MASTER DEVELOPMENT DRAINAGE REPORT FOR THE RIDGE AT CUMBRE VISTA MASTER PLAN AND FINAL DRAINAGE REPORT FOR THE RIDGE AT CUMBRE VISTA FILING NO. 1

October 2014

Prepared for:

Rivers Development, Inc.

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Prepared by:



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DRAINAGE PLAN STATEMENTS

ENGINEER'S STATEMENT

The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria acceptable to the City of Colorado Springs. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Virgil A. Sanchez, P.E. #37160

For and on Behalf of M & S Civil Consultants, Inc.



DEVELOPER'S STATEMENT

I, the developer, have read and will comply with all the requirements specified in this drainage report and plan.

Jonathan Moore

TITLE Dir. of Engineering

ADDRESS:

Rivers Development, Inc.

13530 Northgate Estates Drive, Suite 200

Colorado Springs, CO 80921

CITY OF COLORADO SPRINGS

Filed in accordance with Section 7-7-906 of the Code of the City of Colorado Springs, 2001, as amended.

or The City Engineer

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MASTER DEVELOPMENT DRAINAGE REPORT FOR THE RIDGE AT CUMBRE VISTA MASTER PLAN AND FINAL DRAINAGE REPORT FOR THE RIDGE AT CUMBRE VISTA FILING NO. 1

PURPOSE

The purpose of this Master Development Drainage and Final Drainage Report is to establish the existing conditions and identify and analyze the proposed drainage patterns, determine proposed runoff quantities, size drainage structures for conveyance of developed runoff, and present solutions to drainage impacts on-site and off-site resulting from this development. The site to be known as The Ridge at Cumbre Vista Filing No. 1 will be developed as single family lots with on site detention. This site was annexed into the City of Colorado Springs by the Saddletree Village Annexation.

GENERAL LOCATION AND DESCRIPTION

The site is 13.7 acres and is located in a portion of the southeast quarter of Section 6, Township 13 South, Range 65 West of the 6th Principal Meridian currently within unincorporated El Paso County, Colorado. The site is bounded on the north by the existing Cowpoke Rd., on the south by Tri-Lakes Development Corporation (REC NO. 206170929), on the east by the Kit Carson Riding Club, and on the west by KF 103 CV LLC. (REC NO. 206170929).

The site is contained within the Sand Creek and Cottonwood Creek Basins. Flows from this site are tributary to both Sand Creek and Cottonwood Creek.

SOILS

Soils for this project are delineated by the map in the appendix as Columbine gravelly sandy loam (19). Soils in the study area are shown as mapped by S.C.S. in the "Soils Survey of El Paso County Area" are 51% of Hydrologic Group A and 49% Hydrologic Group B.

HYDROLOGIC CALCULATIONS

Hydrologic calculations were performed using the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual. The Rational Method was used to estimate storm water runoff anticipated from design storms with 5-year and 100-year recurrence intervals.

HYDRAULIC CALCULATIONS

Hydraulic calculations were estimated using the Manning's Formula and the methods described in the El Paso County and City of Colorado Springs Storm Drainage Design Criteria manual the pertinent data sheets are included in the appendix of this report.

CLIMATE

This area of El Paso County can be described as the foothills, with total precipitation amounts typical of a semi-arid region. Winters are generally cold and dry, and summers relatively warm and dry. Precipitation ranges from 12 to 14 inches per year, with the majority of this moisture occurring in the spring and summer in the form of rainfall. Thunderstorms are common during the summer months.

FLOODPLAIN STATEMENT

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel No. 08041C0529, effective date March 17, 1997, no portion of the site lies within a designated floodplain.

DRAINAGE CRITERIA

The drainage analysis has been prepared in accordance with the current City of Colorado Springs/El Paso County Drainage Criteria Manual. Calculations were performed to determine runoff quantities during the 5- year and 100-year frequency storms for developed conditions using the Rational Method as required for basins having areas less than 100 acres.

EXISTING DRAINAGE CONDITIONS

The overall site consists of 13.7 acres, and is currently occupied by three structures. The study area consists of undeveloped land with existing natural, grassy vegetation. The existing topography is sloping from the northwest to the southeast with slopes ranging from 2% to 10%. The initial grading project proposed will disturb 13.7 acres. A portion of the site drains to the Sand Creek Basin (12.64 acres) and the other portion of the site drains to the Cottonwood Creek Basin (1.08 acres). The Ridge at Cumbre Vista Filing No. 1 site proposes 65 single family residential lots. The proposed 65 single family lots will not adversely impact the existing surrounding residential infrastructure. The proposed BMP's in the plan and report shall be installed and maintained to accomplish this task.

As per the Historic Drainage flows map:

Basin A is located in the northwest portion of the site and contains 0.83 of undeveloped land. Basin A has existing flows of 0.7 cfs for the minor storm event (5-Year) and 1.7 cfs for the major storm event (100-Year). Runoff from Basin A will sheet flow offsite to the north of the site and will be conveyed west along Cowpoke Road to the Design Point two and ultimately to the Cottonwood Creek Basin.

Basin A1 is located in the northwest portion of the site and contains 0.25 of undeveloped land. Basin A1 has existing flows of 0.2 cfs for the minor storm event (5-Year) and 0.5 cfs for the major storm event (100-Year). Runoff from Basin A1 will sheet flow offsite to the northwest corner of the site and will combine with flows from Basin A at design point 2. Flows will be conveyed west

along Cowpoke Road and ultimately to the Cottonwood Creek Basin.

Basin B is located in the northeast portion of the site and contains 6.66 of undeveloped land. Basin B has existing flows of 4.4 cfs for the minor storm event (5-Year) and 11.0 cfs for the major storm event (100-Year). Runoff from Basin B will sheet flow offsite to the north and east of the site and will ultimately flow to the Sand Creek Basin.

Basin C is located in the northeast portion of the site and contains 5.98 of undeveloped land. Basin C has existing flows of 4.1 cfs for the minor storm event (5-Year) and 10.1 cfs for the major storm event (100-Year). Runoff from Basin C will sheet flow offsite to the south of the site. Off site developed flows per the "Amendment No. 1 to the Final Drainage Report for Cumbre Vista Filing No. 1 and Preliminary/Final Drainage Report for Cumbre Vista Filing No. 2, 3, 4 and 5,) prepared by JR Engineering, revised January 2007 (see appendix for drainage plan approval page and drainage map), are tributary to Basin C. Per the historic drainage map, Basin OS1 has existing flows of Q5=1.5 cfs and Q100=3.2 cfs at Design Point 1. These flows sheet flow onto Basin C. The combined flows at Design Point 4 ~ Q5=4.9 cfs and Q100=11.8 cfs will ultimately flow to the Sand Creek Basin.

PROPOSED DRAINAGE CONDITIONS

The following is a description of the onsite basins, offsite bypass flows and the overall proposed drainage characteristics for the development of The Ridge at Cumbre Vista Filing No. 1. The following Design Points and Basins were determined using the Rational Method since each individual basin is less then 100 acres and the combined acreage at any Design Point is also less than 100 acres. This method offers a more conservative approach to calculating swale cross sections and storm drain. The proposed drainage design for this subdivision is typical for single family residential, consisting of homes, landscaping, rear and side lot drainage swales curb & gutter, streets, curb inlets, and pipes to convey developed flows downstream.

Basin A is located in the east portion of the site and contains 0.34 acres of single family residential landscaping. Basin A has proposed design flows of 0.4 cfs for the minor storm event (5-Year) and 1.1 cfs for the major storm event (100-Year). Runoff from Basin A will sheet flow offsite to the east of the site and will be conveyed southeasterly to offsite Design Point 5. Design point 5 does not exceed the historic design flows of 4.4 cfs for the minor storm event (5-Year) and 11.0 cfs for the major storm event (100-Year).

Basin B is located in the east central portion of the site and contains 2.21 acres of single family residential lots, homes, landscaping and an asphalt roadway. Basin B has proposed design flows of 3.2 cfs for the minor storm event (5-Year) and 6.6 cfs for the major storm event (100-Year). Runoff from Basin B will flow, via side lot swales, to the curb and gutter and will be conveyed south to Design Point 1, a 10 foot D-10-R inlet in a sump condition. Collected flows from Design Point 1 will be conveyed via a 36 inch RCP (Pipe 1) directly to the water/quality detention facility for The Ridge at Cumbre Vista Filing No.1. In the event of clogging or total inlet failure, flows from Design Point 1 will overtop the curb and be conveyed directly to the water/quality detention facility.

Basin C is located in the central portion of the site and contains 6.84 acres of single family residential lots, homes, landscaping and an asphalt roadway. Basin C has proposed design flows of 12.7 cfs for the minor storm event (5-Year) and 26.3 cfs for the major storm event (100-Year). Runoff from Basin C will flow, via side lot swales, to the curb and gutter and will be conveyed south to Design Point 2, a 10 foot D-10-R inlet in a sump condition. Per this drainage report, Basin C will accept developed flows from Basin OS1 (Exist. Cumbre Vista Filing No. 5) and convey them via side lot swales to curb and gutter. Collected flows at Design Point 2 (Q5= 13.6 cfs, Q100= 28.3 cfs) will be conveyed in a 30 inch RCP (Pipe 2) to Design Point 1. In the event clogging or total inlet failure, flows from Design Point 2 will overtop the curb and be conveyed directly to the water/quality detention facility for The Ridge at Cumbre Vista Filing No. 1.

Basin D is located in the north portion of the site and contains 0.80 acres of single family residential lots, homes, landscaping and an asphalt roadway. Basin D has proposed design flows of 1.7 cfs for the minor storm event (5-Year) and 3.5 cfs for the major storm event (100-Year). Runoff from Basin D will sheet flow to the curb and gutter and will be conveyed north to Design Point 3, the existing curb and gutter located on the south side of Cowpoke Road. Collected flows from Design Point 3 will be conveyed through the existing infrastructure in Cowpoke Road to the Sand Creek Detention Pond No. 6.

Basin E is located in the northwest portion of the site and contains 1.27 acres of single family residential lots, homes, landscaping and an asphalt roadway. Basin E has proposed design flows of 2.0 cfs for the minor storm event (5-Year) and 4.1 cfs for the major storm event (100-Year). Roof drains and runoff, in this basin, shall drain to the front of the lot and will flow, via side lot swales, to the curb and gutter and will be conveyed north to Design Point 4, the existing curb and gutter located on the south side of Cowpoke Road. Collected flows from Design Point 4 will be conveyed through the existing infrastructure in Cowpoke Road west to Cottonwood Creek. Flows from Basin E will remain in the Cottonwood Creek drainage basin.

Water quality has been provided, for this basin, via a curb cut and sidewalk chase on Sunshine Drive which outlet into a T-3 Rain Garden water quality pond. The pond design is per the T-3 bioretention in the Urban Storm Drainage Criteria Manual Volume 3. Actual total capture volume is 949 cu.ft., The partial infiltration system will filtrate flow via a 1.5' deep Rain Garden growing media and export via a 4" perforated PVC pipe. A solid 4" PVC pipe will carry flow from the T-3 pond to the downstream curb and gutter on Cowpoke Road and outlet through a Neenah R-3262 storm water curb opening (See Neenah detail in Appendix). In case of system failure, emergency overflow will overtop the north top of berm and outfall onto Cowpoke Road. An emergency over flow has been provided for the 100 year flow. Flow will follow historic patterns along curb and gutter in Cowpoke Road.

Basin F is located in the southeast portion of the site and contains 0.32 acres and is the location of the water/quality detention facility for The Ridge at Cumbre Vista Filing No. 1. Basin F has proposed design flows of 0.4 cfs for the minor storm event (5-Year) and 1.0 cfs for the major storm event (100-Year). Runoff from Basin F is contained within its boundary in the water quality and detention facility. See paragraph **Detention** for pond details.

Basin G is located in the southern portion of the site and contains 0.47 acres of single family residential landscaping. Basin G has proposed design flows of 1.4 cfs for the minor storm event (5-

Year) and 3.0 cfs for the major storm event (100-Year). Runoff from Basin G will sheet flow offsite to the south of the site and will be conveyed south to offsite Design Point 6. Design point 6 does not exceed the historic design flows of of 4.4 cfs for the minor storm event (5-Year) and 11.0 cfs for the major storm event (100-Year).

Basin H is located in the southeast portion of the site and contains 0.12 acres of pond side slope and landscaping. Basin H has proposed design flows of 0.2 cfs for the minor storm event (5-Year) and 0.4 cfs for the major storm event (100-Year). Runoff from Basin H will sheet flow offsite to the south of the site and will be conveyed south to offsite Design Point 7. Design point 7 does not exceed the historic design flows of of 4.4 cfs for the minor storm event (5-Year) and 11.0 cfs for the major storm event (100-Year).

Basin I is located in the north central portion of the site and contains 0.95 acres of single family residential lots, homes, landscaping and an asphalt roadway. Basin I has proposed design flows of 1.8 cfs for the minor storm event (5-Year) and 3.8 cfs for the major storm event (100-Year). Runoff from Basin I will flow, via side lot swales, to the curb and gutter and will be conveyed north to Design Point 8, the existing curb and gutter located on the south side of Cowpoke Road. Collected flows from Design Point 8 will be conveyed through the existing infrastructure in Cowpoke Road to the Sand Creek Detention Pond No. 6.

Basin D & Basin I are tributary to Sand Creek Detention Basin No. 6 and was originally studied in the "Sand Creek Drainage Basin Planning Study Preliminary Design Report" (DBPS) prepared by Kiowa Engineering. This study was then updated in the "Sand Creek Drainage Basin Planning Study Preliminary Design Report Technical Addendum" by Kiowa, revised October 1995. This site was most currently studied in the "Master Development Drainage Plan Update for Woodmen Heights and Final Drainage Report for Forest Meadows Filing No. 1 and No. 4, and is being revised for a new single-family residential layout. Water quality has been provided within the Sand Creek Detention Pond No. 6 study for release onto Cowpoke Road.

Basin J is located in the west portion of the site and contains 0.05 acres of single family residential landscaping. Basin J has proposed design flows of 0.1 cfs for the minor storm event (5-Year) and 0.2 cfs for the major storm event (100-Year). Runoff from Basin J will sheet flow offsite to the west of the site and will be conveyed southerly, via historic topography within the utility corridor, to Design Point 9.

Basin K is located in the west portion of the site and contains 0.25 acres of single family residential landscaping. Basin K has proposed design flows of 0.3 cfs for the minor storm event (5-Year) and 0.7 cfs for the major storm event (100-Year). Runoff from Basin K will sheet flow offsite to the west of the site and will be conveyed northerly, via historic topography within the utility corridor, to Design Point 11. Basin K flows match those of the Historic Basin A1.

Basin OS1 is located in the west portion of the site and contains 0.54 acres of single family residential landscaping and natural native grass within the utility corridor. Basin OS1 has proposed design flows of 1.1 cfs for the minor storm event (5-Year) and 2.2 cfs for the major storm event (100-Year). Runoff from Basin OS1 will sheet flow onsite to the east onto Basin C and Design Point 2.

DETENTION

The water/quality detention facility will provide sufficient rainfall storage for the entire site. The detention pond will be private and maintained by the Homeowners Association. The pond was designed in accordance with the guidelines set forth by the "El Paso County and City of Colorado Springs Drainage Criteria Manual", Volumes 1 &2. The two stage release control structure shall be constructed for water quality and both the 5-year and 100-year detention requirements. The calculated release rates are provided in the appendix of this report.

All collected flows shall be detained within the 1.3 ac/ft detention pond facility and released through an outlet structure via a 18" PVC pipe discharging into the historic outfall location south of project site. The 18" PVC pipe shall be designed at a 1.0% slope to minimize velocities. A riprap pad with a flow speader will be constructed to dissipate energy and prevent local scour at the outlet. Discharged flows shall be restricted to a release rate of $(Q_{100}=9.2cfs)$ via a restrictor orifice/plate. In the event of clogging or total outlet failure, flows will over top the spillway overflow at elevation 6950.50 and continue southerly to discharge to the historic outfall location south of project site. The restricted release rate does not exceed the historic design flows of of 4.4 cfs for the minor storm event (5-Year) and 11.0 cfs for the major storm event (100-Year).

EROSION CONTROL

It is the policy of the City of Colorado Springs that we submit an erosion control plan with the drainage report. At this time we respectfully request that the erosion control plan be submitted in conjunction with the final grading plan. Proposed straw bale check dams, silt fence, vehicle traffic control, and reseeding are proposed as erosion control measures.

CONSTRUCTION COST OPINION

Public Drainage Facilities NON- Reimbursable

Item	Description	Quantity	Unit Cost		Cost
1.	18" RCP	31 LF	\$30/LF		\$ 930.00
2.	30" RCP	33 LF	\$40/LF		\$ 1,320.00
3.	36" RCP	24 LF	\$45/LF		\$ 1,080.00
4.	10' Sump Inlet	2 EA	\$5,000/EA		\$10,000.00
5.	WQCV System	1 EA	\$4,000/EA		\$ 4,000.00
6.	Pond Outlet Structure	1 EA	\$12,000/EA		\$12,000.00
				Total:	\$29,330.00

DRAINAGE FEES

A portion of this site is in the <u>Sand Creek Drainage Basin</u>. The 2014 Drainage Bridge and Pond fees per the City of Colorado Springs for THE RIDGE AT CUMBRE VISTA FILING NO. 1, are as follows;

*DRAINAGE FEES:	12.64 acres	X	\$10,247.00	=	\$129,522.08
BRIDGE FEES:	12.64 acres	X	\$ 622.00	=	\$ 7,862.08
POND FEES:					
LAND:	12.64 acres	X	\$1,070.00	=	\$ 13,524.80

FACILITIES:

12.64 acres

X

\$3,005.00

\$ 37,983.20

Total: \$188,892.16

A portion of this site is in the Cottonwood Creek Drainage Basin. The 2014 Drainage Bridge and Pond fees per the City of Colorado Springs for THE RIDGE AT CUMBRE VISTA FILING NO. 1, are as follows;

*DRAINAGE FEES: 1.08 acres

\$12,532.00 $\mathbf{X}^{'}$

\$ 13,534.56

BRIDGE FEES:

1.08 acres

\$ 924.00 \mathbf{x}

997.92

Total: \$ 14,532.48

DRAINAGE COST COMPARISON AND CREDIT SUMMARY

Public Facilities:

Total Public, reimbursable on-site drainage facility portion

\$0.00

*The Ridge at Cumbre Vista Filing No. 1 does not contain reimbursable facilities. Therefore, there are no fee off-sets.

M & S Civil Consultants, Inc. (M & S) cannot and does not guarantee the construction cost will not vary from these opinions of probable costs. These opinions represent our best judgment as design professionals familiar with the construction industry and this development in particular. The above is only an estimate of the facility cost and drainage basin fee amounts in 2014. Upon completion of the aforementioned improvements, M & S shall submit the actual construction costs to the City of Colorado Springs/City Drainage Board for reimbursement.

SUMMARY

Development of this site will provide protection from flooding to all residents and downstream interests for the 100-year storm event. Emergency overflows are provided where necessary. The drainage plan provided here-in fully complies with the "El Paso County and City of Colorado Springs Drainage Criteria Manual", Volumes 1 &2. Therefore, the construction of The Ridge at Cumbre Vista Filing No.1, will not adversely affect the downstream infrastructure of the site.

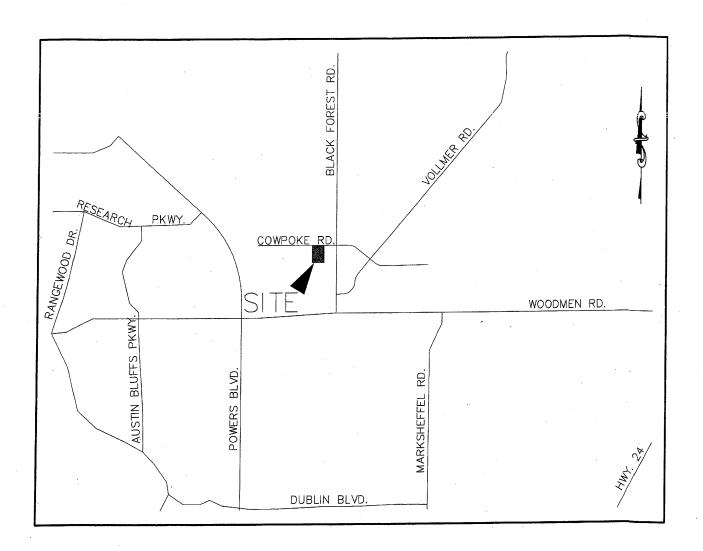
The Final Drainage Map is provided in the back pocket of this report.

REFERENCES

- 1.) "El Paso County and City of Colorado Springs Drainage Criteria Manual", Volumes 1 &2.
- 2.) "Urban Storm Drainage Criteria Manual", Volume 3.
- 3.) SCS Soils Map for El Paso County.
- 4.) "Sand Creek Drainage Basin Planning Study Preliminary Design Report" (DBPS), prepared by Kiowa Engineering, revised December 1998.
- 5.) "Sand Creek Drainage Basin Planning Study Preliminary Design Report Technical Addendum", prepared by Kiowa Engineering, revised October 1995.
- 6.) "Master Development Drainage Plan Update for Woodmen Heights and Final Drainage Report for Forest Meadows Filing No. 1 and No. 4", prepared by Engineering and Surveying, Inc., approved February 5, 2006.
- 7.) "Amendment No. 1 to the Final Drainage Report for Cumbre Vista Filing No. 1 and Preliminary/Final Drainage Report for Cumbre Vista Filing No. 2, 3, 4 and 5", prepared by JR Engineering, revised January 2007.

APPENDIX

VICINITY MAP



VICINITY MAP

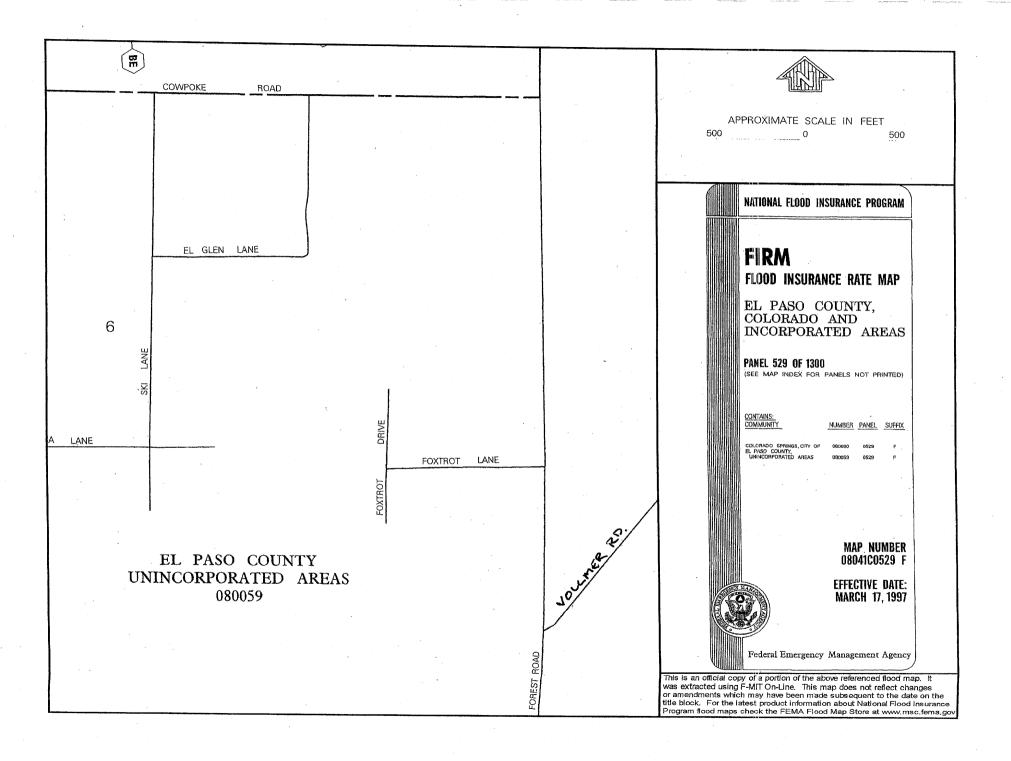
SOILS MAP



Map Unit Legend

	El Paso County Area,		Percent of AOI
Map Unit Symbol	Map Unit Name	Acres in AOI	Percention ACI
8	Blakeland loamy sand, 1 to 9 percent slopes	0.0	0.0%
9	Blakeland-Fluvaquentic Haplaquolls	10.3	4.1%
19	Columbine gravelly sandy loam, 0 to 3 percent slopes	128.8	51.0%
71	Pring coarse sandy loam, 3 to 8 percent slopes	6.6	2.6%
85	Stapleton-Bernal sandy loams, 3 to 20 percent slopes	106.8	42.3%
Totals for Area of Interest	1	252.5	100.0%

FLOODPLAIN MAP



HYDROLOGIC CALCULATIONS

The Ridge at Cumbre Vista Filing No.1 FINAL DRAINAGE REPORT (Historic Area Drainage Summary)

From Com	posite Runoff (Coefficient St	ummary		OVER	LAND		STRE	ET / CH	ANNEL F	LOW	Time of Travel (T_t)	INTEN	SITY *	TOTAL .	FLOWS
BASIN	AREA TOTAL	C ₅	C ₁₀₀	C ₅	Length	Height	T _C	Length	Slope	Velocity	T _t	TOTAL	I ₅	I ₁₀₀	Q ₅	Q ₁₀₀
	(Acres)	From DCM	f Table 5-1		(ft)	(ft)	(min)	(ft)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
OS1	0.54	0.25	0.35	0.25	62	10	5.0	0	0.0%	0.0	0.0	14.1	3.6	6.3	0.5	1.2
												*from CVS report	-			
\boldsymbol{A}	0.83	0.25	0.35	0.25	280	10	17.5	0	0.0%	0.0	0.0	17.5	3.2	5.7	0.7	1.7
	i I			l												
A1	0.25	0.25	0.35	0.25	215	6.5	16.2	0	0.0%	0.0	0.0	16.2	3.3	6.0	0.2	0.5
В	6.66	0.25	0.35	0.25	684	30	25.5	0	0.0%	0.0	0.0	25.5	2.7	4.7	4.4	11.0
	1												ľ			ĺ
C	5.98	0.25	0.35	0.25	684	34	24.5	0	0.0%	0.0	0.0	24.5	2.7	4.8	4.1	10.1
												,				
				ŧ												

CA ₅	Basin	CA ₁₀₀
0.14	OS1	0.19
0.21	Α	0.29
0.06	A1	0.09
1.67	В	2.33
1.50	С	2.09

Calculated by: ET

Date: 8/22/2014

^{*} Report for Cumbre Vista Sub.(CVS) FilingN0. 1, 2, 3,4 & 5

^{*} Intensity equations assume a minimum travel time of 5 minutes.

The Ridge at Cumbre Vista Filing No.1 FINAL DRAINAGE REPORT

(Historic Surface Routing Summary)

					Inte	nsity	Fl	ow	
Design Point(s)	Contributing Basins/Design Points	Equivalent CA 5	Equivalent CA ₁₀₀	Maximum T _C	I_{5}	I 100	Q 5	Q 100	Comments
1	OS1	0.14	0.19	14.1	3.6	6.3	0.5	1.2	SHEET FLOW ONSITE
2	A & A1	0.27	0.38	17.5	3.2	5.7	0.9	2.2	SHEET FLOW OFFSITE
3	В	1.67	2.33	25.5	2.7	4.7	4.4	11.0	SHEET FLOW OFFSITE
4	C & DP1	1.63	2.28	24.5	2.7	4.8	4.4	11.0	SHEET FLOW OFFSITE

Calculated by: ET

Date: 8/22/2014

The Ridge at Cumbre Vista Filing No.1 FINAL DRAINAGE REPORT

(Area Drainage Summary)

From Comp	posite Runoff (Coefficient St	ımmary		OVER	LAND		STRE	EET / CH	ANNEL F	LOW	Time of Travel (T ,)	INTEN	SITY *	TOTAL	FLOWS
BASIN	AREA TOTAL	C ₅	C ₁₀₀	C ₅	Length	Height	$T_{\rm c}$	Length	Slope	Velocity	T _t	TOTAL	I ₅	Ĭ ₁₀₀	Q ₅	Q ₁₀₀
	(Acres)			0.05	(fi)	(fi)	(min)	(fi)	(%)	(fps)	(min)	(min)	(in/hr)	(in/hr)	(c.f.s.)	(c.f.s.)
Ą	0.34	0.25	0.35	0.25	20	6	2.3	0	0.0%	0.0	0.0	5.0	5,1	9.1	0.4	1.1
В	2.21	0.60	0.70	0.25	234	1.5	28.2	550	1.1%	3.7	2.5	30.6	2.4	4.3	3.2	6.6
С	6.84	0.60	0.70	0.25	335	18	16.7	505	1.0%	3.6	2.4	19.1	3.1	5.5	12.7	26.3
D	0.80	0.60	0.70	0.25	258	16	14.0	54	3.7%	6.7	0.1	14.1	3.6	6.3	1.7	3.5
E	1.27	0.60	0.70	0.25	231	2	25.3	274	1.5%	4.2	1.1	26.4	2.6	4.6	2.0	4.1
F	0.32	0.25	0.35	0.25	23	4	3.0	0	0.0%	0.0	0.0	5.0	5.1	9.1	0.4	1.0
G	0.47	0.60	0.70	0.25	63	14	4.5	0	0.0%	0.0	0.0	5.0	5.1	9.1	1.4	3.0
H	0.12	0.25	0.35	0.25	26	8	2.6	0	0.0%	0.0	0.0	5.0	5.1	9.1	0.2	0.4
I	0.95	0.60	0.70	0.25	78	0.5	16.3	400	1.1%	3.7	1.8	18.0	3.2	5.6	1.8	3.8
J	0.05	0.25	0.35	0.25	12	4	1.7	Ó	0.0%	0.0	0.0	5.0	5.1	9.1	0.1	0.2
K	0.25	0.25	0.35	0.25	48	103	8.6	0	0.0%	0.0	0.0	8.6	4.3	7.7	0.3	0.7
OS1	0.54	0.55	0.65	0.25	62	10	5.0	0	0.0%	0.0	0.0	14.1 *from CVS report	3.6	6.3	1.1	2.2

)	CA ₅	Basin	CA ₁₀₀
	0.09	A	0.12
	1.33	В	1.55
	4.10	С	4.79
	0.48	D	0.56
	0.76	E	0.89
	0.08	F	0.11
	0.28	G	0.33
	0.03	H	0.04
	0.57	ı	0.67
	0.01	1	0.02
,	0.06	K	0.09
?	0.30	OS1	0.35

Calculated by: ET
Date: 9/4/2014

^{*} Report for Cumbre Vista Sub.(CVS) FilingN0. 1, 2, 3,4 & 5

^{*} Intensity equations assume a minimum travel time of 5 minutes.

The Ridge at Cumbre Vista Filing No.1 FINAL DRAINAGE REPORT (Surface Routing Summary)

	,				Inte	nsity	Fl	ow	
Design Point(s)	Contributing Basins/Design Points	Equivalent CA 5	Equivalent CA ₁₀₀	Maximum T _C	I_5	I 100	Q ₅	Q 100	Comments
5	. A	0.09	0.12	5.0	5.1	9.1	0.4	1.1	SHEET FLOW OFFSITE
1	В	1.33	1.55	30.6	2.4	4.3	3.2	6.6	10' SUMP INLET
2	C & DP 9 & DP 11	4.41	5.16	19.1	3.1	5.5	13.6	28.3	10' SUMP INLET
3	D & DP 8	1.05	1.23	14.1	3.6	6.3	<i>3.7</i>	7.8	SAND CREEK BASIN
4	Е	0.76	0.89	26.4	2.6	4.6	2.0	4.1	COTTONWOOD BASIN
POND	F & DP1 & DP2	5.82	6.82	30.6	2.4	4.3	13.9	29.0	POND
6	G	0.28	0.33	5.0	5.1	9.1	1.4	3.0	SHEET FLOW OFFSITE
7	H	0.03	0.04	5.0	5.1	9.1	0.2	0.4	SHEET FLOW OFFSITE
8	I	0.57	0.67	18.0	3.2	5.6	1.8	3.8	SAND CREEK BASIN
9	J	0.01	0.02	5.0	5.1	9.1	0.1	0.2	SHEET FLOW OFFSITE
10	K	0.06	0.09	8.6	4.3	7.7	0.3	0.7	SHEET FLOW OFFSITE
11	OS1	0.30	0.35	14.1	3.6	6.3	1.1	2.2	SHEET FLOW BASIN C

Calculated by: ET
Date: 8/4/2014

HYDRAULIC CALCULATIONS

The Ridge at Cumbre Vista Filing No.1 FINAL DRAINAGE REPORT

(Storm Sewer Routing Summary)

	Contributing	<i>Equivalent</i>	Equivalent	Maximum	Inte	nsity	Fl	ow		
Pipe Run	Design Points/Pipe Runs			CA_{100} T_{C}		I_5 I_{100} Q_5		Q 100	Comments	
1	1 & 2	5.74	6.70	30.6	2.39	4.26	13.7	28.6	36" RCP	
2	2	4.41	5.16	19.1	3.08	5.49	13.6	28.3	30" RCP	

DP - Design Point

INT- Intercepted Flow from Design Point

Calculated by: ET

Date: 8/4/2014

The Ridge at Cumbre Vista Filing No.1 FINAL DRAINAGE REPORT

(Street Capacity Summary - Initial Storm)

Street Name	Contributing Basins	Street Side (Cardinal Directions) at max Q5	Street Class	Curb Type	Street Slope (ft/ft)	Actual Q5	Max. Q5 (cfs) (10/12/94 Eq's)	Depth At Curb Face (ft) (Fig 7-12 Eq.)	Q5 Max. Check Max>Actual<20cfs (res ramp), 34cfs(other)	Q5 Depth Check
EAST	. B	E	Residential	RAMP	0.026	3.2	18.2	0.19	OK	OK
WEST	C	W	Residential	RAMP	0.045	13.6	23.9	0.29	OK	OK

Notes:

1. Cross slope of 2% assumed for all streets.

2. Data shown for critical location within basin.

3. Basin Q's for streets not determined by surface routing have been added together (conservative).

Calculated by: ET

Date: 1/3/2014 Checked by: VAS

THE RIDGE AT CUMBRE VISTA FILING NO.1 FINAL DRAINAGE REPORT

(Inlet Calculations - Sump Condition)

DESIGN POINTS 1 AND 2

Total Flow:

 $Q_5 = 16.8 \text{ cfs } *$

 Q_{100}

34.8 cfs *

Maximum allowable ponding depth at sump:

 $Dmax_5 = 0.50'$

 $Dmax_{100} = 0.67'$

 $Qi = 1.7(Li+1.8(W))(Dmax + w/12)^{1.85}$

where: W = 3 feet

w = 4 inches

Clogging Factor = 1.25

Li(1.25) = Length of inlet opening

5-Year Event:

6 foot inlet required

100-Year Event:

10 foot inlet required

(Install a Public 10' D-10-R inlet to accept both 5 yr. & 100 yr. developed flows at this design point.)

*ASSUME FLOWS SPLIT AT SUMP LOCATION

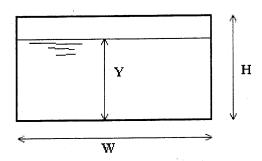
Calculated by: ET

Date: 8/4/2014

BOX CONDUIT FLOW (Normal & Critical Depth Computation)

Project: The Ridge at Cumbre Vista Filing No. 1

Box ID: Curb Cut



Design Information (Input) Box conduit invert slope	So =	0.0140	ft/ft
•	n =	0.0130	+
Box Manning's n-value	W =	2.00	- _{ft}
Box Width	• • • • • • • • • • • • • • • • • • • •	0.67	- <mark>l</mark> it
Box Height	H= -	2.00	cfs
Design discharge	Q =[2.00	Jois
Full-flow capacity (Calculated)	p		
Full-flow area	Af =	1.34	sq ft
Full-flow wetted perimeter	Pf =	5.34	ft
Full-flow capacity	Qf =	7.23	cfs
•			
Calculations of Normal Flow Condition			
Normal flow depth (<h)< td=""><td>Yn =</td><td>0.23</td><td>ft</td></h)<>	Yn =	0.23	ft
Flow area	An =	0.45	sq ft
Wetted perimeter	Pn =	2.45	ft
Flow velocity	Vn =	4.40	fps
Discharge	Qn =	2.00	cfs
Percent Full	Flow =	27.7%	of full flow
Normal Depth Froude Number	Fr _n =	1.63	supercritical
Calculation of Critical Flow Condition			
Critical flow depth	Yc =	0.31	ft
Critical flow area	Ac =	0.63	sq ft
Critical flow velocity	Vc =	3.18	fps
Critical Depth Froude Number	Fr _c =	1.00	

Free Online Manning Pipe Flow Calculator

List of Calculators Hydraulics Language

Manning Formula Uniform Pipe Flow at Given Slope and Depth

Can you help me translate this calculator to your language or host this calculator at your web site?

QBC	and administration of the property of the prop			00.00000000000000000000000000000000000	
PIPE CULVERT	_ :				
		Results:			-
		Flow, q	34.3378	cfs	V
Set units: m mm ft inches	· · · · · · · · · · · · · · · · · · ·	Velocity, v	9.3562	ft/sec	~
Pipe diameter, d ₀	30	Velocity head, h _v	1.3605	ft	▽
	inches 🗸	Flow area	3.6702	ft^2	V
Manning roughness, n ?	.013	Wetted perimeter	4.9557	ft	V
Pressure slope (possibly ? equal	1.0	Hydraulic radius	0.7406	ft	V
to pipe slope), S ₀	% rise/run 🗸	Top width, T	2.2913	ft	~
Percent of (or ratio to) full depth	70	Froude number, F	1.30		
(100% or 1 if flowing full)	% \	Shear stress (tractive force), tau	1.0927	psf	V

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Technical Documents | Blog (new in 2009) | Personal essays | Collaborative Family Trees

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Free Online Manning Pipe Flow Calculator

List of Calculators Hydraulics Language

Manning Formula Uniform Pipe Flow at Given Slope and

Depth

Can you help me translate this calculator to your language or host this calculator at your web site?

QBC	rogic op judicija konstrukcija poveznika u konstrukcija povjek vyteni dobite na maka na cirki dobi				
PIPE CULVERT					
		Results:			
		Flow, q	55.8370	cfs	Y
Set units: m mm ft inches		Velocity, v	10.5654	ft/sec	>
Pipe diameter, d₀	36	Velocity head, h _v	1.7349	ft	V
	inches 🗸	Flow area	5.2851	ft^2	~
Manning roughness, n ?	.013	Wetted perimeter	5.9469	ft	<
Pressure slope (possibly ? equal	1.0	Hydraulic radius	0.8887	ft	>
to pipe slope), S ₀	% rise/run ✓	Top width, T	2.7495	ft	<
Percent of (or ratio to) full depth (100% or 1 if flowing full)	70 % ∨	Froude number, F	1.34		
(100% of 1 if flowing full)	70	Shear stress (tractive force), tau	1.3112	psf	Y

Please give us your valued words of suggestion or praise. Did this free calculator exceed your expectations in every way?

<u>Home</u> | <u>Support</u> | <u>FreeSoftware</u> | <u>Engineering Services</u> | <u>Engineering Calculators</u> | <u>Technical Documents</u> | <u>Blog (new in 2009)</u> | <u>Personal essays</u> | <u>Collaborative Family Trees</u> | <u>Contact</u>

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Free Online Manning Pipe Flow Calculator

List of Calculators Hydraulics Language

Manning Formula Uniform Pipe Flow at Given Slope and

Depth

Can you help me translate this calculator to your language or host this calculator at your web site?

Shiloh Mesa					
PIPE CULVERT			-	·	
		Results:			
Cat with		Flow, q	9.1167	cfs	V
Set units: m mm ft inches		Velocity, v	6.6933	ft/sec	~
Pipe diameter, d₀	18	Velocity head, h _v	0.6963	ft	V
	inches V	Flow area	1.3621	ft^2	V
Manning roughness, n ?	.013	Wetted perimeter	3.0396	ft	V
Pressure slope (possibly ? equal to	7············		0.4481	ft	V
pipe slope), S ₀	% rise/run ✓	Top width, T	1.3470	ft	~
Percent of (or ratio to) full depth	72	Froude number, F	1.17	k	
(100% or 1 if flowing full)	% ✓	Shear stress (tractive force), tau	0.6743	psf	>

Please give us your valued words of suggestion or praise. Did this free calculator exceed your expectations in every way?

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Last Modified 10/07/2014 15:02:27

WOCV EMERGENCY OVERFLOW

Other Calculators

- Air Flow Conversion
 Calculator
- ** Atmospheric Calculator
- Block Wall Calculator
- Concrete Column
 Calculator
- Concrete Volume
 Calculator
- Energy Conversion
 Calculator
- lsentropic Flow Relations
 Calculator
- Laser Real Time Unit
 Converter
- Normal Flow Relations
 Calculator
- Oblique Flow Relations
 Calculator
- Open-channel Flow Calculator
- Properties of Welds

 Treated as Lines
 Calculator
- Shaft Speed Calculator
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- **Mathematics**

This calculator uses Chéry and Manning's formula to calculate the wetted perimeter

This calculator uses Chézy and Manning's formula to calculate the wetted perimeter, hydraulic radius, flow area, Chézy coefficient and flow velocity.

For experimental values of Manning's n factor, click here

Required Information

Open-Channel Flow

Enter the Slope: 0.01 Enter the Channel Top Width (ft):

Enter the Channel Bottom 10 Enter the Channel Width (ft):

0.25 Enter the n value:

0.035

12

0.25

Results

The wetted perimeter is 12.061 ft

The flow is 4.36921 ft³/s

The flow area is 2.75 ft²

Enter the Flow Depth (ft):

The flow is 1960.905 gal/min

The hydraulic radius is 0.2279 ft

The velocity is 1.58880 ft/s

The C value is 33.2741

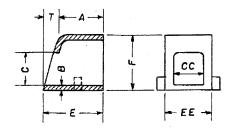
Calculate Reset

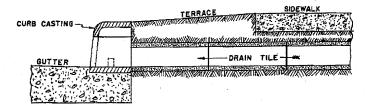
NEENAH TF

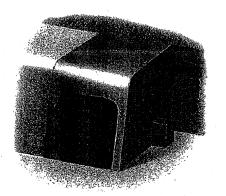
R-3262 Series

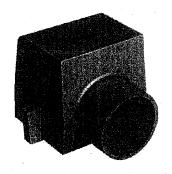
Storm Water Curb Openings

Heavy Duty









Rear view of R-3262-3 only. (optional)

Curb opening castings are used as shown, where it is advantageous to transmit stormwater from downspout in shallow drains and discharge it through the curb to the street gutter.

Catalog No.	A	. В	С	C-C	E	E-E	F	T
R-3262-1	5	1/2	4	4	6	5	7	1
R-3262-2	6	1/2	4	4	8 1/4	5	6	2 1/4
R-3262-3*	5	1/2	4	5 1/2	6	6 1/2	6 1/2	1
R-3262-4	5	1/2	4	16	7	17	6 3/8	2
R-3262-6	6	1/2	6	6	8	7 1/4	9	2

^{* 4&}quot; ID outlet is optional

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DETENTION POND & WQCV CALCULATIONS

Design Procedure Form: Rain Garden (RG)

Sheet 1 of 2

Desi	ia.	20	•

EUGENE TELLEZ

Company:

MS CIVIL CONSULTANTS, INC

Date:

September 12, 2014

Project:

THE RIDGE AT CUMBRE VISTA FILING NO. 1

Location:

ADJACENT TO COWPOKE ROAD AND WEST OF BLACK FOREST ROAD

1. Basin Storage Volume

- A) Effective Imperviousness of Tributary Area, I_a (100% if all paved and roofed areas upstream of rain garden)
- B) Tributary Area's Imperviousness Ratio (i = I_a/100)
- C) Water Quality Capture Volume (WQCV) for a 12-hour Drain Time (WQCV= $0.8 * (0.91^{\circ})^3 1.19 * i^2 + 0.78 * i)$
- D) Contributing Watershed Area (including rain garden area)
- E) Water Quality Capture Volume (WQCV) Design Volume Vol = (WQCV / 12) * Area
- F) For Watersheds Outside of the Denver Region, Depth of Average Runoff Producing Storm
- G) For Watersheds Outside of the Denver Region, Water Quality Capture Volume (WQCV) Design Volume
- H) User Input of Water Quality Capture Volume (WQCV) Design Volume (Only if a different WQCV Design Volume is desired)

- I_a = 54.0 %
- i = 0.540

WQCV = 0.17 watershed inches

V_{WQCV} = 865 cu ft

$$d_6 = in$$

V_{WQCV OTHER} =

V_{WQCV USER} = ____ cu ft

2. Basin Geometry

- A) WQCV Depth (12-inch maximum)
- B) Rain Garden Side Slopes (Z = 4 min., horiz. dist per unit vertical) (Use "0" if rain garden has vertical walls)
- C) Mimimum Flat Surface Area
- D) Actual Flat Surface Area
- E) Area at Design Depth (Top Surface Area)
- F) Rain Garden Total Volume (V_T= ((A_{Top} + A_{Actual}) / 2) * Depth)

- D_{wqcv} = 9 in
 - Z = 4.00 ft / ft
 - A_{Min} = <u>577</u> sq ft
- A_{Actual} = _____ 767 ____ sq ft
 - $A_{\mathsf{Top}} = \underline{1763} \quad \mathsf{sq} \; \mathsf{ft}$
 - V_T= 949 cu ft

3. Growing Media

- Choose One
 18" Rain Garden Growing Media
- Other (Explain):

4. Underdrain System

- A) Are underdrains provided?
- B) Underdrain system orifice diameter for 12 hour drain time
 - i) Distance From Lowest Elevation of the Storage Volume to the Center of the Orifice
 - ii) Volume to Drain in 12 Hours
 - iii) Orifice Diameter, 3/8" Minimum

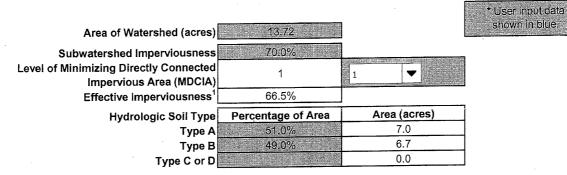
- Choose One -
- YES ○ NO
- y = <u>1.8</u> ft
- Vol₁₂ = 865 cu ft
 - $D_0 = 0.70$ i

	Design Procedu	re Form: Rain Garden (RG)
		Sheet 2 of 2
Designer:	EUGENE TELLEZ	The state of the s
Company:	MS CIVIL CONSULTANTS, INC	· · · · · · · · · · · · · · · · · · ·
Date:	September 12, 2014 THE RIDGE AT CUMBRE VISTA FILING NO. 1	
Project:	ADJACENT TO COWPOKE ROAD AND WEST OF BLACK FORE	STROAD
Location:	ADJACENT TO COWFORE ROAD AND WEST OF BEACK PORE	ST NOAD
A) Isani	able Geomembrane Liner and Geotextile Separator Fabric impermeable liner provided due to proximity uctures or groundwater contamination?	Choose One — O YES O NO
6. Inlet / Out	tlet Control	Choose One Sheet Flow- No Energy Dissipation Required
A) Inlet C	Control	Concentrated Flow- Energy Dissipation Provided
7. Vegetatio	in	Choose One Seed (Plan for frequent weed control) Plantings Sand Grown or Other High Infiltration Sod
		Sand Grown or Ottler High Inhitiation 300
8. Irrigation		Choose One
		O YES
A) Will th	e rain garden be irrigated?	● NO
Notes:		

DETENTION VOLUME BY THE FULL SPECTRUM METHOD

Project: The Ridge @ Cumbre Vista Filing 1

Basin ID: Attenuate runoff from Basins B, C, & F

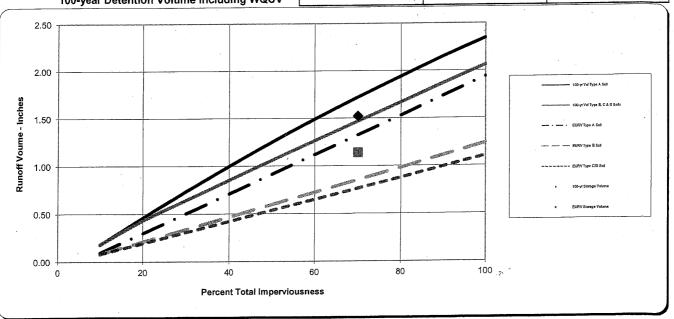


Recommended	Horton's Equation Para	ameters for CUHP
	ches per hour)	Decay
Initial f_i	Finalfo	Coefficientα
4.755	0.8	0.0012

Detention Vo	lumes -	NA CONTRACTOR A Manualada
(watershed inches)	(acre-feet)	Maximum Allowable Release Rate, cfs ³
1.14	1.30	Design Oulet to Empty EURV in 72 Hours
1.52	1.74	9.21

Excess Urban Runoff Volume⁴

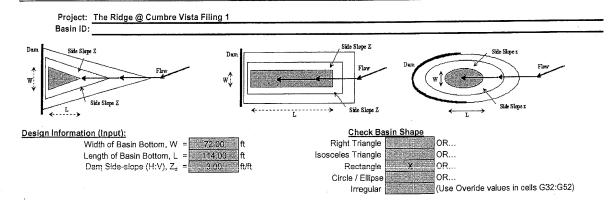
100-year Detention Volume Including WQCV 5



Notes:

- 1) Effective imperviousness is based on Figure ND-1 of the Urban Storm Drainage Criteria Manual (USDCM).
- 2) Results shown reflect runoff reduction from Level 1 or 2 MDCIA and are plotted at the watershed's total imperviousness value; the impact of MDCIA is reflected by the results being below the curves.
- 3) Maximum allowable release rates for 100-year event are based on Table SO-1. Outlet for the Excess Urban Runoff Volume (EURV) to be designed to empty out the EURV in 72 hours. Outlet design is similar to one for the WQCV outlet of an extended detention basin (i.e., perforated plate with a micro-pool) and extends to top of EURV water surface elevation.
- 4) EURV approximates the difference between developed and pre-developed runoff volume.
- 5) 100-yr detention volume includes EURV. No need to add more volume for WQCV or EURV

STAGE-STORAGE SIZING FOR DETENTION BASINS



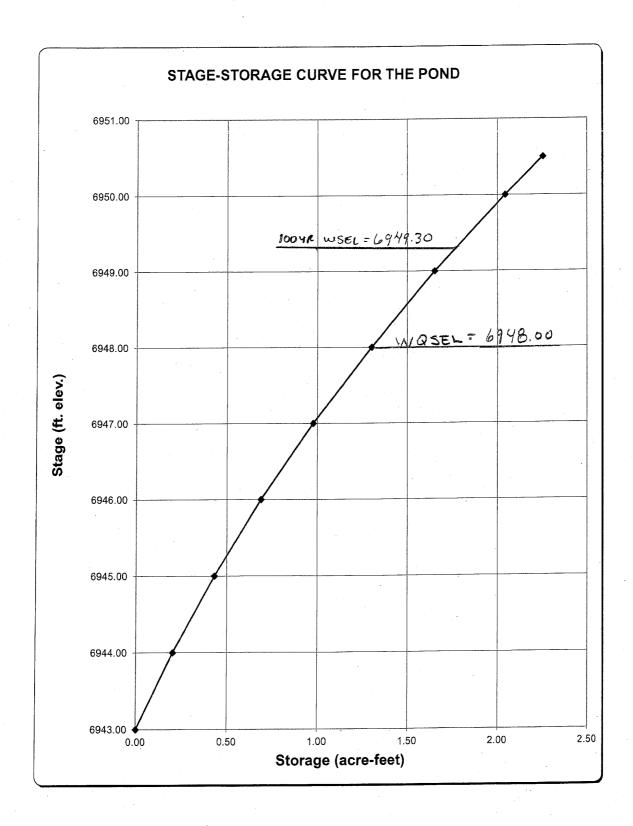
Stage-Storage Relationship:

	MINOR	MAJUK	
Storage Requirement from Sheet 'Modified FAA':			acre-ft.
Storage Requirement from Sheet 'Hydrograph':			acre-ft.
Storage Requirement from Sheet 'Full-Spectrum':	1.30	1 74	acre-ft.

	1		· - ·			1 . 0 . 6	I Malana	Surface	Volume	Target Volume
Labels	Water	Side	Basin	Basin	Surface	Surface	Volume		Below	for WQCV, Mine
for WQCV, Minor,	Surface	Slope	Width at	Length at	Area at	Area at	Below	Area at	į.	& Major Storag
& Major Storage	Elevation	(H:V)	Stage	Stage	Stage	Stage	Stage	Stage	Stage	Volumes
Stages	ft	ft/ft	ft	ft	ft ²	ft ² User	ft ³	acres	acre-ft	The second secon
(input)	(input)	Below El.	(output)	(output)	(output)	Overide	(output)	(output)	(output)	(for goal seek
6943	6943.00	(input)	72.00	114.00	8,208.0			0.188	0.000	
	6944.00	3,00	78.00	120.00	9,360.0		8,784	0.215	0.202	
	6945.00	3.00	84.00	126.00	10,584.0		18,756	0.243	0.431	
	6946.00	3.00	90.00	132.00	11,880.0		29,988	0.273	0.688	
	6947.00	3.00	96.00	138.00	13,248.0		42,552	0.304	0.977	
	6948.00	3.00	102.00	144.00	14,688.0		56,520	0.337	1.298	
	6949.00	3.00	108.00	150.00	16,200.0		71,964	0.372	1.652	•
	6950.00	3.00	114.00	156.00	17,784.0		88,956	0.408	2.042	
	6950.50	3.00	117.00	159.00	18,603.0		98,053	0.427	2.251	
	0000.00	0,00					#N/A		#N/A	
							#N/A		#N/A	
							#N/A	***************************************	#N/A	
							#N/A		#N/A	—
			***************************************	***************************************			#N/A	······	#N/A	
·							#N/A		#N/A	
				· · · · · · · · · · · · · · · · · · ·		-	L.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		#N/A	
					·		#N/A		······································	
							#N/A		#N/A	
			-				#N/A		#N/A	
							#N/A		#N/A	
			·				#N/A	.,	#N/A	
				-			#N/A		#N/A	
				4			#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
					***************************************		#N/A		#N/A	
	i i						······		#N/A	
							#N/A			
							#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
-							#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
							#N/A		#N/A	
									#N/A	
							#N/A		#IN/A	l

STAGE-STORAGE SIZING FOR DETENTION BASINS

Project: THE RIDGE AT CUMBRE VISTA FZLING No. Basin ID:



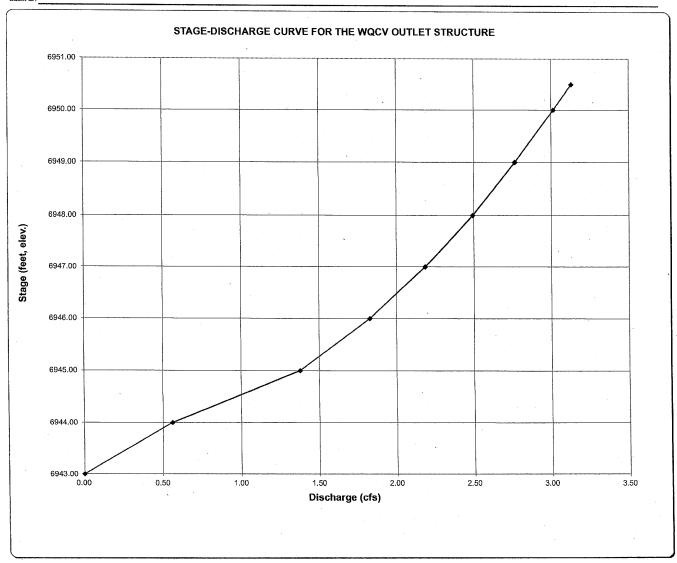
STAGE-DISCHARGE SIZING OF THE WATER QUALITY CAPTURE VOLUME (WQCV) OUTLET

Project: The Ridge @ Cumbre Vista			
Basin ID:			
WQCV Design Volume (Input): Catchment Imperviousness, I _a = 66.5 percent Diameter of Catchment Area, A = 1870, acres Number of holes p	f holes, D = in. er row, N = OR	Time to Drain the Pond = 72 hour	\$
Vertical distance between rows, h = 4.00 inches Number of rows, NL = 3 Height	of slot, H = 2.00 in. of slot, W = 5.61 in.		Perforated Plate Examples
Excess Urban Runoff Volume (From 'Full-Spectr Outlet area pe Total opening area at each row based on user-input a Total opening area at each row based on user-input a	r row, Ao = 2.53 square inches		4"

ft 89 iput) 43.00 o	Row 1 1943.33	Row 2	Row 3	Row 4	Row 5																				
iput) 43.00 o	943.33			11011	TOW J	Row 6	Row 7	Row 8	Row 9	Row 10	Row 11	Row 12	Row 13	Row 14	Row 15	Row 16	Row 17	Row 18	Row 19	Row 20	Row 21	Row 22	Row 23	Row 23	Σ
43.00 O		6943.66	6944.00			Ĺ	<u> </u>	<u> </u>															i		Flow
		·	·····			.	,	·			Collection C	apacity for	Each Row o	f Holes in cl	fs										
THEOREM (0.0000	0.0000	0.0000			<u> </u>				<u> </u>	į	<u> </u>				<u> </u>									0,00
	0.3267	0,2328	0.0000				<u> </u>	<u> </u>	<u></u>		<u> </u>	L													0.56
	0.5159	0.4621	0.3992			<u>.</u>	ļ	Į			<u> </u>														1.38
	0.6523	0.6106	0.5645					<u> </u>	L		l	l	-			I							ĺ		1.83
	0.7647	0.7295	0,6914		<u> </u>						1														2,19
	0.8626	0.8316	0.7984	<u> </u>			1																[2.49
	0.9505	0.9225	0.8926	<u> </u>			<u> </u>											1							2.77
	1.0310	1.0051	0.9778													1	1	l				1	Î	ì	3,01
50.50 1	1.0689	1.0440	1.0177	İ								I						<u> </u>					İ		3,13
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Project: The Ridge @ Cumbre Vista

Basin ID:

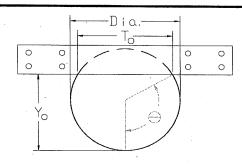


RESTRICTOR PLATE SIZING FOR CIRCULAR VERTICAL ORIFICES

Project: The Ridge @ Cumbre Vista Filing 1

Basin ID:

Х



Sizing the Restrictor Plate for Circular Vertical Orifices or Pipes (Input)

Water Surface Elevation at Design Depth Pipe/Vertical Orifice Entrance Invert Elevation Required Peak Flow through Orifice at Design Depth Pipe/Vertical Orifice Diameter (inches)

Orifice Coefficient

Full-flow Capacity (Calculated)

Full-flow area Half Central Angle in Radians Full-flow capacity

Calculation of Orifice Flow Condition

Half Central Angle (0<Theta<3.1416)

Flow area

Top width of Orifice (inches)

Height from Invert of Orifice to Bottom of Plate (feet)

Elevation of Bottom of Plate

Resultant Peak Flow Through Orifice at Design Depth

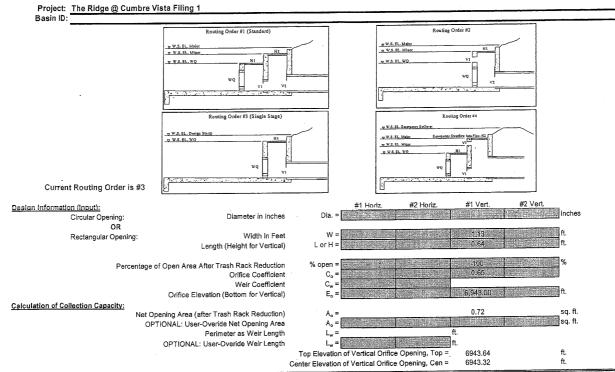
Width of Equivalent Rectangular Vertical Orifice Centroid Elevation of Equivalent Rectangular Vertical Orifice

	#1 Vertical	#2 Vertical	
	Orifice	Orifice	
Elev: WS =	6,949.30		feet
Elev: Invert =	6,943.00		feet
Q =	9.20		cfs
Dia =	18.0		inches
C _o =	0.65		
	<u> </u>		•

. Af =	1.77	***************************************	sq ft
Theta =	3.14		rad
Qf =	21.7		cfs
Percent of Design Flow =			en en en en en en en en en en en en en e

Theta =	1.43	rad
$A_o =$	0.72	sq ft
T _o =	17.81	inches
$Y_0 =$	0.64	feet
Elev Plate Bottom Edge =	6,943.64	feet
$Q_0 =$	9.2	cfs

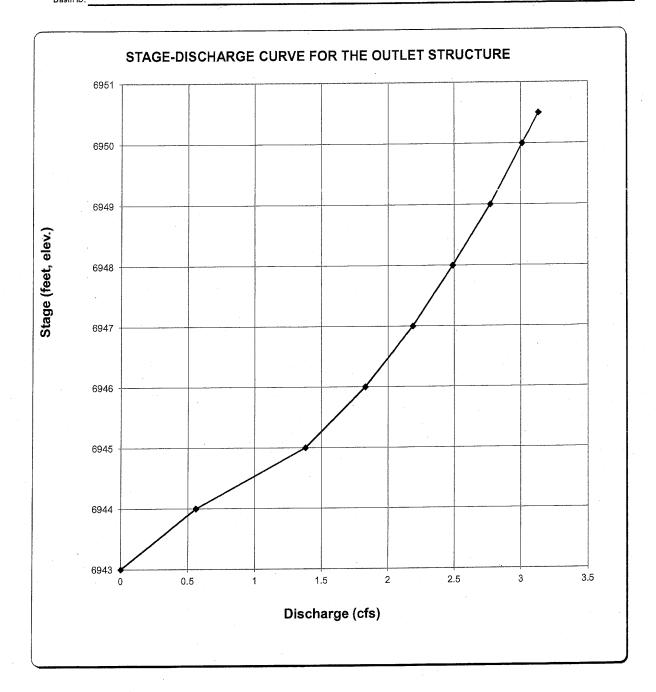
Equivalent Width =	1.13	feet
Equiv. Centroid El. =	6,943.32	feet



Routing 3: Single Stage - Water flows through WQCV plate and #1 horizontal opening into #1 vertical opening. This flow will be applied to culvert sheet (#2 vertical & horizontal openings is not used).

			Horizontal Orific	es			Vertical Orifices			
Labels	Water	WQCV	#1 Horiz.	#1 Horiz.	#2 Horiz.	#2 Horiz.	#1 Vert.	#2 Vert.	Total	Target Volume
for WQCV, Minor,	Surface	Plate/Riser	Weir	Orifice	Weir	Orifice	Collection	Collection	Collection	for WQCV, Min
& Major Storage	Elevation	Flow	Flow	Flow	Flow'	Flow	Capacity	Capacity	Capacity	& Major Stora
W.S. Elevations	ft	cfs	cfs	cfs	cfs	cfs	cfs	cfs	cfs	Volumes
(input)	(linked)	(User-linked)	(output)	(output)	(output)	(output)	(output)	(output)	(output)	(link for goal se
(11)(2,01)	6943.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
	6944.00	0.56	0.00	0.00	0.00	0.00	3.11	0.00	0.56	
	6945.00	1.38	0.00	0.00	0.00	0.00	4.89	0.00	1.38	
	6946.00	1.83	0.00	0.00	0.00	0.00	6.18	0.00	1.83	
	6947.00	2.19	0.00	0.00	0.00	0.00	7.24	0.00	2.19	
	6948.00	2,49	0.00	0.00	0.00	0.00	8.16	0.00	2.49	
	6949.00	2.77	0.00	0.00	0.00	0.00	8.99	0.00	2.77	
	6950.00	3.01	0.00	0.00	0.00	0.00	9.75	0.00	3.01	
		3.13	0.00	0.00	0.00	0.00	10.11	0.00	3.13	
	6950.50		·····	#N/A	#N/A	#N/A	#N/A	0.00	#N/A	
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Project: The Ridge @ Cumbre Vista Filing 1
Basin ID:

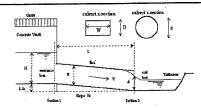


### STAGE-DISCHARGE SIZING OF THE OUTLET CULVERT (INLET vs. OUTLET CONTROL WITH TAILWATER EFFECTS)

Project: The Ridge @ Cumbre Vista Filing 1

Basin ID:

Status: Culvert Data is valid!



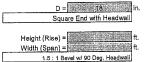
#### Design Information (Input):

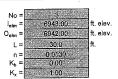
Circular Culvert: Barrel Diameter in Inches
Circular Culvert: Inlet Edge Type (choose from pull-down list)
OR:

Box Culvert: Barrel Height (Rise) in Feet Box Culvert: Barrel Width (Span) in Feet

Box Culvert: Inlet Edge Type (choose from pull-down list)

Number of Barrels
Inlet Elevation at Culvert Invert
Outlet Elevation at Culvert Invert
Culvert Length in Feet
Manning's Roughness
Bend Loss Coefficient
Exit Loss Coefficient





#### Design Information (calculated):

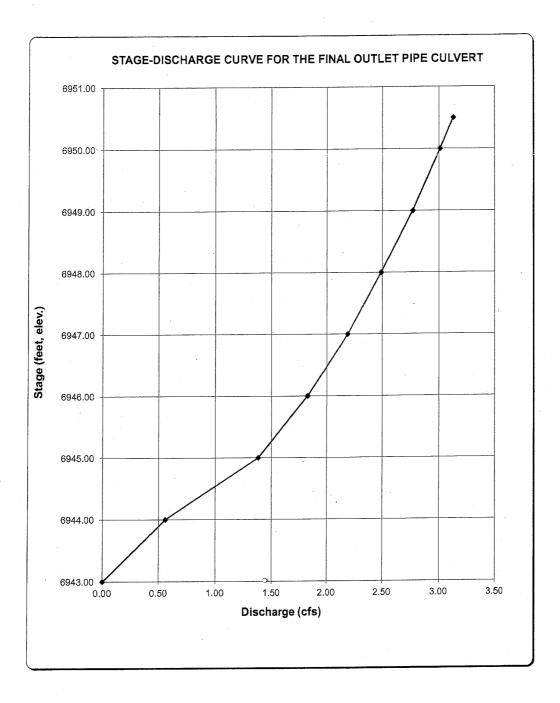
Entrance Loss Coefficient
Friction Loss Coefficient
Sum of All Loss Coefficients
Orifice Inlet Condition Coefficient
Minimum Energy Condition Coefficient

K. =	0.50
K _f =	0.54
K _s =	2.04
Cd=	0.86
low =	-0.09

Calculations of Culvert Capacity (output):

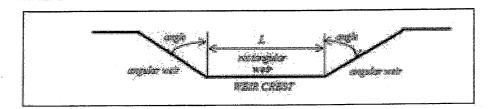
	Water Surface	Tallwater	Culvert	Culvert	Flowrate	Controlling	Inlet
	Elevation	Surface	Inlet-Control	Outlet-Control	Into Cuivert	Culvert	Equation
	From Sheet	Elevation	Flowrate	Flowrate	From Sheet	Flowrate	Used
	"Basin"	ft	cfs	cfs	"Outlet"	cfs	
	(ft., linked)	(input if known)	(output)	(output)	(cfs, linked)	(output)	(output)
	6943.00	6942.00	0.00	0.00	0.00	0.00	No Flow (WS < inlet)
	6944.00	0.00	10.20	21.29	0.56	0.56	Regression Eqn.
	6945.00	0.00	27.00	29.92	1.38	1.38	Regression Eqn.
	6946.00	0.00	38.10	38.84	1.83	1.83	Regression Eqn.
	6947.00	0.00	46.50	45.74	2.19	2.19	Regression Egn.
	6948.00	0.00	53.40	51.78	2.49	2.49	Orifice Eqn.
	6949.00	0.00	59.40	57.25	2.77	2.77	Orifice Eqn.
	6950.00	0.00	64.80	62.43	3.01	3.01	Orifice Eqn.
	6950.50	0.00	67.50	. 64.73	3.13	3,13	Orifice Eqn.
	0.00	0,00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS ≤ inlet)
	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
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İ	0.00	0.00	. 0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
ı	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
- 1	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
	. 0.00	0.00	0.00	0.00	#N/A	+ #N/A	No Flow (WS < inlet)
ı	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
.	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
	0.00	0:00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
ı	0.00	0.00	0.00	0.00	. #N/A	#N/A	No Flow (WS < inlet)
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ı	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
ı	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
ı	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
ı	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
ŀ	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
ŀ	0.00	D:00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
ŀ	0.00	0,00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
ŀ	0.00	0:00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
ŀ	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
1	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)
ŀ	0.00	0.00	0.00	0.00	#N/A	#N/A	No Flow (WS < inlet)

Project: The Ridge @ Cumbre Vista Filing 1
Basin ID:



'roject: The Ridge @ Cumbre Vista

asin ID:



# Information (input):

Bottom Length of Weir Angle of Side Slope Weir Elev. for Weir Crest Coef. for Rectangular Weir Coef. for Trapezoidal Weir

	10.00	feet
Angle =	71.57	degrees
EL_Crest =	6.950.00	feet
C _w =		
<b>C</b> , =	3.10	· 例

# Degree

# tion of Spillway Capacity (output):

Water	Rect	Triangle	Total	Total
Surface	Weir	Weir	Spillway	Pond
Elevation	Flowrate	Flowrate	Release	Release
	c is	ΘŚ	cis	cfs
(linked)	(ou <b>tputi</b> e	(dipul)	s 40utput)	(output)
6943.00	0.00	0.00	0.00	0.00
6944.00	0.00	0,00	0.00	0.56
6945.00	0.00	0.00	0.00	1.38
6946.00	0.00	0.00	0.00	1.83
6947.00	0.00	0.00	0.00	2.19
6948.00	0.00	0.00	0.00	2.49
6949.00	0.00	0.00	0.00	2.77
6950.00	0.00	0.00	0.00	3.01
6951.00	0.00	9.30	9.30	12.54
#N/A	#IWA	#N/A	#N/A	#N/A
#N/A	#N/A	#N/A	#N/A	#NA
#N/A	#N/A	#N/A	#N/A	₩WA
#N/A	#N/A	#N/A	#WA	#N/A
#N/A	#N/A	#N/A	#N/A	#NA
#N/A	#N/A	#N/A	#N/A	#N/A
#N/A	#M/A	#N/A	#N/A	#NA
#N/A	#N/A	#N/A	#N/A	#1/4
#N/A	#N/A	#N/A	#NA	#N/A

# fs: STAGE-DISCHARGE SIZING OF THE SPILLWAY Project: The Ridge @ Cumbre Vista Basin ID: Update Graph STAGE-STORAGE-DISCHARGE CURVES FOR THE POND Storage (Acre-Feet) 3 2.5 1.5 7 0.5 ator 6952 -6951 6950 6949 6948 6947 6946 6945 6944 10 12 2 6 4 Pond Discharge (cfs) 70%0 GT0A.KG TOTAL DISCULPAN

# EXISTING DRAINAGE MAP HISTORIC DRAINAGE MAP PROPOSED DRAINAGE MAP

# AMENDMENT NO. 1 TO THE FINAL DRAINAGE REPORT FOR CUMBRE VISTA FILING NO. 1

## AND

# PRELIMINARY/FINAL DRAINAGE REPORT **FOR**



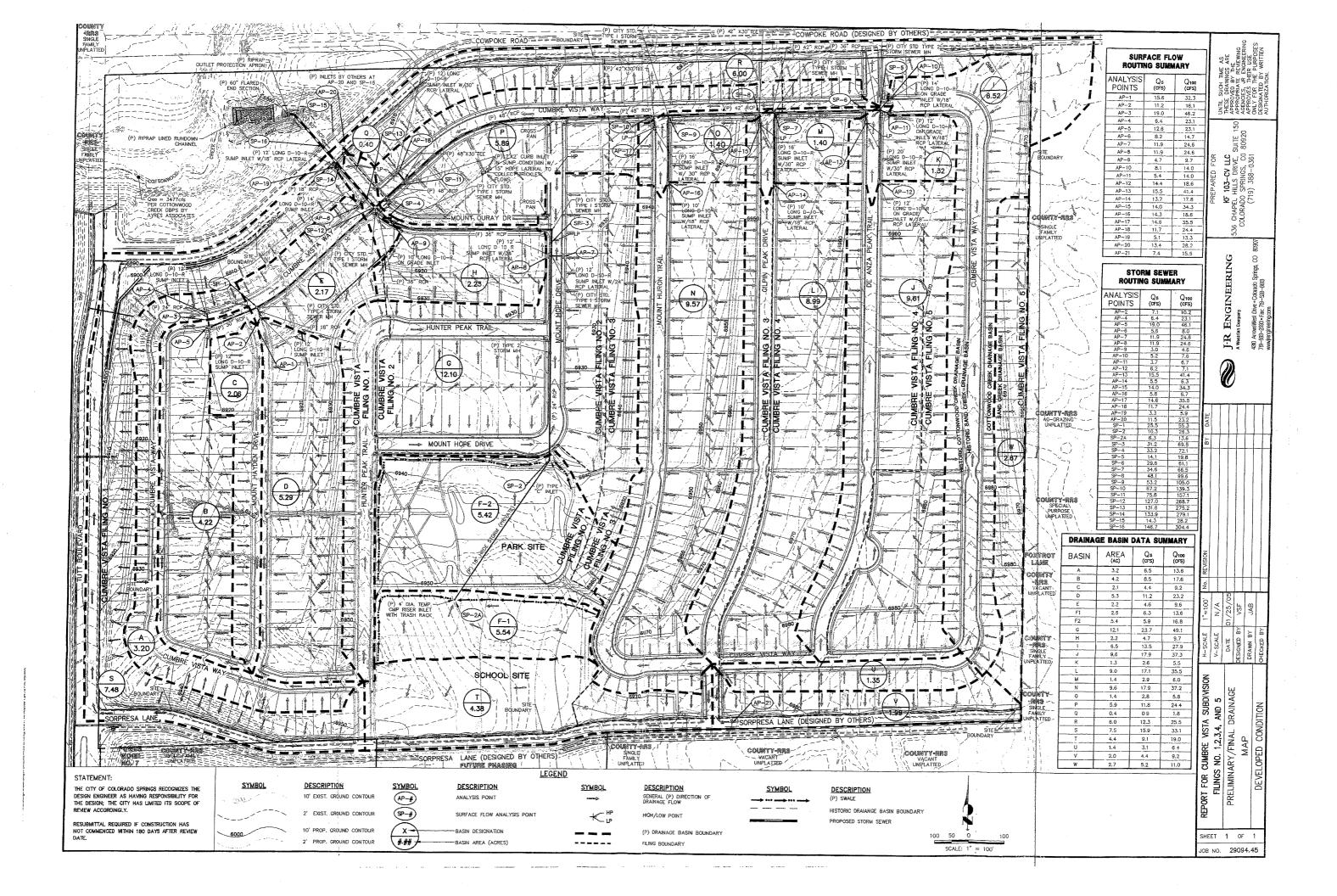


### DRAINAGE REPORT STATEMENT

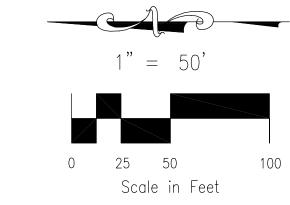
# ENGINEER'S STATEMENT: The attached drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors, or omissions on my part in preparing Vancel S. Fossinger, Colorado P.E. #31972 For and On Behalf of JR Engineering DEVELOPER'S STATEMENT: I, the developer, have read and will comply with all of the requirements specified in this drainage report and plan. Business Name: By: ard Gonzalez Manager Title: 536 Chapel Hills Drive, Suite 150 Address: Colorado Springs, CO 80920 CITY OF COLORADO SPRINGS ONLY: Filed in accordance with Section 7.7.906 of the Code of the City of Colorado Springs, 2001, as amended. City Engineer Date

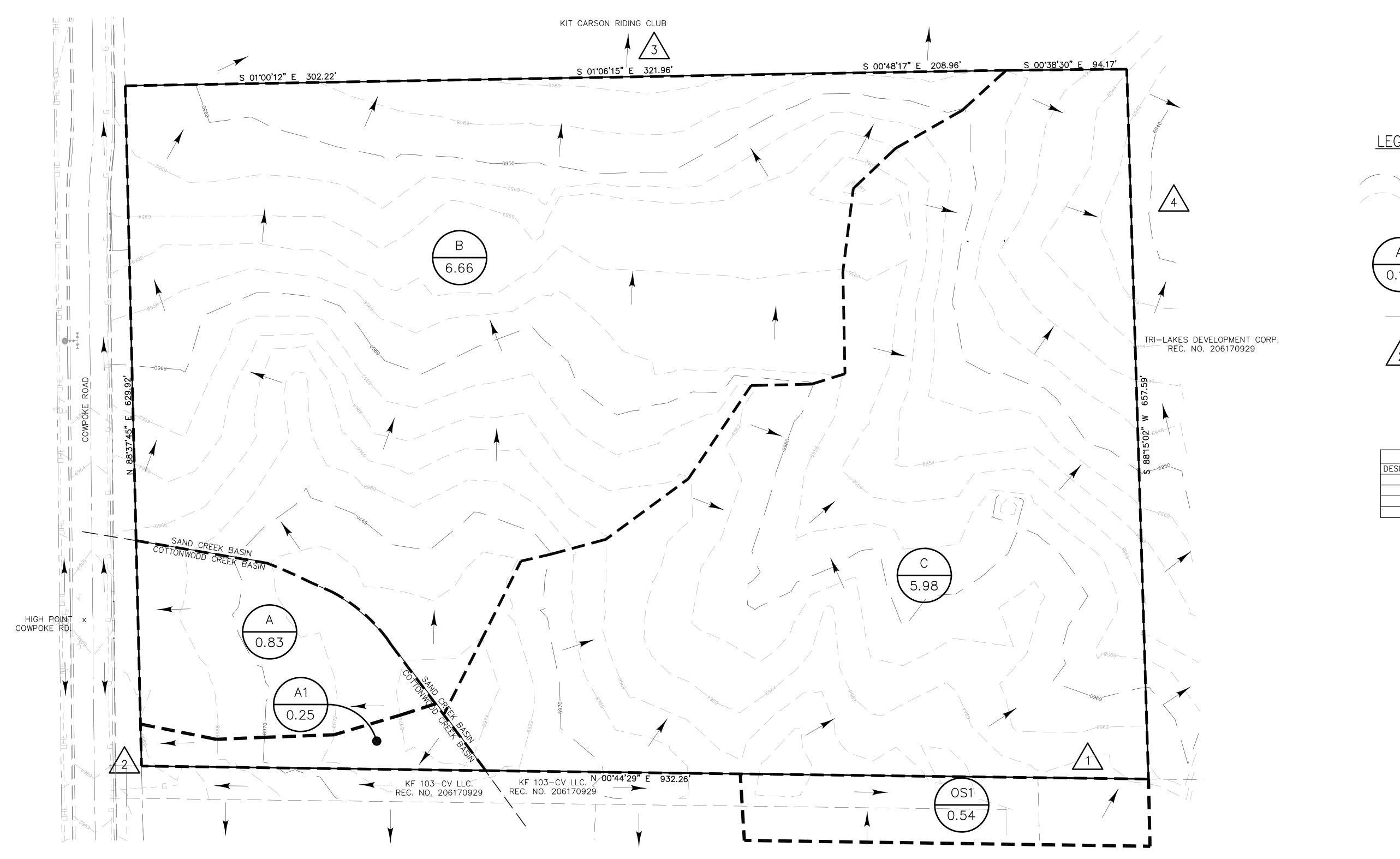
City Engineer

Conditions:



# THE RIDGE AT CUMBRE VISTA FILING NO. 1 HISTORIC DRAINAGE FLOWS

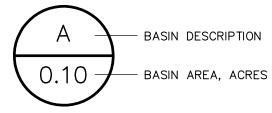








EX MAJ CONT EX MIN CONT





SURFACE ROUTING POINT

DESIG	N POINT	TABLE
DESIGN PT.	FLOW Q5	FLOW Q100
1	0.5	1.2
2	0.9	2.2
3	4.4	11.0
4	4.4	11.0

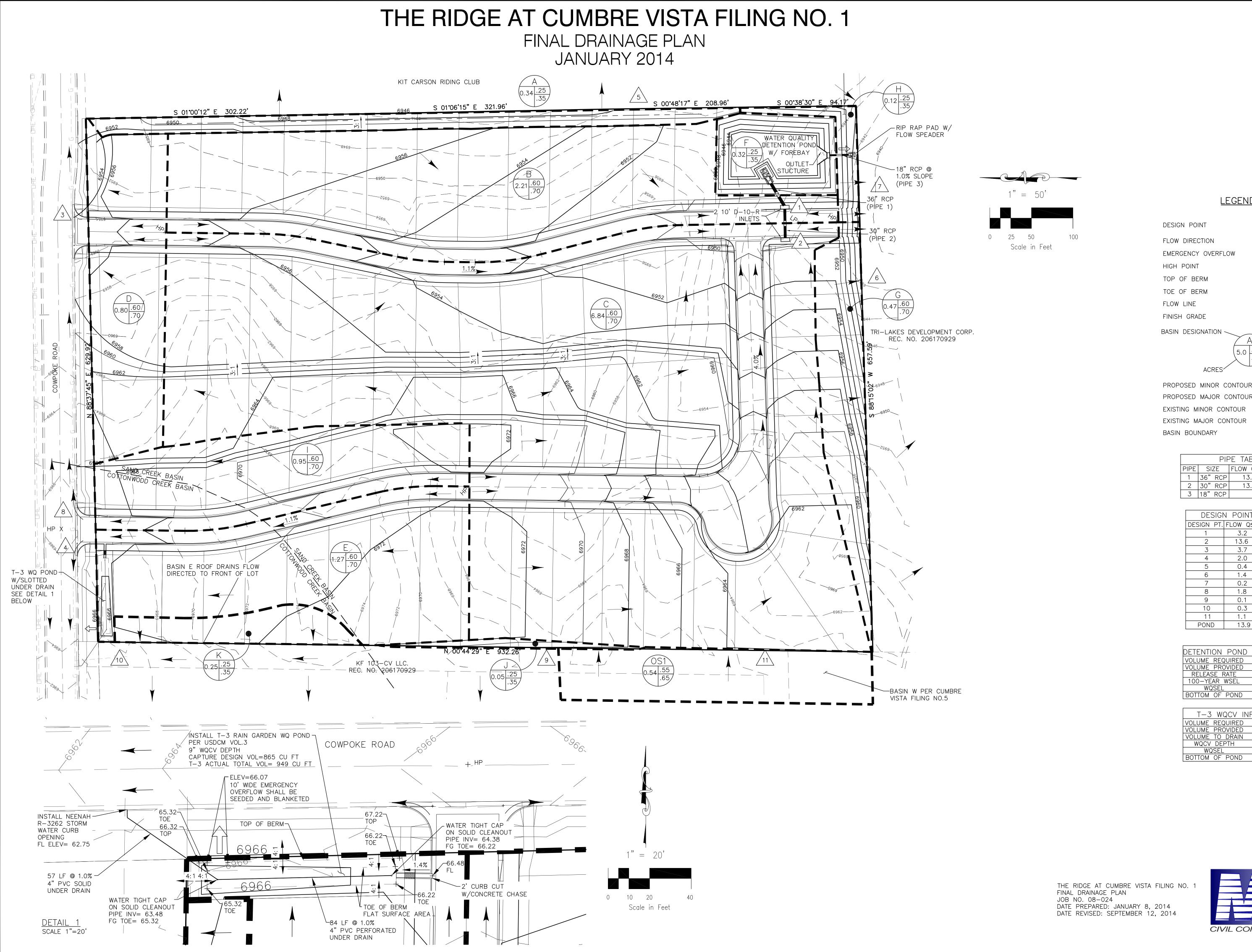
THE RIDGE AT CUMBRE VISTA FILING NO. 1
HISTORIC DRAINAGE PLAN
JOB NO. 08-024
DATE PREPARED: JANUARY 8, 2014
DATE REVISED: SEPTEMBER 4, 2014



102 E. PIKES PEAK AVE., STE 306 COLORADO SPRINGS, COLORADO 80903

> v 719.235.5249 f 719. 444.8427

SHEET 1 OF 1



<u>LEGEND</u>

DESIGN POINT FLOW DIRECTION EMERGENCY OVERFLOW HIGH POINT TOP OF BERM TOE OF BERM FLOW LINE FINISH GRADE BASIN DESIGNATION

PROPOSED MINOR CONTOU EXISTING MINOR CONTOUR EXISTING MAJOR CONTOUR BASIN BOUNDARY

PIPE TABLE						
PIPE	SI	ZE	FLOW	Q50	FLOW	Q100
1	36"	RCP	13	5.7	2	8.5
2	30"	RCP	13	5.6	2	8.3
3	18"	RCP			9	.2

DE	DESIGN POINT			TABLE	- -
DESIGN	PT.	FLOW	Q5	FLOW	Q100
1		3.:	2	6.	9
2		13.	6	28.	.3
3		3.	7	7.	8
4		2.	0	4.	1
5		0.	4	1.	1
6		1.4	4	3.	0
7		0	2	0.	4
8		1.8	3	3.	8
9		0.	1	2.:	2
10	)	0	3	0.	7
1	1	1.	1	2.:	2
PON	1D	13.9		29	0.0

DETENTION POND	INFORMATI
VOLUME REQUIRED	1.74 ACF7
VOLUME PROVIDED	2.25 ACF
RELEASE RATE	9.21 CFS
100-YEAR WSEL	6949.30
WQSEL	6948.00
l	

T-3 WQCV II	NFORMATION
VOLUME REQUIRED	865 CU. FT
VOLUME PROVIDED	949 CU. FT
VOLUME TO DRAIN	12 HOUR
WQCV DEPTH	9 INCHES
WQSEL	6966.07
BOTTOM OF POND	6965.32



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SHEET 1 OF 1