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**DESIGN ANALYSIS REPORT  
FOR  
PIKES PEAK GREENWAY TRAIL  
LOW WATER CROSSING AT  
FOUNTAIN CREEK**



**JR ENGINEERING**  
A Subsidiary of JRC



**DESIGN ANALYSIS REPORT  
FOR  
PIKES PEAK GREENWAY TRAIL  
LOW WATER CROSSING AT  
FOUNTAIN CREEK**

June 2001

Prepared For:  
**CITY OF COLORADO SPRINGS  
FLOODPLAIN ADMINISTRATION**  
101 West Costilla  
Colorado Springs, CO 80903  
(719) 327-2880

Prepared By:  
**JR ENGINEERING**  
4310 ArrowsWest Drive  
Colorado Springs, CO 80907  
(719) 593-2593

9247.20

**DESIGN ANALYSIS REPORT FOR  
PIKES PEAK GREENWAY TRAIL LOW WATER  
CROSSING AT FOUNTAIN CREEK**

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# **DESIGN ANALYSIS REPORT FOR PIKES PEAK GREENWAY TRAIL LOW WATER CROSSING AT FOUNTAIN CREEK**

## **PURPOSE**

The purpose of this project is to enhance and lengthen the popular Pikes Peak Greenway Trail and allow it to continue south of the creek and city.

## **BACKGROUND**

The Pikes Peak Greenway Trail runs along the corridor of Fountain Creek as it travels through the City of Colorado Springs. In 1996, the Parks and Recreation Department built a low water crossing across Fountain Creek along with major trail improvements and additions. After a storm in 1999, the low water crossing was washed out and now lies in a heap along the bank of the creek. A large portion of the northern bank of the creek has also been eroded as an effect of this storm. In addition to the modifications that the Parks and Recreation Department have made to the creek, there have also been large amounts of soil and debris dumped along the banks of the creek.

## **PREVIOUS REPORTS**

In 1994, Muller Engineering Company, Inc. performed a Drainage Basin Planning Study for Fountain Creek. In their report they detailed creek improvements including sloping boulder drops, acquiring property in frequently flooding areas, and adding trails and look-out stations to make the area more aesthetically pleasing. Among other locations, this report suggested the placement of sloped boulder drops at stations 164+00, 154+00, 150+30, and 150+20, which are between the Nevada Street Bridge and the natural confluence with Shooks Run.

There is also information on Fountain Creek in the Federal Emergency Management Act (F.E.M.A.) Flood Insurance Study (F.I.S.) publications. According to the F.I.S., the F.I.S. water surface elevations are based on a study prepared by the United States Army Corp of Engineers (A.C.O.E.) Flood Plain Information study on Fountain Creek in Colorado Springs and Fountain in 1973. Appendix A contains parts of the F.E.M.A. Flood Insurance Rate Map (F.I.R.M.) panels #08041C0729F and #08041C0737F, which

encompass the project location. The proposed project is located in Zone AE as indicated on these F.I.R.M. panels.

### **GENERAL LOCATION**

The project location is just downstream of the Nevada Avenue Bridge over Fountain Creek and just upstream of the natural confluence with Shooks Run. Appendix A contains a map of the project location. As shown on Project Plan Sheet 4 in Appendix D, the proposed low water crossing and trails begin at the existing trail on the north side of the creek, crosses over the creek and continues downstream to an existing trail. The proposed low water crossing is at the same location as the previous one and the additional creek improvements are in close proximity to and resemble those of the Drainage Basin Planning Study by Muller Engineering.

### **TOPOGRAPHIC INFORMATION**

Since there have been numerous studies performed along Fountain Creek, the changes in the bed elevations can be traced. Appendix A contains a contour map with FIMS contours supplemented by JR Engineering contour data and A.C.O.E./F.E.M.A. contours overlaid. According to the contour maps used by the A.C.O.E. for the F.E.M.A. F.I.S. in 1973 and shown in Appendix A, the bed elevation of the creek near the proposed structure was approximately 5886.3 feet. In 1994, Muller Engineering Company reported the bed elevation to be 5887.8 feet and in 2001 the survey data collected by JR Engineering shows the bed elevation to be 5883.1 feet. Appendix B contains two graphs showing the comparison between F.E.M.A. elevations and the most recent survey data. The first is a comparison of elevations for a cross section near the proposed structure. This graph shows the F.E.M.A., F.I.M.S. and JR Engineering elevations, as well as the creek after the proposed project. The second graph shows the channel bed slope according to the different elevation data and for the proposed project. There have been several major storms in Fountain Creek since 1973, which can explain some of the changing bed elevations. Between 1973 and 2001 the creek slope in this area has changed from .63% to a more stable .4%. In 1994, there appeared to be a significant change in elevation (a head cut) just downstream of the confluence with Shooks Run and now, the significant change in bed elevation appears to have moved upstream to be closer to the Nevada Avenue Bridge. Based on the comparison of the 1973 F.E.M.A. contours to current F.I.M.S. contours, supplemented by JR Engineering contour data, it appears

that substantial fill has been added on both sides of the banks in the vicinity of the low water crossing. This can be seen in the contour map in Appendix A.

### **HYDRAULIC ANALYSIS**

According to the effective F.E.M.A. Flood Insurance Rate Study (F.I.S.), the 100-year flow rate in the project reach is 44,700 cfs. Using this flow rate and cross section data from F.E.M.A.'s HEC-2 analysis and contour maps, 100-year floodplain and floodway levels were estimated using the HEC River Analysis System (HEC-RAS). All modeled conditions were run in sub-critical flow regime, as were runs in F.E.M.A.'s original flow analysis.

Four cross sections were used to model the section of Fountain Creek near the proposed low water crossing. The most upstream cross section for the models, STA 157+00, is at the same location as F.E.M.A. Flood Insurance Rate Map (F.I.R.M.) cross section "DT." Similarly, the most downstream cross section, STA 144+00, is at the same location as F.E.M.A. F.I.R.M. cross section "DS." The locations of these cross sections can be seen in the contour map in Appendix A. The original HEC-2 input from the F.E.M.A. F.I.R.M. Study was not available from F.E.M.A. so HEC-2 input was obtained locally. This input was used for both cross sections STA 157+00 and STA 144+00 for each of the models.

The first model is a Duplicate Effective. This model has only two cross sections, 157+00 and 144+00, and models the local HEC-2 input in HEC-RAS in order to duplicate the published base flood elevations in the F.E.M.A. F.I.S. Although HEC-2 and HEC-RAS are different versions of the same program, they do have a tendency to give different results due to slightly different methods of calculations. The F.I.S. base flood elevations were matched at the lower cross section without adjustment. At the upper cross section, the "n" values were adjusted to match the F.I.S. base flood elevation.

The second model, the Modified Effective, represents the Duplicate Effective model with cross sections added near the low water crossing. The added cross sections were defined from the contour map used for the original flood study. In the overbank areas, the cross sections were defined to represent an average condition of the general area, as the topography varies considerably within the area. Localized depressions such as Shooks Run were omitted.

The next model shows the pre-project conditions or the present-day conditions. The cross sections at the F.I.S. locations were kept the same as previous models while the cross sections near the proposed low water crossing, STA 152+79 and STA 152+81, were adjusted based on the recent survey data, collected by JR Engineering, for this Pre-Project Model. This model shows that the base flood elevations have increased since the F.E.M.A. F.I.S. This increase is caused by the apparent previously mentioned fill added on both sides of the creek that can be seen in the contour map in Appendix A.

The last of the models is the Post-Project Model which models how the creek will function after the proposed low water crossing, creek improvements and grading have been done. The model indicates that the base flood elevations will decrease from the existing condition base flood elevations with completion of the project.. The chart in Appendix B compares the base flood elevations for the different models. HEC-RAS generated profiles, elevation reports and cross sections for each of the four models are contained in Appendix C. The proposed structure and creek improvements do not impede the original F.E.M.A. creek bed or have an apparent negative affect on the existing 100-year flood elevations as seen in the cross section elevation comparison, bed slope elevation comparison and base flood elevation chart in Appendix B.

## **SUMMARY OF PROPOSED IMPROVEMENTS**

There are several types of proposed improvements along this stretch of Fountain Creek including trails and grading, a low water crossing, a sloped boulder drop, and rip-rap protection along the banks. Plan Sheets 3 through 5, found in Appendix D provide details of the proposed improvements.

Approximately 415 feet of concrete trails will be added to the existing trails along Fountain Creek. The 290 feet of trail on the north side of the creek will begin at the existing trail where it was washed out by previous storms and then turn towards the creek and slope down at 8.3% to the low water crossing. The 125 feet of trail on the south side will begin at the low water crossing and slope up at 4.0%, curve to be parallel to the creek and connect to the existing gravel trail. Some gravel trail on both the north and south sides of the creek will need to be removed and possibly replaced.

The proposed low water crossing is a reinforced concrete bridge structure that will span the distance between banks of the creek allowing normal flows to pass below the path while limiting the amount of mass blocking the creek during larger flows. With an opening of 1.5 feet, an estimated flow of approximately 380 cfs will flow under the deck of the structure without over topping it. A table of the results of various methodologies used to estimate the low flow conveyance capacity is in Appendix B. The table indicates flow rates yielding a maximum elevation of 5885, the bottom of the crossing slab, and 5886, the top of the crossing slab. The calculations that produced the data contained in the summary table are also contained in Appendix B. It is estimated that a flow greater than the capacity of the opening of the structure will occur 2-3 times every year. This estimation is based on the past 25 years worth of peak flow rates through the creek measured from U.S.G.S. at gage 07105500 near the Tejon and Nevada Street Bridges. A graph of these peak daily flows is contained in Appendix B. It was determined from the data on the graph that if the capacity of the low water crossing is 380 cfs, it would be usable, on average, for 97% of the days in a given year which is only 10 days of being over topped. A table of low flows through Fountain Creek, located in Appendix B, provides more detail to these historic flow rates. Project Plan Sheets 6 and 7 show the structural details of the low water crossing.

The proposed sloped boulder drop begins at STA 153+16.88 and continues to STA 152+63.68. This is approximately 115 feet downstream from the proposed location of a drop structure in the Fountain Creek Drainage Basin Planning Study (D.B.P.S.) and does not interfere with the other proposed drop locations. Appendix B contains a diagram showing the locations of these drop structures as proposed in the D.B.P.S. The proposed drop for this project will have a 1:5 slope and a drop of 2.5 feet. Boulders with a minimum diameter of 3-feet grouted-in-place along with several hard point grade control structures have been included in the design to maintain the integrity of the drop. The D.B.P.S. specified 24" diameter boulders and no hard point grade control structures. Plan Sheets 8 and 9 show details of the sloped boulder drop.

Because the water and soil in the creek are constantly moving, bank protection is needed to help stabilize the trail and crossing. Rip rap with a  $d_{50} = 24"$  to be grouted in place, is proposed on both sides of the creek and trails. In addition to the permanent rip-rap, reinforcement matting will be placed along the trail and some graded areas to facilitate vegetation re-growth. Plan Sheet 3 shows the location of the proposed reinforcement matting and Sheet 4 shows the location of the rip rap.




**CONCLUSION**

Currently, Fountain Creek between the Nevada Avenue Bridge and Shooks Run is an eyesore. Parts of the banks are washed out, the existing trail ends abruptly, and there is a pile of concrete rubble from the remains of the last low water crossing. This proposed project will reconnect the currently segmented trail. The project calls for removal of the rubble pile, removal of the old gravel and broken asphalt trail, and the addition of 415 feet of new concrete trail. Not only will this project enhance the Pikes Peak Greenway Trail, but it will also help to stabilize Fountain Creek. The proposed drop structure will create a more stable creek bed and the rip rap bank protection will reduce the erosive effects of future storms. Also, the low water crossing is proposed to be five feet lower than the previous one allowing large storms to freely overtop it. Moreover, the fact that the low water crossing is constructed on caissons that are approximately 18' long, and the low water crossing is tied to the drop structure which is secured to bedrock gives it additional stability. The Fountain Creek D.B.P.S. prepared in 1994 suggested additional trails, creek improvements, and the acquisition of property adjacent to the creek in this section of Fountain Creek. This project is the first step to making the Fountain Creek floodplain a safer place to be and fulfilling the suggestions of the Fountain Creek D.B.P.S.

PREPARED BY:

**JR Engineering**

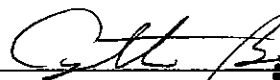


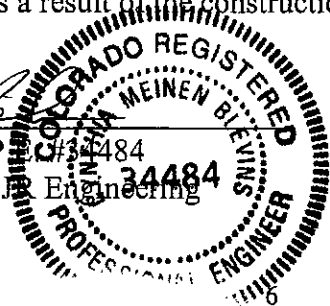
Julie Anne Wildschut, E.I.,  
Design Engineer I

/kd/9247.20/Greenway Report

**ENGINEER'S STATEMENT:**

The above letter, report and attachments were prepared under my direction and supervision and are correct to the best of my knowledge and belief. The evaluation performed for this report indicates that no significant increase to the existing flood elevation will occur as a result of the construction of the proposed improvements.

  
Cynthia M. Blevins, P.E. #34484  
For and On Behalf of JR Engineering



7-03-01  
Date

## **BIBLIOGRAPHY:**

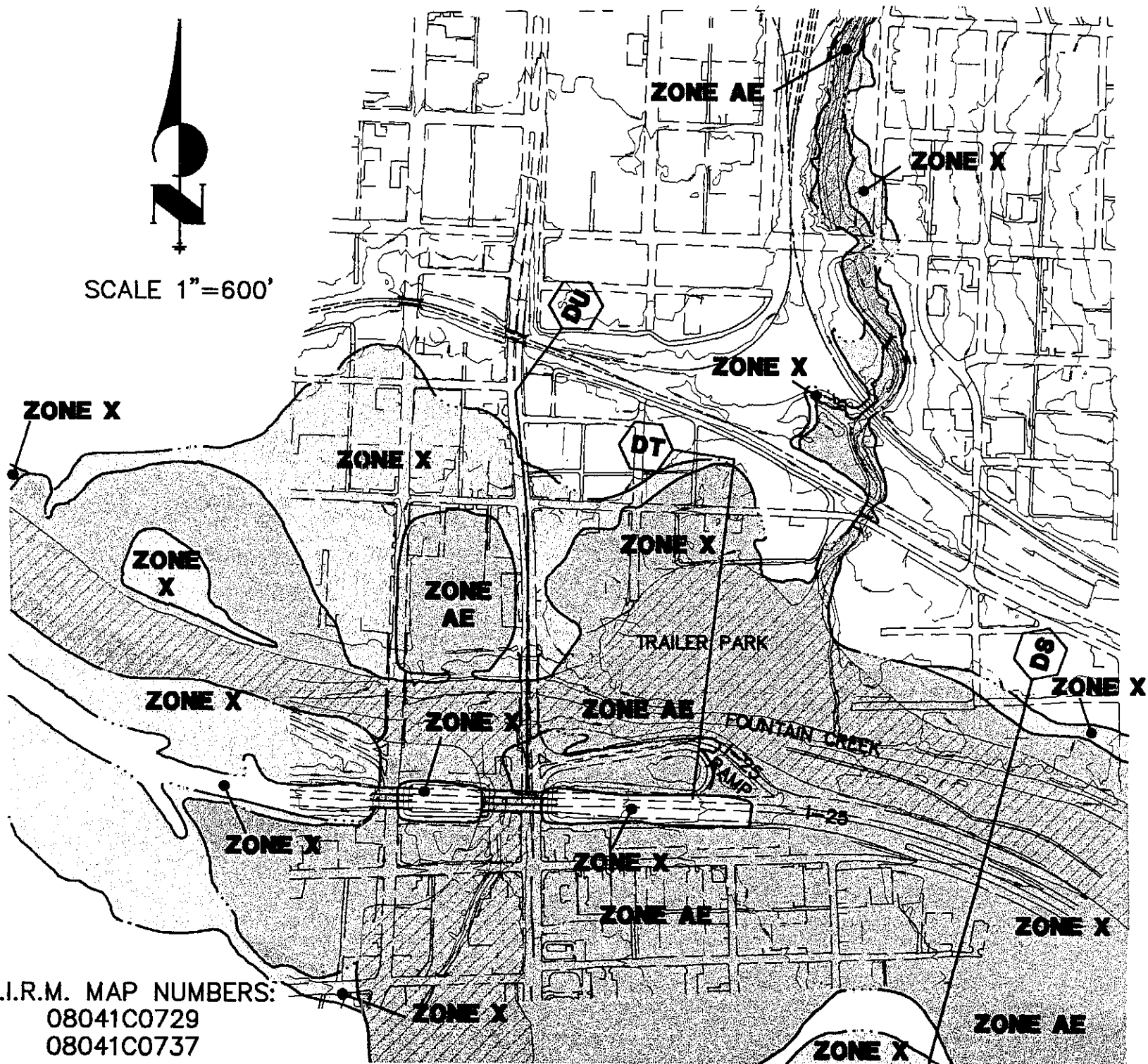
1. Federal Emergency Management Agency 1990. Flood Insurance Study for the City of Colorado Springs. Washington, D.C.
2. Federal Emergency Management Agency 1997. Flood Insurance Rate Map, El Paso County, Colorado and Incorporated Areas, Panels #08041C0 729F and 737F. Washington, D.C.
3. Muller Engineering Company, Inc. 1994. Fountain Creek Drainage Basin Planning Study. Prepared for The City of Colorado Springs, Colorado.
4. U.S. Army Corps of Engineers, Albuquerque District 1973. Floodplain Information, Fountain Creek and Jimmy Camp Creek, Colorado Springs and Fountain, El Paso County, Colorado. Prepared for Pikes Peak Area Council of Governments.
5. US Geological Survey data for gage 07105500 on Fountain Creek near Tejon and Nevada via USGS website, [www.usgs.gov](http://www.usgs.gov)

## **APPENDIX A**

**F.E.M.A. F.I.R.M. MAP**

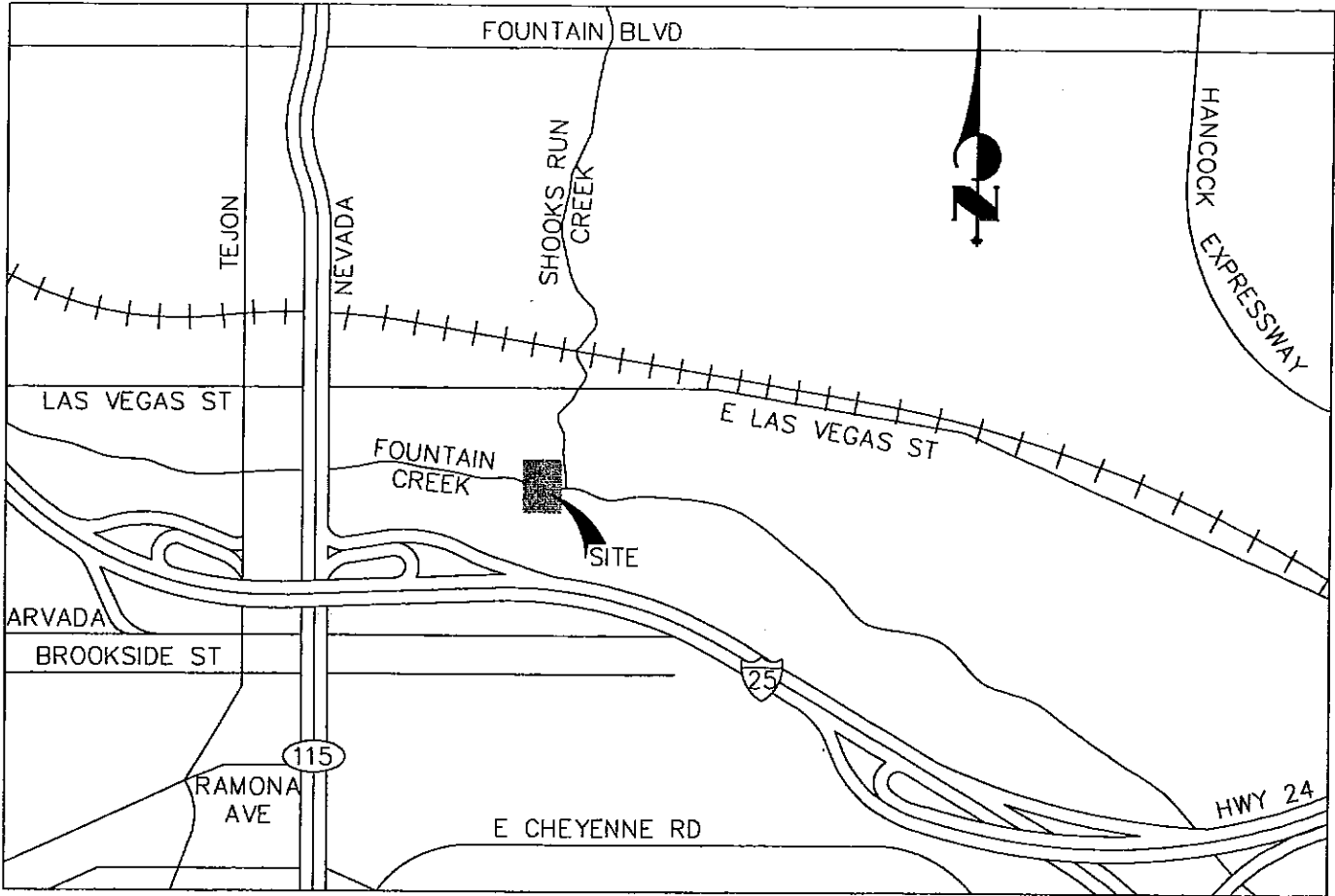


SCALE 1"=600'



F.I.R.M. MAP NUMBERS:  
08041C0729  
08041C0737

**VICINITY MAP**



**VICINITY MAP**

NTS

**CONTOUR MAP**



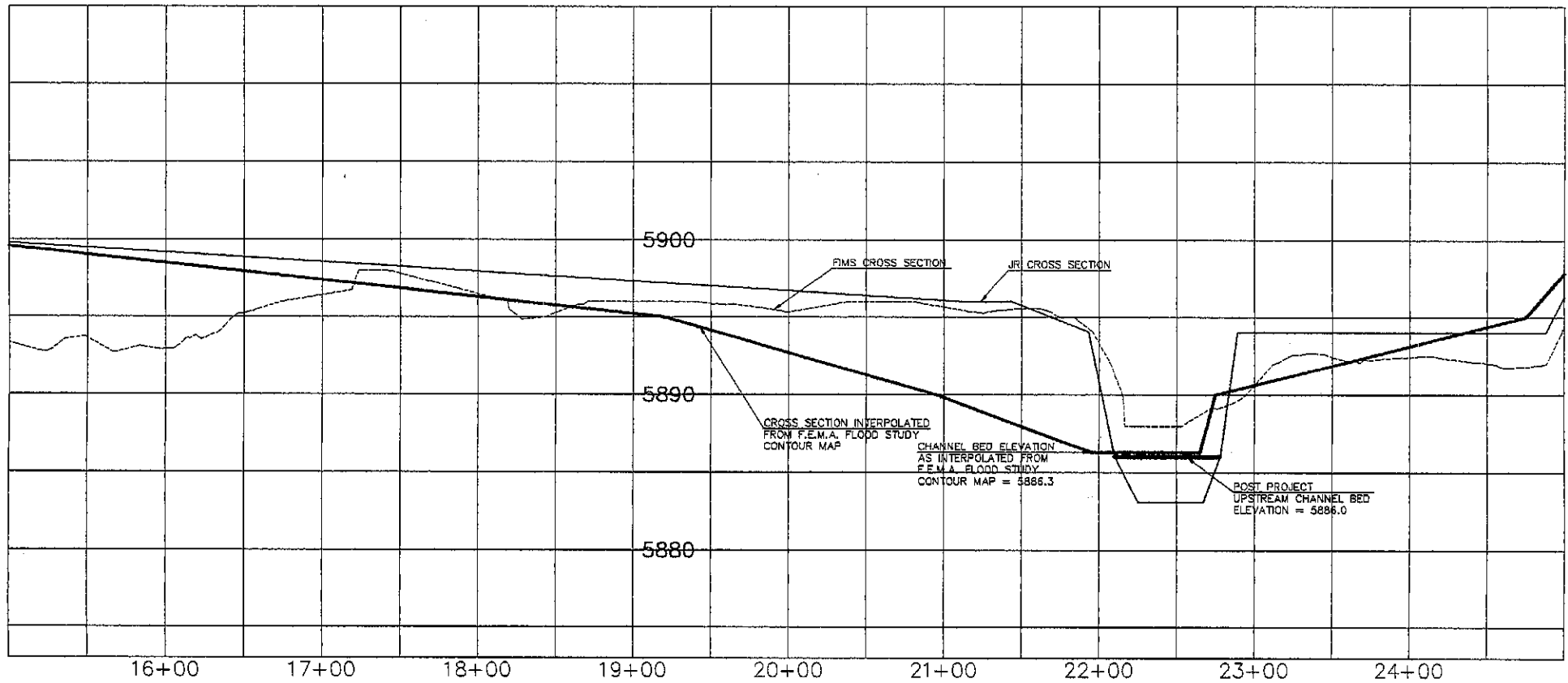
**APPENDIX B**

**COMPARISON OF CROSS SECTIONAL ELEVATIONS AT PROPOSED  
STRUCTURE**

# COMPARISON OF CROSS SECTION ELEVATIONS AT PROPOSED STRUCTURE

SCALE: 1" = 100' HORIZ

1" = 10' VERT



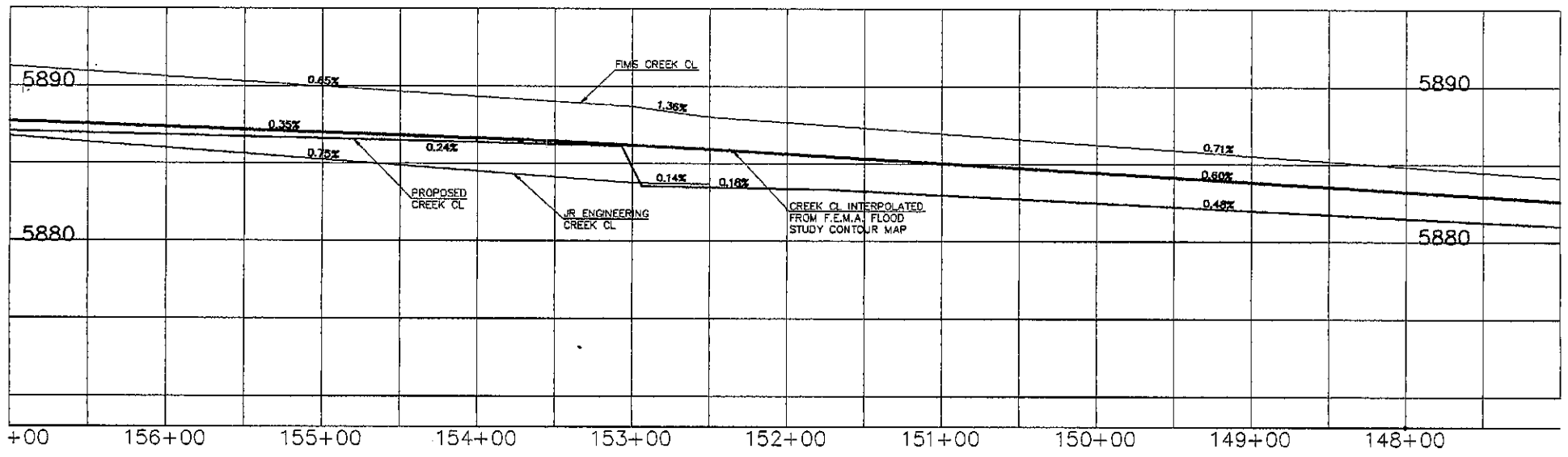
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**COMPARISON OF BED SLOPE ELEVATIONS**

### COMPARISON OF BED SLOPE ELEVATIONS

SCALE: 1" = 100' HORIZ

1" = 10' VERT



**COMPARISON OF BASE FLOOD ELEVATIONS**

## Comparison of Base Flood Elevations in Different Models

### Station 157+00

Model	Effective (F.E.M.A.)	Duplicate Effective	Modified Effective	Pre-Project	Post-Project
Floodplain WSE	5903	5903.03	5903.03	5906.09	5904.82
Increase in Floodplain WSE from Preceding Model	NA	0.03	0	3.06	-1.27
Floodway WSE	5903	5902.87	5902.86	5907.54	5906.36
Increase in Floodway WSE from Preceding Model	NA	-0.13	-0.01	4.68	-1.18
Floodway Width	800	794	794	800	800

### Station 152+81

Model	Effective (F.E.M.A.)	Duplicate Effective	Modified Effective	Pre-Project	Post-Project
Floodplain WSE	NA	NA	5898.98	5901.92	5900.88
Increase in Floodplain WSE from Preceding Model	NA	NA	NA	2.94	-1.04
Floodway WSE	NA	NA	5899.33	5902.9	5902.02
Increase in Floodway WSE	NA	NA	NA	3.57	-0.88
Increase in Floodway WSE from Preceding Model	NA	NA	647	579	521

### Station 152+79

Model	Effective (F.E.M.A.)	Duplicate Effective	Modified Effective	Pre-Project	Post-Project
Floodplain WSE	NA	NA	5898.96	5901.91	5900.75
Increase in Floodplain WSE from Preceding Model	NA	NA	NA	2.95	-1.16
Floodway WSE	NA	NA	5899.32	5902.89	5901.77
Increase in Floodway WSE from Preceding Model	NA	NA	NA	3.57	-1.12
Floodway Width	NA	NA	646	578	518

**Station 144+00**

Model	Effective (F.E.M.A.)	Duplicate Effective	Modified Effective	Pre-Project	Post-Project
Floodplain WSE	5891.6	5891.62	5891.62	5891.62	5891.61
Increase in Floodplain WSE from Preceding Model	NA	0.02	0	0	-0.01
Floodway WSE	5891.9	5891.79	5891.79	5891.79	5891.79
Increase in Floodway WSE	NA	-0.11	0	0	0
Increase in Floodway WSE from Preceding Model	400	400	400	400	400



**LOW FLOW CONVEYANCE CAPACITY CALCULATIONS**

## Table of Predicted Low Flows Passing Through Low Water Crossing

### Flow UNDER Low Water Crossing

<u>Method</u>	<u>Flow Rate (cfs)</u>
Mannings Formula (water touching bottom of crossing slab)	168
Mannings Formula (water NOT touching bottom of crossing slab)	180
Flow Master	160
HEC-RAS	166

### Flow to TOP of Low Water Crossing (but not over topping)

<u>Method</u>	<u>Flow Rate (cfs)</u>
Flow Master	380
HEC-RAS	317
Orifice Equation	426
Culvert Nomograph	426

Allowable flows under the low water crossing are at an elevation of 5885 whereas flows to the top of the low water crossing are at 5886. Flows corresponding to these elevation limits were calculated by several different methods.

Manning's Formula was used twice. The first represented the situation where the water moving under the low water crossing was assumed to be touching the ground, creek banks, and concrete on the piers and slab of the low water crossing. This is the most conservative Manning's Formula method. The second may be more representative of true conditions because when the water flows through the crossing, if it touches the top slab before going through, it will dip slightly so that it will not be touching the slab the whole way through the crossing. Flow Master was used for both elevation limits by inputting the typical cross section at the proposed low water crossing and finding the flows through it at the two elevations. HEC-RAS was also used for both elevation limits in a similar fashion as Flow Master, but with HEC-RAS there are additional cross sections up and down stream of the proposed low water crossing which impact the resulting flows. The last two methods used, the orifice equation and culvert nomograph, are based on the same theory that the proposed structure acts like an orifice or culvert with a controlled inlet.

\* Methods using Manning's "n" values have "n" values as follows: Concrete "n" = 0.013; Rough Rip Rap "n" = 0.045; Smooth Rip Rap "n" = 0.035. The weighted "n" value for the surface when water passes through the crossing and touches the slab = 0.022 and when water does not touch the top slab = 0.032.



To solve for maximum capacity through low water crossing as an orifice:

ORIFICE EQUATION:

$$Q = 0.6 \cdot A \sqrt{2gh}$$

$$A = 64.35 \text{ ft}^2$$

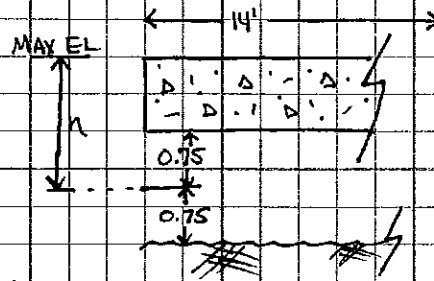
$$g = 32.2 \text{ ft/s}^2$$

$$h_1 = 1.75' \rightarrow \text{assumes still water at opening}$$

$$h_2 = V_{\text{HEAD}} + h_1 \rightarrow \text{take velocity into account} = \underline{1.89}$$

$$V_{\text{HEAD}} = \frac{V^2}{2g} = \underline{0.140}$$

$$V = 3.0 \text{ ft/s} \rightarrow \text{as estimated by HEC-RAS}$$



$$Q = 0.6 (64.35) (2 \cdot 32.2 \cdot 1.89)^{1/2}$$

$$Q = 425.96 \rightarrow 5886 \text{ (TOP OF CROSSING) AS MAX ELEVATION}$$

$$h_1 = 0.75$$

$$h_2 = 0.89$$

$$Q = 0.6 (64.35) (2 \cdot 32.2 \cdot 0.89)^{1/2}$$

$$Q = 292.31 \text{ cfs} \rightarrow 5885 \text{ (TOP OF OPENING) AS MAX ELEV}$$



To solve for maximum capacity of flow under low water crossing:

MANNING'S FORMULA:

$$Q = \frac{1.49}{n} \cdot A R^{2/3} \cdot S_o^{1/2}$$

$$S_o = 0.00214$$

$$R = \frac{\text{AREA}}{\text{PERIMETER}}$$

$$A = \frac{1}{2} (B_1 + B_2) h$$

$$P_w = B_1 + B_2 + 4h$$

$$B_1 = 39' - 1.5' = 37.5'$$

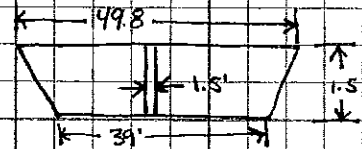
$$P_w = \underline{91.8 \text{ ft}}$$

$$B_2 = 49.8' - 1.5' = 48.3'$$

$$h = 1.5'$$

$$R = \frac{64.35}{91.8} = \underline{0.70098 \text{ ft}}$$

$$A = \underline{64.35 \text{ ft}^2}$$



$$Q = \frac{1.49}{n} (64.35 \text{ ft}^2) (0.70098 \text{ ft})^{2/3} (0.00214)^{1/2}$$

$$Q = \frac{3.71}{n}$$

"n"	Q
0.013	285 cfs
0.022	168 cfs
0.030	124 cfs
0.032	116 cfs
0.040	92.75 cfs
0.050	74.2 cfs

\* This is not the flow before overtopping, it is the flow under concrete slab.

Client: \_\_\_\_\_ Job No: 29247.20

Project: River Peak Greenway Trail By: JAW Chk. By: \_\_\_\_\_ Date: 6.27.01

Subject: \_\_\_\_\_ Sheet No: 2 of 2



**J-R ENGINEERING**  
A Subsidiary of Westrian

MANNING'S FORMULA CONTINUED!

- ASSUME FLOW IS NOT TOUCHING BOTTOM OF LOW WATER CROSSING SLAB

$$P_w = B_1 + 4h$$

$$P_w = 43.5$$

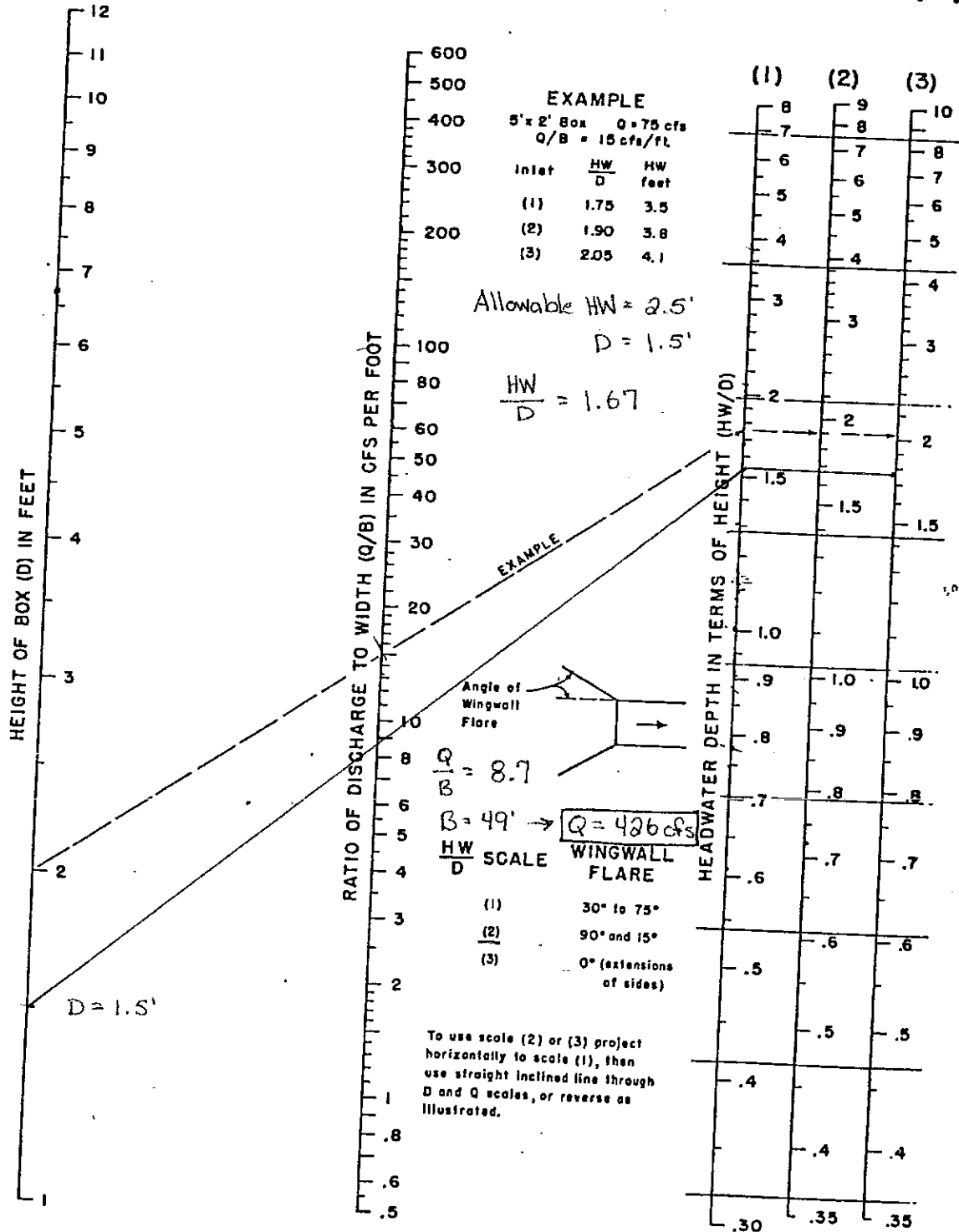
$$R = \frac{\text{AREA}}{P_{wLW}} = \frac{64.35}{43.5} = \underline{1.48}$$

$$Q = \frac{1.49}{n} (64.35)(1.48)^{2/3} (0.00214)^{1/2}$$

$$Q = \frac{5.76}{n}$$

"n"	Q
0.013	443
0.022	262 cfs
0.030	192
→ 0.032	180 cfs
0.040	144
0.050	115.2

# CHART I

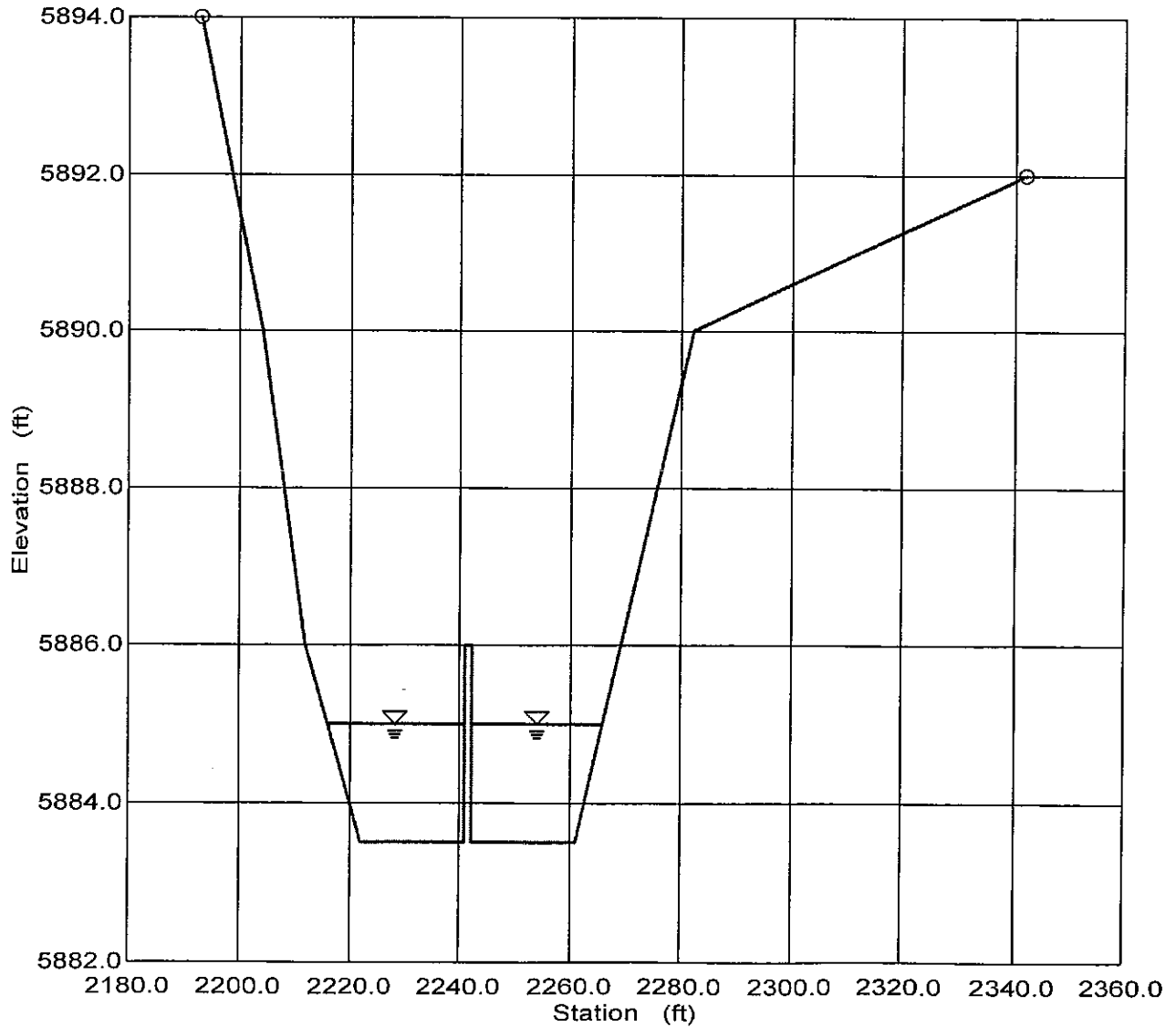


**HEADWATER DEPTH FOR BOX CULVERTS WITH INLET CONTROL**

## Low Flows @ Proposed Low Water Crossing Cross Section for Irregular Channel

Project Description	
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Worksheet	XS @ Proposed Low Water Crossing
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

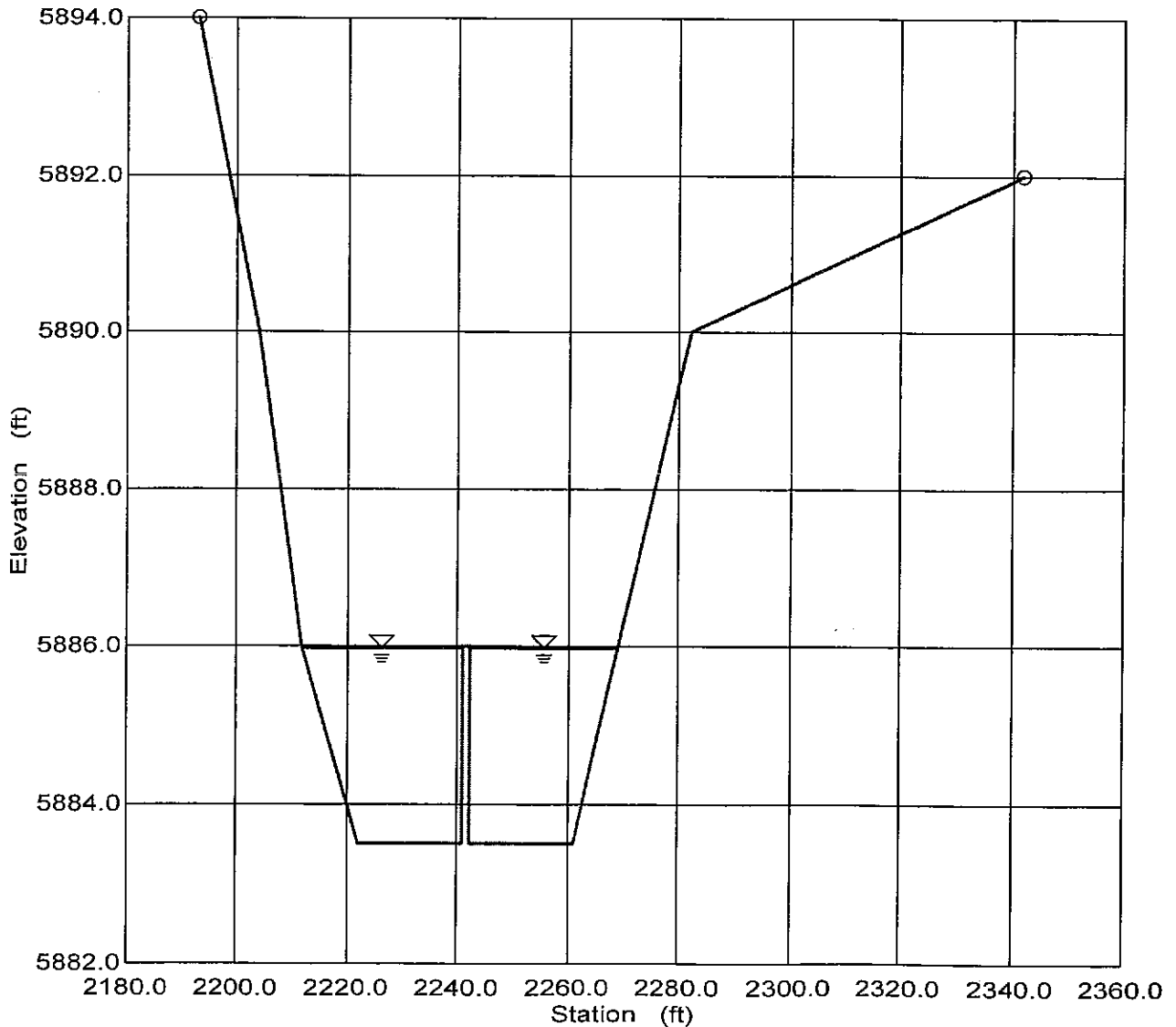
Section Data	
Wtd. Mannings Coefficient	0.032
Channel Slope	0.002140 ft/ft
Water Surface Elevation	5,885.00 ft
Discharge	160.00 cfs - MAX EL = 5885



## Low Flows @ Proposed Low Water Crossing Cross Section for Irregular Channel

Project Description	
Project File	h:\fmw\project3.fm2
Worksheet	XS @ Proposed Low Water Crossing
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Water Elevation

Section Data	
Wtd. Mannings Coefficient	0.032
Channel Slope	0.002140 ft/ft
Water Surface Elevation	5,885.99 ft
Discharge	380.00 cfs — MAX EL = 5886

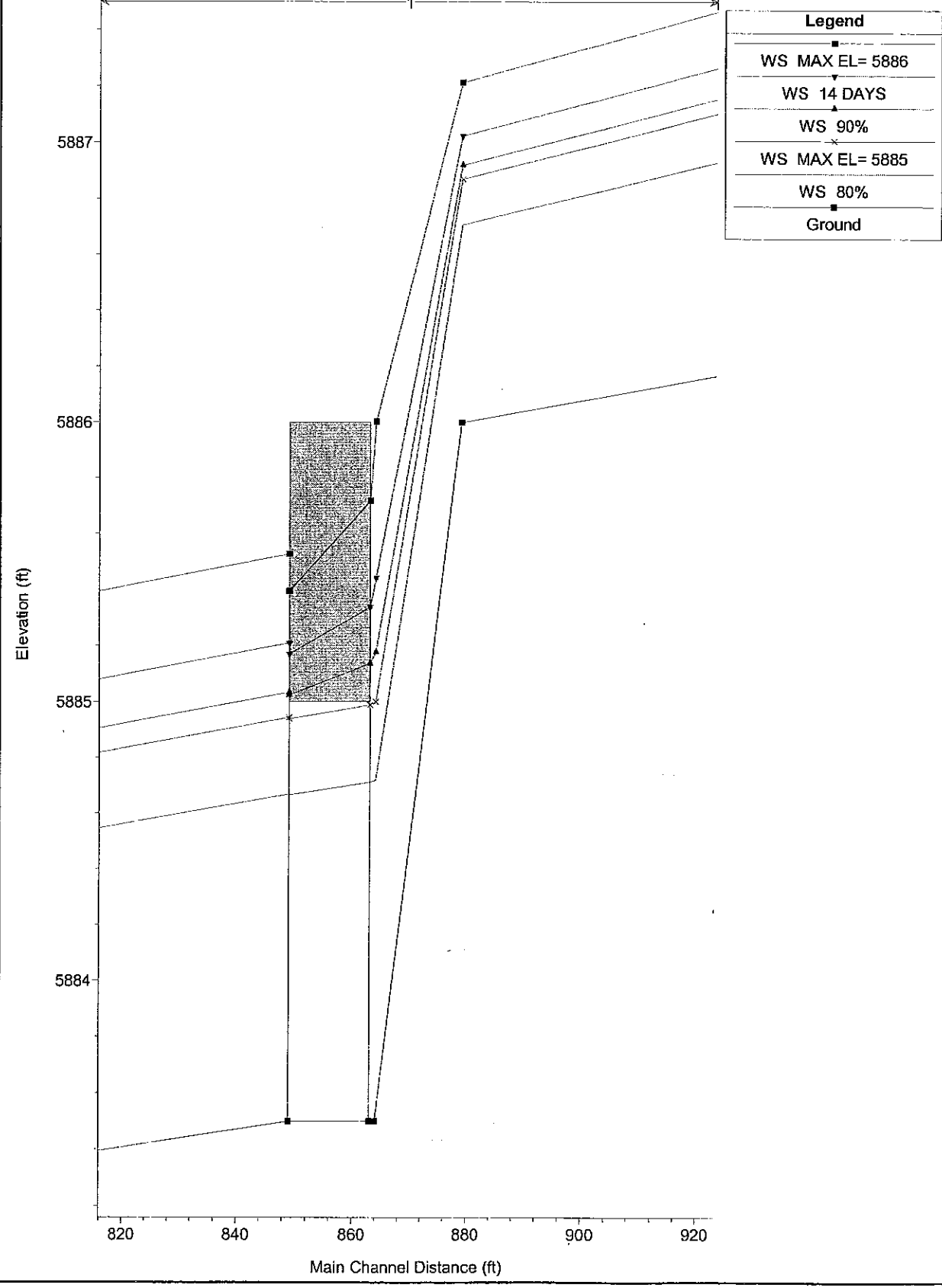




HEC-RAS Plan: PostProject12 River: Fountain Creek Reach: 1

Reach	River Sta	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Ch
1	15700	166.0	5887.70	5889.17	5888.5	5889.3	0.001889	2.2	75.1	65	0.36
1	15700	317.0	5887.70	5889.74	5888.9	5889.9	0.002028	2.8	114.7	75	0.39
1	15300	166.0	5886.00	5886.87	5886.9	5887.2	0.021101	4.6	35.7	54	1.01
1	15300	317.0	5886.00	5887.23	5887.2	5887.7	0.018248	5.6	66.2	57	1.00
1	15285	166.0	5883.50	5885.00	5884.3	5885.1	0.001725	2.5	66.8	50	0.38
1	15285	317.0	5883.50	5886.00	5884.7	5886.1	0.001069	2.6	120.2	57	0.32
1	15280	Bridge									
1	15270	166.0	5883.50	5884.96	5884.3	5885.1	0.002622	2.6	64.4	50	0.40
1	15270	317.0	5883.50	5885.56	5884.7	5885.7	0.002684	3.3	96.6	54	0.44
1	14400	166.0	5880.80	5881.69	5881.5	5881.9	0.005907	3.2	51.1	65	0.64
1	14400	317.0	5880.80	5882.10	5881.8	5882.4	0.005904	4.0	79.4	74	0.68

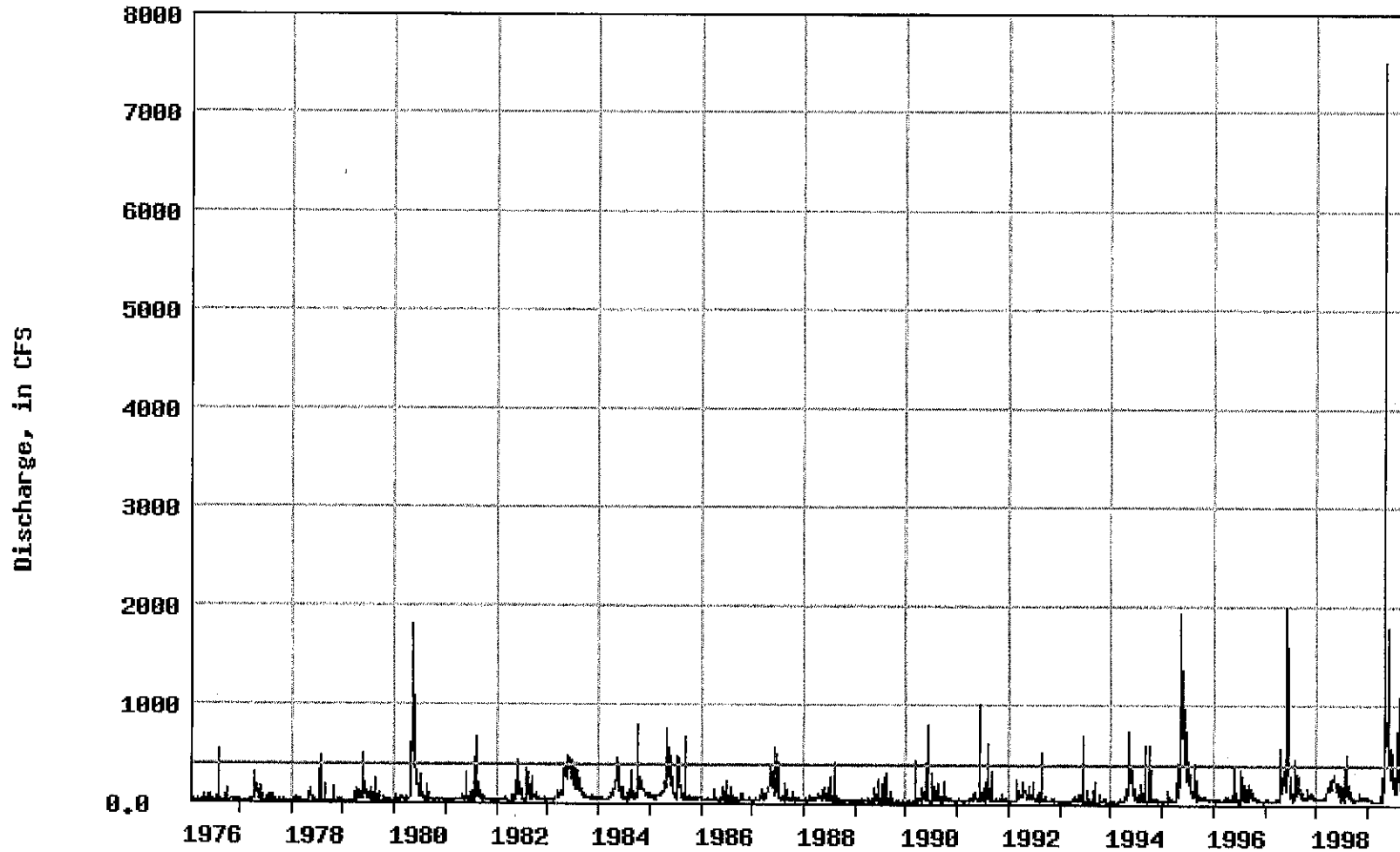
FOUNTAIN CREEK @ GW LW CROSSING Post-Project2 6/27/2001



**GRAPH OF HISTORIC DAILY PEAK FLOWS**

# Graph of Daily Peak Flows from USGS Gage

Fountain Creek At Colorado Springs, Co.  
Station Number: 07105500



Legend: — Discharge, in CFS  
— Estimated Discharge, in CFS  
... Discharge Passing Under Low Water Crossing, in CFS

**TABLE OF HISTORIC PEAK FLOWS**

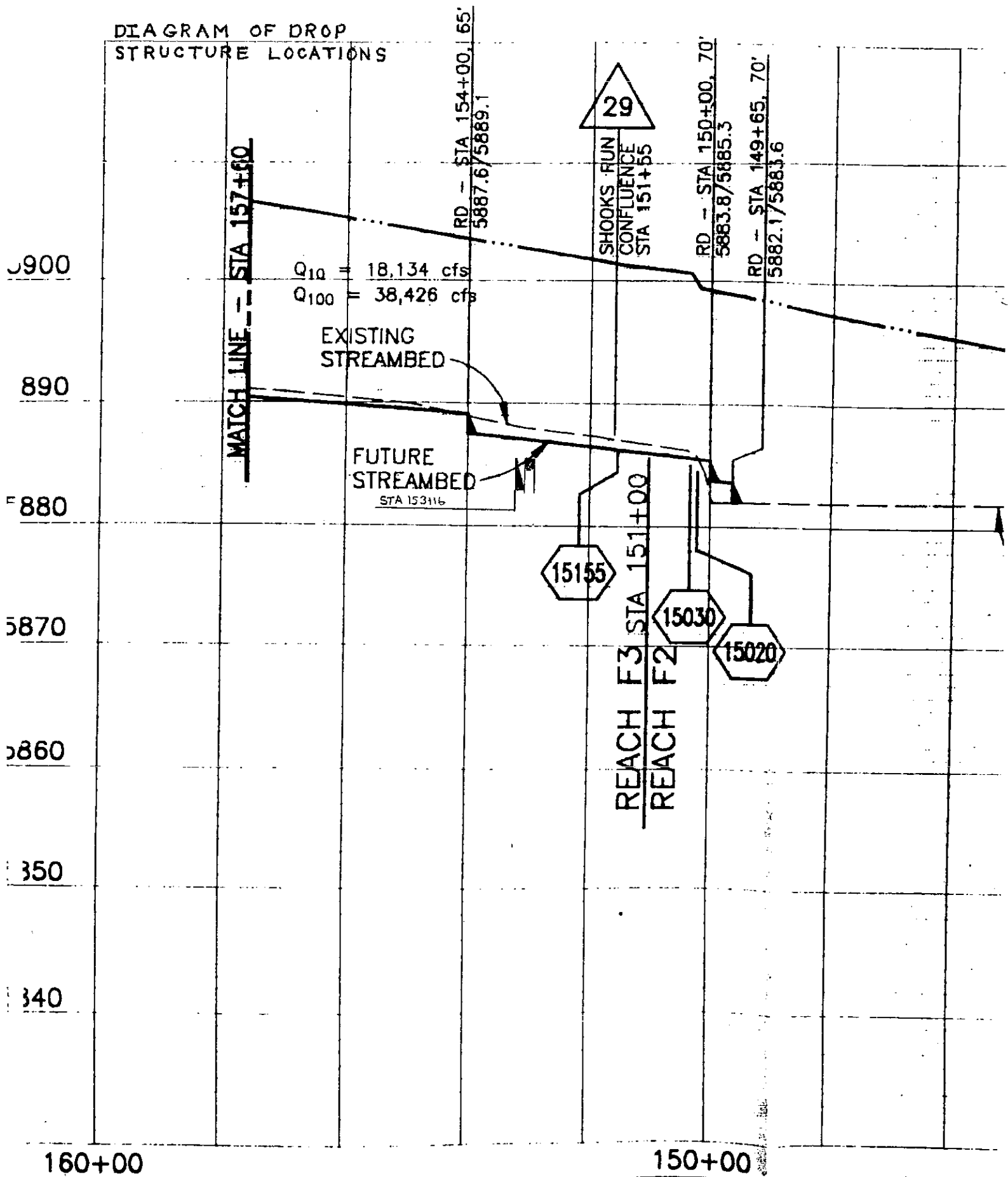
**Table of Low Flows in Fountain Creek**

Year	Flow (cfs) at: 80th Percentile of Days	Flow (cfs) at: 90th Percentile of Days	A maximum of 14 days in a row had flows (cfs) greater than:	Peak Flows (cfs) in a given year (shaded flows indicate those that would overtop low water crossing)																
1976	25	30	25	540	140															
1977	40	66	127	302	216															
1978	30	48	65	473	320	170														
1979	68	100	75	501	335	230														
1980	100	375	740	1813	1330	833	620	425	280											
1981	50	80	76	655	440	305	260													
1982	80	130	75	427	350	310	275													
1983	273	350	378	467	467	430	401	380	351	349	340	335	325	270						
1984	170	225	225	790	440	325	290	260												
1985	180	300	350	730	665	580	560	470	450	380	270									
1986	52	65	40	225																
1987	123	200	230	551	482	375	325	260												
1988	62	76	88	420	280															
1989	38	60	38	308	254															
1990	65	115	70	780	437	302	218													
1991	70	120	95	995	605	318	255													
1992	82	123	123	510	240															
1993	37	40	60	683	225															
1994	107	213	238	725	582	575	480	375	345	340	238									
1995	250	435	740	1940	1344	942	813	740	740	690	450	401	400	300	280					
1996	65	75	110	395	340	270														
1997	180	275	400	2000	1250	510	505	440	435	420	300	290	280							
1998	154	206	250	488	305	290	255													
1999	375	680	740	7500	1875	1100	1000	813	813	750	570	565	520	500	400					
AVERAGE	111.50	182.79	223.25		380	375	360	250												

\* All information is interpolated off of USGS data for gage 07105500 on Fountain Creek near Tejon and Nevada  
 \* A flow at the nth percentile of days signifies that for n% of the days out of a given year, the creek has flows less than the nth percentile flow

**DIAGRAM OF DROP STRUCTURE LOCATIONS AS PRESENTED  
IN THE MULLER ENGINEERING FOUNTAIN CREEK DRAINAGE  
BASIN PLANNING STUDY**

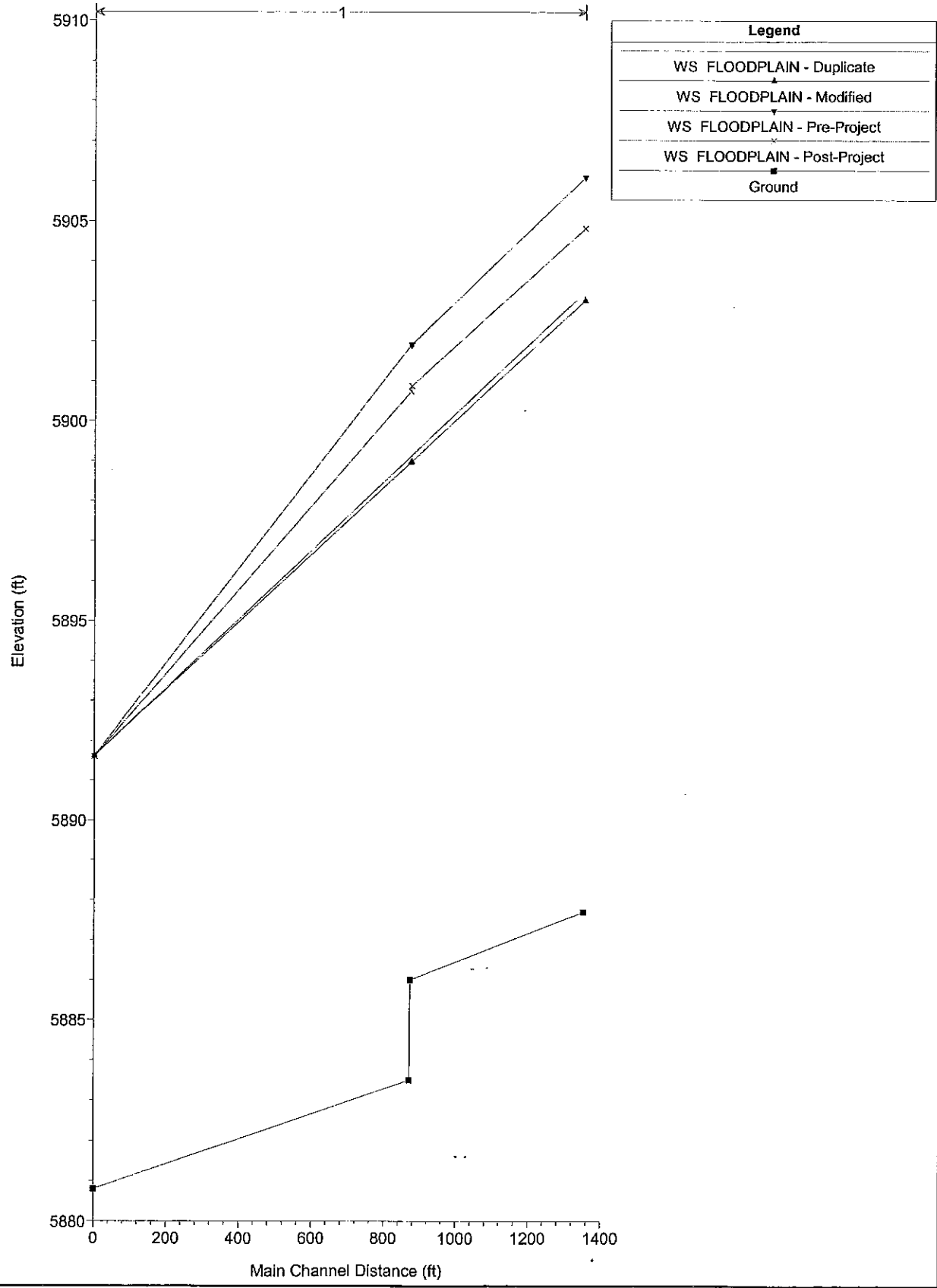
DIAGRAM OF DROP  
STRUCTURE LOCATIONS





## **APPENDIX C**

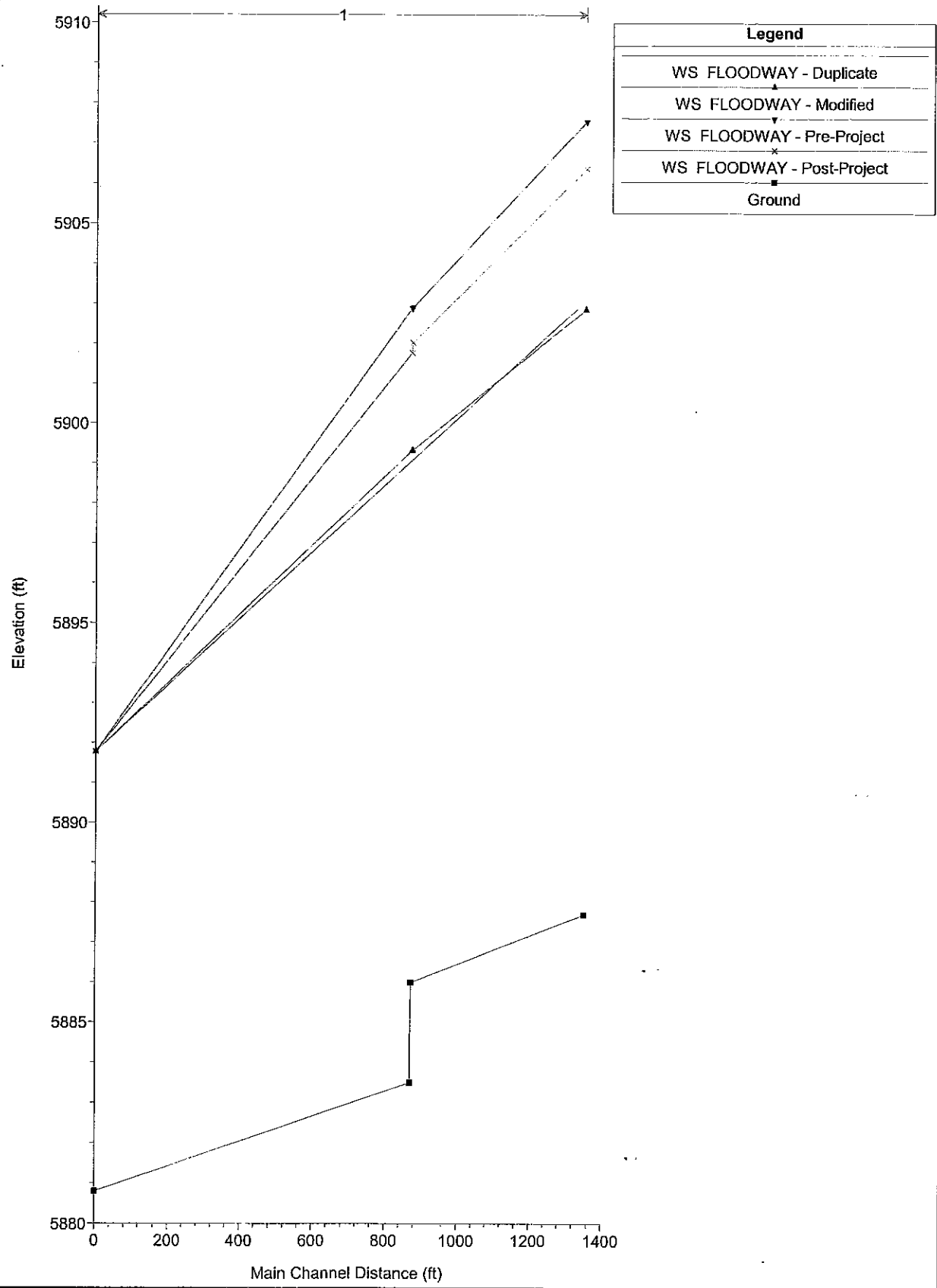
**FLOODPLAIN PROFILE AND ELEVATIONS**



HEC-RAS River: Fountain Creek Reach: 1

Reach	River Sta	Profile	Plan	Q Total (cfs)	Mfr Ch El (ft)	W.S. Elev (ft)	Crk W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Ch
	15700	FLOODPLAIN	Duplicate	44700.00	5887.70	5903.03	5903.03	5905.45	0.004216	17.52	5940.67	1106.77	0.80
	15700	FLOODPLAIN	Modified	44700.00	5887.70	5903.03	5903.03	5905.45	0.004216	17.52	5940.67	1106.77	0.80
	15700	FLOODPLAIN	Pre-Project	44700.00	5887.70	5906.09		5906.86	0.001276	10.93	9840.09	1409.24	0.46
	15700	FLOODPLAIN	Post-Project	44700.00	5887.70	5904.82	5903.03	5906.02	0.002040	13.16	8091.26	1291.49	0.57
	15281	FLOODPLAIN	Modified	44700.00	5886.30	5898.98	5898.98	5902.30	0.005198	18.07	5145.04	791.74	0.95
	15281	FLOODPLAIN	Pre-Project	44700.00	5883.10	5901.92		5905.63	0.003627	18.63	4549.15	634.87	0.81
	15281	FLOODPLAIN	Post-Project	44700.00	5886.00	5900.88	5900.88	5904.15	0.007943	18.48	3987.96	626.85	0.89
	15279	FLOODPLAIN	Modified	44700.00	5886.30	5898.98	5898.96	5902.30	0.005217	18.09	5136.02	791.22	0.96
	15279	FLOODPLAIN	Pre-Project	44700.00	5883.10	5901.91	5901.91	5905.63	0.003630	18.64	4544.50	634.81	0.81
	15279	FLOODPLAIN	Post-Project	44700.00	5883.50	5900.75	5900.75	5904.09	0.006958	18.35	4042.25	625.85	0.84
	14400	FLOODPLAIN	Duplicate	44700.00	5880.80	5891.62	5891.62	5894.79	0.005861	16.66	3492.58	563.68	0.97
	14400	FLOODPLAIN	Modified	44700.00	5880.80	5891.62	5891.62	5894.79	0.005861	16.66	3492.58	563.68	0.97
	14400	FLOODPLAIN	Pre-Project	44700.00	5880.80	5891.62	5891.62	5894.79	0.005871	16.67	3490.38	563.56	0.97
	14400	FLOODPLAIN	Post-Project	44700.00	5880.80	5891.61	5891.60	5894.79	0.005902	16.70	3483.78	563.21	0.97

**FLOODWAY PROFILE AND ELEVATIONS**



HEC-RAS River: Fountain Creek Reach: 1

Reach	River Sta	Profile	Plan	Q Total (cfs)	Min Ch Elev (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Ch
	16700	FLOODWAY	Duplicate	44700.00	5887.70	5902.87	5902.87	5905.89	0.004770	18.50	5289.20	793.60	0.85
	16700	FLOODWAY	Modified	44700.00	5887.70	5902.86	5902.86	5905.89	0.004787	18.52	5281.84	793.57	0.86
	16700	FLOODWAY	Pre-Project	44700.00	5887.70	5907.54		5908.30	0.001052	10.46	9021.04	800.00	0.42
	16700	FLOODWAY	Post-Project	44700.00	5887.70	5908.38	5902.86	5907.36	0.001455	11.79	8081.59	800.00	0.49
	15281	FLOODWAY	Modified	44700.00	5885.30	5899.33	5899.32	5903.18	0.005448	19.89	4609.42	646.78	0.98
	15281	FLOODWAY	Pre-Project	44700.00	5883.10	5902.90		5907.13	0.003560	19.18	4245.39	578.82	0.81
	15281	FLOODWAY	Post-Project	44700.00	5885.00	5902.02	5902.02	5905.77	0.007622	19.11	3806.66	521.46	0.68
	15279	FLOODWAY	Modified	44700.00	5886.30	5899.32	5899.32	5903.18	0.005468	19.91	4602.47	646.33	0.98
	15279	FLOODWAY	Pre-Project	44700.00	5883.10	5902.89	5902.89	5907.13	0.003567	19.19	4241.16	578.14	0.81
	15279	FLOODWAY	Post-Project	44700.00	5883.50	5901.77	5901.77	5905.63	0.006862	19.04	3810.81	518.26	0.84
	14400	FLOODWAY	Duplicate	44700.00	5880.80	5891.79	5891.43	5895.18	0.005902	16.92	3262.80	400.00	0.97
	14400	FLOODWAY	Modified	44700.00	5880.80	5891.79	5891.43	5895.18	0.005902	16.92	3262.80	400.00	0.97
	14400	FLOODWAY	Pre-Project	44700.00	5880.80	5891.79	5891.38	5895.18	0.005902	16.92	3262.80	400.00	0.97
	14400	FLOODWAY	Post-Project	44700.00	5880.80	5891.79	5891.43	5895.18	0.005902	16.92	3262.80	400.00	0.97

**DUPLICATE EFFECTIVE MODEL**



FCGWLWC.rep

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 U.S. Army Corp of Engineers  
 Hydrologic Engineering Center  
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 Davis, California 95616-4687  
 (916) 756-1104

```

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PROJECT DATA

Project Title: FOUNTAIN CREEK @ GW LW CROSSING  
 Project File : FCGWLWC.prj  
 Run Date and Time: 6/26/2001 9:20:21 AM

Project in English units

Project Description:

Flood Plain Development Permit Model

GEOMETRY DATA

Geometry Title: Duplicate Effective  
 Geometry File : x:\2920000.a11\2924720\HEC RAS Models\FPpermit\FCGWLWC.g02

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 15700

INPUT

Description: FEMA FIRM Section DT (260)

Station Elevation Data num= 31									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
1000	5925	1008	5920	1018	5915	1025	5910	1070	5905
1325	5902	1355	5902	1505	5900	2195	5895	2210	5890
2220	5888.6	2230	5887.7	2265	5887.7	2275	5888.6	2290	5890
2320	5895	2335	5900	2350	5905	2400	5905	2410	5903
2430	5905	2610	5910	2725	5910	2740	5905	2750	5900
2830	5898	2875	5900	3310	5905	3935	5910	4075	5915
4220	5920								

Manning's n Values num= 3					
Sta	n Val	Sta	n Val	Sta	n Val
1000	.06	2210	.033	2290	.06

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 2210 2290 1325.8 1325 1350 .1 .3

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 14400

INPUT

Description: FEMA FIRM Section DS (250)

Station Elevation Data		num= 29							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
1000	5915	1050	5910	1160	5905	1390	5900	1490	5895
1640	5890	1750	5885	1760	5882	1770	5880.8	1820	5880.8
1830	5882	1920	5884.7	2030	5883.2	2090	5885	2115	5890
2125	5891	2155	5891	2165	5890	2170	5888	2175	5890
2180	5891	2240	5891	2250	5890	2270	5885	2290	5884
2320	5885	2950	5890	3110	5895	3125	5900		

Manning's n Values		num= 6							
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
1000	.07	1640	.04	1750	.03	1920	.04	2115	.02
2165	.07								

Bank Sta:	Left	Right	Lengths:	Left	Channel	Right	Coeff	Contr.	Expan.
	1750	1920		0	0	0		.1	.3

SUMMARY OF MANNING'S N VALUES

River: Fountain Creek

Reach	River Sta.	n1	n2	n3	n4	n5
1	15700	.06	.033	.06		
1	14400	.07	.04	.03	.04	.02

SUMMARY OF REACH LENGTHS

River: Fountain Creek

Reach	River Sta.	Left	Channel	Right
1	15700	1325.8	1325	1350
1	14400	0	0	0

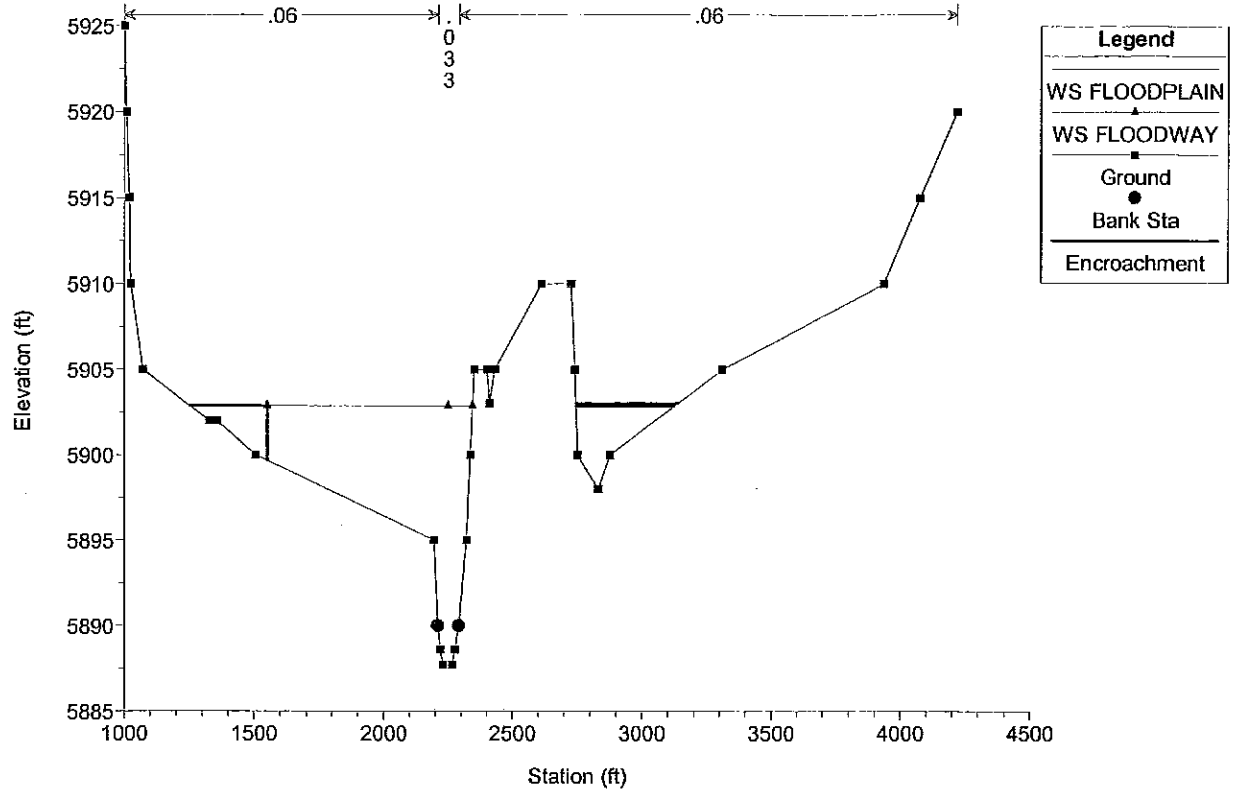
SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: Fountain Creek

Reach	River Sta.	Contr.	Expan.
1	15700	.1	.3
1	14400	.1	.3

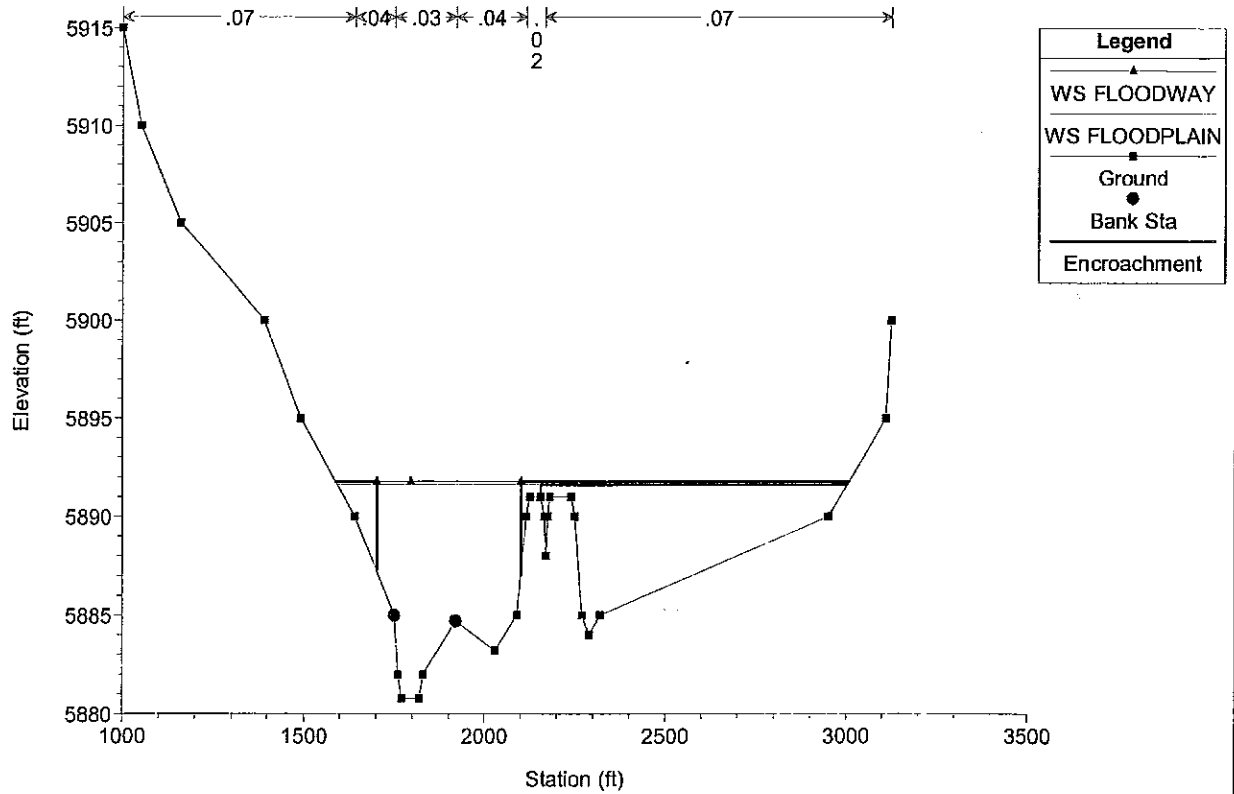
FOUNTAIN CREEK @ GW LW CROSSING Duplicate Effective 6/26/2001

RS = 15700



FOUNTAIN CREEK @ GW LW CROSSING Duplicate Effective 6/26/2001

RS = 14400



**MODIFIED EFFECTIVE MODEL**

FCGWLWC.rep

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 U.S. Army Corp of Engineers  
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PROJECT DATA

Project Title: FOUNTAIN CREEK @ GW LW CROSSING  
 Project File : FCGWLWC.prj  
 Run Date and Time: 6/26/2001 9:28:38 AM

Project in English units

Project Description:  
 Flood Plain Development Permit Model

GEOMETRY DATA

Geometry Title: Modified Effective  
 Geometry File : x:\2920000.all\2924720\HEC RAS Models\FPpermit\FCGWLWC.g03

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 15700

INPUT

Description: FEMA FIRM Section DT (260)  
 Station Elevation Data num= 31

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
1000	5925	1008	5920	1018	5915	1025	5910	1070	5905
1325	5902	1355	5902	1505	5900	2195	5895	2210	5890
2220	5888.6	2230	5887.7	2265	5887.7	2275	5888.6	2290	5890
2320	5895	2335	5900	2350	5905	2400	5905	2410	5903
2430	5905	2610	5910	2725	5910	2740	5905	2750	5900
2830	5898	2875	5900	3310	5905	3935	5910	4075	5915
4220	5920								

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
1000	.06	2210	.033	2290	.06

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 2210 2290 453 478 453 .1 .3

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 15281

INPUT

Description: Section at downstream end of proposed low water crossing

Station Elevation Data		num= 10							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
1640	5905	1675	5900	2095	5890	2170	5887	2195	5886.3
2265	5886.3	2275	5890	2475	5895	2510	5899	2512	5905

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
1640	.07	2170	.03	2275	.07

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	2170	2275		2	2	.1	.3

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 15279

INPUT

Description: Section at downstream end of proposed low water crossing

Station Elevation Data		num= 10							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
1640	5905	1675	5900	2095	5890	2170	5887	2195	5886.3
2265	5886.3	2275	5890	2475	5895	2510	5899	2512	5905

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
1640	.07	2170	.03	2275	.07

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	2170	2275		870	870	.1	.3

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 14400

INPUT

Description: FEMA FIRM Section DS (250)

Station Elevation Data		num= 29							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
1000	5915	1050	5910	1160	5905	1390	5900	1490	5895
1640	5890	1750	5885	1760	5882	1770	5880.8	1820	5880.8
1830	5882	1920	5884.7	2030	5883.2	2090	5885	2115	5890
2125	5891	2155	5891	2165	5890	2170	5888	2175	5890
2180	5891	2240	5891	2250	5890	2270	5885	2290	5884
2320	5885	2950	5890	3110	5895	3125	5900		

Manning's n Values		num= 6					
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
1000	.07	1640	.04	1750	.03	1920	.04
2165	.07					2115	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	1750	1920		0	0	.1	.3

SUMMARY OF MANNING'S N VALUES

River:Fountain Creek

n6	Reach	River Sta.	n1	n2	n3	n4	n5

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1		15700	.06	.033	.06		
1		15281	.07	.03	.07		
1		15279	.07	.03	.07		
1	.07	14400	.07	.04	.03	.04	.02

SUMMARY OF REACH LENGTHS

River: Fountain Creek

Reach	River Sta.	Left	Channel	Right
1	15700	453	478	453
1	15281	2	2	2
1	15279	870	870	870
1	14400	0	0	0

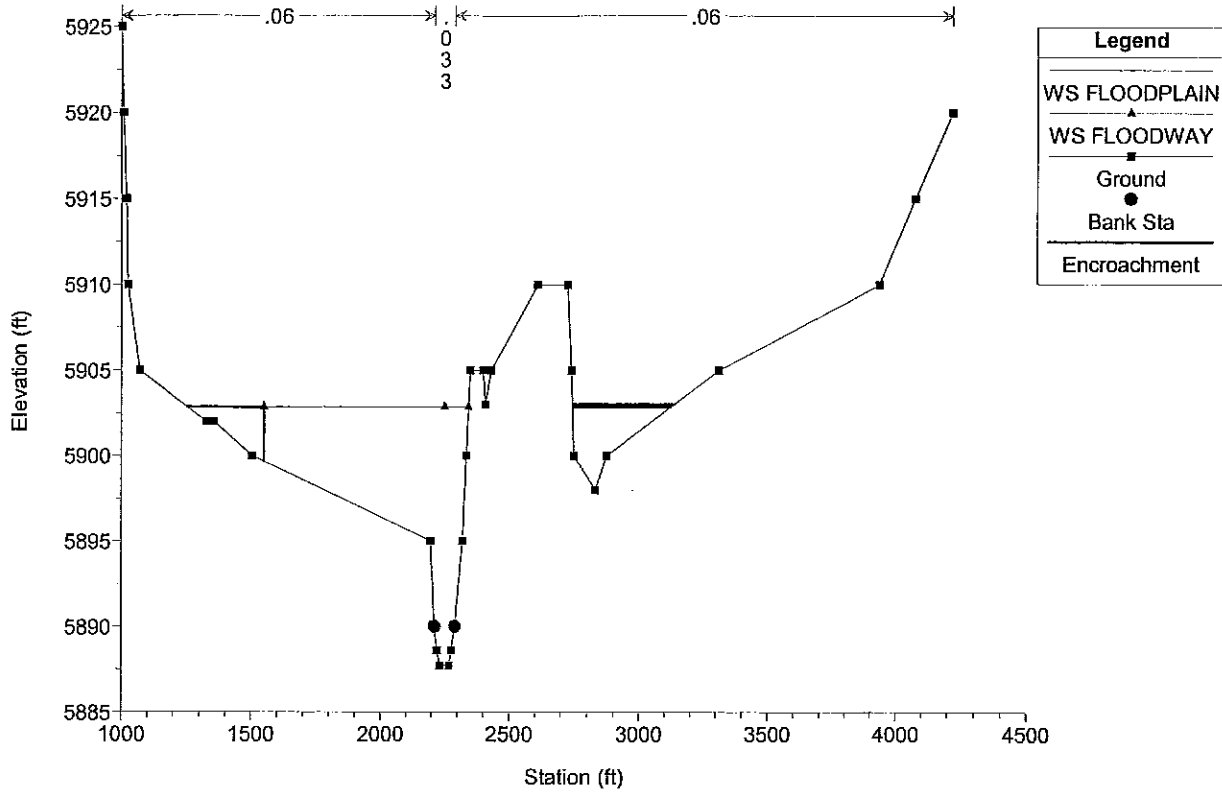
SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: Fountain Creek

Reach	River Sta.	Contr.	Expan.
1	15700	.1	.3
1	15281	.1	.3
1	15279	.1	.3
1	14400	.1	.3

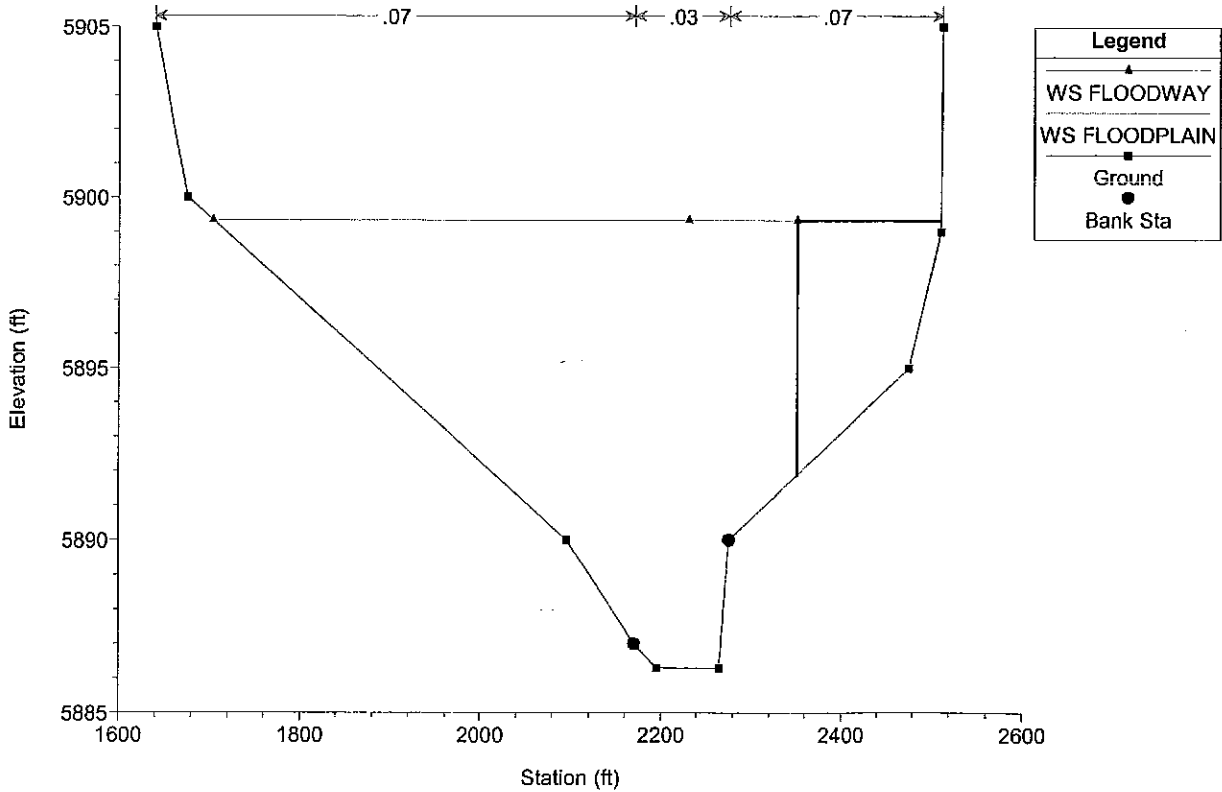
FOUNTAIN CREEK @ GW LW CROSSING Modified Effective 6/26/2001

RS = 15700

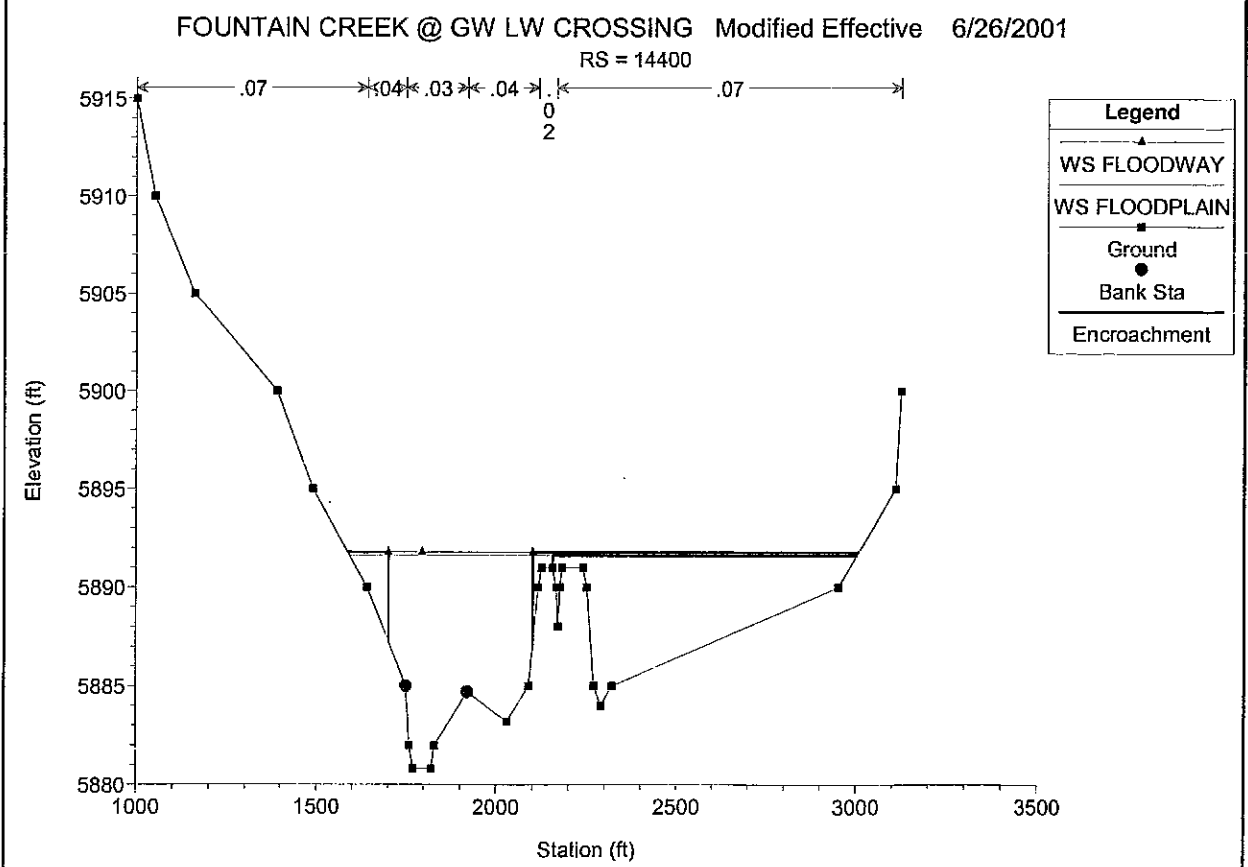
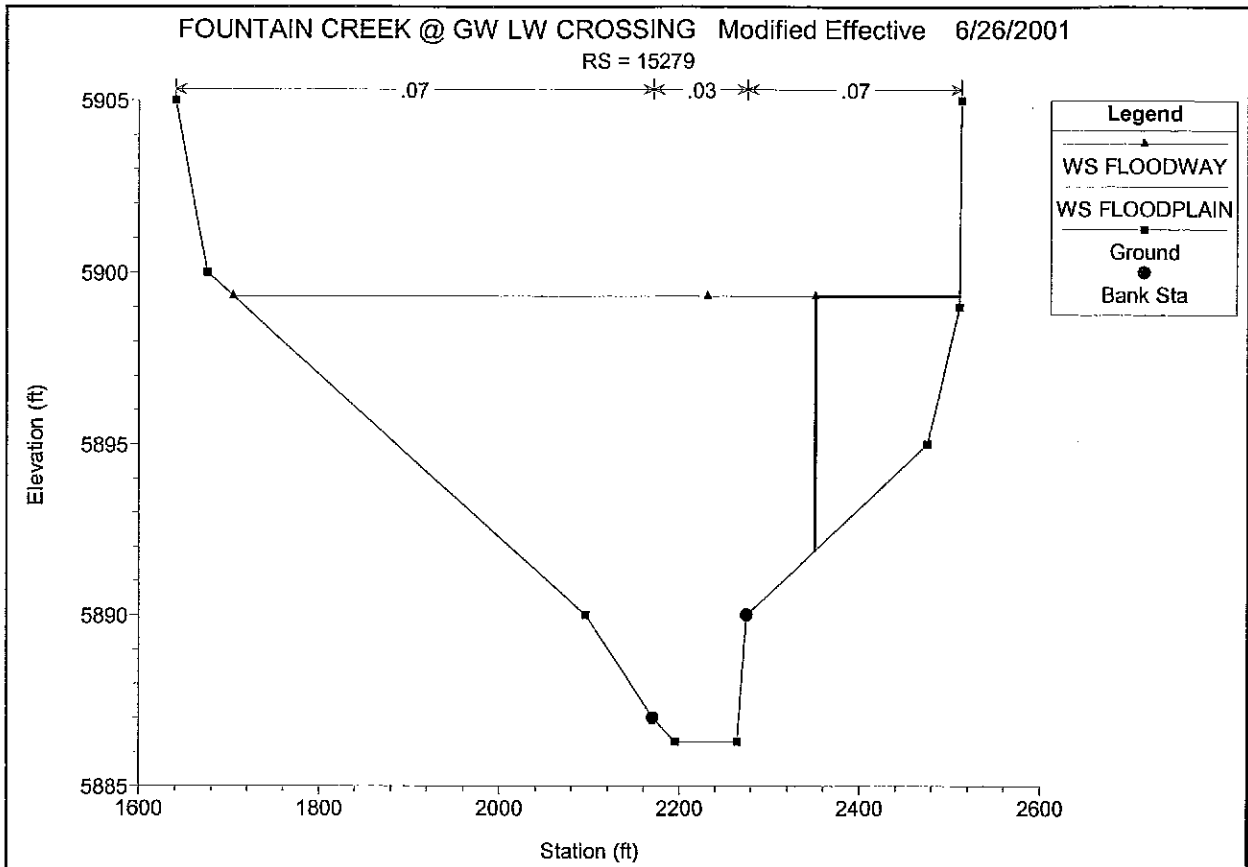


FOUNTAIN CREEK @ GW LW CROSSING Modified Effective 6/26/2001

RS = 15281







**PRE-PROJECT MODEL**

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 Hydrologic Engineering Center  
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 Davis, California 95616-4687  
 (916) 756-1104

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PROJECT DATA

Project Title: FOUNTAIN CREEK @ GW LW CROSSING  
 Project File : FCGWLWC.prj  
 Run Date and Time: 6/26/2001 9:29:50 AM

Project in English units

Project Description:  
 Flood Plain Development Permit Model

GEOMETRY DATA

Geometry Title: Pre-Project  
 Geometry File : x:\2920000.all\2924720\HEC RAS Models\FPpermit\FCGWLWC.g04

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 15700

INPUT

Description: FEMA FIRM Section DT (260)  
 Station Elevation Data num= 31

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
1000	5925	1008	5920	1018	5915	1025	5910	1070	5905
1325	5902	1355	5902	1505	5900	2195	5895	2210	5890
2220	5888.6	2230	5887.7	2265	5887.7	2275	5888.6	2290	5890
2320	5895	2335	5900	2350	5905	2400	5905	2410	5903
2430	5905	2610	5910	2725	5910	2740	5905	2750	5900
2830	5898	2875	5900	3310	5905	3935	5910	4075	5915
4220	5920								

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
1000	.06	2210	.033	2290	.06

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.  
 2210 2290 453 478 453 .1 .3

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 15281

INPUT

Description: Section at downstream end of proposed low water crossing

Station Elevation Data		num= 17							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
1678	5906	1750	5904	1880	5902	1895	5900	2075	5898
2110	5896	2143	5896	2193	5894	2210	5886	2220	5884
2225	5883.1	2267	5883.1	2278	5886	2289	5894	2488	5894
2515	5899.3	2516	5905						

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
1678	.07	2193	.03	2289	.055

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	2193	2289		2	2	.1	.3

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 15279

INPUT

Description: Section at downstream end of proposed low water crossing

Station Elevation Data		num= 17							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
1678	5906	1750	5904	1880	5902	1895	5900	2075	5898
2110	5896	2143	5896	2193	5894	2210	5886	2220	5884
2225	5883.1	2267	5883.1	2278	5886	2289	5894	2488	5894
2515	5899.3	2516	5905						

Manning's n Values		num= 3			
Sta	n Val	Sta	n Val	Sta	n Val
1678	.07	2193	.03	2289	.055

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	2193	2289		870	870	.1	.3

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 14400

INPUT

Description: FEMA FIRM Section DS (250)

Station Elevation Data		num= 29							
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
1000	5915	1050	5910	1160	5905	1390	5900	1490	5895
1640	5890	1750	5885	1760	5882	1770	5880.8	1820	5880.8
1830	5882	1920	5884.7	2030	5883.2	2090	5885	2115	5890
2125	5891	2155	5891	2165	5890	2170	5888	2175	5890
2180	5891	2240	5891	2250	5890	2270	5885	2290	5884
2320	5885	2950	5890	3110	5895	3125	5900		

Manning's n Values		num= 6					
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
1000	.07	1640	.04	1750	.03	1920	.04
2165	.07					2115	.02

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	1750	1920		0	0	.1	.3

SUMMARY OF MANNING'S N VALUES

River: Fountain Creek

FCGWLWC.rep

n6	Reach	River Sta.	n1	n2	n3	n4	n5
1		15700	.06	.033	.06		
1		15281	.07	.03	.055		
1		15279	.07	.03	.055		
1	.07	14400	.07	.04	.03	.04	.02

SUMMARY OF REACH LENGTHS

River: Fountain Creek

Reach	River Sta.	Left	Channel	Right
1	15700	453	478	453
1	15281	2	2	2
1	15279	870	870	870
1	14400	0	0	0

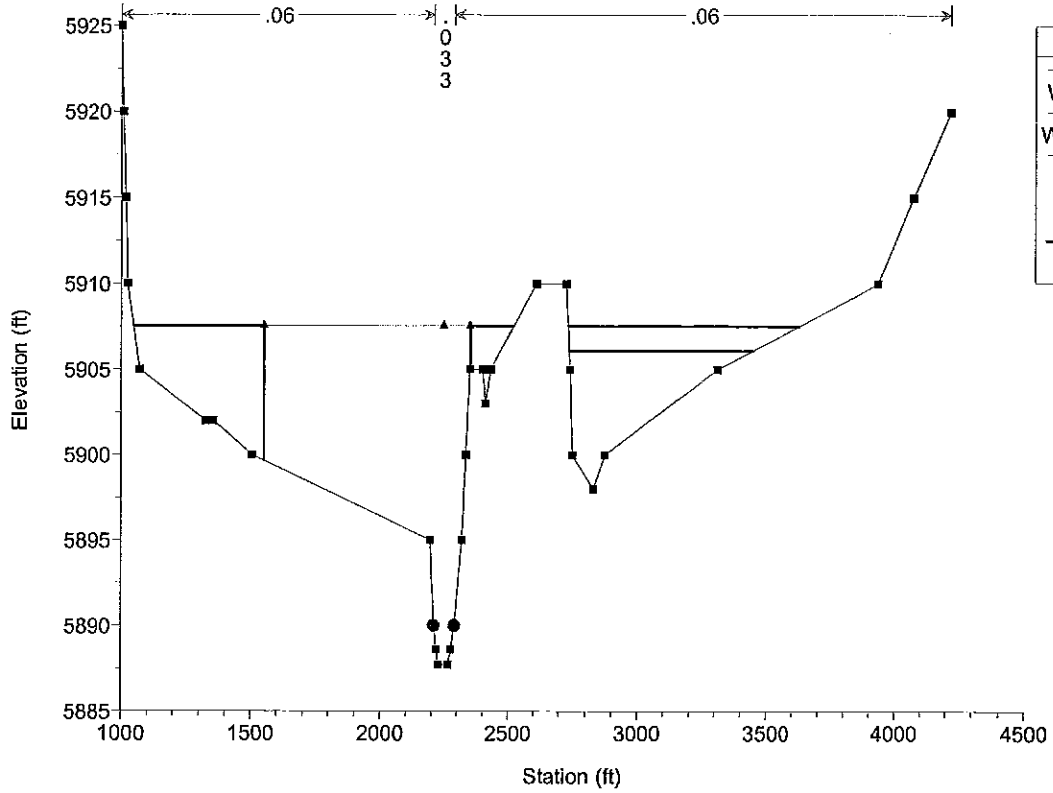
SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: Fountain Creek

Reach	River Sta.	Contr.	Expan.
1	15700	.1	.3
1	15281	.1	.3
1	15279	.1	.3
1	14400	.1	.3

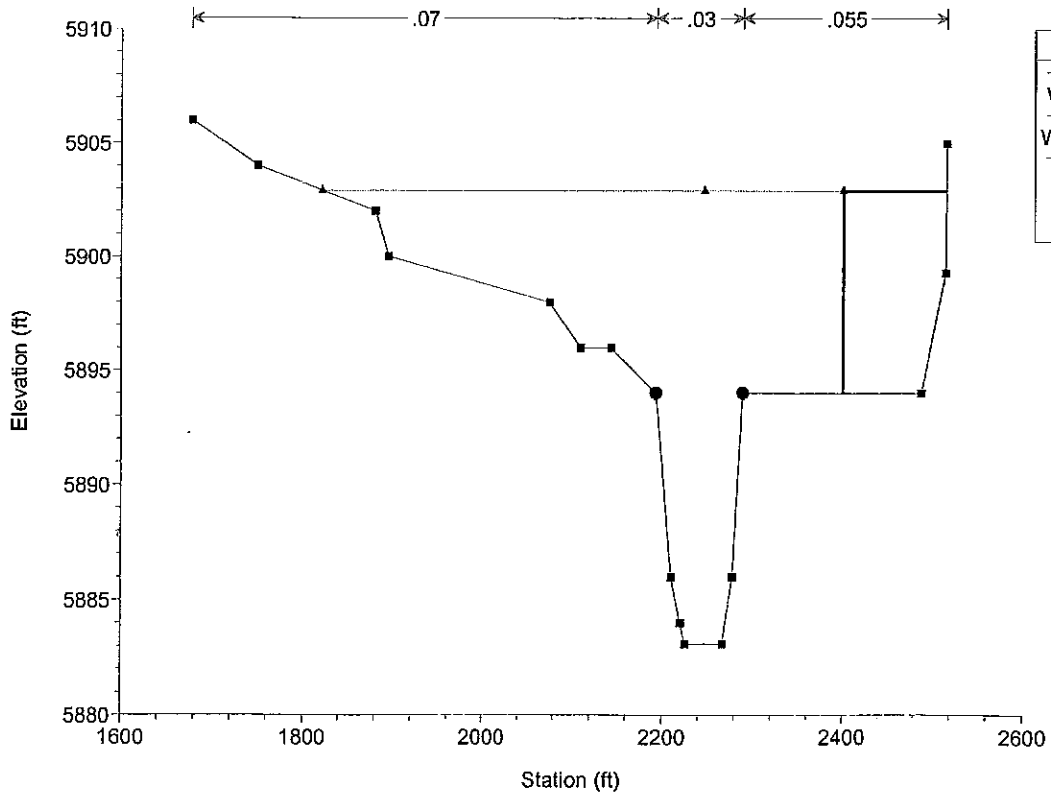
FOUNTAIN CREEK @ GW LW CROSSING Pre-Project 6/26/2001

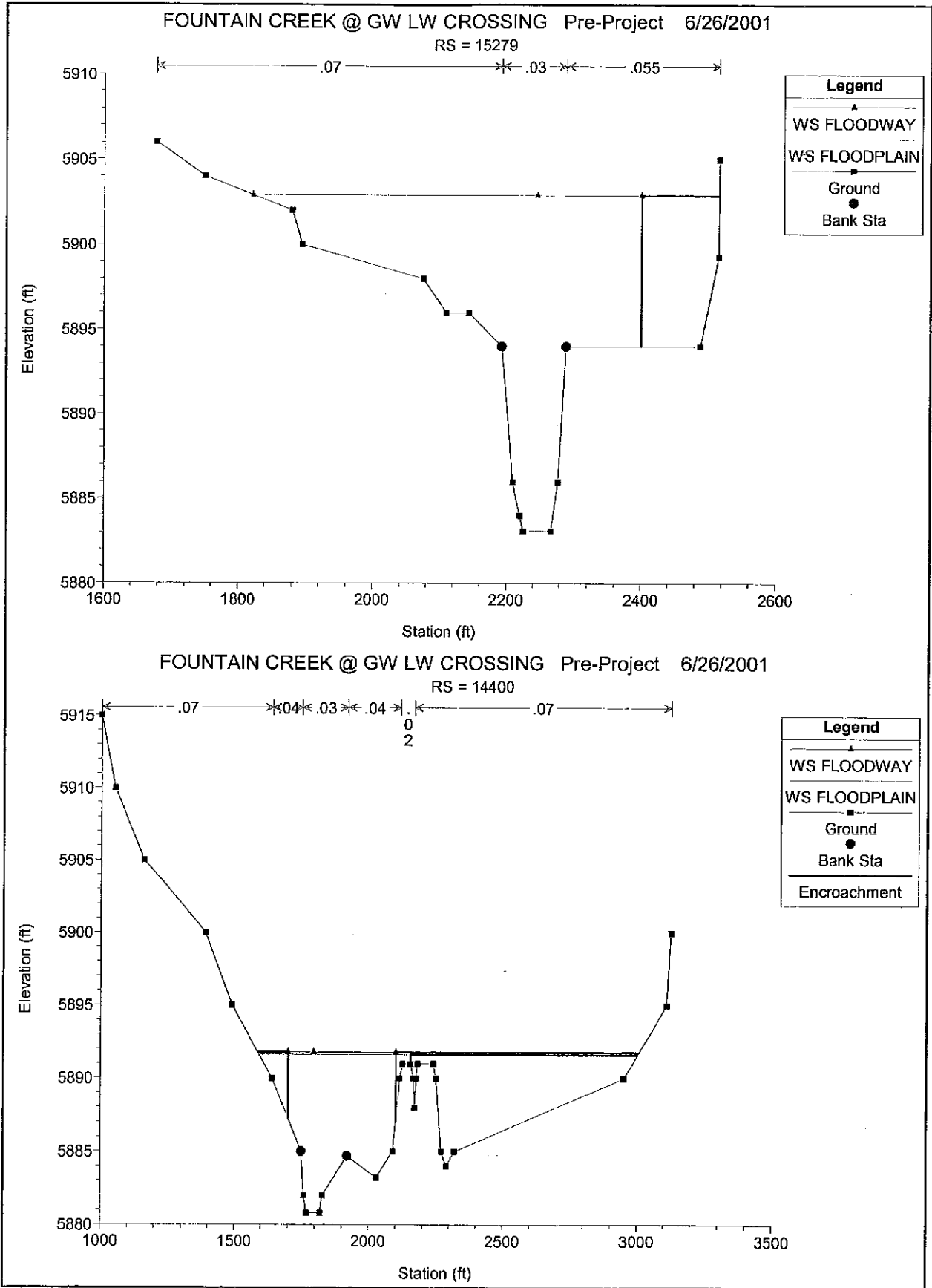
RS = 15700



FOUNTAIN CREEK @ GW LW CROSSING Pre-Project 6/26/2001

RS = 15281





**POST-PROJECT MODEL**



HEC-RAS September 1998 Version 2.2  
 U.S. Army Corp of Engineers  
 Hydrologic Engineering Center  
 609 Second Street, Suite D  
 Davis, California 95616-4687  
 (916) 756-1104

```

X      X  XXXXXX      XXXX      XXXX      XX      XXXX
X      X  X          X  X      X  X      X  X      X
X      X  X          X          X  X      X  X      X
XXXXXXXX XXXX      X          XXX XXXX      XXXXXX      XXXX
X      X  X          X          X  X      X  X          X
X      X  X          X          X  X      X  X      X
X      X  XXXXXX      XXXX      X  X      X  X      XXXXX
    
```

PROJECT DATA

Project Title: FOUNTAIN CREEK @ GW LW CROSSING  
 Project File : FCGWLWC.prj  
 Run Date and Time: 6/26/2001 10:16:11 AM

Project in English units

Project Description:

Flood Plain Development Permit Model

GEOMETRY DATA

Geometry Title: Post-Project  
 Geometry File : x:\2920000.all\2924720\HEC RAS Models\FPpermit\FCGWLWC.g01

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 15700

INPUT

Description: FEMA FIRM Section DT (260)

Station	Elevation	Data	num=	31	Sta	Elev	Sta	Elev	Sta	Elev
1000	5925				1008	5920	1018	5915	1025	5910
1325	5902				1355	5902	1505	5900	2195	5895
2220	5888.6				2230	5887.7	2265	5887.7	2275	5888.6
2320	5895				2335	5900	2350	5905	2400	5905
2430	5905				2610	5910	2725	5910	2740	5905
2830	5898				2875	5900	3310	5905	3935	5910
4220	5920								4075	5915

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
1000	.06	2210	.033	2290	.06

Bank Sta: Left 2210 Right 2290 Lengths: Left Channel 453 Right Channel 478 Coeff Contr. .1 Expan. .3

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 15281

INPUT

Description: Section at upstream end of low water crossing

Station Elevation Data num= 17									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
1678	5906	1750	5904	1880	5902	1895	5900	2075	5898
2110	5896	2143	5896	2193	5894	2204	5890	2212	5886
2222	5886	2261	5886	2282	5890	2342	5892	2488	5894
2515	5899.3	2516	5905						

Manning's n Values num= 3					
Sta	n Val	Sta	n Val	Sta	n Val
1678	.07	2193	.04	2282	.055

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	2193	2282		2	2		.1	.3

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 15279

INPUT

Description: Section at downstream end of proposed low water crossing

Station Elevation Data num= 17									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
1678	5906	1750	5904	1880	5902	1895	5900	2075	5898
2110	5896	2143	5896	2193	5894	2204	5890	2212	5886
2222	5883.5	2261	5883.5	2282	5890	2342	5892	2488	5894
2515	5899.3	2516	5905						

Manning's n Values num= 3					
Sta	n Val	Sta	n Val	Sta	n Val
1678	.07	2193	.04	2282	.055

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	2193	2282		870	870		.1	.3

CROSS SECTION RIVER: Fountain Creek  
 REACH: 1 RS: 14400

INPUT

Description: FEMA FIRM Section DS (250)

Station Elevation Data num= 29									
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
1000	5915	1050	5910	1160	5905	1390	5900	1490	5895
1640	5890	1750	5885	1760	5882	1770	5880.8	1820	5880.8
1830	5882	1920	5884.7	2030	5883.2	2090	5885	2115	5890
2125	5891	2155	5891	2165	5890	2170	5888	2175	5890
2180	5891	2240	5891	2250	5890	2270	5885	2290	5884
2320	5885	2950	5890	3110	5895	3125	5900		

Manning's n Values num= 6									
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
1000	.07	1640	.04	1750	.03	1920	.04	2115	.02
2165	.07								

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	1750	1920		0	0		.1	.3

SUMMARY OF MANNING'S N VALUES

River: Fountain Creek

FCGWLWC.rep

n6	Reach	River Sta.	n1	n2	n3	n4	n5
1		15700	.06	.033	.06		
1		15281	.07	.04	.055		
1		15279	.07	.04	.055		
1	.07	14400	.07	.04	.03	.04	.02

SUMMARY OF REACH LENGTHS

River: Fountain Creek

Reach	River Sta.	Left	Channel	Right
1	15700	453	478	453
1	15281	2	2	2
1	15279	870	870	870
1	14400	0	0	0

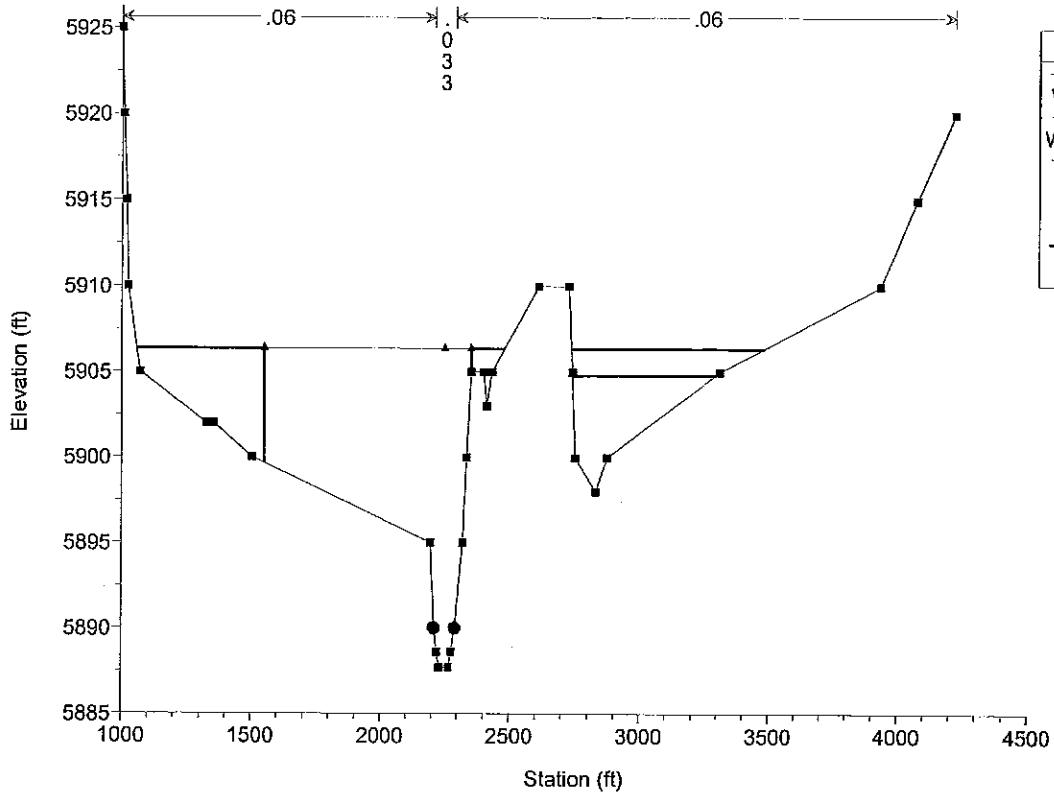
SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: Fountain Creek

Reach	River Sta.	Contr.	Expan.
1	15700	.1	.3
1	15281	.1	.3
1	15279	.1	.3
1	14400	.1	.3

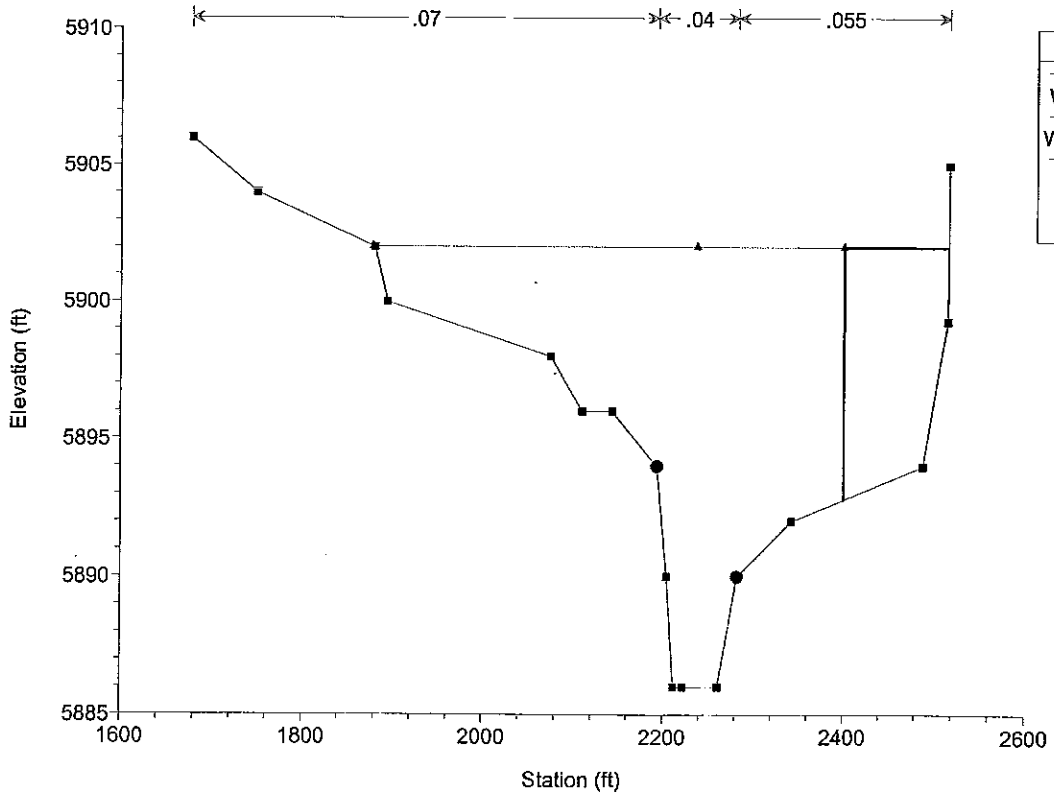
FOUNTAIN CREEK @ GW LW CROSSING Post-Project 6/26/2001

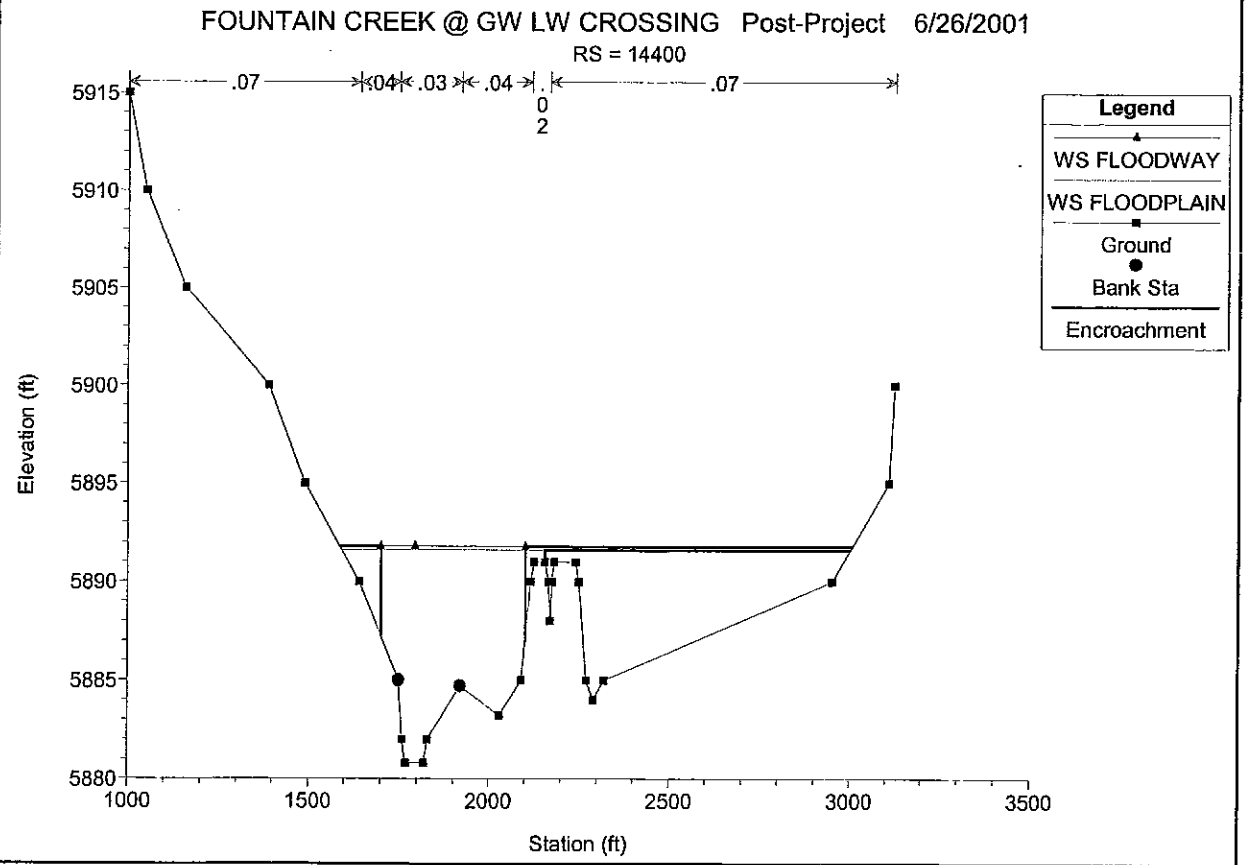
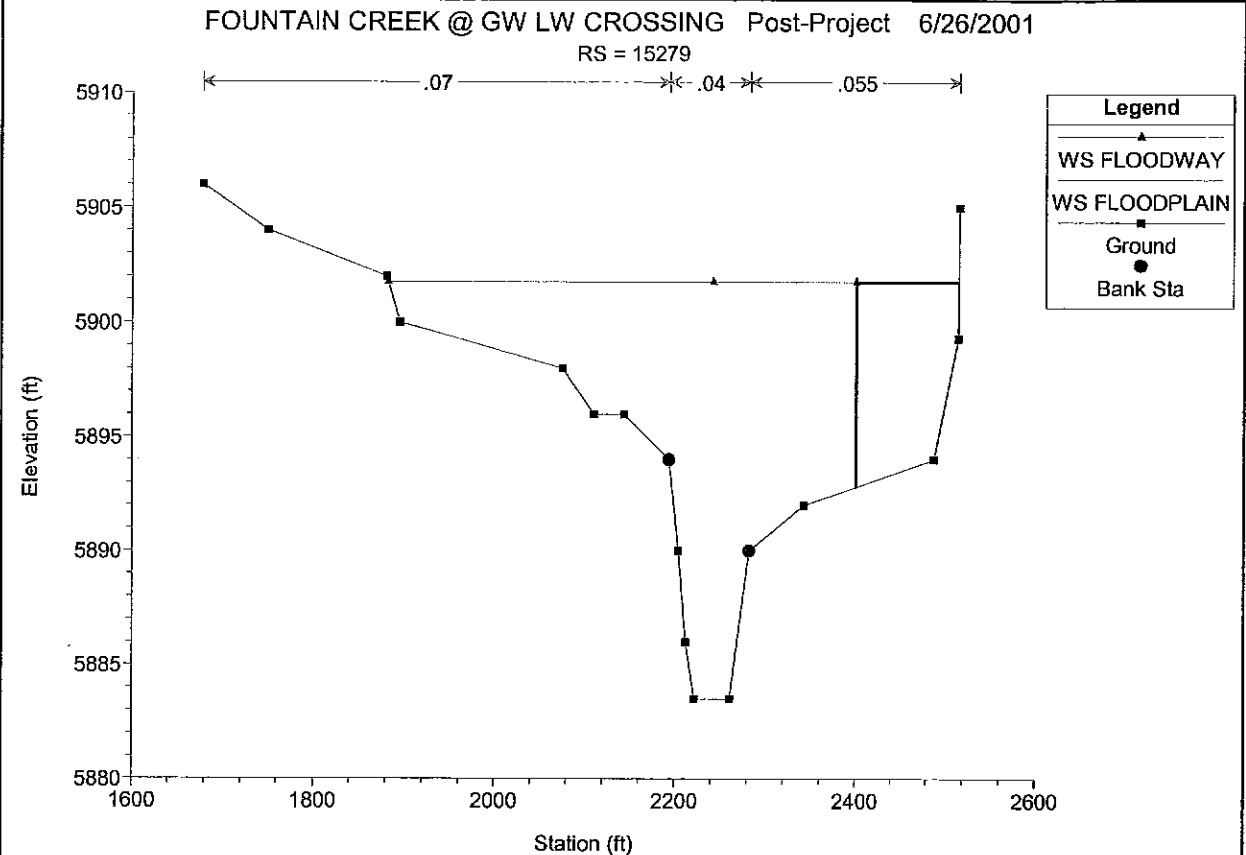
RS = 15700



FOUNTAIN CREEK @ GW LW CROSSING Post-Project 6/26/2001

RS = 15281



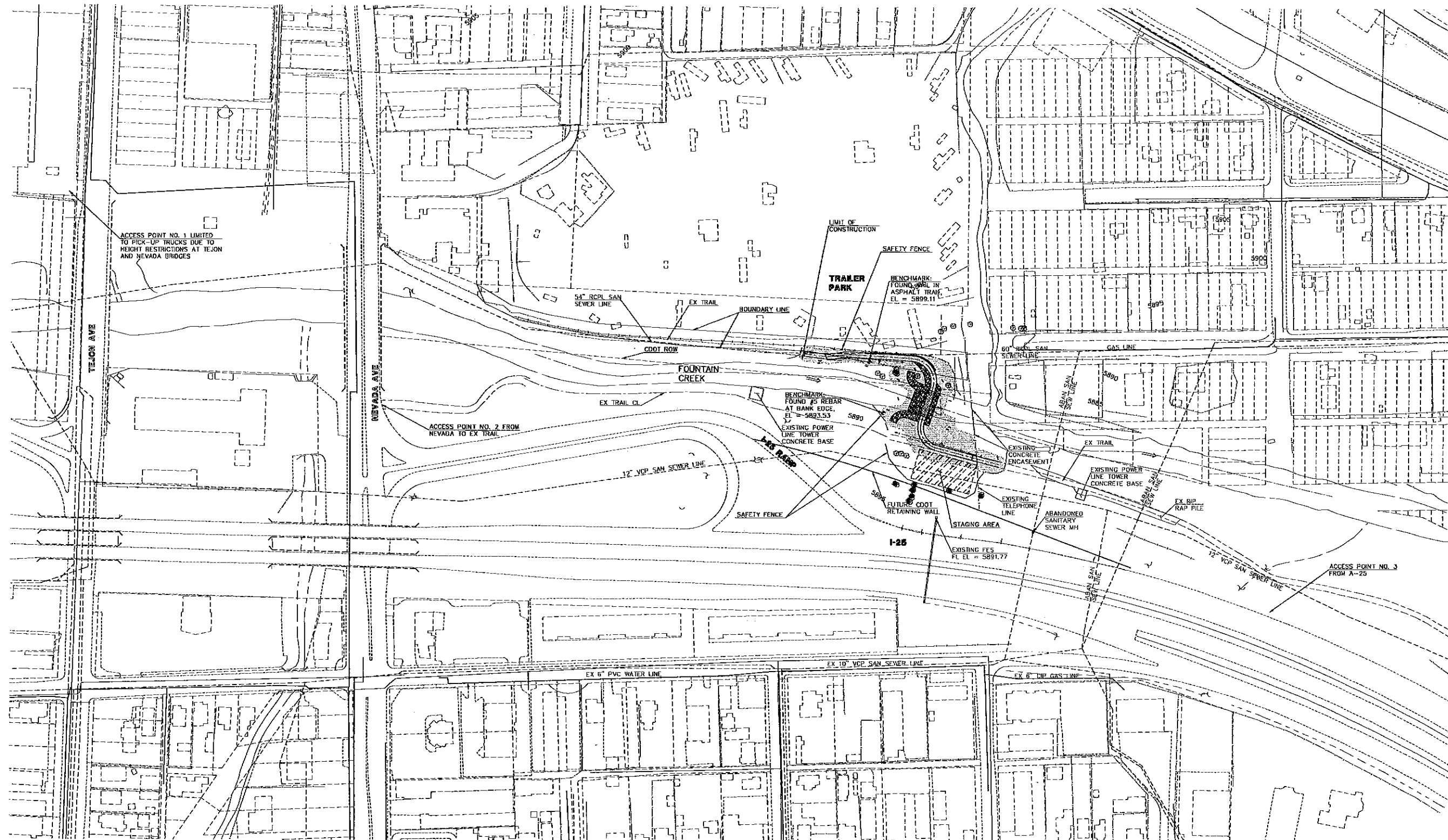


**APPENDIX D**

**PROJECT PLAN SHEETS**







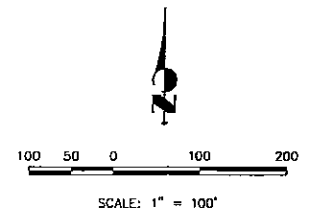
**NOTES:**

ACCESS POINT NO. 1: ACCESS EXISTING TRAIL FROM TEJON, DRIVE EAST ON EXISTING TRAIL TO SITE. THIS ACCESS POINT IS LIMITED TO PICKUP TRUCKS DUE TO HEIGHT RESTRICTIONS AT TEJON AND NEVADA BRIDGES.

ACCESS POINT NO. 2: ACCESS SITE FROM SOUTHBOUND NEVADA AVE. FOLLOW EXISTING TRAIL TO SITE.

ACCESS POINT NO. 3: ACCESS SITE FROM NORTHBOUND I-25. MAY REQUIRE COORDINATION WITH CDOT CONTRACTOR.

CONTRACTOR TO ALLOW CREEK FLOW DURING CONSTRUCTION OF PROJECT. THIS MAY BE ACCOMPLISHED THROUGH USE OF COFFER DAM OR TEMPORARY PIPING SYSTEM.



UNTIL SUCH TIME AS THESE DRAWINGS ARE APPROVED BY THE APPROPRIATE REVIEWING AGENCIES, OR ENGINEERING AGENCIES, THE CONTRACTOR SHALL BE RESPONSIBLE ONLY FOR THE PURPOSES DESIGNATED BY WRITTEN AUTHORIZATION.

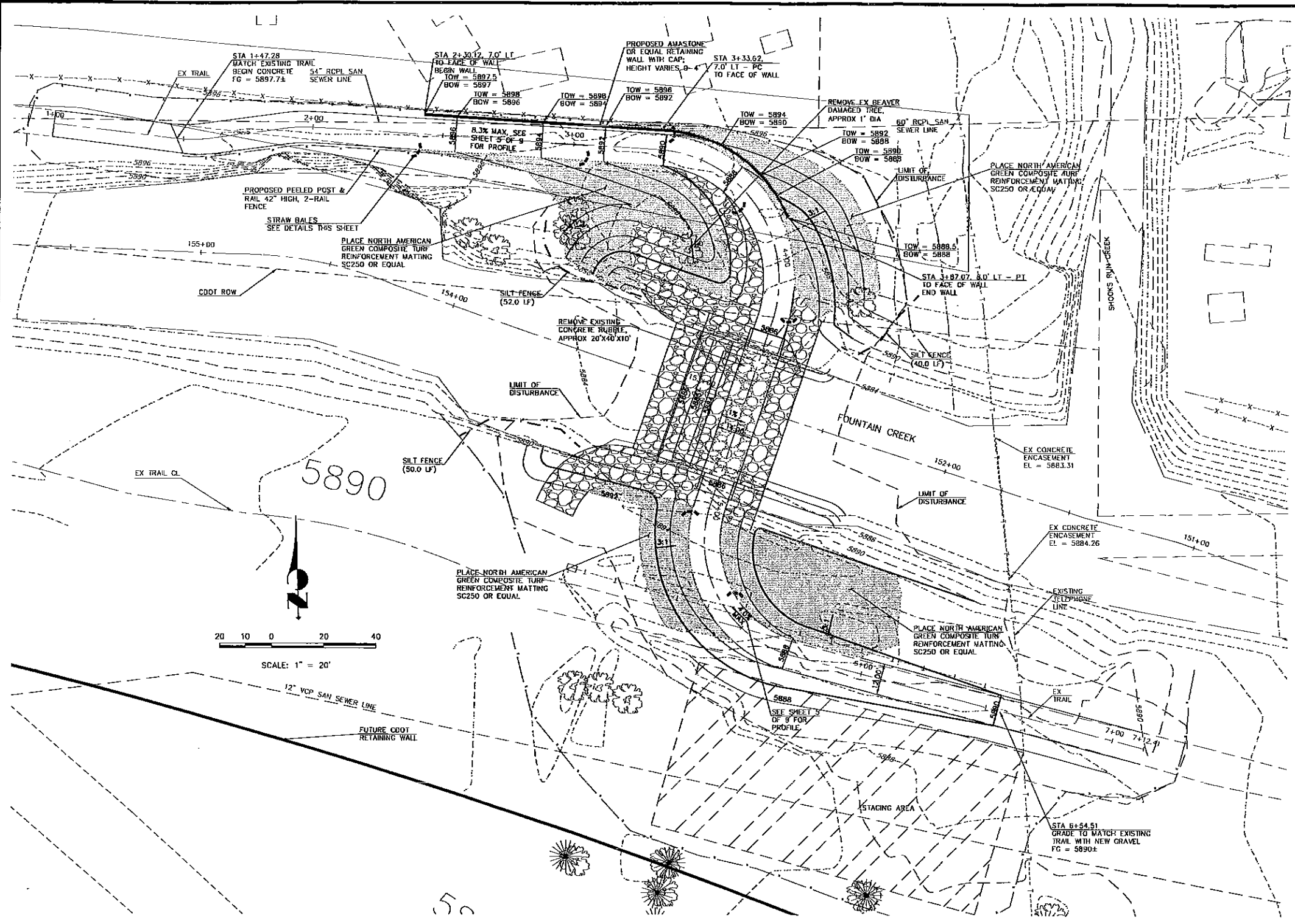
PREPARED FOR  
**CITY OF COLORADO SPRINGS**  
 PUBLIC WORKS DIVISION  
 430 ARROWHEAD DRIVE, COLORADO SPRINGS, CO 80907  
 TEL: 719-580-8800 FAX: 719-580-8801 WWW.COLORADOENGINEERING.COM

**J.R. ENGINEERING**  
 A Subsidiary of Woodman  
 Public Works Division  
 430 Arrowhead Drive • Colorado Springs, CO 80907  
 719-580-8800 • Fax 719-580-8801 • www.jrengineering.com

No.	BY	DATE

H-SCALE	V-SCALE	DATE	DESIGNED BY	DRAWN BY	CHECKED BY
VARIES	N/A	3/15/01	JAW	RCM	

PIKES PEAK GREENWAY TRAIL  
 LOW WATER CROSSING  
 CONSTRUCTION DRAWINGS  
 PROPERTY MAP AND CONSTRUCTION ACCESS



**EROSION PROTECTION & VEGETATION REQUIREMENTS**  
PER U.S.D.A. SOIL CONSERVATION SERVICE GUIDELINES (OR EQUIVALENT)

1. PRACTICE NO. & NAME: 342 - CRITICAL AREA TREATMENT SANDY FOOD-BILLS RANGE SITE

2. PLANNED: SEEDING PREP: A. METHOD: B. DATES: OCTOBER 15 - MAY 1 C. DATE: OCTO 15 - MAY 31 D. PLANTING DEPTH: 1/2" - 1/2"

SEEDING OPERATION: A. METHOD: DRILL XX INTERSEED BROADCAST B. DRILL SPACING: 12" TYPE: GRASS/AOITATOR C. DATE: OCTO 15 - MAY 31 D. PLANTING DEPTH: 1/2" - 1/2"

FERTILIZER: POUNDS ACTUAL PER ACRE N2 (AVAILABLE) P2O5 K

MULCH: KIND: LONG - STEM NATIVE HAY AMOUNT: 4,000 POUNDS/ACRE HOW-APPLIED: N/A HOW-ANCHORED: COMPACTED ANCHORAGE DEPTH: 4"

VARIETY	SPECIES	REQUIRED PLS RATES PER ACRE (100%)
COSMOS	FRASER SANDREED	6.5
VAUGHN	SOEDALIS GRAMA	2.0
LOUNGIN	BLUE GRAMA	3.0
BLACKWELL	WHITE GRAMA	4.5
PASTURA	LITTLE BLUESTEM	7.0

(2) % OF SPECIES IN MIXTURE	(3) PLS SEEDING RATE PER SPECIES/ACRE	(4) PLANNED ACRE	(5) TOTAL PLS LBS./SPECIES PLANNED (3) x (4)
15	0.98	13	12.7
22	2.22	13	28.9
15	0.45	13	5.9
20	0.90	13	11.7
28	1.72	13	22.8

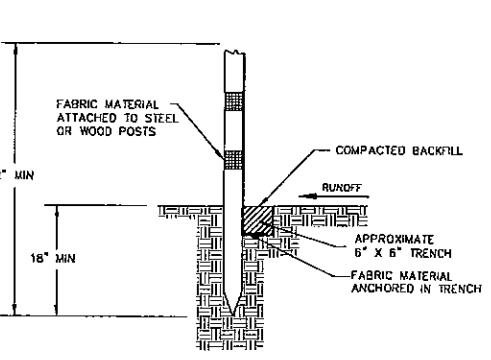
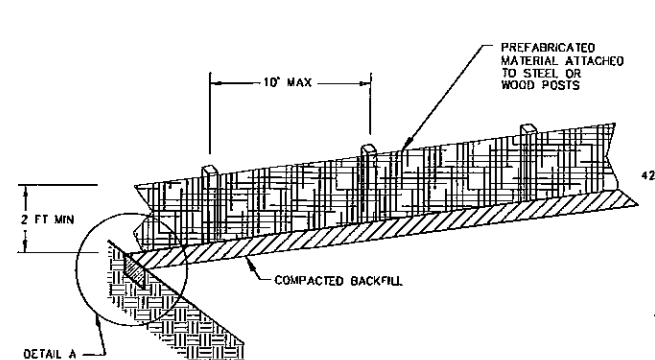
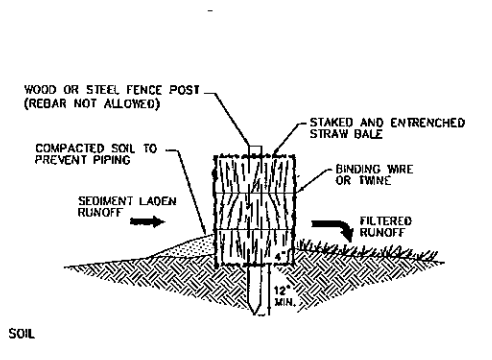
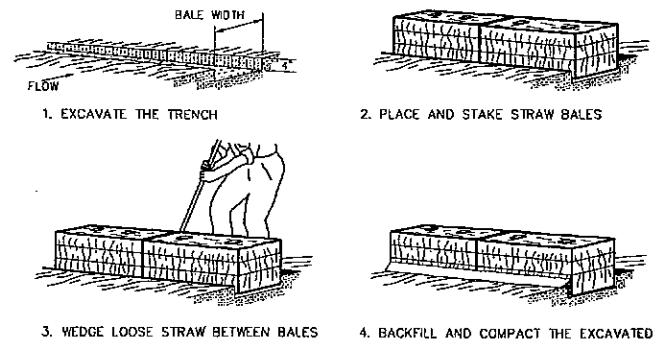
**TEMPORARY SEEDING**  
N.T.S.

**SEEDING GUIDELINES**

- SEEDBED PREPARATION**  
THE SEEDBED SHOULD BE WELL-SETTLED AND FIRM, BUT FRAGILE ENOUGH THAT THE SEED CAN BE PLACED AT THE SPECIFIED DEPTH. COMPETITIVE STANDS OF WEEDS THAT ARE RESISTANT BEFORE SEEDING MUST BE CONTROLLED BY SHALLOW TILLAGE OR BY APPLICATION OF HERBICIDES. SOILS THAT HAVE BEEN OVER-COMPACTED BY TRAFFIC OR EQUIPMENT, ESPECIALLY WHEN WET, SHOULD BE TILLED TO BREAK UP ROOTING-RESTRICTIVE LAYERS, THEN HARROWED, ROLLED, OR PACKED TO PREPARE THE REQUIRED FIRM SEEDBED.
- FERTILIZER**  
FERTILIZER SHOULD BE APPLIED AT A RATE OF 50 POUNDS OF AVAILABLE NITROGEN PER ACRE AND 40 POUNDS OF AVAILABLE PHOSPHATE PER ACRE. THE TIME OF APPLICATION SHOULD BE IMMEDIATELY PRIOR TO SEEDING, AT THE TIME OF SEEDING, OR IMMEDIATELY FOLLOWING SEEDING, DEPENDING ON THE KIND OF FERTILIZER AND TYPE OF EQUIPMENT USED.
- SEEDING**  
SEED SHOULD BE PLANTED WITH A GRASS DRILL ON ALL SLOPES OF 3:1 OR FLATTER. SEED MAY BE BROADCAST BY HAND, BY 33 MECHANICAL SPREADER, OR BY HYDRAULIC EQUIPMENT ON AREAS THAT ARE SMALL, TOO STEEP, OR NOT ACCESSIBLE FOR SEED DRILL OPERATIONS. SEED PLANTED WITH A DRILL SHOULD BE COVERED WITH SOIL TO A DEPTH OF 1/4 TO 3/4 INCH. SEED PLANTED BY THE BROADCAST METHOD SHALL BE INCORPORATED INTO THE SOIL SURFACE, NOT TO EXCEED A DEPTH OF 1 INCH, BY RAKING, HARROWING, OR OTHER PROVEN METHOD. THE TIME OF SEEDING IS FROM OCTOBER 15TH - MAY 31ST. SEED PLANTED IN THE LATE FALL WILL REMAIN DORMANT UNTIL SPRING, WHEN IT WILL GERMINATE.
- MULCHING**  
SEEDING AREAS SHOULD BE MULCHED TO CONSERVE MOISTURE; PREVENT SURFACE COMPACTION OR CRUSTING; REDUCE WIND AND EROSION; CONTROL INSECTS; AND HELP ESTABLISH PLANT COVER. NATIVE HAY OR STRAW SHOULD BE APPLIED AT A RATE OF 4,000 POUNDS PER ACRE AND CRUSHED INTO THE GROUND. ON SLOPES GREATER THAN 3:1, AN AGRONOMY BLANKET SHOULD BE USED.
- SUPPLEMENTAL WATER**  
IN LOW RAINFALL AREAS, WHERE WATER IS AVAILABLE AND WHERE RAPID ESTABLISHMENT IS NEEDED, IRRIGATION OF NEW SEEDING SHOULD BE PERFORMED DURING THE FIRST GROWING SEASON. WATER SHOULD BE APPLIED AT APPROXIMATELY ONE WEEK INTERVALS, AT A RATE OF 3/4 TO 1 INCH PER APPLICATION, WHEN RAINFALL IS DEFICIENT FOR PLANT DEVELOPMENT.

**LEGEND**

DESCRIPTION	SYMBOL
EXISTING GRADE INDEX CONTOUR	6910
EXISTING FINISH NOMINAL CONTOUR	6910
PROPOSED FINISH INDEX CONTOUR	6910
PROPOSED FINISH NOMINAL CONTOUR	6910
PROPERTY LINE	---
EXISTING STORM SEWER	---
SILT FENCE	---
STRAW BALE CHECK DAM	---



**STB STRAW BALE BARRIOR**  
N.T.S.

**SF SILT FENCE**  
N.T.S.

**STB STRAW BALE CHECK DAM**  
N.T.S.

THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK. THE CONTRACTOR SHALL BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE CAUSED BY HIS FAILURE TO EXACTLY LOCATE, AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.

48 HOURS BEFORE YOU DIG,  
CALL UTILITY LOCATORS  
**1-800-922-1987**  
UTILITY NOTIFICATION CENTER OF COLORADO  
GAS, ELECTRIC, WATER AND WASTEWATER

PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF OF J.R. ENGINEERING

**FOR REVIEW PURPOSES ONLY**

CYNTHIA M. BLEVINS, COLORADO P.E. #34484 DATE

UNTL SUCH TIME AS THESE DRAWINGS ARE APPROVED BY THE APPROPRIATE ENGINEERING AGENCIES, OR ENGINEERING APPROVES THEIR USE ONLY FOR THE PURPOSES AUTHORIZED.

PREPARED FOR

**CITY OF COLORADO SPRINGS**  
PARKS & RECREATION DEPARTMENT  
140 RESEARCH WAY, COLORADO SPRINGS, CO 80907

**J.R. ENGINEERING**  
A Subsidiary of Wertenit  
Public Works Division  
4310 Arroyo West Drive • Colorado Springs, CO 80907  
719-597-8800 • Fax: 719-528-6515 • www.jrengineering.com

BY	DATE	NO.	REVISION

H-SCALE 1"=20'  
V-SCALE N/A  
DATE 8/30/00  
DESIGNED BY JAW  
DRAWN BY RGM  
CHECKED BY

PIKES PEAK GREENWAY TRAIL  
LOW WATER CROSSING  
CONSTRUCTION DRAWINGS  
GRADING AND EROSION CONTROL PLAN

SHEET 3 OF 9  
JOB NO. 9247.20



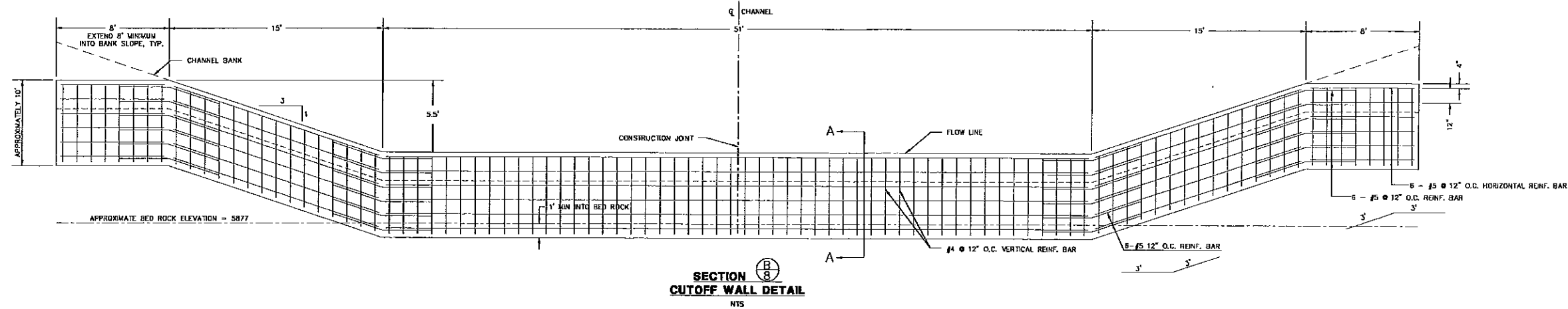




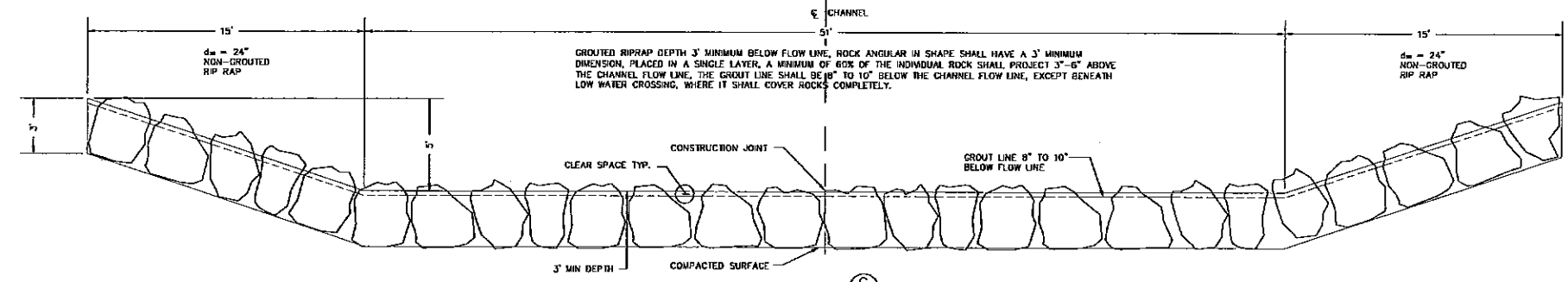




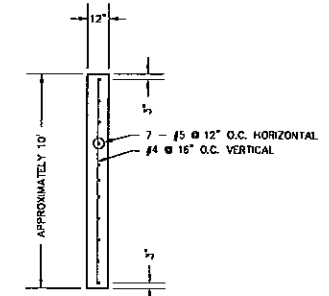




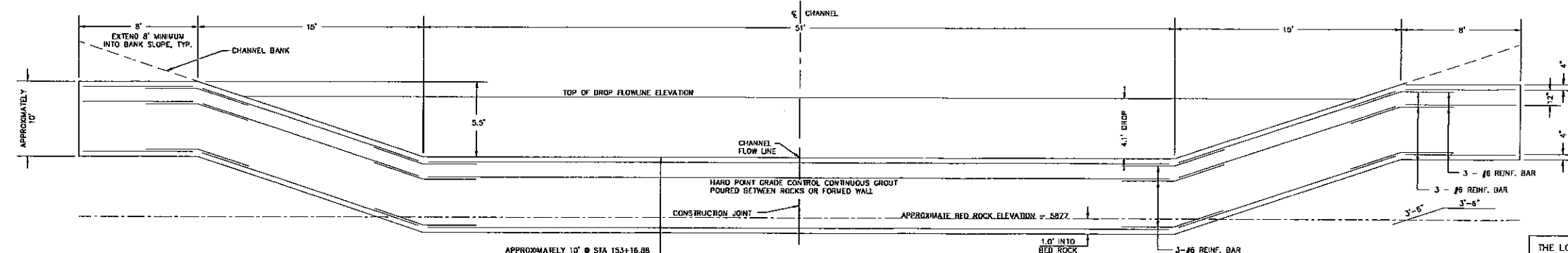
**SECTION B-B  
CUTOFF WALL DETAIL**  
NTS



**SECTION C-C  
HARD POINT GRADE CONTROL**  
NTS



**SECTION A-A  
REINFORCED CONCRETE CUTOFF WALL**



**SECTION D-D  
HARD POINT GRADE CONTROL**  
NTS

THE LOCATIONS OF EXISTING ABOVE GROUND AND UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK. THE CONTRACTOR SHALL BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE CAUSED BY HIS FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL ABOVE GROUND AND UNDERGROUND UTILITIES.

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CALL UTILITY LOCATORS  
1-800-922-1987**  
UTILITY NOTIFICATION CENTER OF COLORADO  
GAS, ELECTRIC, WATER AND WASTEWATER

PREPARED UNDER MY DIRECT SUPERVISION FOR AND ON BEHALF OF J.R. ENGINEERING

**FOR REVIEW PURPOSES ONLY**

CYNTHIA M. BLEVINS, COLORADO P.E. #34484 DATE

UNLESS SUCH TIME AS APPLICABLE IS SPECIFICALLY APPROVED BY THE APPROPRIATE REVIEWING AGENCIES, J.R. ENGINEERING APPROVES THEIR USE ONLY FOR THE PURPOSES INDICATED BY WRITTEN AUTHORIZATION.

**J.R. ENGINEERING**  
A Subsidiary of Weithin  
Public Works Division  
430 Arapahoe Drive • Colorado Springs, CO 80907  
719-590-8600 • Fax: 719-528-6650 • www.jrengineering.com

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Public Works Division  
430 Arapahoe Drive • Colorado Springs, CO 80907  
719-590-8600 • Fax: 719-528-6650 • www.jrengineering.com

NO.	REVISION	BY	DATE
1	ISSUED FOR PERMIT		
2			
3			
4			
5			
6			
7			
8			
9			
10			

H-SCALE	V-SCALE	DATE	DESIGNED BY	DRAWN BY	CHECKED BY
VARIES	N/A	4/20/01	JAW	JAW	