

Return to  
Tim MITROS

DRAINAGE MEMORANDUM FOR  
PIKES PEAK COMMUNITY COLLEGE  
NORTH CAMPUS  
COLORADO SPRINGS, COLORADO  
EL PASO COUNTY

October 7, 1996

RETURN WITHIN 2 WEEKS TO:  
CITY OF COLORADO SPRINGS  
SUBDIVISION ENGINEERING  
30 SOUTH NEVADA AVE., SUITE 702  
COLORADO SPRINGS, CO 80903  
(719) 385-5979

---

**URS Greiner**

**DRAINAGE MEMORANDUM FOR  
PIKES PEAK COMMUNITY COLLEGE  
NORTH CAMPUS  
COLORADO SPRINGS, COLORADO  
EL PASO COUNTY**

**October 7, 1996**

**Prepared for:  
DAVIS PARTNERSHIP, P.C.  
1175 Sherman Street, Suite 3100  
DENVER, CO 80203-3027**

**Prepared by:  
URS CONSULTANTS, INC.  
1040 S. 8TH STREET, SUITE 100  
COLORADO SPRINGS, CO 80906**

**URS PROJECT NO. 67.42154**

# Drainage Memorandum for Pikes Peak Community College North Campus

## I. GENERAL LOCATION AND PROPERTY DESCRIPTION

The Pikes Peak Community College (PPCC) North Campus is located along the northern Colorado Springs city limits. The site is bounded to the north by state highway 83 (SH-83), proposed Fairlane Technology Park to the south, New Life Church to the west, and unplatted land to the east. Other development within proximity to the site include the International Bible Society in the Northgate Development to the north.

The site is located within the northwest 1/4 of Section 21, Township 12 south, Range 67 west and consists of approximately 75 acres as shown on Figure 1. Planned development consists of a 121,000 sqft building on a 60,000 sqft footprint. Full development of the site is not currently known.

The terrain is generally flat with gentle slopes ranging between 1% to 2% from the northeast to the southwest. A high point is located at the center of the property extending from near the northern property line. The vegetation is typical eastern Colorado prairie grasses with no shrubs. There are no well defined drainages on the property. Runoff generally sheet flows through the property before being intercepted by drainage ditches located outside of the property.

The site and surrounding areas have soil characteristics of Hydrologic Soil group A with isolated areas having characteristics of Hydrologic Soil Group B as classified by the Soil Conservation Service.

There are no irrigation facilities, utilities, or other encumbrances that affect the drainage analysis.

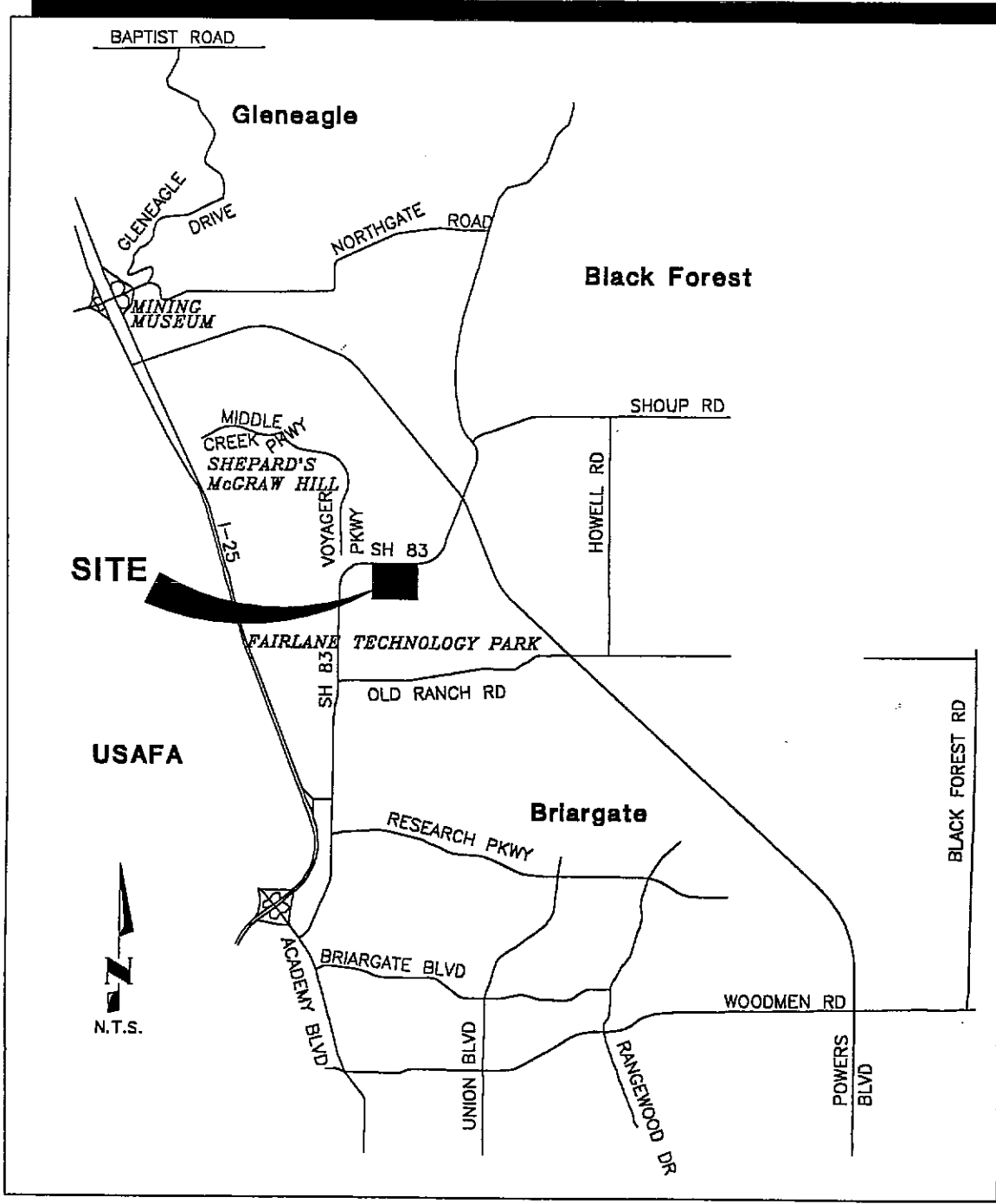
No portion of this site is located within a designated FEMA Floodplain.

## II. DRAINAGE BASINS AND SUB-BASINS

The following report was used as a reference in developing this Drainage Memorandum:

Title: Fairlane Technology Park  
Master Development Drainage Report  
Date: October 22, 1993, Revised January 6, 1994  
Owner: Ford Colorado Properties  
Engineer: URS Consultants, Inc.

This report makes certain assumptions that would require the implementation of proposed regional detention facilities based on the then current 10 year and 100 year design storms. To this date, improvements as discussed in the MDDP have been minimal in regards to the immediate area around the proposed site. Detention pond "A" has been constructed southwest of the site, north of



VICINITY MAP

FIG1.DWG RJS 09/05/96

**URS**  
 CONSULTANTS, INC.  
 COLORADO SPRINGS, COLORADO

PROJ NO. 67.42154

PIKES PEAK COMMUNITY COLLEGE  
 NORTH CAMPUS BUILDING

FIGURE  
 1

## **Drainage Memorandum for Pikes Peak Community College North Campus**

Old Ranch Road and east of I-25. Detention pond "A" serves the development within the southern portion of Fairlaine Technology Park. Detention pond "B" is proposed east of I-25, west of SH-83 and south of Stout Allen Road. Development that will trigger the need for detention pond "B" is not currently known. Adjacent property owners have constructed on-site detention facilities to meet the historical flow requirements. It is anticipated that improvements to Stout Allen will constitute a need for the proposed pond.

The site is located between the Black Squirrel and Kettle Creek Basins and drains directly into Monument Creek, west of the Air Force Academy property line. Off-site flows as identified in the MDDP were Basin O-1 and O-2. Basin O-1 enters the eastern property line and drains to the south into the Kettle Creek Basin. Basin O-2 is conveyed beneath SH-83 via a 24" corrugated metal pipe (CMP) along the north property line. Flow is intercepted by a roadside ditch traversing along SH-83 to the west.

The 74 acre site was considered as a basin for drainage analysis purposes. Historic and developed flows were analyzed to determine allowable flow release rates from the site. The site was subdivided into sub-basin 1-1 and sub-basin 1-2. Sub-basin 1-1 consists of the developed area of the site, which includes the building and parking facilities. Sub-basin 1-2 largely consists of undeveloped areas not intercepted by a roadside ditch along the access road.

The existing basins lying in and around the proposed development are illustrated in Figures 2 and 3.

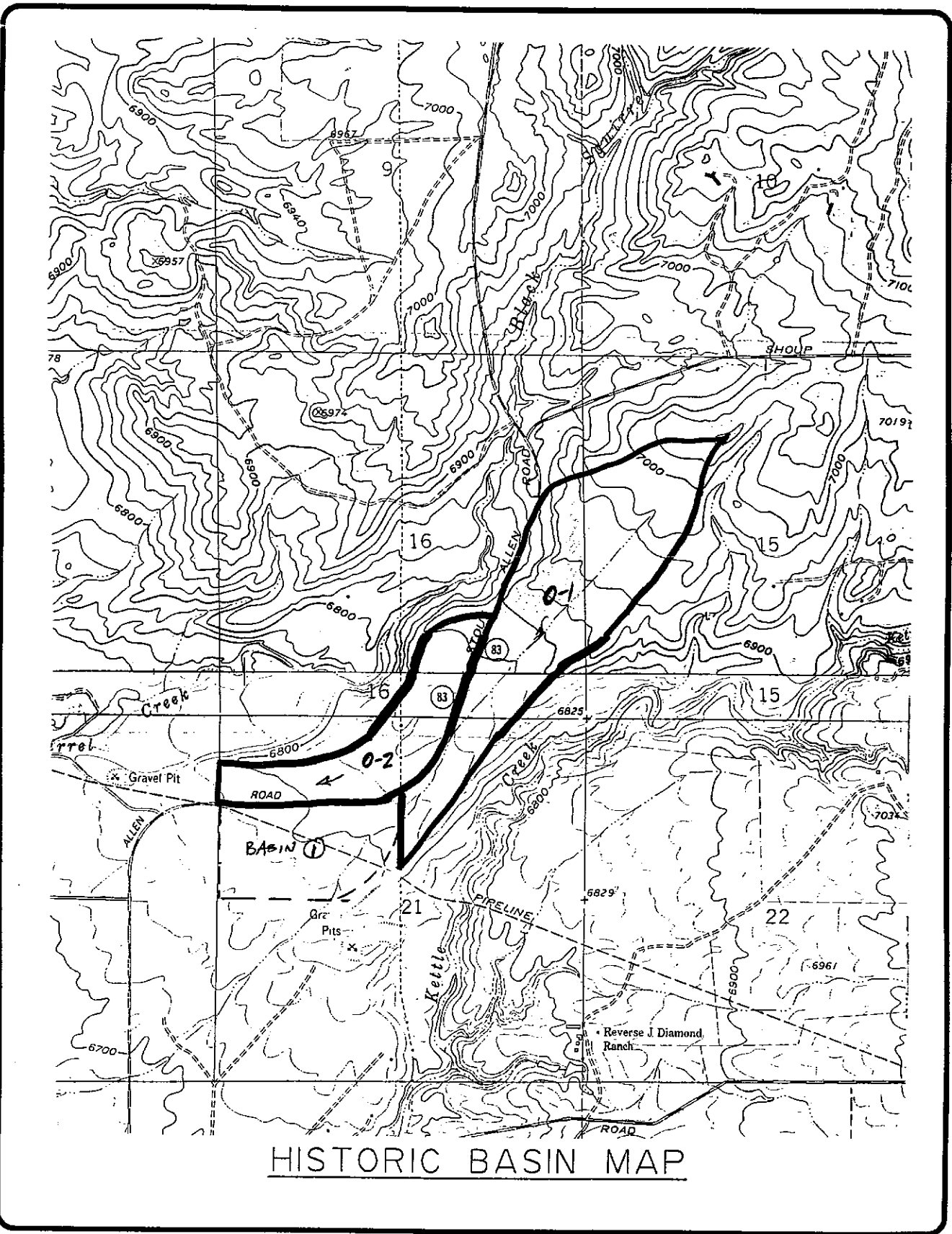
### **III. DRAINAGE DESIGN CRITERIA**

#### **A. SCS Hydrologic Criteria**

Basin areas were calculated using a planimeter on USGS topographic maps and working drawings. Time of concentration was estimated using the SCS procedures described in the Drainage Criteria Manual. Based upon the Drainage Criteria Manual requirement to use type B soil conditions for type A soils after development, the SCS curve number selected from Table 5-5 of the Drainage Criteria Manual for undeveloped conditions was 68 and 75 for developed conditions. The 100-year, 24 hour storm rainfall intensity selected from the NOAA isopluvial map in Figure 5-4e from the Drainage Criteria Manual was 4.4 inches per hour. The 5-year, 24 hour storm rainfall intensity selected from the NOAA isopluvial maps was 2.6 inches per hour.

The HEC-1 computer model results and SCS calculations are located in the Appendix.

Peak design flows are also shown on the drainage design drawing and tabulated in Table 1.



HISTORIC BASIN MAP

FIG.DWG RJS 09/05/96

**URS**  
CONSULTANTS, INC.  
COLORADO SPRINGS, COLORADO

PIKES PEAK COMMUNITY COLLEGE  
NORTH CAMPUS BUILDING

FIGURE







2

PROJ NO. 67.42154

PIKES PEAK COMMUNITY COLLEGE  
NORTH CAMPUS BUILDING

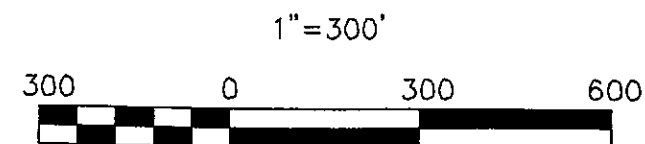
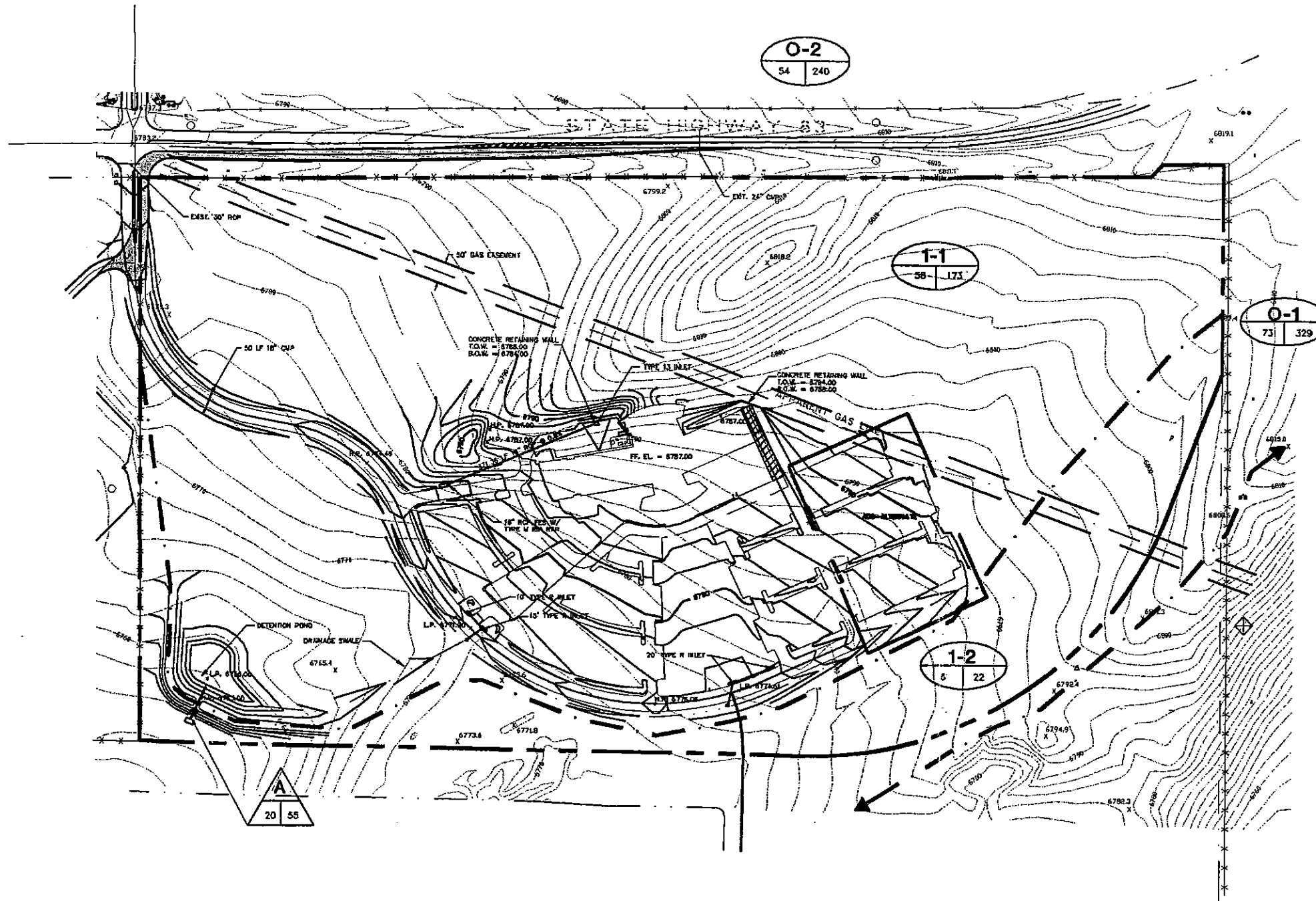
DEVELOPED DRAINAGE  
BASIN MAP

LEGEND

	BASIN NO.
	DESIGN POINT
	SITE BASIN BOUNDARY
	SITE SUB-BASIN/OFF SITE-BASIN
	EXISTING CONTOURS
	PROPOSED CONTOURS

**URS**  
CONSULTANTS, INC.  
PROJ. NO. 67.42154

FIGURE 3



P:\1000\67.42154\67.42154.dwg RJS 09/03/96

# Drainage Memorandum for Pikes Peak Community College North Campus

Table 1  
Summary of Basin Flows

Basin No.	Historic	Developed	Flow	% Change
	Q5	Q5	(+) increase	(+) increase
	Q100	Q100	(-) decrease	(-) decrease
	(cfs)	(cfs)	(cfs)	
O-1	73	n/a	n/a	n/a
	329	n/a	n/a	n/a
O-2	54	n/a	n/a	n/a
	240	n/a	n/a	n/a
Basin 1	37	63	26	70.3 %
	147	196	49	33.3 %
Sub-basin 1-1	31	58	27	87.1 %
	124	173	49	39.5 %
Sub-basin 1-2	6	n/a	n/a	n/a
	22	n/a	n/a	n/a
Sub-basin 1-1* (Design Pt. A)	31	20	-11	-35.5 %
	124	55	-69	-55.6 %
Sub-basin 1-1 (+) 1-2	37	26	-11	-29.7 %
	146	77	-69	-47.3 %

\* Denotes HEC-1 Run w/ Detention Pond

## B. Detention Ponds

An iterative process utilizing HEC-1 detention pond routing was used to size the required detention pond facilities. Release rates from the detention pond (sub-basin 1-1) when combined with historic flows from sub-basin 1-2 was maintained below historic levels for the site basin 1.

## III. Drainage Facility Design

### General

Off-site flows entering the site will continue to follow historic patterns. Proposed development will not alter these drainage patterns. Historic flow patterns within the site will be altered by development. Sub-basin 1-1 will sheetflow through out the basin and will be intercepted by natural drainage ways and roadside ditches located along the internal access road. Flow will be conveyed to the detention pond to release at below historic rates. Sub-basin 1-2 will follow historic patterns and will not be altered. The detention pond will decrease the developed flow leaving the entire site to 26 cubic feet per second (cfs) and 77 cfs for the 5 and 100 year storms, respectively.

### Detention Facilities

A detention pond will be located at the southwest corner of the property to maintain flowrates leaving the property at historic levels or below. Flow intercepted by drainage swales will be directed to the pond. The outlet structure will consist of a single 36" Reinforced Concrete Pipe (RCP) with an invert elevation of 6757.50 ft and invert out elevation of 6755.00. The culvert will



## **Drainage Memorandum for Pikes Peak Community College North Campus**

discharge into a riprap stilling basin to dissipate energy and overflow to follow historic sheetflow drainage patterns. The pond will have a surface area of 1.4 acres and a storage volume of 4.4 acre-ft. The maximum stage and discharge elevation for the 100 year and 5 year storm is 6762.00 ft. and 55 cfs and 6758.53 and 23 cfs, respectively. A 20 ft. wide emergency spillway with an elevation of 6763.00 ft. will be in place should the outlet structure become inoperable. The spillway will be capable of passing the 100 year design storm. The detention pond will consist of a trapezoidal berm with a 5:1 slope at the upstream face and a 3:1 slope on the downstream face. Buried rip rap will be used along the emergency spillway to reduce erosion.

### **Inlets**

A CDOT Type 13 inlet will be located at a low point in the rear service area of the building. This will drain local runoff from the rear parking area, roof and embankment. An 18" RCP will convey flow to a drainage swale and eventually discharge to the detention pond.

Four CDOT Type R inlets will be used to collect surface runoff from the parking areas. The inlets will consist of 10 ft., 15 ft., and two 20 ft. Runoff will spill onto the internal access road and be intercepted by inlets as shown on figure 3. Runoff will then be discharged into the drainage swale and into the detention pond.

Area drain inlets will be located near the building to capture local runoff directed into them. The area drains will consist of a 12" x 12" perforated lid and discharge into the roof drain collection system. Collection lines will discharge into standard 4 ft. diameter manholes, and ultimately downstream into CDOT Type R inlets described above via 10"/12" PVC pipe.

### **Culverts**

A 36" CMP with flared end sections will be located along a sump condition along the internal access road and convey flow from the north to the south side of the road. Extension of an existing 30" RCP located at the highway access south of SH-83 and Jet Stream Drive will be installed as required by the proposed paving in the area.

## **IV. EROSION CONTROL**

The contractor will be responsible for implementing best management practices to prevent the loss of soil from the site. During construction the detention pond will act as the primary erosion control feature as runoff will deposit suspended solids. Periodic maintenance will be required during construction. Silt fences and hay bales will be utilized as required to minimize site erosion. Commercially available products will be utilized to prevent the erosion of all areas of cut and fill.

## APPENDICES

EXHIBIT 5.5-2

URS Consultants, Inc.  
CALCULATION COVER SHEET

Client: Davis Parkershy Project Name: TPCC  
Project/Calculation Number: 42154  
Title: DRAINAGE Analysis.  
Total number of pages (including cover sheet): 10  
Total number of computer runs: 4  
Prepared by: Ron Sanchez Date: 2/96  
Checked by: Charles N. Cothran Date: 8/25/96

Description and Purpose:

Determine Historic + Developed  
Flows for site.

Design bases/references/assumptions:

City/County Drainage Manual.  
HEC-1

Remarks/conclusions:

$$Q_{H_{100}} = 147 \text{ cfs} \quad Q_{D_{100}} = 196 \text{ cfs}$$

$$Q_{H_5} = 37 \text{ cfs} \quad Q_{D_5} = 63 \text{ cfs}$$

Calculation Approved by: Charles N. Cothran 8/25/96  
Project Manager/Date

Revision No.:	Description of Revision:	Approved by:
_____	_____	_____
_____	_____	_____
_____	_____	_____

Project Manager/Date

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 02/26/1996 TIME 09:13:11 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

*etc 8/25/96*

```

X   X   XXXXXXX   XXXXX           X
X   X   X         X   X           XX
X   X   X         X               X
XXXXXXXX XXXX     X           XXXXX X
X   X   X         X               X
X   X   X         X   X           X
X   X   XXXXXXX   XXXXX           XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1         ID          MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154-SH.INP
2         ID          USING UNDEVELOPED CRITERIA TO DETERMINE HISTORIC FLOWS
3         ID          USING THE 5-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA
4         ID          RUN DATE 02-1996
5         *DIAGRAM
6         IT          5 02FEB96      800      300
6         IO          5
7         KK          BAS-1
8         KM          RUNOFF FROM BASIN 1
9         BA          .116
10        LS          0          68
11        UD          .114
12        IN          15
13        PB          0
14        PC          0.000  0.001  0.004  0.008  0.012  0.016  0.021  0.026  0.031  0.037
15        PC          0.043  0.049  0.055  0.061  0.066  0.072  0.083  0.101  0.120  0.138
16        PC          0.156  0.195  0.260  1.040  1.820  1.885  1.950  1.989  2.028  2.054
17        PC          2.080  2.106  2.132  2.145  2.158  2.171  2.184  2.197  2.210  2.223
18        PC          2.236  2.246  2.256  2.265  2.275  2.283  2.295  2.304  2.314  2.324
19        PC          2.334  2.343  2.353  2.362  2.370  2.379  2.387  2.395  2.402  2.410
20        PC          2.418  2.425  2.431  2.438  2.444  2.451  2.457  2.464  2.470  2.477
21        PC          2.483  2.490  2.496  2.503  2.509  2.516  2.522  2.529  2.535  2.542
22        PC          2.548  2.551  2.555  2.558  2.561  2.564  2.568  2.571  2.574  2.577
23        PC          2.581  2.584  2.587  2.590  2.594  2.597  2.600
24        ZZ
  
```

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT  
 LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW  
 7 BAS-1

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 02/26/1996 TIME 09:13:11 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154-5H.INP  
 USING UNDEVELOPED CRITERIA TO DETERMINE HISTORIC FLOWS  
 USING THE 5-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA  
 RUN DATE 02-1996

6 IO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 2FEB96 STARTING DATE  
 ITIME 0800 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 3FEB96 ENDING DATE  
 NDTIME 0855 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	BAS-1	37.	6.08	4.	1.	1.	.12		

\*\*\* NORMAL END OF HEC-1 \*\*\*

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 02/26/1996 TIME 09:10:34 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

```

X   X   XXXXXXX   XXXXX   X
X   X   X       X     X   XX
X   X   X       X       X
XXXXXXX XXXX   X       XXXXX X
X   X   X       X       X
X   X   X       X     X   X
X   X   XXXXXXX   XXXXX   XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154-100H.INP									
2	ID	USING UNDEVELOPED CRITERIA TO DETERMINE HISTORIC FLOWS									
3	ID	USING THE 100-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA.									
4	ID	RUN DATE 02-1996									
	*DIAGRAM										
5	IT	5	02FEB96	800	300						
6	IO	5									
7	KK	BAS-1									
8	KM	RUNOFF FROM BASIN 1									
9	BA	.116									
10	LS	0	68								
11	UD	0.114									
12	IN	15									
13	PB	0									
14	PC	0.000	0.002	0.007	0.013	0.020	0.026	0.035	0.044	0.053	0.063
15	PC	0.073	0.083	0.092	0.103	0.112	0.122	0.141	0.172	0.202	0.233
16	PC	0.264	0.330	0.440	1.760	3.080	3.190	3.300	3.366	3.432	3.476
17	PC	3.520	3.564	3.608	3.630	3.652	3.674	3.696	3.718	3.740	3.762
18	PC	3.784	3.801	3.817	3.834	3.850	3.867	3.883	3.900	3.916	3.933
19	PC	3.949	3.966	3.982	3.997	4.011	4.025	4.039	4.052	4.066	4.079
20	PC	4.092	4.103	4.114	4.125	4.136	4.147	4.158	4.169	4.180	4.191
21	PC	4.202	4.213	4.224	4.235	4.246	4.257	4.268	4.279	4.290	4.301
22	PC	4.312	4.318	4.323	4.329	4.334	4.340	4.345	4.351	4.356	4.362
23	PC	4.367	4.373	4.378	4.384	4.389	4.395	4.400			
24	ZZ										

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW  
 7 BAS-1

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 02/26/1996 TIME 09:10:34 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154-100H.INP  
 USING UNDEVELOPED CRITERIA TO DETERMINE HISTORIC FLOWS  
 USING THE 100-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA  
 RUN DATE 02-1996

6 IO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 2FEB96 STARTING DATE  
 ITIME 0800 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 3FEB96 ENDING DATE  
 NDTIME 0855 ENDING TIME  
 ICENT 19 CENTURY MARK  
 COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	BAS-1	147.	6.00	14.	5.	4.	.12		

\*\*\* NORMAL END OF HEC-1 \*\*\*

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 02/26/1996 TIME 09:16:11 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

```

X   X   XXXXXXX   XXXXX   X
X   X   X         X     X   XX
X   X   X         X         X
XXXXXXX XXXX     X         XXXXX X
X   X   X         X         X
X   X   X         X     X   X
X   X   XXXXXXX   XXXXX   XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
  1      ID      MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154-5D.INP
  2      ID      USING UNDEVELOPED CRITERIA TO DETERMINE DEVELOPED FLOWS
  3      ID      USING THE 5-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA
  4      ID      RUN DATE 02-1996
  5      *DIAGRAM
  6      IT      5 02FEB96      800      300
  7      IO      5
  8      KK      BAS-1
  9      KM      RUNOFF FROM BASIN 1
 10      BA      .116
 11      LS      0      74
 12      UD      .114
 13      IN      15
 14      PB      0
 15      PC      0.000  0.001  0.004  0.008  0.012  0.016  0.021  0.026  0.031  0.037
 16      PC      0.043  0.049  0.055  0.061  0.066  0.072  0.083  0.101  0.120  0.138
 17      PC      0.156  0.195  0.260  1.040  1.820  1.885  1.950  1.989  2.028  2.054
 18      PC      2.080  2.106  2.132  2.145  2.158  2.171  2.184  2.197  2.210  2.223
 19      PC      2.236  2.246  2.256  2.265  2.275  2.283  2.295  2.304  2.314  2.324
 20      PC      2.334  2.343  2.353  2.362  2.370  2.379  2.387  2.395  2.402  2.410
 21      PC      2.418  2.425  2.431  2.438  2.444  2.451  2.457  2.464  2.470  2.477
 22      PC      2.483  2.490  2.496  2.503  2.509  2.516  2.522  2.529  2.535  2.542
 23      PC      2.548  2.551  2.555  2.558  2.561  2.564  2.568  2.571  2.574  2.577
 24      PC      2.581  2.584  2.587  2.590  2.594  2.597  2.600
 25      ZZ
  
```

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE      (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.      (.) CONNECTOR      (<---) RETURN OF DIVERTED OR PUMPED FLOW
  7      BAS-1
  
```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 02/26/1996 TIME 09:16:11 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*



MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154-5D.INP  
 USING UNDEVELOPED CRITERIA TO DETERMINE DEVELOPED FLOWS  
 USING THE 5-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA  
 RUN DATE 02-1996

6 IO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 2FEB96 STARTING DATE  
 ITIME 0800 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 3FEB96 ENDING DATE  
 NDTIME 0855 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	BAS-1	63.	6.00	6.	2.	2.	.12		

\*\*\* NORMAL END OF HEC-1 \*\*\*

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 02/26/1996 TIME 09:14:53 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

```

X   X   XXXXXXX   XXXXX   X
X   X   X         X   X   XX
X   X   X         X         X
XXXXXXX XXXX   X         XXXXX X
X   X   X         X         X
X   X   X         X   X   X
X   X   XXXXXXX   XXXXX   XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

LINE	ID	.....1	.....2	.....3	.....4	.....5	.....6	.....7	.....8	.....9	.....10
1	ID	MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154-100D.INP									
2	ID	USING UNDEVELOPED CRITERIA TO DETERMINE DEVELOPED FLOWS									
3	ID	USING THE 100-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA									
4	ID	RUN DATE 02-1996									
	*DIAGRAM										
5	IT	5	02FEB96	800	300						
6	IO	5									
7	KK	BAS-1									
8	KM	RUNOFF FROM BASIN 1									
9	BA	.116									
10	LS	0	74								
11	UD	0.114									
12	IN	15									
13	PB	0									
14	PC	0.000	0.002	0.007	0.013	0.020	0.026	0.035	0.044	0.053	0.063
15	PC	0.073	0.083	0.092	0.103	0.112	0.122	0.141	0.172	0.202	0.233
16	PC	0.264	0.330	0.440	1.760	3.080	3.190	3.300	3.366	3.432	3.476
17	PC	3.520	3.564	3.608	3.630	3.652	3.674	3.696	3.718	3.740	3.762
18	PC	3.784	3.801	3.817	3.834	3.850	3.867	3.883	3.900	3.916	3.933
19	PC	3.949	3.966	3.982	3.997	4.011	4.025	4.039	4.052	4.066	4.079
20	PC	4.092	4.103	4.114	4.125	4.136	4.147	4.158	4.169	4.180	4.191
21	PC	4.202	4.213	4.224	4.235	4.246	4.257	4.268	4.279	4.290	4.301
22	PC	4.312	4.318	4.323	4.329	4.334	4.340	4.345	4.351	4.356	4.362
23	PC	4.367	4.373	4.378	4.384	4.389	4.395	4.400			
24	ZZ										

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW  
 7 BAS-1

{\*\*\*} RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 02/26/1996 TIME 09:14:53 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154-100D.INP  
 USING UNDEVELOPED CRITERIA TO DETERMINE DEVELOPED FLOWS  
 USING THE 100-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA  
 RUN DATE 02-1996

6 IO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 2FEB96 STARTING DATE  
 ITIME 0800 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 3FEB96 ENDING DATE  
 NDTIME 0855 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	BAS-1	196.	6.00	19.	6.	6.	.12		

\*\*\* NORMAL END OF HEC-1 \*\*\*

SUBJECT DRAINAGE

DETERMINE DEVELOPED FLOW

SITE CHARACTERISTICS

Hydrolc SOIL GROUP: A/B

elev: High = 6818.2

low = 6756.

Flow length = 2200 LF.

$$T_c = \frac{(11.9(L)^{0.385}}{H} = 0.19 \text{ hr}$$

$$T_L = \frac{1}{5} T_c = 0.114 \text{ hr}$$

Area = 74.29 ac.	<u>CN</u>
	68
Developed Area = 14.45	98
GRASS AREA = 1.41	68

$$\text{Weighted CN} = \frac{14.45(98) + 59.84(68)}{74.29} = 74 \checkmark$$

FROM HEC-1.

HISTORIC FLOW  $Q_{100} = 147 \text{ cfs.}$   
 $Q_5 = 37 \text{ cfs.}$

Developed FLOW  $Q_{100} = 196 \text{ cfs.}$   
 $Q_5 = 63 \text{ cfs.}$

$$\Delta Q_{100} = 196 - 147 = 49 \text{ cfs} \sim 33.3\%$$

$$\Delta Q_5 = 63 - 37 = 26 \text{ cfs} \sim 70.3\%$$

Drain BT.

**EXHIBIT 5.3-1**  
**URS Consultants, Inc.**  
**CALCULATION COVER SHEET**

Client: Davis Parkway, Inc. Project Name: PPCC  
 Project/Calculation Number: 07421521  
 Title: Historic/Developed Basin 1 HEC1 w/ Pond  
 Total number of pages (including cover sheet): 14  
 Total number of computer runs: 6  
 Prepared by: Tom Sanchez Date: 8/30/96  
 Checked by: Charles K. Cothern Date: 9/1/96

**Description and Purpose:**  
 Determine Historic & Developed flows for  
 Basin 1-1, 1-2

**Design bases/references/assumptions:**

City/County Criteria  
 PCC-1

**Remarks/conclusions:**

	<u>Historic</u>	<u>Developed</u>	<u>Developed w/ Pond</u>	<u>TOTAL</u>
Basin 1-1	Q <sub>100</sub> = 124 cfs Q <sub>5</sub> = 31 cfs	Q <sub>100</sub> = 173 cfs. Q <sub>5</sub> = 58 cfs.	Q <sub>100</sub> = 55 cfs. Q <sub>5</sub> = 20 cfs.	Q <sub>100</sub> = <u>77 cfs</u> Q <sub>5</sub> = <u>26 cfs</u>
Basin 1-2	Q <sub>100</sub> = 22 cfs Q <sub>5</sub> = 6 cfs	Q <sub>100</sub> = N/A Q <sub>5</sub> = N/A		Less than historic for site.

Calculation Approved by: Charles K. Cothern 9/1/96

Project Manager/Date

Revision No.:	Description of Revision:	Approved by:
_____	_____	_____
_____	_____	_____
_____	_____	_____

Project Manager/Date

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 08/30/1996 TIME 12:11:23 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

*CKE 9/1/96*

```

X   X   XXXXXXX   XXXXX   X
X   X   X         X   X   XX
X   X   X         X         X
XXXXXXXX XXXX   X         XXXXX   X
X   X   X         X         X
X   X   X         X   X   X
X   X   XXXXXXX   XXXXX   XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1         ID          MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154B1-5H.INP
2         ID          USING UNDEVELOPED CRITERIA TO DETERMINE HISTORIC FLOWS
3         ID          USING THE 5-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA
4         ID          RUN DATE 02-1996
5         *DIAGRAM
6         IT          5 02FEB96      800      300
6         IO          5
7         KK          BS1-1
8         KM          RUNOFF FROM SUB-BASIN 1-1
9         BA          .098
10        LS          0      68
11        UD          0.114
12        IN          15
13        PB          0
14        PC          0.000  0.001  0.004  0.008  0.012  0.016  0.021  0.026  0.031  0.037
15        PC          0.043  0.049  0.055  0.061  0.066  0.072  0.083  0.101  0.120  0.138
16        PC          0.156  0.195  0.260  1.040  1.820  1.885  1.950  1.989  2.028  2.054
17        PC          2.080  2.106  2.132  2.145  2.158  2.171  2.184  2.197  2.210  2.223
18        PC          2.236  2.246  2.256  2.265  2.275  2.283  2.295  2.304  2.314  2.324
19        PC          2.334  2.343  2.353  2.362  2.370  2.379  2.387  2.395  2.402  2.410
20        PC          2.418  2.425  2.431  2.438  2.444  2.451  2.457  2.464  2.470  2.477
21        PC          2.483  2.490  2.496  2.503  2.509  2.516  2.522  2.529  2.535  2.542
22        PC          2.548  2.551  2.555  2.558  2.561  2.564  2.568  2.571  2.574  2.577
23        PC          2.581  2.584  2.587  2.590  2.594  2.597  2.600
24        ZZ
  
```

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT LINE (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.        (.) CONNECTOR    (<---) RETURN OF DIVERTED OR PUMPED FLOW
7          BS1-1
  
```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 08/30/1996 TIME 12:11:23 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154B1-5H.INP  
 USING UNDEVELOPED CRITERIA TO DETERMINE HISTORIC FLOWS  
 USING THE 5-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA  
 RUN DATE 02-1996

6 IO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 2FEB96 STARTING DATE  
 ITIME 0800 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 3FEB96 ENDING DATE  
 NDTIME 0855 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-Feet  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	BS1-1	31.	6.08	3.	1.	1.	.10		

\*\*\* NORMAL END OF HEC-1 \*\*\*

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 08/30/1996 TIME 12:07:29 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

```

X   X   XXXXXXX   XXXXX   X
X   X   X         X     X   XX
X   X   X         X         X
XXXXXXXX XXXX   X         XXXXX X
X   X   X         X         X
X   X   X         X     X   X
X   X   XXXXXXX   XXXXX   XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154B1-1H.INP									
2	ID	USING UNDEVELOPED CRITERIA TO DETERMINE HISTORIC FLOWS									
3	ID	USING THE 100-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA									
4	ID	RUN DATE 02-1996									
	*DIAGRAM										
5	IT	5	02FEB96	800	300						
6	IO	5									
7	KK	BS1-1									
8	KM	RUNOFF FROM SUB-BASIN 1-1									
9	BA	.098									
10	LS	0	68								
11	UD	0.114									
12	IN	15									
13	PB	0									
14	PC	0.000	0.002	0.007	0.013	0.020	0.026	0.035	0.044	0.053	0.063
15	PC	0.073	0.083	0.092	0.103	0.112	0.122	0.141	0.172	0.202	0.233
16	PC	0.264	0.330	0.440	1.760	3.080	3.190	3.300	3.366	3.432	3.476
17	PC	3.520	3.564	3.608	3.630	3.652	3.674	3.696	3.718	3.740	3.762
18	PC	3.784	3.801	3.817	3.834	3.850	3.867	3.883	3.900	3.916	3.933
19	PC	3.949	3.966	3.982	3.997	4.011	4.025	4.039	4.052	4.066	4.079
20	PC	4.092	4.103	4.114	4.125	4.136	4.147	4.158	4.169	4.180	4.191
21	PC	4.202	4.213	4.224	4.235	4.246	4.257	4.268	4.279	4.290	4.301
22	PC	4.312	4.318	4.323	4.329	4.334	4.340	4.345	4.351	4.356	4.362
23	PC	4.367	4.373	4.378	4.384	4.389	4.395	4.400			
24	ZZ										

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW  
 7 BS1-1

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION  
 \*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 08/30/1996 TIME 12:07:29 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*



MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154B1-1H.INP  
 USING UNDEVELOPED CRITERIA TO DETERMINE HISTORIC FLOWS  
 USING THE 100-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA  
 RUN DATE 02-1996

6 IO      OUTPUT CONTROL VARIABLES  
           IPRNT        5    PRINT CONTROL  
           IPLOT        0    PLOT CONTROL  
           QSCAL        0.    HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA  
           NMIN        5    MINUTES IN COMPUTATION INTERVAL  
           IDATE       2FEB96    STARTING DATE  
           ITIME       0800    STARTING TIME  
           NQ          300    NUMBER OF HYDROGRAPH ORDINATES  
           NDDATE      3FEB96    ENDING DATE  
           NDTIME      0855    ENDING TIME  
           ICENT       19    CENTURY MARK  
  
           COMPUTATION INTERVAL    .08 HOURS  
           TOTAL TIME BASE        24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA            SQUARE MILES  
 PRECIPITATION DEPTH     INCHES  
 LENGTH, ELEVATION       FEET  
 FLOW                      CUBIC FEET PER SECOND  
 STORAGE VOLUME          ACRE-FEET  
 SURFACE AREA            ACRES  
 TEMPERATURE            DEGREES FAHRENHEIT

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	BS1-1	124.	6.00	12.	4.	4.	.10		

\*\*\* NORMAL END OF HEC-1 \*\*\*

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 08/30/1996 TIME 12:12:42 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

```

X X XXXXXXX XXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 15482-5H.INP									
2	ID	USING UNDEVELOPED CRITERIA TO DETERMINE HISTORIC FLOWS									
3	ID	USING THE 5-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA									
4	ID	RUN DATE 02-1996									
	*DIAGRAM										
5	IT	5	02FEB96	800	300						
6	IO	5									
7	KK	BS1-2									
8	KM	RUNOFF FROM SUB-BASIN 1-2									
9	BA	.0182									
10	LS	0	68								
11	UD	0.126									
12	IN	15									
13	PB	0									
14	PC	0.000	0.001	0.004	0.008	0.012	0.016	0.021	0.026	0.031	0.037
15	PC	0.043	0.049	0.055	0.061	0.066	0.072	0.083	0.101	0.120	0.138
16	PC	0.156	0.195	0.260	1.040	1.820	1.885	1.950	1.989	2.028	2.054
17	PC	2.080	2.106	2.132	2.145	2.158	2.171	2.184	2.197	2.210	2.223
18	PC	2.236	2.246	2.256	2.265	2.275	2.283	2.295	2.304	2.314	2.324
19	PC	2.334	2.343	2.353	2.362	2.370	2.379	2.387	2.395	2.402	2.410
20	PC	2.418	2.425	2.431	2.438	2.444	2.451	2.457	2.464	2.470	2.477
21	PC	2.483	2.490	2.496	2.503	2.509	2.516	2.522	2.529	2.535	2.542
22	PC	2.548	2.551	2.555	2.558	2.561	2.564	2.568	2.571	2.574	2.577
23	PC	2.581	2.584	2.587	2.590	2.594	2.597	2.600			
24	ZZ										

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT  
 LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW  
 7 BS1-2

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 08/30/1996 TIME 12:12:42 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 15482-5H.INP  
 USING UNDEVELOPED CRITERIA TO DETERMINE HISTORIC FLOWS  
 USING THE 5-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA  
 RUN DATE 02-1996

6 IO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 2FEB96 STARTING DATE  
 ITIME 0800 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 3FEB96 ENDING DATE  
 NDTIME 0855 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	BS1-2	6.	6.08	1.	0.	0.	.02		

\*\*\* NORMAL END OF HEC-1 \*\*\*

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 08/30/1996 TIME 12:08:31 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

```

X   X   XXXXXXX   XXXXX   X
X   X   X         X     X   XX
X   X   X         X     X   X
XXXXXXX XXXX   X         XXXXX X
X   X   X         X     X   X
X   X   X         X     X   X
X   X   XXXXXXX   XXXXX   XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154B2-1H.INP									
2	ID	USING UNDEVELOPED CRITERIA TO DETERMINE HISTORIC FLOWS									
3	ID	USING THE 100-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA									
4	ID	RUN DATE 02-1996									
	*DIAGRAM										
5	IT	5	02FEB96	800	300						
6	IO	5									
7	KK	BS1-2									
8	KM	RUNOFF FROM SUB-BASIN 1-2									
9	BA	.0182									
10	LS	0	68								
11	UD	0.126									
12	IN	15									
13	PB	0									
14	PC	0.000	0.002	0.007	0.013	0.020	0.026	0.035	0.044	0.053	0.063
15	PC	0.073	0.083	0.092	0.103	0.112	0.122	0.141	0.172	0.202	0.233
16	PC	0.264	0.330	0.440	1.760	3.080	3.190	3.300	3.366	3.432	3.476
17	PC	3.520	3.564	3.608	3.630	3.652	3.674	3.696	3.718	3.740	3.762
18	PC	3.784	3.801	3.817	3.834	3.850	3.867	3.883	3.900	3.916	3.933
19	PC	3.949	3.966	3.982	3.997	4.011	4.025	4.039	4.052	4.066	4.079
20	PC	4.092	4.103	4.114	4.125	4.136	4.147	4.158	4.169	4.180	4.191
21	PC	4.202	4.213	4.224	4.235	4.246	4.257	4.268	4.279	4.290	4.301
22	PC	4.312	4.318	4.323	4.329	4.334	4.340	4.345	4.351	4.356	4.362
23	PC	4.367	4.373	4.378	4.384	4.389	4.395	4.400			
24	ZZ										

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW  
 7 BS1-2

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 08/30/1996 TIME 12:08:31 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154B2-1H.INP  
 USING UNDEVELOPED CRITERIA TO DETERMINE HISTORIC FLOWS  
 USING THE 100-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA  
 RUN DATE 02-1996

6 IO      OUTPUT CONTROL VARIABLES  
           IPRNT        5    PRINT CONTROL  
           IPLOT        0    PLOT CONTROL  
           QSCAL        0.    HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA  
           NMIN        5    MINUTES IN COMPUTATION INTERVAL  
           IDATE       2FEB96    STARTING DATE  
           ITIME       0800    STARTING TIME  
           NQ          300    NUMBER OF HYDROGRAPH ORDINATES  
           NDDATE      3FEB96    ENDING DATE  
           NDTIME      0855    ENDING TIME  
           ICENT       19    CENTURY MARK

          COMPUTATION INTERVAL    .08 HOURS  
           TOTAL TIME BASE        24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA            SQUARE MILES  
 PRECIPITATION DEPTH     INCHES  
 LENGTH, ELEVATION       FEET  
 FLOW                      CUBIC FEET PER SECOND  
 STORAGE VOLUME          ACRE-FEET  
 SURFACE AREA            ACRES  
 TEMPERATURE            DEGREES FAHRENHEIT

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	BS1-2	22.	6.00	2.	1.	1.	.02		

\*\*\* NORMAL END OF HEC-1 \*\*\*

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 08/15/1996 TIME 16:04:46 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

```

X   X   XXXXXXX   XXXXX   X
X   X   X         X     X   XX
X   X   X         X         X
XXXXXXXX XXXX   X         XXXXX X
X   X   X         X         X
X   X   X         X     X   X
X   X   XXXXXXX   XXXXX   XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1         ID      MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154D1-1D.INP
2         ID      USING DEVELOPED CRITERIA TO DETERMINE DEVELOPED FLOWS W/ DET.POND
3         ID      USING THE 5-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA
4         ID      OUTLET STRUCTURE: 36" CMP
5         ID      RUN DATE : 08/08/96
6         *DIAGRAM
7         IT      5 02FEB96      800      300
8         IO      5
9         KK      BAS-1-\
10        KM      RUNOFF FROM BASIN 1-\
11        BA      .098
12        LS      0      75
13        UD      0.114
14        IN      15
15        PB      0
16        PC      0.000 0.001 0.004 0.008 0.012 0.016 0.021 0.026 0.031 0.037
17        PC      0.043 0.049 0.055 0.061 0.066 0.072 0.083 0.101 0.120 0.138
18        PC      0.156 0.195 0.260 1.040 1.820 1.885 1.950 1.989 2.028 2.054
19        PC      2.080 2.106 2.132 2.145 2.158 2.171 2.184 2.197 2.210 2.223
20        PC      2.236 2.246 2.256 2.265 2.275 2.283 2.295 2.304 2.314 2.324
21        PC      2.334 2.343 2.353 2.362 2.370 2.379 2.387 2.395 2.402 2.410
22        PC      2.418 2.425 2.431 2.438 2.444 2.451 2.457 2.464 2.470 2.477
23        PC      2.483 2.490 2.496 2.503 2.509 2.516 2.522 2.529 2.535 2.542
24        PC      2.548 2.551 2.555 2.558 2.561 2.564 2.568 2.571 2.574 2.577
25        KK      DPOUT
26        KM      ROUTE POND THROUGH 1-36" CMP
27        SV      0      .75 1.92 3.67 4.425 5.175 5.175
28        SE      6756 6758 6760 6762 6763 6764 6765
29        SQ      0      15 35 55 62 137 268
30        RS      1      ELEV 6756
31        ZZ
  
```

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
8 BAS-1
V
V
25 DPOUT
  
```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \*\*\*\*\*

\* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \*  
 \* RUN DATE 08/15/1996 TIME 16:04:46 \*  
 \*  
 \*\*\*\*\*

\* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*  
 \*\*\*\*\*

MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154D1-1D.INP  
 USING DEVELOPED CRITERIA TO DETERMINE DEVELOPED FLOWS W/ DET.POND  
 USING THE 5-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA  
 OUTLET STRUCTURE: 36" CMP  
 RUN DATE : 08/08/96

7 IO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 2FEB96 STARTING DATE  
 ITIME 0800 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 3FEB96 ENDING DATE  
 NDTIME 0855 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	BAS-1	58.	6.00	6.	2.	2.	.10		
ROUTED TO	DPOUT	20.	6.25	6.	2.	2.	.10	6758.53	6.25

\*\*\* NORMAL END OF HEC-1 \*\*\*

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* RUN DATE 08/15/1996 TIME 11:51:13 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \*\*\*\*\*

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154D1-1D.INP									
2	ID	USING DEVELOPED CRITERIA TO DETERMINE DEVELOPED FLOWS W/ DET.POND									
3	ID	USING THE 100-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA									
4	ID	OUTLET STRUCTURE: 36" CMP									
5	ID	RUN DATE : 08/08/96									
	*DIAGRAM										
6	IT	5	02FEB96	800	300						
7	IO	5									
8	KK	BAS-1									
9	KM	RUNOFF FROM BASIN 1									
10	BA	.098									
11	LS	0	75								
12	UD	0.114									
13	IN	15									
14	PB	0									
15	PC	0.000	0.002	0.007	0.013	0.020	0.026	0.035	0.044	0.053	0.063
16	PC	0.073	0.083	0.092	0.103	0.112	0.122	0.141	0.172	0.202	0.233
17	PC	0.264	0.330	0.440	1.760	3.080	3.190	3.300	3.366	3.432	3.476
18	PC	3.520	3.564	3.608	3.630	3.652	3.674	3.696	3.718	3.740	3.762
19	PC	3.784	3.801	3.817	3.834	3.850	3.867	3.883	3.900	3.916	3.933
20	PC	3.949	3.966	3.982	3.997	4.011	4.025	4.039	4.052	4.066	4.079
21	PC	4.092	4.103	4.114	4.125	4.136	4.147	4.158	4.169	4.180	4.191
22	PC	4.202	4.213	4.224	4.235	4.246	4.257	4.268	4.279	4.290	4.301
23	PC	4.312	4.318	4.323	4.329	4.334	4.340	4.345	4.351	4.356	4.362
24	PC	4.367	4.373	4.378	4.384	4.389	4.395	4.400			
25	KK	DPOUT									
26	KM	ROUTE POND THROUGH 1-36" CMP									
27	SV	0	.75	1.92	3.67	4.425	5.175	5.175			
28	SE	6756	6758	6760	6762	6763	6764	6765			
29	SQ	0	15	35	55	62	137	268			
30	RS	1	ELEV	6756							
31	ZZ										

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

8 BAS-1  
 V  
 V  
 25 DPOUT

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DODSON AND ASSOCIATES, INC. \*  
 \*\*\*\*\*



\* BY THE COE IN FEBRUARY 1981 \*  
 \* REVISED 02 AUG 88 \*  
 \* \*  
 \* RUN DATE 08/15/1996 TIME 11:51:13 \*  
 \* \*  
 \*\*\*\*\*

\* HYDROLOGIST AND CIVIL ENGINEERS \*  
 \* 7015 W TIDWELL SUITE 107 \*  
 \* HOUSTON, TEXAS 77092 \*  
 \* (713) 895-8322 \*  
 \* \*  
 \*\*\*\*\*

MAJOR STORM HYDROLOGY FOR THE BASIN - INPUT FILE 154D1-1D.INP  
 USING DEVELOPED CRITERIA TO DETERMINE DEVELOPED FLOWS W/ DET.POND  
 USING THE 100-YEAR 24-HOUR STORM IN THE CITY/COUNTY CRITERIA  
 OUTLET STRUCTURE: 36" CMP  
 RUN DATE : 08/08/96

7 IO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 2FEB96 STARTING DATE  
 ITIME 0800 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 3FEB96 ENDING DATE  
 NDTIME 0855 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	BAS-1	173.	6.00	17.	5.	5.	.10		
ROUTED TO	DPOUT	55.	6.25	16.	5.	5.	.10	6762.02	6.25

\*\*\* NORMAL END OF HEC-1 \*\*\*

EXHIBIT 5.3-1  
URS Consultants, Inc.  
CALCULATION COVER SHEET

Client: Davis Partnership Project Name: PRC  
Project/Calculation Number: 40154  
Title: OFF SITE FLOWS  
Total number of pages (including cover sheet): 3  
Total number of computer runs: \_\_\_\_\_  
Prepared by: D. Gandy Date: 8/30/96  
Checked by: Charles R. Colten Date: 9/1/96

Description and Purpose:

Determine off site flows.

Design bases/references/assumptions:

City/County Criteria

Remarks/conclusions:

Calculation Approved by: Charles R. Colten 9/1/96  
Project Manager/Date

Revision No.:	Description of Revision:	Approved by:
_____	_____	_____
_____	_____	_____
_____	_____	_____

Project Manager/Date

SUBJECT PPCC DRAINAGE

DETERMINE OFF SITE DRAINAGE

BASIN 0-1

CHARACTERISTICS

AREA = 131.3 Ac.  
 HI ELEV = 7040 ft  
 LOW ELEV = 6810 ft.  
 Run Length = 7300 ft.  
 SOIL GROUP = B.  
 CN: = 61 - Range land Good CONDITION.

TIME OF CONC.

$$T_c = \left( \frac{11.9 L^3}{H} \right)^{.385}$$

$$= \left[ \frac{(11.9) \left( \frac{7300}{5280} \right)^3}{6040 - 6810} \right]^{.385} = .46 \text{ hr} = 27.8 \text{ min.}$$

DIRECT Runoff

$R_5 = 2.6 \text{ in/hr}$   
 $R_{100} = 4.4 \text{ in/hr}$

$$Q = \frac{(P - 0.25)^2}{(P + 0.83)} \quad S = \frac{1000}{CN} - 10$$

$S = 6.39$

$$Q_5 = \frac{(2.6 - 0.2(6.39))^2}{2.6 + 0.8(6.39)} = .23 \text{ in}$$

$$Q_{100} = \frac{(4.4 - 0.2(6.39))^2}{4.4 + 0.8(6.39)} = 1.02 \text{ in}$$

Peak Runoff

$$Q_p = \frac{484 A Q}{t_p}$$

$$Q_5 = \frac{484 \left( \frac{131.3}{640} \right) .23}{107(.46)} = \underline{73.0 \text{ cfs}}$$

$$Q_{100} = \frac{484 \left( \frac{131.3}{640} \right) 1.02}{107(.46)} = \underline{328.6 \text{ cfs}}$$

SUBJECT ZPCC DRAINAGE

BASIN 0-2

CHARACTERISTICS

AREA = 71.62 Ac  
Hi ELEV = 6880 ft.  
Low ELEV = 6800  
Flow Length = 4,000  
SOIL GROUP = B.  
C<sub>v</sub> = 61

Time of Conc T<sub>c</sub>

$$T_c = \left[ \frac{11.9 \left( \frac{4,000}{6880} \right)^3}{80} \right]^{.385} = .35 \text{ hr}$$

$$T_p = .67(.35) = .23 \text{ hr}$$

Direct Runoff

See Basin 0-1

Peak Runoff

$$Q_s = \frac{484 \left( \frac{71.62}{640} \right) \cdot .23}{.23} = \underline{\underline{54 \text{ cfs}}}$$

$$Q_w = \frac{484 \left( \frac{71.62}{640} \right) \cdot .102}{.23} = \underline{\underline{240.2 \text{ cfs}}}$$

EXHIBIT 5.3-1  
URS Consultants, Inc.  
CALCULATION COVER SHEET

Client: Davis Partnership Project Name: Mike Peak College  
Project/Calculation Number: 42154  
Title: Retention Pond  
Total number of pages (including cover sheet): 7 14  
Total number of computer runs: \_\_\_\_\_  
Prepared by: R. Sandley Date: 8/30/96  
Checked by: Charles H. Colburn Date: 9/1/96

Description and Purpose:  
Size Retention structures.

Design bases/references/assumptions:

Remarks/conclusions:

Calculation Approved by: \_\_\_\_\_

Project Manager/Date

Revision No.:	Description of Revision:	Approved by:
_____	_____	_____
_____	_____	_____
_____	_____	_____

Project Manager/Date

SUBJECT DRAINAGE Analysis

ASSUMPTIONS

Location of PPCC has altered drainage patterns.  
 (BASIN 2) APPROX. 11.66 acres follow historic patterns. Remaining  
 (BASIN 1) 62.63 acres drains into detention pond.

REQ'D

size retention pond such that discharge from retention plus historic drainage from 11.66 acres does not exceed historic flows for the site.

SOLN:

use Hec-1 to size retention pond.

1) Historic Runoff for site.

$$Q_{100} = 147 \text{ cfs.}$$

$$Q_5 = 37 \text{ cfs.}$$

2) Determine Runoff for Basin ① + ②.

Site Characteristics.

BASIN 1 (See Previous Calc),  $A = 62.63$   
 developed.  $CN = 75$

BASIN 2

Hydraulic Soil Group B.

Elev:  $H_1 = 6807$

$6770$

Flow length: 2,000 ft

$$T_C = \left( \frac{11.9(L^0.385)}{H} \right) = 0.211$$

$$T_{lag} = 3/5(.21) = 0.126$$

Area = 11.66

CN = 68 ✓

SUBJECT \_\_\_\_\_

Determine Allowable discharge from pond.

HISTORIC FLOW FROM SITE = 147 cfs. ✓

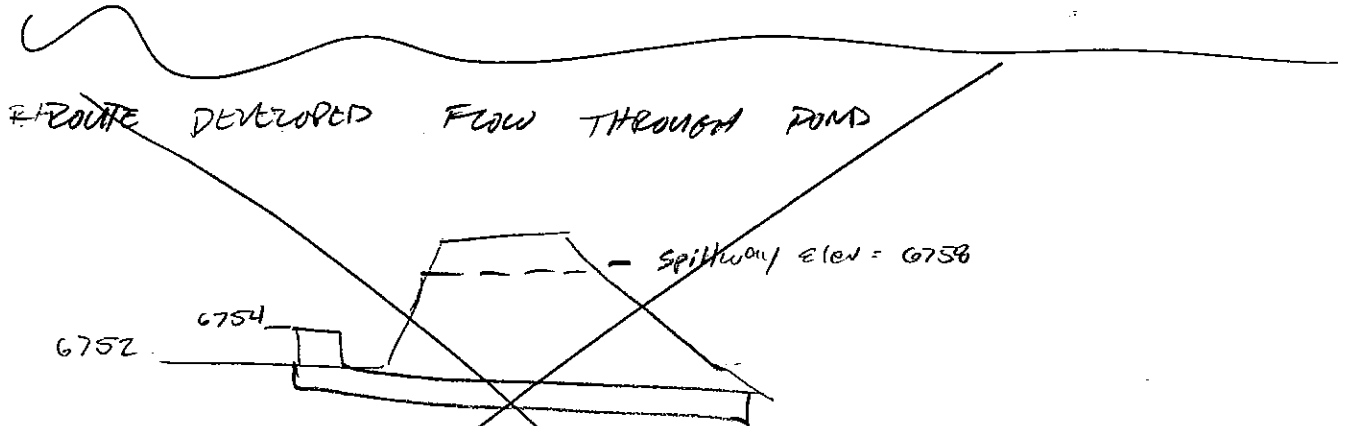
HISTORIC FLOW (B1+B2) = 140 cfs. ✓

HISTORIC BASIN 1 = 124 cfs.

" BASIN 2 = 22 cfs

Developed BASIN 1 = 173 cfs

ALLOWABLE DISCHARGE from Basin 1 = 124 cfs



~~BASED ON ACTUAL TOPO OF PROPOSED POND  
PEAK FLOW FOR 100 YR. DEVELOPED WILL BE~~

~~Q = 115 cfs, elev = 6757.84.~~

# URS CONSULTANTS, INC.

URS JOB NO. 421521 PAGE 4 OF 11  
 DATE 8/16/96 BY lit CHECKED BY cm 7/1/96  
 CLIENT Louis Routhier (date)  
 PROJECT PTCC

SUBJECT Det Road - Stage - Discharge

SIZE INLET FOR STORM ROUTING

ELEV.	18" CMP WEIR			TOTAL	24" CMP			TOTAL
	HWD	Q	WEIR		HWD	Q	TOTAL	
INV = 6757.0	0	0			0	0		
6760.0	2	11	22		15	18	36	
6762.0	3.3	16	32		2.5	29	58	
TOP OF SPILLWAY ↓ WEIR FLOW 6763.0	4	18	36		3	32	64	
6764.0	4.6	20	67	87	3.5	35	67	102
6765.0	5.3	22	190	212	4	37	190	227

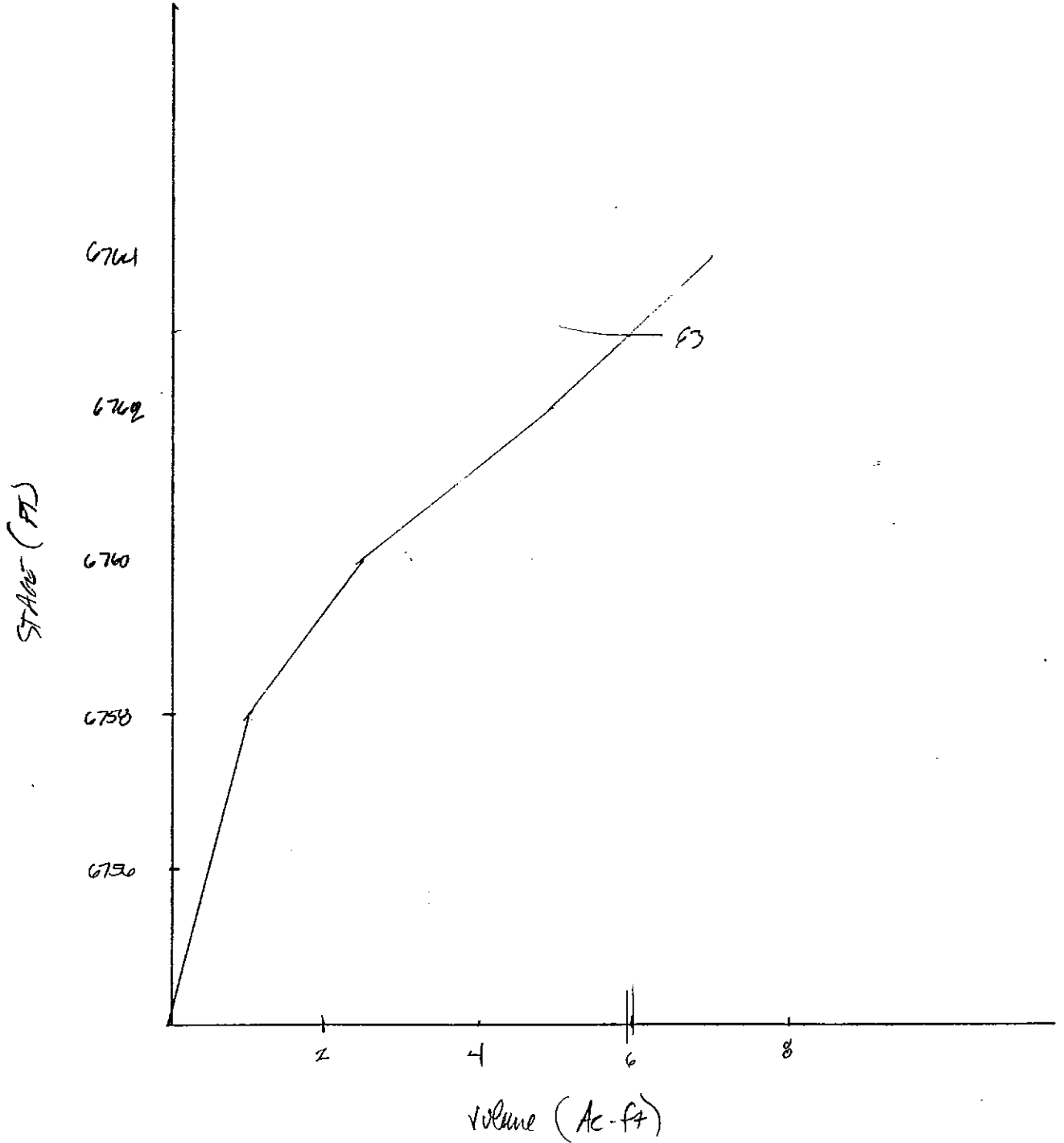
ELEV.	30"			TOTAL	36"			TOTAL
	HWD	Q	WEIR		HWD	Q	TOTAL	
6757.0		0	0		0	0		
6760	1.2	26	52		1.0	35	70	
6762	2	40	80		1.67	55	110	
6763	2.4	45	90		2.0	62	124	
6764	2.8	51	116	169	2.3	70	137	207
6765	3.2	56	246	302	2.67	78	268	346

154-CID? = 55 cfs wsl = 6762.01  
 30" @ 2.5% V = 8.0 f.p.s.

10  
 11



SUBJECT Detention Pond



### STORAGE ROUTING FORM

**1. INFLOW HYDROGRAPH GENERATION**

a. Hydrograph method used:

b. Time interval selected for routing:  
(inflow hydrograph attached)

**2. APPROXIMATE FLOW REDUCTION DUE TO ROUTING**

a. Peak inflow:  $Q_p =$  \_\_\_\_\_  $\text{ft}^3/\text{s}$

b. Upstream storage:  $S =$  \_\_\_\_\_  $\text{ft}^3$

c. Time to peak:  $t_p =$  \_\_\_\_\_ min

$$Q_r = Q_p \frac{S}{80 t_p}$$

**3. ELEVATION - DISCHARGE RELATIONSHIP FOR TRIAL CULVERT**

ELEVATION ft							
DISCHARGE $\text{ft}^3/\text{s}$							

**4. ELEVATION-STORAGE RELATIONSHIP FOR UPSTREAM PONDING**

ELEVATION ft	AREA $\text{ft}^2$	INCREMENTAL VOLUME $\text{ft}^3$	ACCUMULATED VOLUME $\text{ft}^3$
6756	16925	43750	0
6756	26925	67850	43750
6760	41025	101830	111600
6762	60805	151083	213430
6764	90278	305708	305708

**5. STORAGE - OUTFLOW RELATIONSHIP**

Elevation ft	Discharge (O) $\text{ft}^3/\text{s}$	Storage (S) $\text{ft}^3$	2s/Δt $\text{ft}^3/\text{s}$	2sΔt + O $\text{ft}^3/\text{s}$

**6. STORAGE-INDICATION ROUTING TABLE**

(1) TIME min	(2) INFLOW (I) $\text{ft}^3/\text{s}$	(3) 2sΔt - O $\text{ft}^3/\text{s}$	(4) 2sΔt + O $\text{ft}^3/\text{s}$	(5) OUTFLOW (O) $\text{ft}^3/\text{s}$

11-19



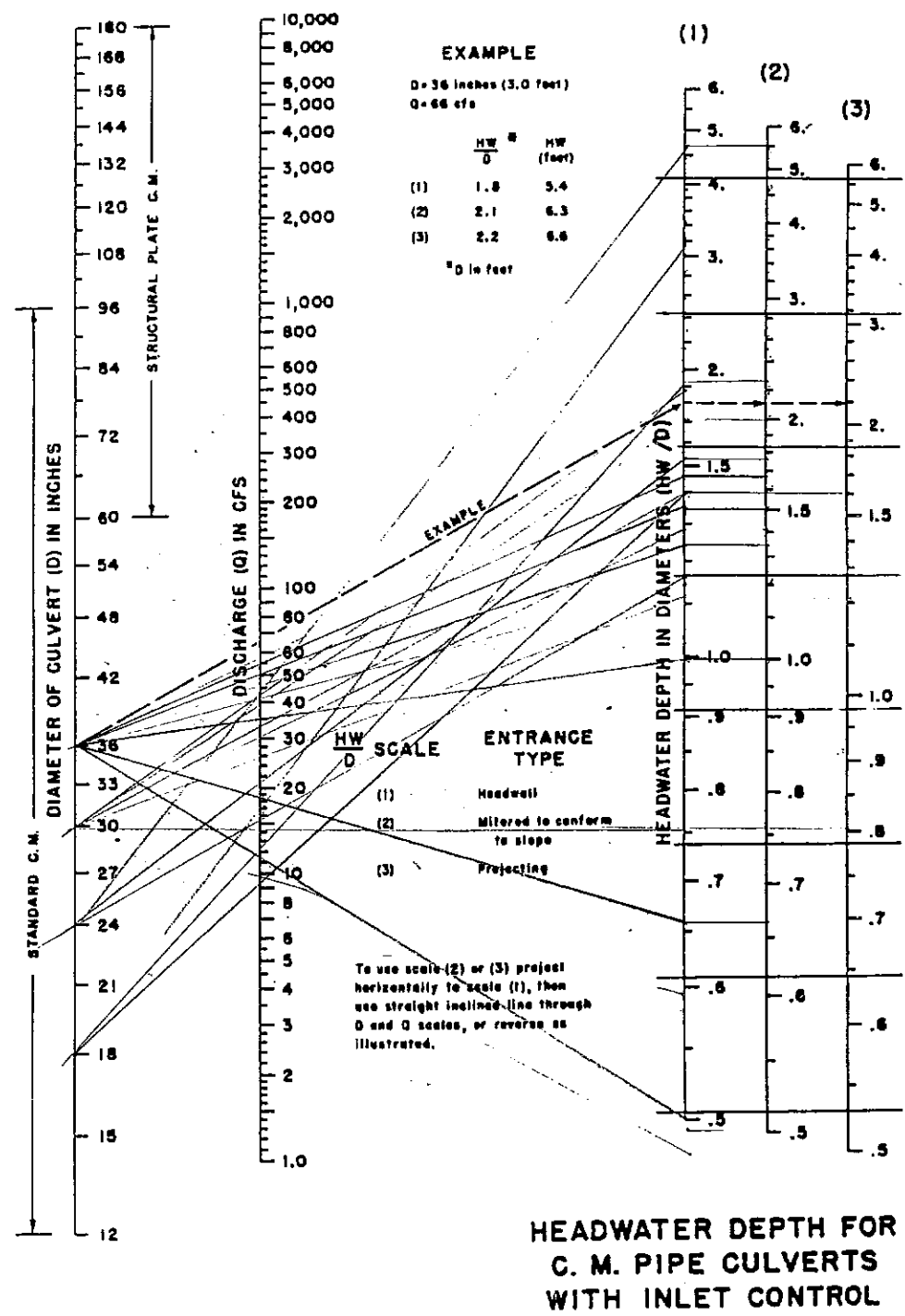
The City of Colorado Springs / El Paso County  
Drainage Criteria Manual

Date  
**OCT. 1987**

Figure  
**11 - 3**

7/12/87  
 9/1/87

YH  
etc  
9/1/74



BUREAU OF PUBLIC ROADS JAN. 1963



HDR Infrastructure, Inc.  
A Centerra Company

The City of Colorado Springs / El Paso County  
Drainage Criteria Manual

Date  
OCT. 1987

Figure  
9-37

SUBJECT \_\_\_\_\_

SIZE RIP RAP STILLING BASIN FOR REG. POND.

Assumptions

$Q = 55 \text{ cfs.}$  full flow conditions  $TW = 1.0'$

$Y/d_0 = .94$

$A/d_0^2 = 1.7662$   $A = 6.89 \text{ ft}^2$

$R/d_0 = 2.896$   $R = .8688$

FROM DRAINAGE CRITERIA MANUAL.

$V = Q/A = 8 \text{ fps.}$

$y = 2.82 \text{ ft}$

$y_e = (A/E)^{1/2} = 1.88$

$F = \frac{V}{\sqrt{32.2 y_e}} = \frac{8}{\sqrt{32.2(1.88)}} = 1.03$

$\frac{TW}{y_e} = \frac{1.0}{1.88} = 0.53 \leq 0.75 \text{ O.K.}$

Size Rip RAP  
 $(\text{try}) \frac{d_{50}}{y_e} = 0.2 \therefore d_{50} = 0.376$

$\frac{h_s}{y_e} = 1.0$   $h_s = 1.88$

$\frac{h_s}{d_{50}} = \frac{1}{.376} = 2.65$   $2 < \frac{h_s}{d_{50}} < 4 \therefore \text{O.K.}$

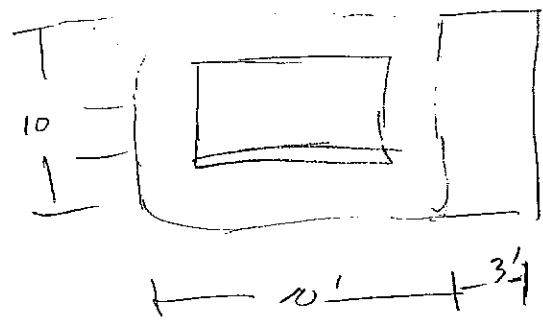
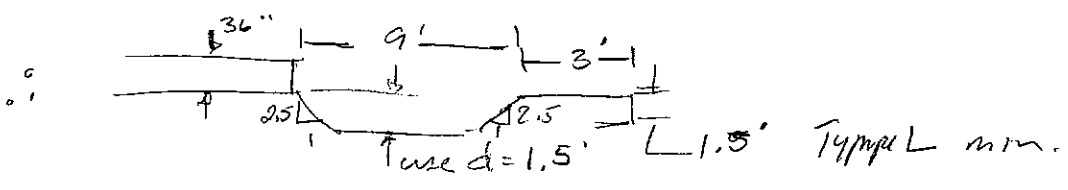
O.K.  
use  $d_{50} = 9''$   
 $h_s = 1.5'$

try  $\frac{d_{50}}{y_e} = .25$   $d_{50} = .47$

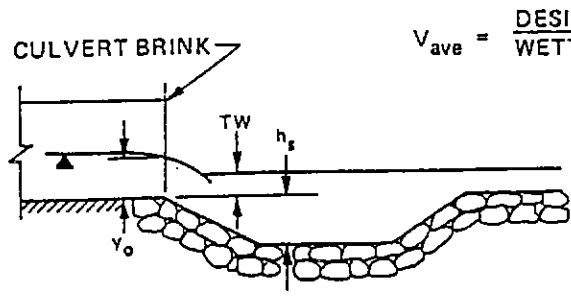
$\frac{h_s}{y_e} = .30$   $h_s = 0.56'$

$\frac{h_s}{d_{50}} = \frac{0.56}{.47} = 1.19$

SUBJECT \_\_\_\_\_



10/21  
C/KC  
9/1/90



$$V_{ave} = \frac{\text{DESIGN DISCHARGE} - Q}{\text{WETTED AREA AT BRINK OF CULVERT}}$$

$d_{50}$  = THE MEDIAN SIZE OF ROCK BY WEIGHT. ROUNDED ROCK OR ANGULAR ROCK.

$y_e$  = EQUIVALENT BRINK DEPTH  
 = BRINK DEPTH FOR BOX CULVERT  
 =  $\left(\frac{A}{2}\right)^{1/2}$  FOR NON-RECTANGULAR SECTIONS

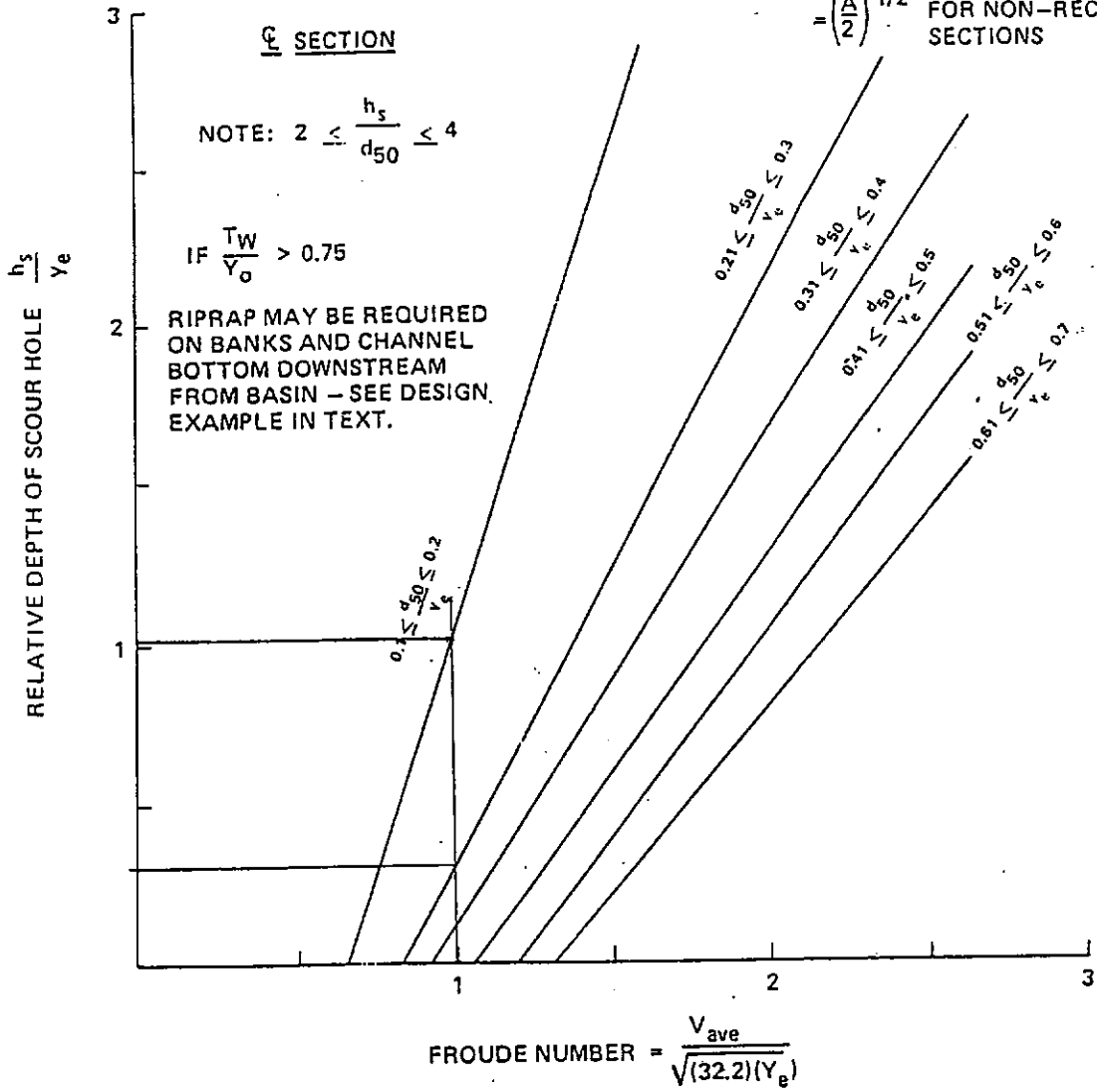


FIGURE 10-C.4 RELATIVE DEPTH OF SCOUR HOLE VERSUS FROUDE NUMBER AT BRINK OF CULVERT WITH RELATIVE SIZE OF RIPRAP AS A THIRD VARIABLE

TABLE 10.1 GEOMETRIC ELEMENTS FOR CIRCULAR SECTION

$\frac{y}{d_0}$	$\frac{A}{d_0^2}$	$\frac{P}{d_0}$	$\frac{R}{d_0}$	$\frac{T}{d_0}$	$\frac{D}{d_0}$	$\frac{A\sqrt{D}}{d_0^{5/2}}$	$\frac{AR^{2/3}}{d_0^{8/3}}$
0.01	0.0013	0.2003	0.0066	0.1990	0.0066	0.0001	0.0000
0.05	0.0147	0.4510	0.0326	0.4359	0.0336	0.0027	0.0015
0.10	0.0409	0.6435	0.0635	0.6000	0.0682	0.0107	0.0065
0.15	0.0739	0.7954	0.0929	0.7141	0.1034	0.0238	0.0152
0.20	0.1118	0.9273	0.1206	0.8000	0.1398	0.0418	0.0273
0.25	0.1535	1.0472	0.1466	0.8660	0.1774	0.0646	0.0427
0.30	0.1982	1.1593	0.1709	0.9165	0.2162	0.0921	0.0610
0.35	0.2450	1.2661	0.1935	0.9539	0.2568	0.1241	0.0820
0.40	0.2934	1.3694	0.2142	0.9798	0.2994	0.1603	0.1050
0.45	0.3428	1.4706	0.2331	0.9950	0.3446	0.2011	0.1298
0.50	0.3927	1.5708	0.2500	1.0000	0.3928	0.2459	0.1558
0.55	0.4426	1.6710	0.2649	0.9950	0.4448	0.2949	0.1825
0.60	0.4920	1.7722	0.2776	0.9798	0.5022	0.3438	0.2092
0.65	0.5404	1.8755	0.2881	0.9539	0.5666	0.4066	0.2358
0.70	0.5872	1.9823	0.2962	0.9165	0.6408	0.4694	0.2608
0.75	0.6318	2.0944	0.3017	0.8660	0.7296	0.5392	0.2840
0.80	0.6736	2.2143	0.3042	0.8000	0.8420	0.6177	0.3045
0.85	0.7115	2.3462	0.3033	0.7141	0.9964	0.7098	0.3212
0.90	0.7445	2.4981	0.2980	0.6000	1.2408	0.8285	0.3324
0.94 <sup>a</sup>	0.7662	2.6467	0.2896	0.4750	1.6130	0.9725	0.3353
0.95	0.7707	2.6906	0.2864	0.4359	1.7682	1.0242	0.3349
1.00	0.7854	3.1416	0.2500	0.0000	$\infty$	$\infty$	0.3117

<sup>a</sup>Maximum flow occurs at 0.94 full depth.

**Example 10.1**

For the channel section shown in Figure 10.2, determine the geometric elements.

**Solution**

$$y = 36 \text{ in. or } 3 \text{ ft} \quad d_0 = 60 \text{ in. or } 5 \text{ ft}$$

$$\frac{y}{d_0} = \frac{3}{5} = 0.6$$

From Table 10.1:

$$\frac{A}{d_0^2} = 0.492, \quad A = 0.492(5)^2 = 12.3 \text{ ft}^2$$

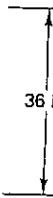
$$\frac{P}{d_0} = 1.7722, \quad P = 1.7722(5) = 8.861 \text{ ft}$$

$$\frac{R}{d_0} = 0.2776, \quad R = 0.2776(5) = 1.39 \text{ ft}$$

$$\frac{Z_c}{d_0^{5/2}} = \frac{A\sqrt{D}}{d_0^{5/2}} = 0.3438, \quad A\sqrt{D} = 0.3438(5)^{5/2} = 1.92$$

$$\frac{Z}{d_0^{8/3}} = \frac{AR^{2/3}}{d_0^{8/3}} = 0.2092, \quad AR^{2/3} = 0.2092(5)^{8/3} = 15.29$$

Figure 10.2 Partial full circular channel section of Example 10.1.



**10.3-TYPES OF FLOW**

The flow in an open channel is classified with respect to space and time. If the section of the channel, the flow is known as varied or nonuniform flow, the depth changes abruptly or gradually. If the change in the depth occurs abruptly, it is a rapidly varied flow; otherwise, it is a gradually varied flow.

If the depth of flow does not change with time, it is referred to as the steady flow. Combining the space and time criteria, flow is classified as follows:

Type of Flow
Steady uniform flow
Steady gradually varied flow
Steady rapidly varied flow
Unsteady gradually varied flow
Unsteady rapidly varied flow

For an unsteady uniform flow, the water surface always remains parallel to the channel bottom. Even the steady uniform flow is difficult to maintain in an irregular section and in artificial channels. The steady uniform flow, however, is a fundamental condition in all channel design problems. The effect of the unsteady flow condition to determine the characteristics of flow in natural streams, the steady flow condition is under consideration. The unsteady flow wave in the channel which is outside the scope of this chapter.

*Handwritten notes:* 1/11/14, 1/12/14, 1/13/14

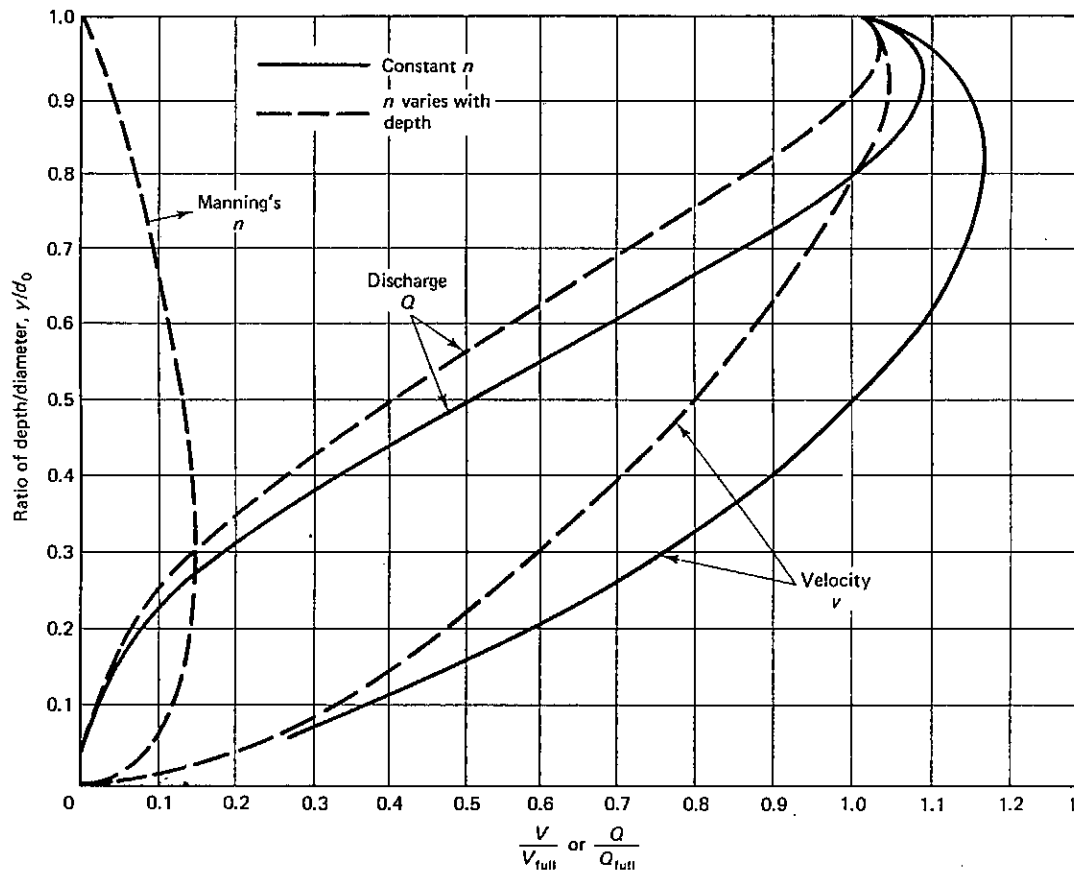


Figure 10.11 Hydraulic elements of a circular section.

**Solution**

1. From Table 10.4,  $n = 0.018$ .
2.  $S = \frac{1}{4500} = 2.22 \times 10^{-4}$ .
3.  $\frac{y_n}{d_0} = \frac{1.5}{3} = 0.5$ .
4. From Table 10.1,  $\frac{AR^{2/3}}{d_0^{8/3}} = 0.1558$ .
5.  $AR^{2/3} = 0.1558(3)^{8/3} = 2.92$ .
6.  $Q = \frac{1.49}{0.018} (2.92) (2.22 \times 10^{-4})^{1/2} = 3.60$  cfs.

**Alternative Solution** From Figure 10.11 for constant  $n$ ,  $y/d_0$  of 0.5,  $Q/Q_{full} = 0.5$ ,

$$Q_{full} = \frac{1.49}{0.018} \left[ \frac{\pi}{4} (3)^2 \right] \left( \frac{3}{4} \right)^{2/3} (2.22 \times 10^{-4})^{1/2} = 7.19 \text{ cfs}$$

$$Q = 0.5 Q_{full} = 0.5(7.19) = 3.60 \text{ cfs}$$

**Example 10.8**

A trapezoidal channel of 450 cfs with a normal depth of 685 ft. The channel area is 685 ft<sup>2</sup> if  $n = 0.02$ .

**Solution** Refer to Fig.

1. This is a problem
2.  $A = \frac{1}{2}(25 + 42) \cdot 685$   
 $P = 25 + 2 \cdot 685$   
 $R = \frac{A}{P} = \frac{685}{2.7}$
3.  $S = \left[ \frac{Q}{(1.49/n)AR} \right]^2$
4.  $\frac{H_1 - H_2}{L} = S$  or  
 $L = \frac{H_1 - H_2}{S}$

**Example 10.9**

The channel of Example (a) normal depth, (b) cri

**Solution**

- (a) 1.  $S = \frac{0.1}{100} = 0.001$
2.  $\frac{Qn}{S^{1/2}} = \frac{30(0.025)}{(0.001)^{1/2}}$
3.  $A = (4 + 4y)y$   
 $P = 4 + 2y$   
 $R = \frac{(4 + 4y)y}{4 + 2y}$

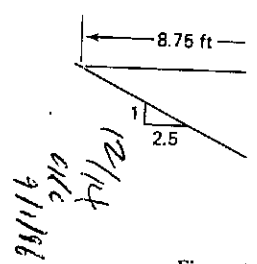


Figure 1





14/12  
CR 9/1/86

FHWA CULVERT ANALYSIS, HY-8, VERSION 4.1

CURRENT DATE 08-15-1996 CURRENT TIME 15:09:12 FILE NAME PPCC FILE DATE 08-15-1996

CULVERT AND CHANNEL DATA

CULVERT NO. 1 DOWNSTREAM CHANNEL

CULVERT TYPE: 3.0 FT CIRCULAR CHANNEL TYPE : TRAPEZOIDAL
CULVERT LENGTH = 47.0 FT BOTTOM WIDTH = 10.0 FT
NO. OF BARRELS = 1.0 TAILWATER DEPTH = -0.9 FT
FLOW PER BARREL = 55.0 CFS TOTAL DESIGN FLOW = 55.0 CFS
INVERT ELEVATION = 55.3 FT BOTTOM ELEVATION = 53.0 FT
OUTLET VELOCITY = 9.8 FPS NORMAL VELOCITY = 3.1 FPS

RIPRAP STILLING BASIN -- FINAL DESIGN

THE LENGTH OF THE BASIN = 12.0 FT
THE LENGTH OF THE POOL = 9.0 FT
THE LENGTH OF THE APRON = 3.0 FT
THE WIDTH OF THE BASIN AT THE OUTLET = 10.0 FT
THE DEPTH OF POOL BELOW CULVERT INVERT = 0.3 FT
\* THE THICKNESS OF THE RIPRAP ON THE APRON = 3.5 FT
\* THE THICKNESS OF THE RIPRAP ON THE REST OF THE BASIN = 2.6 FT
THE BASIN OUTLET VELOCITY = 3.6 FPS
THE DEPTH OF FLOW AT BASIN OUTLET = 1.5 FT

Type in Riprap

\* USE depth of 1.5' below culvert to lower Riprap thickness to 1.5' at all areas.

**EXHIBIT 5.3-1**  
**URS Consultants, Inc.**  
**CALCULATION COVER SHEET**

Client: URS Project Name: 1000  
Project/Calculation Number: 1000  
Title: Site  
Total number of pages (including cover sheet): 14  
Total number of computer runs: \_\_\_\_\_  
Prepared by: V. S. ... Date: \_\_\_\_\_  
Checked by: Charles H. Collier Date: 9/1/96

Description and Purpose:  
Site site mapping services

Design bases/references/assumptions:  
Rational Method

Remarks/conclusions:  
  
  
Calculation Approved by: Charles H. Collier 9/1/96

Project Manager/Date

Revision No.:	Description of Revision:	Approved by:
_____	_____	_____
_____	_____	_____
_____	_____	_____

Project Manager/Date

SUBJECT 71E DE-1000

determine flows for each drainage area.

#1

$A = 20.38A$   
 $HIC = 6818$   
 $low IC = 6774$   
 $length = 1300'$

Time of Conc:

$T = \left( \frac{11.92^3}{H} \right)^{.385} = .12 hr = 7.18 min.$

Rainfall Intensity

$i = \frac{7.25}{100} in/hr$  |  $CS = 4.5$   
 $T_c = 7 min$

Runoff

$Q = CiA$   
 $C = .45$  (15% imp.)

i.  $Q = \frac{.45(7.25)(20.38)}{100} = \underline{\underline{66.5 cfs}}$   
 $Q_5 = \underline{\underline{41.3 cfs}}$

#2

$A = 2.5$   
 $HIC = 6787$   
 $low IC = 6772$   
 $L = 900'$

T<sub>c</sub> = 7 min.

i.  $Q = CiA$   
 $C = .90$  (90% imp.)

$Q = \frac{.90(7.25)(2.5)}{100} = \underline{\underline{16.3 cfs}}$   
 $Q_5 = \frac{.90(4.5)(2.5)}{100} = \underline{\underline{10.1 cfs}}$

SUBJECT ...

#3

$$A = 3.32 \text{ Ac.}$$

$$H_i = 6787.$$

$$low = 6772.$$

$$L = 950.$$

$$T_c = 7.5 \text{ min.}$$

$$Q = C_i A.$$

$$C = .90 \quad \therefore Q = 3.32 (7.25) (.90) = \underline{\underline{21.7 \text{ cfs.}}}$$

$$Q_5 = \underline{\underline{13.4 \text{ cfs.}}}$$

#4

$$A = 12.94 \text{ Ac.}$$

$$H_i = 6818$$

$$low = 6775.$$

$$L = 1375$$

$$T_c = 7.7 \text{ min.}$$

$$Q = C_i A$$

$$C = .70 \text{ (65\% impervious)}$$

$$Q = .70 (7.25) (12.94) = \underline{\underline{65.6 \text{ cfs.}}}$$

$$Q_5 = 40.76.$$

SUBJECT 2-1-10-11

CURB INLET DESIGN

$Q_1 = 16.3 \text{ cfs.}$

$Q_2 = 45.4 \text{ cfs.}$

$Q_2 = 21.7 \text{ cfs.}$

Size Inlet: (NON-Depressed)

$Q = 3.04 d^{1.5}$

Solve for L.

$L = \frac{Q}{3d^{1.5}}$

For  $d = 0.5$ ,  $Q = 16.3$

$L = 15.3$

$d = 0.5$ ,  $Q = 21.7$

$L = 20.4$

(WEIR Flow)

$d = 0.7$ ,  $Q = 16.3$

$L = 9.12'$

$d = 0.7$ ,  $Q = 21.7$

$L = 12.3'$

$d = 0.7$   
 $Q = 45.6$

$L = 37.3'$

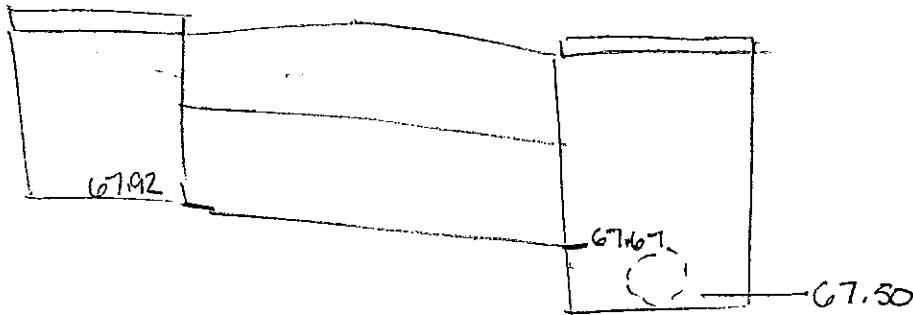
USE 10' or 15' inlet + 40' inlet.

TYPE R MC604-12

SUBJECT \_\_\_\_\_

SIZE CONCRETE AT INLET DISCHARGE  
 USE Chart 2.

INLET ①  $Q = 16.3 + 3.3 = 19.6 \text{ cfs.}$  } 24" 3.0' Depth  
 $Q_{50} = 10.01 + 1.93 = 11.94$  }  
 INLET ②  $Q = 19.6 + 21.7 = 41.3 \text{ cfs.}$  } 30" RCP 4.5' Basin  
 $Q_{50} = 11.94 + 13.4 = 25.34$  }  
 Inlet ③  $Q = 65.6 + 6.04 = 71.6 \text{ cfs.}$  } 42" RCP 4.5' Basin  
 $Q_{50} = 40.76 + 3.52 = 44.28$  } 30" " 6.0'



SUBJECT Final Design

Size Roof Drain collectors.

Use Rational Method.

Typical Area Drained =  $A = .33 \text{ Ac.}$

$C = .90$

$i_{100} = 9.0$

$L_5 = 5.25$

$t_c = 5 \text{ min}$

$Q_5 = .90(.33)(5.25) = \underline{1.50 \text{ cfs.}}$

$Q_{100} = .90(.33)(9) = \underline{2.67 \text{ cfs}}$

Area Drains

Area (A) - SW  $A = 1.078 \text{ Ac.}$

(B) SE  $A = 0.036$

(A)  $Q_5 = (.9)(1.078)(5.25) = 0.37 \text{ cfs.}$

$Q_{100} = (.9)(1.078)(9) = \underline{0.63 \text{ cfs.}}$

(B)  $Q_5 = .9(0.036)(5.25) = .140$

$Q_{100} = .9(0.036)(9) = \underline{0.14 \text{ cfs.}}$

R4030-15" DRAIN  
IN 15" RCP.

(C)  $A = 1.07$

$Q_5 = (.9)(5.25)(1.07) = \underline{5.06 \text{ cfs}}$

$Q_{100} = (.9)(9)(1.07) = \underline{8.67 \text{ cfs.}}$

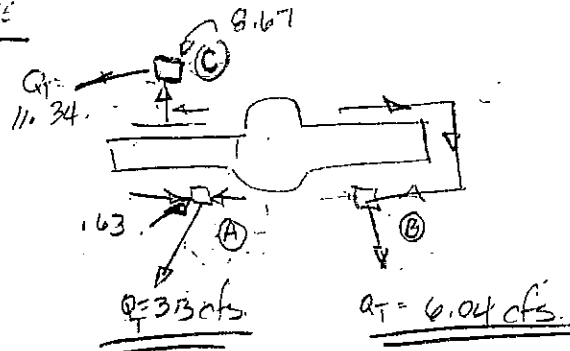
Use Type B inlet.



SUBJECT Site Drainage

SIZE DRAIN PIPE

- (A) Area ( )  
Q = 3.3 cfs
- (B) 6.04 cfs
- (C) 11.34 cfs



PIPE SIZE

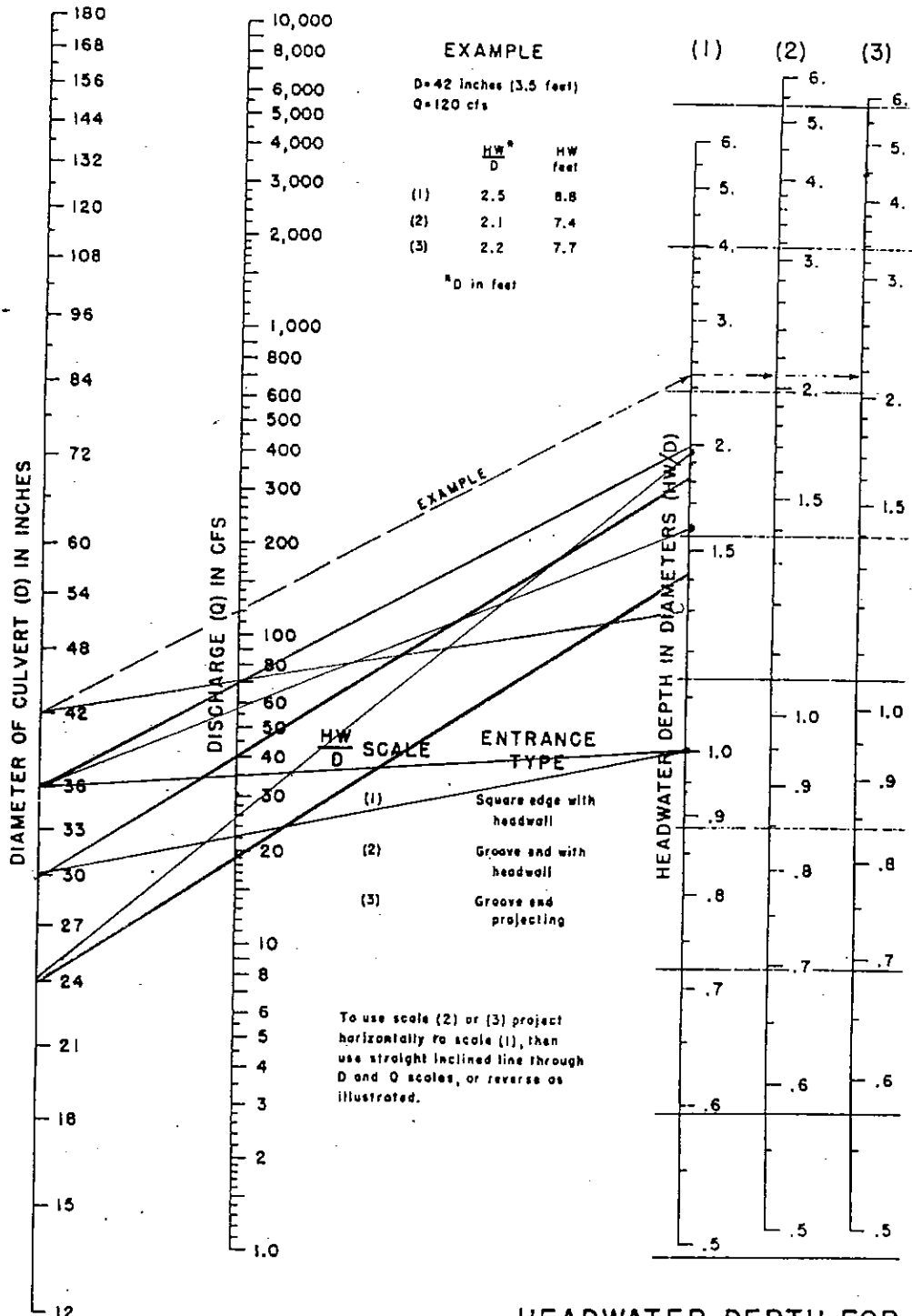
	Slope			
	1.0%	1.5%	2.0%	2.5
Q = 3.3	.97 (12")	.90	.85	.82 (10 1/2")
Q = 6.04	1.22 (14")	1.13	1.07	1.03 (12")
Q = 11.34	1.54 (18")	1.43	1.36	1.30 (18")
Q = 2.67	.9 (10")	.83	.79	.76 (10")

REMARKS

- Area (A) - 10" DRAIN CINE PVC
- (B) - 12" PVC
- (C) - 18" RCP

8/13  
 c/c 7/1/96

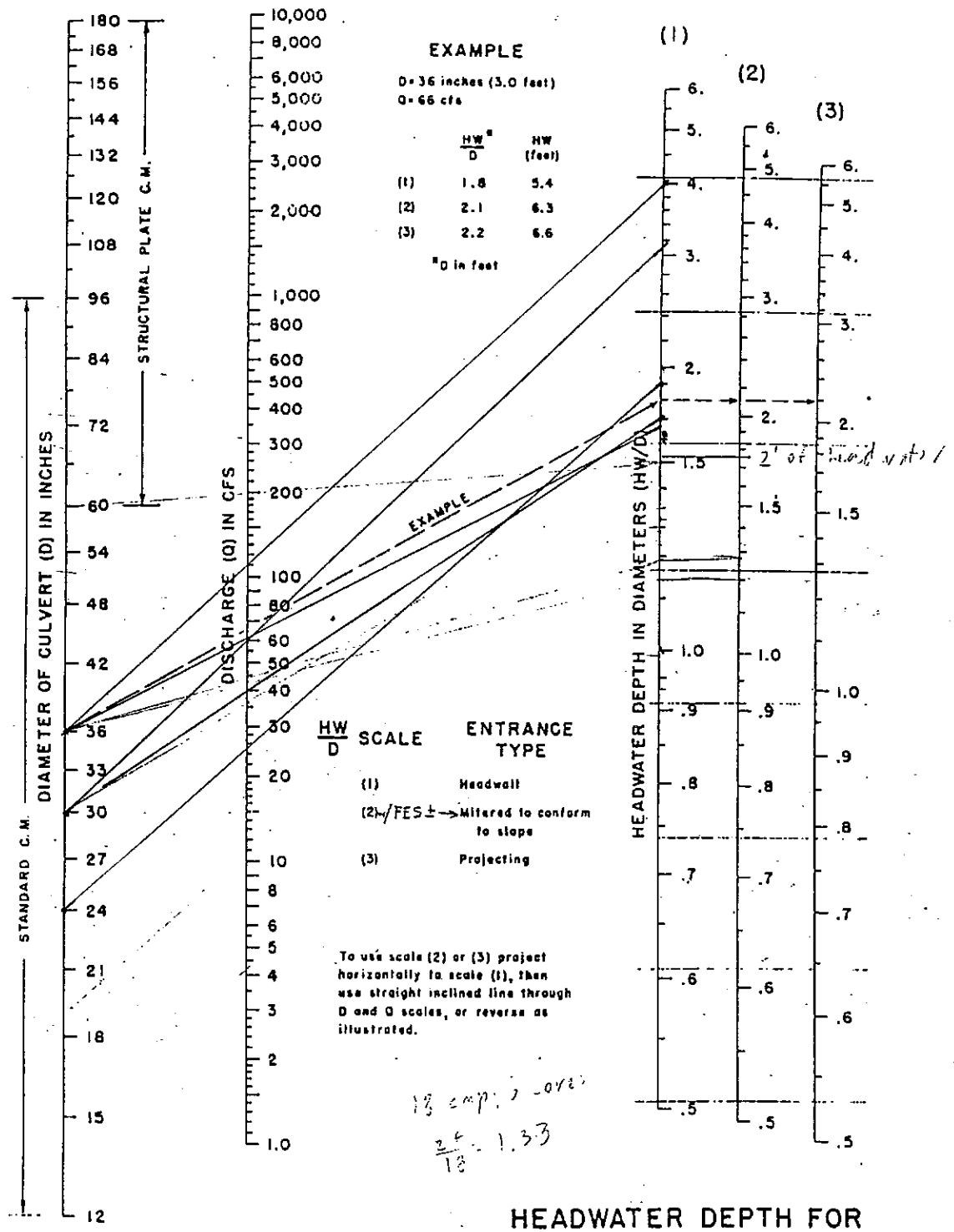
# CHART 2



HEADWATER DEPTH FOR  
 CONCRETE PIPE CULVERTS  
 WITH INLET CONTROL

4/11/96

# CHART 5

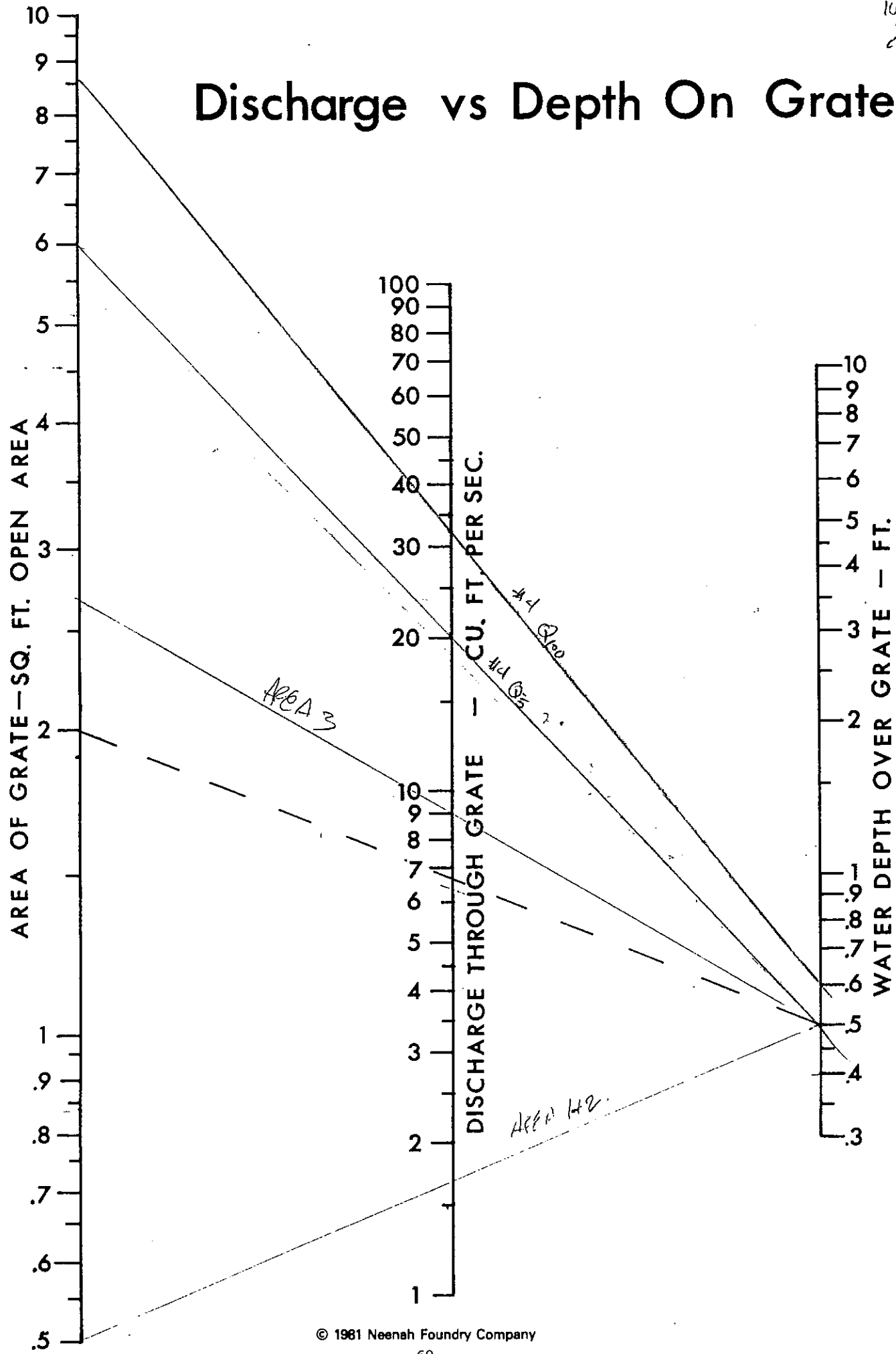


BUREAU OF PUBLIC ROADS JAN 1963

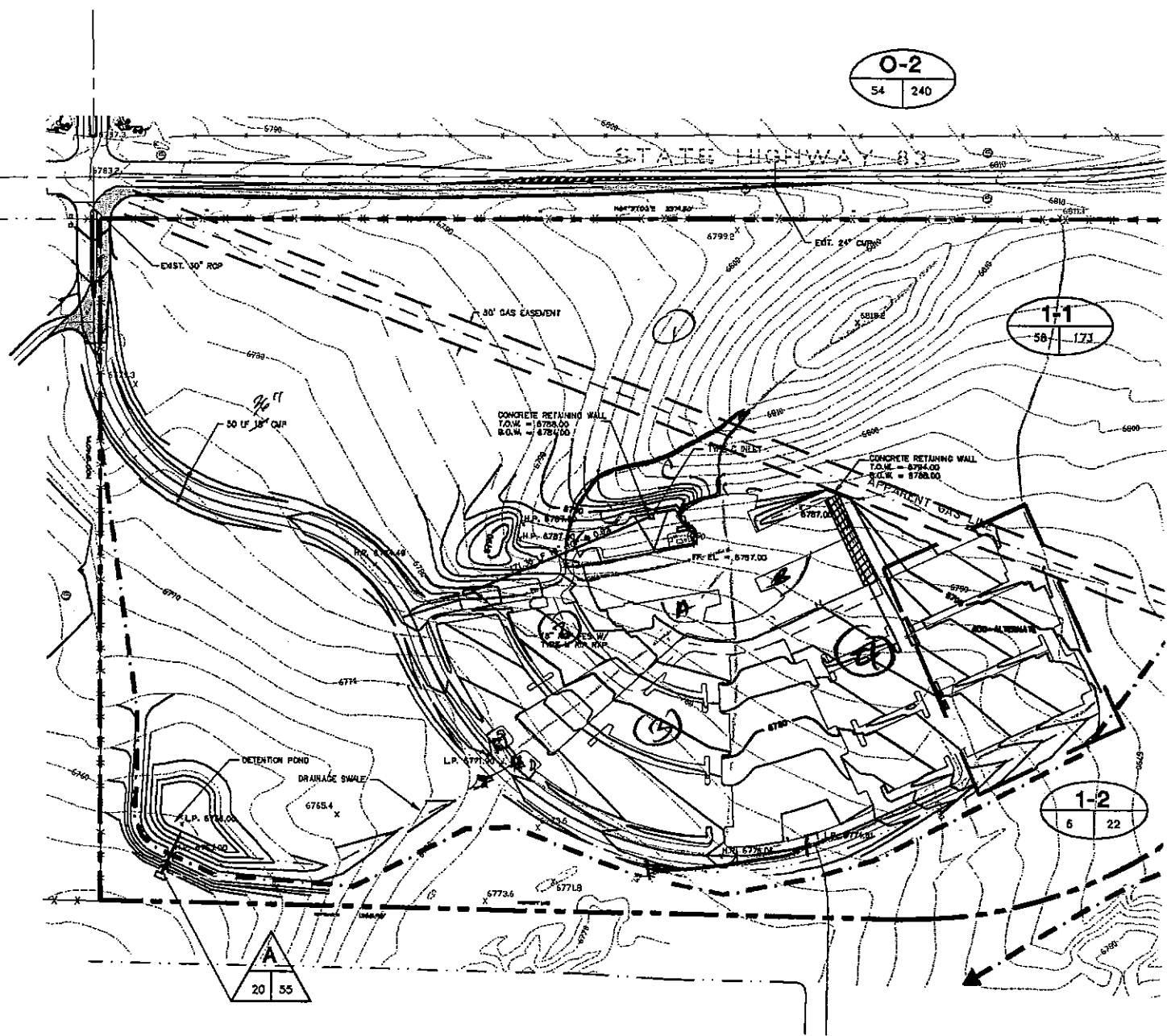
## HEADWATER DEPTH FOR C. M. PIPE CULVERTS WITH INLET CONTROL

10/17/96  
CKC 9/1/96

# Discharge vs Depth On Grate



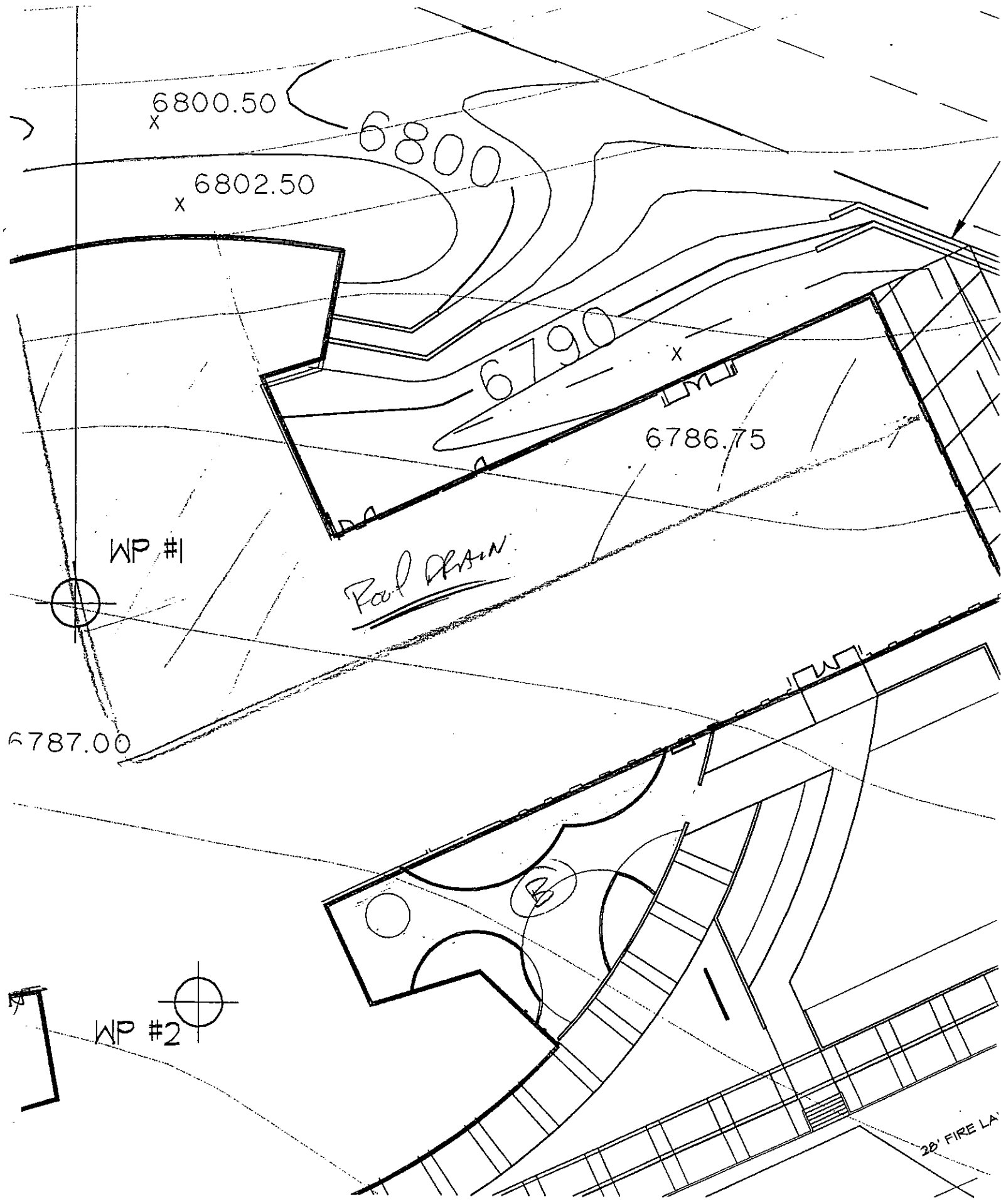
17/13  
etc 9/1/86



1" = 300'



1/1/83  
C/R 9/1/86



6800.50  
x

6802.50  
x

6800

6790  
x

6786.75

WP #1

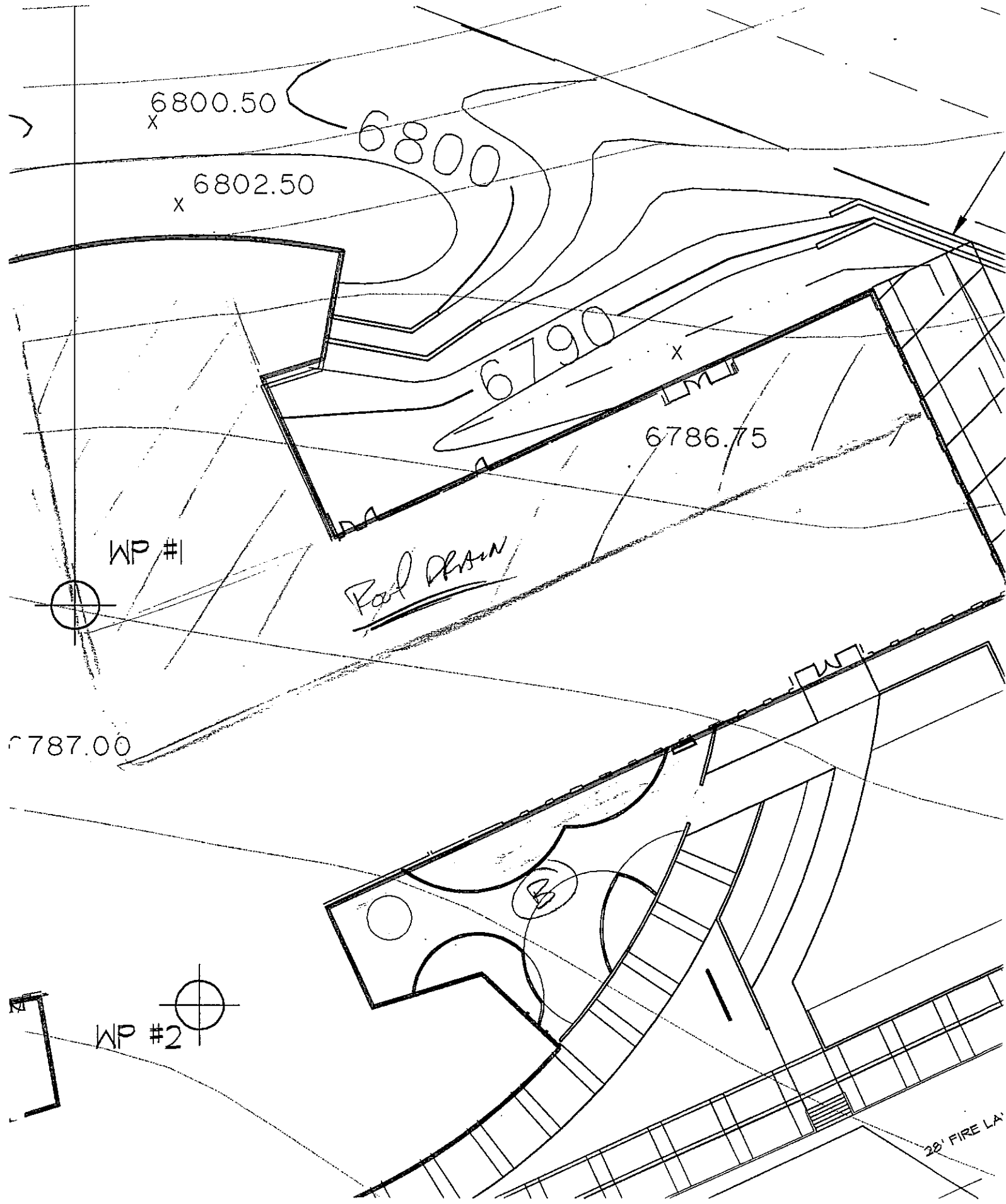
Paul Olson

6787.00

WP #2

28' FIRE LA'

13<sup>A</sup>/13  
etc 11/14



6800.50  
x

6800

6802.50  
x

6790  
x

6786.75

WP #1

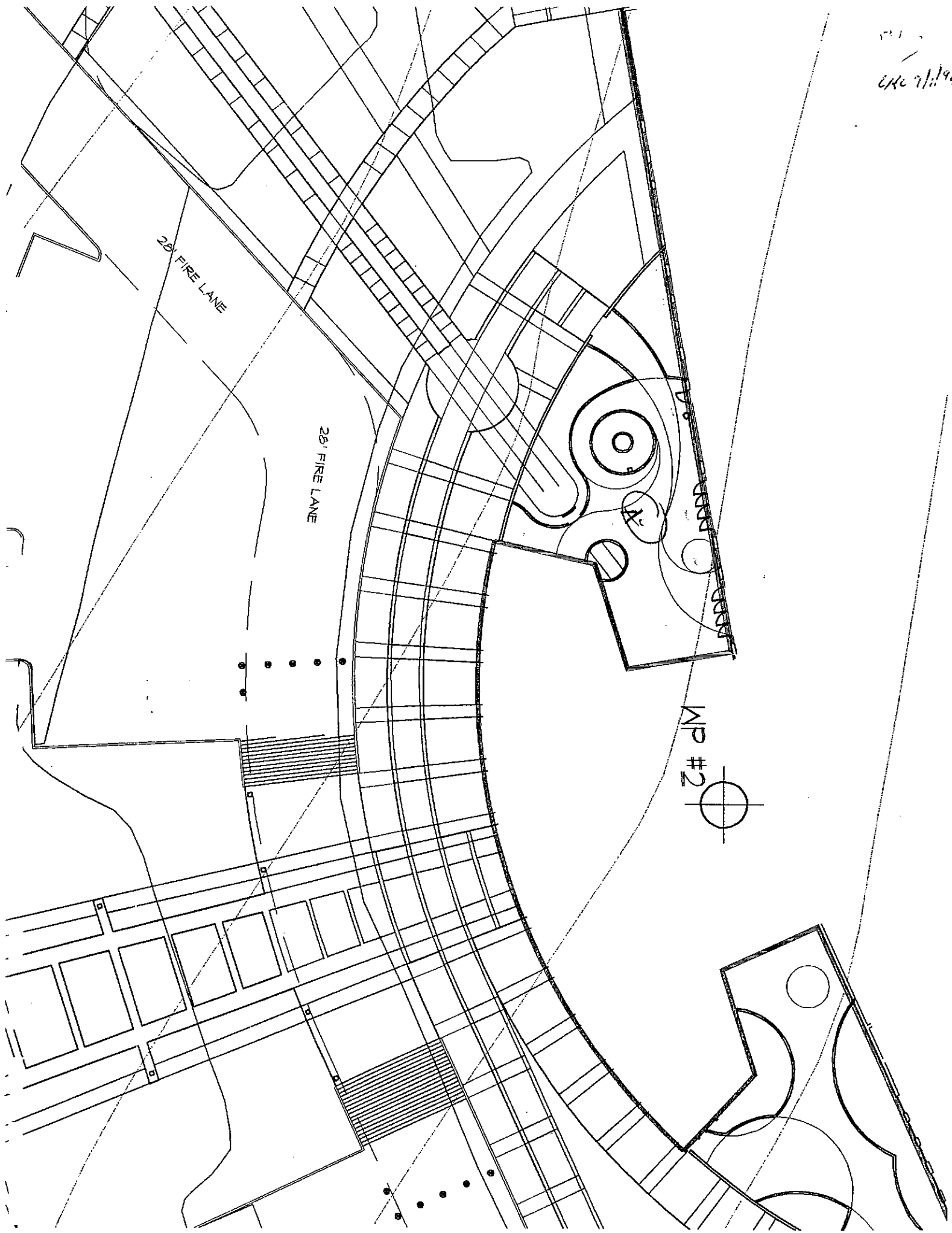
Pool Basin

6787.00

WP #2

28' FIRE LA'

21  
C/KC 7/1/98



28' FIRE LANE

28' FIRE LANE

NIP #2

