

RETURN WITHIN 2 WEEKS TO:  
CITY OF COLORADO SPRINGS  
STORM WATER & SUBDIVISION  
101 W. COSTILLA, SUITE 113  
COLORADO SPRINGS, CO 80903  
(719) 385-5979

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**NEVADA/TEJON INTERCHANGE  
CDOT PROJECT NO. IM0252-309**

**FINAL HYDRAULICS REPORT**

Submitted by:

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November 5, 1999  
JF9790

NEVADA/TEJON INTERCHANGE  
CDOT PROJECT NO. M0252-309

FINAL HYDRAULICS REPORT

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NEVADA/TEJON INTERCHANGE  
CDOT PROJECT NO. IM0252-309  
FINAL HYDRAULICS REPORT

I. INTRODUCTION

The Colorado Department of Transportation - Region 2 contracted with the firm of Felsburg Holt & Ullevig (FHU) for the provision of engineering services for the Nevada/Tejon Interchange Improvement project. The firm of J. F. Sato and Associates (JFSA) signed a sub-consultant agreement with FHU to provide services in the area of hydrology / hydraulic engineering required for this project.

The existing Nevada/Tejon Interchange complex and the proposed improvements are located in the City of Colorado Springs, El Paso County along I-25 in the immediate vicinity of the Fountain Creek / Cheyenne Creek confluence. The project area is partially in Township 14 South, Range 66 West, and partially in T15S, R66W. **Figure 1, Vicinity Map** shows the project area. Fountain Creek flows in a south-easterly direction parallel to I-25 in the project area. Cheyenne Creek flows north along Nevada Avenue. An elevated structure carries I-25 over Cheyenne Creek and Nevada Avenue. Cheyenne Creek joins Fountain Creeks just downstream of I-25.

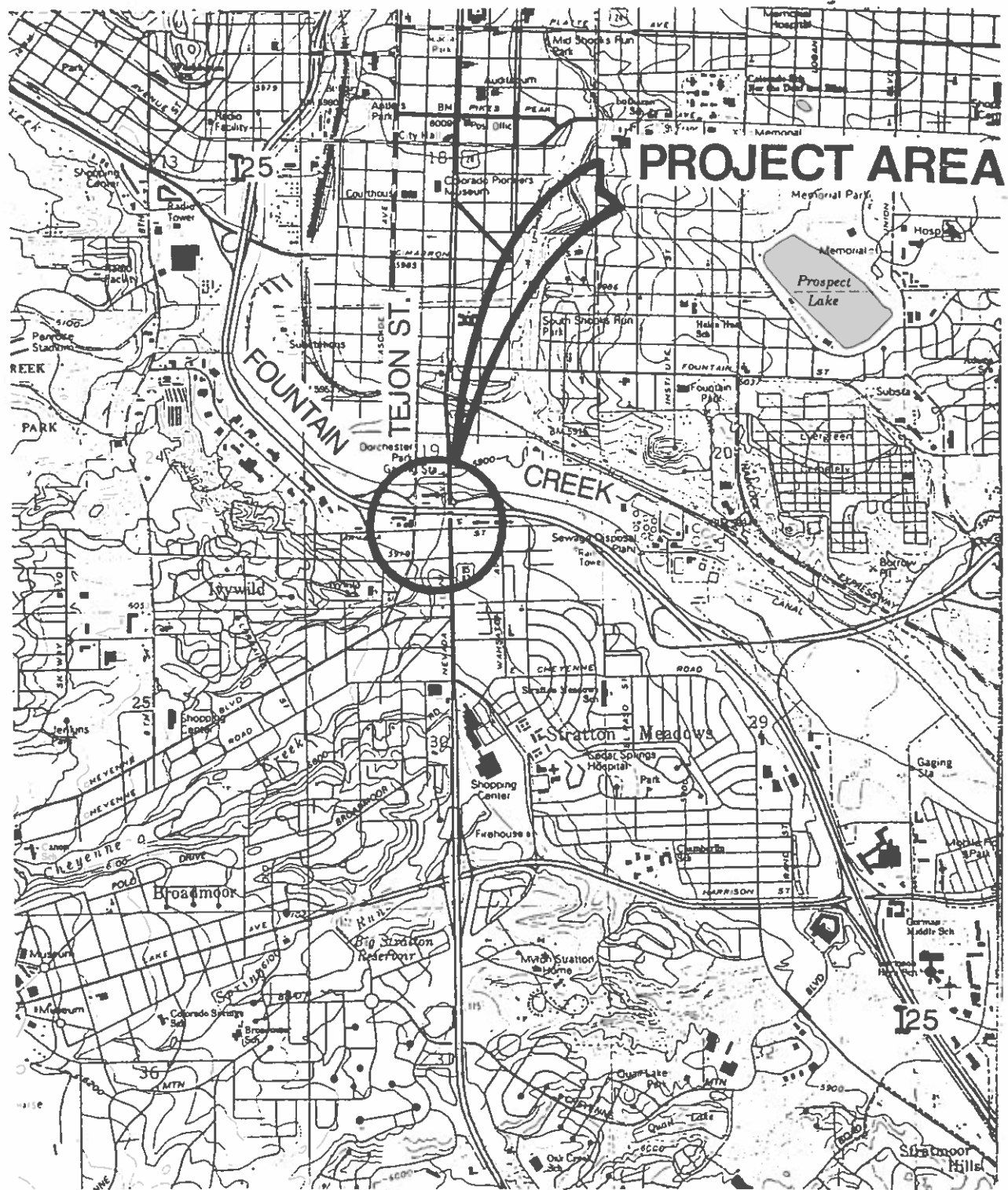
The proposed improvements to the existing Nevada/Tejon Interchange consist of providing acceleration/deceleration lanes for ramps; providing increased capacity for Nevada Avenue, Tejon Street, and Arvada Street; and other minor modifications to local streets. The project also includes widening of I-25 from four to six lanes within the project limits, and new bridge structures over Nevada Avenue - Cheyenne Creek and Tejon Street. The ultimate widening of I-25 will include eight lanes with two HOV lanes added. The horizontal alignment of I-25 will be slightly moved to the north. The profile of I-25 will be slightly raised near the Nevada/Tejon crossings. The project limits include approximately 1.5 miles of I-25.

A floodplain assessment report was prepared during the project development phase (Reference 1). This report summarizes the hydrologic and hydraulic investigations carried out during the project development phase and preliminary and final design phases. Floodplain / floodway and stream crossing issues are included in Chapter III, and stormwater drainage is discussed in Chapter IV.

II. HYDROLOGY

A. Fountain Creek

Hydrologic analyses for the Fountain Creek basin were carried out by the U. S. Army Corps of Engineers in 1976 for Flood Insurance Studies in El Paso County. The following peak discharge-frequency data for Fountain Creek in the project area were obtained from Reference 2.



**FIGURE 1**  
**VICINITY MAP**

Location	Drainage Area Km <sup>2</sup> /(Square Miles)	Peak Discharge, cms/(cfs)*			
		10-yr	50-yr	100-yr	500-yr
Downstream of confl. W/Monument Creek	927.2 (358.0)	261 (9,200)	807 (28,500)	1,195 (42,200)	2,275 (98,000)
Upstream of confl. W/Monument Creek	310.8 (120.0)	125 (4,400)	396 (14,000)	581 (20,500)	1,331 (47,000)

\* cms: cubic meters per second  
cfs: cubic feet per second

#### B. Cheyenne Creek

Peak discharges near the confluence with Fountain Creek obtained from Reference 2 are:

<u>Return Period, years</u>	<u>Q, cms - (cfs)</u>
10	159 - (5,600)
50	300 - (10,600)
100	377 - (13,300)
500	609 - (21,500)

Extrapolation in log-probability paper indicates that the 2-year peak discharge is approximately 43 cms (1,600 cfs) and the 5-year peak discharge is 113 cms (4,000 cfs). A copy of the peak flow - frequency curve is included in the appendix.

### III. EXISTING STRUCTURES

#### A. Storm Drainage Facilities

The alignment of I-25 within the project area runs on the south side of and parallel to Fountain Creek. The topography of the areas south of I-25 slope down in a general north-easterly direction towards Fountain Creek. The roadway embankment of I-25 constitute a major storm drainage feature in the project area.

Storm surface runoff that drains towards Fountain Creek is intercepted and collected by I-25 roadway side channels. Cross drainage culverts under I-25 convey the collected storm runoff to Fountain Creek. There are four major cross drainage culverts west of the Nevada/Tejon interchange and one east. Surface runoff from the I-25 highway pavement and median areas are collected at inlets that discharge into the following cross drainage culverts.

<u>I-25 Station</u>	<u>Size and Type</u>
300 + 760	900 mm (36-in.) RCP
301 + 160	1,200 mm & 600 mm (48-in. & 24-in.) RCPs
301 + 470	900 mm & 2-600 mm (36-in. & 2-24-in.) RCPs
301 + 900	450 mm (18-in.) RCP
302 + 700	1,200 mm (48-in.) RCP

The area immediately south of I-25 and west of Tejon Street includes large paved areas and other light industrial and commercial land use areas. The total area is approximately 14.7 ha (36 ac), of which 7.9 ha (19.5 ac) drain towards the portion of Arvada Street included in the project. A small roadside ditch along Arvada Street intercepts and conveys some surface runoff directly to Cheyenne Creek. Currently, there is no storm sewer on Arvada Street. There is a small storm sewer system along Tejon Street that discharges into Fountain Creek. On Nevada Avenue there are three small drainage systems that include curb and gutter, curb-opening (Type R) inlets, and storm pipes that discharge directly into Cheyenne Creek.

B. Stream Crossing Structures.

The following structures are located in the vicinity of the project area:

Fountain Creek. Nevada Avenue and Tejon Street are carried over Fountain Creek by separate structures. These two bridge structures are outside the project limits.

Cheyenne Creek. The existing I-25 highway crosses Nevada Avenue and Cheyenne Creek on a single elevated structure. Cheyenne Creek runs under this structure in its open natural channel. Downstream of I-25 a single cell concrete box culvert (CBC) carries Cheyenne Creek towards its outfall in Fountain Creek. The inlet of this CBC is approximately 30.5 m (100 feet) downstream of I-25. It has a length of approximately 45.7 m (150 feet). The outlet is about 36.5 m (120 feet) from Fountain Creek.

IV. DESIGN DISCUSSION

A. Floodplains and Floodways

1. Existing Conditions

The assessment report titled "Nevada/Tejon Interchange, Fountain Creek and Cheyenne Creek Floodplain and Floodway Boundaries under Existing Conditions" (Reference 1) was prepared by JFSA in August 1998.

As indicated in Reference 1 the floodplain boundaries shown in the current Flood Insurance Rate Maps are not valid. Roadway projects such as the US 24 bypass project that includes a bridge across Fountain Creek were built after the FIRM

panels were developed. The area in the vicinity of the Fountain Creek and Cheyenne Creek confluence do not correctly represent the floodplain limits in the area where I-25 is overtopped by the 100-year peak flow in Fountain Creek. The overbank areas south of I-25 are not effective flow areas. Peak flow in Cheyenne Creek for the 100-year event does not overtop I-25 with or without a median barrier. HEC-2 data file for Fountain Creek is not available in FEMA's archives managed by Michael Baker Engineering Co.

HEC-2 / HEC-RAS model of Fountain Creek was developed using current mapping provided by the City of Colorado Springs and topographic data developed by CDOT for this project. Correct floodplain and floodway boundaries for existing conditions were delineated on updated mapping. (Please see Reference 1.)

## 2. Proposed Conditions

The new cross sections with future widening of I-25 and future retaining wall on the south side of Fountain Creek, new ramps, and other roadway improvements were coded into the HEC-RAS model. The adopted I-25, ramp and wall alignments on the south side of Fountain Creek do not cause any floodplain encroachment. As shown in **Figure 2**, the 100-year water surface profiles for the existing and proposed conditions are substantially the same.

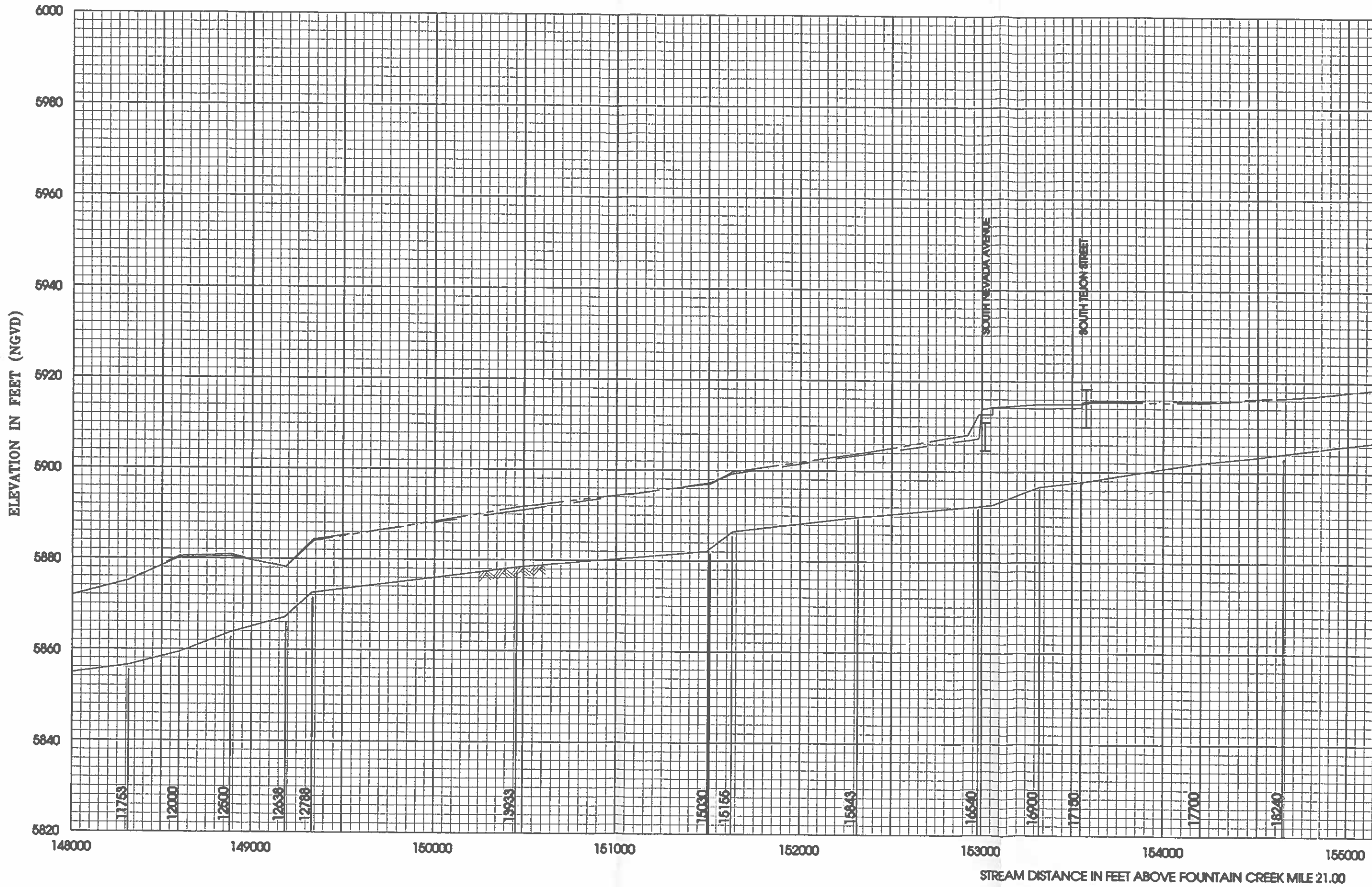
The profiles and other project data were presented to the El Paso County floodplain administrator. After review of the submitted material the Floodplain Administrator of El Paso County concluded that the proposed project will not increase the base flood elevations (BFEs) and the project will comply with current floodplain regulations. He also indicated that the map revision process for updating the current FIRM will be conducted by the County in the near future.

A copy of the letter from the Floodplain Administrator is included in the Appendix. Please see Reference 1 for a detailed discussion of hydraulic modeling of Fountain Creek. **A composite of the current Flood Insurance Rate Maps along Fountain and Cheyenne Creeks in the project area included in Reference 1 is included in the back cover pocket of this report also. It shows the location of the cross sections used in HEC-RAS.**

## B. Proposed Storm Drainage Plan

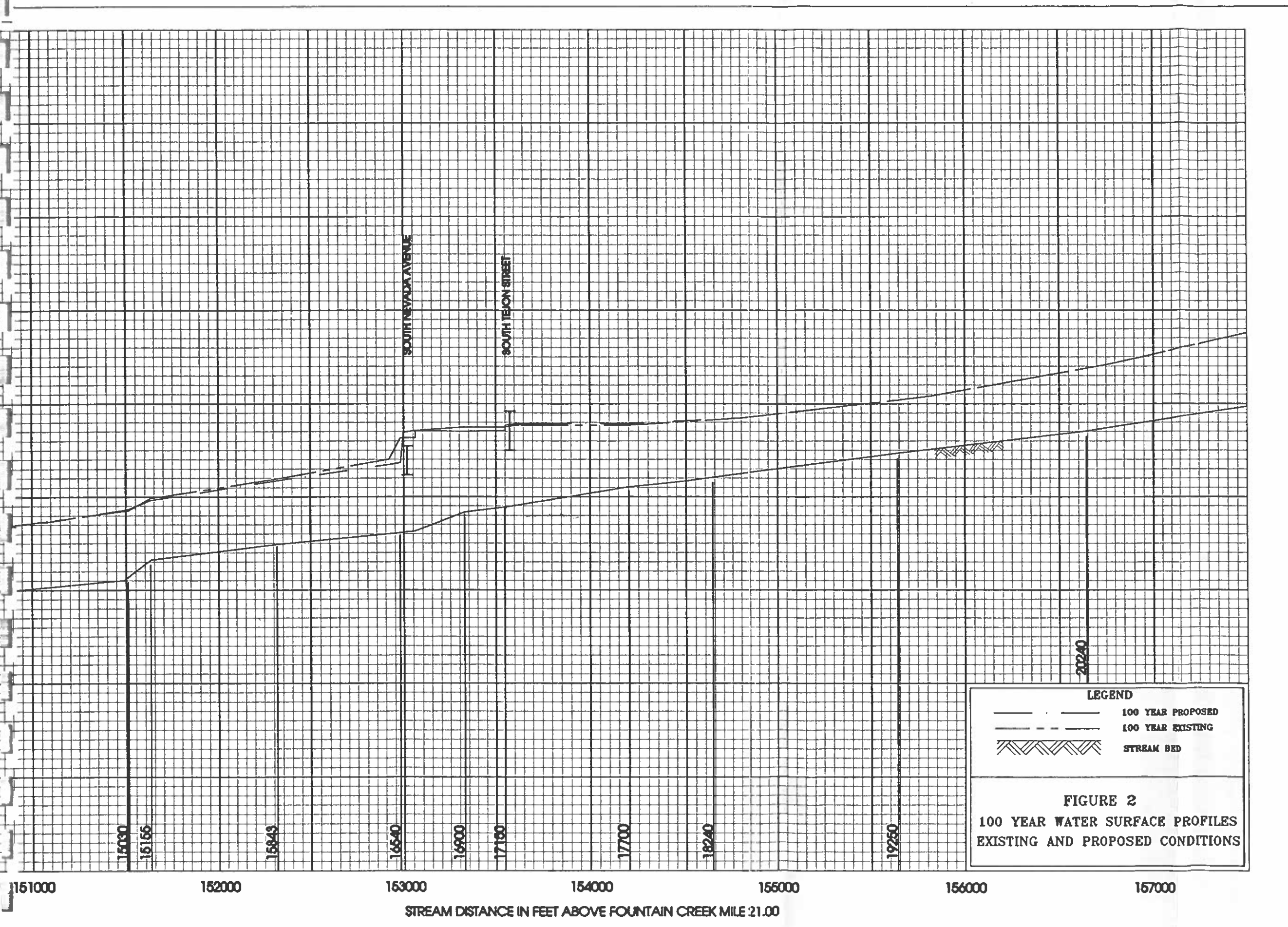
The proposed roadway improvements for the Nevada/Tejon Interchange will neither cause major changes to the predominant drainage patterns in the project area, nor significantly modify the existing drainage system.





ELEVATION IN FEET (NGVD)

STREAM DISTANCE IN FEET ABOVE FOUNTAIN CREEK MILE 21.00



**FLOOD PROFILES**  
**FOUNTAIN CREEK**

**JF SATO AND ASSOCIATES**  
**EL PASO COUNTY, CO**  
**AND INCORPORATED AREAS**  
**CITY OF COLORADO SPRINGS**

## 1. Methodology and Design Criteria

The design frequency and other design criteria were obtained from CDOT's Drainage Design Manual (Reference 3) and the City of Colorado Springs and El Paso County Drainage Criteria Manual (Reference 4). The Rational Method was used to estimate the peak rates of runoff at adopted design points. The more conservative criteria from the referenced manuals were selected for design of proposed drainage facilities. The following design frequencies were adopted.

Storm drains, major system: (all culverts across I-25)	100-year
Storm drains, minor system: (includes inlets)	10-year
Parallel Drainage: (side drains/roadside ditches, no overflow onto highway)	100-year

Peak flow rates for the 10-year and 100-year frequencies at designated design points were calculated using the Rational Method as prescribed by the City of Colorado Springs' Drainage Criteria Manual for drainage areas up to 100 acres (Reference 4). Rainfall intensity-frequency curves and runoff coefficients given in Reference 4 were used (Copies are included in the Appendix). Drainage basin boundaries, design points, and directions of flow were defined using FIMS mapping and 2-foot contour interval topographic maps provided by CDOT. The drainage basins are shown in **Exhibit 1** located in the back cover pocket of this report. Electronic data files or hard copy of FIMS topographic mapping used to delineate basin boundaries can be provided upon request.

## 2. Considered Storm Drainage Plan Alternatives

Two storm drainage plans for future developed conditions were considered. Future developed conditions include ultimate widening of I-25 to eight lanes with two HOV lanes added. Plan A with storm drain (sewer) systems and a detention pond on the south side of I-25, and plan B with storm drain systems only. All proposed storm drainage facilities were sized for the adopted design frequencies and were verified for the major storm event, namely the 100-year flood.

The detention pond of Plan A is located in Basin A10 to store runoff from basins A5, A6, A7, and A10 with releases to the existing 250 mm (18-in.) RCP that discharges in Fountain Creek (Please see Exhibit 1). The detention pond is located in CDOT's right of way near CDOT Region 2 office on Arvada Street.

Plan B includes storm drain systems on Nevada Avenue and Tejon Street with a single outfall to Cheyenne Creek.

The preliminary layout of plan A was discussed in the progress meeting of June 1999. Appraisal of Plan A was discontinued per CDOT's recommendation as CDOT land availability for a detention pond was not certain. Evaluation of Plan B continued to final design level. Estimates of 10-year and 100-year peak flow rates for proposed Plan B conditions are shown in **Table 1** and **Table 2**, respectively.

Considering that storm runoff for existing conditions is substantially unmodified, no peak flow rates for existing conditions were calculated. The I-25 roadway stations shown in these tables refer to the metric stationing adopted by CDOT for this project. The project limits along I-25 are located at approximately Sta. 300 + 700 and Sta.303 + 000 on the north and south limits, respectively. A set of preliminary design drawings have been submitted to CDOT under separate cover.

### C. Stream Crossing Structures

The Fountain Creek bridge structures that carry Nevada Avenue and Tejon Street will remain unmodified. The following Cheyenne Creek crossings structures are included in the project.

Interchange Structures. Two new crossing structures on Cheyenne Creek are included in the improved interchange. These structures carry the proposed roadways that link Nevada Avenue and Tejon Street on the north and south side of I-25 (North Connector and South Connector Roads, see Exhibit 2, page 14).

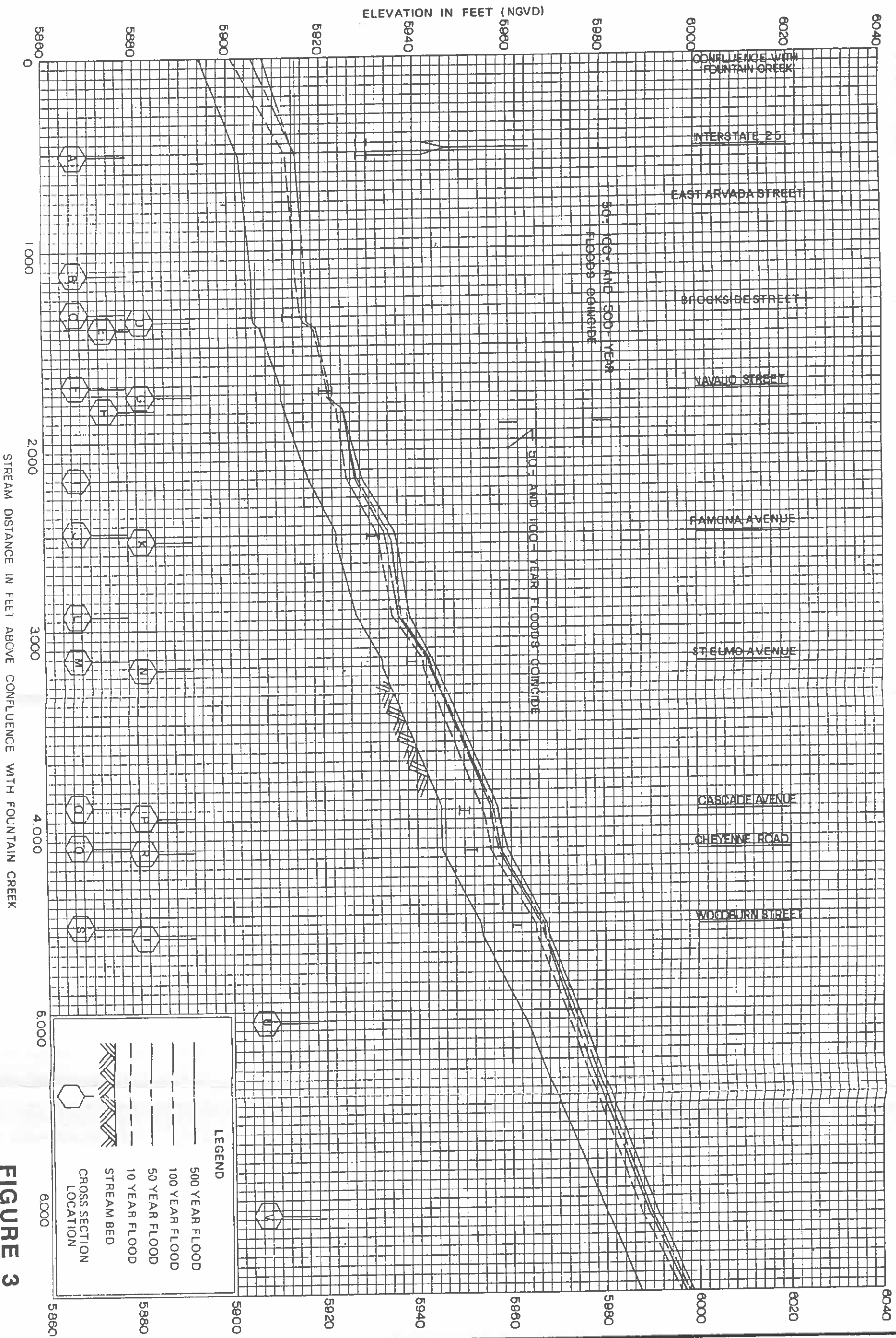
Arvada Street. The existing bridge across Cheyenne Creek will be replaced.

As indicated in Reference 1, the HEC-2 data file for Cheyenne Creek was available in FEMA's archives and a copy was provided by Michael Baker. The base flood elevations and floodway data obtained from this model do match the Floodway Data Table for Cheyenne Creek in the FIS dated March 1997 (Reference 4). The HEC-2 model was converted to a HEC-RAS model to analyze the proposed crossing structures. The Cheyenne Creek flood profiles drawing of Reference 4 is included in this report as **Figure 3**.

Figure 3 shows that the 50-, 100-, and 500-year flood water surface profiles coincide from just upstream of I-25 to the Navajo Street bridge, a stream distance of approximately 460 m (1,500 feet). The water level at elevation 5915 ft under the I-25 crossing is the same for 50-, 100-, and 500-year floods but is approximately 3 feet lower for the 10-year event. This indicates that the water level on Fountain Creek backs up the water level on Cheyenne Creek for major floods but not for the 10-year or more frequent events.







**FIGURE 3**

FEDERAL EMERGENCY MANAGEMENT AGENCY  
 EL PASO COUNTY, CO  
 AND INCORPORATED AREAS

**FLOOD PROFILES**  
**CHEYENNE CREEK**

The design frequency for the Cheyenne Creek crossing structures near the confluence with Fountain Creek was selected to avoid overtopping by events more frequent than the 10-year flood. By trial-and-error runs of HEC-RAS it was determined that the 2-year flood with a peak discharge of 45 cms (1,600 cfs) is the adequate design flood for the Cheyenne Creek crossing structures on the north and south connector roads, and replacement of the Arvada Street bridge.

Adequate alternative structures that will not be overtopped by the 2-year event are triple 4.6 m x 1.8 m (span x rise) (15' x 6') concrete box culvert, double 4.6 m x 2.1 m (15' x 7') RCP, or 12.2 m (40') single span bridge. HEC-RAS output plots of profile and cross sections and tables are included in the Appendix.

## V. RECOMMENDED DESIGN

- A. I-25 Cross Drainage Culverts - The existing cross drainage culverts under I-25 will be extended to accommodate the proposed interchange improvements.

Location (Sta)	Existing RCP Culvert	Q10 cms (cfs)	Q100 cms (cfs)	Remarks
300 + 760	900 mm (36-in.)	0.63 (22.1)	1.03 (36.2)	I-25 not widened at this location. Existing culvert with adequate capacity.
301 + 160	1200 mm & 600 mm (48-in. & 24-in)	1.02 (35.9)	1.66 (58.6)	Extend existing culvert. Adequate capacity.
301 + 470	900 mm & 2-600 mm (36-in & 2-24-in)	1.08 (38.0)	1.75 (61.9)	Extend existing 900 mm. RCP. Replace 2-600 mm with 900 mm RCP.
301 + 900	450 mm (18-in.)	N/A	N/A	Existing storm runoff drainage pipe that starts in parking lot of CDOT's office on Arvada Street, runs under I-25 and discharges in Fountain Creek. To be abandoned and replaced by Tejon/Arvada storm drainage system.
302 + 700	1200 mm (48-in)	1.18 (41.7)	1.66 (58.5)	Extend existing culvert. Adequate capacity.

The capacity of the existing cross drainage culverts were verified using CDOT criteria. Hydraulic calculations spread sheets are included in the Appendix.



I-25 Pavement Drainage

Drop (grate) inlets were selected to intercept drainage of I-25 pavement surfaces. The inlets were sized and placed for the design 10-year event and water spread verified for the 100-year event. Inlets were placed approximately every 100 m (300 ft.) and connected to 450 mm (18-in.) discharge pipes.

B. Tejon / Arvada Storm Drain System.

Storm runoff from areas south of I-25/west of Tejon Street and from portions of Tejon Street, South Connector Road, and Arvada Street will be collected and discharged into an underground storm sewer system that will outfall into Cheyenne Creek. The runoff peak flow rates for this system are shown in Tables 1 and 2. The main features of this system are:

Storm Sewer Line	Required Diameter, mm - (inch)	Approx. Length, m - (ft)	Remarks
Tejon St.	450 - (18) 1200 - (48) 1200 - (48) 1350 - (54)	26.8 - (88) 25.3 - (83) 35.0 - (115) <u>16.9 - (55)</u> 96.3 - (316)	Approximate lengths between inlet and manhole, between MHs, and between MH and outlet
Arvada St.	900 - (36) 1050 - (42)	241.5 - (792) <u>18.8 - (62)</u> 240.3 - (789)	Total distance between MHs
Ramp A- S. Connector Rd.	525 - (21)* 1350 - (54)	41.2 - (135) <u>154.0 - (505)</u> 195.2 - (640)	Distance from inlet to MH Outfall to Cheyenne Creek - distance between MHs

\* Required size can be changed to 600 - (24) size if adequate cover is available

A grass-lined roadside channel with very flat slope from approximately Sta. 301 + 700 to Tejon Street will provide some water quality improvement to the runoff flows originating on the area just south of I-25.

C. Nevada Avenue Storm Drain System

Runoff from an area south of I-25/East of Nevada Avenue and from portions of Nevada Avenue and S. Connector road will be conveyed to Cheyenne Creek by a storm sewer system. The main features of this small system are:

Storm Sewer Line	Required Diameter mm - (inch)	Approx. Length m - (ft)	Remarks
Nevada Ave.	450 - (18)	80.9 - (265)	Line includes pipe along Nevada Ave. and lateral lines from Type R inlets near Arvada St.
Ramp C - Outfall to Cheyenne Creek	530 - (21)* 675 - (27)	74.2 - (343) <u>24.8 - (80)</u> 99.0 - (423)	Total distance between Ramp C inlet and MH3. Distance between inlet in Nevada Ave. and outlet.

\* Required size can be changed to 600 - (24) size if adequate cover is available

A general layout of these storm drainage systems is shown in **Exhibit 2**.

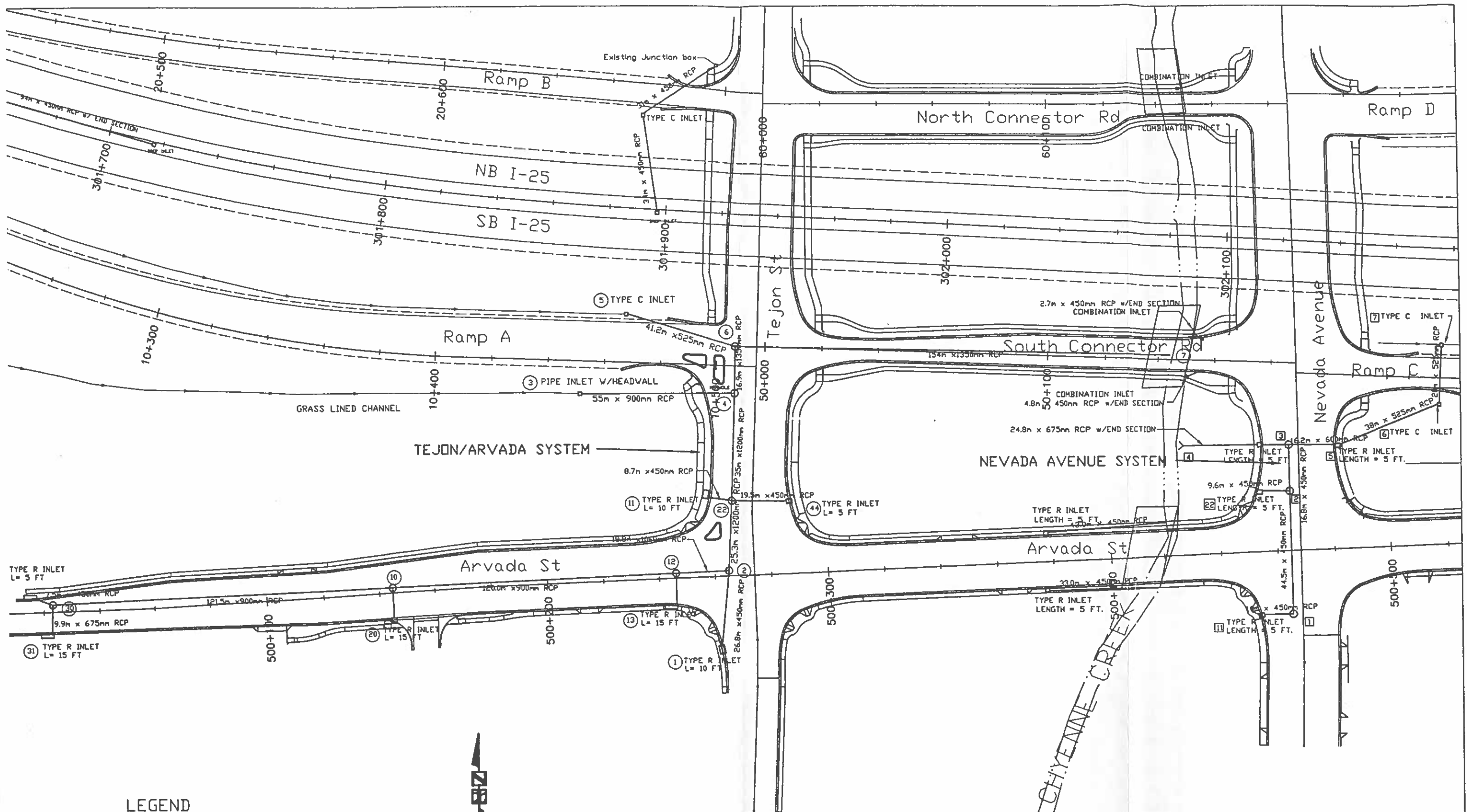
Hydraulic calculations for the proposed storm drain systems were done using the program UDSEWER. The design peak discharges were obtained from Table 1, 10-year Peak Runoff Flow Rates. A schematic layout of the proposed storm drain systems shown in Exhibit 2, and a table showing the design peak flows are included in the Appendix. Sizing of curb opening in a sump condition for Type R inlets was done using the chart and graph included in the Appendix.

D. Cheyenne Creek Crossing Structures

After the FIR presentation and discussion with CDOT project staff, it was decided to use the bridge alternative for all the structures on Cheyenne Creek. The three structures are single span bridges:

	Length of Single Span
North Connector Road	12.2 m (40 ft)
South Connector Road	12.2 m (40 ft)
Arvada Street	11.5 m (37.7 ft)

These structures can accommodate the 2-year flood with no overtopping.



LEGEND

- ② DESIGN POINT TEJON/ARVADA SYSTEM
- ② DESIGN POINT NEVADA SYSTEM

EXHIBIT 2  
NEVADA/TEJON INTERCHANGE  
GENERAL LAYOUT OF  
STORM SEWER SYSTEMS

Estimates of potential contraction scour at these three bridges were estimated using flow distribution and hydraulic parameters calculated with HEC-RAS:

<u>Frequency</u>	<u>Total Potential Scour, ft</u>		
	<u>N. Connector</u>	<u>South Connector</u>	<u>Arvada</u>
2-year	0.0	0.0	2.5
100-year	4.0	7.4	6.6
500-year	5.5	9.8	7.5

No local nor degradation scour is anticipated. Similar depths of potential scour at the north and south connector roadway culverts can be used for design of these structures.

The recommended highway improvements will not cause an increase in the 100-year water surface elevation on either Fountain Creek or Cheyenne Creek. The proposed project is in compliance with current floodplain development regulations in El Paso County.

The proposed widening of I-25 from four lanes to eight lanes will result in some increase of peak runoff flows in the existing cross drainage culverts. The existing culverts have capacity to safely pass the design peak flows. Some modifications to the existing cross drainage system will be required.

The storm drainage systems for Tejon/Arvada streets and Nevada Avenue include storm drains to convey the runoff flows to Cheyenne Creek. Roadway drainage facilities have been provided on all proposed ramps and connector roadways.

## VI. REFERENCES

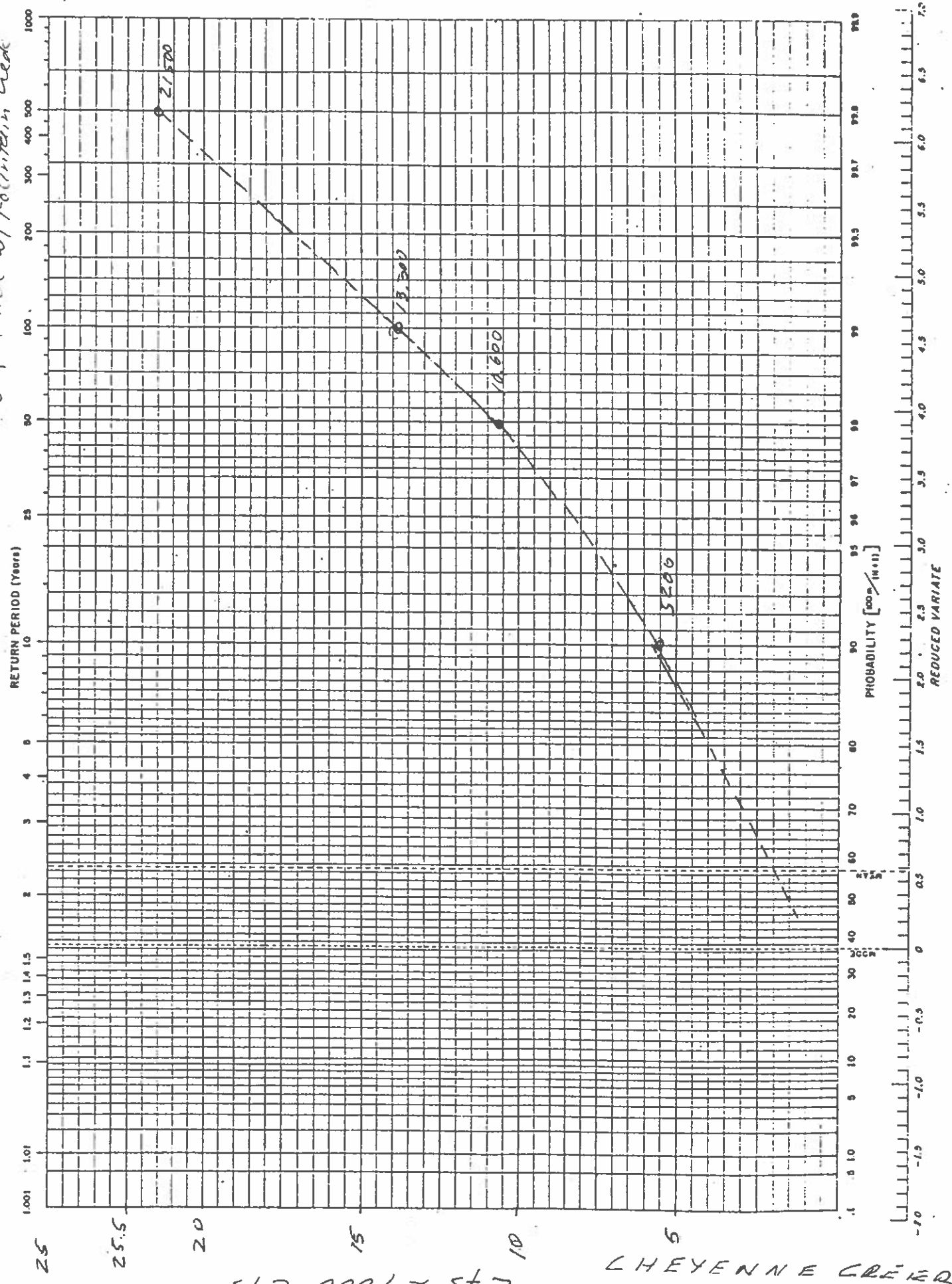
1. J. F. Sato and Associates, Nevada/Tejon Interchange - Assessment Report- Fountain Creek and Cheyenne Creek Floodplain Boundaries under Existing Conditions, August 1998
2. Federal Emergency Management Agency - Flood Insurance Study, El Paso County, Colorado and Incorporated Areas, March 17 1997
3. Colorado Department of Transportation - Drainage Design Manual, July 1995.
4. City of Colorado Springs and El Paso County - Drainage Criteria Manual, July 1996.

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## **APPENDIX**

- Cheyenne Creek Flood Frequency Curve
- Copy of Regional Floodplain Administrator's Letter
- Rainfall-Intensity-Frequency Curves - El Paso County,  
and Recommended Average Runoff Coefficients
- HEC-RAS Output and Scour Calculations, Cheyenne Creek
- Culvert Capacity Calculations
- Storm Sewer Profile Calculations, Inlet Sizing Chart

Cheyenne Creek  
 @ Confluence w/ Fountain Creek



ST 0 0001 + ST 0

CHEYENNE CREEK  
 FLOOD FREQUENCY  
 CURVE

PIKES PEAK REGIONAL BUILDING DEPARTMENT  
101 WEST COSTILLA  
COLORADO SPRINGS COLORADO 80903-3879

February 22, 1999

James Flohr, P.E.  
Colorado Department of Transportation  
16 East Arvada Street  
Colorado Springs, CO 80906

Re: Nevada Avenue/Tejon Street Interchange

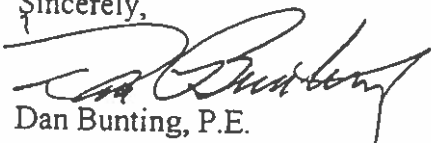
Dear James Flohr:

I have reviewed the hydraulic analysis for this project, as prepared by J.F. Sato. That analysis indicated that the proposed improvements would not cause an increase in the 100 year water surface elevation, therefore the project would comply with the current floodplain development requirements. Based on this information, a floodplain development permit could be issued for construction of the proposed interchange.

A separate application for a floodplain development permit will be needed prior to construction.

If I can provide any additional information or assistance, please give me a call, 719-327-2906 or fax 719-327-2953.

Sincerely,



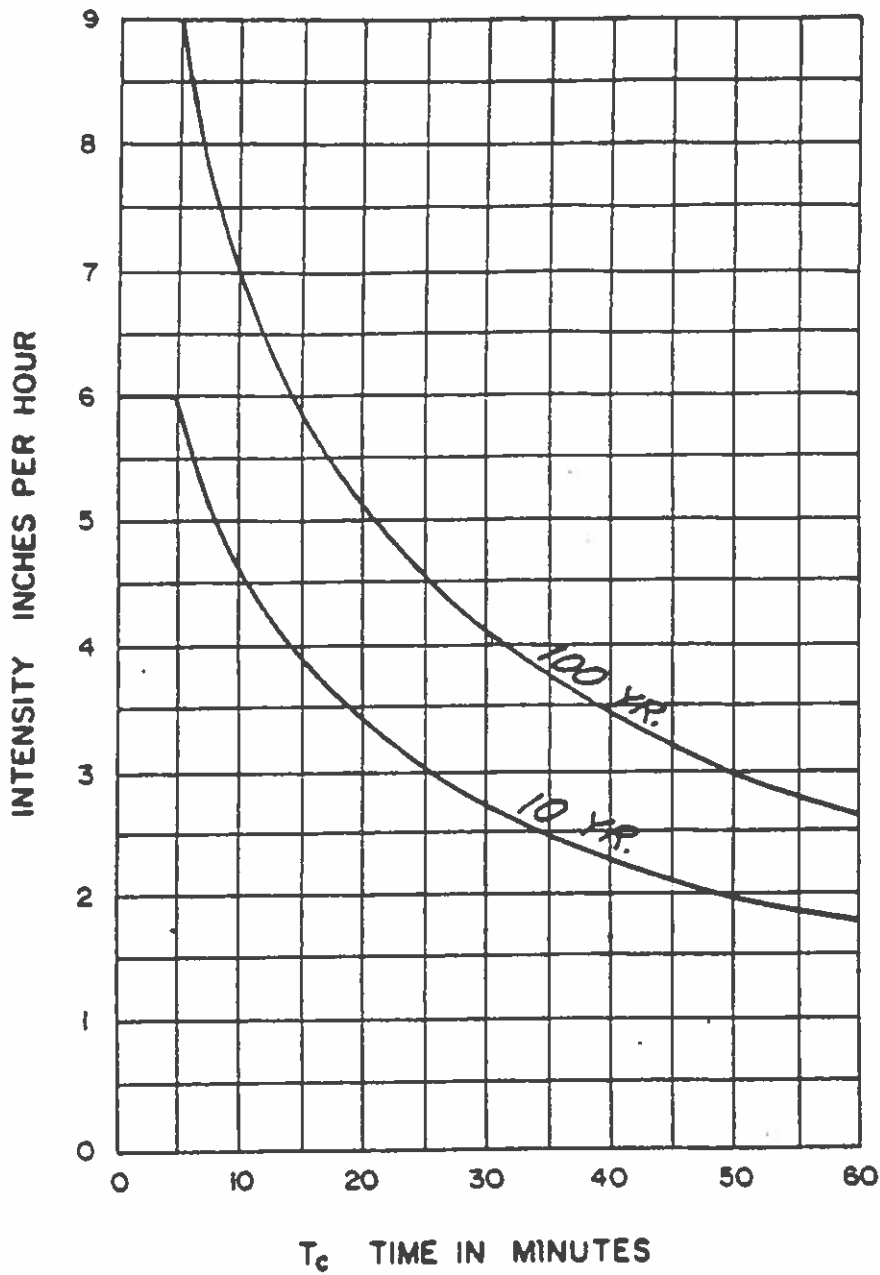
Dan Bunting, P.E.  
Regional Floodplain Administrator

Hunt

FH4

Sato





RE: Based upon Pikes Peak area council of governments/  
areawide urban runoff control manual.



HDR Infrastructure, Inc.  
A Centerra Company

The City of Colorado Springs / El Paso County  
Drainage Criteria Manual

Storm Rainfall  
Time Intensity-Frequency Curves

Date

OCT. 1987

Figure

5 - 1

TABLE 5-1

RECOMMENDED AVERAGE RUNOFF COEFFICIENTS AND PERCENT IMPERVIOUS

LAND USE OR SURFACE CHARACTERISTICS	PERCENT IMPERVIOUS	"C" FREQUENCY			
		10		100	
		A&B*	C&D*	A&B*	C&D*
<b>Business</b>					
Commercial Areas	95	0.90	0.90	0.90	0.90
Neighborhood Areas	70	0.75	0.75	0.80	0.80
<b>Residential</b>					
1/8 Acre or less	65	0.60	0.70	0.70	0.80
1/4 Acre	40	0.50	0.60	0.60	0.70
1/3 Acre	30	0.40	0.50	0.55	0.60
1/2 Acre	25	0.35	0.45	0.45	0.55
1 Acre	20	0.30	0.40	0.40	0.50
<b>Industrial</b>					
Light Areas	80	0.70	0.70	0.80	0.80
Heavy Areas	90	0.80	0.80	0.90	0.90
<b>Parks and Cemeteries</b>	7	0.30	0.35	0.55	0.60
<b>Playgrounds</b>	13	0.30	0.35	0.60	0.65
<b>Railroad Yard Areas</b>	40	0.50	0.55	0.60	0.65
<b>Undeveloped Areas</b>					
Historic Flow Analysis- Greenbelts, Agricultural Pasture/Meadow	0	0.25	0.30	0.35	0.45
Forest	0	0.10	0.15	0.15	0.20
Exposed Rock	100	0.90	0.90	0.95	0.95
Offsite Flow Analysis (when land use not defined)	45	0.55	0.60	0.65	0.70
<b>Streets</b>					
Paved	100	0.90	0.90	0.95	0.95
Gravel	80	0.80	0.80	0.85	0.85
<b>Drive and Walks</b>	100	0.90	0.90	0.95	0.95
<b>Roofs</b>	90	0.90	0.90	0.95	0.95
<b>Lawns</b>	0	0.25	0.30	0.35	0.45

\* Hydrologic Soil Group

9/30/90

- HEC-RAS Output and Scour Calculations, Cheyenne Creek

HEC-RAS Plan: Imported Pla River: RIVER-1 Reach: Reach-1

Reach	River Sta	Q Total	Min Ch El	W.S. Elev	Crit W.S	E.G. Elev	E.G. Slope	Vel Chg	Flow Area	Top Width	Froude Ch
		(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq.ft)	(ft)	
Reach-1	2040	1600.00	5911.90	5918.02		5919.67	0.007047	10.82	188.92	46.66	0.82
Reach-1	2040	13300.00	5911.90	5925.07	5925.07	5926.43	0.004647	15.33	3532.25	1093.56	0.77
Reach-1	2040	21500.00	5911.90	5926.29	5926.29	5927.70	0.005302	17.42	4929.73	1187.60	0.83
Reach-1	2036	1600.00	5911.10	5918.42	5917.39	5918.67	0.005835	6.24	547.97	258.92	0.57
Reach-1	2036	13300.00	5911.10	5922.95	5921.47	5923.23	0.005041	8.51	4035.65	1172.48	0.59
Reach-1	2036	21500.00	5911.10	5924.08	5922.25	5924.45	0.005522	9.91	5412.65	1249.15	0.63
Reach-1	2035.5	Bridge									
Reach-1	2035	1600.00	5911.10	5918.40		5918.66	0.005896	6.27	545.19	257.57	0.58
Reach-1	2035	13300.00	5911.10	5922.11		5922.64	0.011096	11.52	3088.17	1097.87	0.85
Reach-1	2035	21500.00	5911.10	5923.23		5923.83	0.010391	12.57	4374.78	1193.97	0.85
Reach-1	2032	1600.00	5907.00	5913.24	5913.24	5915.40	0.012749	11.77	136.04	32.80	1.01
Reach-1	2032	13300.00	5907.00	5919.31	5919.31	5920.32	0.005304	13.30	3820.17	1495.83	0.74
Reach-1	2032	21500.00	5907.00	5920.10	5920.10	5921.26	0.006638	15.66	5018.72	1521.81	0.84
Reach-1	2031	1600.00	5905.50	5913.15	5910.80	5914.44	0.005999	9.09	176.04	23.00	0.58
Reach-1	2031	13300.00	5905.50	5918.29	5917.28	5918.70	0.003376	9.42	3745.59	1378.46	0.46
Reach-1	2031	21500.00	5905.50	5919.36	5918.03	5919.85	0.004092	10.94	5390.35	1669.55	0.52
Reach-1	2030.5	Bridge									
Reach-1	2030	1600.00	5905.30	5912.60		5914.01	0.006843	9.53	167.97	23.00	0.62
Reach-1	2030	13300.00	5905.30	5917.08	5917.08	5918.09	0.007997	13.73	2615.79	1020.19	0.70
Reach-1	2030	21500.00	5905.30	5917.83	5917.83	5919.13	0.010668	16.53	3429.67	1138.93	0.82
Reach-1	2024	1600.00	5905.30	5912.28	5912.28	5912.66	0.002209	6.04	595.56	857.74	0.45
Reach-1	2024	13300.00	5905.30	5914.18	5914.18	5914.95	0.006318	12.39	2521.80	1234.44	0.79
Reach-1	2024	21500.00	5905.30	5916.48		5916.77	0.001553	7.33	5372.83	1240.20	0.41

HEC-RAS Plan: Imported Pla River: RIVER-1 Reach: Reach-1 (Continued)

Reach	River Sta	Q Total	Min Ch El	W/S Elev	Gr/W/S	E.G. Elev	E.G. Slope	Vel Ch	Flow Area	Top Width	Flood Coef
		(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Reach-1	6	1600.00	5904.01	5909.16	5908.40	5909.28	0.001510	3.80	679.97	381.78	0.35
Reach-1	6	13300.00	5904.01	5914.18	5911.11	5914.29	0.000503	3.75	5398.96	1150.00	0.23
Reach-1	6	21500.00	5904.01	5916.51	5911.88	5916.63	0.000366	3.78	8078.55	1150.00	0.20
Reach-1	5.5	Bridge									
Reach-1	5	1600.00	5902.00	5908.06	5908.06	5908.61	0.005048	7.29	393.59	344.69	0.62
Reach-1	5	13300.00	5902.00	5913.90		5914.12	0.000913	5.51	4063.31	1050.00	0.31
Reach-1	5	21500.00	5902.00	5916.35		5916.54	0.000575	5.05	6636.02	1050.00	0.25
Reach-1	4	1600.00	5900.00	5906.23	5904.10	5906.61	0.002043	4.99	353.32	243.61	0.42
Reach-1	4	13300.00	5900.00	5913.37	5909.87	5913.92	0.001169	7.26	2425.88	303.23	0.38
Reach-1	4	21500.00	5900.00	5915.45	5911.44	5916.33	0.001481	9.13	3056.47	303.23	0.44
Reach-1	3.5	Bridge									
Reach-1	3	1600.00	5900.00	5905.59	5904.29	5906.29	0.004097	6.71	238.53	59.47	0.59
Reach-1	3	13300.00	5900.00	5911.76	5911.03	5913.47	0.004211	12.55	1454.17	240.18	0.70
Reach-1	3	21500.00	5900.00	5912.81	5912.81	5915.92	0.006846	17.09	1705.26	240.18	0.90
Reach-1	2	1600.00	5898.01	5904.45	5903.19	5905.48	0.005655	8.13	196.82	45.07	0.69
Reach-1	2	13300.00	5898.01	5911.86	5911.13	5912.65	0.002630	9.50	2471.09	751.68	0.54
Reach-1	2	21500.00	5898.01	5913.06	5912.28	5914.02	0.002987	10.94	3397.75	778.32	0.58
Reach-1	1.75	Bridge									
Reach-1	1.5	1600.00	5897.51	5902.69	5902.69	5904.59	0.012821	11.08	144.42	38.39	1.01
Reach-1	1.5	13300.00	5897.51	5910.63	5910.63	5911.99	0.004618	11.94	1947.24	674.02	0.70
Reach-1	1.5	21500.00	5897.51	5911.78	5911.78	5913.33	0.005074	13.56	2788.96	769.52	0.75

HEC-RAS Plan: Imported Pla River: RIVER-1 Reach: Reach-1 (Continued)

Reach	River Sta	Q Total	Min Ch El	W/S Elev	Crit W/S	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude	Gal
		(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)		
Reach-1	1	1600.00	5896.00	5900.34	5900.34	5901.13	0.015996	7.14	224.03	145.30		1.01
Reach-1	1	13300.00	5896.00	5909.85		5910.60	0.001316	6.97	1967.34	250.13		0.39
Reach-1	1	21500.00	5896.00	5909.53		5911.63	0.003840	11.68	1887.54	241.38		0.67
Reach-1	0.5	1600.00	5893.00	5900.00	5897.35	5900.10	0.000572	2.48	644.50	167.11		0.22
Reach-1	0.5	13300.00	5893.00	5910.00	5902.00	5910.38	0.000488	5.05	2881.08	311.51		0.25
Reach-1	0.5	21500.00	5893.00	5910.00	5904.18	5910.99	0.001275	8.16	2881.08	311.51		0.40

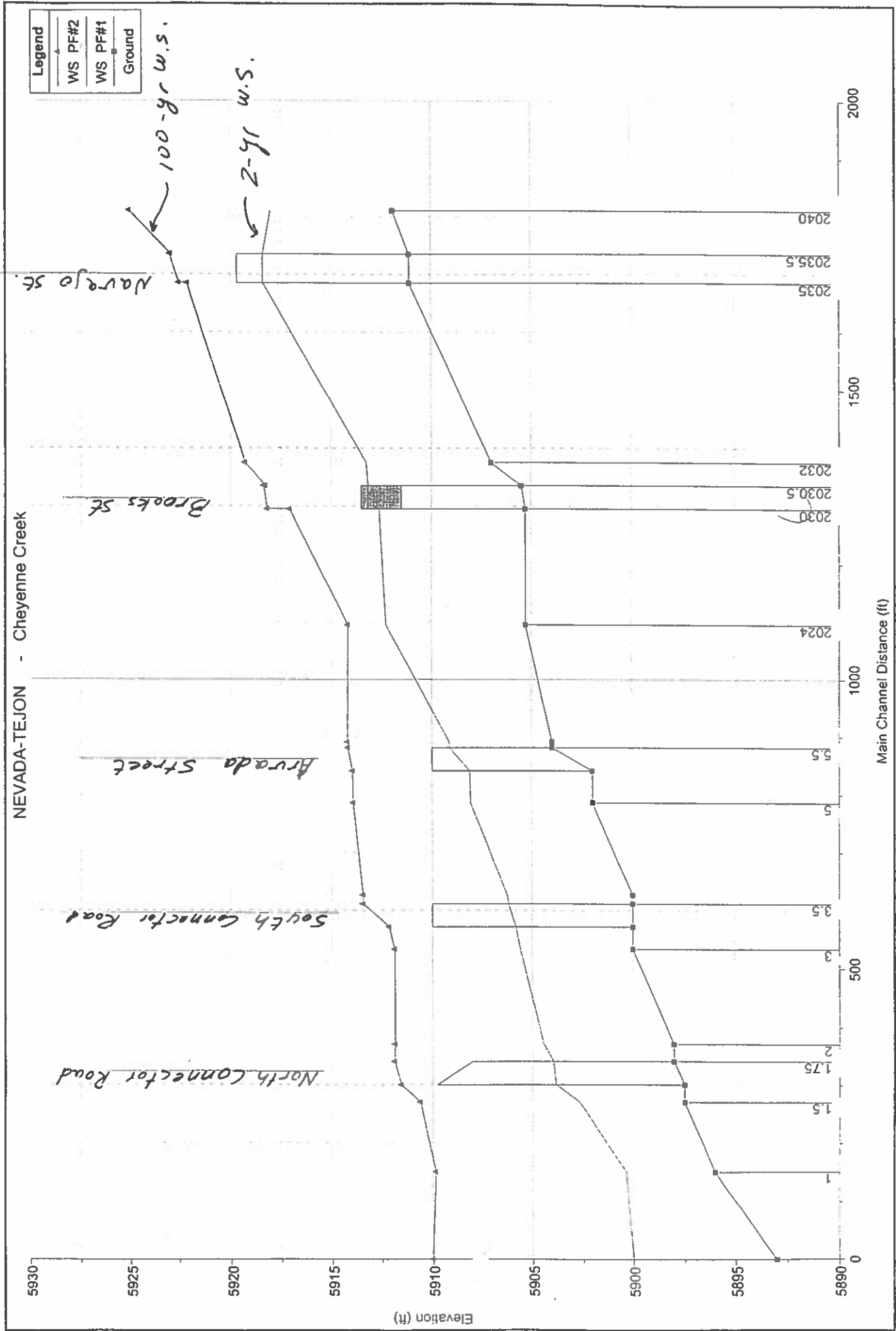
HEC-RAS Plan: Imported Pla River: RIVER-1 Reach: Reach-1

Reach	River Station	F.G. Elev. (ft)	W.S. Elev. (ft)	Vel Head (ft)	Frcnl Loss (ft)	C & E Loss (ft)	Q Left (cfs)	Q Channel (cfs)	Q Right (cfs)	Ch Width (ft)
Reach-1	2040	5919.67	5918.02	1.65	0.44	0.56	17.72	1434.53	147.75	46.66
Reach-1	2040	5926.43	5925.07	1.36	0.31	0.43	532.54	4679.10	8088.36	1093.56
Reach-1	2040	5927.70	5926.29	1.41	0.34	0.42	1166.02	5836.89	14497.09	1187.60
Reach-1	2036	5918.67	5918.42	0.25				521.11	1078.89	258.92
Reach-1	2036	5923.23	5922.95	0.28	0.00	0.06	28.92	1846.50	11424.58	1172.48
Reach-1	2036	5924.45	5924.08	0.37	0.00	0.07	171.30	2527.11	18801.58	1249.15
Reach-1	2035.5	Bridge								
Reach-1	2035	5918.66	5918.40	0.26	2.51	0.76		521.80	1078.20	257.57
Reach-1	2035	5922.64	5922.11	0.53	2.13	0.19	1.29	2179.34	11119.37	1097.87
Reach-1	2035	5923.83	5923.23	0.60	2.34	0.22	74.59	2848.94	18576.47	1193.97
Reach-1	2032	5915.40	5913.24	2.15	0.34	0.35		1599.95	0.05	32.80
Reach-1	2032	5920.32	5919.31	1.01	0.17	0.24	800.87	4581.54	7917.59	1495.83
Reach-1	2032	5921.26	5920.10	1.16	0.21	0.27	1801.30	5828.58	13870.11	1521.81
Reach-1	2031	5914.44	5913.15	1.28				1600.00		23.00
Reach-1	2031	5918.70	5918.29	0.41	0.00	0.12	6915.56	2772.53	3611.90	1378.46
Reach-1	2031	5919.85	5919.36	0.49	0.00	0.13	11552.83	3488.76	6458.41	1669.55
Reach-1	2030.5	Bridge								
Reach-1	2030	5914.01	5912.60	1.41	0.74	0.61		1600.00		23.00
Reach-1	2030	5918.09	5917.08	1.01	1.61	0.14	6580.57	3720.20	2999.23	1020.19
Reach-1	2030	5919.13	5917.83	1.29	0.74	0.60	10981.31	4764.80	5753.89	1138.93
Reach-1	2024	5912.66	5912.28	0.39	0.35	0.08	391.07	1063.34	145.59	857.74
Reach-1	2024	5914.95	5914.18	0.77	0.18	0.20	8794.17	2905.87	1599.95	1234.44

HEC-RAS Plan: Imported Pla River: RIVER-1 Reach: Reach-1 (Continued)

Reach	River Sta	E.G. Elev. (ft)	W.S. Elev. (ft)	Vel/Head (ft)	Frctn. Loss (ft)	C & E Loss (ft)	Q Left (cfs)	Q Channel (cfs)	Q Right (cfs)	Top Width (ft)
Reach-1	2024	5916.77	5916.48	0.29	0.09	0.05	15774.85	2241.13	3484.02	1240.20
Reach-1	5	5909.28	5909.16	0.12	0.02	0.00	0.24	585.38	1014.38	381.78
Reach-1	6	5914.29	5914.18	0.11	0.01	0.00	4597.72	1460.99	7241.29	1150.00
Reach-1	6	5916.63	5916.51	0.12	0.00	0.00	9061.78	1886.13	10552.09	1150.00
Reach-1	5.5	Bridge								
Reach-1	5	5908.61	5908.06	0.55	0.49	0.05	0.00	1014.15	585.85	344.69
Reach-1	5	5914.12	5913.90	0.23	0.17	0.03	2988.98	1815.24	8495.77	1050.00
Reach-1	5	5916.54	5916.35	0.19	0.14	0.07	8022.29	2069.18	11408.52	1050.00
Reach-1	4	5906.61	5906.23	0.38	0.03	0.00	0.03	1576.92	23.05	243.61
Reach-1	4	5913.92	5913.37	0.55			271.41	6101.80	6926.80	303.23
Reach-1	4	5916.33	5915.45	0.88			501.09	9069.08	11929.83	303.23
Reach-1	3.5	Bridge								
Reach-1	3	5906.29	5905.59	0.70	0.78	0.03		1600.00		59.47
Reach-1	3	5913.47	5911.76	1.71	0.54	0.27	93.87	7700.56	5505.57	240.18
Reach-1	3	5915.92	5912.81	3.12	0.71	0.65	166.26	11571.98	9761.75	240.18
Reach-1	2	5905.48	5904.45	1.03	0.19	0.03		1600.00		45.07
Reach-1	2	5912.65	5911.86	0.79	0.12	0.06	760.38	6253.31	6286.31	751.68
Reach-1	2	5914.02	5913.06	0.96	0.12	0.06	2292.01	8096.26	11111.74	778.32
Reach-1	1.75	Bridge								
Reach-1	1.5	5904.59	5902.69	1.91	1.71	0.33		1600.00		38.39
Reach-1	1.5	5911.99	5910.63	1.36	0.27	0.18	473.85	7267.47	5558.69	674.02







Project Nevada / Tipton / I-25 Reference \_\_\_\_\_ JFSA Job No. 9790  
 Subject Bridge scour Designed \_\_\_\_\_ Date \_\_\_\_\_  
 Item Cherokee Creek Checked \_\_\_\_\_ Date \_\_\_\_\_

$Q_2 = 1,600 \text{ cfs}$        $Q_{100} = 13,300 \text{ cfs}$        $Q_{500} = 21,500 \text{ cfs}$

$D_{50} = 2 \text{ mm} = 0.0066 \text{ ft}$  (Assume)

Shear Vel.,  $V_{*c} = (g y_1 s_1)^{0.5}$

Fall Velocity,  $w = 0.9 \text{ fps}$

$$\frac{y_2}{y_1} = \left( \frac{Q_{mc2}}{Q_{mc1}} \right)^{6/7} \left( \frac{w_{c1}}{w_{c2}} \right)^{k_1} \left( \frac{n_2}{n_1} \right)^{k_2}$$

(1) : Main channel

(2) : Contracted channel

	Bridge		
	N.Conn.	S.Conn.	Arvada
	(1.75)	(3.5)	(5.5)

100-y1:

$y_1, \text{ft}$	17.18	15.55	11.92
$Q_{mc2}$	13,300	13,300	13,300
$Q_{mc1}$	9519	7702	7274
$S \times 10^{-4}$	3.6	5.7	1.84
$V_{*c}$	0.50	0.59	0.30
$k_1$	0.64	0.64	0.50
$k_2$	0.21	0.21	0.066
$n_1$	0.035	0.035	0.035
$n_2$	0.024	0.024	0.024
$w_{c1}/w_{c2}$	1	1	1
$y_2/y_1$	1.231	1.476	1.55
$y_2$	4.0	7.4	6.6



J.F. SATO AND ASSOCIATES  
Consulting Engineers  
Project Managers & Planners

Sheet 2/2

Project \_\_\_\_\_ Reference \_\_\_\_\_ JFSA Job No. \_\_\_\_\_  
Subject \_\_\_\_\_ Designed \_\_\_\_\_ Date \_\_\_\_\_  
Item \_\_\_\_\_ Checked \_\_\_\_\_ Date \_\_\_\_\_

	(1.75)	(3.5)	(5.5)
	NC	SC	Atwood
<u>500-yr</u>			
y <sub>1</sub>	17.49	15.91	12.8
Q <sub>mc2</sub>	21,500	21,500	21,500
Q <sub>mc1</sub>	15,600	12,267	12,500
y <sub>2/y<sub>1</sub></sub>	1.317	1.618	1.592
y <sub>s</sub>	5.5	9.8	7.5
<u>2-yr</u>			
y <sub>1</sub>	6.44	6.23	5.15
Q <sub>mc2</sub>	1600	1,600	1600
Q <sub>mc1</sub>	1600	1576	1013
y <sub>2/y<sub>1</sub></sub>	1	1.013	1.48
y <sub>s</sub>	0.0	0.08	2.5

- 
- **Culvert Hydraulic Calculations**

# PRELIMINARY CULVERT DESIGN WITH CONSIDERATION OF INLET/OUTLET CONTROL

Project: Tejon/Nevada Interchange at 300+760  
 Date: April 1, 1999

## I. Culvert Hydraulics

Culvert ID	Culvert Hydraulic Control	Design Flow cfs	Length ft	Slope ft/ft	Conduit Shape	Dia or Rise ft	Dia or Span ft	Number of Cell	Flow per Cell cfs/ft	Flow per ft	Hw/D Ratio	Manning's N	Hydr. Radius ft	Flow Area sq ft	Flow Vel. fps	Vel. Head ft	Friction Slope ft/ft	Entrance Loss ft	Exit Loss ft	Friction Losses ft	Invert Drop ft	HW
300+760	Inlet	36.21	175.00	0.0100	R	3.50	3.50	1.00	36.21	10.35	0.78										1.75	2.73
	Outlet	36.21	175.00	0.0100	R	3.50	3.50	1.00	36.21	10.35		0.0130	0.88	9.62	3.76	0.22	0.00129	0.0660	0.0440	0.2255	1.75	2.09
	Control				R	3.50	3.50	1.00	36.21	10.35											1.75	2.73
300+760	Inlet	36.21	175.00	0.0100	R	3.00	3.00	1.00	36.21	12.07	1.00										1.75	3.00
	Outlet	36.21	175.00	0.0100	R	3.00	3.00	1.00	36.21	12.07		0.0130	0.75	7.07	5.12	0.41	0.00293	0.1222	0.0815	0.5130	1.75	2.47
	Control				R	3.00	3.00	1.00	36.21	12.07											1.75	3.00
300+760	Inlet	36.21	175.00	0.0100	R	2.00	2.00	2.00	18.11	9.05	1.35										1.75	2.70
	Outlet	36.21	175.00	0.0100	R	2.00	2.00	2.00	18.11	9.05		0.0130	0.50	3.14	5.76	0.52	0.00637	0.1547	0.1031	1.1149	1.75	3.12
	Control				R	2.00	2.00	2.00	18.11	9.05											1.75	3.12





# PRELIMINARY CULVERT DESIGN WITH CONSIDERATION OF INLET/OUTLET CONTROL

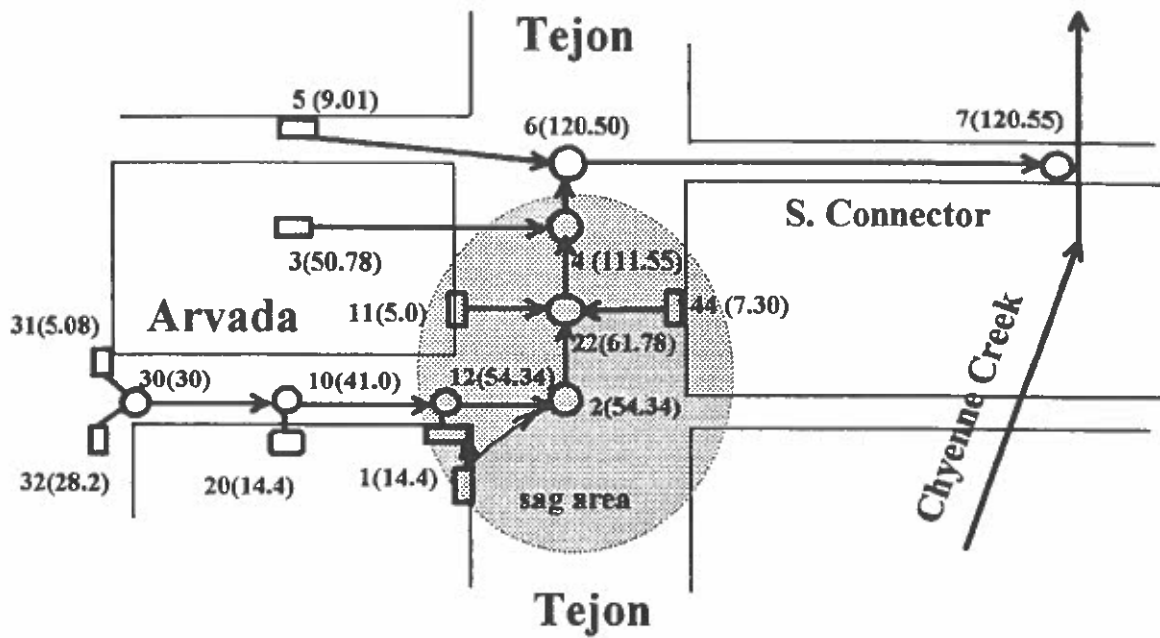
Project: Tejon/Nevada Interchange at 310+160  
 Date: April 1, 1999

## I. Culvert Hydraulics

Culvert ID	Culvert Hydraulic Control	Design Flow cfs	Length ft	Slope ft/ft	Conduit Shape	Dis or Rise ft	Dis or Span ft	Number of Cell	Flow per Cell cfs/ft	Flow per ft cfs/ft	Hw/D Ratio	Manning's N	Hydr. Radius ft	Flow Area sq ft	Flow Vel. fps	Vel. Head ft	Friction Slope ft/ft	Entrance Loss ft	Exit Loss ft	Friction Losses ft	Invert Drop ft	HW
310+160	Inlet	58.59	215.00	0.0100	R	4.00	4.00	1.00	58.59	14.65	0.88										2.15	3.52
	Outlet	58.59	215.00	0.0100	R	4.00	4.00	1.00	58.59	14.65		0.0130	1.00	12.57	4.66	0.34	0.00165	0.1013	0.0675	0.3558	2.15	2.67
	Control				R	4.00	4.00	1.00	58.59	14.65											2.15	3.52
310+160	Inlet	58.59	215.00	0.0100	R	3.50	3.50	1.00	58.59	16.74	1.10										2.15	3.85
	Outlet	58.59	215.00	0.0100	R	3.50	3.50	1.00	58.59	16.74		0.0130	0.88	9.62	6.09	0.58	0.00337	0.1728	0.1152	0.7253	2.15	3.16
	Control				R	3.50	3.50	1.00	58.59	16.74											2.15	3.85
310+160	Inlet	58.59	215.00	0.0100	R	2.00	3.00	2.00	29.30	9.77	0.90										2.15	1.80
	Outlet	58.59	215.00	0.0100	R	2.00	3.00	2.00	29.30	9.77		0.0130	0.50	3.14	9.32	1.35	0.01668	0.4051	0.2700	3.5862	2.15	8.41
	Control				R	2.00	3.00	2.00	29.30	9.77											2.15	8.41



- Storm Sewer Profile Calculations & Inlet Size Chart



Note: 2(54.34) = manhole ID (flowrate in cfs)

Sewer ID id defined as





STORM SEWER SYSTEM DESIGN USING UDSEWER MODEL  
 Developed by Dr. James Guo, Civil Eng. Dept, U. of Colorado at Denver  
 Metro Denver Cities/Counties & UDFCD Pool Fund Study

USER: J F Sato and Associates.....  
 ON DATA 11-04-1999 AT TIME 14:16:58 VERSION=07-15-1995

\*\*\* PROJECT TITLE :Tejon/Nevada Interchange

\*\*\* RETURN PERIOD OF FLOOD IS 10 YEARS

\*\*\* SUMMARY OF HYDRAULICS AT MANHOLES

MANHOLE ID NUMBER	DESIGN PEAK FLOW CFS	GROUND ELEVATION FEET	WATER ELEVATION FEET	COMMENTS
1.00	3.58	5910.20	5906.67	OK
2.00	7.04	5908.90	5906.34	OK
3.00	13.67	5908.90	5905.95	OK
4.00	13.48	5911.20	5905.00	OK
6.00	7.50	5907.82	5906.46	OK
5.00	10.09	5909.60	5906.22	OK
11.00	3.58	5910.23	5906.74	OK
7.00	7.50	5907.28	5906.66	OK
22.00	3.58	5910.23	5906.59	OK

OK MEANS WATER ELEVATION IS LOWER THAN GROUND ELEVATION

\*\*\* SUMMARY OF SEWER HYDRAULICS

NOTE: THE GIVEN FLOW DEPTH-TO-SEWER SIZE RATIO= 1

SEWER ID NUMBER	MANHOLE NUMBER UPSTREAM ID NO.	MANHOLE NUMBER DNSTREAM ID NO.	SEWER SHAPE	REQUIRED DIA(RISE) (IN) (FT)	SUGGESTED DIA(RISE) (IN) (FT)	EXISTING DIA(RISE) (IN) (FT)	WIDTH (FT)
12.00	1.00	2.00	ROUND	13.29	18.00	18.00	0.00
23.00	2.00	3.00	ROUND	17.12	18.00	18.00	0.00
34.00	3.00	4.00	ROUND	25.01	27.00	27.00	0.00
53.00	5.00	3.00	ROUND	22.32	24.00	24.00	0.00
65.00	6.00	5.00	ROUND	19.97	21.00	21.00	0.00
111.00	11.00	1.00	ROUND	13.29	18.00	18.00	0.00
76.00	7.00	6.00	ROUND	19.97	21.00	21.00	0.00
222.00	22.00	2.00	ROUND	13.29	18.00	18.00	0.00

DIMENSION UNITS FOR ROUND AND ARCH SEWER ARE IN INCHES

DIMENSION UNITS FOR BOX SEWER ARE IN FEET

REQUIRED DIAMETER WAS DETERMINED BY SEWER HYDRAULIC CAPACITY.

SUGGESTED DIAMETER WAS DETERMINED BY COMMERCIALY AVAILABLE SIZE.

FOR A NEW SEWER, FLOW WAS ANALYZED BY THE SUGGESTED SEWER SIZE; OTHERWISE,  
 EXISITNG SIZE WAS USED

SEWER ID NUMBER	DESIGN FLOW Q CFS	FLOW FULL Q CFS	NORMAL DEPTH FEET	NORAML VLCITY FPS	CRITIC DEPTH FEET	CRITIC VLCITY FPS	FULL VLCITY FPS	FROUDE NO.	COMMENT
12.0	3.6	8.1	0.70	4.43	0.75	4.08	2.03	1.06	V-OK
23.0	7.0	8.1	1.08	5.15	1.03	5.46	3.98	0.90	V-OK
34.0	13.7	16.8	1.54	4.71	1.28	5.83	3.44	0.71	V-OK
53.0	10.1	12.3	1.38	4.37	1.14	5.47	3.21	0.69	V-OK
65.0	7.5	8.6	1.26	4.03	1.01	5.20	3.12	0.65	V-OK
111.0	3.6	8.1	0.70	4.43	0.75	4.08	2.03	1.06	V-OK
76.0	7.5	8.6	1.26	4.03	1.01	5.20	3.12	0.65	V-OK
222.0	3.6	8.1	0.70	4.43	0.75	4.08	2.03	1.06	V-OK

FROUDE NUMBER=0 INDICATES THAT A PRESSURED FLOW OCCURS

SEWER ID NUMBER	SLOPE %	INVERT ELEVATION UPSTREAM (FT)	INVERT ELEVATION DNSTREAM (FT)	BURIED DEPTH UPSTREAM (FT)	BURIED DEPTH DNSTREAM (FT)	COMMENTS
12.00	0.50	5904.37	5903.64	4.33	3.76	OK
23.00	0.50	5903.44	5903.16	3.96	4.24	OK
34.00	0.25	5903.03	5902.83	3.62	6.12	OK
53.00	0.25	5903.34	5903.21	4.26	3.69	OK
65.00	0.25	5903.63	5903.32	2.44	4.53	OK
111.00	0.50	5904.73	5904.57	4.00	4.13	OK
76.00	0.25	5903.77	5903.61	2.01	2.71	OK
222.00	0.50	5904.37	5904.21	4.36	3.19	OK

OK MEANS BURIED DEPTH IS GREATER THAN REQUIRED SOIL COVER OF 2 FEET

\*\*\* SUMMARY OF HYDRAULIC GRADIENT LINE ALONG SEWERS

SEWER ID NUMBER	SEWER LENGTH FEET	SURCHARGED LENGTH FEET	CROWN ELEVATION		WATER ELEVATION		FLOW CONDITION
			UPSTREAM FEET	DNSTREAM FEET	UPSTREAM FEET	DNSTREAM FEET	
12.00	145.96	145.96	5905.87	5905.14	5906.67	5906.34	PRSS'ED
23.00	55.10	55.10	5904.94	5904.66	5906.34	5906.95	PRSS'ED
34.00	81.34	81.34	5905.28	5905.08	5906.95	5906.00	PRSS'ED
53.00	53.14	53.14	5905.34	5905.21	5906.22	5906.95	PRSS'ED
65.00	124.64	124.64	5905.38	5905.07	5906.46	5906.22	PRSS'ED
111.00	32.80	32.80	5906.23	5906.07	5906.74	5906.67	PRSS'ED
76.00	65.60	65.60	5905.52	5905.36	5906.66	5906.46	PRSS'ED
222.00	32.00	32.00	5905.87	5905.71	5906.59	5906.34	PRSS'ED

PRSS'ED=PRESSURED FLOW; JUMP=POSSIBLE HYDRAULIC JUMP; SUBCR=SUBCRITICAL FLOW

\*\*\* SUMMARY OF ENERGY GRADIENT LINE ALONG SEWERS

SEWER ID NO	UPST MANHOLE ID NO	SEWER ELEV FT	ENERGY FT	FRICTION FT	BEND K COEF	JUNCTURE LOSSES			DOWNST MANHOLE ID	SEWER ELEV FT
						BEND LOSS FT	LATERAL LOSS FT	LATERAL LOSS FT		
12.0	1.00	5906.74	0.14	0.05	0.00	0.00	0.00	2.00	5906.59	
23.0	2.00	5906.59	0.21	1.00	0.25	0.00	0.00	3.00	5906.13	
34.0	3.00	5906.13	0.13	0.05	0.00	0.00	0.00	4.00	5906.00	
53.0	5.00	5906.38	0.09	0.05	0.01	0.25	0.14	3.00	5906.13	
65.0	6.00	5906.61	0.24	0.00	0.00	0.00	0.00	5.00	5906.38	
111.0	11.00	5906.80	0.03	0.50	0.03	0.00	0.00	1.00	5906.74	
76.0	7.00	5906.81	0.12	0.50	0.08	0.00	0.00	6.00	5906.61	
222.0	22.00	5906.65	0.03	0.50	0.03	0.00	0.00	2.00	5906.59	

BEND LOSS = BEND K \* FLOWING FULL VHEAD IN SEWER.  
 LATERAL LOSS = OUTFLOW FULL VHEAD - JCT LOSS K \* INFLOW FULL VHEAD  
 FRICTION LOSS = 0 MEANS IT IS NEGLIGIBLE OR POSSIBLE ERROR DUE TO JUMP.  
 FRICTION LOSS INCLUDES SEWER INVERT DROP AT MANHOLE  
 NOTICE: VHEAD DENOTES THE VELOCITY HEAD OF FULL FLOW CONDITION.  
 A MINIMUM JUNCTION LOSS OF 0.05 FT WOULD BE INTRODUCED UNLESS LATERAL K=0.  
 FRICTION LOSS WAS ESTIMATED BY BACKWATER CURVE COMPUTATIONS.

\*\*\* SUMMARY OF EARTH EXCAVATION VOLUME FOR COST ESTIMATE.

THE TRENCH SIDE SLOPE = 1

MANHOLE ID NUMBER	GROUND ELEVATION FT	INVERT ELEVATION FT	MANHOLE HEIGHT FT
1.00	5910.20	5904.37	5.83
2.00	5908.90	5903.44	5.46
3.00	5908.90	5903.03	5.87
4.00	5911.20	5902.83	8.37
6.00	5907.82	5903.61	4.21
5.00	5909.60	5903.32	6.28
11.00	5910.23	5904.73	5.50
7.00	5907.28	5903.77	3.51
22.00	5910.23	5904.37	5.86

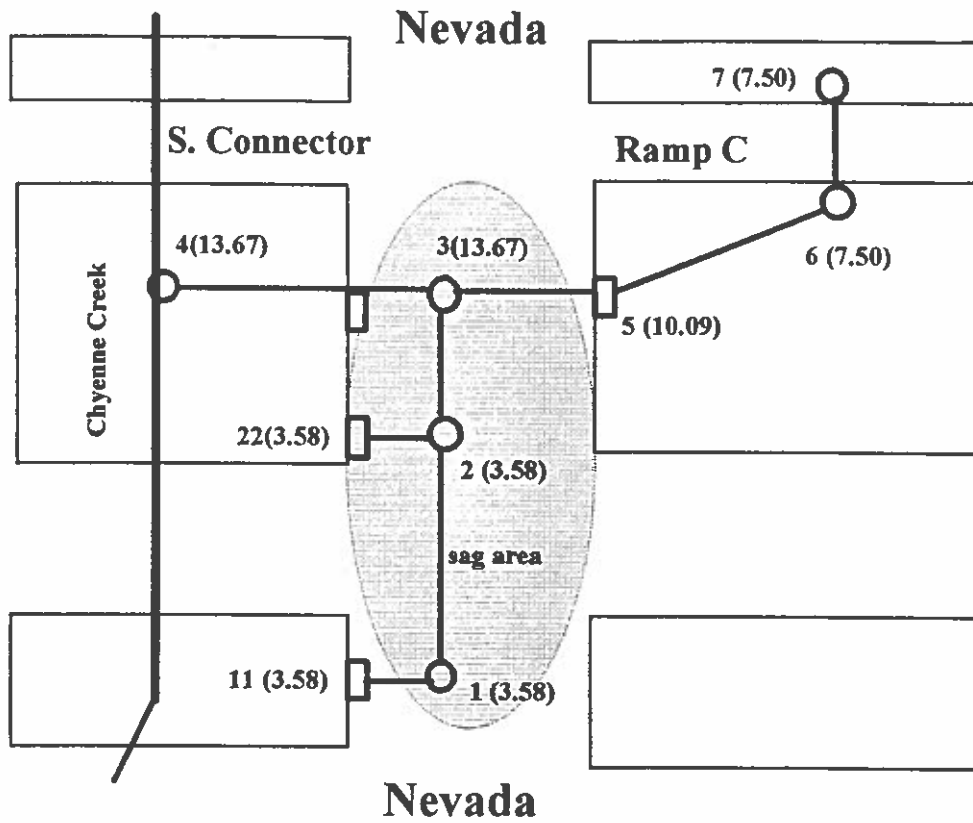
SEWER ID NUMBER	UPST TRENCH WIDTH ON GROUND AT INVERT FT	DNST TRENCH WIDTH ON GROUND AT INVERT FT	TRENCH LENGTH FT	WALL THICKNESS INCHES	EARTH VOLUME CUBIC YD
12.00	11.74	3.92	10.60	3.92	145.96
23.00	11.00	3.92	11.55	3.92	55.10
34.00	10.95	4.79	15.96	4.79	81.34
53.00	12.02	4.50	10.89	4.50	53.14
65.00	8.17	4.21	12.36	4.21	124.64
111.00	11.08	3.92	11.35	3.92	32.80
76.00	6.81	4.21	8.22	4.21	65.60
222.00	11.80	3.92	9.46	3.92	32.00

TOTAL EARTH VOLUME FOR SEWER TRENCHES = 870.2893 CUBIC YARDS

EARTH VOLUME WAS ESTIMATED TO HAVE

BOTTOM WIDTH = DIAMETER OR WIDTH OF SEWER + 2 \* B  
 B = ONE FOOT WHEN DIAMETER OR WIDTH <= 48 INCHES  
 B = TWO FEET WHEN DIAMETER OR WIDTH > 48 INCHES  
 IF BOTTOM WIDTH < MINIMUM WIDTH, 2 FT, THE MINIMUM WIDTH WAS USED.

BACKFILL DEPTH UNDER SEWER WAS ASSUMED TO BE ONE FOOT  
SEWER WALL THICKNESS=EQIVLNT DIAMATER IN INCH/12 +1 IN INCHES  
ED.  
BACKFILL DEPTH UNDER SEWER WAS ASSUMED TO BE ONE



Note: 1(3.58) = manhole ID (flowrate in cfs)

Inlets for Manholes 1, 2, and 3 are placed at low points for the same design capacity.

Sewer ID number is defined as



STORM SEWER SYSTEM DESIGN USING UDSEWER MODEL  
 Developed by Dr. James Guo, Civil Eng. Dept, U. of Colorado at Denver  
 Metro Denver Cities/Counties & UDFCO Pool Fund Study

USER: J F Sato and Associates.....  
 ON DATA 11-04-1999 AT TIME 11:51:49 VERSION=07-15-1995

\*\*\* PROJECT TITLE :Sewer System for Tejon/Arvada 10 flood

\*\*\* SUMMARY OF HYDRAULICS AT MANHOLES

MANHOLE ID NUMBER	DESIGN PEAK FLOW CFS	GROUND ELEVATION FEET	WATER ELEVATION FEET	COMMENTS
7.00	120.50	5908.80	5906.00	OK
6.00	120.50	5914.80	5907.69	OK
4.00	111.56	5914.20	5910.09	OK
22.00	61.89	5912.30	5911.35	OK
2.00	54.34	5912.30	5911.86	OK
1.00	5.35	5912.30	5912.27	OK
5.00	9.01	5912.20	5909.30	OK
3.00	50.78	5913.80	5911.42	OK
11.00	10.00	5912.50	5911.95	OK
44.00	7.30	5912.50	5911.86	OK
10.00	41.00	5914.20	5913.09	OK
20.00	14.40	5914.20	5913.57	OK
30.00	30.00	5914.90	5914.02	OK
12.00	54.30	5912.80	5912.05	OK
13.00	11.70	5912.90	5912.62	OK
31.00	28.20	5914.90	5914.14	OK
32.00	5.00	5914.90	5914.22	OK

OK MEANS WATER ELEVATION IS LOWER THAN GROUND ELEVATION

\*\*\* SUMMARY OF SEWER HYDRAULICS

NOTE: THE GIVEN FLOW DEPTH-TO-SEWER SIZE RATIO= 1

SEWER ID NUMBER	MANHOLE UPSTREAM ID NO.	MANHOLE DNSTREAM ID NO.	SEWER SHAPE	REQUIRED DIA(RISE) (IN) (FT)	SUGGESTED DIA(RISE) (IN) (FT)	EXISTING DIA(RISE) (IN) (FT)	EXISTING WIDTH (FT)
67.00	6.00	7.00	ROUND	50.66	54.00	54.00	0.00
46.00	4.00	6.00	ROUND	50.32	54.00	54.00	0.00
224.00	22.00	4.00	ROUND	40.34	42.00	48.00	0.00
222.00	2.00	22.00	ROUND	38.42	42.00	48.00	0.00
12.00	1.00	2.00	ROUND	15.45	18.00	18.00	0.00
56.00	5.00	6.00	ROUND	18.78	21.00	24.00	0.00
34.00	3.00	4.00	ROUND	31.54	33.00	36.00	0.00
1122.00	11.00	22.00	ROUND	17.15	18.00	18.00	0.00
4422.00	44.00	22.00	ROUND	15.24	18.00	18.00	0.00
2010.00	20.00	10.00	ROUND	19.66	21.00	24.00	0.00
3010.00	30.00	10.00	ROUND	35.02	36.00	36.00	0.00
1012.00	10.00	12.00	ROUND	32.57	33.00	36.00	0.00
122.00	12.00	2.00	ROUND	38.41	42.00	42.00	0.00
1312.00	13.00	12.00	ROUND	18.19	21.00	24.00	0.00
3130.00	31.00	30.00	ROUND	25.30	27.00	27.00	0.00
3230.00	32.00	30.00	ROUND	15.06	18.00	18.00	0.00

DIMENSION UNITS FOR ROUND AND ARCH SEWER ARE IN INCHES  
 DIMENSION UNITS FOR BOX SEWER ARE IN FEET  
 REQUIRED DIAMETER WAS DETERMINED BY SEWER HYDRAULIC CAPACITY.  
 SUGGESTED DIAMETER WAS DETERMINED BY COMMERCIALY AVAILABLE SIZE.  
 FOR A NEW SEWER, FLOW WAS ANALYZED BY THE SUGGESTED SEWER SIZE; OTHERWISE,  
 EXISITNG SIZE WAS USED

SEWER ID NUMBER	DESIGN FLOW Q CFS	FLOW FULL Q CFS	NORMAL DEPTH FEET	NORAML VLOCITY FPS	CRITIC DEPTH FEET	CRITIC VLOCITY FPS	FULL VLOCITY FPS	FROUDE NO.	COMMENT
67.0	120.5	143.3	3.16	10.10	3.19	10.01	7.58	1.05	V-OK
46.0	111.6	135.1	3.12	9.49	3.19	9.27	7.01	0.99	V-OK
224.0	61.9	98.7	2.30	8.30	2.37	8.00	4.93	1.06	V-OK
222.0	54.3	98.7	2.12	8.05	2.22	7.59	4.32	1.09	V-OK
12.0	5.3	8.1	0.89	4.88	0.89	4.91	3.03	1.00	V-OK
56.0	9.0	17.4	1.02	5.58	1.08	5.22	2.87	1.10	V-OK
34.0	50.8	72.5	1.85	11.10	2.32	8.66	7.18	1.56	V-OK
1122.0	10.0	11.4	1.09	7.28	1.22	6.52	5.66	1.27	V-OK
4422.0	7.3	11.4	0.87	6.85	1.06	5.46	4.13	1.42	V-OK
2010.0	14.4	24.6	1.10	8.13	1.37	6.30	4.58	1.52	V-OK
3010.0	30.0	32.4	2.28	5.20	1.77	6.91	4.24	0.61	V-OK



1012.0	41.0	53.7	1.96	8.37	2.12	7.66	5.80	1.13	V-OK
122.0	54.3	69.1	2.34	7.96	2.30	8.10	5.64	0.97	V-OK
1312.0	11.7	24.6	0.97	7.72	1.22	5.81	3.72	1.56	V-OK
3130.0	28.2	33.6	1.58	9.48	1.84	8.10	7.09	1.39	V-OK
3230.0	5.0	8.1	0.85	4.81	0.86	4.77	2.83	1.01	V-OK

FROUDE NUMBER=0 INDICATES THAT A PRESSURED FLOW OCCURS

SEWER ID NUMBER	SLOPE %	INVERT ELEVATION		BURIED DEPTH		COMMENTS
		UPSTREAM (FT)	DNSTREAM (FT)	UPSTREAM (FT)	DNSTREAM (FT)	
67.00	0.45	5904.50	5902.23	5.80	2.07	OK
46.00	0.40	5904.90	5904.68	4.80	5.62	OK
224.00	0.40	5905.54	5905.08	2.76	5.12	OK
222.00	0.40	5906.00	5905.67	2.30	2.63	OK
12.00	0.50	5908.80	5908.36	2.00	2.44	OK
56.00	0.50	5905.40	5904.72	4.80	8.08	OK
34.00	1.00	5906.00	5904.85	4.80	6.35	OK
1122.00	1.00	5906.40	5906.11	4.60	4.69	OK
4422.00	1.00	5906.20	5905.56	4.80	5.24	OK
2010.00	1.00	5908.40	5908.07	3.80	4.13	OK
3010.00	0.20	5909.20	5908.40	2.70	2.80	OK
1012.00	0.55	5908.00	5906.16	3.20	3.64	OK
122.00	0.40	5906.50	5906.25	2.80	2.55	OK
1312.00	1.00	5906.90	5906.57	4.00	4.23	OK
3130.00	1.00	5909.65	5909.32	3.00	3.33	OK
3230.00	0.50	5909.70	5909.58	3.70	3.82	OK

OK MEANS BURIED DEPTH IS GREATER THAN REQUIRED SOIL COVER OF 2 FEET

\*\*\* SUMMARY OF HYDRAULIC GRADIENT LINE ALONG SEWERS

SEWER ID NUMBER	SEWER LENGTH FEET	SURCHARGED LENGTH FEET	CROWN ELEVATION		WATER ELEVATION		FLOW CONDITION
			UPSTREAM FEET	DNSTREAM FEET	UPSTREAM FEET	DNSTREAM FEET	
67.00	505.10	0.00	5909.00	5906.73	5907.69	5906.00	JUMP
46.00	55.40	55.40	5909.40	5909.18	5910.09	5907.69	PRSS'ED
224.00	114.80	114.80	5909.54	5909.08	5911.35	5910.09	PRSS'ED
222.00	83.00	83.00	5910.00	5909.67	5911.86	5911.35	PRSS'ED
12.00	87.90	87.90	5910.30	5909.86	5912.27	5911.86	PRSS'ED
56.00	135.10	135.10	5907.40	5906.72	5909.30	5907.69	PRSS'ED
34.00	114.80	114.80	5909.00	5907.85	5911.42	5910.09	PRSS'ED
1122.00	28.54	28.54	5907.90	5907.61	5911.95	5911.35	PRSS'ED
4422.00	64.00	64.00	5907.70	5907.06	5911.86	5911.35	PRSS'ED
2010.00	32.80	32.80	5910.40	5910.07	5913.57	5913.09	PRSS'ED
3010.00	398.50	398.50	5912.20	5911.40	5914.02	5913.09	PRSS'ED
1012.00	334.50	334.50	5911.00	5909.16	5913.09	5912.05	PRSS'ED
122.00	62.00	62.00	5910.00	5909.75	5912.05	5911.86	PRSS'ED
1312.00	33.00	33.00	5908.90	5908.57	5912.62	5912.05	PRSS'ED
3130.00	32.80	32.80	5911.90	5911.57	5914.14	5914.02	PRSS'ED
3230.00	24.60	24.60	5911.20	5911.08	5914.22	5914.02	PRSS'ED

PRSS'ED=PRESSURED FLOW; JUMP=POSSIBLE HYDRAULIC JUMP; SUBCR=SUBCRITICAL FLOW

\*\*\* SUMMARY OF ENERGY GRADIENT LINE ALONG SEWERS

SEWER ID NO	UPST MANHOLE ID NO	SEWER ELEV FT	ENERGY FRCTION FT	BEND K COEF	JUNCTURE LOSSES				DOWNST MANHOLE ID	MANHOLE ENERGY FT
					BEND LOSS FT	LATERAL LOSS FT	LATERAL LOSS FT	LATERAL LOSS FT		
67.0	6.00	5909.24	3.24	0.00	0.00	0.00	0.00	7.00	5906.00	
46.0	4.00	5910.86	0.15	1.00	0.76	0.25	0.70	6.00	5909.24	
224.0	22.00	5911.73	0.18	0.05	0.02	0.25	0.67	4.00	5910.86	
222.0	2.00	5912.15	0.10	0.05	0.01	0.25	0.30	22.00	5911.73	
12.0	1.00	5912.41	0.19	0.50	0.07	0.00	0.00	2.00	5912.15	
56.0	5.00	5909.43	0.18	0.05	0.01	0.00	0.00	6.00	5909.24	
34.0	3.00	5912.22	0.56	1.00	0.80	0.00	0.00	4.00	5910.86	
1122.0	11.00	5912.44	0.22	1.00	0.50	0.00	0.00	22.00	5911.73	
4422.0	44.00	5912.12	0.26	0.50	0.13	0.00	0.00	22.00	5911.73	
2010.0	20.00	5913.89	0.11	0.50	0.16	0.00	0.00	10.00	5913.62	
3010.0	30.00	5914.30	0.68	0.00	0.00	0.00	0.00	10.00	5913.62	
1012.0	10.00	5913.62	1.07	0.00	0.00	0.00	0.00	12.00	5912.55	
122.0	12.00	5912.55	0.15	0.50	0.25	0.00	0.00	2.00	5912.15	
1312.0	13.00	5912.84	0.07	1.00	0.22	0.00	0.00	12.00	5912.55	
3130.0	31.00	5914.92	0.23	0.50	0.39	0.00	0.00	30.00	5914.30	
3230.0	32.00	5914.35	0.05	0.00	0.00	0.00	0.00	30.00	5914.30	

BEND LOSS =BEND K\* FLOWING FULL VHEAD IN SEWER.  
LATERAL LOSS= OUTFLOW FULL VHEAD-JCT LOSS K\*INFLOW FULL VHEAD

FRICTION LOSS=0 MEANS IT IS NEGLIGIBLE OR POSSIBLE ERROR DUE TO JUMP.  
 FRICTION LOSS INCLUDES SEWER INVERT DROP AT MANHOLE  
 NOTICE: VHEAD DENOTES THE VELOCITY HEAD OF FULL FLOW CONDITION.  
 A MINIMUM JUNCTION LOSS OF 0.05 FT WOULD BE INTRODUCED UNLESS LATERAL K=0.  
 FRICTION LOSS WAS ESTIMATED BY BACKWATER CURVE COMPUTATIONS.

\*\*\* SUMMARY OF EARTH EXCAVATION VOLUME FOR COST ESTIMATE.

THE TRENCH SIDE SLOPE = 1

MANHOLE ID NUMBER	GROUND ELEVATION FT	INVERT ELEVATION FT	MANHOLE HEIGHT FT
7.00	5908.80	5902.23	6.57
6.00	5914.80	5904.50	10.30
4.00	5914.20	5904.85	9.35
22.00	5912.30	5905.54	6.76
2.00	5912.30	5906.00	6.30
1.00	5912.30	5908.80	3.50
5.00	5912.20	5905.40	6.80
3.00	5913.80	5906.00	7.80
11.00	5912.50	5906.40	6.10
44.00	5912.50	5906.20	6.30
10.00	5914.20	5908.00	6.20
20.00	5914.20	5908.40	5.80
30.00	5914.90	5909.20	5.70
12.00	5912.80	5906.16	6.64
13.00	5912.90	5906.90	6.00
31.00	5914.90	5909.65	5.25
32.00	5914.90	5909.70	5.20

SEWER ID NUMBER	UPST ON GROUND FT	TRENCH WIDTH AT INVERT FT	DNST ON GROUND FT	TRENCH WIDTH AT INVERT FT	TRENCH LENGTH FT	WALL THICKNESS INCHES	EARTH VOLUME CUBIC YD
67.00	19.18	9.42	11.73	9.42	505.10	5.50	1897.8
46.00	17.18	9.42	18.83	9.42	55.40	5.50	245.1
224.00	10.69	6.83	15.40	6.83	114.80	5.00	306.7
222.00	9.77	6.83	10.43	6.83	83.00	5.00	165.1
12.00	7.08	3.92	7.96	3.92	87.90	2.50	70.9
56.00	13.10	4.50	19.65	4.50	135.10	3.00	402.3
34.00	13.93	5.67	17.03	5.67	114.80	4.00	335.6
1122.00	12.28	3.92	12.45	3.92	28.54	2.50	48.4
4422.00	12.68	3.92	13.56	3.92	64.00	2.50	120.2
2010.00	11.10	4.50	11.76	4.50	32.80	3.00	52.7
3010.00	9.73	5.67	9.93	5.67	398.50	4.00	628.4
1012.00	10.73	5.67	11.61	5.67	334.50	4.00	615.4
122.00	10.35	6.25	9.85	6.25	62.00	4.50	111.5
1312.00	11.50	4.50	11.96	4.50	33.00	3.00	55.1
3130.00	9.71	4.79	10.36	4.79	32.80	3.25	45.7
3230.00	10.48	3.92	10.73	3.92	24.60	2.50	32.5

TOTAL EARTH VOLUME FOR SEWER TRENCHES = 5133.6 CUBIC YARDS

EARTH VOLUME WAS ESTIMATED TO HAVE

BOTTOM WIDTH=DIAMETER OR WIDTH OF SEWER + 2 \* B

B=ONE FEET WHEN DIAMETER OR WIDTH <=48 INCHES

B=TWO FEET WHEN DIAMETER OR WIDTH >48 INCHES

IF BOTTOM WIDTH < MINIMUM WIDTH, 2 FT, THE MINIMUM WIDTH WAS USED.

BACKFILL DEPTH UNDER SEWER WAS ASSUMED TO BE ONE FOOT

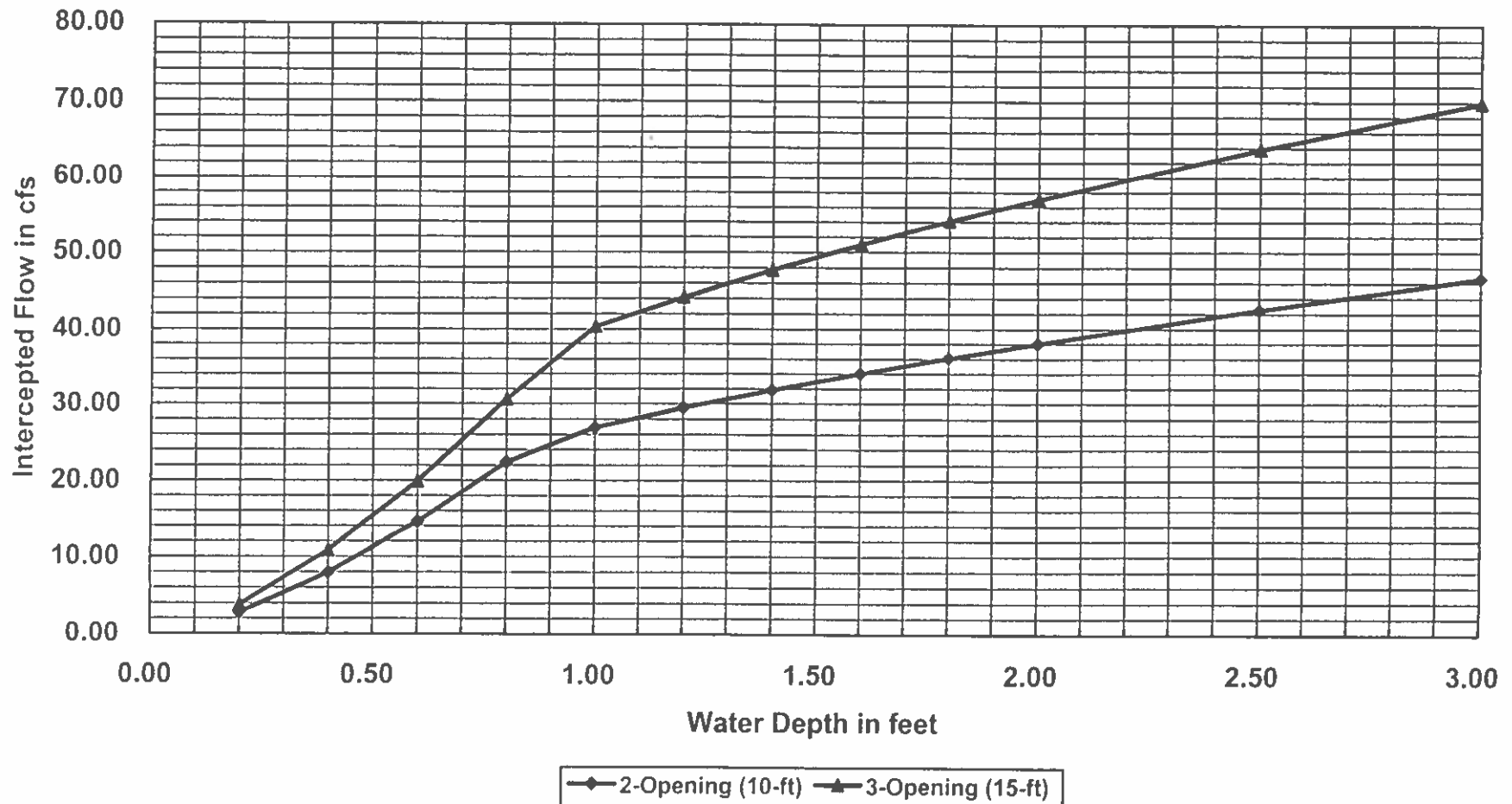
SEWER WALL THICKNESS=EQUIV. DIA. IN INCH/12 +1 IN INCHES

USED.

BACKFILL DEPTH UNDER SEWER WAS ASSUMED TO BE ONE FOOT

SEWER WALL THICKNESS=EQUIV. DIA. IN INCH/12 +1 IN INCHES

Curb Opening in a Sump  
Depth of Six Inches for Nevada/Tejon Project



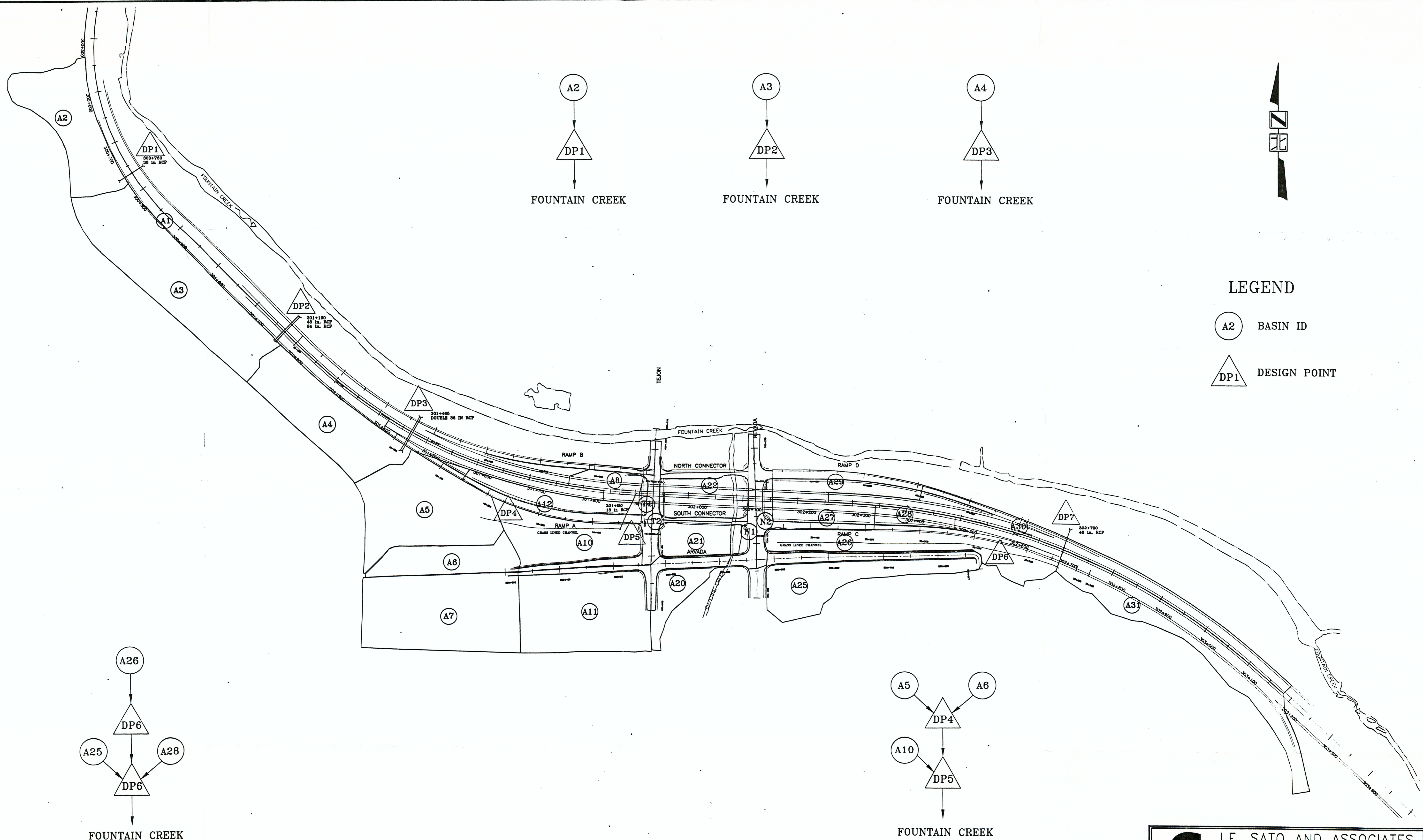
## Curb Opening in a Sump

Curb Opening            L=            5 ft  
 Curb Height            H=            0.5 ft  
 Pan Width                W=            2 ft

Weir                       $Q=2.3 (L+1.8*W)Y^{1.5}$   
 Orifice                    $Q=0.67 HL (64.4Y)^{0.5}$

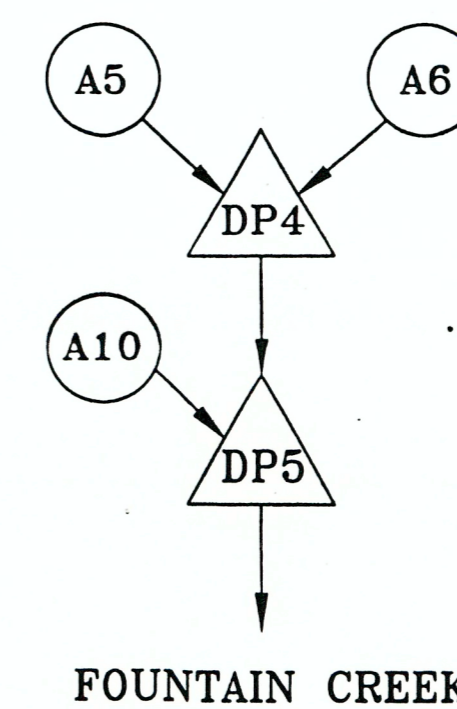
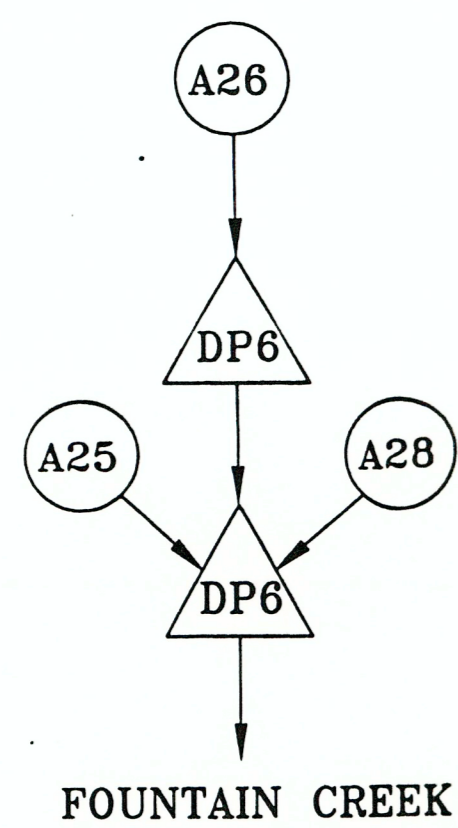
No of Curb Opening	Net Area sq ft	Perimeter ft
1	2.5	8.6
2	5	13.6
3	7.5	18.6

Water Depth ft	1-opening Q cfs	2-opening Q cfs	3-opening Q cfs
0.20	1.77	2.80	3.83
0.40	5.00	7.91	10.82
0.60	9.19	14.54	19.88
0.80	12.02	22.38	30.61
1.00	13.44	26.88	40.33
1.20	14.72	29.45	44.17
1.40	15.90	31.81	47.71
1.60	17.00	34.01	51.01
1.80	18.03	36.07	54.10
2.00	19.01	38.02	57.03
2.50	21.25	42.51	63.76
3.00	23.28	46.56	69.85



LEGEND

- A2 BASIN ID
- DP1 DESIGN POINT



**J.F. SATO AND ASSOCIATES**  
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 Project Managers, Planners & Surveyors  
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EXHIBIT 1  
 NEVADA/TEJON INTERCHANGE  
 DRAINAGE BASINS

