20	1	4.8	100	3.0%	3.5	0.5	5.3	4.05	5.07	8.52	1	1.3	2.4
P5	0.29	0.30	0.34	0.08	10	1	2.7	100	2.0%	2.8	0.6	5.0	4.12	5.17	8.68	1	1.6	2.9
P6	0.78	0.80	0.89	0.08	10	1	2.7	100	3.0%	3.5	0.5	5.0	4.12	5.17	8.68	3	4	8
Q	1.60	1.63	1.79	0.08	20	1	4.8	50	2.0%	2.8	0.3	5.1	4.09	5.13	8.61	7	8	15
R	1.19	1.21	1.29	0.08	0	0	0.0	50	1.0%	2.0	0.4	5.0	4.12	5.17	8.68	5	6	11
S1	0.52	0.53	0.60	0.08	40	6	4.8	220	3.0%	3.5	0.0	5.0	4.12	5.17	8.68	2	3	5
S2	0.34	0.35	0.39	0.08	20	0.5	6.1	220	3.0%	3.5	1.0	7.1	3.70	4.65	7.80	1	2	3
T	2.69	2.76	3.14	0.08	100	1	18.4	500	1.0%	2.0	4.2	22.6	2.33	2.91	4.88	6	8	15
U1	0.47	0.63	1.37	0.08	100	7	9.7	800	1.0%	2.0	6.7	16.4	2.71	3.39	5.69	1	2	8
U2	0.55	0.59	0.79	0.08	15	10	1.8	300	1.0%	2.0	2.5	5.0	4.12	5.17	8.68	2	3	7
٧	1.10	1.12	1.19	0.08	0	0	0.0	50	1.0%	2.0	0.4	5.0	4.12	5.17	8.68	5	6	10
W	5.35	5.47	6.11	0.08	20	1	4.8	300	1.0%	2.0	2.5	7.3	3.66	4.59	7.71	20	25	47
X	0.81	0.82	0.87	0.08	20	1	4.8	100	1.0%	2.0	0.8	5.7	3.97	4.98	8.36	3	4	7
Y	1.03	1.04	1.11	0.08	20	1	4.8	100	1.0%	2.0	0.8	5.7	3.97	4.98	8.36	4	5	9

JOB NAME: FOOTHILLS FARM - MARKETPLACE MDDP UPDATE JOB NUMBER: 2399.86 07/26/06 DATE: CALC'D BY: CMT

 $t_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{S^{0.33}}$ $V = C_v S_w^{0.5}$ Tc=L/V

Table 6-7. Conveyance Coefficient, C.

Type of Land Surface	Cv
Heavy meadow	2.5
Tillage/field $t = \frac{L}{L} + 10$	5
Riprap (not buried)* $I_c = \frac{1}{180} + 10$	6.5
Short pasture and lawns	7
Nearly bare ground	10
Grassed waterway	15
Paved areas and shallow paved swales	20

FINAL DRAINAGE REPORT ~ BASIN RUNOFF SUMMARY

		WEIGHTE	D		OVER	LAND		STRE	ET / CH	ANNEL I	FLOW	Tc	II	NTENSIT	Υ	TOT	AL FLO	SWC
BASIN	CA(2)	CA(5)	CA(100)	C(5)	Length (ft)	Height (ft)	Tc (min)	Length (ft)	Slope (%)	Velocity (fps)	Tc (min)	TOTAL (min)	l(2) (in/hr)	I(5) (in/hr)	I(100) (in/hr)	Q(2) (cfs)	Q(5) (cfs)	Q(100) (cfs)
Z	1.61	1.64	1.81	0.08	20	1	4.8	50	2.0%	2.8	0.3	5.1	4.09	5.13	8.61	7	8	16
AA	0.23	0.34	0.87	0.08	10	6	1.5	350	1.0%	2.0	2.9	5.0	4.12	5.17	8.68	1	2	8
BB	0.29	0.44	1.13	0.08	12	8	1.6	650	1.0%	2.0	5.4	7.0	3.72	4.66	7.83	1	2	9

JOB NAME: FOOTHILLS FARM - MARKETPLACE MDDP UPDATE

 JOB NUMBER:
 2399.86

 DATE:
 06/27/19

 CALCULATED BY:
 CMT

FINAL DRAINAGE REPORT ~ SURFACE ROUTING SUMMARY

					inte	nsity	F	low	
Design Point(s)	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	I(5)	I(100)	Q(5)	Q(100)	COMMENT
1	BASIN A & B	19.14	21.04	10.5	4.05	6.80	78	143	SPRINGS @FF APTS A FUTURE PARCEL
2	BASIN C	6.01	6.71	12.7	3.78	6.34	23	43	EX. FED DRIVE
3	BASINS D , E	3.57	3.92	5.0	5.17	8.68	18	34	FF CAMPUS FIL .1 AND FUTURE
4	BASIN Q	1.63	1.79	5.1	5,13	8.61	8	15	FUTURE COMMERCIAL
5	BASIN K, L	1.91	2.06	5.6	5.01	8.41	10	17	FUTURE COMMERCIA
6	BASIN M	2.39	2.67	6.3	4.83	8.10	12	22	FUTURE COMMERCIA
7	BASIN N, 1/2 BASIN O, P3, P4	2.68	2.93	8.6	4.35	7.31	12	21	PROP.8' PRIV. INLET
8	BASIN P5, 1/2 BASIN O	1.16	1.25	8.6	4.35	7.31	5	9	PROP. 6' PRIV. INLET
9	BASIN P1	0.69	0.77	5.0	5.17	8.68	4	7	PROP. 4' PRIV. INLET
10	BASIN P2	0.51	0.57	5.0	5.17	8.68	3	5	PROP. 4' PRIV. INLET
11	BASIN P6	0.80	0.89	5.0	5.17	8.68	4	8	PROP. 4' PRIV. INLET
12	BASIN S1	0.53	0.60	5.0	5.17	8.68	3	5	PROP. 4' PRIV. INLET
13	BASIN S2	0.35	0.39	7.1	4.65	7.80	2	3	PROP. 4' PRIV. INLET
14	BASIN U1	0.63	1.37	16.4	3.39	5.69	2	8	PROP. 4' PRIV. INLET
15	BASIN U2	0.59	0.79	5.0	5.17	8.68	3	7	PROP. 4' PRIV. INLET
16	BASIN W, X, Y	7.33	8.10	7.3	4.59	7.71	34	62	FUTURE COMMERCIA
17	BASIN Z	1.64	1.81	5.1	5.13	8.61	8	16	FUTURE COMMERCIA

JOB NAME:	FOOTHILLS FARM - MARKETPLACE MDDP UPDATE
JOB NUMBER:	2399.86
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CALCULATED BY:	CMT

^{*} PIPES ARE LISTED AT MAXIMUM SIZE REQUIRED TO ACCOMMODATE Q100 FLOWS AT MINIMUM GRADE. REFER TO INDIVIDUAL PIPE SHEETS FOR HYDRAULIC INFORMATION.

FINAL DRAINAGE REPORT ~ PIPE ROUTING SUMMARY

	Ì				Inten	sity	FI	DW	
Pipe Run	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	I(5)	I(100)	Q(5)	Q(100)	Pipe Size*
1	DP 1+ DP2	25.15	27.75	14.1	3.62	6.07	91	169	SPRINGS @FF APTS AND FUTURE PARCEL
2	DP 3	3.57	3.92	5.0	5.17	8.68	18	34	FFC Fil. 1and Fut. commercial
3	PIPE 1+2	28.71	31.67	14.1	3.62	6.07	104	192	TOTAL FLOW AT FEDERAL OUTFALL
4	DP 4 + PIPE 3	30.34	33.46	14.1	3.62	6.07	110	203	OUTFALL TO POND D
5	BASINS F, G, H	19.31	20.60	15.8	3.44	5.78	66	119	Marketplace IQ Scheels, Fut. Commercial, and ex. commercial
6	BASIN I	3.19	3.57	7.3	4.59	7.71	15	28	Future GWL expansion commercial parcel /ex. stub
7	BASIN J	6.37	7.00	7.2	4.62	7.75	29	54	Ex. GWL buidling/parking lot
8	PIPES 5, 6, 7	28.88	31.17	18.5	3.21	5.38	93	168	TOTAL FLOW AT GWL OUTFALL
9	DP 5	1.91	2.06	5.6	5.01	8.41	10	17	24" @ 0.5% PRIV.
10	PIPE 8+9	30.79	33.23	18.5	3.21	5.38	99	179	60" @ 0.5% PUBLIC
11	DP 6	2.39	2.67	6.29	4.83	8.10	12	22	30" @ 0.5% PRIV.
12	PIPE 10 + 11 + BASIN AA	33.52	36.77	20.5	3.05	5.12	102	188	66" @ 0.5% PUBLIC
13	DP 9 + BASIN T (1/2)	2.07	2.34	5.00	5.17	8.68	11	20	24" @ 1% PRIV
1 4	DP 10	0.51	0.57	5.00	5.17	8.68	3	5	18" @ 0.5% PRIV.

JOB NAME:	FOOTHILLS FARM - MARKETPLACE MDDP UPDATE
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^{*} PIPES ARE LISTED AT MAXIMUM SIZE REQUIRED TO ACCOMMODATE Q100 FLOWS AT MINIMUM GRADE. REFER TO INDIVIDUAL PIPE SHEETS FOR HYDRAULIC INFORMATION.

FINAL DRAINAGE REPORT ~ PIPE ROUTING SUMMARY

					Inten	sity	Fle	ow	
Pipe Run	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	I(5)	l(100)	Q(5)	Q(100)	Pipe Size*
15	PIPE 13 + 14	2.58	2.91	5.0	5.17	8.68	13	25	30" @ 0.5% PRIV.
16	DP 7+ PIPE 15	5.26	5.84	8.6	4.35	7.31	23	43	30" @ 1.0% PRIV.
17	DP 8 + PIPE 16	6.42	7.09	8.6	4.35	7.31	28	52	36" @ 1.0% PRIV.
18	DP 11	0.80	0.89	5.00	5.17	8.68	4	8	18" @ 0.5% PRIV.
19	PIPE 17 + 18 + BASIN R	8.42	9.28	8.6	4.35	7.31	37	68	36" @1.0% PRIV.
20	PIPE 19 + 12	41.94	46.04	23.6	2.84	4.77	119	220	66" @0.5% PUBLIC
21	DP 12	0.53	0.60	5.00	5.17	8.68	3	5	18" @ 1.0% PRIVATE
22	DP 13 + PIPE 21	0.88	1.00	7.1	4.65	7.80	4	8	18" @ 1.0% PRIVATE
23	PIPE 20 + 22 + BASIN BB	43.26	47.49	24.3	2.80	4.69	121	223	TOTAL FLOW TO POND G - 66" OUTFALL
24	BASIN T 1/2	1.38	1.57	22.6	2.91	4.88	4	8	24" @ 0.5% PRIV.
25	DP 14 + PIPE 24	2.01	2.94	22.6	2.91	4.88	6	14	24" @ 1.0% PRIV.
26	BASIN V + DP 15	1.71	1.98	5.0	5.17	8.68	9	17	24" @ 1.0% PRIV.
27	PIPE 25+ 26	3.72	4.93	22.6	2.91	4.88	11	24	30" @ 0.5% PRIV.
28	PIPE 25+ 27	5.73	7.87	22.6	2.91	4.88	17	38	36" @ 0.5% PRIV.

JOB NAME:	FOOTHILLS FARM - MARKETPLACE MDDP UPDATE
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^{*} PIPES ARE LISTED AT MAXIMUM SIZE REQUIRED TO ACCOMMODATE Q100 FLOWS AT MINIMUM GRADE. REFER TO INDIVIDUAL PIPE SHEETS FOR HYDRAULIC INFORMATION.

FINAL DRAINAGE REPORT ~ PIPE ROUTING SUMMARY

					Inten	sity	Flo	ow .	
Pipe Run	Contributing Basins	Equivalent CA(5)	Equivalent CA(100)	Maximum Tc	I(5)	I(100)	Q(5)	Q(100)	Pipe Size*
29	DP 16 + PIPE 28	13.06	15.97	22.6	2.91	4.88	38	78	TOTAL POND G - 36" @ 1.5% PRIV. OUTFALL
30	PIPE 23 + 29	56.32	63.46	23.1	2.87	4.82	162	306	TOTAL POND G INFLOW

INLET MANAGEMENT

INLET NAME	DP7	DP8	DP9	DP10	DP11	DP12
Site Type (Urban or Rural)	URBAN	URBAN	URBAN	URBAN	URBAN	URBAN
nlet Application (Street or Area)	STREET	STREET	STREET	STREET	STREET	STREET
lydraulic Condition	In Sump	In Sump	In Sump	In Sump	In Sump	In Sump
nlet Type	Colorado Springs D-10-R	Colorado Springs D-10-R	Colorado Springs D-10-R	Colorado Springs D-10-R	Colorado Springs D-10-R	Colorado Springs D-10-I
50 055W50 W0W5				300	Solorado Opinigo D-10-10	Colorado Springs D-10-1
ER-DEFINED INPUT						
User-Defined Design Flows Minor Q _{Known} (cfs)	12.0	5.0				
Major Q _{Known} (cfs)	21.0		4.0	3.0	4.0	3.0
Wajor Q _{Known} (Cra)	21.0	9.0	7.0	5.0	8.0	5.0
Bypass (Carry-Over) Flow from Upstream						
Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received	No Disease Flow Bossins		
Minor Bypass Flow Received, Q _b (cfs)	0.0	140 Bypass Flow Received	0.0	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Receive
Major Bypass Flow Received, Q _b (cfs)	0.0		0.0			
			0,0			
Watershed Characteristics						
Subcatchment Area (acres)						
Percent Impervious						
NRCS Soil Type						
Watershed Profile						
Overland Slope (ft/ft)						
Overland Length (ft)						
Channel Slope (ft/ft)						
Channel Length (ft)						
and the state of t						
Minor Storm Rainfall Input						
Design Storm Return Period, T, (years)						
One-Hour Precipitation, P ₁ (inches)						
and the state of t						
Major Storm Rainfall Input						
Design Storm Return Period, T, (years)						
One-Hour Precipitation, P ₁ (inches)						
One-Hour Precipitation, P ₁ (inches)						
One-Hour Precipitation, P, (inches)						
One-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs)	12.0	5.0	4.0	3.0	4.0	30
One-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs)	21.0	5.0 9.0	4.0 7.0		4.0	3.0
One-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _h (cfs)	21.0 N/A			5.0	8.0	5.0
One-Hour Precipitation, P ₁ (inches) ALCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs)	21.0	9.0	7.0		8.0 N/A	5.0 N/A
One-Hour Precipitation, P ₁ (inches) ALCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs)	21.0 N/A N/A	9.0 N/A	7.0 N/A	5.0 N/A	8.0	5.0
One-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _h (cfs)	21.0 N/A N/A	9.0 N/A N/A	7.0 N/A N/A	5.0 N/A	8.0 N/A	5.0 N/A
One-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs)	21.0 N/A N/A me	9.0 N/A N/A	7.0 N/A N/A	5.0 N/A	8.0 N/A N/A	5.0 N/A N/A
One-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti C C C C	21.0 N/A N/A me N/A N/A	9.0 N/A N/A N/A	7.0 N/A N/A N/A N/A	5.0 N/A N/A	8.0 N/A N/A	5.0 N/A N/A
One-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti C C S Overland Flow Velocity, Vi	21.0 N/A N/A MA N/A N/A	9.0 N/A N/A N/A N/A	7.0 N/A N/A	5.0 N/A N/A	8.0 N/A N/A N/A N/A	5.0 N/A N/A N/A N/A
One-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti C C ₅ Overland Flow Velocity, Vi Channel Flow Velocity, Vi Channel Flow Velocity, Vi	21.0 N/A N/A N/A N/A N/A N/A N/A	9.0 N/A N/A N/A N/A N/A N/A	7.0 N/A N/A N/A N/A	5.0 N/A N/A N/A N/A	8.0 N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A
One-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti C C C C C C C C C C C C C C C C C C C	21.0 N/A N/A Me N/A N/A N/A N/A N/A	9.0 N/A N/A N/A N/A N/A N/A N/A	7.0 N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A	8.0 N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A
One-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti C C ₂ Overland Flow Velocity, Vi Channel Flow Velocity, VI Overland Flow Time, Ti Channel Travel Time, Ti	21.0 N/A N/A N/A N/A N/A N/A N/A N/A	9.0 N/A N/A N/A N/A N/A N/A N/A	7.0 N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A	8.0 N/A N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A N/A
One-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti	21.0 N/A N/A N/A N/A N/A N/A N/A N/A	9.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A	7.0 N/A N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A N/A	B.0 N/A N/A N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A N/A
One-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti Companies of Calculated (Companies) Diverland Flow Velocity, Vi Channel Flow Velocity, Vi Channel Travel Time, Ti Channel Travel Time, Ti Calculated Time of Concentration, T _c Regional T _c	21.0 N/A	9.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	7.0 N/A N/A N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A	8.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A
One-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti Calculated Flow Velocity, Vi Dhannel Flow Velocity, Vi Dannel Flow Velocity, Vi Dannel Flow Time, Ti Calculated Time of Concentration, T _c Regional T _c Rescommended T _c	21.0 N/A N/A N/A Me N/A N/A N/A N/A N/A N/A N/A N/A N/A N/	9.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	7.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	B.0 NVA NVA NVA NVA NVA NVA NVA NVA NVA NVA	5.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A
Cone-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti Cosponent (Calculated) Ana	21.0 N/A	9.0 N/A N/A N/A N/A N/A N/A N/A N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A	8.0 N/A N/A N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
One-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Nethod Proceedings (cfs) Major Flow, Q (cfs) Major Flow,	21.0 N/A	9.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A	8.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
One-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Nethod Proceedings (cfs) Major Flow, Q (cfs) Major Flow,	21.0 N/A	9.0 N/A N/A N/A N/A N/A N/A N/A N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A	8.0 N/A N/A N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
One-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q ₆ (cfs) Major Flow Bypassed Downstream, Q ₆ (cfs) Minor Storm (Calculated) Analysis of Flow Ti C C C C C C C C C C C C C C C C C C C	21.0 N/A	9.0 N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A	8.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
One-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti C C ₂ Overland Flow Velocity, Vi Channel Travel Time, Ti Channel Travel Time, Ti Calculated Time of Concentration, T _c Regional T _c Recommended T _c T _c selected by Use	21.0 N/A	9.0 N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A	8.0 N/A N/A N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
Doe-Hour Precipitation, P ₁ (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti C	21.0 N/A	9.0 N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A	8.0 N/A N/A N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
Doe-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Storm (Second Downstream, Q _b (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Storm (Calculated) Analysis of Flow Tick Downland Flow Velocity, Vi Channel Flow Velocity, Vi Channel Flow Velocity, Vi Channel Flow Velocity, Vi Channel Travel Time, Ti Calculated Time of Concentration, T, Recommended T, Quickless Concen	21.0 N/A	9.0 N/A	7.0 N/A	5.0 N/A	8.0 N/A N/A N/A N/A N/A N/A N/A N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
Concention Precipitation, Pr. (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti Calculated Interpretation (cfs) Deverland Flow Velocity, Vi Doverland Flow Velocity, Vi Doverland Flow Time, Ti Calculated Time of Concentration, T _c Regional Travel Time, Ti Calculated Time of Concentration, T _c Regional Travel Time, Ti Calculated Time of Concentration, T _c Regional Travel Time, Ti Calculated Time of Concentration, T _c Regional Travel Time, Ti Calculated Local Peak Flow, Q _p Major Storm (Calculated) Analysis of Flow Ti Calculated Local Peak Flow, Q _p Major Storm (Calculated) Analysis of Flow Ti Calculated Flow Velocity, Vi	21.0 N/A	9.0 N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/	8.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
One-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti C C C C C C C C C C C C C C C C C C C	21.0 N/A N/A N/A N/A N/A N/A N/A N/	9.0 N/A	7.0 N/A	5.0 N/A	8.0 N/A	5.0 N/A
One-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Wajor Storm (Calculated) Analysis of Flow Ti Calculated Time of Concentration, T _c Recommended T _c T, selected by User Recommended T _c T, selected by User Major Storm (Calculated) Analysis of Flow Ti Calculated Local Peak Flow, Q _p Major Storm (Calculated) Analysis of Flow Ti Calculated Flow Velocity, Vi Channel Flow Velocity Channel	21.0 N/A	9.0 N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/	8.0 N/A N/A N/A N/A N/A N/A N/A N/	5.0 N/A
Doe-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Storm (Calculated) Analysis of Flow Ti Calculated Flow Velocity, Vi Doverland Flow Velocity, Vi Doverland Flow Flow, Ti Calculated Time of Concentration, T _c Regional T _c Regional T _c Regional T _c Recommended T _c T _c selected by User Design Rainfail Intensity, I Calculated Local Peak Flow, Q _p Major Storm (Calculated) Analysis of Flow Ti Calculated Local Peak Flow, Vi Doverland Flow Velocity, Vi	21.0 N/A N/A N/A N/A N/A N/A N/A N/	9.0 N/A	7.0 N/A	5.0 N/A	8.0 N/A	5.0 N/A
One-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti C C C C C C C C C C C C C C C C C C C	21.0 N/A	9.0 N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/	8.0 N/A	5.0 N/A
One-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Flow Bypassed Downstream, Q _b (cfs) Minor Storm (Calculated) Analysis of Flow Ti Calculated Flow Velocity, Vi Channel Flow Velocity, Vi Channel Flow Velocity, Vi Channel Flow Time, Ti Calculated Time of Concentration, T _c Recommended T _c T _c selected by User Design Rainfall intensity, I Calculated Local Peak Flow, Q _p Major Storm (Calculated) Analysis of Flow Ti Calculated Time of Concentration, T _c The Storm (Calculated) Analysis of Flow Ti Calculated Time Of Concentration, T _c The Storm (Calculated) Analysis of Flow Ti Calculated Time Of Concentration, T _c The Storm (Calculated) Analysis of Flow Ti Calculated Time Of Concentration, T _c The Storm (Calculated) Analysis of Flow Ti Calculated Time of Concentration, T _c The Storm (Calculated) Analysis of Flow Time Ti Calculated Time of Concentration, T _c	21.0 N/A N/A N/A N/A N/A N/A N/A N/	9.0 N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/	8.0 N/A N/A N/A N/A N/A N/A N/A N/	5.0 N/A
One-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Flow Place In Inches In Inches In	21.0 N/A N/A N/A N/A N/A N/A N/A N/	9.0 N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/	8.0 N/A N/A N/A N/A N/A N/A N/A N/	5.0 N/A
Cone-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Flow Plow Interpretation of Flow Ti Calculated Flow Velocity, Vi Doverland Flow Velocity, Vi Doverland Flow Flow, Ti Calculated Time of Concentration, T _c Regional T _c Regional T _c Regional Flow Velocity, Vi Doverland Flow Velocity, Vi Channel Flow Velocity, Vi Doverland Flow Velo	21.0 N/A	9.0 N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/	8.0 N/A	5.0 N/A
Cone-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Minor Storm (Secondary Peak Flow, Q (cfs) Minor Storm (Secondary Peak Flow, Q (cfs) Minor Storm (Calculated) Analysis of Flow Ti Control Flow Velocity, Vi Channel Flow Velocity, Vi Channel Flow Velocity, Vi Channel Flow Velocity, Vi Channel Travel Time, Ti Calculated Time of Concentration, T, Recommended T, T, selected by User Major Storm (Calculated) Analysis of Flow Ti Concentration (Calculated) Analysis of Flow T	21.0 N/A N/A N/A N/A N/A N/A N/A N/	9.0 N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/	8.0 N/A N/A N/A N/A N/A N/A N/A N/	5.0 N/A
One-Hour Precipitation, P, (inches) LCULATED OUTPUT Minor Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Total Design Peak Flow, Q (cfs) Major Flow Bypassed Downstream, Q _b (cfs) Major Storm (Calculated) Analysis of Flow Ti Calculated Flow Velocity, Vt Doverland Flow Time, Ti Calculated Time of Concentration, T _c Regional T _c Regional T _c Regional T _c Regional T _c Recommended T _c T _c selected by User Design Rainfail intensity, I Calculated Local Peak Flow, Q _p Major Storm (Calculated) Analysis of Flow Ti Calculated Flow Velocity, Vt Doverland Flow Velocity, Vt	21.0 N/A	9.0 N/A	7.0 N/A	5.0 N/A N/A N/A N/A N/A N/A N/A N/	8.0 N/A	5.0 N/A

INLET MANAGEMENT

INLET NAME	DP13	DP14	DP15
Site Type (Urban or Rural)	URBAN	URBAN	URBAN
Inlet Application (Street or Area)	STREET	STREET	STREET
Hydraulic Condition	In Sump	In Sump	In Sump
Inlet Type	Colorado Springs D-10-R	Colorado Springs D-10-R	Colorado Springs D-10-R
ER-DEFINED INPUT			
User-Defined Design Flows			
Minor Q _{Known} (cfs)	2.0	6.0	3.0
Major Q _{Knovn} (cfs)	3.0	15.0	7.0
Bypass (Carry-Over) Flow from Upstream			
Receive Bypass Flow from:	No Bypass Flow Received	No Bypass Flow Received	No Bypass Flow Received
Minor Bypass Flow Received, Q, (cfs)	Dypuss i ion i tocolved	140 Dypass Flow NecelVed	140 Dypass Flow Received
Major Bypass Flow Received, Q. (cfs)			
Percent Impervious NRCS Soil Type			
Watershed Profile			
Overland Slope (ft/ft)			
Overland Length (ft)			
Channel Slope (ft/ft)			
Channel Length (ft)			
Minor Storm Rainfall Input			
Design Storm Return Period, T, (years)			
Design Storm Return Period, T, (years) One-Hour Precipitation, P ₁ (inches)			
One-Hour Precipitation, P ₁ (inches)			

CALCULATED OUTPUT

Minor Total Design Peak Flow, Q (cfs)	2.0	6.0	3.0
Major Total Design Peak Flow, Q (cfs)	3.0	15.0	7.0
Minor Flow Bypassed Downstream, Q _b (cfs)	N/A	N/A	N/A
Major Flow Bypassed Downstream, Q _b (cfs)	N/A	N/A	N/A
Minor Storm (Calculated) Analysis of Flow T			
C	N/A	N/A	N/A
C ₅	N/A	N/A	N/A
Overland Flow Velocity, Vi	N/A	N/A	N/A
Channel Flow Velocity, Vt	N/A	N/A	N/A
Overland Flow Time, Ti	N/A	N/A	N/A
Channel Travel Time, Tt	N/A	N/A	N/A
Calculated Time of Concentration, T _c	N/A	N/A	N/A
Regional T	N/A	N/A	N/A
Recommended T _c	N/A	N/A	N/A
T _c selected by User	N/A	N/A	N/A
Design Rainfall Intensity, I	N/A	N/A	N/A
Calculated Local Peak Flow, Q _p	N/A	N/A	N/A
Major Storm (Calculated) Analysis of Flow T	N/A	N/A	****
C ₅	N/A N/A		N/A
Overland Flow Velocity, Vi		N/A	N/A
Channel Flow Velocity, Vt	N/A N/A	N/A	N/A
Overland Flow Time. Ti	N/A N/A	N/A N/A	N/A
Channel Travel Time. Tt	N/A N/A	N/A N/A	N/A
Calculated Time of Concentration, T.	N/A	7.2.1	N/A
Regional T _c		N/A	N/A
Recommended T.	N/A	N/A	N/A
T _c selected by User	N/A	N/A	N/A
Design Rainfall Intensity, I	N/A	N/A	N/A
Calculated Local Peak Flow, Q,	N/A N/A	N/A	N/A
		N/A	N/A

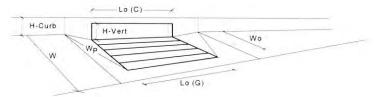
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) FOOTHLLS FARM CAMPUS FIL. 2 ENT Project: Inlet ID: DP7 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0 012 and 0 020) 0.020 Height of Curb at Gutter Flow Line Hours 6.00 inches Distance from Curb Face to Street Crown TCROWN 20.0 Gutter Width 2.00 W: Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So = 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) NSTREET : 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 20.0 20.0 Warning 02 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm **d**MAX 8.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm

MAJOR STORM Allowable Capacity is based on Depth Criterion

Major Storm

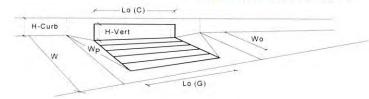
SUMP

SUMP



Design Information (Input)	Colorado Springs D-10-R ▼		MINOR	MAJOR	
ype of Inlet	DECEMBER 100 DECEM	Type =	Colorado Sp	orings D-10-R	
ocal Depression (additional to d	continuous gutter depression 'a' from above)	a _{local} =	4.00		inches
Number of Unit Inlets (Grate or 0		No =	1		
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	8.0	12.0	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L ₀ (G) =	N/A		feet
Width of a Unit Grate		W _a =	N/A		feet
Area Opening Ratio for a Grate (typical values 0 15-0 90)	A _{ratio} =	N/A		
Clogging Factor for a Single Gra	te (typical value 0.50 - 0.70)	C ₁ (G) =	N/A	N/A	
Grate Weir Coefficient (typical va	alue 2.15 - 3.60)	C _w (G) =	N/A		
Grate Orifice Coefficient (typical	value 0.60 - 0.80)	C ₀ (G) =	N/A		
Curb Opening Information		_	MINOR	MAJOR	_
ength of a Unit Curb Opening		$L_{\alpha}(C) =$	8.00		feet
Height of Vertical Curb Opening	in Inches	H _{vert} =	8.00		inches
Height of Curb Orifice Throat in I	nches	H _{throat} =	8.00		inches
Angle of Throat (see USDCM Fig	gure ST-5)	Theta =	81.00		degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	30	feet
Clogging Factor for a Single Cur	D Opening (typical value 0 10)	C _t (C) =	0.10	0.10	
Curb Opening Weir Coefficient (ypical value 2.3-3.7)	C _N (C) =	3.60		T
Curb Opening Orifice Coefficient	(typical value 0 60 - 0.70)	C ₀ (C) =	0.67		
ow Head Performance Reduc	tion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Eq	uation	d _{Curb} =	0.50	0.83	ft
Combination Inlet Performance F	Reduction Factor for Long Inlets	RF _{Combination} =	0.81	1.00	9
Curb Opening Performance Red	uction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	To the second
Grated Inlet Performance Reduc	tion Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
			MINOR	MAJOR	
Total Inlet Interception C	apacity (assumes clogged condition)	$Q_a =$	13.9	26.4	cfs
nlet Capacity IS GOOD for Min	or and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	12.0	21.0	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) FOOTHLLS FARM CAMPUS FIL. 2 ENT Project: Inlet ID: DP8 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} 6.00 inches Distance from Curb Face to Street Crown TCROWN 20.0 Gutter Width W= 2.00 Street Transverse Slope Sx : 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Sa 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) NSTREET = 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 20.0 Warning 02 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 8.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP cfs

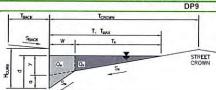


Design Information (Input)	Colorado Springs D-10-R		MINOR	MAJOR	
Type of Inlet		Type =	Colorado Sp	rings D-10-R	
Local Depression (additional to conf	inuous gutter depression 'a' from above)	a _{local} =	4.00		inches
Number of Unit Inlets (Grate or Curl	Opening)	No =	1		
Water Depth at Flowline (outside of	local depression)	Ponding Depth =	8.0	12.0	inches
Grate Information			MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate		L ₀ (G) =	N/A		feet
Width of a Unit Grate		W _o =	N/A	38	feet
Area Opening Ratio for a Grate (typ	cal values 0.15-0.90)	A _{ratio} =	N/A		
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _t (G) =	N/A	N/A	
Grate Weir Coefficient (typical value	2.15 - 3.60)	C., (G) =	N/A	1	1
Grate Orifice Coefficient (typical val	ue 0 60 - 0 80)	C ₀ (G) =	N/A	-	
Curb Opening Information			MINOR	MAJOR	_
Length of a Unit Curb Opening		L _a (C) =	6.00		feet
Height of Vertical Curb Opening in I	nches	H _{vert} =	8.00		inches
Height of Curb Orifice Throat in Inch	es	H _{throat} =	8.00		inches
Angle of Throat (see USDCM Figure	ST-5)	Theta =	81.00		degrees
Side Width for Depression Pan (typi	cally the gutter width of 2 feet)	W _p =	2.00		feet
Clogging Factor for a Single Curb O	pening (typical value 0.10)	C _i (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typi	cal value 2.3-3.7)	C _w (C) =	3.60		
Curb Opening Orifice Coefficient (ty	pical value 0.60 - 0.70)	C ₀ (C) =	0.67		
Low Head Performance Reduction	(Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equat	on	d _{Curb} =	0.50	0.83	ft
Combination Inlet Performance Red	uction Factor for Long Inlets	RF _{Compination} =	0.94	1.00	
Curb Opening Performance Reducti	on Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduction	Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
			MINOR	MAJOR	2
Total Inlet Interception Cap	acity (assumes clogged condition)	Q _a =	11.2	19.8	cfs
nlet Capacity IS GOOD for Minor	and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	5.0	9.0	cfs

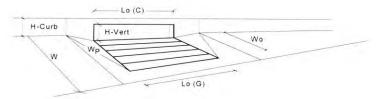
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)

Project: Inlet ID: FOOTHLLS FARM CAMPUS FIL. 2 ENT



Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) n_{BACK} : 0.020 Height of Curb at Gutter Flow Line HCURB 6.00 inches Distance from Curb Face to Street Crown TOROWN 18.0 Gutter Width W= 2.00 Street Transverse Slope Sy 0.030 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft) Sw = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition Sa 0.000 ft/ft Manning's Roughness for Street Section (typically between 0.012 and 0.020) n_{STREET} = 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 18.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm dmax 6.0 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion Minor Storm Major Storm MAJOR STORM Allowable Capacity is based on Depth Criterion SUMP SUMP



Design Information (Input)	Colorado Springs D-10-R ▼		MINOR	MAJOR	
Type of Inlet	The state of the s	Type =	Colorado Sp	orings D-10-R	
Local Depression (additional to	continuous gutter depression 'a' from above)	a _{local} =	4.00		inches
Number of Unit Inlets (Grate or 0	37	No =	11		
Water Depth at Flowline (outside	e of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information			MINOR	MAJOR	∇ Override Depths
Length of a Unit Grate		$L_{\sigma}(G) =$	N/A		feet
Width of a Unit Grate		W ₀ =	N/A		feet
Area Opening Ratio for a Grate	typical values 0.15-0.90)	A _{ratio} =	N/A	1.0	
Clogging Factor for a Single Gra	te (typical value 0.50 - 0.70)	C ₁ (G) =	N/A	N/A	
Grate Weir Coefficient (typical v.	alue 2.15 - 3.60)	C _N (G) =	N/A		
Grate Orifice Coefficient (typical	value 0.60 - 0.80)	C ₀ (G) =	N/A		
Curb Opening Information			MINOR	MAJOR	
Length of a Unit Curb Opening		L ₂ (C) =	4.00	-	feet
Height of Vertical Curb Opening	in Inches	H _{vert} =	8.00		inches
Height of Curb Orifice Throat in	nches	H _{throat} =	8.00		inches
Angle of Throat (see USDCM Fig	gure ST-5)	Theta =	81.00		degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00		feet
Clogging Factor for a Single Cur	b Opening (typical value 0.10)	C, (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60		
Curb Opening Orifice Coefficient	(typical value 0.60 - 0.70)	C _n (C) =	0.67		
Low Head Performance Reduc	tion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Ed	uation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance F		RF _{Combination} =	0.85	1.00	
Curb Opening Performance Red		RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduc	tion Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
			MINOR	MAJOR	
Total Inlet Interception C	apacity (assumes clogged condition)	$Q_a =$	4.6	12.6	cfs
nlet Capacity IS GOOD for Mir	or and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	4.0	7.0	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) FOOTHLLS FARM CAMPUS FIL. 2 ENT Project: Inlet ID: DP10 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TBACK = 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) 0.020 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 Distance from Curb Face to Street Crown 18.0 Gutter Width W= 2.00 Street Transverse Slope Sx = 0.030 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0 083 ft/ft) Sw = 0.083 ft/ft Street Longitudinal Slope - Enter 0 for sump condition So 0.000 ft/ft Manning's Roughness for Street Section (typically between 0 012 and 0 020) NSTREET = 0.020 Minor Storm Major Storm Max. Allowable Spread for Minor & Major Storm 18.0 18.0 Max. Allowable Depth at Gutter Flowline for Minor & Major Storm 12.0 Check boxes are not applicable in SUMP conditions MINOR STORM Allowable Capacity is based on Depth Criterion

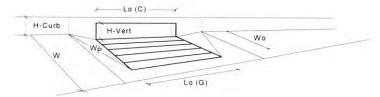
MAJOR STORM Allowable Capacity is based on Depth Criterion

Minor Storm

SUMP

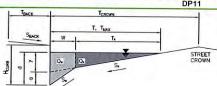
Major Storm

SUMP

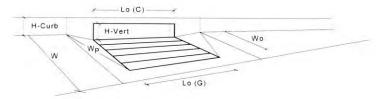


Design Information (Input)	Coloredo Cortero D 10 D		MINOR	MAJOR	
Type of Inlet	Colorado Springs D-10-R	Type =	Colorado Sp	orings D-10-R	
Local Depression (additional to	continuous gutter depression 'a' from above)	a _{local} =	4.00		inches
Number of Unit Inlets (Grate or		No =	1	1.00	
Water Depth at Flowline (outside	e of local depression)	Ponding Depth =	6.0	7.8	inches
Grate Information			MINOR	MAJOR	Covernide Depths
Length of a Unit Grate		L ₀ (G) =	N/A	1 - 1 -	feet
Width of a Unit Grate		W _o =	N/A		feet
Area Opening Ratio for a Grate	(typical values 0.15-0.90)	A _{ratio} =	N/A		
Clogging Factor for a Single Gra	ate (typical value 0 50 - 0 70)	C, (G) =	N/A	N/A	
Grate Weir Coefficient (typical v	alue 2.15 - 3.60)	C _w (G) =	N/A	750	
Grate Orifice Coefficient (typical	value 0.60 - 0.80)	C _o (G) =	N/A		
Curb Opening Information		_	MINOR	MAJOR	_
Length of a Unit Curb Opening		L ₀ (C) =	4.00		feet
Height of Vertical Curb Opening	in Inches	H _{vert} =	8.00		inches
Height of Curb Orifice Throat in	Inches	H _{throat} =	8.00		inches
Angle of Throat (see USDCM Fig.	gure ST-5)	Theta =	81.00		degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00		feet
Clogging Factor for a Single Cur	b Opening (typical value 0.10)	C, (C) =	0.10	0.10	7
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	7	
Curb Opening Orifice Coefficient	t (typical value 0.60 - 0.70)	C ₀ (C) =	0.67		
Low Head Performance Reduc	ction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Ed	quation	d _{Curb} =	0.33	0.48	ft
Combination Inlet Performance I		RF _{Combination} =	0.85	1.00	
Curb Opening Performance Red		RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduc	tion Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
			MINOR	MAJOR	
Total Inlet Interception C	apacity (assumes clogged condition)	Q _a =	4.6	8.0	cfs
nlet Capacity IS GOOD for Mir	nor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	3.0	5.0	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)



Gutter Geometry (Enter data in the blue cells)				
Maximum Allowable Width for Spread Behind Curb	TBACK =	10.0	T _{ff}	
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	S _{BACK} =	0.020	ft/ft	
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	n _{BACK} =	0.020		
Height of Curb at Gutter Flow Line	H _{curs} =	6.00	Inches	
Distance from Curb Face to Street Crown	T _{CROWN} =	18.0	fi fi	
Gutter Width	W =	2.00	ff	
Street Transverse Slope	S _x =	0.030	ft/ft	
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	S _W =	0.083	ft/ft	
Street Longitudinal Slope - Enter 0 for sump condition	So =	0.000	ft/ft	
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	n _{street} =	0.020		
		Minor Storm	Major Storm	
Max. Allowable Spread for Minor & Major Storm	T _{MAX} =	18.0	18.0 ft	
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	d _{MAX} =	6.0	12.0 inch	nes
Check boxes are not applicable in SUMP conditions		Г	Г	
MINOR STORM Allowable Capacity is based on Depth Criterion		14-01-00-0		
MAJOR STORM Allowable Capacity is based on Depth Criterion	ο Γ	Minor Storm	Major Storm	
and of ordin Allowable Capacity is based on Depth Criterion	Q _{allow} =	SUMP	SUMP cfs	



Design Information (Input)	Colorado Springs D-10-R ▼		MINOR	MAJOR	
Type of Inlet	Colorado Springs D-10-R	Type =	Colorado Sp	orings D-10-R	
Local Depression (additional to o	ontinuous gutter depression 'a' from above)	a _{local} =	4.00	V 1	inches
Number of Unit Inlets (Grate or C	Curb Opening)	No =	1		TO Y
Water Depth at Flowline (outside	of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information			MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate		L ₀ (G) =	N/A		feet
Width of a Unit Grate		W ₀ =	N/A		feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A		
Clogging Factor for a Single Gra	te (typical value 0 50 - 0.70)	C ₁ (G) =	N/A	N/A	
Grate Weir Coefficient (typical va	alue 2.15 - 3.60)	C _w (G) =	N/A	1	
Grate Orifice Coefficient (typical	value 0 60 - 0 80)	C ₀ (G) =	N/A	11 11 11 11 11 11	
Curb Opening Information		_	MINOR	MAJOR	_
Length of a Unit Curb Opening		L ₀ (C) =	4.00	-	feet
Height of Vertical Curb Opening	in Inches	H _{vert} =	8.00		inches
Height of Curb Orifice Throat in I	nches	H _{throat} =	8.00		inches
Angle of Throat (see USDCM Fig	jure ST-5)	Theta =	81.00		degrees
Side Width for Depression Pan (ypically the gutter width of 2 feet)	W _p =	2.00		feet
Clogging Factor for a Single Curl	Opening (typical value 0.10)	C, (C) =	0.10	0.10	7
Curb Opening Weir Coefficient (t	ypical value 2.3-3.7)	C _w (C) =	3.60		7
Curb Opening Orifice Coefficient	(typical value 0.60 - 0.70)	C ₀ (C) =	0.67		
Low Head Performance Reduc	tion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Eq	uation	d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance F	Reduction Factor for Long Inlets	RF _{Combination} =	0.85	1.00	
Curb Opening Performance Redi	uction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduct	ion Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
			MINOR	MAJOR	
Total Inlet Interception C	apacity (assumes clogged condition)	$Q_a =$	4.6	12.6	cfs
nlet Capacity IS GOOD for Min	or and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	4.0	8.0	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) FOOTHLLS FARM CAMPUS FIL. 2 ENT Project: Inlet ID: DP12 STREET Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb TRACK = 10.0 Side Slope Behind Curb (leave blank for no conveyance credit behind curb) SBACK 0.020 ft/ft Manning's Roughness Behind Curb (typically between 0.012 and 0.020) nBACK = 0.020 Height of Curb at Gutter Flow Line H_{CURB} = 6.00 Distance from Curb Face to Street Crown 15.0 Gutter Width W= 3.00 Street Transverse Slope Sx = 0.020 ft/ft Gutter Cross Slope (typically 2 inches over 24 inches or 0 083 ft/ft) Sw = 0.083 ft/ft

Max. Allowable Depth at Gutter Flowline for Minor & Major Storm Check boxes are not applicable in SUMP conditions

Manning's Roughness for Street Section (typically between 0.012 and 0.020)

Street Longitudinal Slope - Enter 0 for sump condition

Max. Allowable Spread for Minor & Major Storm

MINOR STORM Allowable Capacity is based on Depth Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion ft/ft

Major Storm

15.0

12.0

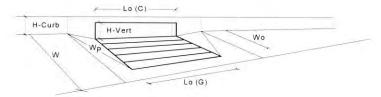
So:

0.000

0.020 Minor Storm

15.0

6.0

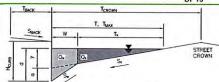


Design Information (Input)	Colorado Springs D-10-R		MINOR	MAJOR	
Type of Inlet	Colorado Springs D-10-R	Type =	Colorado Sp	rings D-10-R	
Local Depression (additional to	continuous gutter depression 'a' from above)	a _{local} =	4.00		inches
Number of Unit Inlets (Grate or 0	Curb Opening)	No =	1		
Water Depth at Flowline (outside	e of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information			MINOR	MAJOR	Override Depths
Length of a Unit Grate		L ₀ (G) =	N/A		feet
Width of a Unit Grate		W ₀ =	N/A		feet
Area Opening Ratio for a Grate	(typical values 0 15-0.90)	A _{ratio} =	N/A		
Clogging Factor for a Single Gra	ate (typical value 0.50 - 0.70)	C ₁ (G) =	N/A	N/A	
Grate Weir Coefficient (typical v	alue 2.15 - 3.60)	C _w (G) =	N/A		
Grate Orifice Coefficient (typical	value 0.60 - 0.80)	C ₀ (G) =	N/A		
Curb Opening Information			MINOR	MAJOR	_
Length of a Unit Curb Opening		L ₀ (C) =	4.00		feet
Height of Vertical Curb Opening	in Inches	H _{vert} =	8.00		inches
Height of Curb Orifice Throat in	Inches	H _{throat} =	8.00		inches
Angle of Throat (see USDCM Fig	gure ST-5)	Theta =	81.00	-	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	3.00		feet
Clogging Factor for a Single Cur	b Opening (typical value 0.10)	C, (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C, (C) =	3.60		
Curb Opening Orifice Coefficient	t (typical value 0.60 - 0.70)	C ₀ (C) =	0.67		
Low Head Performance Reduc	tion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Ed	quation	d _{Curb} =	0.25	0.75	ft
Combination Inlet Performance I	Reduction Factor for Long Inlets	RF _{Combination} =	0.85	1.00	
Curb Opening Performance Red	luction Factor for Long Inlets	RF _{Curb} =	1.00	1.00	10
Grated Inlet Performance Reduc	tion Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
			MINOR	MAJOR	
Total Inlet Interception C	apacity (assumes clogged condition)	$Q_a =$	3.7	12.6	cfs
nlet Capacity IS GOOD for Mir	nor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	3.0	5.0	cfs

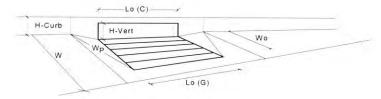
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)
FOOTHLLS FARM CAMPUS FIL. 2 ENT
DP13

Project: Inlet ID:



Gutter Geometry (Enter data in the blue cells)				
Maximum Allowable Width for Spread Behind Curb	T _{BACK} =	10.0	ft	
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	SBACK =	0.020	ft/ft	
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	n _{BACK} =	0.020		
Height of Curb at Gutter Flow Line	H _{CURB} =	6.00	linches	
Distance from Curb Face to Street Crown	T _{CROWN} =	15.0	ft	
Gutter Width	W =	2.00	ft	
Street Transverse Slope	S _X =	0.020	ft/ft	
Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	S _w =	0.083	ft/ft	
Street Longitudinal Slope - Enter 0 for sump condition	So =	0.000	ft/ft	
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	n _{street} =	0.020		
		Minor Storm	Major Storm	
Max. Allowable Spread for Minor & Major Storm	T _{MAX} =	15.0	15.0	ft
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	d _{MAX} =	6.0	12.0	inches
Check boxes are not applicable in SUMP conditions		Г	Г	
MINOR STORM Allowable Capacity is based on Depth Criterion		Minor Storm	Major Storm	
MAJOR STORM Allowable Capacity is based on Depth Criterion	Qallow =	SUMP	SUMP	cfs

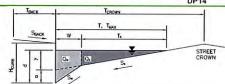


Design Information (Input)	Colorado Springs D-10-R	1	MINOR	MAJOR	4.
Type of Inlet	Colorado Springs D-10-R	Type =	Colorado Sp	orings D-10-R	
Local Depression (additional to	a _{local} =	4.00	-	inches	
Number of Unit Inlets (Grate or	Curb Opening)	No =	11		
Water Depth at Flowline (outside	e of local depression)	Ponding Depth =	5.1	5.1	inches
Grate Information			MINOR	MAJOR	C Overnide Depths
Length of a Unit Grate		L ₀ (G) =	N/A		feet
Width of a Unit Grate		W _a =	N/A	-	feet
Area Opening Ratio for a Grate	(typical values 0.15-0.90)	A _{ratio} =	N/A	-	
Clogging Factor for a Single Gra	ite (typical value 0 50 - 0 70)	C, (G) =	N/A	N/A	
Grate Weir Coefficient (typical v	alue 2.15 - 3.60)	C, (G) =	N/A		
Grate Orifice Coefficient (typical	value 0.60 - 0.80)	C ₀ (G) =	N/A	-	
Curb Opening Information		_	MINOR	MAJOR	_
Length of a Unit Curb Opening		L _o (C) =	4.00		feet
Height of Vertical Curb Opening	in Inches	H _{vert} =	8.00		inches
Height of Curb Orifice Throat in	Inches	H _{throat} =	8.00		inches
Angle of Throat (see USDCM Fig	gure ST-5)	Theta =	81.00		degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		W _p =	2.00		feet
Clogging Factor for a Single Cur	b Opening (typical value 0 10)	C ₁ (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60		
Curb Opening Onfice Coefficien	t (typical value 0.60 - 0.70)	C, (C) =	0.67		
Low Head Performance Reduc	tion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Gtate} =	N/A	N/A	ft
Depth for Curb Opening Weir Ed	quation	d _{Curb} =	0.26	0.26	ft
Combination Inlet Performance I	Reduction Factor for Long Inlets	RF _{Combination} =	0.72	0.72	
Curb Opening Performance Red	uction Factor for Long Inlets	RF _{curb} =	1.00	1.00	
Grated Inlet Performance Reduc	tion Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
			MINOR	MAJOR	
Total Inlet Interception C	apacity (assumes clogged condition)	Q _a =	3.2	3.2	cfs
nlet Capacity IS GOOD for Mir	nor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.0	3.0	cfs

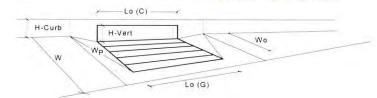
ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)
FOOTHLLS FARM CAMPUS FIL. 2 ENT
DP14

Project: Inlet ID:

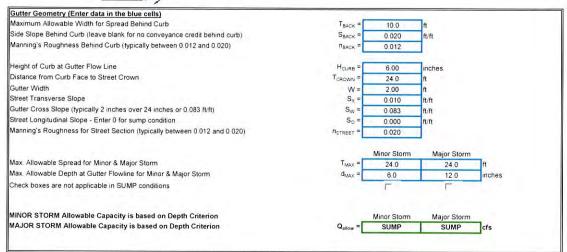


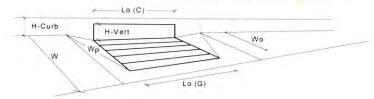
Gutter Geometry (Enter data in the blue cells)	A CONTRACTOR OF THE PERSON OF			
Maximum Allowable Width for Spread Behind Curb	TBACK =	10.0	ft	
Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	SBACK =	0.020	ft/ft	
Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	n _{BACK} =	0.012		
Height of Curb at Gutter Flow Line	H _{CURB} =	6.00	inches	
Distance from Curb Face to Street Crown	T _{CROWN} =	24.0	ft	
Gutter Width	W =	1.00	ft	
Street Transverse Slope	S _x =	0.010	ft/ft	
Gutter Cross Slope (typically 2 inches over 24 inches or 0 083 ft/ft)	S _W =	0.083	ft/ft	
Street Longitudinal Slope - Enter 0 for sump condition	So =	0.000	ft/ft	
Manning's Roughness for Street Section (typically between 0.012 and 0.020)	n _{street} =	0.012		
		Minor Storm	Major Storm	
Max. Allowable Spread for Minor & Major Storm	T _{MAX} =	24.0	24.0	ft
Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	d _{MAX} =	6.0	12.0	inches
Check boxes are not applicable in SUMP conditions			F	
MINOR STORM Allowable Capacity is based on Depth Criterion		Minor Storm	Major Storm	
MAJOR STORM Allowable Capacity is based on Depth Criterion	Q _{allow} =	SUMP	SUMP	cfs



Design Information (Input)	Colorado Springs D-10-R ▼		MINOR	MAJOR	
Type of Inlet	Colorado Springs D-10-R	Type =	Colorado Sp	rings D-10-R	
Local Depression (additional to	a _{focal} =	4.00	1	inches	
Number of Unit Inlets (Grate or	Curb Opening)	No =	1		
Water Depth at Flowline (outside	e of local depression)	Ponding Depth =	6.0	12.0	inches
Grate Information			MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate		L _o (G) =	N/A		feet
Width of a Unit Grate		W _o =	N/A		feet
Area Opening Ratio for a Grate	(typical values 0.15-0.90)	A _{ratio} =	N/A		
Clogging Factor for a Single Gra	ite (typical value 0 50 - 0 70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical v	alue 2.15 - 3.60)	C _w (G) =	N/A		
Grate Orifice Coefficient (typical	value 0.60 - 0.80)	C _o (G) =	N/A		
Curb Opening Information		-	MINOR	MAJOR	_
Length of a Unit Curb Opening		L ₀ (C) =	6.00		feet
Height of Vertical Curb Opening in Inches		H _{vert} =	8.00		inches
Height of Curb Orifice Throat in	Inches	H _{throat} =	8.00		inches
Angle of Throat (see USDCM Fi	gure ST-5)	Theta =	81.00		degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		W _p =	1.00		feet
Clogging Factor for a Single Cur	b Opening (typical value 0.10)	C ₁ (C) =	0.10	0.10	1
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60		
Curb Opening Orifice Coefficien	t (typical value 0.60 - 0.70)	C _a (C) =	0.67		
Low Head Performance Reduc	tion (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Ed	quation	d _{Curb} =	0.42	0.92	ft
Combination Inlet Performance	Reduction Factor for Long Inlets	RF _{Combination} =	0.71	1.00	
Curb Opening Performance Red	uction Factor for Long Inlets	RF _{Corb} =	1.00	1.00	I
Grated Inlet Performance Reduc	tion Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
			MINOR	MAJOR	
Total Inlet Interception C	apacity (assumes clogged condition)	Q _a =	6.9	19.7	cfs
	nor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	6.0	15.0	cfs

ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm) (Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Inlet ID: Tologom Tologo





Design Information (Input) Colorado Sprin	as D 10 B		MINOR	MAJOR	
Type of Inlet		Type =	Colorado Sp	rings D-10-R	
Local Depression (additional to continuous gutter depression 'a' from above)		a _{local} =	4.00		inches
Number of Unit Inlets (Grate or Curb Opening)		No =	1		
Water Depth at Flowline (outside of local depression		Ponding Depth =	6.0	12.0	inches
Grate Information			MINOR	MAJOR	✓ Override Depths
Length of a Unit Grate		L ₀ (G) =	N/A		feet
Width of a Unit Grate		W _o =	N/A	h	feet
Area Opening Ratio for a Grate (typical values 0.15-0	.90)	A _{ratio} =	N/A		1
Clogging Factor for a Single Grate (typical value 0.50	- 0.70)	C _t (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)		C _w (G) =	N/A		
Grate Orifice Coefficient (typical value 0.60 - 0.80)		C ₀ (G) =	N/A		-
Curb Opening Information		3000	MINOR	MAJOR	
Length of a Unit Curb Opening		$L_{o}(C) =$	4.00		feet
leight of Vertical Curb Opening in Inches		H _{vert} =	8.00	1 - 300	inches
Height of Curb Orifice Throat in Inches		H _{throat} =	8.00		inches
Angle of Throat (see USDCM Figure ST-5)		Theta =	81.00		degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)		W _p =	2.00		feet
Clogging Factor for a Single Curb Opening (typical value 0 10)		C, (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)		C,, (C) =	3.60		
Curb Opening Orifice Coefficient (typical value 0.60 -	0.70)	C ₀ (C) =	0.67		
_ow Head Performance Reduction (Calculated)			MINOR	MAJOR	
Depth for Grate Midwidth		d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation		d _{Curb} =	0.33	0.83	ft
Combination Inlet Performance Reduction Factor for		RF _{Combination} =	0.85	1.00	
Curb Opening Performance Reduction Factor for Lon		RF _{Curb} =	1.00	1.00	
Grated Inlet Performance Reduction Factor for Long I	nlets	RF _{Grate} =	N/A	N/A	
			MINOR	MAJOR	
Total Inlet Interception Capacity (assume	es clogged condition)	Q _a =	4.6	12.6	cfs
nlet Capacity IS GOOD for Minor and Major Storm	s(>Q PEAK)	Q PEAK REQUIRED =	3.0	7.0	cfs

	Workshe	et for Pil	PE 1
Project Description			
Friction Method	Manning Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.00800	ft/ft
Diameter		5.00	ft
Discharge		169.00	ft³/s
Results			
Normal Depth		3.16	ft
Flow Area		13.07	ft²
Wetted Perimeter		9.19	ft
Hydraulic Radius		1.42	ft
Top Width		4.82	ft
Critical Depth		3.73	ft
Percent Full		63.2	%
Critical Slope		0.00514	ft/ft
Velocity		12.93	ft/s
Velocity Head		2.60	ft
Specific Energy		5.76	ft
Froude Number		1.39	
Maximum Discharge		250.57	ft³/s
Discharge Full		232.93	ft³/s
Slope Full		0.00421	ft/ft
Flow Type	SuperCritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Average End Depth Over Rise		0.00	%
Normal Depth Over Rise		63.16	%

Infinity ft/s

Downstream Velocity

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	3.16	ft
Critical Depth	3.73	ft
Channel Slope	0.00800	ft/ft
Critical Slope	0.00514	ft/ft

	TTUINSIIC	erial Li	764
Project Description		VIII III III III III III III III III II	,
Friction Method	Manning Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.00500	ft/ft
Diameter		3.00	ft
Discharge		34.00	ft³/s
Results			
Normal Depth		1.89	ft
Flow Area		4.68	ft²
Wetted Perimeter		5.49	ft
Hydraulic Radius		0.85	ft
Top Width		2.90	ft
Critical Depth		1.89	ft
Percent Full		62.9	%
Critical Slope		0.00494	ft/ft
Velocity		7.26	ft/s
Velocity Head		0.82	ft
Specific Energy		2.71	ft
Froude Number		1.01	
Maximum Discharge		50.73	ft³/s
Discharge Full		47.16	ft³/s
Slope Full		0.00260	ft/ft
Flow Type	SuperCritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Average End Depth Over Rise		0.00	%
Name of Bankla Grand Bina		00.00	

62.88 %

Infinity ft/s

Normal Depth Over Rise

Downstream Velocity

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	1.89	ft
Critical Depth	1.89	ft
Channel Slope	0.00500	ft/ft
Critical Slope	0.00494	ft/ft

	Workshee	et for PIF	PE 3	
Project Description				
Friction Method	Manning Formula			
Solve For	Normal Depth			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00800	ft/ft	
Diameter		5.00	ft	
Discharge		192.00	ft³/s	
Results				
Normal Depth		3.46	ft	
Flow Area		14.49	ft²	
Wetted Perimeter		9.82	ft	
Hydraulic Radius		1.48	ft	
Top Width		4.62	ft	
Critical Depth		3.96	ft	
Percent Full		69.2	%	
Critical Slope		0.00580	ft/ft	
Velocity		13.25	ft/s	
Velocity Head		2.73	ft	
Specific Energy		6.19	ft	
Froude Number		1.32		
Maximum Discharge		250.57	ft³/s	
Discharge Full		232.93	ft³/s	
Slope Full		0.00544	ft/ft	
Flow Type	SuperCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Average End Depth Over Rise		0.00	%	

......

69.18 %

Infinity ft/s

Normal Depth Over Rise Downstream Velocity

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	3.46	ft
Critical Depth	3.96	ft
Channel Slope	0.00800	ft/ft
Critical Slope	0.00580	ft/ft

Worksheet for PIPE 4					
Project Description					
Friction Method	Manning Formula				
Solve For	Normal Depth				
Input Data					
Roughness Coefficient	0.01	3			
Channel Slope	0.0080	0 ft/ft			
Diameter	5.0	O ft			
Discharge	203.0	0 ft³/s			
Results					
Normal Depth	3.6	1 ft			
Flow Area	15.1	9 ft²			
Wetted Perimeter	10.1	6 ft			
Hydraulic Radius	1.5	O ft			
Top Width	4.4	B ft			
Critical Depth	4.0	5 ft			
Percent Full	72.	2 %			
Critical Slope	0.0061	7 ft/ft			
Velocity	13.3	7 ft/s			
Velocity Head	2.7	3 ft			
Specific Energy	6.3	9 ft			
Froude Number	1.2	3			
Maximum Discharge	250.5	7 ft³/s			
Discharge Full	232.9	3 ft³/s			
Slope Full	0.0060	3 ft/ft			
Flow Type	SuperCritical				
GVF Input Data					
Downstream Depth	0.00) ft			
Length	0.00) ft			
Number Of Steps	•)			
GVF Output Data					
Upstream Depth	0.00) ft			
Profile Description					
Profile Headloss	0.00) ft			

0.00 %

72.23 %

Infinity ft/s

Average End Depth Over Rise

Normal Depth Over Rise

Downstream Velocity

.....

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 3.61
 ft

 Critical Depth
 4.06
 ft

 Channel Slope
 0.00800
 ft/ft

 Critical Slope
 0.00617
 ft/ft

Project I	Description	

Friction Method Manning Formula Solve For Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.00500	ft/ft
Diameter	2.00	ft
Discharge	17.00	ft³/s

Results

Normal Depth		1.79	ft
Flow Area		2.96	ft²
Wetted Perimeter		4.96	ft
Hydraulic Radius		0.60	ft
Top Width		1.23	ft
Critical Depth		1.49	ft
Percent Full		89.4	%
Critical Slope		0.00694	ft/ f t
Velocity		5.74	ft/s
Velocity Head		0.51	ft
Specific Energy		2.30	ft
Froude Number		0.65	
Maximum Discharge		17.21	ft³/s
Discharge Full		16.00	ft³/s
Slope Full		0.00565	ft/ft
Flow Type	SubCritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	89.42	%
Downstream Velocity	Infinity	ft/s

Infinity	ft/s
1.79	ft
1.49	ft
0.00500	ft/ft
0.00694	ft/ft
	1.79 1.49 0.00500

Project Description	7/2		
Friction Method	Manning Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.00500	ft/ft
Diameter		5.00	ft
Discharge		179.00	ft³/s
Results			
Normal Depth		3.98	ft
Flow Area		16.75	ft²
Wetted Perimeter		11.02	ft
Hydraulic Radius		1.52	ft
Top Width		4.03	ft
Critical Depth		3.83	ft
Percent Full		79.6	%
Critical Slope		0.00541	ft/ft
Velocity		10.69	ft/s
Velocity Head		1.77	ft
Specific Energy		5.75	ft
Froude Number		0.92	
Maximum Discharge		198.09	ft³/s
Discharge Full		184.15	ft³/s
Slope Full		0.00472	ft/ft
Flow Type	SubCritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft

0.00 %

79.55 %

Infinity ft/s

Average End Depth Over Rise

Normal Depth Over Rise

Downstream Velocity

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 3.98
 ft

 Critical Depth
 3.83
 ft

 Channel Slope
 0.00500
 ft/ft

 Critical Slope
 0.00541
 ft/ft

4 for DIDE 44

Worksheet for PIPE 11			
Manning Formula			
Normal Depth			
0.013			
0.00500	ft/ft		
2.50	ft		
22.00	ft³/s		
1.63	ft		
3.39	ft²		
4.70	ft		
0.72	ft		
2.38	ft		
1.60	ft		
65.1	%		
0.00530	ft/ft		
6.50	ft/s		
0.66	ft		
2.28	ft		
0.96			
31.20	ft³/s		
29.00	ft³/s		
0.00288	ft/ft		
SubCritical			
0.00	ft		
0.00	ft		
0			
	Manning Formula Normal Depth 0.013 0.00500 2.50 22.00 1.63 3.39 4.70 0.72 2.38 1.60 65.1 0.00530 6.50 0.66 2.28 0.96 31.20 29.00 0.00288 SubCritical		

0.00 ft

0.00 %

65.14 %

Infinity ft/s

Profile Description Profile Headloss

Average End Depth Over Rise

Normal Depth Over Rise

Downstream Velocity

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 1.63
 ft

 Critical Depth
 1.60
 ft

 Channel Slope
 0.00500
 ft/ft

 Critical Slope
 0.00530
 ft/ft

	Worksheet for PIP	PE 12
Project Description		
Friction Method	Manning Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.00500	ft/ft
Diameter	5.50	ft
Discharge	189.00	ft³/s
Results		
Normal Depth	3.71	ft
Flow Area	17.04	ft²
Wetted Perimeter	10.60	ft
Hydraulic Radius	1.61	ft
Top Width	5.16	ft
Critical Depth	3.85	ft
Percent Full	67.4	%
Critical Slope	0.00452	ft/ft
Velocity	11.09	ft/s
Velocity Head	1.91	ft
Specific Energy	5.62	ft
Froude Number	1.08	
Maximum Discharge	255.42	ft³/s
Discharge Full	237.44	ft³/s
Slope Full	0.00317	ft/ft
Flow Type	SuperCritical	
GVF Input Data		
Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	
GVF Output Data		

Bentley Systems, Inc. Haestad Methods So	l uBienti6 y iFler wMaster	V8i (SELECTserie	s 1) [08	.11.01.0	3]
amana Campany Drive Suite 200 Mt Material CT 0	070F LICA . 4 000 755	1000	_		_

0.00 ft

0.00 ft

0.00 %

67.41 %

Infinity ft/s

Upstream Depth Profile Description Profile Headloss

Average End Depth Over Rise

Normal Depth Over Rise

Downstream Velocity

Upstream Velocity	Infinity	ft/s
Normal Depth	3.71	ft
Critical Depth	3.85	ft
Channel Slope	0.00500	ft/ft
Critical Slope	0.00452	ft/ft

Project Description

Friction Method Manning Formula Solve For Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01000	ft/ft
Diameter	2.00	ft
Discharge	20.00	ft³/s

Results			
Normal Depth		1.46	ft
Flow Area		2.46	ft²
Wetted Perimeter		4.10	ft
Hydraulic Radius		0.60	ft
Top Width		1.77	ft
Critical Depth		1.6 1	ft
Percent Full		73.1	%
Critical Slope		0.00812	ft/ft
Velocity		8.13	ft/s
Velocity Head		1.03	ft
Specific Energy		2.49	ft
Froude Number		1.22	
Maximum Discharge		24.33	ft³/s
Discharge Full		22.62	ft³/s
Slope Full		0.00782	ft/ft
Flow Type	SuperCritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	73.08	%
Downstream Velocity	Infinity	ft/s

Bentley Systems, Inc. Haestad Methods SoluBientl@p@lewMaster V8i (SELECTseries 1) [08.11.01.03] 27 Siemons Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Page 1 of 2

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 1.46
 ft

 Critical Depth
 1.61
 ft

 Channel Slope
 0.01000
 ft/ft

 Critical Slope
 0.00812
 ft/ft

2.66 ft

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Wetted Perimeter

Roughness Coefficient	0.013	
Channel Slope	0.00500	ft/ft
Diameter	1.50	ft
Discharge	5.00	ft³/s
Results		
Normal Depth	0.90	ft
Flow Area	1 11	ft2

Hydraulic Radius 0.42 Top Width 1.47 ft Critical Depth 0.86 ft Percent Full 60.1 Critical Slope 0.00578 ft/ft Velocity 4.51 ft/s Velocity Head 0.32 ft Specific Energy 1.22

 Specific Energy
 1.22 ft

 Froude Number
 0.91

 Maximum Discharge
 7.99 ft³/s

 Discharge Full
 7.43 ft³/s

 Slope Full
 0.00227 ft/ft

Flow Type SubCritical

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	60.08	%
Downstream Velocity	Infinity	ft/s

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 0.90
 ft

 Critical Depth
 0.86
 ft

 Channel Slope
 0.00500
 ft/ft

 Critical Slope
 0.00578
 ft/ft

Project Description	
---------------------	--

Friction Method Manning Formula Solve For Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.00500	ft/ft
Diameter	2.50	ft
Discharge	25.00	ft³/s

Results

Normal Depth		1.79	ft
Flow Area		3.76	ft²
Wetted Perimeter		5.04	ft
Hydraulic Radius		0.75	ft
Top Width		2.25	ft
Critical Depth		1.70	ft
Percent Full		71.6	%
Critical Slope		0.00569	ft/ft
Velocity		6.65	ft/s
Velocity Head		0.69	ft
Specific Energy		2.48	ft
Froude Number		0.91	
Maximum Discharge		31.20	ft³/s
Discharge Full		29.00	ft³/s
Slope Full		0.00372	ft/ft
Flow Type	SubCritical		

GVF Input Data

Downstream Depth	0.00	ft	
Length	0.00	ft	
Number Of Stens	Λ		

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	71.61	%
Downstream Velocity	Infinity	ft/s

Upstream Velocity	Infinity	ft/s
Normal Depth	1.79	ft
Critical Depth	1.70	ft
Channel Slope	0.00500	ft/ft
Critical Slope	0.00569	ft/ft

	Worksheet for PIP	PE 16
Project Description		
Friction Method	Manning Formula	
Solve For	Normal Depth	
Input Data		
Roughness Coefficient	0.013	
Channel Slope	0.01000	ft/ft
Diameter	2.50	ft
Discharge	43.00	ft³/s
Results		
Normal Depth	2.18	ft
Flow Area	4.54	ft²
Wetted Perimeter	6.02	ft
Hydrautic Radius	0.75	ft
Top Width	1.67	ft
Critical Depth	2.19	ft
Percent Full	87.2	%
Critical Slope	0.00994	ft/ft
Velocity	9.47	ft/s
Velocity Head	1.39	ft
Specific Energy	3.57	ft
Froude Number	1.01	
Maximum Discharge	44.12	ft³/s
Discharge Full	41.01	ft³/s
Slope Full	0.01099	ft/ft
Flow Type	SuperCritical	
GVF Input Data		
Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.00	ft

0.00 ft

0.00 %

87.19 %

Infinity ft/s

Profile Description
Profile Headloss

Average End Depth Over Rise

Normal Depth Over Rise

Downstream Velocity

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 2.18
 ft

 Critical Depth
 2.19
 ft

 Channel Slope
 0.01000
 ft/ft

 Critical Slope
 0.00994
 ft/ft

Worksheet for DIDE 17

	Workshee	t for PIP	E 17	
Project Description				
Friction Method	Manning Formula			
Solve For	Normal Depth			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00600	ft/ft	
Diameter		3.00	ft	
Discharge		52.00	ft³/s	
Results				
Normal Depth		2.48	ft	
Flow Area		6.24	ft²	
Wetted Perimeter		6.84	ft	
Hydraulic Radius		0.91	ft	
Top Width		2.28	ft	
Critical Depth		2.34	ft	
Percent Full		82.6	%	
Critical Slope		0.00667	ft/ft	
Velocity		8.33	ft/s	
Velocity Head		1.08	ft	
Specific Energy		3.56	ft	
Froude Number		0.89		
Maximum Discharge		55.57	ft³/s	
Discharge Full		51.66	ft³/s	
Slope Full		0.00608	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	

0.00 %

82.57 %

Infinity ft/s

Average End Depth Over Rise

Normal Depth Over Rise

Downstream Velocity

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 2.48 ft
 ft

 Critical Depth
 2.34 ft
 ft

 Channel Slope
 0.00600 ft/ft
 ft/ft

 Critical Slope
 0.00667 ft/ft
 ft/ft

Proj	ject	Desc	гірі	tion
-			•	

Friction Method Manning Formula Solve For Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01000	ft/ft
Diameter	1.50	ft
Discharge	8.00	ft³/s

Results

Results			
Normal Depth		0.98	ft
Flow Area		1.22	ft²
Wetted Perimeter		2.82	ft
Hydraulic Radius		0.43	ft
Top Width		1.43	ft
Critical Depth		1.10	ft
Percent Fulf		65.3	%
Critical Slope		0.00743	ft/ft
Velocity		6.54	ft/s
Velocity Head		0.67	ft
Specific Energy		1.64	ft
Froude Number		1.25	
Maximum Discharge		11.30	ft³/s
Discharge Full		10.50	ft³/s
Slope Full		0.00580	ft/ft
Flow Type	SuperCritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	65.32	%
Downstream Velocity	Infinity	ft/s

Infinity	ft/s
0.98	ft
1.10	ft
0.01000	ft/ft
0.00743	ft/ft
	0.98 1.10 0.01000

Project Description	
Friction Method	Manning Forr

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01000	ft/ft
Diameter	3.00	ft
Discharge	68.00	ft³/s

Results

Normal Depth		2.52	ft
Flow Area		6.33	ft²
Wetted Perimeter		6.94	ft
Hydraulic Radius		0.91	ft
Top Width		2.21	ft
Critical Depth		2.63	ft
Percent Full		83.8	%
Critical Stope		0.00939	ft/ft
Velocity		10.75	ft/s
Velocity Head		1.79	ft
Specific Energy		4.31	ft
Froude Number		1.12	
Maximum Discharge		71.74	ft³/s
Discharge Full		66.69	ft³/s
Slope Full		0.01040	ft/ft
Flow Type	SuperCritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	83.85	%
Downstream Velocity	Infinity	ft/s

Upstream Velocity	Infinity	ft/s
Normal Depth	2.52	ft
Critical Depth	2.63	ft
Channel Slope	0.01000	ft/ft
Critical Slope	0.00939	ft/ft

Normal Depth 2.52 ft Flow Area 6.34 ft² Wetted Perimeter 6.96 ft Hydraulic Radius 0.91 ft Top Width 2.20 ft Critical Depth 2.45 ft Percent Full 84.0 % Critical Slope 0.00737 ft/ft Velocity 8.99 ft/s Velocity Head 1.26 ft Specific Energy 3.78 ft Froude Number 0.93 Maximum Discharge 60.03 ft³/s Discharge Full 55.80 ft³/s Slope Full 0.00730 ft/ft Flow Type SubCritical GVF Input Data Downstream Depth 0.00 ft Length 0.00 ft Number Of Steps 0 GVF Output Data Upstream Depth 0.00 ft		Worksheet for PII	PE 19B
Solve For Normal Depth	Project Description		
Input Data Roughness Coefficient 0.013 Channel Slope 0.00700 ft/ft Diameter 3.00 ft Discharge 57.00 ft/fs Results	Friction Method	Manning Formula	
Roughness Coefficient 0.013 Channel Slope 0.00700 ft/ft 1.00 ft/ft 1.00 ft 1.0	Solve For	Normal Depth	
Channel Slope	Input Data		
Diameter 3.00 ft Discharge 57.00 ft*/s Results Normal Depth Flow Area 6.34 ft² Wetted Perimeter 6.96 ft Hydraulic Radius 0.91 ft Top Width 2.20 ft Critical Depth 2.45 ft Percent Full 84.0 % Critical Slope 0.00737 ft/ft Velocity 8.99 ft/s Velocity Head 1.26 ft Specific Energy 3.78 ft Froude Number 0.93 Maximum Discharge 60.03 ft*/s Discharge Full 55.80 ft*/s Slope Full 0.00730 ft/ft Flow Type SubCritical GVF Input Data Downstream Depth 0.00 ft Length 0.00 ft Number Of Steps 0 GVF Output Data Upstream Depth 0.00 ft	Roughness Coefficient	0.01	3
Discharge 57.00 ft/s	Channel Slope	0.0070	00 ft/ft
Normal Depth	Diameter	3.0	00 ft
Normal Depth 2.52 ft Flow Area 6.34 ft² Wetted Perimeter 6.96 ft Hydraulic Radius 0.91 ft Top Width 2.20 ft Critical Depth 2.45 ft Percent Full 84.0 % Critical Slope 0.00737 ft/ft Velocity 8.99 ft/s Velocity Head 1.26 ft Specific Energy 3.78 ft Froude Number 0.93 Maximum Discharge 60.03 ft³/s Discharge Full 55.80 ft³/s Slope Full 0.00730 ft/ft Flow Type SubCritical GVF Input Data Downstream Depth 0.00 ft Length 0.00 ft Number Of Steps 0 GVF Output Data Upstream Depth 0.00 ft	Discharge	57.0	00 ft³/s
Flow Area 6.34 ft² Wetted Perimeter 6.96 ft Hydraulic Radius 0.91 ft Top Width 2.20 ft Critical Depth 2.45 ft Percent Full 84.0 % Critical Slope 0.00737 ft/ft Velocity 8.99 ft/s Velocity Head 1.26 ft Specific Energy 3.78 ft Froude Number 0.93 Maximum Discharge 60.03 ft²/s Discharge Full 55.80 ft²/s Slope Full 0.00730 ft/ft Flow Type SubCritical GVF Input Data Downstream Depth 0.00 ft Number Of Steps 0.00 ft GVF Output Data Upstream Depth 0.00 ft	Results		
Wetted Perimeter 6.96 ft Hydraulic Radius 0.91 ft Top Width 2.20 ft Critical Depth 2.45 ft Percent Full 84.0 % Critical Slope 0.00737 ft/ft Velocity 8.99 ft/s Velocity Head 1.26 ft Specific Energy 3.78 ft Froude Number 0.93 Maximum Discharge 60.03 ft³/s Discharge Full 55.80 ft³/s Slope Full 0.00730 ft/ft Flow Type SubCritical GVF Input Data Downstream Depth 0.00 ft Length 0.00 ft Number Of Steps 0.00 ft GVF Output Data Upstream Depth 0.00 ft	Normal Depth	2.5	52 ft
Hydraulic Radius	Flow Area	6.3	34 ft²
Top Width 2.20 ft Critical Depth 2.45 ft Percent Full 84.0 % Critical Slope 0.00737 ft/ft Velocity 8.99 ft/s Velocity Head 1.26 ft Specific Energy 3.78 ft Froude Number 0.93 Maximum Discharge 60.03 ft//s Discharge Full 55.80 ft//s Slope Full 0.00730 ft/ft Flow Type SubCritical GVF Input Data Downstream Depth 0.00 ft Length 0.00 ft Number Of Steps 0 GVF Output Data Upstream Depth 0.00 ft	Wetted Perimeter	6.9	96 ft
Critical Depth 2.45 ft Percent Full 84.0 % Critical Slope 0.00737 ft/ft Velocity 8.99 ft/s Velocity Head 1.26 ft Specific Energy 3.78 ft Froude Number 0.93 ft Maximum Discharge 60.03 ft*/s Discharge Full 55.80 ft*/s Slope Full 0.00730 ft/ft Flow Type SubCritical GVF Input Data Downstream Depth 0.00 ft Length 0.00 ft Number Of Steps 0 0 GVF Output Data 0.00 ft	Hydraulic Radius	0.9	01 ft
Percent Full 84.0 % Critical Slope 0.00737 ft/ft Velocity 8.99 ft/s Velocity Head 1.26 ft Specific Energy 3.78 ft Froude Number 0.93 Maximum Discharge 60.03 ft³/s Discharge Full 55.80 ft³/s Slope Full 0.00730 ft/ft Flow Type SubCritical GVF Input Data Downstream Depth 0.00 ft Length 0.000 ft Number Of Steps 0 GVF Output Data Upstream Depth 0.00 ft	Top Width	2.2	0 ft
Critical Slope 0.00737 ft/ft Velocity 8.99 ft/s Velocity Head 1.26 ft Specific Energy 3.78 ft Froude Number 0.93 ft Maximum Discharge 60.03 ft²/s Discharge Full 55.80 ft²/s Slope Full 0.00730 ft/ft Flow Type SubCritical SubCritical GVF Input Data 0.00 ft Number Of Steps 0 0 GVF Output Data 0.00 ft	Critical Depth	2.4	.5 ft
Velocity 8.99 ft/s Velocity Head 1.26 ft Specific Energy 3.78 ft Froude Number 0.93 ft Maximum Discharge 60.03 ft³/s Discharge Full 55.80 ft³/s Slope Full 0.00730 ft/ft Flow Type SubCritical GVF Input Data Downstream Depth 0.00 ft Length 0.00 ft Number Of Steps 0 0 GVF Output Data Upstream Depth 0.00 ft	Percent Full	84.	0 %
Velocity Head 1.26 ft Specific Energy 3.78 ft Froude Number 0.93 Maximum Discharge 60.03 ft³/s Discharge Full 55.80 ft³/s Slope Full 0.00730 ft/ft Flow Type SubCritical GVF Input Data 0.00 ft Length 0.00 ft Number Of Steps 0 GVF Output Data Upstream Depth 0.00 ft	Critical Slope	0.0073	7 ft/ft
Specific Energy 3.78 ft	Velocity	8.9	9 ft/s
Froude Number	Velocity Head	1.2	6 ft
Maximum Discharge 60.03 ft³/s Discharge Full 55.80 ft³/s Slope Full 0.00730 ft/ft Flow Type SubCritical GVF Input Data Downstream Depth 0.00 ft Length 0.00 ft Number Of Steps 0 GVF Output Data Upstream Depth 0.00 ft	Specific Energy	3.7	8 ft
Discharge Full	Froude Number	0.9	3
Slope Full	Maximum Discharge	60.0	3 ft³/s
GVF Input Data Downstream Depth 0.00 ft Length 0.00 ft Number Of Steps 0 GVF Output Data Upstream Depth 0.00 ft	Discharge Full	55.8	0 ft³/s
GVF Input Data Downstream Depth 0.00 ft Length 0.00 ft Number Of Steps 0 GVF Output Data Upstream Depth 0.00 ft	Slope Full	0.0073	0 ft/ft
Downstream Depth 0.00 ft Length 0.00 ft Number Of Steps 0 GVF Output Data Upstream Depth 0.00 ft	Flow Type	SubCritical	
Length 0.00 ft Number Of Steps 0 GVF Output Data Upstream Depth 0.00 ft	GVF Input Data		
Number Of Steps 0 GVF Output Data Upstream Depth 0.00 ft	Downstream Depth	0.0	0 ft
Number Of Steps 0 GVF Output Data Upstream Depth 0.00 ft	Length	0.0	
Upstream Depth 0.00 ft	Number Of Steps		0
	GVF Output Data		
	Upstream Depth	0.0	0 ft
	Profile Description	•	

0.00 ft

0.00 %

84.04 %

Infinity ft/s

Profile Headloss

Average End Depth Over Rise

Normal Depth Over Rise

Downstream Velocity

Worksheet for PIPE 19B

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 2.52
 ft

 Critical Depth
 2.45
 ft

 Channel Slope
 0.00700
 ft/ft

 Critical Slope
 0.00737
 ft/ft

	Workshee	t for PIP	E 20
Project Description			
Friction Method	Manning Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.00500	ft/ft
Diameter		5.50	ft
Discharge		216.00	ft³/s
Results			
Normal Depth		4.12	ft
Flow Area		19.07	ft²
Wetted Perimeter		11.50	ft
Hydraulic Radius		1.66	ft
Top Width		4.77	ft
Critical Depth		4.11	ft
Percent Full		74.8	%
Critical Slope		0.00501	ft/ft
Velocity		11.32	ft/s
Velocity Head		1.99	ft
Specific Energy		6.11	ft
Froude Number		1.00	
Maximum Discharge		255.42	ft³/s
Discharge Full		237.44	ft³/s
Slope Full		0.00414	ft/ft
low Type	SubCritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
lumber Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			

0.00 ft

0.00 %

74.85 %

Infinity ft/s

Profile Headloss

Average End Depth Over Rise

Normal Depth Over Rise

Downstream Velocity

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 4.12
 ft

 Critical Depth
 4.11
 ft

 Channel Slope
 0.00500
 ft/ft

 Critical Slope
 0.00501
 ft/ft

Friction Method Manning Formula Solve For Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.00500	ft/ft
Diameter	1.50	ft
Discharge	5.00	ft³/s
Reculte		

Results

Normal Depth		0.90	ft
Flow Area		1.11	ft²
Wetted Perimeter		2.66	ft
Hydraulic Radius		0.42	ft
Top Width		1.47	ft
Critical Depth		0.86	ft
Percent Full		60.1	%
Critical Slope		0.00578	ft/ft
Velocity		4.51	ft/s
Velocity Head		0.32	ft
Specific Energy		1.22	ft
Froude Number		0.91	
Maximum Discharge		7.99	ft³/s
Discharge Full		7.43	ft³/s
Slope Full		0.00227	ft/ft
Flow Type	SubCritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	60.08	%
Downstream Velocity	Infinity	ft/s

Infinity	ft/s
0.90	ft
0.86	ft
0.00500	ft/ft
0.00578	ft/ft
	0.90 0.86 0.00500

			T 11777/8/8 444
Project Description			
Friction Method	Manning Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.01000	ft/ft
Diameter		1.50	ft
Discharge		8.00	ft³/s
Results			
Normal Depth		0.98	ft
Flow Area		1.22	ft²
Wetted Perimeter		2.82	ft
Hydraulic Radius		0.43	ft
Top Width		1.43	ft
Critical Depth		1.10	ft
Percent Full		65.3	%
Critical Slope		0.00743	ft/ft
Velocity		6.54	ft/s
Velocity Head		0.67	ft
Specific Energy		1.64	ft
Froude Number		1.25	
Maximum Discharge		11.30	ft³/s
Discharge Full		10.50	ft³/s
Slope Full		0.00580	ft/ft
Flow Type	SuperCritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft
Average End Depth Over Rise		0.00	%
Normal Depth Over Rise		65.32	%
Davis Assess Malas Ma		1 6.9	

Infinity ft/s

Downstream Velocity

........

Upstream Velocity	Infinity	ft/s
Normal Depth	0.98	ft
Critical Depth	1.10	ft
Channel Slope	0.01000	ft/ft
Critical Slope	0.00743	ft/ft

	Worksheet	for PIF	E 23	
Project Description				
Friction Method	Manning Formula			
Solve For	Normal Depth			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.00500	ft/ft	
Diameter		5.50	ft	
Discharge		223.00	ft³/s	
Results				
Normal Depth		4.23	ft	
Flow Area		19.63	ft²	
Wetted Perimeter		11.78	ft	
Hydraulic Radius		1.67	ft	
Top Width		4.63	ft	
Critical Depth		4.18	ft	
Percent Full		77.0	%	
Critical Slope		0.00515	ft/ft	
Velocity		11.36	ft/s	
Velocity Head		2.01	ft	
Specific Energy		6.24	ft	
Froude Number		0.97		
Maximum Discharge		255.42	ft³/s	
Discharge Full		237.44	ft³/s	
Slope Full		0.00441	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.00	ft	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.00	ft	
Profile Description				
Profile Headloss		0.00	ft	
Average End Depth Over Rise		0.00	%	

76.99 %

Infinity ft/s

Normal Depth Over Rise

.

Downstream Velocity

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 4.23
 ft

 Critical Depth
 4.18
 ft

 Channel Slope
 0.00500
 ft/ft

 Critical Slope
 0.00515
 ft/ft

Project	Description	

Friction Method Manning Formula Solve For Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01000	ft/ft
Diameter	2.00	ft
Discharge	8.00	ft³/s

Results

Normal Depth		0.82	ft
Flow Area		1.22	ft²
Wetted Perimeter		2.78	ft
Hydraulic Radius		0.44	ft
Top Width		1.97	ft
Critical Depth		1.01	ft
Percent Full		41.1	%
Critical Slope		0.00489	ft/ft
Velocity		6.58	ft/s
Velocity Head		0.67	ft
Specific Energy		1.49	ft
Froude Number		1.48	
Maximum Discharge		24.33	ft³/s
Discharge Full		22.62	ft³/s
Slope Full		0.00125	ft/ft
Flow Type	SuperCritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Stens	n	

0.00	ft
0.00	ft
0.00	%
41.07	%
Infinity	ft/s
	0.00 0.00 41.07

GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 0.82
 ft

 Critical Depth
 1.01
 ft

 Channel Slope
 0.01000
 ft/ft

 Critical Slope
 0.00489
 ft/ft

Project Description	

Friction Method Manning Formula Solve For Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01000	ft/ft
Diameter	2.00	ft
Discharge	15.00	ft³/s

Results

Results			
Normal Depth		1.19	ft
Flow Area		1.95	ft²
Wetted Perimeter		3.52	ft
Hydraulic Radius		0.55	ft
Top Width		1.96	ft
Critical Depth		1.40	ft
Percent Full		59.5	%
Critical Slope		0.00632	ft/ft
Velocity		7.70	ft/s
Velocity Head		0.92	ft
Specific Energy		2.11	ft
Froude Number		1.36	
Maximum Discharge		24.33	ft³/s
Discharge Full		22.62	ft³/s
Slope Full		0.00440	ft/ft
Flow Type	SuperCritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	59.50	%
Downstream Velocity	Infinity	ft/s

GVF Output Data

Upstream Velocity Infinity ft/s Normal Depth 1.19 ft Critical Depth 1.40 ft Channel Slope 0.01000 ft/ft Critical Slope 0.00632 ft/ft

Project Description	
Friction Method	Manning Formula

Solve For Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01000	ft/ft
Diameter	2.00	ft
Discharge	17.00	ft³/s

Results

Normal Depth		1.29	ft
Flow Area		2.15	ft²
Wetted Perimeter		3.74	ft
Hydraulic Radius	,	0.58	ft
Top Width		1.91	ft
Critical Depth		1.49	ft
Percent Full		64.7	%
Critical Slope		0.00694	ft/ft
Velocity		7.91	ft/s
Velocity Head		0.97	ft
Specific Energy		2.27	ft
Froude Number		1.31	
Maximum Discharge		24.33	ft³/s
Discharge Full		22.62	ft³/s
Slope Full		0.00565	ft/ft
Flow Type	SuperCritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	64.69	%
Downstream Velocity	Infinity	ft/s

GVF Output Data

Upstream Velocity Infinity ft/s Normal Depth 1.29 ft Critical Depth 1.49 ft Channel Slope 0.01000 ft/ft Critical Slope 0.00694 ft/ft

	Workshee	t for PIP	E 27
Project Description			
Friction Method	Manning Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.00500	ft/ft
Diameter		3.00	ft
Discharge		24.00	ft³/s
Results			
Normal Depth		1.52	ft
Flow Area		3.58	ft²
Wetted Perimeter		4.74	ft
Hydraulic Radius		0.76	ft
Top Width		3.00	ft
Critical Depth		1.58	ft
Percent Full		50.5	%
Critical Slope		0.00436	ft/ft
Velocity		6.70	ft/s
Velocity Head		0.70	ft
Specific Energy		2.21	ft
Froude Number		1.08	
Maximum Discharge		50.73	ft³/s
Discharge Full		47.16	ft³/s
Slope Full		0.00129	ft/ft
Flow Type	SuperCritical		
GVF Input Data			
Downstream Depth		0.00	ft
Length			ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.00	ft
Profile Description			
Profile Headloss		0.00	ft

0.00 % 50.53 %

Infinity ft/s

....

Average End Depth Over Rise

Normal Depth Over Rise Downstream Velocity

Upstream Velocity	Infinity	ft/s
Normal Depth	1.52	ft
Critical Depth	1.58	ft
Channel Slope	0.00500	ft/ft
Critical Slope	0.00436	ft/ft

Project Description	
Friction Method	Manning Formula

Solve For Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01000	ft/ft
Diameter	3.00	ft
Discharge	39.00	ft³/s

Results

results			
Normal Depth		1.65	ft
Flow Area		3.98	ft²
Wetted Perimeter		5.01	ft
Hydraulic Radius		0.79	ft
Top Width		2.99	ft
Critical Depth		2.03	ft
Percent Full		54.9	%
Critical Slope	ı	0.00532	ft/ft
Velocity		9.80	ft/s
Velocity Head		1.49	ft
Specific Energy		3.14	ft
Froude Number		1.50	
Maximum Discharge		71.74	ft³/s
Discharge Full		66.69	ft³/s
Slope Full	(0.00342	ft/ft
Flow Type	SuperCritical		

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	54.94	%
Downstream Velocity	Infinity	ft/s

Infinity	ft/s
1.65	ft
2.03	ft
0.01000	ft/ft
0.00532	ft/ft
	1.65 2.03 0.01000

2.37 ft

Project Description	
Friction Method	Manning Formula

Input Data

Solve For

Roughness Coefficient	0.013	
Channel Slope	0.01500	ft/ft
Diameter	3.00	ft
Discharge	79.00	ft³/s

Normal Depth

Results

Normal Depth

Flow Area	6.00	ft²
Wetted Perimeter	6.58	ft
Hydraulic Radius	0.91	ft
Top Width	2.44	ft
Critical Depth	2.76	ft
Percent Full	79.2	%
Critical Slope	0.01218	ft/ft
Velocity	13.17	ft/s
Velocity Head	2.69	ft
Specific Energy	5.07	ft
Froude Number	1.48	
Maximum Discharge	87.87	ft³/s
Discharge Full	81.68	ft³/s
Slope Full	0.01403	ft/ft

GVF Input Data

Flow Type

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

SuperCritical

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	79.15	%
Downstream Velocity	Infinity	ft/s

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	2.37	ft
Critical Depth	2.76	ft
Channel Slope	0.01500	ft/ft
Critical Slope	0.01218	ft/ft

CHANNEL IMPROVEMENTS



Cathy Tessin

From:

Chris Jorgensen <CJorgensen@laplatallc.com>

Sent:

Friday, October 19, 2018 8:45 AM

To:

Steve Rossoll; Kyle Campbell; Cathy Tessin; P. E. Richard Wray - Kiowa Engineering

Cc:

Corporation (rwray@kiowaengineering.com) Tom Taylor; Douglas Reinelt; Mitchell, Timothy

Subject:

The Farm Channel Embankments Proposed Schedule

Attachments:

20181019082436.pdf

Αli

Here is what I am showing for my development forecast. As I understand, we owe improvements as we build stuff. We seem to have everything going at the same time!

Please see the attached exhibit for embankment name correlation. Please back in the proper design start dates, and provide topo so we can get going. The geotech reports are almost done.

BSC Embankment 6 (Orange) – Start construction in November 2018

BSC Embankment 4 (Yellow) -- Start construction in February 2019

Middle Creek Embankment and Associated Drop Structures – Start construction in April 2019

BSC Embankment 5 and associated Bank Stabilization (Red) - Start construction in June 2019

BSC Embankment 2 (Purple) – Start construction in August 2019

BSC Embankment 1 (Purple) – Start construction in September 2019

BSC Filing 7 Bank Stabilization (Blue) – Start construction in March 2020

Please let me know if you have questions.

Thanks, Chris

Chris Jorgensen, PE (CO,UT)

Project Manager

COMMUNITIES 1755 Telstar Drive, Suite 211 Colorado Springs, CO 80920

Cell: Fax: 801.673.0193 719.260.7088

EXISITNG CONDITIONS





Squirrel Creek channel improvements due to permitting requirements from the Core of Engineers and Fish and Wildlife. If channel improvements have not been started when this detention facility is required, a temporary private detention pond will be provided at that time. Upon construction of the permanent detention facility (BS-1) the temporary detention facility will be removed.

BLACK SQUIRREL – 2 DRAINAGE BASIN 🥮

Basin BS-2A (Q_5 = 17.72 cfs, Q_{100} = 33.20 cfs) is 6.9 acres and consists of building, landscaping, a portion of the Federal Drive extension and parking lot flows. Runoff from this basin will sheet flow across the proposed parking lot and drives and travel as sheet flow and curb and gutter flow into the proposed storm sewer system to Design Point 35 (Q_5 = 85.55 cfs, Q_{100} = 158.06 cfs) combining with flows from Basins BS-2B and BS-2C. At this point, where a 60" RCP pipe Conveyance 31) will accept both the 5-yr. and 100-yr. developed flows and convey them to Design Point 36/ Pond BS-2.

Basin BS-2B (Q_5 = 37.35 cfs, Q_{100} = 68.43 cfs) is 13.7 acres and consists of future building, landscaping and parking lot flows. Runoff from this basin will sheet flow across the parking lot and drives and travel as sheet flow and curb and gutter flow into the storm sewer system to point, where a 42" RCP pipe (Conveyance 30) will accept both the 5-yr. and 100-year developed flows conveying them to Design Point 35.

Basin BS-2C (Q_5 = 30.92 cfs, Q_{100} = 56.77 cfs) is 11.4 acres and consists of future building, landscaping and parking lot flows. Runoff from this basin will sheet flow across the parking lot and drives and travel as sheet flow and curb and gutter flow into the storm sewer system to Design Point 35.

Basin BS-2D (Q_5 = 4.63 cfs, Q_{100} = 8.49 cfs) is 1.7 acres and is the area for Detention Pond BS-2. Runoff from this basin will flow to Design Point 36/ Pond BS-2 (Q_5 = 90.18 cfs, Q_{100} = 166.54 cfs).

Basin BS-2E (Q_5 = 0.44 cfs, Q_{100} = 2.81 cfs) is 1.8 acres in area is a portion of the basin that will not be landscaped and will bypass Detention Pond BS-2. Runoff from this basin will drain to Design Point 13.



Design Point 36 (Q_5 = 90.18 cfs, Q_{100} = 166.54 cfs), is the inflow into Private Detention Pond BS-2 and Design Point 13 represents the restricted released flows. The allowable flow for Design Point 13 (Q_5 = 5.83 cfs, Q_{100} = 43.98 cfs) (based upon the historic flow from an equal area of land draining to Design Point 13 in the developed condition). This pond has been modeled to release flows which are close to the allowable rates (Q_{100} = 42.40 cfs). However, final pond design and appropriate outlet structure will be specified at the time of known site development within a specific final drainage report.

BLACK SQUIRREL – 3 DRAINAGE BASIN

Basin BS-3A (Q_5 = 24.83 cfs, Q_{100} = 45.54 cfs) is 9.1 acres and consists of building, landscaping and parking lot flows. Runoff from this basin will sheet flow across the parking lot and drives and travel as sheet flow and curb and gutter flow into the storm sewer system to a point, where a 36" RCP pipe (Conveyance 35) will route the flows to Design Point 41.

Basin BS-3B (Q_5 = 37.10 cfs, Q_{100} = 71.98 cfs) is 15.2 acres and consists of future building, roadway, landscaping and parking lot flows. Runoff from this basin will sheet flow across the parking lot and drives and travel as sheet flow and curb and gutter flow into the storm sewer system to Design Point 41 (Q_5 = 61.45 cfs, Q_{100} = 117.03 cfs), where a 48" RCP pipe (Conveyance 36) will convey the developed flows to Design Point 42.

Basin BS-3C (Q_5 = 40.58 cfs, Q_{100} = 74.48 cfs) is 14.9 acres and consists of future building, landscaping and parking lot flows. Runoff from this basin will sheet flow across the parking lot and drives and travel as sheet flow and curb and gutter flow into the storm sewer system to Design Point 42 (Q_5 = 100.66 cfs, Q_{100} = 183.49 cfs), where a 60" RCP pipe (Conveyance 37) will convey the flows to Design Point 43/ Pond BS-3.

Basin BS-3D (Q_5 = 54.90 cfs, Q_{100} = 101.33 cfs) is 20.4 acres and consists of future building, landscaping and parking lot flows. Runoff from this basin will sheet flow across the parking lot and drives and travel as sheet flow and curb and gutter flow into the storm sewer system to Design Point 43/ Pond BS-3.



Basin BS-3E (Q_5 = 34.63 cfs, Q_{100} = 63.98 cfs) is 12.9 acres and consists of future building, landscaping and parking lot flows. Runoff from this basin will sheet flow across the parking lot and drives and travel as sheet flow and curb and gutter flow into the storm sewer system to a point, where a 42" RCP pipe (Conveyance 38) will accept both the 5-yr. and 100-yr. developed flows and route to Design Point 43/ Pond BS-3.

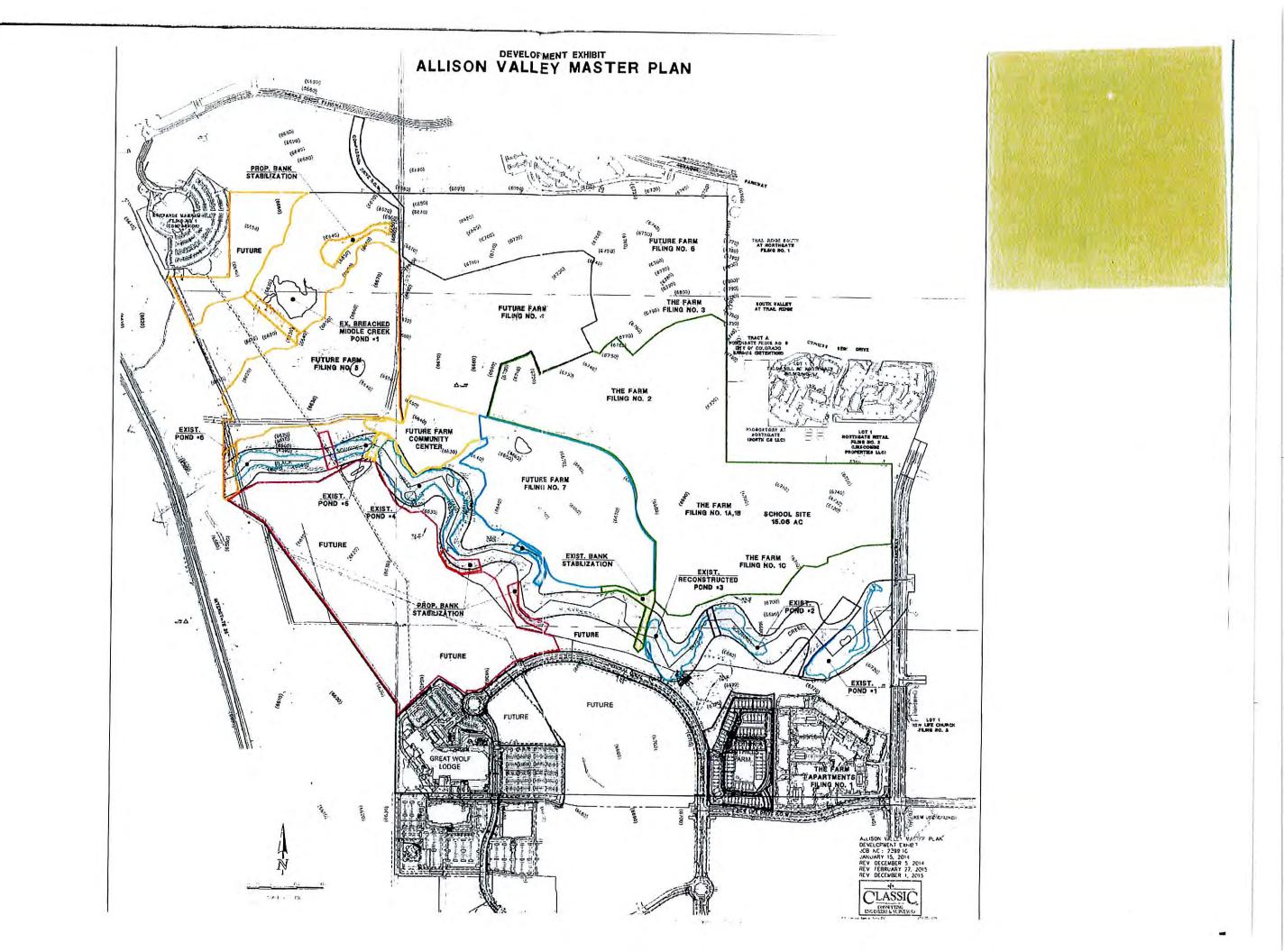
<u>Basin BS-3F</u> (Q_5 = 10.61 cfs, Q_{100} = 19.48 cfs) is 3.9 acres and is the area for Detention Pond BS-3. Runoff from this basin will flow to Design Point 43 (Q_5 = 197.70 cfs, Q_{100} = 366.68 cfs).

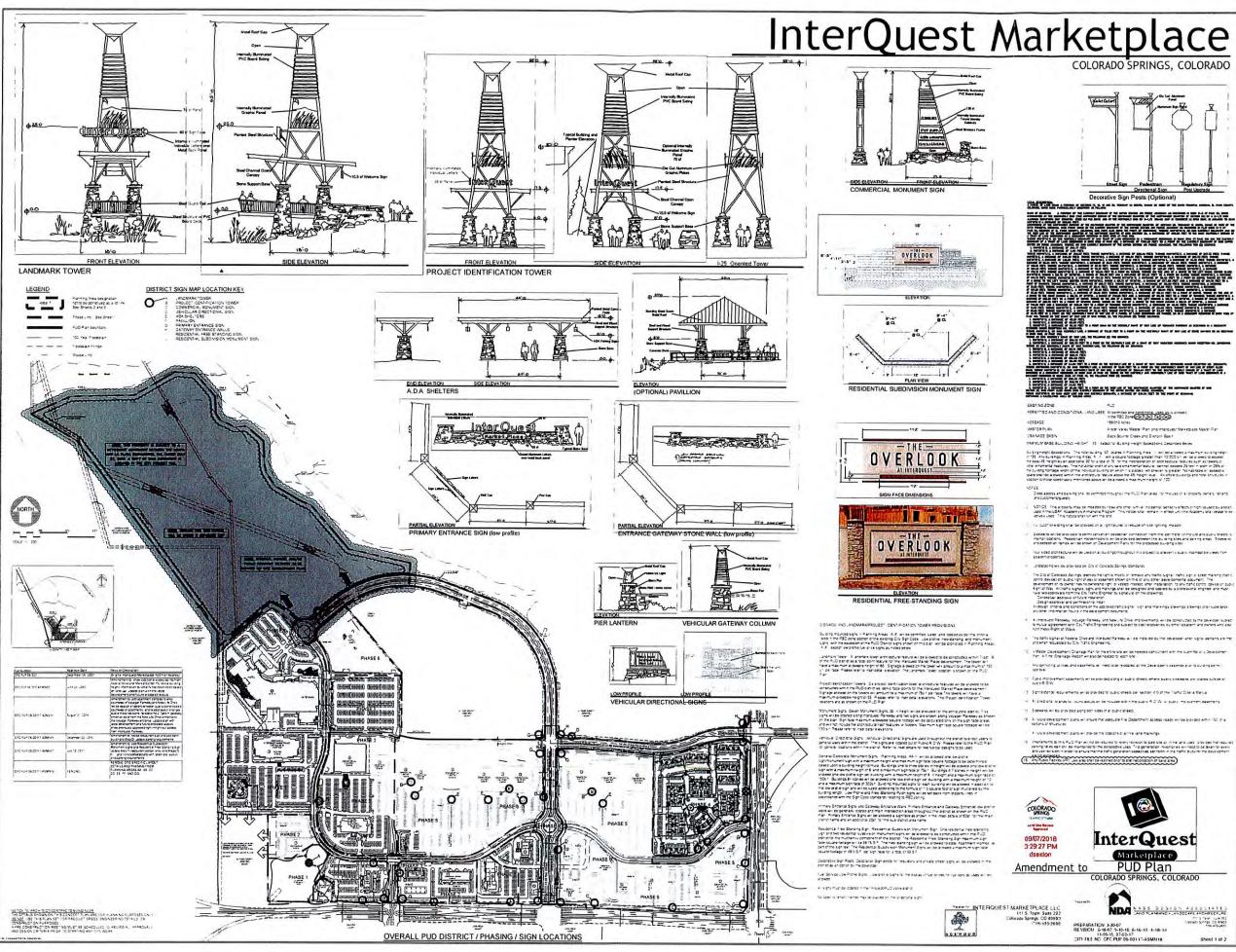
Basin BS-3G (Q_5 = 13.91 cfs, Q_{100} = 26.23 cfs) is 5.6 acres in area is a portion of the basin that will not be developed and will bypass Detention Pond BS-3. Runoff from this basin will drain to Design Point 14.

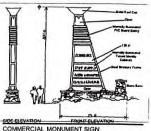
Design Point 43 (Q_5 = 197.70 cfs, Q_{100} = 366.68 cfs) is the inflow into Private Detention Pond BS-3 and DP-14 represents the restricted pond release. The allowable flow for Design Point 14 (Q_5 = 11.06 cfs, Q_{100} = 84.58 cfs) (based upon the historic flow from an equal area of land draining to Design Point 13 in the developed condition). This pond has been modeled to release flows which are close to the allowable rates (Q_{100} = 83.77 cfs). However, final pond design and appropriate outlet structure will be specified at the time of known site development within a specific final drainage report. See "Final Design Report for Allison Valley On-Site Reaches of Black Squirrel Creek and Middle Tributary Creek Channel Improvements," by Classic Consulting, June 2007 for creek/channel improvement specifics.

INTERIM CONDITIONS - Filing Nos. 1 & 2 (see "Interim Conditions Drainage Map)

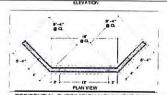
The purpose of this analysis is to prove adequate release rates using the SCS drainage analysis method at the main overall basin outfalls across Interstate 25 with the development of the first phase of construction (Filing No. 1 & 2).







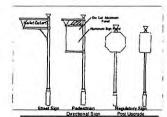








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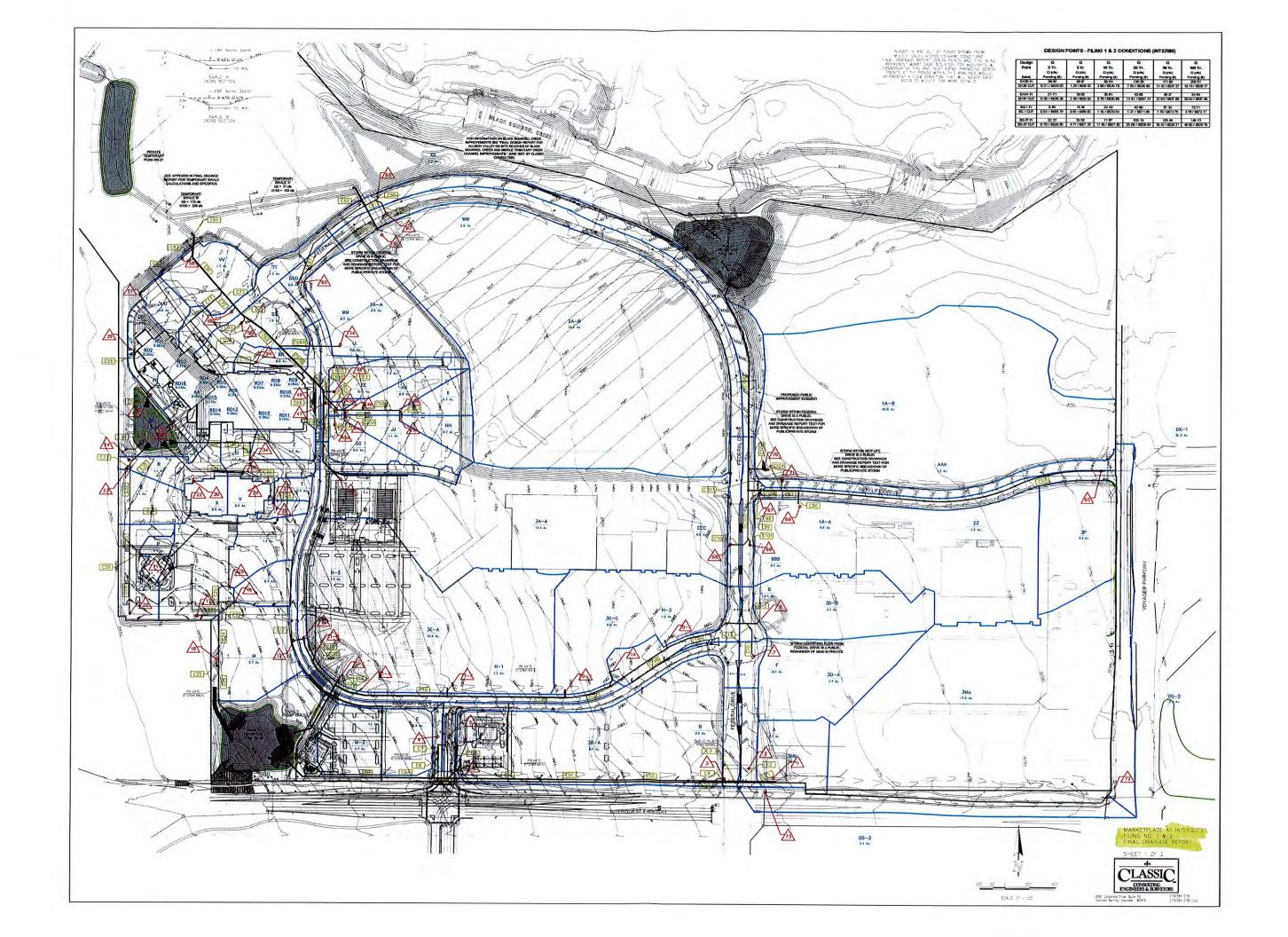


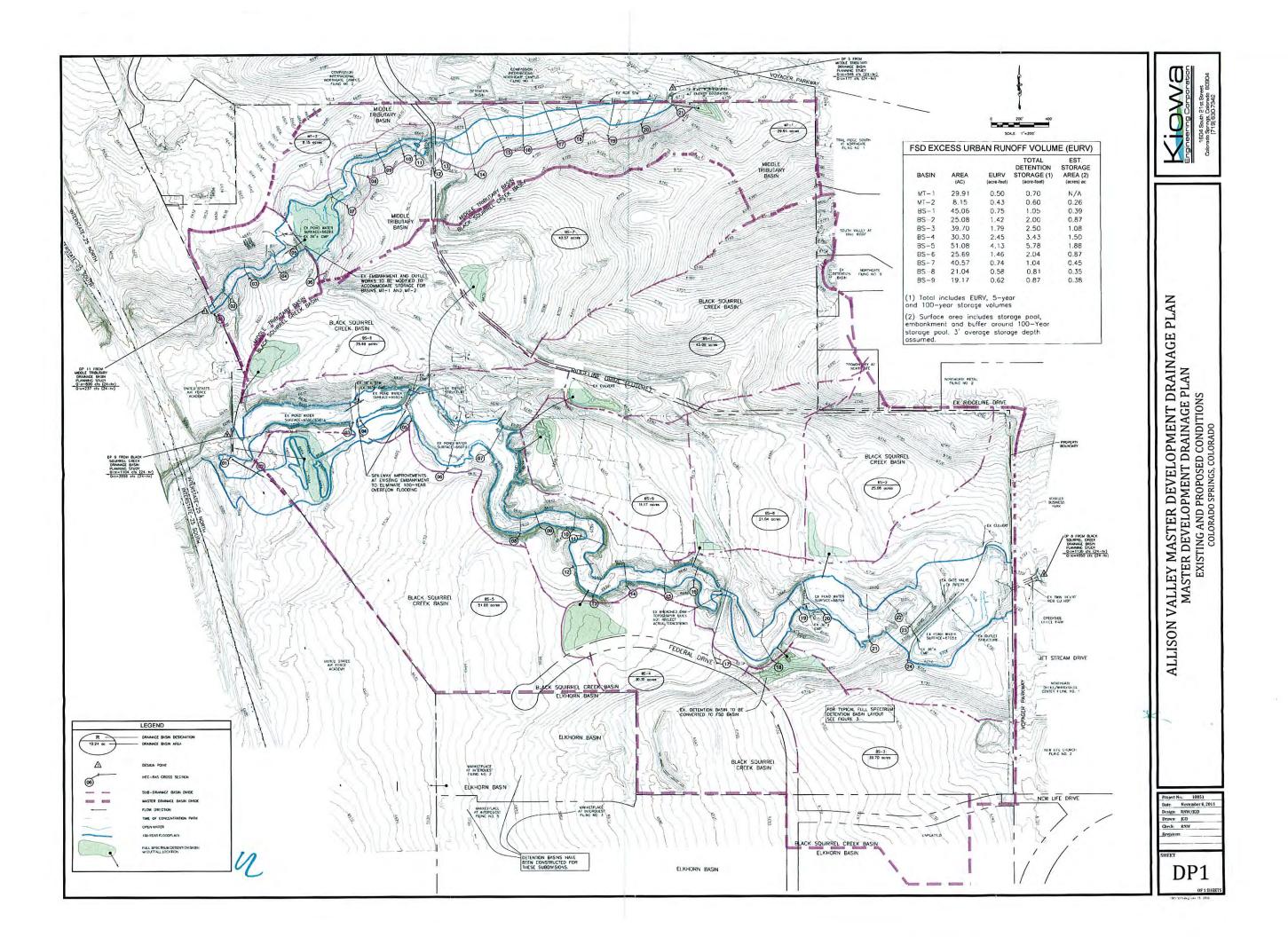


Amendment to



PREPARATION 3-30-07
REVISION 5-18-07, 5-10-10, 6-16-10, 4-18-14
11-09-15, 07-03-17
CITY FRE NO. CPC PUP 06-001-17-A5MN18





DRAINAGE MAP DEVELOPED CONDITIONS



KNOW ALL MEN BY THESE PRESENTS:

THAT ALLISON VALLEY DEVELOPMENT COMPANY, LLC, A COLORADO LIMITED LIABILITY COMPANY AND GINGER I, LLC, A COLORADO LIMITED LIABILITY COMPANY, BEING THE DIRECTS OF THE PROCESS OF THE PROLITY OF THE DIRECTS OF THE DIRECTS OF THE PROLITY OF THE PROCESS OF THE PROCES

LEGAL DESCRIPTION:

A PARCEL OF LAND BEING PORTIONS OF SCCHOOLS 17, 18, 19 AND 20, TOWNSHIP 12 SOUTH, RANGE 66 WEST OF THE SIXTH PRINCIPAL MERIDIAN, EL PASO COUNTY, COLORADO, BEING MORE PARTICULANTY DESCRIBED AS FOLLOWS:

BASS OF BLARNIGS. A PORTION OF THE MORTHERLY BOUNDARY OF LOT 1 AS PLATED IN MANIETH-UCS AT MITISALIST FILING NO. 2 PRODUCED UNDER RECEPTION HOLD AND AN ADMINISTRATION OF THE PROPERTY OF THE PORTION OF THE PROPERTY OF THE PROPERTY OF THE PORTION OF THE PORTION OF THE PROPERTY AND THE PROPERTY OF THE PORTION OF THE PORTIO

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THENCE ON 1934'400"E. A DISTANCE OF 82-48 FEET TO A POINT OF CURVE.

TREME ON THE ARC OF A CURVE TO THE ROUT MANING A BELLAT OF 7872221", A RADUS OF 285.00 FET AND A DISTANCE OF 186.80 FET TO A POINT OF TANGENT PROPERTY ROUTE OF 186.80 FET TO A POINT OF TANGENT ON THE PROPERTY ROUTE OF 451.75 FET TO A POINT ON DURNE, SAD POINT GENE ON THE MORTHERITY ROUTE OF 451.75 FET TO A POINT AS PLATTED IN SAID MARKETPLACE. THE TOWN OF THE MINISTER OF THE PROPERTY ROUTE OF

THENCE ON SAID NORTHERLY RIGHT OF WAY LINE, THE FOLLOWING (5) FIVE COURSES:

- ON THE ARC OF A CURVE TO THE LEFT WHOSE CONTER BEAMS \$2250727°C. HANNING A DULL OF DOOR DAY, A RANNING OF SACIO FIELD AND A DISTANCE OF 5.00 FIELD;

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THÉNCE ON THE NORTHERLY BOUNDARY OF SAID LOT 1, THE FOLLOWING (3) THREE COURSES:

- ON THE ARC OF A CUPNE TO THE LIFT WHIDE CENTER BEARS 3473/35"R; HAWRIG A DELTA OF ZYDOZET, A RAMUS OF HELDO FEET AND A DOTANCE OF 1818/5 FEET TO A CO. THE ARC OF A CUPRE TO THE ROBET HAWRIG A DELTA OF 1819/18", A RABBUS OF 777.00 FEET AND A DISTANCE OF 55.52 FEET TO A POINT ON CURNEY S. SUPPRIGENT, A DISTANCE OF MOUS FEET TO THE POINT OF RECENTING.

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DEDICATION:

DEDICATION:

THE UNDERSORED DINNERS HAVE CAUSED SALD TRACT OF LIMB TO BE PLATTED INTO A LOT, A STRICE, TRACTS AND EXSENSITY, AS SHOWN ON THE PLAT. THE UNDERSORED DOES HIRREST TO A SHOWN OF THE PLAT. THE UNDERSORED DOES HIRREST TO A LOT, A L

FOOTHILLS FARM CAMPUS FILING NO. 2

a portion of sections 17, 18, 19 and 20, township 12 south, range 66 west of the sixth principal meridian, city of Colorado springs, el paso county, colorado

	OHNER.
ALLISON VALLEY DEVELOPMENT COMPANY, LLC, A COLORADO LIMITED LIABILITY COMPANY HAS EXECUTED THIS INSTRUMENT THE	GINGER I, LLC, A COLORADO LIMITED LIABILITY COMPANY HAS EXECUTED THIS INSTRUMENT THE DAY OF
BY: ALLEON VALLEY DEVELOPMENT COMPANY, LLC, A COLORADO LIMITED LIABILITY COMPANY BY: LA PLATA COMMUNITES, INC., A COLORADO CORPORATION, MANAGER B. OCUCIAS CUMBY, PRESIDENT AND CED	BY: CHOCK I, LLC, A COLORADO LIMITED LIABILITY COMPANY
BY: ALISTH VALLEY DEVELOPMENT COMPANY, ILIC, A COLDRADO LIMITED LIABILITY COMPANY BY: LA PLATA COMMUNITES, INC., A COLDRADO CORPORATION, MANAGER DENISE WALLAZE, SECRETARY	
STATE OF COLORADO)	STATE OF COLORADO)
CDUNTY OF EL PASO	COUNTY OF EL PASO
THE FORECOING INSTRUMENT WAS ADDINONALDOED BEFORE ME THIS DAY OF	THE FORECOING INSTRUMENT WAS ACCHONIZED BEFORE ME THIS DAY OF 20 A.D., BY OF GMOER I, LLC A COLORADO LIMITED LIABILITY COMPANY.
WITHESS MY HAND AND OFFICIAL SEAL.	WITHESS MY HAND AND OFFICIAL SEAL
MY COMMISSION EXPRESS	MY COMMISSION EXPIRES: MOTARY PUBLIC
LIEN HOLDER:	
CHOCK I, LLC, A COLORADO LIMITED LIABILITY COMPANY HAS EXECUTED THIS	

GENERAL NOTES:

NOTARY PUBLIC

1. THE DATE OF PREPARATION IS JANUARY 28, 2019.

WITHESS MY HAND AND OFFICIAL SCAL

MY COMMISSION EXPIRES:

AS:

OF GHIGER I, LLC, A COLDRADO LIMITED LIABILITY COMPANY

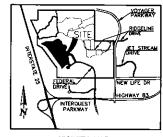
STATE OF _____

- PORTIONS OF TRACTS A AND B ARC INCLIDED IN THE ALLISON VALLEY METROPOLITAN DISTRICT NO. 1 PER FINDINGS AND DECREE RECORDED LINDER RECEIPTION NO. 20617852Z. AND AS AMERICA.
- PORTIONS OF TRACTS A AMO B ARE INCLUDED. IN THE ALLISON VALLEY METROPOLITAN DISTRICT NO. 2 PER FINDINGS AND DISTRICT NO. 2 PER FINDINGS AND ASSAULDED.
- TRACT A IS FOR PUBLIC IMPROVEMENTS, PUBLIC UTLITTES AND ANY OTHER PUBLIC USE THE CITY DEEMS APPROPRIATE. TO BE OWNED AND MAINTAINED BY THE CITY OF COLORADO SPRINGS.
- RAC'S S' FOR PUBLIC UTILITES, PUBLIC IMPROVEMENTS, USAFA EMERGNET LANGUAG MELA, ORAMAGI, LANGGAPE, RIVALIS AND TO SE OWNER APPROVANT, TO SE OWNER AND AN EMPLOYMENT OF THE CONTROL OF THE
- TRACT C IS FOR FUTURE DEVELOPMENT TO BE OWNED AND MAINTAINED BY THE OWNER OF LOT 1.
- B. MOTHER: THIS PROPERTY MAY BE IMPACIED BY MOSE AND OTHER SMILLS SOURCE OFFICING OF FLIGHT BY ARRENATY USED IN THE SMILLS SOURCE SHALL RESAM IN DIFFECT MAIN. THE ARR FORCE ACADEMY SHALL RESAM IN DIFFECT MAIN. THE ARR FORCE ACADEMY SHALL CLASS TO BE USED FOR FLIGHT TRAINING PROPERTY IN SIGN MOTHER SHALL RUN WITH THE LUNG.
- 9. ANY PERSON WHO KNOWINGLY REMOVES, ALTERS OR DEFACES
 ANY PUBLIC LAND SURVEY MONIMENT OR LAND MOMEMENT OF ACCESSORY, COMMETS A CLASS TWO (2) MISDEMEANDR PURSUANT TO STATE STATUE 18-4-508, C.R.S.
- THE ADDRESSES () EIGHEFTED ON THIS PLAT ARE FOR INFORMATIONAL PURPOSES DRLY, THEY ARE NOT THE LEGA DESCRIPTION AND ARE SUBJECT TO CHANGE.
- 11. AL CASDADATS DESCRIPTION FOR FURBLE UTILITY
 PROPERTY AND CONTRACTOR OF THE PROPERTY OF THE

GENERAL HOTES (CONTO):

- BE AFFECTED AND SHALL REMAIN IN FULL FORCE AND EFFECT.
- 12. THE FLAT OCES NOT CONSTITUTE A TITLE SEASON TO CYTEMACE OWNERSHIP OF EASTBORN TO RECORD. FOR ALL WORDSHIPD GEARDING EASTBORN, ROOM-TOF-MAY AND BITLE OF RECORD, CLOSED CONSULTING CHARGES AND SIMPORT OF MAY AND BITLE OF RECORD CHARGES AND SIMPORT OF MAY AND THE CONSTITUTE OF THE CONSTITUTE CONS
- 13. THE ALLISON VALLEY METROPOLITAN DISTRICT NO. 1 SHALL MARYTAN ALL IMPROVEMENTS LYNO WITHIN THE MEDIAN AS CONSTRUCTED IN FEDERAL ORNIC AS PLATTED IN MAINCEPLACE AT INTERQUEST FAIRS (ID. 2.)
- 14. ALL PROPERTY WITHIN THIS SUBDIVISION IS SUBJECT TO AN ANGARDN EASE-BEST TO THE UNITED STATES AIR FORCE ACADEMY AS RECORDED UNDER RECEIPTION HO. THE OFFICE OF THE CLERK AND RECORDER OF EL PASO COUNTY, OR DRAID.
- THE PRIVATE STREET, ENT PARKINAY, SHALL BE DIRECT BY THE OWNER OF RECORD AND MAINTAINED BY THE OWNER OF LOT 1, AS PLATTED.
- 18. THIS PROPERTY IS SUBJECT TO THE FINDMENT, SUMMARY, AND CHINALISSISS OF A ECOLOGIC HAZARD REPORT PREFACE BY AND REPORT HAS BEEN FALCED WHITE FIRE CPT OF COLOGICAD SPRINGS DEVLOPMENT DIVISION. CONTROL DEVLOCATION DIVISION. CONTROL DEVLOCATION TESTINGS.
 DEVISION, 30 SOUTH NEWSON AVAILAT, SURT SO DUISMAND SPRINGS, OF YOU WOULD LIKE TO BREMENT SOM REPORT.
- 17. THE RESTRICTED USE AREA AS SHOWN WITHIN TRACT B IS LIMITED TO CRISTING USES, USAFA USE, PUBLIC TRAILS, TEMPORARY GRADING AND MOUSE HABITAT MITIGATION.

PRELIMINARY THIS DOCUMENT HAS NOT BEEN PLAT CHECKED



VICINITY MAP

NOTICE IS HEREBY GIVEN:

THAT THE AREA INCLUDED IN THE PLAT DESCRIBED HEREIN IS SUBJECT TO THE CODE OF THE CITY OF COLORADO SPRINGS, 2001, AS AMENDED.

NO BULDEN CREMITS SHALL BE ISSUED FOR BULDING STISS WITHIN THIS PLAT UNTO ALL REQUIRED PARTS INFORMATION FOR STISS WITHIN THIS PLAT UNTO ALL REQUIRED PARTS INFORMATION FAMILY BEING ACCEPTABLE OF THE PART OF THE PART OF THE PARTS INFORMATION FOR STISS INFORMATION FOR STIPS INFORMATION FOR STISS INFORMATION FOR STIPS INFORMATION F

FASTMENTS

AS SHOWN HEREON WITH SURFACE MAINTENANCE THE RESPONSIBILITY OF THE INDIVIDUAL LANDOWNER.

SURVEYOR'S STATEMENT

THE UNDERSONED PROFESSIONAL LAND SURVEYOR LICENSED IN THE STATE OF COLORADO, HORSELY STATES AND OFFICIALISTS THAT THE ACCOUNT OFFICE OF A SHORE THE GOOD AND AND A SHORE THE COLORADO AND AND A SHORE THE COLORADO AND AND AND AND THAT THE FELLOMEDIANTS OF THE 280 OF THE COLORADO AND SECTION, AS AMODOED, MAN ESEE THAT LIST OF THE COLORADO AND SECTION AS AMODOED, AND ASSESSION A

DOLIGLAS P. REINELT, PROFESSIONAL LAND SURVEYOR	DATE
COLORADO P.L.S. NO. 30118	
FOR AMD ON BEHALF OF CLASSIC CONSULTING	
FUCHAFFEE AND MIGHTHERE II O	

MOTICE

ACCORDING TO COLORADO LAW YOU MUST COMMEMOE ANY LEGAL ACTION BASED LIPON ANY DEFECT IN THIS SURVEY WITHIN THREE YEARS AFTER YOU PREST DESCOVER SUCH DEFECT. IN ON EVENT, MAY ACTION BESTED LIPON ANY DEFECT IN THIS SURVEY BE COMMEMICED MORE THAN YET YEARS FROM THE DATE OF THE CERTIFICATION SHOWN HERDOW.

CITY APPROVAL:

ON BEHALF OF THE CITY OF COLORADO SPRINGS, THE UNDERSIGNED HOREBY APPRIOVE FOR FIUNG THE ACCOMPANYING PLAT OF "FDOTHILLS FARM CAMPUS STREET OF THE PROPERTY OF

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	COUNTY OF EL PASO)	
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-	AT RECEPTION NO	20 AD., AND IS DULY RECORDED OF THE RECORDS OF EL PASO COUN
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CHUCK BROERMAN, RECORDER

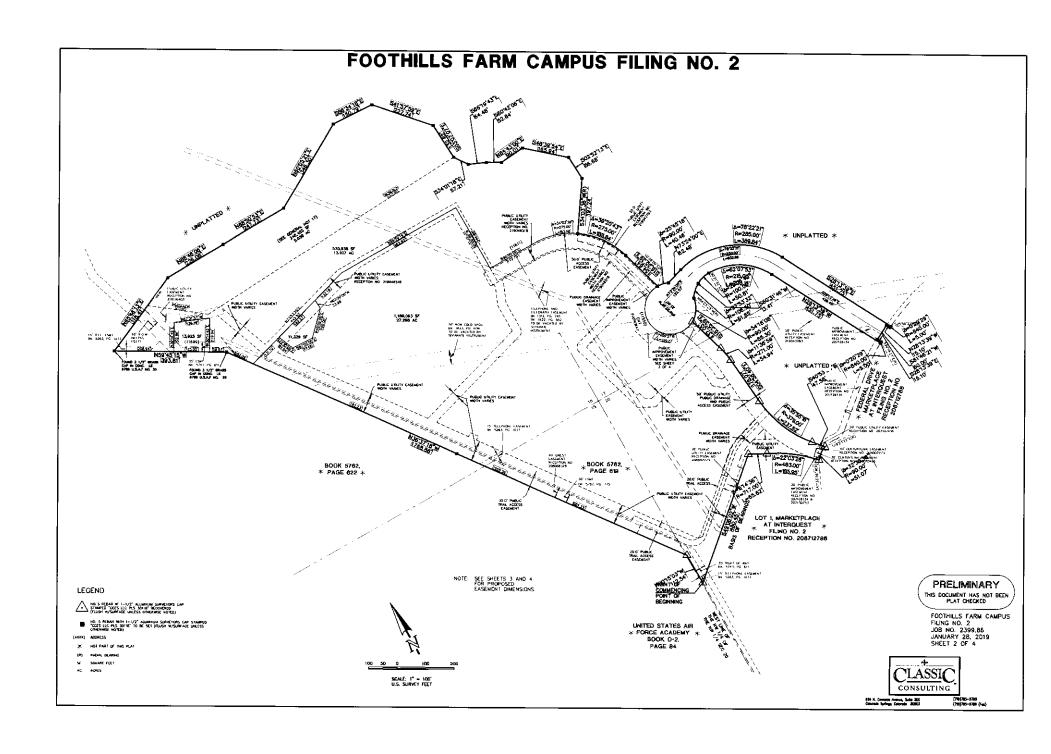
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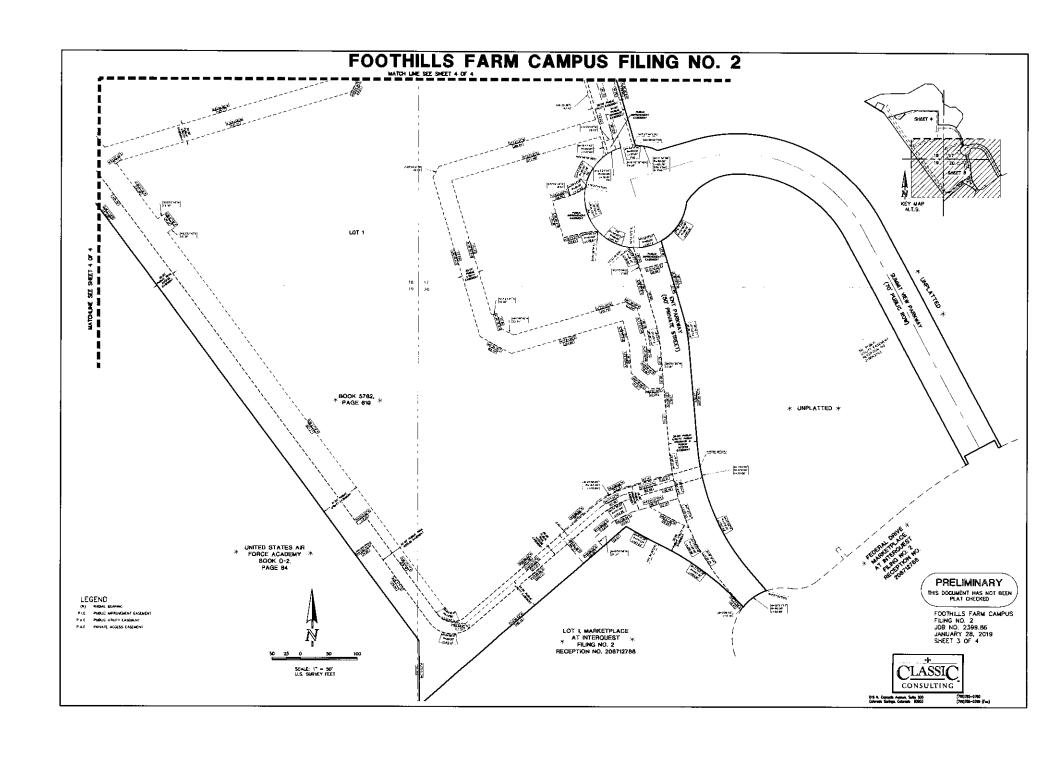
FILING NO. 2 JDB NO. 2399.88 JANUARY 28, 2019 SHEET 1 OF 4 BRIDGE FEES: PARK FEE:

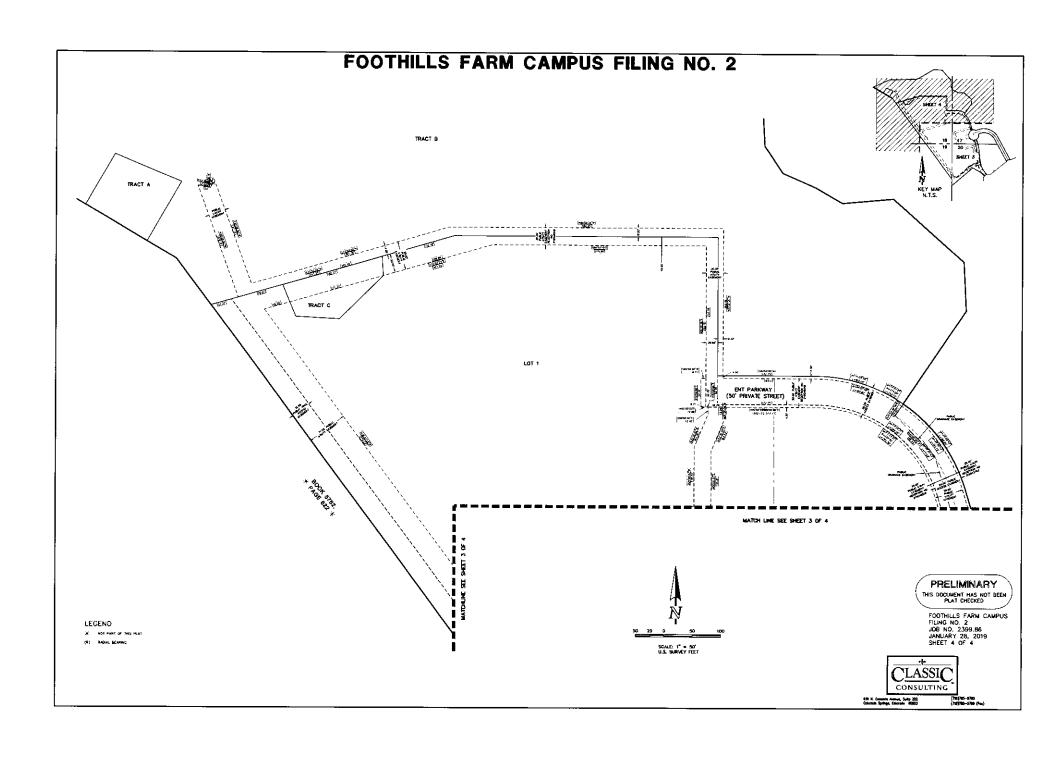


FOOTHILLS FARM CAMPUS

619 M. Councilo Angeles, Suita 200 Calestato Springe, Calestato (ECEC)









June 27, 2019

City of Colorado Springs
Water Resources Engineering Division
30 S. Nevada Avenue, Suite 401
Colorado Springs, CO 80903

ATTN:

Ms. Anna Bergmark

RE:

Foothills Farm Campus Fil. No. 2- Phase 2 Storm Variance Request related to Velocity

Dear Ms. Bergmark:

Classic Consulting Engineers & Surveyors, LLC (CCES), on behalf of our client, Allison Development Company, respectfully requests the City's consideration of the following variance:

1. Maximum velocity in storm sewer pipe -Drainage Criteria Manual Volume 1, (Chapter 9, Section 7.1)

Background:

Foothills Farm Campus Filing No. 2 is a 42.890-acre site located in Sections 17, 18, 19, and 20, Township 12 South, Range 66 West of the Sixth Principal Meridian in the City of Colorado Springs, County of El Paso, State of Colorado. The site is bound on the south by existing Marketplace at Interquest retail development and Federal Drive, to the west by existing USAFA vacant property and Interstate 25, and to the east Black Squirrel Creek. This site includes a platted lot, public street right of way, and tracts to support the proposed Ent Credit Union headquarters office campus development within the previously approved Marketplace at Interquest PUD plan.

The following variance are respectfully requested:

1. Maximum velocity in storm sewer pipe (Chapter 9, Section 7.1) – The maximum velocity is limited to 18 feet per second (fps) for all sewers. However, Appendix 9A section 634.2 allows for additional pipe protection to be used in cases where the velocity exceeds 18 feet per second (fps). Based upon the topography of the site and the design constraints related to pond inlet elevations and upstream pipe crossings, every effort has been made to reduce velocity where possible within the storm pipe. This applies to Pipe 23 Section 4 where the velocity at 19.02 fps. Manufacturer information for this pipe material shows that this pipe has an equivalent strength as Class IV. This data also shows that the proposed Class III RCP also provides the increased abrasion resistance desired for all reaches of storm sewer that exceed 18 feet per second (fps) since the actual concrete compressive strengths exceed the minimum required for RCP Class IV (4000 psi) and RCP Class V (6000 psi). The pipe class required D-load minimum capacity is given in ASTM C 76 or AASHTO M170. Please see attached data sheets for further information. The outfall of the storm pipe system into the pond will be released across appropriate energy dissipation at the concrete impact structure and forebay. The impact structure and forebay will be constructed within the Full Spectrum Detention Facility D in accordance with UDFCD Volume 2.

Justification:

We feel this variance is justified as it meets the criteria of Appendix 9A, Section 634.2 for the Pipe Velocity variance. Based upon this request, the overall design approval will not affect peak flows or water quality in

Page 2; November 16, 2018 Ms. Anna Bergmark Foothills Farm Campus Fil. 2 Phase 2 storm — Velocity Variance

Fountain Creek, as all stormwater will continue to be treated and detained per the approved Final Drainage report.

We respectfully request your favorable consideration of this request.

Respectfully submitted,

Cathy M. Tessin, P.E. Project Manager

Attachment: Vicinity Map

Concrete Pipe testing results



MATERIALS TESTING REPORT

Forterra 9455 Boston Court Henderson, CO 80640 P 303.867.6700 F 303.350.4140

Date of Production: 2-Jan-19
ID Number: Bidi #1 4500 psi

Tester: Derek Coffey Report by: Jose Flores

Test Date:

Batch Time: 11:05

Testing Standard Inf	ormation
Reference:	ASTM C 39
	Compressive Strength of Cylindrical Concrete Specimens Compressive Strength

Sample Information

Description: 4X8 Drycast Cylinder

Product Description: 24 C3 Temp. of Concrete: 46

ary of Results for Compres	sive siter	igin		
			Test Result (psi)	Pass/Fail
Minimum at 28 days (psi):	4500	<	7420	PASS

"Reference" data refers to Section(s) of Standard Reference
Manually Entered Data

Calculated Data

pecimen Information								
Number	1	2	3	4	5	6	7	Reference
Break (days)	1	2	2	7	28	28	28	
d (in)	4.00	4.00	4.00	4.00	4.00	4.00	4.00	9.1.2
A (in ²)	12.57	12.57	12.57	12.57	12.57	12.57	12.57	9.1.3
L _{MAX} (lbs)		50895	47075	68960	85700	98090	96075	9.1.4
CS (psi)	0	4050	3745	5488	6820	7804	7645	9.1.5
Fracture Type (1-6)		4	5	5	5	2	5	9.1.6

where:

d= Diameter

A= Area

L_{MAX}= Maximum Load

CS= Compressive Strength

Fracture Type= Per ASTM C39, Figure 2

A=

 $(p * d^2) / 4$

CS=

L_{MAX}/A



MATERIALS TESTING REPORT

Forterra 9455 Boston Court Henderson, CO 80640 P 303.867.6700 F 303.350.4140

Date of Production: 18-Feb-19 ID Number: Bidi #1 4500 psi Tester: Jose Flores
Report by: Jose Flores Test Date: Batch Time:

Testing Standard Inf	formation
Reference:	ASTM C 39
Name:	Compressive Strength of Cylindrical Concrete Specimens
Test for:	Compressive Strength

Sample Information Description: 4X8 Drycast Cylinder

Product Description: 36 C3 Temp. of Concrete: 44

			Test Result (psi)	Pass/Fail
Minimum at 28 days (psi):	4500	<	6800	PASS

"Reference" data refers to Section(s) of Standard Reference Manually Entered Data

Calculated Data

Number	1	2	3	4	5	6	7	Reference
Break (days)	1	2	7	7	28	28	28	
d (in)	4.00	4.00	4.00	4.00	4.00	4.00	4.00	9.1.2
A (in ²)	12.57	12.57	12.57	12.57	12.57	12.57	12.57	9.1.3
L _{MAX} (lbs)		54980	55255	80520	80975	97125	78105	9.1.4
CS (psi)	0	4375	4395	6405	6445	7727	6215	9.1.5
Fracture Type (1-6)		4	4	5	5	5	5	9.1.6

where:

d= Diameter

A= Area

L_{MAX}= Maximum Load

CS= Compressive Strength

Fracture Type= Per ASTM C39, Figure 2

A= $(p*d^2)/4$

CS= L_{MAX}/A



MATERIALS TESTING REPORT

Forterra 9455 Boston Court Henderson, CO 80640 P 303.867.6700 F 303.350.4140

Date of Production: 6-May-19

ID Number: Bidi #1 4500 psi Tester: Jose Flores

Report by: Jose Flores Test Date:

Batch Time: 10:40 AM

Testing Standard Information

Reference: ASTM C 39

Name: Compressive Strength of Cylindrical Concrete Specimens

Test for: Compressive Strength

Sample Information

Description: 4X8 Drycast Cylinder

Product Description: 60C3
Temp. of Concrete: 79

Summary of Results for Compressive Strength

Minimum at 28 days (psi): 4500

Test Result (psi) 6400

Pass/Fail

PASS

"Reference" data refers to Section(s) of Standard Reference

Manually Entered Data

Calculated Data

Number	1	2	3	4	5	6	7	Reference
Break (days)	1	2	7	7	28	28	28	
d (in)	4.00	4.00	4.00	4.00	4.00	4.00	4.00	9.1.2
A (in ²)	12.57	12.57	12.57	12.57	12.57	12.57	12.57	9.1.3
L _{MAX} (lbs)		49500	65505	66695	81475	80035	79915	9.1.4
CS (psi)	0	3939	5213	5307	6484	6367	6359	9.1.5
Fracture Type (1-6)		5	2	5	5	5		9.1.6

where:

d= Diameter

A= Area

L_{MAX}= Maximum Load

CS= Compressive Strength Fracture Type= Per ASTM C39, Figure 2

 $(p*d^2)/4$

A= CS=

L_{MAX}/A

