

Master Development Drainage Plan
Sentinel Ridge at the
Garden of the Gods Club
Colorado Springs, Colorado

Master Development Drainage Plan
Sentinel Ridge at the
Garden of the Gods Club

Colorado Springs, Colorado

Prepared For:

Sunshine Company
3310 Mesa Road Suite 150
Colorado Springs, Colorado 80904

Prepared By:

Kiowa Engineering Corporation
1604 South 21st Street
Colorado Springs, Colorado 80904

January 2008
Revised September 2008
Revised October 1, 2008
Project No. 07028

ENGINEER'S STATEMENT:

The attached drainage plan and report was prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors and omissions on my part in preparing this report.

Kiowa Engineering Corporation, 1604 South 21st Street, Colorado Springs, CO 80904


Richard N. Wray
Registered Engineer #19510

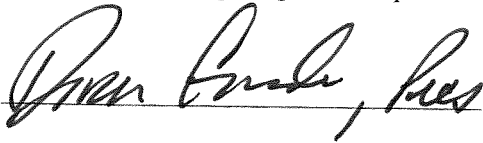
Date

10/1/08

OWNER'S STATEMENT:

The Owner and/or his representative has read and will comply with all of the requirements specified in this drainage report and plan.

BY:

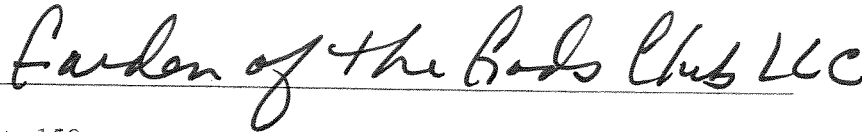


Date

10/4/08

ADDRESS:

~~Sunshine Company~~



3310 Mesa Road Suite 150

Colorado Springs, CO 80904

CITY OF COLORADO SPRINGS

Filed in accordance with Section 7.7.906 of the Code of the City of Colorado Springs, 2001, as amended.



City Engineer

Dated

10/10/08

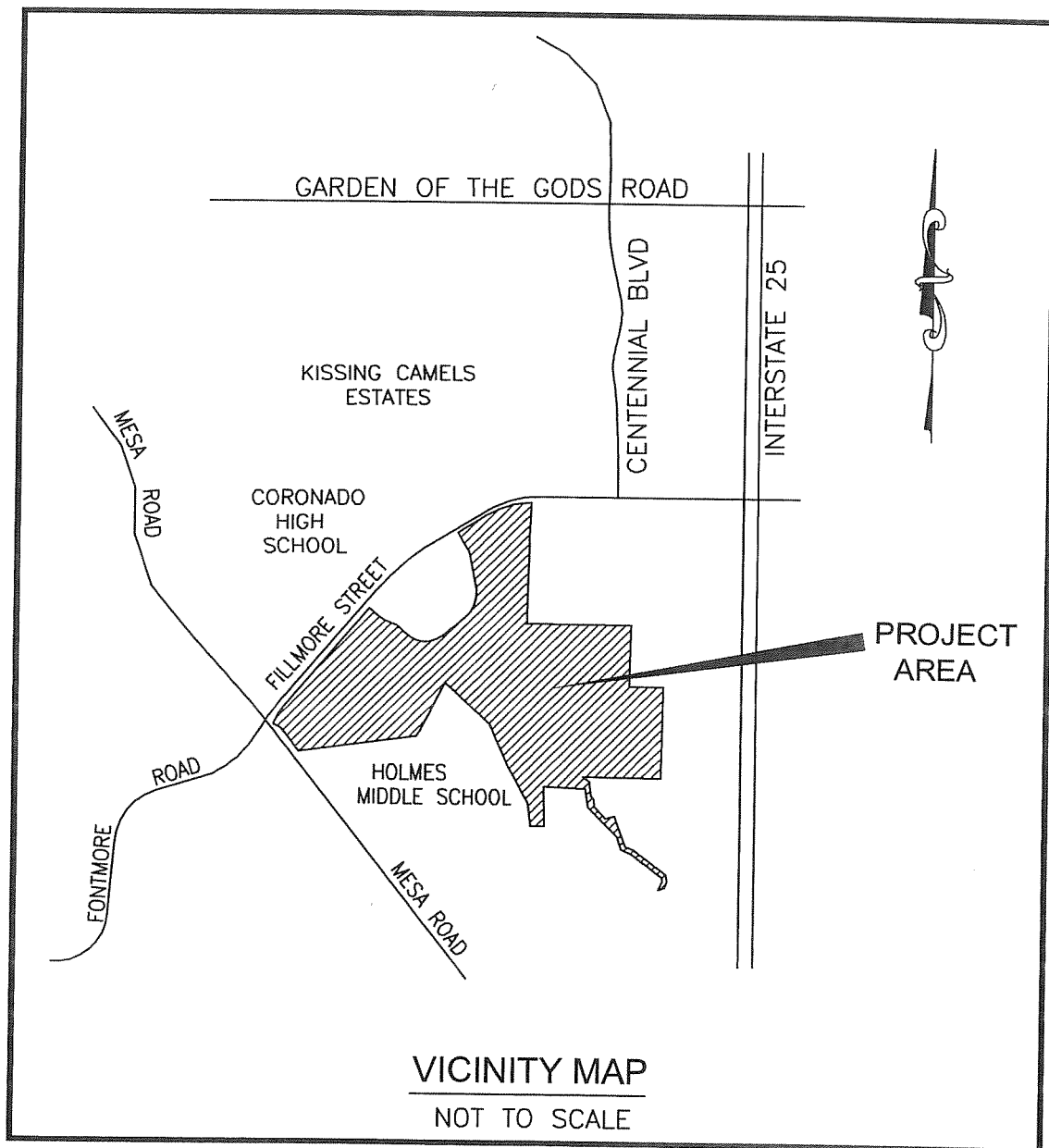
PROJECT DESCRIPTION

The Sentinel Ridge at Garden of the Gods Club will be a varying density residential development located south of West Fillmore Street and west of Centennial Boulevard west-central Colorado Springs. The land encompassed by the Sentinel Ridge project as formerly contained within the ownership of Hill Development. The property will be broken into individual filings as phased development occurs. The overall property subject to this master development drainage plan covers 137 acres. Sentinel Ridge West at the Garden of the Gods Club Filing No. 1 will be the first phase, and covers approximately 40 acres. A separate final drainage report will be prepared for Filing No. 1 and submitted concurrently with this master development drainage plan.

The property is located within portions of Sections 35 and 36 Township 13 South Range 67 West of the 6th Principal Meridian, in Colorado Springs, Colorado. The property is bounded on the south, southwest and east by undeveloped land that is owned by School District 11, privately held parcels and by the City of Colorado Springs and on the northwest by Fillmore Street. The estimated total of the developable land within Sentinel Ridge is 90 acres. The location of the site is shown on Figure 1.

The site lies within the Mesa Drainage basin. The site is drained by two forks of the Mesa Basin Drainageway the flow in generally a southerly direction. The two branches have been termed the as East Fork Mesa Basin and the West Fork Mesa Basin in this master development drainage plan (MDDP). Both of these drainageways are relatively steep with longitudinal gradients ranging from 3 to 5 percent. The East Fork is unimproved with only one stream crossing within the limits of the project. The West Fork is mostly unimproved except at the outfall point from the site where the drainageway enters an existing detention basin.

Soils within the property are classified to be within Hydrologic Soils Group A as shown in the El Paso County Soils Survey. A very small portion of the project area has Hydrologic soils classified as D. The type D soils occur mostly of the slopes of the terraces and mesas. The soils are classified as Ascalon sand and Chaseville sandy gravels. These soils are very well drained and have relatively low runoff curve numbers (i.e., 50 to 60) depending upon vegetative cover and condition. The existing vegetative cover within the area subject to development is in good condition on the mesa areas and poor to fair on the side slopes of the mesas. The mesas and side slopes are vegetated with mostly native grasses and shrubs. There are areas of wetland habitat within the property that occur mainly along the East and West forks of the Mesa Basin drainageway.



Kiowa Engineering Corporation

1604 South 21st Street
 Colorado Springs, Colorado
 80904-4208
 (719) 630-7342

SENTINEL RIDGE
 COLORADO SPRINGS, COLORADO
 FIGURE 1

PROJECT NO.: 07028
 DATE: 12/26/07
 DESIGN: RNW
 REVISIONS:

PREVIOUS REPORTS

The following reports and plans were reviewed in the process of preparing this master development drainage plan:

1. Soil Survey for El Paso County, Colorado, dated June 1981.
2. "City of Colorado Springs/El Paso County Drainage Criteria Manual", prepared by City of Colorado Springs, El Paso County, dated May 1987, revised 1996.
3. "Flood Insurance Studies for Colorado Springs, and El Paso County, Colorado", prepared by the Federal Emergency Management Agency (FEMA), revised March, 1997.
4. Mesa Drainage Basin Drainage Basin Planning Study, prepared GMS, Inc., dated September 1989.
5. Master Development Drainage Plan for Hill Properties, prepared by Rockwell-Minchow Consultants, Inc. dated October 1995.
6. Preliminary and Final Drainage Report for Grand Vista Filing No. 1, prepared by Rockwell-Minchow Consultants, Inc. dated December 1995.
7. Final Design Report and Final Design Plans, Mesa Drainage Basin Detention Basin 5A and 5B, prepared by Kiowa Engineering, Inc. dated March 2000.

Reference 5 was prepared for the City of Colorado Springs and has been used in the planning of major drainageway facilities within the basin since the time that it was approved. This DBPS identified drainageway improvements and detention storage sites within entire basin, several of which were shown within the Hill Development property, and two within the limits of Sentinel Ridge. All of the detention basins in the DBPS that were shown north of West Fillmore have been built as the Hill Development holdings have been developed. The DBPS called for a detention basin on the West Fork located at design point 14 of this MDDP. Design point 14 coincides with design point 26 of the DBPS. This detention basin was built in 2001. On the East Fork, Detention basin 5B was proposed in the DBPS. Detention basin 5B was built in 1999. Downstream of Fillmore along the East Fork five off-stream detention basins and 1 on-stream detention basin were proposed that would lie within Sentinel Ridge. None of the detention basins on the East Fork downstream of Fillmore Street have been constructed at this time. The East Fork drainageway was proposed in the DBPS to remain in its natural condition. Selective areas of bank lining were shown in the DBPS in order to maintain the lateral stability of the West Fork, however none of the locations shown in the DBPS lie within Sentinel Ridge. No major roadway crossings were shown in the DBPS within the Sentinel Ridge property.

Reference 5 was prepared for Hill Development and covers the entire property that was owned by Hill Development, including Sentinel Ridge. This MDDP was used as a supplement to Reference 4, and identified alternative detention storage sites. Two of the regional detention sites north of Fillmore Street, namely detention basins 5A and 5B were constructed in order to achieve the hydrologic goals put forth in Reference 4. Reference 5 was also prepared in order to address changes in the land use patterns from those assumed when Reference 4 was prepared and to assess the affects of development upon the hydrology and in turn the major drainageways of the Mesa Basin drainage basin.

Reference 6 was completed when the multi-family development project known as Grand Vista was advanced through the development planning process. The detention basin noted as detention basin 14 in this report was designed and built as part of the Grand Vista project. Detention basin 14 is owned and operated by the City of Colorado Springs and designed to accommodate the developed runoff from Grand Vista as well as area offsite from Grand Vista that included the Sentinel Ridge property.

Reference 7 was prepared in order to supplement the analyses contained within References 4 and 5 and to provide the hydrologic and hydraulic information needed to design detention basin 5A and 5B. These detention basins are owned and operated by the owner of the Garden of the Gods Club and provides regional storage of developed runoff and water quality volume for the portion of Mesa Basin that were then part of the Hill Development holdings. As part of the development of the Grandview Marketplace that lies east of detention basin 5B and north of West Fillmore Street, a water quality grate and trash rack were added to the outlet structure of detention basin 5B. The hydrology model was updated in order to revise the storage and outflow curve so that the water quality storage aspect of the detention basin was accounted for.

EXISTING BASIN CONDITIONS

Contained within map pocket of this report is Exhibit 1 that displays the hydrologic sub-basins and peak discharges for all the sub-basins and design points within Sentinel Ridge. Sub-basin and design points were developed in this MDDP to coincide with the sub-basins and design points depicted in the DBPS so that hydrologic comparisons could be made. Offsite design points and sub-basins are also presented on Exhibit 1. The 100-year floodplain for the East and West forks are presented on Exhibit 1.

Five sub-basins were delineated within Sentinel Ridge in order to assess the existing hydrologic conditions. Fours sub-basins were delineated that are tributary to the

East Fork (i.e., sub-basins M17.1, M17.2, M18.1 and M18.2), and one sub-basin delineated for the West Fork, (sub-basin M14). Each of these sub-basins can be characterized as watersheds that have terraces with slopes varying from one to five percent, and slopes off of the terraces ranging from 10 to 30 percent. Per the soil survey, the side slopes of the terraces have soils classified in the Hydrologic Soil class D, and the terraces themselves have soils classified into Hydrologic soils class A. Both the East and the West forks of the Mesa Basin drainageway are unimproved except for an outfall structure that was built with detention basin 14 on the West Fork, and a utility crossing over the East Fork at design point 18.1.

Presented on Table 1 is a comparison of the peak discharges for the existing development condition between this MMDP and the DBPS. The variance in the discharges between the DBPS and the MDDP are mostly attributable differences in methodology, basin divides, land use assumptions and whether or not detention storage was modeled. A good correlation in discharge between the DBPS and the MDDP was obtained at the inflow point to detention basin 5B. All of the other points of comparison do not show any strong correlations. The existing condition discharges obtained for this MDDP and Reference 6 correlate closely at each of the West Fork design points on Fillmore Street.

PROPOSED BASIN DESCRIPTIONS

Two major flow paths with five sub-basins on the East Fork and three sub-basins on the West Fork were defined in order to estimate runoff rates for the proposed development condition. The sub-basins and design points for the proposed conditions are displayed on Exhibit 2 that is contained within the map pocket of this report. The 100-year floodplain for the East and West forks are presented on Exhibit 1. A description of each sub-basin follows.

Sub-basin M14A: This sub-basin is comprised mostly of the natural drainageways and valley with a small portion of single-family development proposed for about ten percent of the total sub-basin area. The sub-basin covers 20.2 acres. Contained within this sub-basin is existing detention basin 14 that was built with the Grand Vista apartment project was developed. The drainageways through this sub-basin are both unimproved but stable as they outfall to detention basin 14. Within the DBPS pipe outfalls were called for to carry runoff arriving at design points 10 and 13 (DBPS design points 20 and 25, respectively) to the existing detention basin at design point 14. Due to the wetland resources along these drainageways it was decided to not outfall the runoff

**Table 1: Comparison of DBPS and MDDP Design Point Discharges
Sentinel Ridge at Garden of the Gods Club Master Development Drainage Plan**

DBPS DP NO.	Discharge (4)		EQUIV. MDDP DP NO.	Discharge (4)	
	5 year	100-year		5 year	100-year
20	75	136	10	20	68
25	10	19	13	30	155
26 (3)	93	302	14	54	245
9 (1)	212	647	5B	176	729
12 (2)	193	375	18.1	111	261

Notes:

- (1) Inflow to detention basin 5B
- (2) DBPS discharges do not reflect storage in detention basin 5B
- (3) DBPS discharges do not reflect storage in detention basins within Kissing Camels Golf course
- (4) 24-hour duration Type IIA storm

from design points 10 and 13 via a storm sewer in favor of utilizing the natural swales described above. Soils in this basin are mostly Type A, with Type D soils occurring on slopes of the terraces. Surface soils in the areas that will be subject to grading were assumed to be Type B. The development will occur on the terraces, and will consist of single-family residential homes accessed by public streets. Three local storm sewers will pass into this sub-basin and outfall to the West Fork Mesa Basin channel. The 5-year and 100-year discharges for this sub-basin are estimated at 1 and 11 cubic feet per second, respectively.

Sub-basin M14C: This sub-basin will be comprised mostly of single-family development proposed for the majority of the area but a small neighborhood park is proposed near design point 14.1. This sub-basin covers 13.9 acres. This sub-basin will be drained to inlets within a low point at design point 13.1 and then to a storm sewer that will convey the 100-year discharge to the West Fork Mesa Basin downstream of design point 13.2. Soils in this sub-basin are mostly Type A, but were assumed to be Type B in the developed condition. Slopes in this sub-basin are expected to range from 2 to 4 percent. Offsite runoff enters the basin at design point 13 via a 48-inch storm sewer that conveys runoff from areas west of Fillmore Street. The 5-year and 100-year discharges for this sub-basin are estimated at 7 and 31 cubic feet per second, respectively.

Sub-basin M14D: This sub-basin will be comprised mostly of single-family development. This sub-basin covers 7.9 acres. This sub-basin will be drained to inlets within a low point at design point 14.1 then to a storm sewer that will convey the 100-year discharge to the West Fork Mesa Basin downstream of design point 14.2. Soils in this sub-basin are mostly Type A, but were assumed to be Type B in the developed condition. Slopes in this sub-basin are expected to range from 2 to 4 percent. Offsite runoff enters the basin at design point 14.1 via a 36-inch storm sewer that conveys runoff from areas west of Fillmore Street as well as the runoff from the Grand Vista apartment complex. The 5-year and 100-year discharges for this sub-basin are estimated at 6 and 19 cubic feet per second, respectively.

Sub-basin M17A: This sub-basin will be comprised mostly of the natural terrace slopes that cover a third of the basin with the balance of the area being developed into office and commercial uses. The majority of this sub-basin does not lie within Sentinel Ridge but will outfall to the East Fork Mesa Basin at design point 17.1 that does lie within Sentinel Ridge. It has been assumed that this sub-basin will discharge to the East

Fork at fully developed condition rates of runoff. The sub-basin covers 24.7 acres. Soils in this basin are comprised of Type D soils occurring on slopes of the terraces and Type B soils for the area that will be subject to grading. The development will occur on the terrace and will consist of office/commercial uses. The 5-year and 100-year discharges for this sub-basin are estimated at 40 and 91 cubic feet per second, respectively.

Sub-basin M17B: This sub-basin will be comprised mostly of the natural terrace slopes that cover almost two-thirds of the basin with the balance of the area being developed into office and commercial uses. It has been assumed that this sub-basin will discharge to the East Fork at fully developed condition rates of runoff carried to the drainageway by a storm sewer. Offsite runoff from areas west of Fillmore Street will enter this sub-basin at design point 5B via the 36-inch outlet pipe from detention basin 5B. The East Fork drainageway through this sub-basin is unimproved but stable. Wetland vegetation exists along the drainageway. The sub-basin covers 19.5 acres. Soils in this basin are comprised of Type D soils occurring on slopes of the terraces and Type B soils for the area that will be subject to grading. The development that will occur on the terrace has been assumed to consist of office/commercial uses. The 5-year and 100-year discharges for this sub-basin are estimated at 24 and 64 cubic feet per second, respectively.

Sub-basin M18A: This sub-basin will be comprised mostly of the natural terrace slopes that cover most of the sub-basin with a very small portion area being developed into office or commercial uses. Approximately one-third of the sub-basin is comprised of area that is offsite from Sentinel Ridge and will outfall to the East Fork Mesa Basin at design point 18.1. The East Fork drainageway through this sub-basin is unimproved but stable. Wetland vegetation exists along the drainageway. It has been assumed that this sub-basin will discharge to the East Fork at fully developed condition rates of runoff. The sub-basin covers 22.7 acres. Soils in this basin are comprised of Type D soils occurring on slopes of the terraces and Type B soils for the area that will be subject to grading.

Sub-basin M18B: This sub-basin will be comprised mostly of the natural and graded terrace slopes that cover most of the sub-basin. A public roadway is proposed to cross through this sub-basin. The embankment of this roadway will form the impoundment for detention basin 18.1. This sub-basin will be drained via public streets to inlets within at the low point located at design point 18.1. At the low point a storm

sewer will convey the 100-year discharge to detention basin 18.1. The sub-basin covers 13.2 acres. Soils in this basin are comprised of Type D soils occurring on slopes of the terraces and Type B soils for the area that will be subject to grading. The 5-year and 100-year discharges for this sub-basin are estimated at 1 and 12 cubic feet per second, respectively.

Sub-basin M18C: This sub-basin will be comprised mostly of single-family development proposed for the majority of the area. This sub-basin covers 20.1 acres. This sub-basin will be drained via public streets to inlets within at the terminus of the cul-de-sac shown on Exhibit 2. At this point a storm sewer will convey the 100-year discharge to the East Fork Mesa Basin upstream of design point 18.2. It has been assumed that this sub-basin will discharge to the East Fork at fully developed condition rates of runoff. The impact of the development within this sub-basin upon peak discharges will be addressed by over-detaining the developed runoff that reaches design point 18.1, so that the 100-year existing rate of runoff at design point 18.2 can be maintained at 279 cubic feet per second. Soils in this sub-basin are mostly Type A, but were assumed to be Type B in the developed condition. Slopes in this sub-basin are expected to range from 2 to 4 percent. The 5-year and 100-year discharges for this sub-basin are estimated at 18 and 53 cubic feet per second, respectively.

Sub-basin M18D: This sub-basin will be comprised mostly of the natural terrace slopes that cover most of the sub-basin with approximately one-fourth of the sub-basin being developed with single-family homes. The East Fork drainageway through this sub-basin is unimproved but stable. Wetland vegetation exists along the drainageway. It has been assumed that this sub-basin will discharge to the East Fork at fully developed condition rates of runoff. The impact of the development within this sub-basin upon peak discharges will be addressed by over-detaining the developed runoff that reaches design point 18.1, so that the 100-year existing rate of runoff at design point 18.2 can be maintained at 279 cubic feet per second. The sub-basin covers 24.7 acres. Soils in this basin are comprised of Type D soils occurring on slopes of the terraces and Type B soils for the area that will be subject to grading. The 5-year and 100-year discharges for this sub-basin are estimated at 28 and 78 cubic feet per second, respectively.

HYDROLOGY

The onsite hydrology for the site was estimated using the methods outlined in the City/County Storm Drainage Criteria Manual. Topographic mapping was prepared in

June 2007. The mapping was compiled from a field survey at a one-foot contour interval and a horizontal scale of 100-feet. The mapping was used to verify the onsite and offsite sub-basin boundaries. The evaluation of offsite runoff that reaches the site was conducted using field review and FIMS mapping.

The hydrologic analysis for the sub-basins contained within the Sentinel Ridge property was completed using the U. S. Army Corps of Engineers HEC-1 Flood Hydrograph Program. This method was used to estimate peak discharges for the 5- and 100-year frequencies for the existing and proposed development conditions. The peak flow data and volumes generated using HEC-1 were used to size storm sewers within the project subdivision, evaluate major drainageway improvements for the East and West forks, to verify the capacity of detention basin 14, and to size detention storage for the area tributary to the East Fork. The drainage basin area, time of concentration, and rainfall intensity were determined for each of the sub-basins within the property. Because of the small acreages associated some of the sub-basin a ten-minute minimum time of concentration was applied to the sub-basins that were less than 5 acres in size. For the estimation of runoff, curve numbers as supplied in Table 5-5 of the DCM were used in the hydrograph model. Presented on Exhibits 1 and 2 is the existing and proposed condition sub-basin boundaries and peak discharges for the various sub-basins and design points within and adjacent to Sentinel Ridge. Peak discharges for each sub-basin and design points are presented in the calculations contained within Appendix.

HYDRAULICS AND PROPOSED FACILITIES

The evaluation related to the sizing of the onsite drainage improvements were carried out in accordance with the City/County Storm Drainage Criteria Manual. The capacities of the proposed onsite facilities were calculated in accordance with the Criteria Manual. The developed portions of the site will be drained primarily via sheet flow into the public streets. Once the street capacity has been reached, inlets will be provided that will collect the surface runoff and convey it to storm sewer. All inlets and storm sewers should be sized to collect and convey the 100-year runoff, thus minimizing the potential for overflow onto terrace slopes. The size, type and locations of the proposed stormwater collection facilities are presented on Exhibit 3.

The East and West Fork major drainageways are proposed to remain in their present location and cross-section. Geotechnical concerns regarding slope stability issues related to the terraces above the drainageways requires that minimal disturbance be affected at the toe of the terrace slopes. Also it is necessary to prevent the invert of the major drainageways from degrading and dropping in elevation. It has therefore been

proposed to construct check structures at the general locations shown on the plan and profiles. It is further recommended that the checks be constructed from soil cement so that they can withstand overtopping in a major event. Finally, soil/riprap bank linings should be constructed at outside bends of each drainageway where the stability of the terrace slope above could be comprised by bank sloughing. The location of the selective bank lining has been shown on the plan and profiles, along with typical bank and check sections.

Stormwater detention needs to be implemented within the Sentinel Ridge site so that peak rates of runoff can be maintained at present levels. Due to the clustering of the development activities on the top of the terraces there are limited locations to implement stormwater detention basins. There is also a geotechnical concern regarding the storage of stormwater on the terraces as it relates to slope stability. On the West Fork, detention basin 14 functions to limit discharges from the developed areas to historic conditions. Hydrologic modeling of detention basin 14 confirmed that the present embankment and outlet structure is sufficient to detain and route the runoff collected from the area downstream of Fillmore Street, including Sentinel Ridge and discharge the runoff to the West Fork at historic conditions.

On the East Fork a stormwater detention basin is proposed upstream of design point 18.1. At this point along the drainageway a roadway crossing is proposed. It is recommended that the roadway's embankment be engineered so as to function as stormwater impoundment as well. A phased outlet structure is proposed to limit the discharge from the detention basin to below historic conditions thereby over-detain so that the development downstream of design point 18.1 can be discharged directly to the East Fork without causing the rates of runoff at design point 18.2 to exceed historic levels. An on-stream detention basin was proposed in the DBPS near this location. The detention storage areas shown in the DBPS on the terrace slopes are not recommended due to slope stability and construction issues. An emergency spillway needs to be provided in order to prevent the roadway from being overtopped should the principal outlet become blocked. The location of this detention basin is shown on Exhibit 3 and on the plan and profiles.

The required improvements to the East Fork drainageway between design points 17.1 and 17.2 are to be provided by the owner of the underlying property at the time of development. It is envisioned that selective banks linings and grade control will be needed similar in nature to those proposed for the East Fork in this MDDP.

The East Fork below design point 18.2 is currently and will remain under the ownerships and maintenance of the City of Colorado Springs. It will function as a

natural drainageway in order to preserve the wetland, riparian and flood plain habitat that exists along this reach of the East Fork. In the future selective bank lining and grade control may be needed to stabilize the invert and banks, but at this time the drainageway is generally stable.

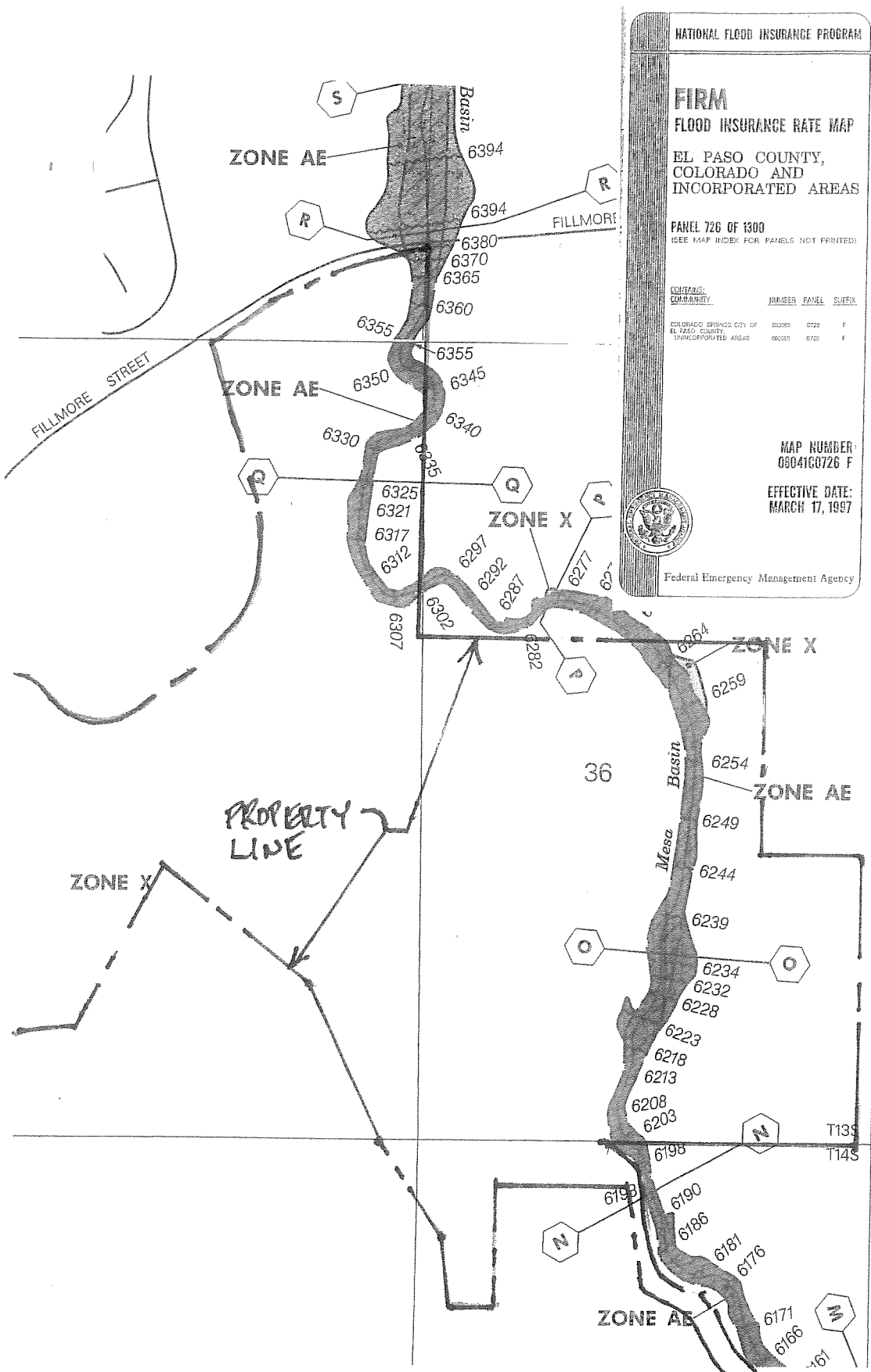
The West Fork below design point 14 is currently and will remain under the ownerships and maintenance of the City of Colorado Springs. It will function as a natural drainageway in order to preserve the wetland, riparian and flood plain habitat that exists along this reach of the West Fork. As part of the Sentinel Ridge project it is proposed to provide a grade control structure and selective bank lining at the outlet side of the existing detention basin at design point 14. These improvements are needed to stabilize the invert and banks in this location that are currently being affected by erosion. Below this point selective bank lining and grade control may be needed to stabilize the invert and banks, but at this time the drainageway is generally stable.

FLOODPLAIN STATEMENT

Shown on Figure 2 is the City of Colorado Springs and El Paso County Flood Insurance Study FIRM panel that covers the area encompassed by the Sentinel Ridge project site. There are areas within the proposed site that lie within a delineated 100-year or 500-year floodplain. The floodplain for the West Fork as depicted in the most current version of the City of Colorado Springs flood insurance study, including map revisions, is shown on all of the exhibits contained within this MDDP. There are no habitable structures that currently or will be proposed to lie within the 100-year floodplain of the West Fork Mesa Basin drainageway. Should improvements to drainageway such as channel and invert linings, relocations to the flow path, or roadway crossing be proposed, a letter of map revision may have to be submitted to FEMA if changes to the base flood elevation of floodway limits are proposed.

DRAINAGE FEES

The site lies within the Mesa Basin Drainage Basin. Drainage and bridge and fees have been established for this basin. As such drainage and bridge fees will be due when platting of parcels within Sentinel Ridge occurs. The cost of construction of major drainageway improvements that were identified in the DBPS can be used to offset drainage fees.



NATIONAL FLOOD INSURANCE PROGRAM

FIRM
FLOOD INSURANCE RATE MAP


EL PASO COUNTY,
COLORADO AND
INCORPORATED AREAS

PANEL 726 OF 1300
(SEE MAP INDEX FOR PANELS NOT PRINTED)

CONTAINS:	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS CITY OF	03000	0720	F
EL PASO COUNTY, UNINCORPORATED AREAS	08000	0720	F

MAP NUMBER:
08041G0726 F

EFFECTIVE DATE:
MARCH 17, 1997



Federal Emergency Management Agency

NATIONAL FLOOD INSURANCE PROGRAM

FIRM
FLOOD INSURANCE RATE MAP


EL PASO COUNTY,
COLORADO AND
INCORPORATED AREAS

PANEL 513 OF 1300
(SEE MAP INDEX FOR PANELS NOT PRINTED)

CONTAINS:	NUMBER	PANEL	SUFFIX
COLORADO SPRINGS CITY OF	05000	0513	F

MAP NUMBER:
08041G0513 F

EFFECTIVE DATE:
MARCH 17, 1997



Federal Emergency Management Agency

FIGURE 2
FLOODPLAIN INFORMATION

DRAINAGE FACILITY COSTS

Presented on Table 2 is a summary of the costs for the major drainageways, detention storage and local storm sewer systems shown on Exhibit 3. The improvements to the major drainageways and the regional detention storage would be subject to reimbursement or could be used as credit against drainage fees owed once approved and accepted by the City of Colorado Springs.

WATER QUALITY MEASURES

As required by the City in Volume 2 of the Drainage Criteria Manual, water quality measures need to be introduced in new developments in order to reduce the detrimental effects of impervious areas upon stormwater runoff. The water quality measures that will be instituted for the Sentinel Ridge project will be phased into interim and permanent facilities.

The existing detention basin at design point 14 was hydrological analyzed to check its ability to store the water quality capture volume generated by the portion of Sentinel Ridge that outfalls to it. It was found that the existing detention basin does have adequate volume to store the developed runoff and reduce it to historic conditions as well as store the required water quality capture volume from the tributary watershed.

The proposed detention basin at design point 18.1 has been sized to be able to store the water quality capture volume from the residential development within Sentinel Ridge that is tributary to it. Water quality capture volume will need to be provided for separately within the proposed commercial area shown on the Exhibits in sub-basin 17B. Water quality capture volume within sub-basin 17A will have to be provided for separately as well when the property within 17A that lies offsite from Sentinel Ridge develops.

Permanent and Interim water quality measures:

1. Within the areas proposed for residential development, it is recommend that the pervious area associated with each lot be disconnected from the street and storm sewer system. This can be achieved by directing roof leaders and runoff from driveways onto grassed areas.
2. Temporary sedimentation basins will be constructed at the outfall points of future subdivisions with the intent that they remain in place until all land disturbing activities tributary to the sediment basin reach final stabilization.
3. The check structures proposed for the West and East forks will slow the low flows along the drainageway and allow for percolation into the soil. This

Table 2: Summary of Storm Drainage Facility Costs
Sentinel Ridge at the Garden of the Gods Club Master Development Drainage Plan

Non-reimbursable storm sewer system costs

Item	Quantity	Units	Unit Cost	Estimated Cost
Storm Sewer Collection Systems				
4' Type 'R' Inlet	3	EA	\$ 3,000.00	\$ 9,000.00
6' Type 'R' Inlet	5	EA	\$ 3,500.00	\$ 17,500.00
8' Type 'R' Inlet	2	EA	\$ 4,000.00	\$ 8,000.00
10' Type 'R' Inlet	1	EA	\$ 5,000.00	\$ 5,000.00
Storm sewer manholes	2	EA	\$ 3,500.00	\$ 7,000.00
18" RCP CLIII	530	LF	\$ 42.00	\$ 22,260.00
24" RCP CL III	1,950	LF	\$ 54.00	\$ 105,300.00
			SUBTOTAL	\$ 174,060.00
			10% Engineering	\$ 17,406.00
			5% Contingency	\$ 8,703.00
			TOTAL	\$ 200,169.00

Reimbursable major drainageway and detention system costs

Item	Quantity	Units	Unit Cost	Estimated Cost
Storm Sewer Outfall Systems				
54" RCP CL III	520	LF	\$ 150.00	\$ 78,000.00
Junction structure	1	EA	\$ 15,000.00	\$ 15,000.00
Storm sewer outlet structure	1	EA	\$ 10,000.00	\$ 10,000.00
Detention Storage				
Storage pool and embankment construction	5	AF	\$ 15,000.00	\$ 75,000.00
Outlet Structure	1	EA	\$ 8,000.00	\$ 8,000.00
Outlet pipe: 48-inch RCP	160	LF	\$ 120.00	\$ 19,200.00
Storm sewer outlet structure	1	EA	\$ 8,000.00	\$ 8,000.00
Major Drainageway Structures				
Soil/riprap channel linings	1,390	LF	\$ 250.00	\$ 347,500.00
Soil cement check structures	12	EA	\$ 20,000.00	\$ 240,000.00
			SUBTOTAL	\$ 800,700.00
			10% Engineering	\$ 80,070.00
			5% Contingency	\$ 40,035.00
			TOTAL	\$ 920,805.00

combined with leaving the drainageway in the natural state will provide for treatment of urban stormwater that will be collected and conveyed by these drainageways.

4. Within the proposed commercial area shown in sub-basin M17B water quality capture can be provided prior to discharge to the storm sewer outfall system. Mechanical systems such as oil and grease separators and stormceptors, could be employed as well as surface retention. Retention of the water quality capture volume on the terraces will require that the receiving storage basin(s) be lined to prevent saturation of the soils beneath them.
5. Within outlying parking areas of the commercial site, porous pavement systems can be implemented to reduce the effective imperviousness of the site. As with the water quality storage areas, these pavement systems should be constructed with an under-drain system to prevent saturation of the soil beneath them.

EROSION CONTROL PLAN

The City of Colorado Springs and El Paso County Drainage Criteria Manual specifies that an Erosion Control Plan and associated cost estimate be submitted in conjunction with Final Drainage Report. It is requested on the behalf of the Owner that the Erosion Control Plan be submitted with the Final Construction Grading Plan upon which the cost for the erosion control will be shown. Assurances for the erosion control facilities will be posted as part of obtaining a grading permit.

CONCLUSIONS

The drainageway and detention storage facilities proposed in this MDDP will combine collect and convey runoff generated from the Sentinel Ridge development and the offsite areas that pass through it in a non-erosive manner and without out impact to the drainageways that lie downstream of the development. The major drainageway and storage facilities are in general conformance with those proposed in the DBPS.

The drainage improvements to the West Fork will be completed as Sentinel Ridge West at Garden of the Gods Club Filing No. 1 is developed. This includes the selective bank lining and grade control structure that lie downstream of the existing detention basin at design point 14.

The drainageway and detention facilities for the East Fork will be constructed as filings that are tributary to them are developed. Onsite storage could be implemented within the proposed commercial site that basin and thereby forego the need to construct the detention basin at design point 18.1. However the storage facility at design point 18.1

will need to be constructed prior to any development occurring within sub-basins M18C and M18D.

Any construction proposed that could affect the wetland areas delineated on the plans will need authorization from the U.S. Army Corps of Engineers. Contact will be made with the Corps as the final design plans for the drainageway improvements are prepared. A re-delineation for the wetland areas may be required if construction within these drainageways does not commence within five years.

APPENDIX A
HYDROLOGY CALCULATIONS

Hydrology - Future Conditions

Basin Data: West Face

Basin #	Area (Ac)	CN	Land Use
M14.1	19.2	85	Apts / multi Family
M14A	20.2	53	90% O/S; 10% SF Ma
M14B	4.1	71	7 SF Lots; 1.7 DU/A
M14C	8.6	69	18 SF lots; 2.1 DU/Ac
M14D	7.9	74	25 SF Lots; 3.2 DU/Ac

Soils assume all 'B'; ~~except~~ for open space where A will remain

CN FOR A-soil, undeveloped; 50

B. Soils

ROADWAY S: CN = 98

MULTI-FAMILY (> 3 lots/ac) CN = 85

COMMERCIAL = 92

Rv. 9/9/08

Hydrology - Future Conditions

Basin DATA: EAST Fork

Basin #	Area (Ac)	CN	Land Use
M17A	24.7	B9	2/3 Off/Comm; 1/3 Slopes
M17B	19.5 25.5	B1	1/3 Comm / 2/3 OS, slope
M18A	22.7	50	OS or Existing
M18B	13.2	60	80% OS; 20% Roads
M18C	20.1	78	SF + Roadways
M18D	24.7	B2	80% OS; 20% SF (CN=75) (at CN)

Assume all 'B' Soils, except for Open Spaces where 'A' Soils will remain.

CN = 50 for OS, terraced (Hyd. Soils A)
 CN = B2 for OS; slopes (Hyd. Soils D)

TABLE 5-5
RUNOFF CURVE NUMBERS FOR HYDROLOGIC SOIL
COVER COMPLEXES - URBAN AND SUBURBAN CONDITIONS 1/
(Antecedent Moisture Condition II)
 (From: U.S. Dept. of Agriculture,
 Soil Conservation Service, 1977)

<u>Land Use</u>	<u>Hydrologic Soil Group</u>			
	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>
Open spaces, lawns, parks, golf courses, cemeteries, etc.				
Good condition: grass cover on 75% or more of the area	39*	61	74	80
Fair condition: grass cover on 50% to 75% of the area	49*	69	79	84
Commercial and Business areas (85% Impervious)	89*	92	94	95
Industrial Districts 72% Impervious)	81*	88	91	93
Residential: <u>2/</u>				
<u>Acres per Dwelling Unit</u>	<u>Average %</u>			
	<u>Impervious</u>	<u>3/</u>		
1/8 acre or less	65	77*	85	90
1/4 acre	38	61*	75	83
1/3 acre	30	57*	72	81
1/2 acre	25	54*	70	80
1 acre	20	51*	68	79
Paved parking lots, roofs, driveways, etc.	98	98	98	98
Streets and Roads:				
paved with curbs and storm sewers	98	98	98	98
gravel	76*	85	89	91
dirt	72*	82	87	89

1/ For a more detailed description of agricultural land use curve numbers, refer to the National Engineering Handbook (U.S. Dept. of Agriculture, Soil Conservation Service, 1972).

2/ Curve numbers are computed assuming the runoff from the house and driveway is directed towards the street with a minimum of roof water directed to lawns where additional infiltration could occur.

3/ The remaining pervious areas (lawn) are considered to be in good pasture condition for these curve numbers.

* Not to be used wherever overlot grading or filling is to occur.

Time of Concentration / Lag Time $T_{lag} = .6 T_c$

<u>Basin #</u>	<u>Length</u>	<u>T_c^* (min)</u>	<u>T_{lag} (hr)</u>
M14A	1600	13.9	.139
M14B	—	10	.10
M14C	840	10.5	.105
M14D	2250	12.5	.125
M17A	(1)	—	.17
M17B	1600	13.9	.139
M18A	1820	15.1	.15
M18B	1720	14.6	.146
M18C	2450	18.6	.186
M18D	2250	12.5	.125

(1) Use existing runoff conditions.

* $T_c = 10$ min for all basins < 5 acres

$$T_c = \text{Length of Basin} / 100 \quad (3 \text{ for average travel time}) + 5$$

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* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
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* RUN DATE 28DEC07 TIME 10:55:05
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* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
1	ID	MESA DRAINAGE BASIN				PROJECT NUMBER	07028				
2	ID	SENTINEL RIDGE MASTER DEVELOPMENT DRAINAGE PLAN									
3	ID	WEST FORK BRANCH									
4	ID	EXISTING DEVELOPMENT CONDITIONS WITH EXISTING DETENTION BASINS									
5	ID	5 AND 100-YEAR STORMS 24-HOUR TYPE IIA									
6	ID	KIOWA ENGINEERING CORPORATION				FILENAME	WFSREX.DAT				
		*DIAGRAM									
7	IF	4	0	0	288						
8	IO	5									
9	JR	PREC	.56	1.0							
10	KK	SBM7									
11	KM	RUNOFF FROM SUB-BASIN M7									
12	IN	15									

WEST FORK EXISN036

13	PB	4.1									
14	PC	0.0	.0005	.0015	.0030	.0045	.0060	.0080	.0100	.0120	.0143
15	PC	.0165	.0189	.0210	.0233	.0255	.0278	.0320	.0390	.0460	.0530
16	PC	.0600	.0750	.1000	.4000	.7000	.7250	.7500	.7650	.7800	.7900
17	PC	.8000	.8100	.8200	.8250	.8300	.8350	.8400	.8450	.8500	.8550
18	PC	.8600	.8638	.8675	.8713	.8750	.8788	.8825	.8863	.8900	.8938
19	PC	.8975	.9013	.9050	.9083	.9115	.9148	.9180	.9210	.9240	.9270
20	PC	.9300	.9325	.9350	.9375	.9400	.9425	.9450	.9475	.9500	.9525
21	PC	.9550	.9575	.9600	.9625	.9650	.9675	.9700	.9725	.9750	.9775
22	PC	.9800	.9813	.9825	.9838	.9850	.9863	.9875	.9888	.9900	.9913
23	PC	.9963	.9975	.9988	1.0000						
24	BA	.0528									
25	LS	0	66								
26	UD	.27									
27	KK	RTM7									
28	KM	ROUTE RUNOFF FROM SUB-BASIN M7 TO DP 8									
29	RK	3000	.021	.03	0	TRAP	20	10			
30	KK	SBM8									
31	KM	RUNOFF FROM SUB-BASIN M8									
32	BA	.1243									
33	LS	0	66								
34	UD	.45									
35	KK	SBM11									
36	KM	RUNOFF FROM SUB-BASIN M11									
37	BA	.0467									
38	LS	0	71.6								
39	UD	.36									
40	KK	RTM11									
41	KM	ROUTE SUB-BASIN M11 TO DP 9									
42	RK	2600	.03	.03	0	TRAP	4	4			
43	KK	M9									
44	KM	RUNOFF FROM SUB-BASIN M9									
45	BA	.0844									
46	LS	0	69								
47	UD	.45									

1

HEC-1 INPUT

LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10.....
48	KK	DP9									
49	KM	COMBINE SMM9 AND RTM11									
50	HC	2									
51	KK	DB9									
52	KM	ROUTE FLOW FROM DP 9 THROUGH DETENTION BASIN DB 9									
53	RS	1	ELEV	6463							

54	SQ	0	16	37	45	158		
55	SA	0	.624	.701	.771	1		
56	SE	6463	6465	6467	6468	6468.5		
57	SS	6468	25	3	1.5			
58	ST	6468	200	3	1.5			
59	KK	RTDB9						
60	KM	ROUTE OUTFLOW FROM DB 9 TO DESIGN POINT 8						
61	RK	1800	.025	.03	0	TRAP	20	10
62	KK	DP8						
63	KM	COMBINE RTDB9, RTM7 AND SUB-BASIN M8						
64	HC	3						
65	KK	DB8						
66	KM	ROUTER RUNOFF AT DP 8 THROUGH DETENTION BASIN DB8						
67	RS	1	ELEV	6401.5				
68	SQ	0	8.5	15	20	220		
69	SA	2.12	2.35	2.73	3.25	3.5		
70	SE	6402	6404	6406	6408	6408.5		
71	SS	6406	25	3	1.5			
72	ST	6408	200	3	1.5			
73	KK	RTDB8						
74	KM	ROUTE OUTFLOW FROM DETENTION BASIN 8 TO DP 10						
75	RK	1300	.02	.013	0	CIRC	2.25	
76	KK	M10						
77	KM	RUNOFF FROM SUB-BASIN M10						
78	BA	.0512						
79	LS	0	77					
80	UD	.35						
81	KK	DP10						
82	KM	COMBINE RUNOFF FROM SUB-BASIN M10 AND RTDB8						
83	HC	2						
84	KK	RTDP10						
85	KM	ROUTE RUNOFF FROM DP 10 TO DP 14A						
86	RK	800	.05	.013	0	CIRC	3	
87	KK	M14.1						
88	KM	RUNOFF FROM SUB-BASIN M14.1						
89	BA	.012						
90	LS	0	95					
91	UD	.15						

1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

92 KK DP14.1

95	KM	COMBINE SUB-BASIN M14.1 AND RTDP10						
94	HC	2						
95	KK	RM14.1						
96	KM	ROUTE RUNOFF FROM DP 14.1 TO DP 14						
97	RK	800	.045	.04	0	TRAP	6	5
98	KK	M12						
99	KM	RUNOFF FROM SUB-BASIN M12						
100	EA	.114						
101	LS	0	70					
102	UD	.43						
103	KK	RTM12						
104	KM	ROUTE RUNOFF FROM SB M12 TO DP 13						
105	RK	1700	.024	.024	0	TRAP	3	1
106	KK	M13						
107	KM	RUNOFF FROM SUB-BASIN M13						
108	BA	.0949						
109	LS	0	67					
110	UD	.39						
111	KK	DP13						
112	KM	COMBINE RUNOFF FROM SB M13 AND RTM12						
113	HC	2						
114	KK	RTDP13						
115	KM	ROUTE RUNOFF AT DP 13 TO DP 14						
116	RK	1700	.029	.018	0	TRAP	8	1
117	KK	M14						
118	KM	RUNOFF FROM SB M14						
119	BA	.0503						
120	LS	0	50					
121	UD	.23						
122	KK	DP14						
123	KM	COMBINE RUNOFF FROM M14, RM14.1 AND RTDP13						
124	HC	3						
125	KK	DB14						
126	KM	ROUTE RUNOFF AT DP 14 THROUGH DETENTION BASIN DB 14						
127	RS	1	ELEV	6306				
128	SQ	0	24.5	73.4	100.8	122	141	157
129	SE	6306	6308	6310	6312	6314	6316	6318
130	SV	0	.18	.66	1.55	3.05	5.22	8.1
131	ZZ							

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT
LINE

(V) ROUTING

(--->) DIVERSION OR PUMP FLOW

NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
10	SEM7	
	V	
	V	
27	RTM7	
	.	
30	.	SEM8
	.	.
35	.	SEM11
	.	V
	.	V
40	.	RTM11
	.	.
	.	.
43	.	.
	.	M9
	.	.
48	.	DP9.....
	.	V
	.	V
51	.	DB9
	.	V
	.	V
59	.	RTDB9
	.	.
	.	.
62	DP8.....	.
	V	.
	V	.
65	DB8	.
	V	.
	V	.
73	RTDB8	.
	.	.
76	.	M10
	.	.
	.	.
81	DP10.....	.
	V	.
	V	.
84	RTDP10	.
	.	.
87	.	M14.1
	.	.
	.	.
92	DP14.1.....	.

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          V
          V
95      RM14.1
          .
          .
98      .      M12
          .      V
          .      V
103     .      RTM12
          .      .
          .      .
106     .      .      M13
          .      .      .
          .      .      .
111     .      DP13.....
          .      V
          .      V
114     .      RTDP13
          .      .
          .      .
117     .      .      M14
          .      .      .
          .      .      .
122     DP14.....
          V
          V
125     DB14

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(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

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*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
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* RUN DATE 28DECO7 TIME 10:55:05 *
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* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
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MESA DRAINAGE BASIN          PROJECT NUMBER 07028
SENTINEL RIDGE MASTER DEVELOPMENT DRAINAGE PLAN
WEST FORK BRANCH
EXISTING DEVELOPMENT CONDITIONS WITH EXISTING DETENTION BASINS
5 AND 100-YEAR STORMS 24-HOUR TYPE IIA
KIOWA ENGINEERING CORPORATION      FILENAME WFSREX.DAT

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8 IO      OUTPUT CONTROL VARIABLES
          IPRNT          5 PRINT CONTROL

```

IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 4 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 288 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 1 0 ENDING DATE
 NDTIME 1906 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .07 HOURS
 TOTAL TIME BASE 19.13 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .56 1.00

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	SBM7	.05	1	FLOW	6. 38.
				TIME	6.20 6.20
ROUTED TO					
+	RTM7	.05	1	FLOW	6. 38.
				TIME	6.47 6.27
HYDROGRAPH AT					
+	SBM8	.12	1	FLOW	9. 64.
				TIME	6.40 6.33
HYDROGRAPH AT					

+	SBM11	.05	1	FLOW TIME	9. 6.27	40. 6.27
ROUTED TO						
+	RTM11	.05	1	FLOW TIME	9. 6.40	39. 6.27
HYDROGRAPH AT						
+	M9	.08	1	FLOW TIME	10. 6.40	53. 6.33
2 COMBINED AT						
+	DP9	.13	1	FLOW TIME	19. 6.40	92. 6.33
ROUTED TO						
+	DB9	.13	1	FLOW TIME	13. 6.67	44. 6.73
** PEAK STAGES IN FEET **						
	1	STAGE		6464.63	6467.92	
		TIME		6.67	6.73	
ROUTED TO						
+	RTDB9	.13	1	FLOW TIME	13. 6.73	44. 6.80
3 COMBINED AT						
+	DP8	.31	1	FLOW TIME	26. 6.53	128. 6.33
ROUTED TO						
+	DB8	.31	1	FLOW TIME	4. 8.73	16. 9.00
** PEAK STAGES IN FEET **						
	1	STAGE		6402.97	6406.58	
		TIME		8.73	9.00	
ROUTED TO						
+	RTDB8	.31	1	FLOW TIME	4. 8.73	16. 9.00
HYDROGRAPH AT						
+	M10	.05	1	FLOW TIME	17. 6.27	59. 6.20
2 COMBINED AT						
+	DP10	.36	1	FLOW TIME	17. 6.27	61. 6.20
ROUTED TO						

+		RTDP10	.36	1	FLOW TIME	17. 6.27	61. 6.27
	HYDROGRAPH AT						
+		M14.1	.01	1	FLOW TIME	18. 6.00	36. 6.00
	2 COMBINED AT						
+		DP14.1	.37	1	FLOW TIME	28. 6.07	82. 6.13
	ROUTED TO						
+		RM14.1	.37	1	FLOW TIME	28. 6.13	81. 6.13
	HYDROGRAPH AT						
+		M12	.11	1	FLOW TIME	16. 6.40	79. 6.33
	ROUTED TO						
+		RTM12	.11	1	FLOW TIME	16. 6.40	78. 6.33
	HYDROGRAPH AT						
+		M13	.09	1	FLOW TIME	9. 6.33	58. 6.27
	2 COMBINED AT						
+		DP13	.21	1	FLOW TIME	25. 6.40	135. 6.33
	ROUTED TO						
+		RTDP13	.21	1	FLOW TIME	24. 6.40	135. 6.33
	HYDROGRAPH AT						
+		M14	.05	1	FLOW TIME	0. 19.07	8. 6.20
	3 COMBINED AT						
+		DP14	.63	1	FLOW TIME	44. 6.33	210. 6.27
	ROUTED TO						
+		DB14	.63	1	FLOW TIME	42. 6.47	130. 6.60

** PEAK STAGES IN FEET **
 1 STAGE 6308.71 6314.81
 TIME 6.47 6.60

*** NORMAL END OF HEC-1 ***

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* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
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* RUN DATE 08SEP08 TIME 11:50:25
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* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 755-1104
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X X XXXXXXX XXXXX XXXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DE, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION. NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	MESA DRAINAGE BASIN									
2	ID	SENTINEL RIDGE MASTER DEVELOPMENT DRAINAGE PLAN									
3	ID	WEST FORK BRANCH									
4	ID	24-HOUR TYPE IIA RAINFALL DISTRIBUTION									
5	ID	FUTURE DEVELOPMENT CONDITIONS WITH EXISTING DETENTION AT DP 14									
6	ID	5 AND 100-YEAR STORMS 24HOUR TYPE IIA									
7	ID	KIOWA ENGINEERING CORPORATION FILENAME WFSREUT.DAT									
	*DIAGRAM										
8	IT	3	0	C	288						
9	IO	5									
10	JR	PREC	.56	1.0							
11	KK	SBM?									
12	KM	RUNOFF FROM SUB-BASIN M7									

WEST FORK FUTURE

13	IN	15										
14	PB	4.1										
15	PC	C.0	.0005	.0015	.0030	.0045	.0060	.0080	.0100	.0120	.0143	
16	PC	.0165	.0188	.0210	.0233	.0255	.0278	.0320	.0390	.0460	.0530	
17	PC	.0600	.0750	.1000	.1400	.1700	.2250	.2500	.2650	.2800	.2900	
18	PC	.8000	.8100	.8200	.8250	.8300	.8350	.8400	.8450	.8500	.8550	
19	PC	.8600	.8638	.8675	.8713	.8750	.8788	.8825	.8863	.8900	.8938	
20	PC	.8975	.9013	.9050	.9083	.9115	.9148	.9180	.9210	.9240	.9270	
21	PC	.9300	.9325	.9350	.9375	.9400	.9425	.9450	.9475	.9500	.9525	
22	PC	.9550	.9575	.9600	.9625	.9650	.9675	.9700	.9725	.9750	.9775	
23	PC	.9800	.9813	.9825	.9838	.9850	.9863	.9875	.9888	.9900	.9913	
24	PC	.9963	.9975	.9988	1.0000							
25	BA	.0528										
26	LS	0	66									
27	UD	.27										

28	KK	RTM7										
29	KM	ROUTE RUNOFF FROM SUB-BASIN M7 TO DP 8										
30	RK	3000	.021	.03	0	TRAP	20	10				

31	KK	SEM8										
32	KM	RUNOFF FROM SUB-BASIN M8										
33	BA	.1243										
34	LS	0	66									
35	UD	.45										

36	KK	SBM11										
37	KM	RUNOFF FROM SUB-BASIN M11										
38	BA	.0467										
39	LS	0	71.6									
40	UD	.36										

41	KK	RTM11										
42	KM	ROUTE SUB-BASIN M11 TO DP 9										
43	RK	2600	.03	.03	0	TRAP	4	4				

HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

44	KK	M9										
45	KM	RUNOFF FROM SUB-BASIN M9										
46	BA	.0844										
47	LS	0	69									
48	UD	.45										

49	KK	DP9										
50	KM	COMBINE SMM9 AND RTM11										
51	HC	2										

52	KK	DB9										
53	KM	ROUTE FLOW FROM DP 9 THROUGH DETENTION BASIN DB 9										

54	RS	1	ELEV	6463					
55	SQ	0	16	37	45	158			
56	SA	0	.624	.701	.771	1			
57	SE	6463	6465	6467	6468	6469.5			
58	SS	6468	25	3	1.5				
59	ST	6468	200	3	1.5				
60	KK	RTDB9							
61	KM	ROUTE OUTFLOW FROM DB 9 TO DESIGN POINT 8							
62	RK	1800	.025	.03	0	TRAP	20	10	
63	KK	DP8							
64	KM	COMBINE RTDB9, RTM7 AND SUB-BASIN M8							
65	HC	3							
66	KK	DB8							
67	KM	ROUTER RUNOFF AT DP 8 THROUGH DETENTION BASIN DB8							
68	RS	1	ELEV	6401.5					
69	SQ	0	3.5	15	20	220			
70	SA	2.12	2.35	2.73	3.25	3.5			
71	SE	6402	6404	6406	6408	6409.5			
72	SS	6406	25	3	1.5				
73	ST	6408	200	3	1.5				
74	KK	RTDB8							
75	KM	ROUTE OUTFLOW FROM DETENTION BASIN 8 TO DP 10							
76	RK	1300	.02	.013	0	CIRC	2.25		
77	KK	M10							
78	KM	RUNOFF FROM SUB-BASIN M10							
79	EA	.0512							
80	LS	0	77						
81	UD	.35							
82	KK	DP10							
83	KM	COMBINE RUNOFF FROM SUB-BASIN M10 AND RTDB8							
84	HC	2							

HEC-1 INPUT

LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
85	KK	RDP10									
86	KM	ROUTE RUNOFF FROM DP 10 TO DP 14.1									
87	RK	800	.05	.013	0	CIRC	3				
88	KK	M14.1									
89	KM	RUNOFF FROM SUB-BASIN M14.1									
90	EA	.012									
91	LS	0	85								
92	UD	.15									

93	KK	DP14.1							
94	KM		COMBINE SUB-BASIN M14.1 AND RDF10						
95	HC		2						
96	KK	RD14.1							
97	KM		ROUTE RUNOFF FROM DP 14.1 TO DP 14.2						
98	RK	300	.045 .013 0 CIRC 3.5						
99	KK	M14D							
100	KM		RUNOFF FROM SUB-BASIN M14D						
101	BA	.0104							
102	LS	0	75						
103	UD	.125							
104	KK	DP14.2							
105	KM		COMBINE M14D AND RD14.1						
106	HC		2						
107	KK	RD14.2							
108	KM		ROUTE DP 14.2 TO DETENTION BASIN DE14						
109	RK	500	.045 .035 TRAP 6 5						
110	KK	M12							
111	KM		RUNOFF FROM SUB-BASIN M12						
112	BA	.114							
113	LS	0	70						
114	UD	.43							
115	KK	RTM12							
116	KM		ROUTE RUNOFF FROM SB M12 TO DP 13						
117	RK	1700	.024 .024 0 TRAP 3 1						
118	KK	M13							
119	KM		RUNOFF FROM SUB-BASIN M13						
120	BA	.0949							
121	LS	0	67						
122	UD	.39							
123	KK	DP13							
124	KM		COMBINE RUNOFF FROM SB M13 AND RTM12						
125	HC		2						

1

HEC-1 INPUT

PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

126	KK	RDP13							
127	KM		ROUTE RUNOFF AT DP 13 TO DP 13.1						
128	RK	350	.05 .013 0 CIRC 4						
129	KK	M14C							
130	KM		RUNOFF FROM SB M14C						

131	BA	.0217							
132	LS		69						
133	UD	.115							
134	KK	DP13.1							
135	KM		COMBINE RUNOFF FROM M14C AND RDE13						
136	HC	2							
137	KK	RD13.1							
138	KM	ROUTE DP13.1 TO DP 13.2							
139	RK	350	.03	.013		CIRC	4		
140	KK	RD13.2							
141	KM	ROUTE RD 13.1 TO DETENTION BASIN DR14							
142	RK	1450	.045	.03		TRAP	6	2	
143	KK	M14A							
144	KM		RUNOFF FROM SUB-BASIN M14A						
145	BA	.0315							
146	LS	0	53						
147	UD	.139							
148	KK	DP14							
149	KM		COMBINE M14A, RD14.2 AND RD13.2						
150	HC	3							
151	KK	DE14							
152	KM		ROUTE RUNOFF AT DP 14 THROUGH DETENTION BASIN DE 14						
153	RS	1	ELEV	6306					
154	SQ	0	24.5	73.4	100.8	122	141	157	
155	SE	6306	6308	6310	6312	6314	6316	6318	
156	SV	0	.18	.66	1.55	3.05	5.22	8.1	
157	ZZ								

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
11	SEM7	
	V	
	V	
28	RTM7	
	.	
	.	
31	SEM8	
	.	
	.	
36	SEM11	
	V	
	V	

41	.	.	RTM11	
	.	.	.	
44	.	.	.	M9
	.	.	.	
49	.	.	DP9.....	
	.	.	V	
	.	.	V	
52	.	.	DB9	
	.	.	V	
	.	.	V	
60	.	.	RTDB9	
	.	.	.	
	.	.	.	
63	DP8.....	.	.	
	V	.	.	
	V	.	.	
66	DB8	.	.	
	V	.	.	
	V	.	.	
74	RTDB8	.	.	
	.	.	.	
77	.	M10	.	
	.	.	.	
	.	.	.	
82	DP10.....	.	.	
	V	.	.	
	V	.	.	
85	RDP10	.	.	
	.	.	.	
88	.	M14.1	.	
	.	.	.	
	.	.	.	
93	DP14.1.....	.	.	
	V	.	.	
	V	.	.	
96	RD14.1	.	.	
	.	.	.	
	.	.	.	
99	.	M14D	.	
	.	.	.	
	.	.	.	
104	DP14.2.....	.	.	
	V	.	.	
	V	.	.	
107	RD14.2	.	.	
	.	.	.	
	.	.	.	
110	.	M12	.	


```

      .
      .      V
      .      V
115      .      RTM12
      .
      .
118      .      .      M13
      .      .
      .
123      .      DP13.....
      .      V
      .      V
126      .      RDP13
      .
      .
129      .      .      M14C
      .      .
      .
134      .      DP13.1.....
      .      V
      .      V
137      .      RD13.1
      .      V
      .      V
140      .      RD13.2
      .
      .
143      .      .      M14A
      .      .
      .
148      .      DP14.....
      .      V
      .      V
151      .      DB14

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
*
* RUN DATE 08SEPC8 TIME 11:50:25 *
*
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*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

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MESA DRAINAGE BASIN
 SENTINEL RIDGE MASTER DEVELOPMENT DRAINAGE PLAN
 WEST FORK BRANCH

24-HOUR TYPE IIA RAINFALL DISTRIBUTION
 FUTURE DEVELOPMENT CONDITIONS WITH EXISTING DETENTION AT DP 14
 5 AND 100-YEAR STORMS 24HOUR TYPE IIA
 KIOWA ENGINEERING CORPORATION FILENAME WFSRFUI.DAT

9 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 3 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 288 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 1 0 ENDING DATE
 NDTIME 1421 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .05 HOURS
 TOTAL TIME BASE 14.35 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .56 1.00

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	SBM7	.05	1	FLOW	7.
				TIME	45. 6.20 6.15

ROUTED TO
+ RTM7 .05 1 FLOW 7. 44.
TIME 6.40 6.25

HYDROGRAPH AT
+ SEM8 .12 1 FLOW 12. 74.
TIME 6.40 6.35

HYDROGRAPH AT
+ SEM11 .05 1 FLOW 11. 45.
TIME 6.30 6.25

ROUTED TO
+ RTM11 .05 1 FLOW 10. 45.
TIME 6.35 6.30

HYDROGRAPH AT
+ M9 .08 1 FLOW 12. 61.
TIME 6.40 6.35

2 COMBINED AT
+ DP9 .13 1 FLOW 23. 105.
TIME 6.40 6.30

ROUTED TO
+ DB9 .13 1 FLOW 15. 77.
TIME 6.70 6.55

** PEAK STAGES IN FEET **
1 STAGE 6464.83 6468.08
TIME 6.70 6.55

ROUTED TO
+ RTDB9 .13 1 FLOW 15. 75.
TIME 6.75 6.60

3 COMBINED AT
+ DP8 .31 1 FLOW 31. 149.
TIME 6.50 6.60

ROUTED TO
+ DB8 .31 1 FLOW 5. 18.
TIME 8.70 9.00

** PEAK STAGES IN FEET **
1 STAGE 6403.16 6407.08
TIME 8.70 9.00

ROUTED TO
+ RTDB8 .31 1 FLOW 5. 18.
TIME 8.70 9.00

HYDROGRAPH AT						
+	M10	.05	1	FLOW	20.	66.
				TIME	6.25	6.20
2 COMBINED AT						
+	DP10	.36	1	FLOW	20.	68.
				TIME	6.25	6.25
ROUTED TO						
+	RDP10	.36	1	FLOW	20.	68.
				TIME	6.25	6.25
HYDROGRAPH AT						
+	M14.1	.01	1	FLOW	12.	30.
				TIME	6.05	6.05
2 COMBINED AT						
+	DP14.1	.37	1	FLOW	26.	85.
				TIME	6.15	6.15
ROUTED TO						
+	RD14.1	.37	1	FLOW	26.	85.
				TIME	6.15	6.15
HYDROGRAPH AT						
+	M14D	.01	1	FLOW	6.	19.
				TIME	6.05	6.05
2 COMBINED AT						
+	DP14.2	.38	1	FLOW	31.	100.
				TIME	6.10	6.10
ROUTED TO						
+	RD14.2	.38	1	FLOW	30.	99.
				TIME	6.10	6.10
HYDROGRAPH AT						
+	M12	.11	1	FLOW	19.	89.
				TIME	6.35	6.30
ROUTED TO						
+	RTM12	.11	1	FLOW	19.	89.
				TIME	6.40	6.35
HYDROGRAPH AT						
+	M13	.09	1	FLOW	12.	67.
				TIME	6.35	6.30
2 COMBINED AT						
+	DP13	.21	1	FLOW	30.	155.
				TIME	6.40	6.30

ROUTED TO						
+	RDP13	.21	1	FLOW	30.	155.
				TIME	6.40	6.30
HYDROGRAPH AT						
+	M14C	.02	1	FLOW	7.	31.
				TIME	6.05	6.05
2 COMBINED AT						
+	DP13.1	.23	1	FLOW	32.	161.
				TIME	6.40	6.30
ROUTED TO						
+	RD13.1	.23	1	FLOW	32.	161.
				TIME	6.40	6.30
ROUTED TO						
+	RD13.2	.23	1	FLOW	32.	159.
				TIME	6.40	6.30
HYDROGRAPH AT						
+	M14A	.03	1	FLOW	0.	13.
				TIME	8.00	6.10
3 COMBINED AT						
+	DP14	.64	1	FLOW	54.	245.
				TIME	6.30	6.25
ROUTED TO						
+	DB14	.64	1	FLOW	51.	143.
				TIME	6.45	6.65

** PEAK STAGES IN FEET **

1	STAGE	6309.08	6316.19
	TIME	6.45	6.65

1
1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DE9
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1

	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
STORAGE		6463.00	6468.00	6468.00
OUTFLOW		0.	2.	2.
			45.	45.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
--------------	----------------------------	------------------------	-----------------------	---------------------	-------------------------	---------------------------	-----------------------

	.56	6464.83	.00	0.	15.	.00	6.70	.00
1	1.00	6468.08	.08	3.	77.	.30	6.55	.00

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION CB8
 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1

	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
		6401.50	6406.30	6408.00
STORAGE		0.	10.	16.
OUTFLOW		0.	15.	20.

RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
.56	6403.16	.00	3.	5.	.00	8.70	.00
1.00	6407.08	.00	13.	18.	.00	9.00	.00

*** NORMAL END OF HEC-1 ***

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 31DEC07 TIME 09:55:19
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X X YXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X YXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIME- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	MESA DRAINAGE BASIN									
2	ID	SENTINEL RIDGE MASTER DEVELOPMENT DRAINAGE PLAN									
3	ID	EAST FORK BRANCH MESA BASIN EXISTING CONDITIONS									
4	ID	24-HOUR TYPE IIA RAINFALL DISTRIBUTION									
5	ID	EXISTING DEVELOPMENT CONDITIONS WITH EXISTING DETENTION BASINS									
6	ID	5 AND 100-YEAR STORMS 24HOUR TYPE IIA									
7	ID	KIOWA ENGINEERING CORPORATION FILENAME EFSREX.DAT									
	*DIAGRAM										
8	IT	5	0	0	288						
9	IO	5									
10	JR	PREC	.56	1.0							
11	KK	PKR3									
12	KM	PARKER DESIGN POINT 3 (BASINS 1 2 AND 3)									

EAST FORK BRANCH

IN	15										
PB	4.1										
PC	0.0	.0005	.0015	.0030	.0045	.0060	.0080	.0100	.0120	.0143	
PC	.0165	.0188	.0210	.0233	.0255	.0278	.0320	.0390	.0460	.0530	
PC	.0600	.0750	.1000	.4000	.7000	.7250	.7500	.7650	.7800	.7900	
PC	.8000	.8100	.8200	.8250	.8300	.8350	.8400	.8450	.8500	.8550	
PC	.8600	.8638	.8675	.8713	.8750	.8788	.8825	.8863	.8900	.8938	
PC	.8975	.9013	.9050	.9083	.9115	.9148	.9180	.9210	.9240	.9270	
PC	.9300	.9325	.9350	.9375	.9400	.9425	.9450	.9475	.9500	.9525	
PC	.9550	.9575	.9600	.9625	.9650	.9675	.9700	.9725	.9750	.9775	
PC	.9800	.9813	.9825	.9838	.9850	.9863	.9875	.9888	.9900	.9913	
PC	.9963	.9975	.9988	1.0000							
BA	.2244										
LS	0	84.5									
UD	.38										

KK RTPKR3
 KM ROUTE PKR3 THRU PKR3A
 RK 2930 .024 .03 0 TRAP 5 4

KK PRK3A
 KM PARKER DESIGN POINT 3A (HILL CIRCLE) PORTION OF PARKER BASIN 4
 BA .134
 LS 0 83
 UD .2

KK DP3A
 KM COMBINE RTPKR3 AND PRK3A
 HC 2

KK RTDP3A
 KM ROUTE DP3A THRU DP5A
 RK 1150 .018 .04 0 TRAP 10 5

KK M6A
 KM RUNOFF FROM SUB-BASIN M6A
 BA .069
 LS 0 74
 UD .12

HEC-1 INPUT

ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

KK DP5A
 KM COMBINE RTDP3A AND M6A
 HC 2

KK DB5A
 KM ROUTE FLOWS THRU DP5A THROUGH DET DET BASIN 5A (48" RCP OUTLET)
 RS 1 ELEV 6398.2
 SQ 0 10 24 73 115 148 180 1500

94	KK	R17.1						
95	KM	ROUTE DP 17.1 TO DP 17.2						
96	RK	800	.04	.030	0	TRAP	8	1
97	KK	M17.2						
98	KM	RUNOFF FROM SUB-BASIN M17.2						
99	BA	.0386						
100	LS	0	61					
101	UD	.17						
102	KK	DP17.2						
103	KM	COMBINE RUNOFF FROM SUB-BASIN M17.2 AND R17.1						
104	HC	2						
105	KK	R17.2						
106	KM	ROUTE DP 17.2 TO DP 18.1						
107	RK	1000	.035	.03	0	TRAP	8	3
108	KK	M18.1						
109	KM	RUNOFF FROM SUB-BASIN M18.1						
110	BA	.0584						
111	LS	0	53					
112	UD	.22						
113	KK	DP18.1						
114	KM	COMBINE SUB-BASIN M18.2 AND R17.2						
115	HC	2						
116	KK	R18.1						
117	KM	ROUTE DP 18.1 TO DP 18.2						
118	RK	1600	.031	.03	0	TRAP	8	2
119	KK	M18.2						
120	KM	RUNOFF FROM SUB-BASIN M18.2						
121	BA	.0556						
122	LS	0	85					
123	UD	.2						
124	KK	DP18.2						
125	KM	COMBINE SUB-BASIN M18.2 AND R18.1						
126	HC	2						
127	ZZ							

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

11 PKR3
 V

```

      V
28  RTPKR3
      .
31      .      ERK3A
      .
36  DP3A.....
      V
39  RTDP3A
      .
42      .      M6A
      .
47  DP5A.....
      V
50  DB5A
      V
56  RTDB5A
      .
59      .      M5
      .
64      .      M6
      .
69  DP5.....
      V
72  DB5B
      V
83  RTDB5B
      .
86      .      M17.1
      .
91  DP17.1.....
      V
94  R17.1
      .
97      .      M17.2
      .

```

```

102 DP17.2.....
      V
      V
105 R17.2
      .
      .
108 . M18.1
      .
      .
113 DP18.1.....
      V
      V
116 R18.1
      .
      .
119 . M18.2
      .
      .
124 DP18.2.....

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1 *****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 31DEC07 TIME 09:55:19 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

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MESA DRAINAGE BASIN
SENTINEL RIDGE MASTER DEVELOPMENT DRAINAGE PLAN
EAST FORK BRANCH MESA BASIN EXISTING CONDITIONS
24-HOUR TYPE IIA RAINFALL DISTRIBUTION
EXISTING DEVELOPMENT CONDITIONS WITH EXISTING DETENTION BASINS
5 AND 100-YEAR STORMS 24HOUR TYPE IIA
KIOWA ENGINEERING CORPORATION FILENAME EFSREX.DAT

```

```

9 IO OUTPUT CONTROL VARIABLES
      IPRNT          5 PRINT CONTROL
      IPLOT          0 PLOT CONTROL
      QSCAL          0. HYDROGRAPH PLOT SCALE

```

```

IT HYDROGRAPH TIME DATA
      NMIN          5 MINUTES IN COMPUTATION INTERVAL
      IDATE          1 0 STARTING DATE
      ITIME          0000 STARTING TIME
      NQ             208 NUMBER OF HYDROGRAPH ORDINATES
      NDDATE          1 0 ENDING DATE
      NDTIME          2355 ENDING TIME
      ICENT           19 CENTURY MARK

```

COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 23.92 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .56 1.00

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	PKR3	.22	1	FLOW	321.
				TIME	6.25
ROUTED TO					
+	RTPKR3	.22	1	FLOW	318.
				TIME	6.25
HYDROGRAPH AT					
+	PRK3A	.13	1	FLOW	247.
				TIME	6.08
2 COMBINED AT					
+	DP3A	.36	1	FLOW	503.
				TIME	6.17
ROUTED TO					
+	RTDP3A	.36	1	FLOW	498.
				TIME	6.17
HYDROGRAPH AT					
+	M6A	.07	1	FLOW	100.
				TIME	6.00

2 COMBINED AT						
+	DF5A	.43	1	FLOW	186.	553.
				TIME	6.17	6.17

ROUTED TO						
+	DB5A	.43	1	FLOW	138.	595.
				TIME	6.42	6.17

** PEAK STAGES IN FEET **						
1	STAGE	6405.40	6408.63			
	TIME	6.42	6.17			

ROUTED TO						
+	RTDB5A	.43	1	FLOW	138.	564.
				TIME	6.50	6.17

HYDROGRAPH AT						
+	M5	.10	1	FLOW	49.	144.
				TIME	6.17	6.17

HYDROGRAPH AT						
+	M6	.02	1	FLOW	11.	31.
				TIME	6.08	6.00

3 COMBINED AT						
+	DP5	.54	1	FLOW	176.	729.
				TIME	6.25	6.17

ROUTED TO						
+	DB5B	.54	1	FLOW	106.	168.
				TIME	6.92	7.17

** PEAK STAGES IN FEET **						
1	STAGE	6379.65	6390.40			
	TIME	6.92	7.17			

ROUTED TO						
+	RTDB5B	.54	1	FLOW	106.	168.
				TIME	6.92	7.17

HYDROGRAPH AT						
+	M17.1	.04	1	FLOW	14.	53.
				TIME	6.08	6.08

2 COMBINED AT						
+	DP17.1	.58	1	FLOW	107.	172.
				TIME	6.92	7.08

ROUTED TO						
+	R17.1	.58	1	FLOW	107.	172.
				TIME	6.92	7.08

HYDROGRAPH AT						
+	M17.2	.04	1	FLOW	1.	23.
				TIME	6.17	6.08
2 COMBINED AT						
+	DP17.2	.62	1	FLOW	108.	177.
				TIME	6.92	6.17
ROUTED TO						
+	R17.2	.62	1	FLOW	107.	176.
				TIME	6.92	6.17
HYDROGRAPH AT						
+	M18.1	.06	1	FLOW	0.	13.
				TIME	22.58	6.17
2 COMBINED AT						
+	DP18.1	.68	1	FLOW	107.	189.
				TIME	6.92	6.17
ROUTED TO						
+	R18.1	.68	1	FLOW	107.	186.
				TIME	7.00	6.17
HYDROGRAPH AT						
+	M18.2	.06	1	FLOW	43.	110.
				TIME	6.08	6.08
2 COMBINED AT						
+	DP18.2	.74	1	FLOW	111.	279.
				TIME	6.92	6.17

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DB5B
(Peaks shown are for internal time step used during breach formation)

PLAN 1

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	6369.70	6392.00	6394.00
STORAGE	0.	29.	34.
OUTFLOW	0.	1600.	4440.

RATIO OF EMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
.56	6379.65	.00	5.	106.	.00	6.92	.00
1.00	6390.40	.00	25.	168.	.00	7.17	.00

*** NORMAL END OF HEC-1 ***

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 09SEP08 TIME 11:42:37
*
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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	MESA DRAINAGE BASIN									
2	ID	SENTINEL RIDGE MASTER DEVELOPMENT DRAINAGE PLAN									
3	ID	EAST FORK BRANCH									
4	ID	24-HOUR TYPE IIA RAINFALL DISTRIBUTION									
5	ID	FUTURE DEVELOPMENT CONDITIONS WITH EXISTING AND PROPOSED DETENTION									
6	ID	5 AND 100-YEAR STORMS 24HOUR TYPE IIA									
7	ID	KIOWA ENGINEERING CORPORATION FILENAME EFSRFUT.DAT									
	*DIAGRAM										
8	IT	5	0	0	288						
9	IO	5									
10	JR	PREC	.56	1.0							
11	KK	PKR3									
12	KM	PARKER DESIGN POINT 3 (BASINS 1 2 AND 3)									

EAST FORK FUTURE

13	IN	15									
14	PB	4.1									
15	PC	0.0	.0005	.0015	.0030	.0045	.0060	.0080	.0100	.0120	.0143
16	PC	.0165	.0188	.0210	.0233	.0255	.0278	.0320	.0390	.0460	.0530
17	PC	.0600	.0750	.1000	.4000	.7000	.7250	.7500	.7650	.7800	.7900
18	PC	.8000	.8100	.8200	.8250	.8300	.8350	.8400	.8450	.8500	.8550
19	PC	.8600	.8638	.8675	.8713	.8750	.8788	.8825	.8863	.8900	.8938
20	PC	.8975	.9013	.9050	.9083	.9115	.9148	.9180	.9210	.9240	.9270
21	PC	.9300	.9325	.9350	.9375	.9400	.9425	.9450	.9475	.9500	.9525
22	PC	.9550	.9575	.9600	.9625	.9650	.9675	.9700	.9725	.9750	.9775
23	PC	.9800	.9813	.9825	.9838	.9850	.9863	.9875	.9888	.9900	.9913
24	PC	.9963	.9975	.9988	1.0000						
25	BA	.2244									
26	LS	0	34.5								
27	UD	.38									

28	KK	RTPKR3									
29	KM	ROUTE PKR3 THRU PKR3A									
30	RK	2930	.024	.03	0	TRAP	5	4			
31	KK	PRK3A									
32	KM	PARKER DESIGN POINT 3A (HILL CIRCLE) PORTION OF PARKER BASIN 4									
33	BA	.134									
34	LS	0	83								
35	UD	.2									
36	KK	DP3A									
37	KM	COMBINE RTPKR3 AND PRK3A									
38	HC	2									
39	KK	RTDP3A									
40	KM	ROUTE DP3A THRU DP5A									
41	RK	1150	.018	.04	0	TRAP	10	.5			
42	KK	M6A									
43	KM	RUNOFF FROM SUB-BASIN M6A									
44	BA	.069									
45	LS	0	74								
46	UD	.12									

1

HEC-1 INPUT

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
47	KK DP5A
48	KM COMBINE RTDP3A AND M6A
49	HC 2
50	KK DB5A
51	KM ROUTE FLOWS THRU DP5A THROUGH DET DET BASIN 5A (48" RCF OUTLET)
52	RS 1 ELEV 6398.2
53	SQ 0 10 24 .73 115 148 180 1500

94	KK	RD17.1							
95	KM		ROUTE DP 17.1 TO DP 17.2						
96	RK	800	.04	.030	0	TRAP	8	1	
97	KK	M17A							
98	KM		RUNOFF FROM SUB-BASIN M17A						
99	BA	.0386							
100	LS	0	89						
101	UD	.17							
102	KK	DP17.2							
103	KM		COMBINE RUNOFF FROM SUB-BASIN M17.2 AND RD17.1						
104	HC	2							
105	KK	RD17.2							
106	KM		ROUTE DP 17.2 TO DP 18.1						
107	RK	1000	.035	.03	0	TRAP	8	3	
108	KK	M18A							
109	KM		RUNOFF FROM SUB-BASIN M18A						
110	BA	.0354							
111	LS	0	50						
112	UD	.15							
113	KK	M18B							
114	KM		RUNOFF FROM SUB-BASIN M18B						
115	BA	.0206							
116	LS	0	60						
117	UD	.146							
118	KK	DP18.1							
119	KM		COMBINE SUB-BASIN M18A, M18B AND RD17.2						
120	HC	3							
121	KK	RD18.1							
122	KM		ROUTE DP 18.1 TO DP 18.2						
123	RK	1600	.031	.03	0	TRAP	8	2	
124	KK	M18C							
125	KM		RUNOFF FROM SUB-BASIN M18C						
126	BA	.0314							
127	LS	0	80						
128	UD	.186							
129	KK	RM18C							
130	KM		ROUTE SUB-BASIN M18C TO DP18.2						
131	RK	520	.05	.013		CIRC	3		

HEC-1 INPUT

PAGE 4

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

132	KK	M18D	
133	KM	RUNOFF FROM SUB BASIN M18D	
134	BA	.0386	
135	LS	0	82
136	UD	.125	
137	KK	DP18.2	
138	KM	COMBINE SUB-BASIN SUBBASIN M18D, RM18C AND RD18.1	
139	HC	3	
140	ZZ		

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW

11	PKR3		
	V		
	V		
28	RTPKR3		
	.		
31	.	PRK3A	
	.		
	.		
36	DP3A.....		
	V		
	V		
39	RTDP3A		
	.		
	.		
42	.	M6A	
	.		
	.		
47	DP5A.....		
	V		
	V		
50	DB5A		
	V		
	V		
56	RTDB5A		
	.		
	.		
59	.	M5	
	.		
	.		
64	.		M6
	.		
	.		
69	DP5.....		

```

      V
      V
72    DB5B
      V
      V
83    RDB5B
      .
      .
86    .          M17B
      .          .
      .          .
91    DP17.1.....
      V
      V
94    RD17.1
      .
      .
97    .          M17A
      .          .
      .          .
102   DP17.2.....
      V
      V
105   RD17.2
      .
      .
108   .          M18A
      .          .
      .          .
113   .          .          M18B
      .          .          .
      .          .          .
118   DP18.1.....
      V
      V
121   RD18.1
      .
      .
124   .          M18C
      .          V
      .          V
129   .          RM18C
      .          .
      .          .
132   .          .          M18D
      .          .          .
      .          .          .
137   DP18.2.....

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

*

*

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*

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* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 09SEP08 TIME 11:42:37 *
*****

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* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

```

```

MESA DRAINAGE BASIN
SENTINEL RIDGE MASTER DEVELOPMENT DRAINAGE PLAN
EAST FORK BRANCH
24-HOUR TYPE IIA RAINFALL DISTRIBUTION
FUTURE DEVELOPMENT CONDITIONS WITH EXISTING AND PROPOSED DETENTION
5 AND 100-YEAR STORMS 24HOUR TYPE IIA
KIOWA ENGINEERING CORPORATION FILENAME EFSRFUT.DAT

```

```

9 IO OUTPUT CONTROL VARIABLES
      IPRNT      5 PRINT CONTROL
      IPLOT      0 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
      NMIN      5 MINUTES IN COMPUTATION INTERVAL
      IDATE      1 0 STARTING DATE
      ITIME      0000 STARTING TIME
      NQ        288 NUMBER OF HYDROGRAPH ORDINATES
      NDDATE      1 0 ENDING DATE
      NDTIME      2355 ENDING TIME
      ICENT      19 CENTURY MARK

      COMPUTATION INTERVAL .08 HOURS
      TOTAL TIME BASE 23.92 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

```

```

JP MULTI-PLAN OPTION
      NELAN      1 NUMBER OF PLANS

```

```

JR MULTI-RATIO OPTION
      RATIOS OF PRECIPITATION
      .56 1.00

```

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	PKR3	.22	1	FLOW	118.
				TIME	6.25
					321.
					6.25
ROUTED TO					
+	RTPKR3	.22	1	FLOW	116.
				TIME	6.33
					318.
					6.25
HYDROGRAPH AT					
+	PRK3A	.13	1	FLOW	90.
				TIME	6.08
					247.
					6.08
2 COMBINED AT					
+	DP3A	.36	1	FLOW	176.
				TIME	6.17
					503.
					6.17
ROUTED TO					
+	RTDP3A	.36	1	FLOW	172.
				TIME	6.25
					498.
					6.17
HYDROGRAPH AT					
+	M6A	.07	1	FLOW	26.
				TIME	6.08
					100.
					6.00
2 COMBINED AT					
+	DP5A	.43	1	FLOW	186.
				TIME	6.17
					553.
					6.17
ROUTED TO					
+	DB5A	.43	1	FLOW	138.
				TIME	6.42
					595.
					6.17
				** PEAK STAGES IN FEET **	
				1 STAGE	6405.40
				TIME	6.42
					6408.63
					6.17
ROUTED TO					
+	RTDB5A	.43	1	FLOW	138.
				TIME	6.50
					564.
					6.17
HYDROGRAPH AT					

+	M5	.10	1	FLOW TIME	49. 6.17	144. 6.17
HYDROGRAPH AT						
+	M6	.02	1	FLOW TIME	11. 6.08	31. 6.00
3 COMBINED AT						
+	DP5	.54	1	FLOW TIME	176. 6.25	729. 6.17
ROUTED TO						
+	DB5B	.54	1	FLOW TIME	106. 6.92	168. 7.17
** PEAK STAGES IN FEET **						
1	STAGE				6379.65	6390.40
	TIME				6.92	7.17
ROUTED TO						
+	RDB5B	.54	1	FLOW TIME	106. 6.92	168. 7.17
HYDROGRAPH AT						
+	M17B	.03	1	FLOW TIME	24. 6.00	64. 6.00
2 COMBINED AT						
+	DP17.1	.57	1	FLOW TIME	107. 6.92	171. 7.08
ROUTED TO						
+	RD17.1	.57	1	FLOW TIME	107. 6.92	171. 7.08
HYDROGRAPH AT						
+	M17A	.04	1	FLOW TIME	40. 6.08	91. 6.00
2 COMBINED AT						
+	DP17.2	.61	1	FLOW TIME	111. 6.08	245. 6.09
ROUTED TO						
+	RD17.2	.61	1	FLOW TIME	111. 6.17	243. 6.08
HYDROGRAPH AT						
+	M18A	.04	1	FLOW TIME	0. 22.58	6. 6.08
HYDROGRAPH AT						

+	M18B	.02	1	FLOW TIME	1. 6.08	12. 6.08
3 COMBINED AT						
+	DP18.1	.67	1	FLOW TIME	111. 6.17	261. 6.08
ROUTED TO						
+	RD18.1	.67	1	FLOW TIME	110. 7.00	255. 6.08
HYDROGRAPH AT						
+	M18C	.03	1	FLOW TIME	18. 6.08	53. 6.08
ROUTED TO						
+	RM18C	.03	1	FLOW TIME	17. 6.08	53. 6.08
HYDROGRAPH AT						
+	M18D	.04	1	FLOW TIME	28. 6.00	78. 6.00
3 COMBINED AT						
+	DP18.2	.74	1	FLOW TIME	145. 6.08	378. 6.08
1						

*** NORMAL END OF HEC-1 ***

APPENDIX B

HYDRAULIC CALCULATIONS

WEIGHTED CURVE NUMBER ESTIMATION EAST FORK MESA BASIN
PROJECT: SENTINEL RIDGE MDDP
PROJECT NO: 07028

SUB-BASIN NO.	AREA (SM)	PERCENT OF AREA	EXISTING CN	SUB-BASIN NO.	AREA (SM)	PERCENT OF AREA	DEVELOPED CN
M17.1	0.0399	0.2073	74	M17B	0.0278	0.1445	85
M17.2	0.0386	0.2005	61	M17A	0.0386	0.2006	89
M18.1	0.0584	0.3034	53	M18A	0.0354	0.1840	50
M18.2	0.0556	0.2888	85	M18B	0.0206	0.1071	60
				M18C	0.0314	0.1632	80
				M18D	0.0386	0.2006	82

0.1925

0.1924

WEIGHTED CN

68.2

75.3

Req'd Det. Storage Est. RF: 2.3" 5yr ; 4.1" 100 year

100-year e CN = 68 Runoff = 1.27" $\Delta = .47"$
 e CN = 75 Runoff = 1.74"

$$Vol = .47 \frac{1}{2} (.1924)(640) = \underline{4.8 AF}$$

5-year e CN = 68 Runoff = .31" $\Delta = .23"$
 e CN = 75 Runoff = .54"

$$Vol = .23 \frac{1}{2} (.1924)(640) = \underline{2.4 AF}$$

OUTLET PIPE
DET BASIN 18

CURRENT DATE: 12-31-2007
CURRENT TIME: 14:51:33

FILE DATE: 12-31-2007
FILE NAME: EFDET

FHWA CULVERT ANALYSIS
HY-8, VERSION 6.1

C U L V E R T N O.	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (ft)	OUTLET ELEV. (ft)	CULVERT LENGTH (ft)	BARRELS SHAPE MATERIAL	SPAN (ft)	RISE (ft)	MANNING n	INLET TYPE
1	6019.00	6016.00	160.03	1 RCP	4.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (cfs) FILE: EFDET DATE: 12-31-2007

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
6019.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	1
6021.27	30.0	30.0	0.0	0.0	0.0	0.0	0.0	0.00	1
6022.50	60.0	60.0	0.0	0.0	0.0	0.0	0.0	0.00	1
6023.70	90.0	90.0	0.0	0.0	0.0	0.0	0.0	0.00	1
6025.24	120.0	120.0	0.0	0.0	0.0	0.0	0.0	0.00	1
6027.27	150.0	150.0	0.0	0.0	0.0	0.0	0.0	0.00	1
6029.79	180.0	180.0	0.0	0.0	0.0	0.0	0.0	0.00	1
6032.75	210.0	210.0	0.0	0.0	0.0	0.0	0.0	0.00	1
6035.86	240.0	237.8	0.0	0.0	0.0	0.0	0.0	0.00	1
6036.21	270.0	240.6	0.0	0.0	0.0	0.0	0.0	0.00	13
6036.33	300.0	241.7	0.0	0.0	0.0	0.0	0.0	27.82	6
6036.00	238.9	238.9	0.0	0.0	0.0	0.0	0.0	56.80	4
							0.0	OVERTOPPING	

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: EFDET DATE: 12-31-2007

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
6019.00	0.000	0.00	0.00	0.00
6021.27	0.000	30.00	0.00	0.00
6022.50	0.000	60.00	0.00	0.00
6023.70	0.000	90.00	0.00	0.00
6025.24	0.000	120.00	0.00	0.00
6027.27	0.000	150.00	0.00	0.00
6029.79	0.000	180.00	0.00	0.00
6032.75	0.000	210.00	0.00	0.00
6035.86	-0.010	240.00	0.00	0.00
6036.21	-0.004	270.00	2.21	0.92
6036.33	-0.004	300.00	1.54	0.57
			1.50	0.50

<1> TOLERANCE (ft) = 0.010

<2> TOLERANCE (%) = 1.000

CURRENT DATE: 12-31-2007
 (RENT TIME: 14:51:33

FILE DATE: 12-31-2007
 FILE NAME: EFDCT

PERFORMANCE CURVE FOR CULVERT 1 - 1(4.00 (ft) BY 4.00 (ft)) RCP

DIS-CHARGE FLOW (cfs)	HEAD-WATER ELEV. (ft)	INLET CONTROL DEPTH (ft)	OUTLET CONTROL DEPTH (ft)	FLOW TYPE <F4>	NORMAL DEPTH (ft)	CRIT. DEPTH (ft)	OUTLET DEPTH (ft)	TW DEPTH (ft)	OUTLET VEL. (fps)	TW VEL. (fps)
0.00	6019.00	0.00	0.00	0-NF	0.00	0.00	0.00	0.00	0.00	0.00
30.00	6021.27	2.27	2.27	1-S2n	0.99	1.62	0.92	0.56	13.57	4.54
60.00	6022.50	3.50	3.50	1-S2n	1.44	2.33	1.52	0.84	13.68	5.72
90.00	6023.70	4.70	4.70	5-S2n	1.81	2.87	1.94	1.05	14.90	6.50
120.00	6025.24	6.24	6.24	5-S2n	2.14	3.28	2.32	1.23	15.88	7.10
150.00	6027.27	8.27	8.27	5-S2n	2.47	3.59	2.68	1.39	16.75	7.60
180.00	6029.79	10.79	10.79	5-S2n	2.81	3.91	3.03	1.54	17.69	8.02
210.00	6032.74	13.74	10.40	6-S2n	3.22	4.00	3.44	1.67	18.33	8.39
237.79	6035.86	16.86	13.06	6-S2n	4.00	4.00	3.90	1.79	19.17	8.72
240.64	6036.20	17.20	13.35	6-S2n	4.00	4.00	3.90	1.90	19.40	9.02
241.70	6036.33	17.33	13.46	6-S2n	4.00	4.00	3.90	2.01	19.49	9.29

El. inlet face invert 6019.00 ft El. outlet invert 6016.00 ft
 El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

*** SITE DATA ***** CULVERT INVERT *****
 INLET STATION 100.00 ft
 INLET ELEVATION 6019.00 ft
 OUTLET STATION 260.00 ft
 OUTLET ELEVATION 6016.00 ft
 NUMBER OF BARRELS 1
 SLOPE (V/H) 0.0188
 CULVERT LENGTH ALONG SLOPE 160.03 ft

***** CULVERT DATA SUMMARY *****
 BARREL SHAPE CIRCULAR
 BARREL DIAMETER 4.00 ft
 BARREL MATERIAL CONCRETE
 BARREL MANNING'S n 0.012
 INLET TYPE CONVENTIONAL
 INLET EDGE AND WALL SQUARE EDGE WITH HEADWALL
 INLET DEPRESSION NONE

CURRENT DATE: 12-31-2007
 CURRENT TIME: 14:51:33

FILE DATE: 12-31-2007
 FILE NAME: EFDCT

TAILWATER

***** REGULAR CHANNEL CROSS SECTION *****
 BOTTOM WIDTH 10.00 ft
 SIDE SLOPE H/V (X:1) 3.0
 CHANNEL SLOPE V/H (ft/ft) 0.030
 MANNING'S n (.01-0.1) 0.035
 CHANNEL INVERT ELEVATION 6016.00 ft
 CULVERT NO.1 OUTLET INVERT ELEVATION 6016.00 ft

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (cfs)	W.S.E. (ft)	FROUDE NUMBER	DEPTH (ft)	VEL. (f/s)	SHEAR (psf)
0.00	6016.00	0.000	0.00	0.00	0.00
30.00	6016.56	1.066	0.56	4.54	1.06
60.00	6016.84	1.100	0.84	5.72	1.57
90.00	6017.05	1.117	1.05	6.50	1.97
120.00	6017.23	1.127	1.23	7.10	2.31
150.00	6017.39	1.134	1.39	7.60	2.61
180.00	6017.54	1.140	1.54	8.02	2.88
210.00	6017.67	1.144	1.67	8.39	3.12
240.00	6017.79	1.148	1.79	8.72	3.35
270.00	6017.90	1.151	1.90	9.02	3.57
300.00	6018.01	1.154	2.01	9.29	3.77

ROADWAY OVERTOPPING DATA

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH	40.00 ft
CREST LENGTH	100.00 ft
OVERTOPPING CREST ELEVATION	6036.00 ft

Detention Storage Volume Calculation
Sentinel Ridge
Colorado Springs, Colorado

PN 07028

DET BASIN
1B

elevation	area (sf)	area (ac)	average area (ac)	Interval (ft)	Incremental Volume (ac-ft)	Cumulative Volume (ac-ft)
6023	0	0.000				
6024	967	0.02	0.01	1	0.01	0.01
6030	15000	0.34	0.18	6	1.10	1.11
6032	18800	0.43	0.39	2	0.78	1.89
6034	19800	0.45	0.44	2	0.89	2.77
6036	36000	0.83	0.64	2	1.28	4.05

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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
*   VERSION 4.1
*
* RUN DATE 09SEP08 TIME 12:03:07
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION.

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
1	ID	MESA DRAINAGE BASIN									
2	ID	SENTINEL RIDGE MASTER DEVELOPMENT DRAINAGE PLAN									
3	ID	EAST FORK BRANCH WITH DETENTION AT DEP 18.1									
4	ID	24-HOUR TYPE IIA RAINFALL DISTRIBUTION									
5	ID	FUTURE DEVELOPMENT CONDITIONS WITH EXISTING AND PROPOSED DETENTION									
6	ID	5 AND 100-YEAR STORMS 24HOUR TYPE IIA									
7	ID	KIOWA ENGINEERING CORPORATION FILENAME EFSRDET.DAT									
	*DIAGRAM										
8	IT	5	0	0	288						
9	IO	5									
10	JR	PREC	.56	1.0							
11	KK	PKR3									
12	KM	PARKER DESIGN POINT 3 (BASINS 1 2 AND 3)									

EAST FORK WY DESIGN

13	IN	15									
14	PB	4.1									
15	PC	0.0	.0005	.0015	.0030	.0045	.0060	.0080	.0100	.0120	.0143
16	PC	.0165	.0198	.0210	.0233	.0255	.0278	.0320	.0390	.0460	.0530
17	PC	.0600	.0750	.1000	.4000	.7000	.7250	.7500	.7650	.7800	.7900
18	PC	.8000	.8100	.8200	.8250	.8300	.8350	.8400	.8450	.8500	.8550
19	PC	.8600	.8638	.8675	.8713	.8750	.8788	.8825	.8863	.8900	.8938
20	PC	.8975	.9013	.9050	.9083	.9115	.9148	.9180	.9210	.9240	.9270
21	PC	.9300	.9325	.9350	.9375	.9400	.9425	.9450	.9475	.9500	.9525
22	PC	.9550	.9575	.9600	.9625	.9650	.9675	.9700	.9725	.9750	.9775
23	PC	.9800	.9813	.9825	.9838	.9850	.9863	.9875	.9888	.9900	.9913
24	PC	.9963	.9975	.9988	1.0000						
25	BA	.2244									
26	LS	0	84.5								
27	UD	.38									

28	KK	RTPKR3									
29	KM	ROUTE PKR3 THRU PKR3A									
30	RK	2930	.024	.03	0	TRAP	5		4		
31	KK	PRK3A									
32	KM	PARKER DESIGN POINT 3A (HILL CIRCLE) PORTION OF PARKER BASIN 4									
33	BA	.134									
34	LS	0	83								
35	UD	.2									

36	KK	DP3A									
37	KM	COMBINE RTPKR3 AND PRK3A									
38	HC	2									

39	KK	RTDP3A									
40	KM	ROUTE DP3A THRU DP5A									
41	RK	1150	.018	.04	0	TRAP	10		.5		

42	KK	M6A									
43	KM	RUNOFF FROM SUB-BASIN M6A									
44	BA	.069									
45	LS	0	74								
46	UD	.12									

1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

47	KK	DP5A									
48	KM	COMBINE RTDP3A AND M6A									
49	HC	2									
50	KK	DB5A									
51	KM	ROUTE FLOWS THRU DP5A THROUGH DET DET BASIN 5A (48" RCP OUTLET)									
52	RS	1	ELEV 6398.2								
53	SQ	0	10	24	73	115	148	180	1500		

94	KK	RD17.1							
95	KM		ROUTE DP 17.1 TO DP 17.2						
96	RK	800	.04	.030	0	TRAP	8	1	
97	KK	M17A							
98	KM		RUNOFF FROM SUB-BASIN M17A						
99	BA	.0386							
100	LS	0	89						
101	UD	.17							
102	KK	DP17.2							
103	KM		COMBINE RUNOFF FROM SUB-BASIN M17.2 AND RD17.1						
104	HC	2							
105	KK	RD17.2							
106	KM		ROUTE DP 17.2 TO DP 18.1						
107	RK	1000	.035	.03	0	TRAP	8	3	
108	KK	M18A							
109	KM		RUNOFF FROM SUB-BASIN M18A						
110	BA	.0354							
111	LS	0	50						
112	UD	.15							
113	KK	M18B							
114	KM		RUNOFF FROM SUB-BASIN M18B						
115	BA	.0206							
116	LS	0	60						
117	UD	.146							
118	KK	DP18.1							
119	KM		COMBINE SUB-BASIN M18A, M18B AND RD17.2						
120	HC	3							
121	KK	DB18							
122	KM		ROUTE DP 18.1 THROUGH DETENTION BASIN DB18						
123	RS	1	ELEV	6223					
124	SQ	0	75	150	160	175	180		
125	SV	0	.1	1.1	1.9	2.8	4.1		
126	SE	6223	6224	6230	6232	6234	6236		
127	KK	RD18.1							
128	KM		ROUTE OUTFLOW FROM DB 18 TO DP 18.2						
129	RK	1600	.031	.03	0	TRAP	8	2	

HEC-1 INFUT

PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

130	KK	M18C							
131	KM		RUNOFF FROM SUB-BASIN M18C						

132	BA	.0314				
133	LS	0	80			
134	UD	.186				
135	KK	RM18C				
136	KM	ROUTE SUB-BASIN M18C TO DP18.2				
137	RK	520	.05	.013	CIRC	3
138	KK	M18D				
139	KM	RUNOFF FROM SUB BASIN M18D				
140	BA	.0386				
141	LS	0	82			
142	UD	.125				
143	KK	DP18.2				
144	KM	COMBINE SUB-BASIN SUBBASIN M18D, RM18C AND RD18.1				
145	HC	3				
146	ZZ					

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
LINE		
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
11	PKR3	
	V	
	V	
28	RTPKR3	
	.	
31	PRK3A	
	.	
	.	
36	DP3A.....	
	V	
	V	
39	RTDP3A	
	.	
42	M6A	
	.	
	.	
47	DP5A.....	
	V	
	V	
50	DB5A	
	V	
	V	
56	RTDB5A	
	.	
	.	

59	.	M5	
	.	.	
64	.	.	M6
	.	.	
69	DP5	
	V		
	V		
72	DB5B		
	V		
	V		
83	RDB5B		
	.		
86	.	M17B	
	.	.	
91	DP17.1	
	V		
	V		
94	RD17.1		
	.		
97	.	M17A	
	.	.	
	.	.	
102	DP17.2	
	V		
	V		
105	RD17.2		
	.		
108	.	M18A	
	.	.	
113	.	.	M18B
	.	.	
	.	.	
118	DP18.1	
	V		
	V		
121	DB18		
	V		
	V		
127	RD18.1		
	.		
	.		
130	.	M18C	
	.	V	
	.	V	
135	.	RM18C	

138 . . . M18D
. . .
143 DF18.2.....

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
*
* RUN DATE 09SEP08 TIME 12:03:07 *
*

*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*

MESA DRAINAGE BASIN
SENTINEL RIDGE MASTER DEVELOPMENT DRAINAGE PLAN
EAST FORK BRANCH WITH DETENTION AT DEP 18.1
24-HOUR TYPE IIA RAINFALL DISTRIBUTION
FUTURE DEVELOPMENT CONDITIONS WITH EXISTING AND PROPOSED DETENTION
5 AND 100-YEAR STORMS 24HOUR TYPE IIA
KIOWA ENGINEERING CORPORATION FILENAME EFSRDET.DAT

9 IO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 5 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 288 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 1 0 ENDING DATE
NDTIME 2355 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .03 HOURS
TOTAL TIME BASE 23.92 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND

STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .56 1.00

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

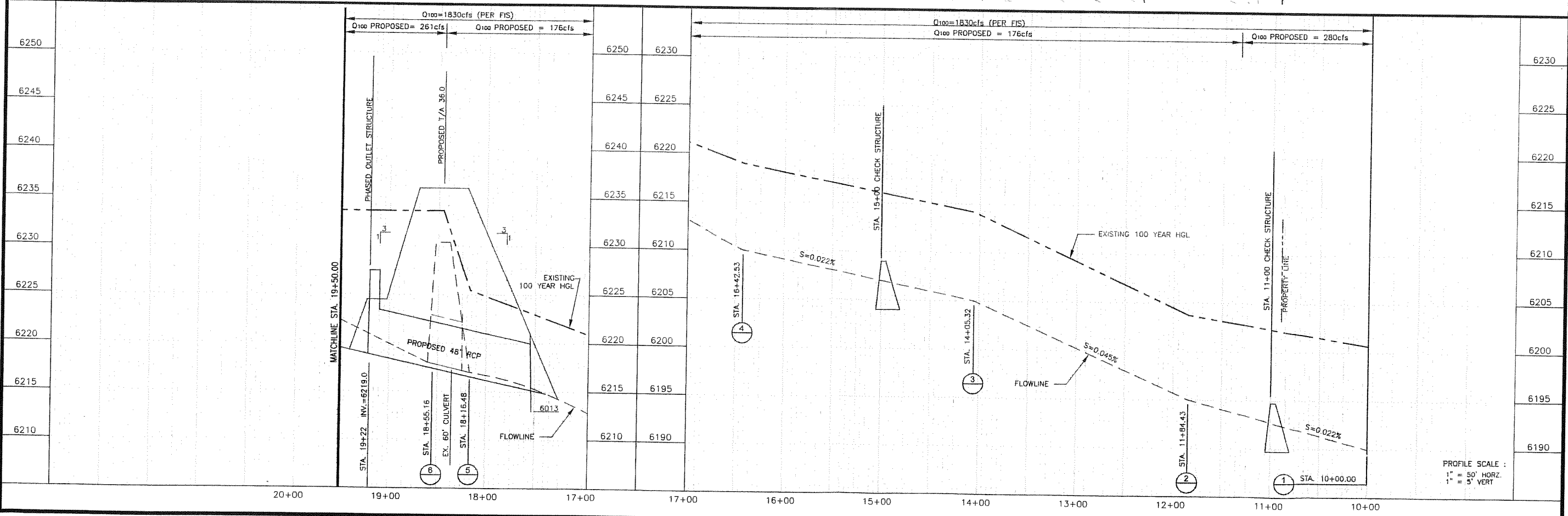
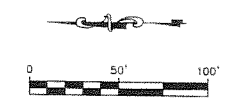
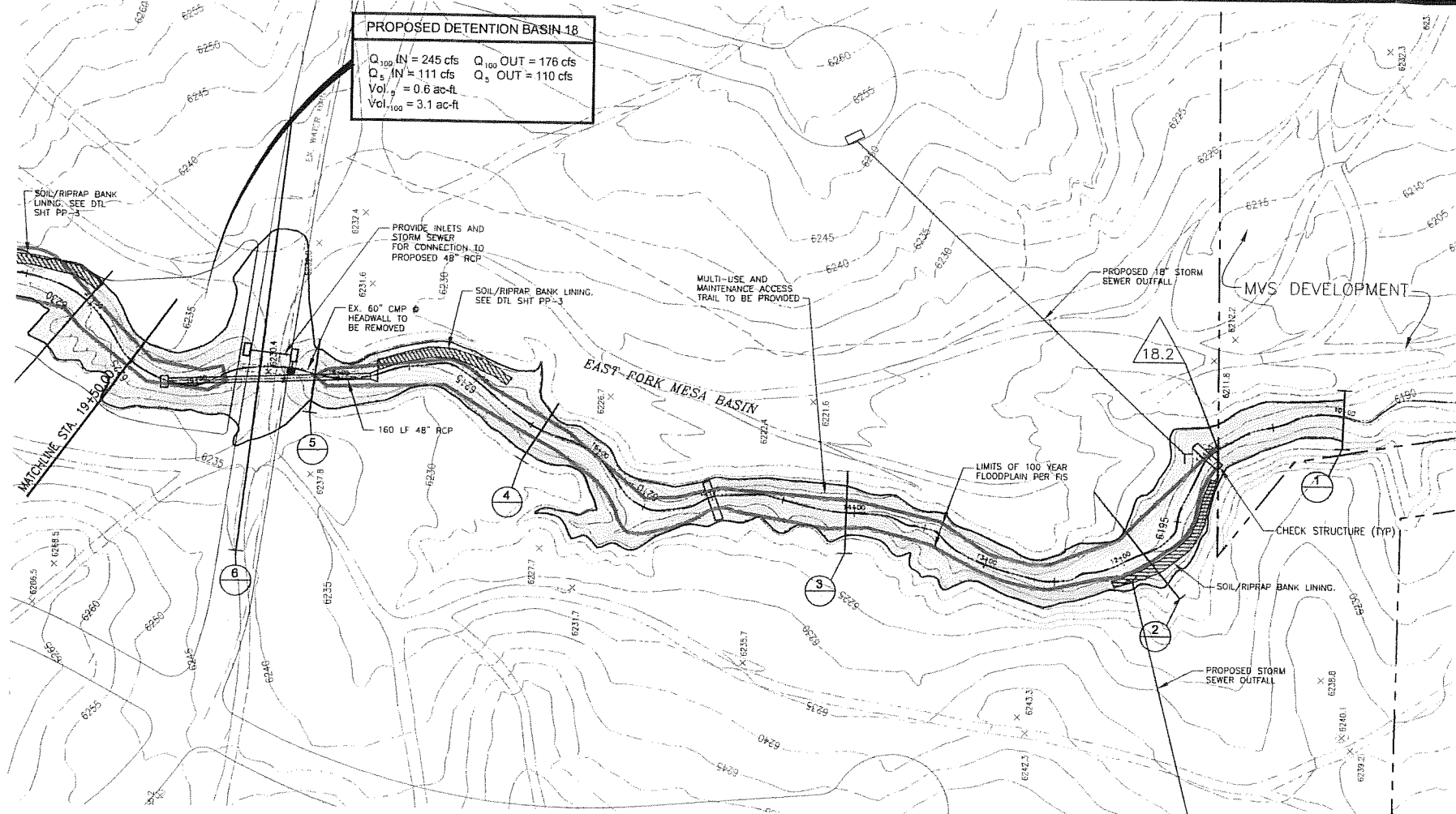
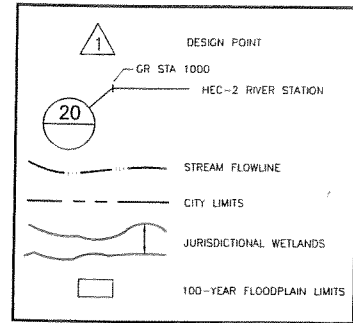
OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	PKR3	.22	1	FLOW	118.
				TIME	6.25
					321.
					6.25
ROUTED TO					
+	RTPKR3	.22	1	FLOW	116.
				TIME	6.33
					318.
					6.25
HYDROGRAPH AT					
+	PRK3A	.13	1	FLOW	90.
				TIME	6.08
					247.
					6.08
2 COMBINED AT					
+	DP3A	.36	1	FLOW	176.
				TIME	6.17
					503.
					6.17
ROUTED TO					
+	RTDP3A	.36	1	FLOW	172.
				TIME	6.25
					498.
					6.17
HYDROGRAPH AT					
+	M6A	.07	1	FLOW	26.
				TIME	6.08
					100.
					6.00
2 COMBINED AT					
+	DP5A	.43	1	FLOW	186.
				TIME	6.17
					553.
					6.17
ROUTED TO					
+	DB5A	.43	1	FLOW	138.
				TIME	6.42
					595.
					6.17

** PEAK STAGES IN FEET **

			1	STAGE	6405.40	6408.63
				TIME	6.42	6.17
ROUTED TO						
+	RTDB5A	.43	1	FLOW	138.	564.
				TIME	6.50	6.17
HYDROGRAPH AT						
+	M5	.10	1	FLOW	49.	144.
				TIME	6.17	6.17
HYDROGRAPH AT						
+	M6	.02	1	FLOW	11.	31.
				TIME	6.08	6.00
3 COMBINED AT						
+	D25	.54	1	FLOW	176.	729.
				TIME	6.25	6.17
ROUTED TO						
+	DB5B	.54	1	FLOW	106.	168.
				TIME	6.92	7.17
** PEAK STAGES IN FEET **						
			1	STAGE	6379.65	6390.40
				TIME	6.92	7.17
ROUTED TO						
+	RDB5B	.54	1	FLOW	106.	168.
				TIME	6.92	7.17
HYDROGRAPH AT						
+	M17B	.03	1	FLOW	24.	64.
				TIME	6.00	6.00
2 COMBINED AT						
+	DP17.1	.57	1	FLOW	107.	171.
				TIME	6.92	7.08
ROUTED TO						
+	RE17.1	.57	1	FLOW	107.	171.
				TIME	6.92	7.08
HYDROGRAPH AT						
+	M17A	.04	1	FLOW	40.	91.
				TIME	6.08	6.00
2 COMBINED AT						
+	DP17.2	.61	1	FLOW	111.	245.
				TIME	6.08	6.08
ROUTED TO						

+	RD17.2	.61	1	FLOW TIME	111. 6.17	243. 6.08
	HYDROGRAPH AT					
+	M18A	.04	1	FLOW TIME	0. 22.58	6. 6.08
	HYDROGRAPH AT					
+	M18B	.02	1	FLOW TIME	1. 6.08	12. 6.08
	3 COMBINED AT					
+	DP18.1	.67	1	FLOW TIME	111. 6.17	261. 6.08
	ROUTED TO					
+	DB18	.67	1	FLOW TIME	110. 7.08	176. 7.33
	** PEAK STAGES IN FEET **					
	1			STAGE TIME	6226.78 7.08	6234.42 7.33
	ROUTED TO					
+	RD18.1	.67	1	FLOW TIME	110. 7.08	176. 7.33
	HYDROGRAPH AT					
+	M18C	.03	1	FLOW TIME	18. 6.08	53. 6.08
	ROUTED TO					
+	RM18C	.03	1	FLOW TIME	17. 6.08	53. 6.08
	HYDROGRAPH AT					
+	M18D	.04	1	FLOW TIME	28. 6.00	78. 6.00
	3 COMBINED AT					
+	DP18.2	.74	1	FLOW TIME	127. 6.08	280. 6.08
1						

*** NORMAL END OF HEC-1 ***



PROFILE SCALE :
 1" = 50' HORIZ.
 1" = 5' VERT

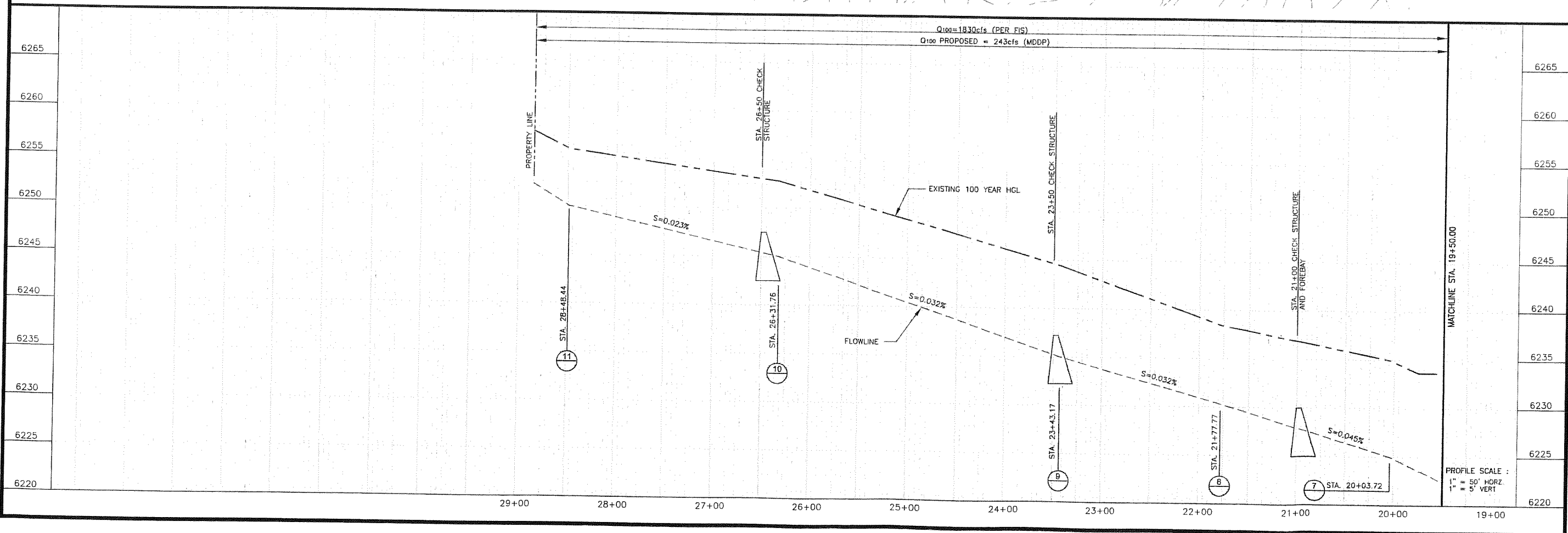
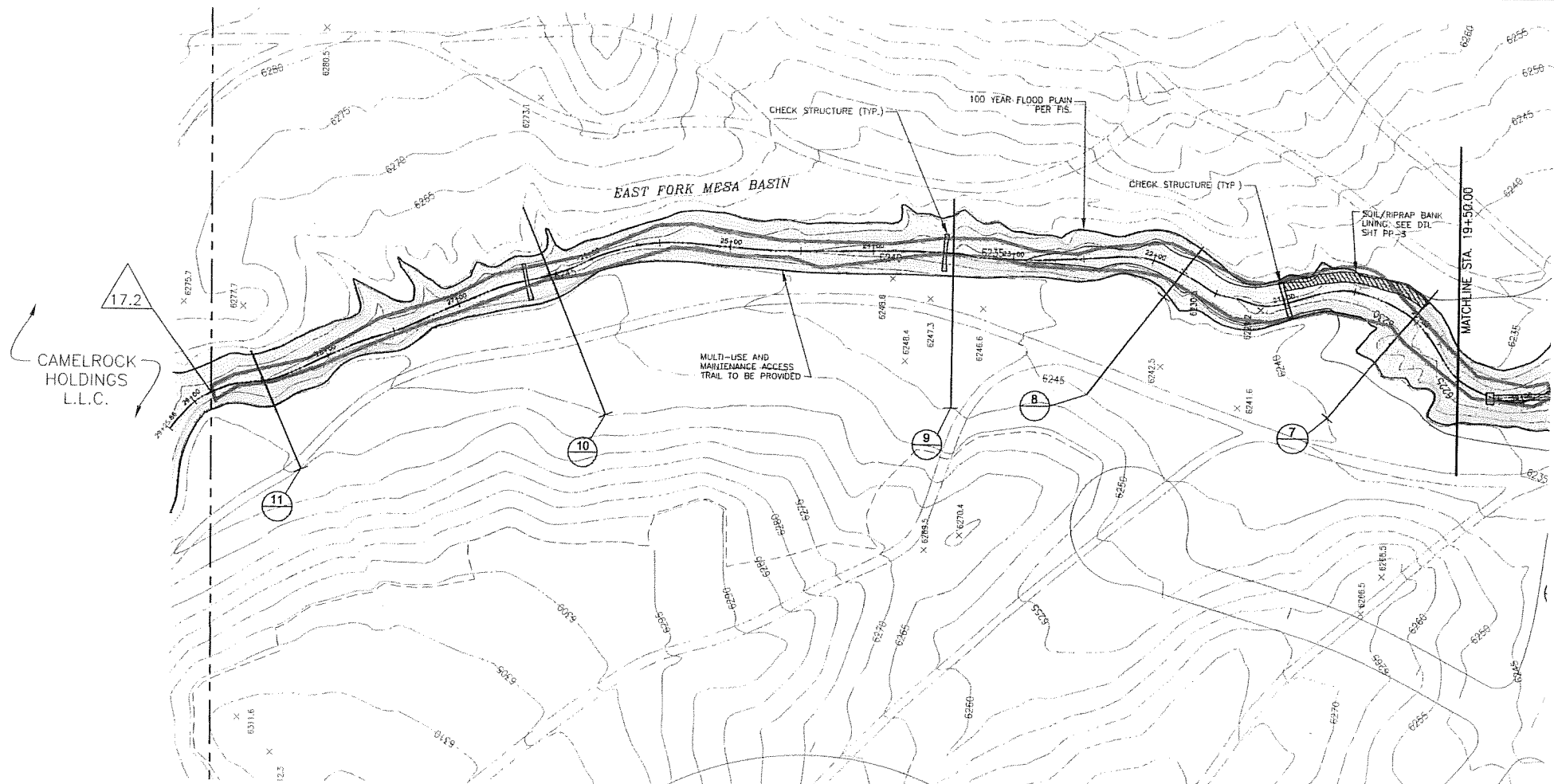
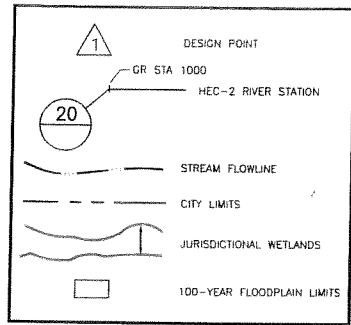
Kiowa Engineering Corporation
 1604 South 21st Street
 Colorado Springs, Colorado 80904
 (719) 630-7342

SENTINEL RIDGE
MASTER DEVELOPMENT DRAINAGE PLAN
EAST FORK MESA BASIN PLAN AND PROFILE
 COLORADO SPRINGS, COLORADO

Project No.:	07028
Date:	SEPTEMBER 2008
Design:	RNW
Drawn:	MFA
Check:	RNW
Revisions:	

SHEET
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 OF X SHEETS

07028-PP1-4.dwg/01 01, 2008

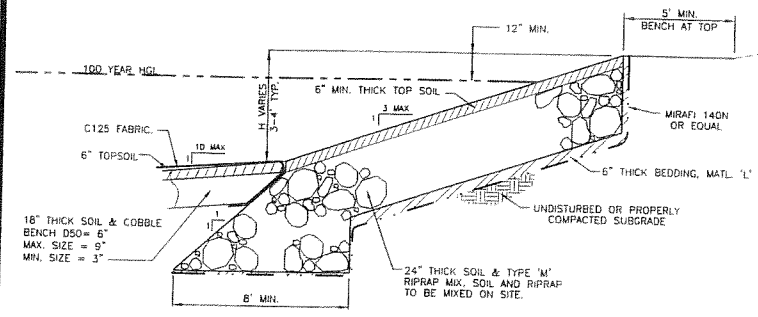


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 1604 South 21st Street
 Colorado Springs, Colorado 80904
 (719) 630-7342

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MASTER DEVELOPMENT DRAINAGE PLAN
EAST FORK MESA BASIN PLAN AND PROFILE
 COLORADO SPRINGS, COLORADO

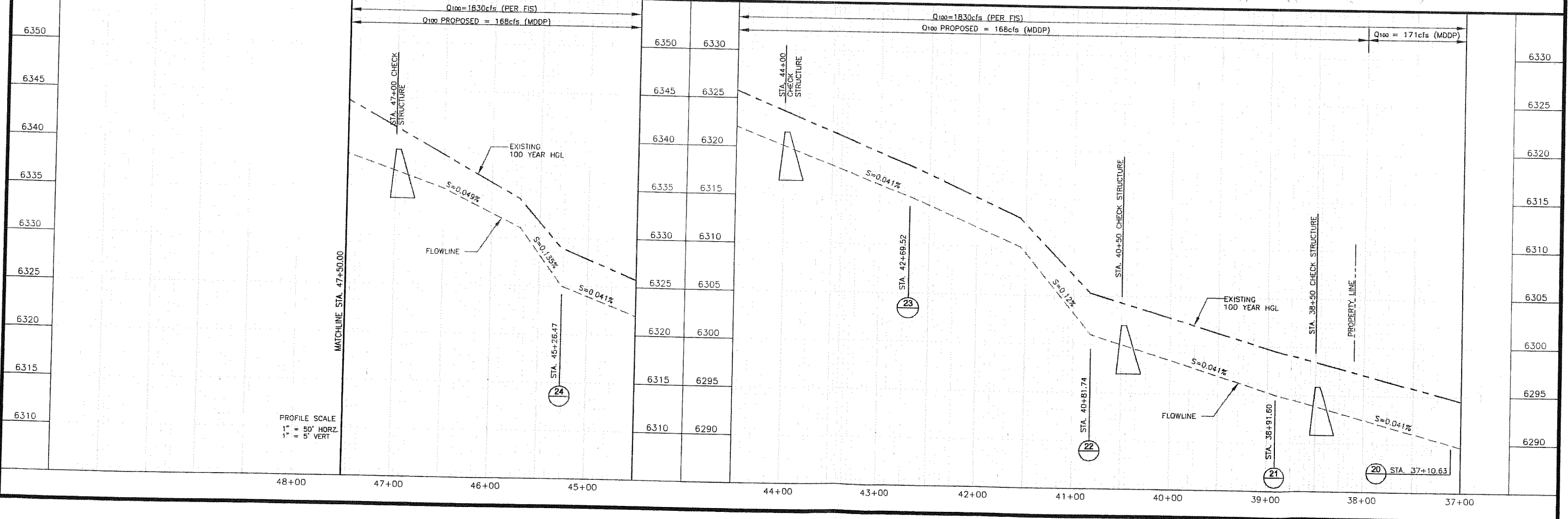
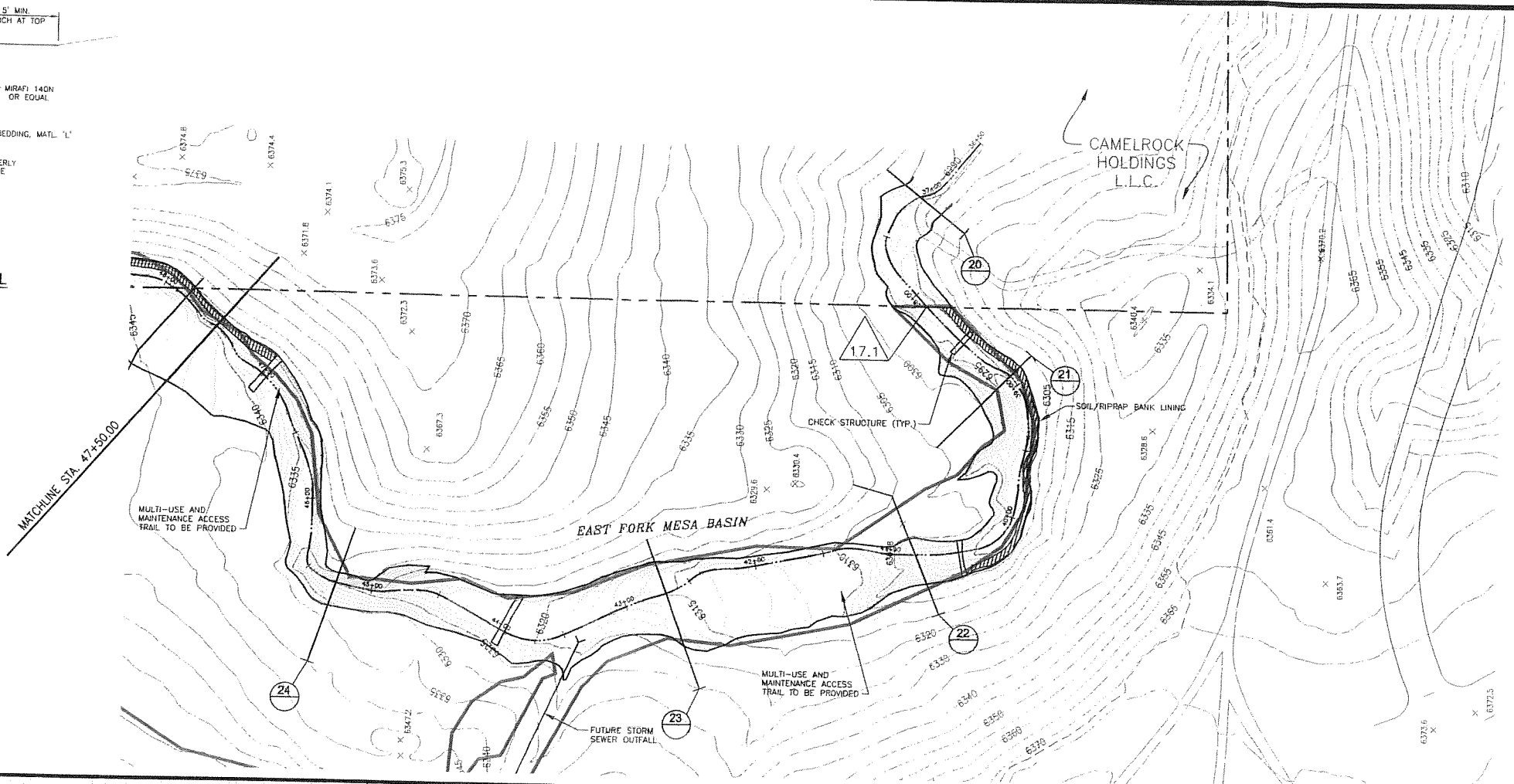
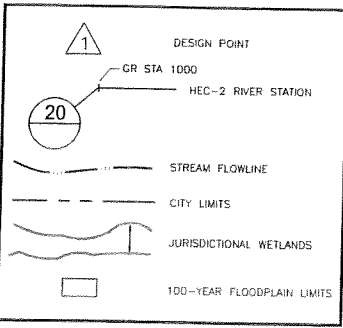
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TYPICAL CHANNEL BANK LINING DETAIL
SCALE: 1/4" = 1'

- SOIL/RIPRAP NOTES:**
1. SOIL USED TO MIX WITH RIPRAP SHALL BE CLEAN, WELL GRADED NATIVE SOIL FREE OF ROOTS, DEBRIS AND OTHER DELETERIOUS MATERIALS. STOCKPILE OF SOIL TO BE USED FOR SOIL/RIPRAP BANK LININGS TO BE APPROVED BY THE ENGINEER.
 2. SOIL SHALL BE MIXED WITH RIPRAP AND STOCKPILED PRIOR TO PLACEMENT. SOIL/RIPRAP STOCKPILE TO BE APPROVED BY ENGINEER.
 3. NO MORE THAN 25% OF THE VOLUME OF THE SOIL/RIPRAP MIXTURE SHALL BE CLEAN NATIVE SOIL MATERIAL.

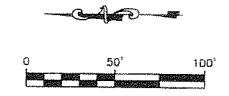
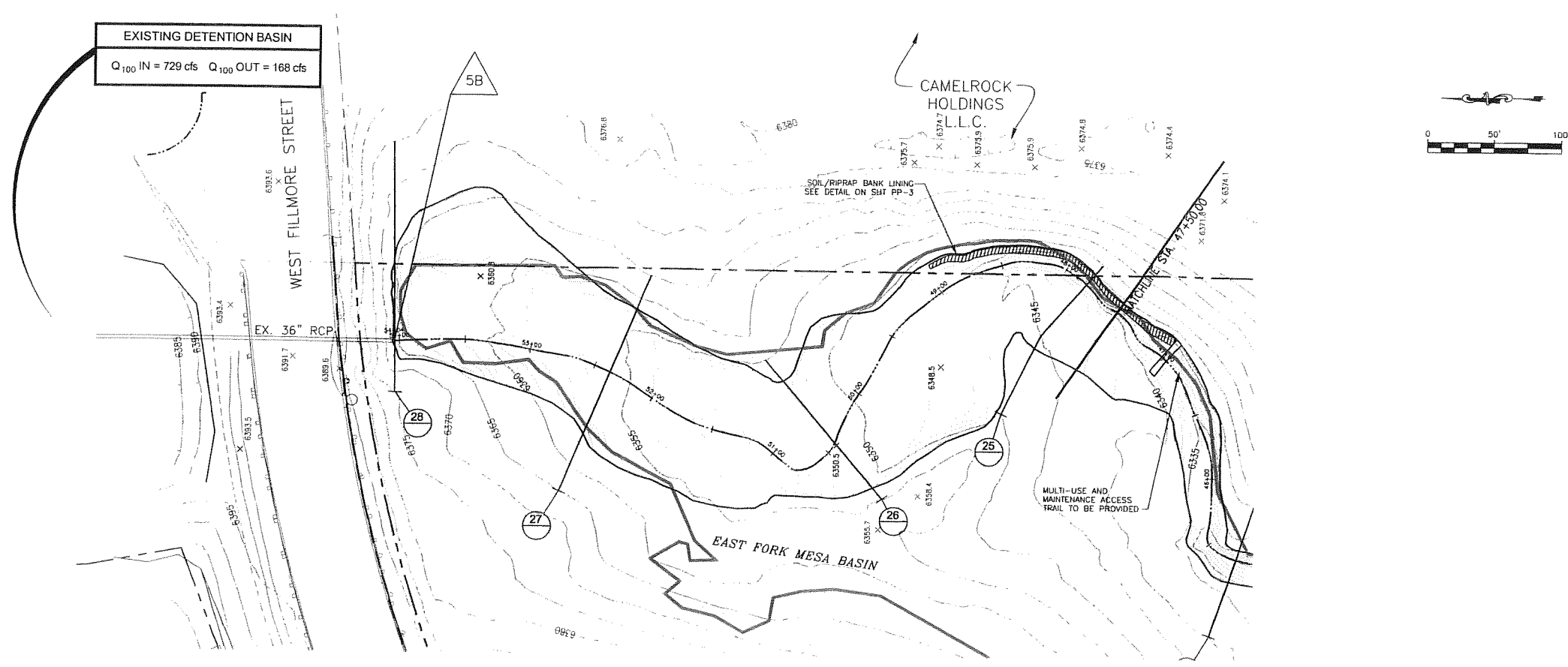
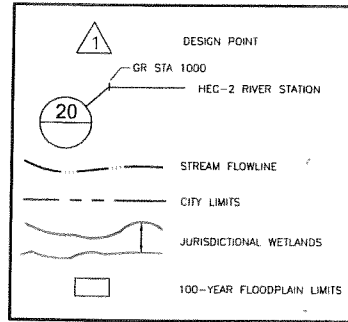


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MASTER DEVELOPMENT DRAINAGE PLAN
EAST FORK MESA BASIN PLAN AND PROFILE
COLORADO SPRINGS, COLORADO

Project No.:	0702B
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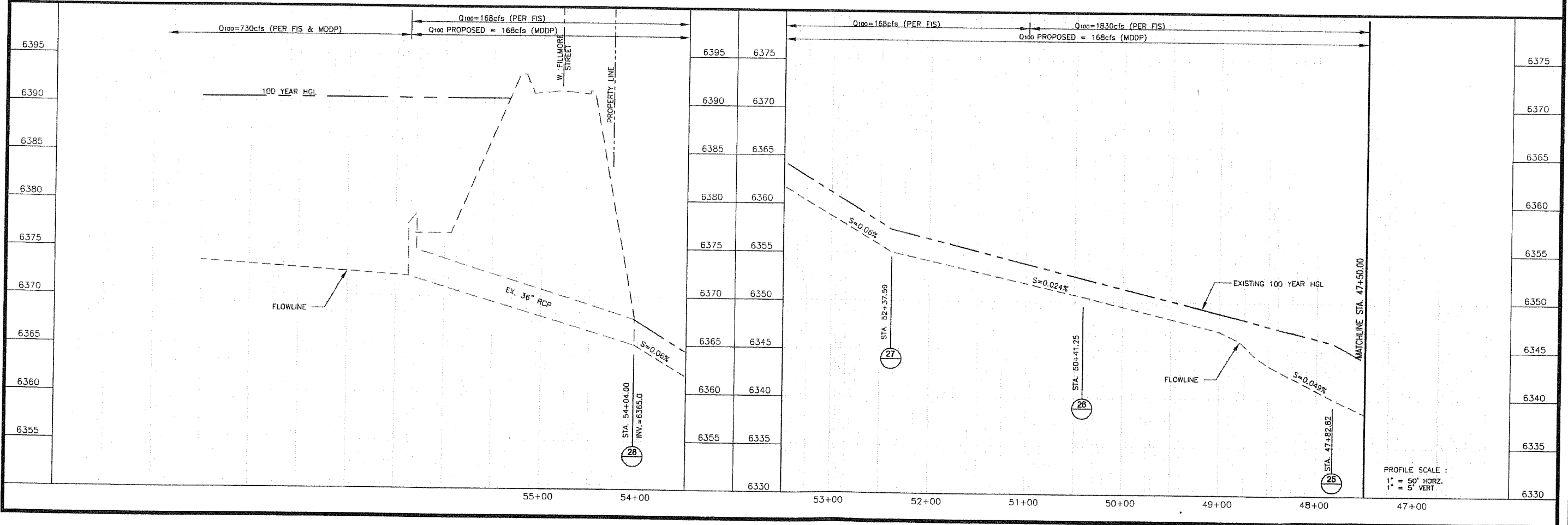


EXISTING DETENTION BASIN
 $Q_{100} \text{ IN} = 729 \text{ cfs}$ $Q_{100} \text{ OUT} = 168 \text{ cfs}$

CAMELROCK HOLDINGS L.L.C.

EAST FORK MESA BASIN

MULTI-USE AND MAINTENANCE ACCESS TRAIL TO BE PROVIDED



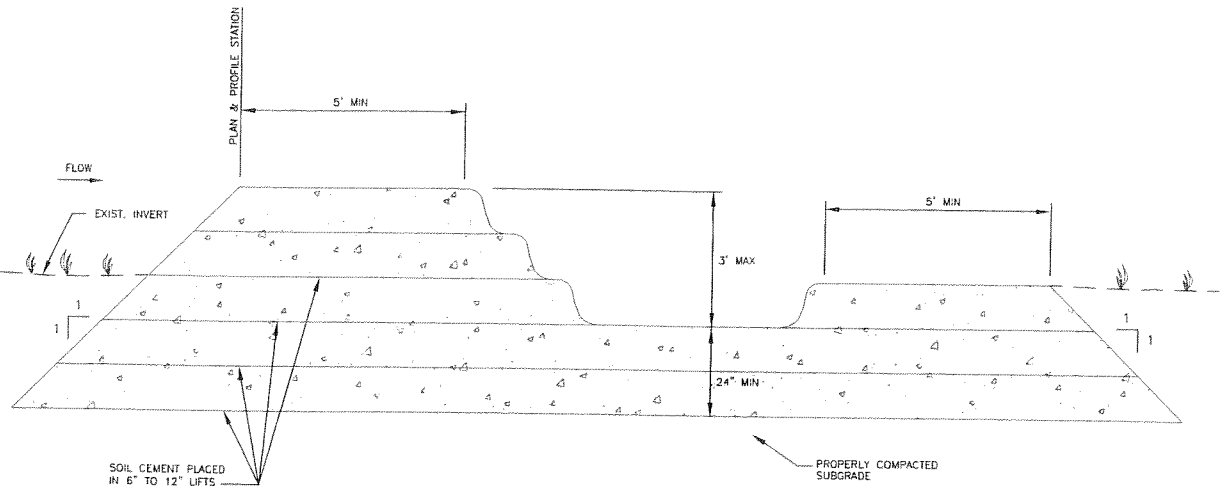
PROFILE SCALE :
 1" = 50' HORZ.
 1" = 5' VERT.

SENTINEL RIDGE
 MASTER DEVELOPMENT DRAINAGE PLAN
 EAST FORK MESA BASIN PLAN AND PROFILE
 COLORADO SPRINGS, COLORADO

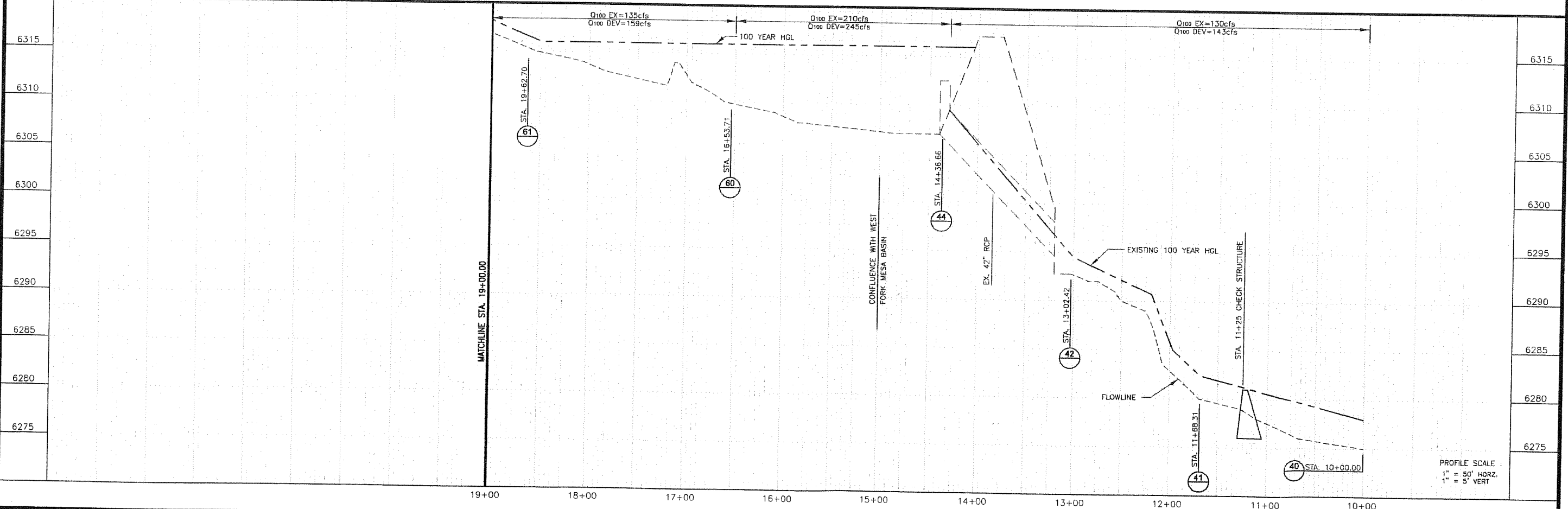
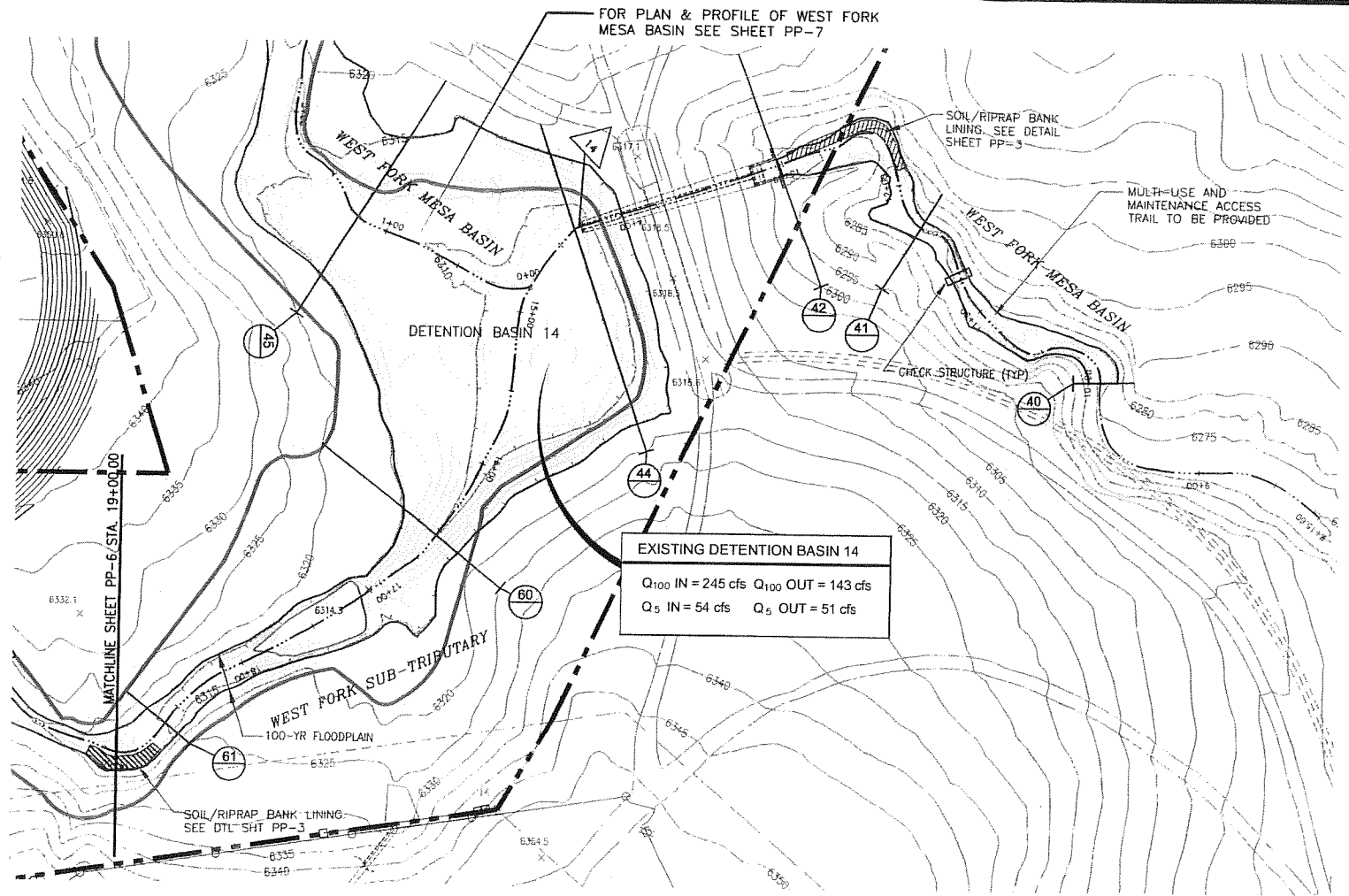
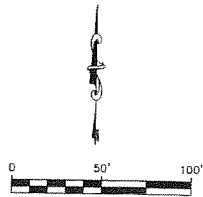
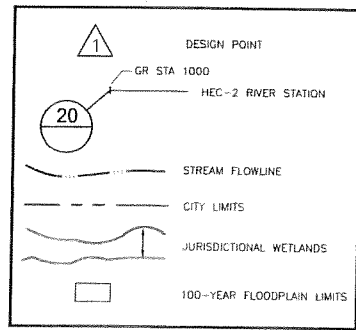
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CHECK STRUCTURE DETAIL
TYPICAL
SCALE: 1"=2'-0"



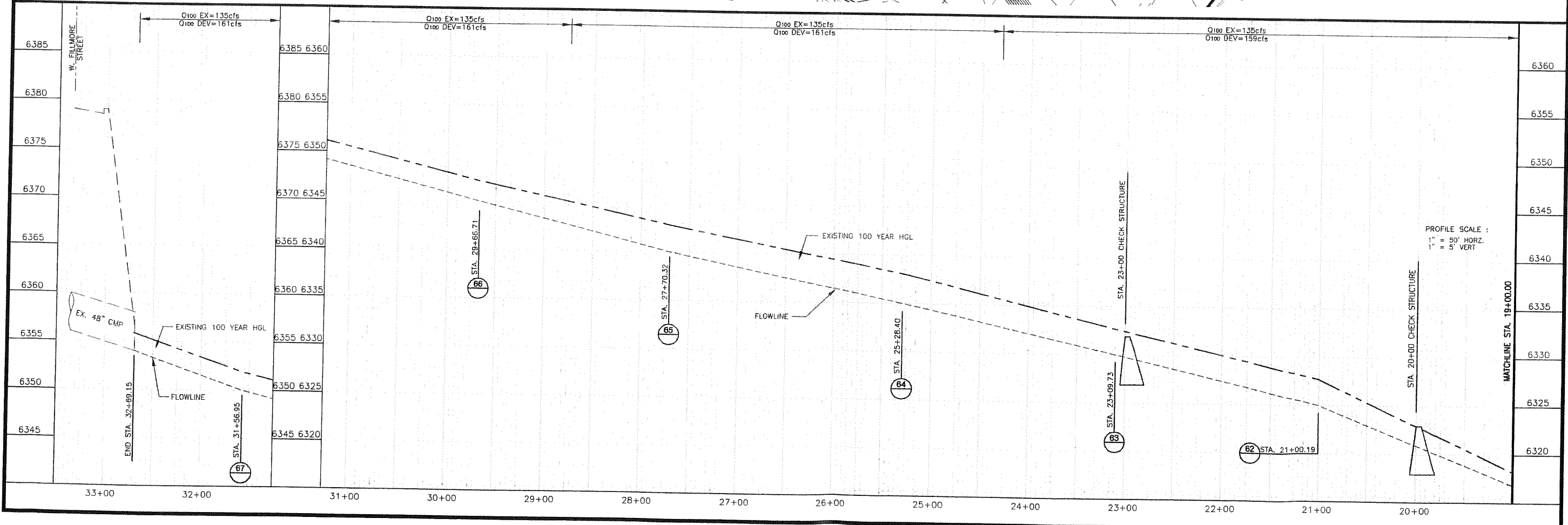
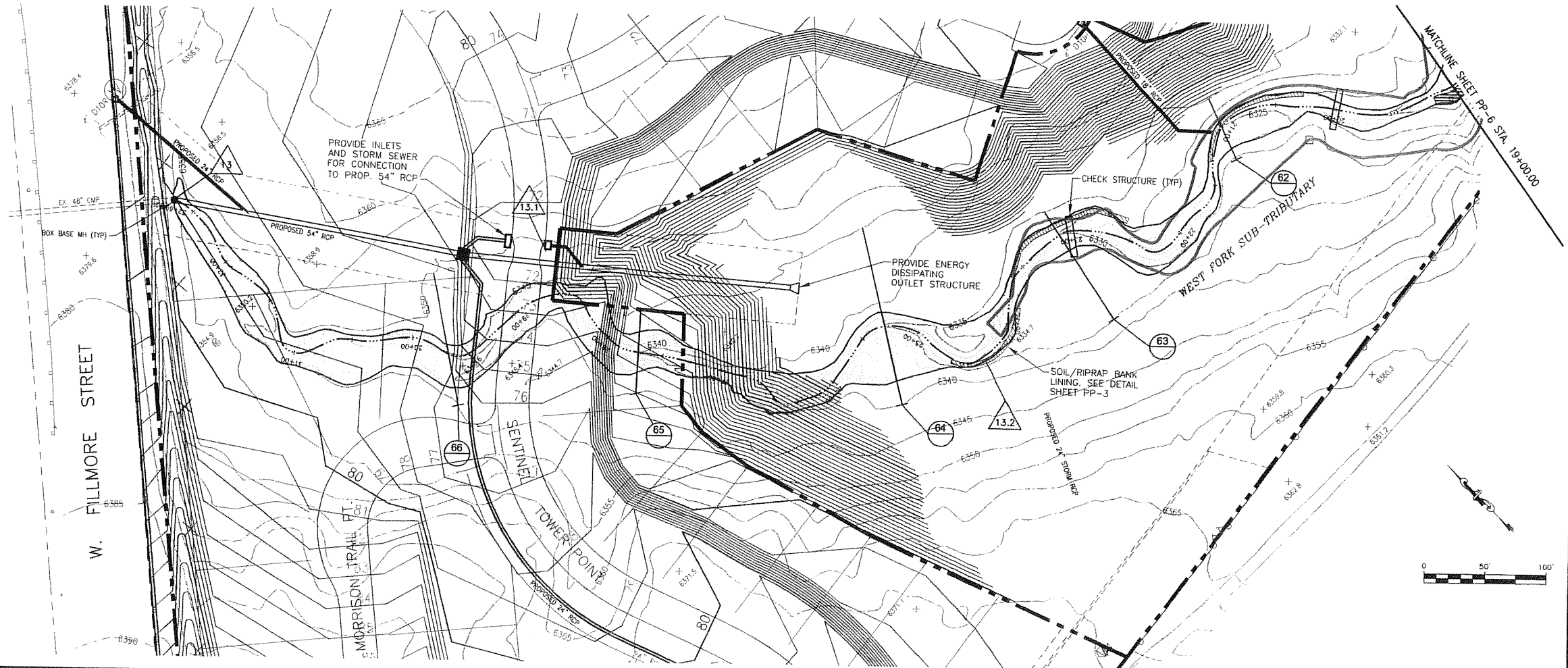
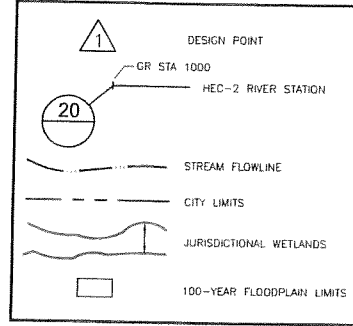
PROFILE SCALE:
1" = 50' HORZ.
1" = 5' VERT

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SENTINEL RIDGE
MASTER DEVELOPMENT DRAINAGE PLAN
WEST FORK SUB-TRIBUTARY MESA BASIN
PLAN AND PROFILE
COLORADO SPRINGS, COLORADO

Project No.: 07028
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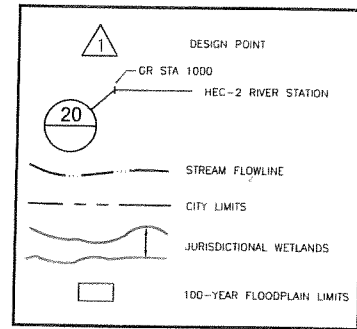


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WEST FORK SUB-TRIBUTARY MESA BASIN
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 COLORADO SPRINGS, COLORADO

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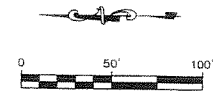


PROVIDE INLETS AND STORM SEWERS FOR CONNECTION TO EXIST. 36" RCP

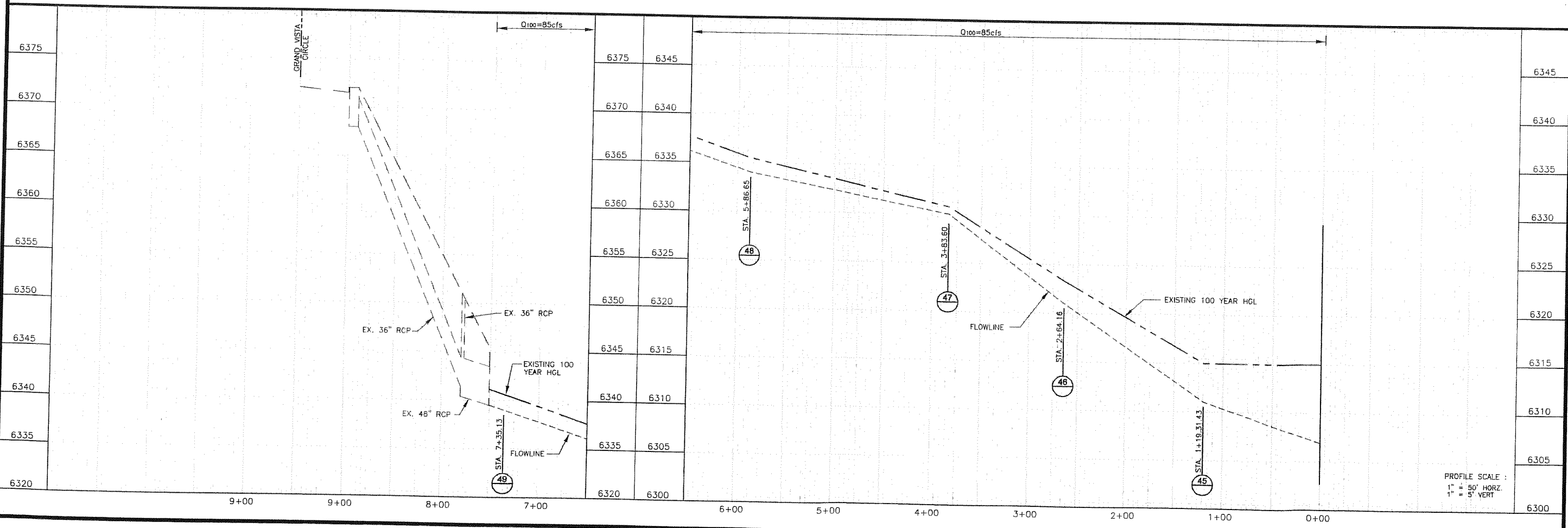
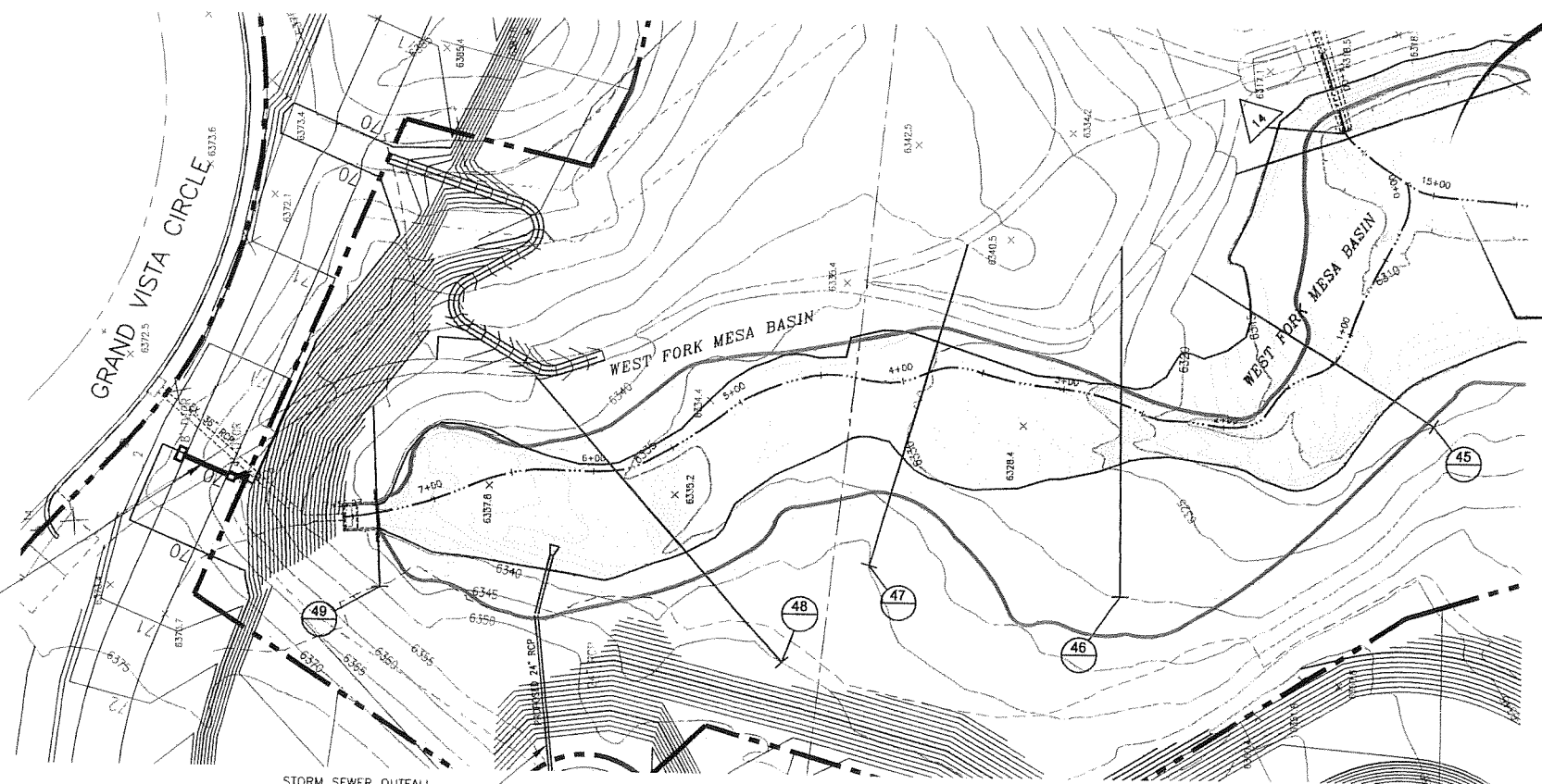
STORM SEWER OUTFALL FROM FILING 1 SUBDIVISION

EXISTING DETENTION BASIN 14

Q₁₀₀ IN = 245 cfs Q₁₀₀ OUT = 143 cfs
Q₅ IN = 54 cfs Q₅ OUT = 51 cfs



FOR PLAN & PROFILE OF WEST FORK SUB-TRIBUTARY SEE SHEETS PP-5 & PP-6



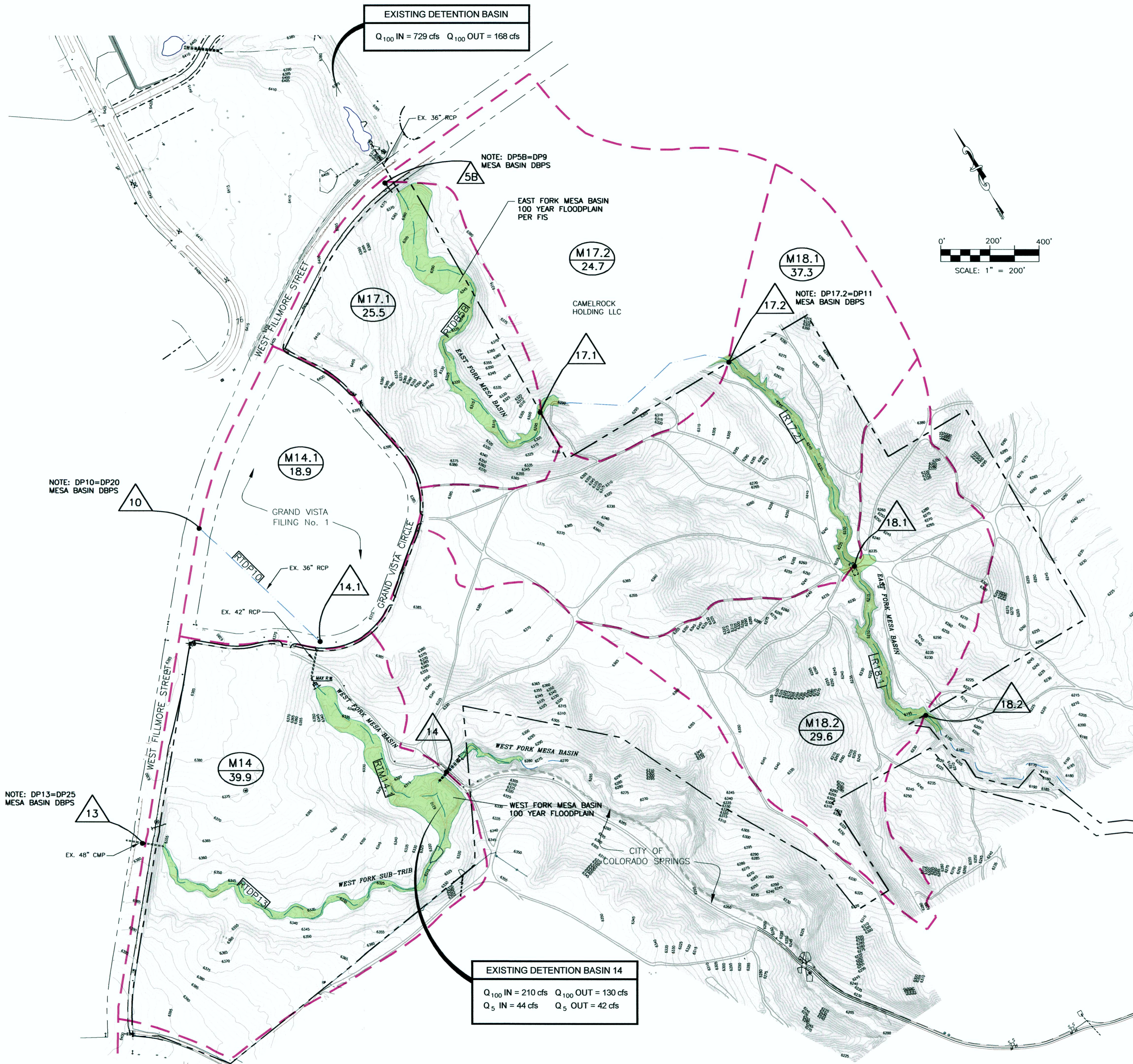
PROFILE SCALE :
1" = 50' HORZ.
1" = 5' VERT

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MASTER DEVELOPMENT DRAINAGE PLAN
WEST FORK MESA BASIN
PLAN AND PROFILE
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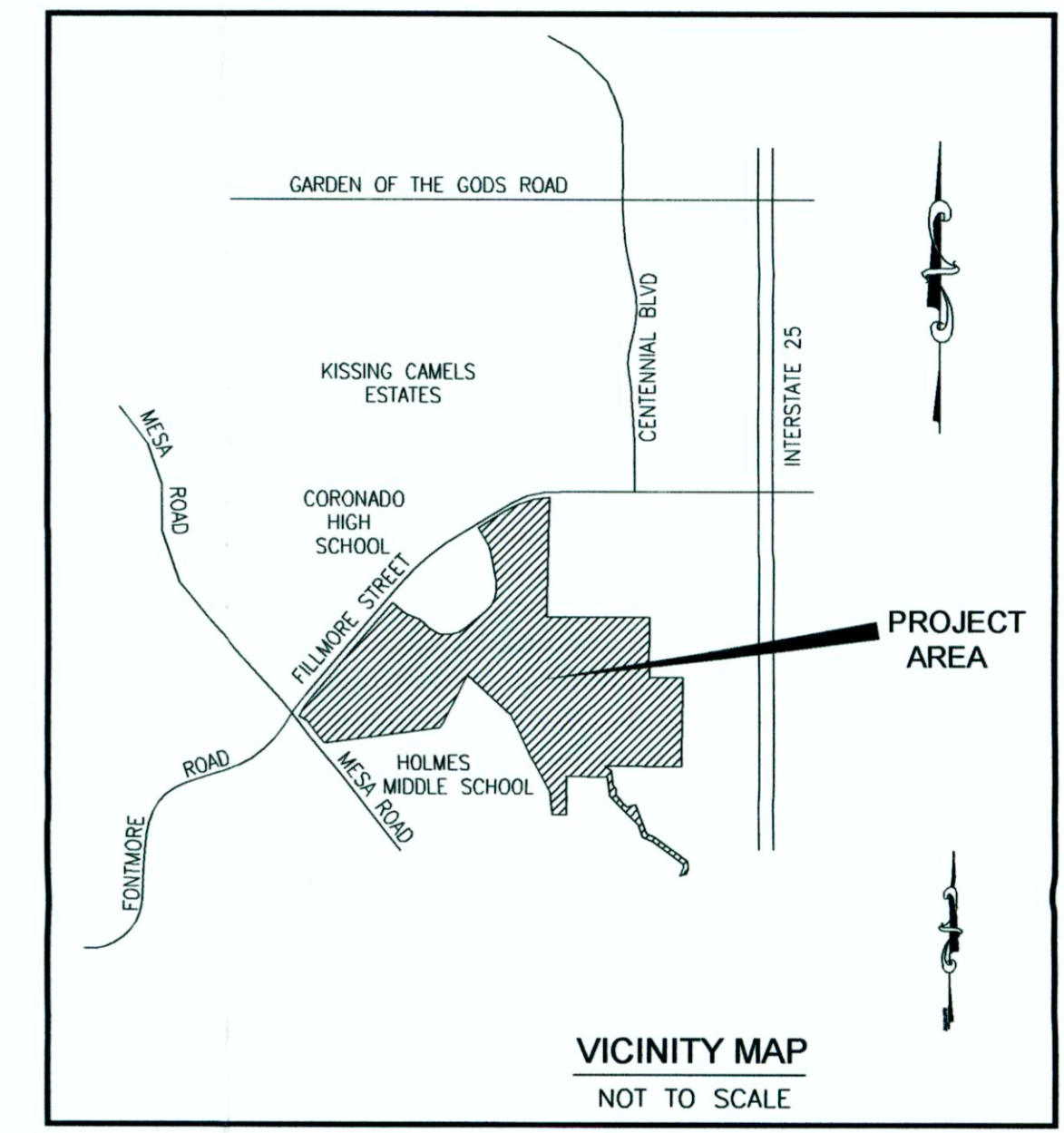
SHEET
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LEGEND

- R — SUB-BASIN DESIGNATION
- 10.4 ac — SUB-BASIN AREA
- 1 — DESIGN POINT
- — DRAINAGE BASIN BOUNDARY
- — STREAM INVERT
- R17.2 — HEC-1 ROUTING ELEMENT



DESIGN POINT DISCHARGES

DESIGN POINT	5-YEAR FLOW	100-YEAR FLOW
5B	106	168
10	17	61
3	25	135
4 (1)	44	210
4.1	28	82
17.1	107	172
17.2	108	177
18.1	107	189
18.2 (2)	111	279

(1) DP 14=DP 26 DBPS
(2) DP 18.1=DP 12 DBPS

SUB-BASIN DISCHARGES

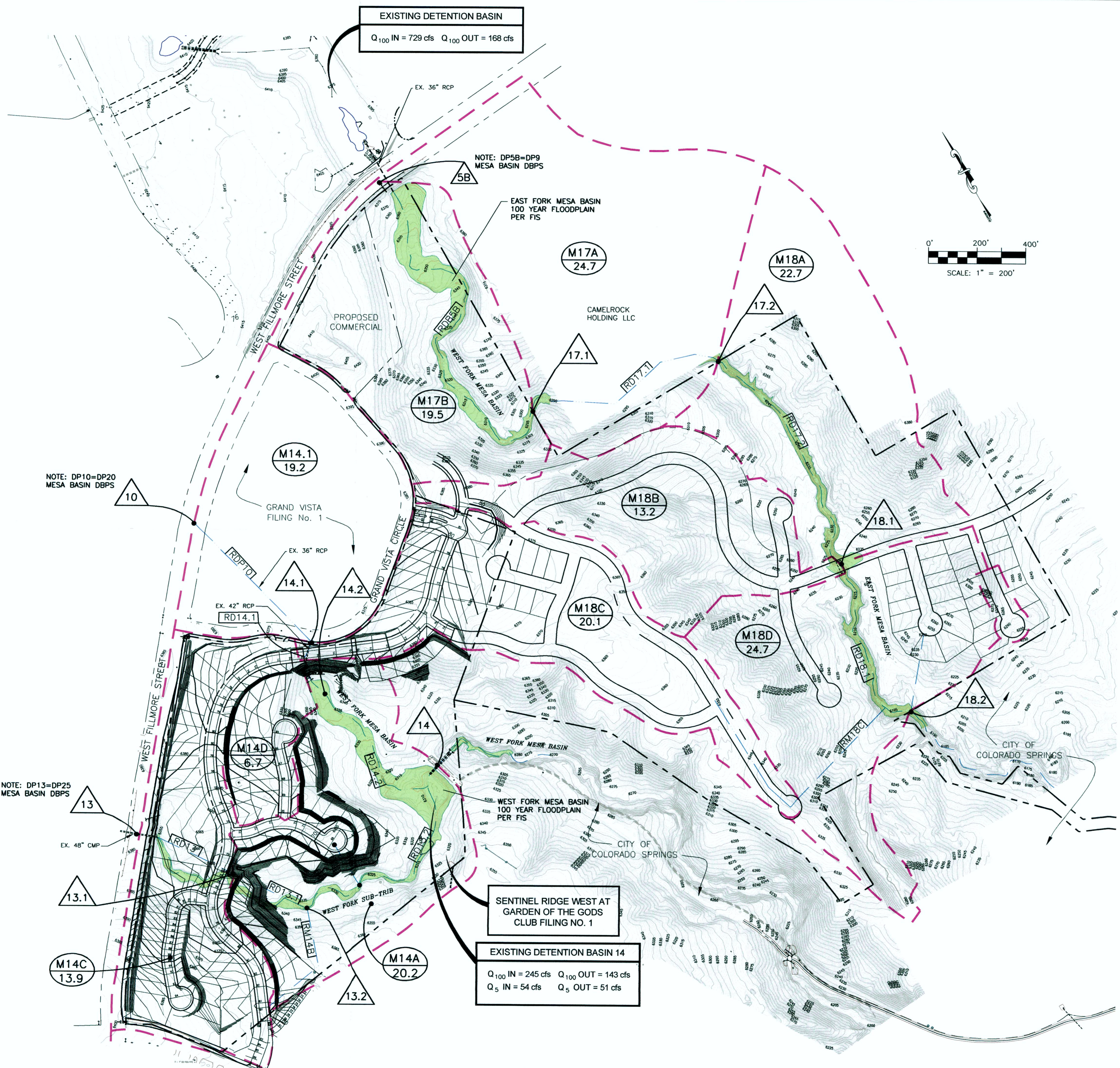
BASIN	Q ₅	Q ₁₀₀
M14	1	6
M14.1	18	35
M17.1	14	53
M17.2	1	23
M18.1	1	13
M18.2	43	110

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SENTINEL RIDGE
MASTER DEVELOPMENT DRAINAGE PLAN
SUB-BASIN MAP
EXISTING BASIN CONDITIONS
COLORADO SPRINGS, COLORADO,

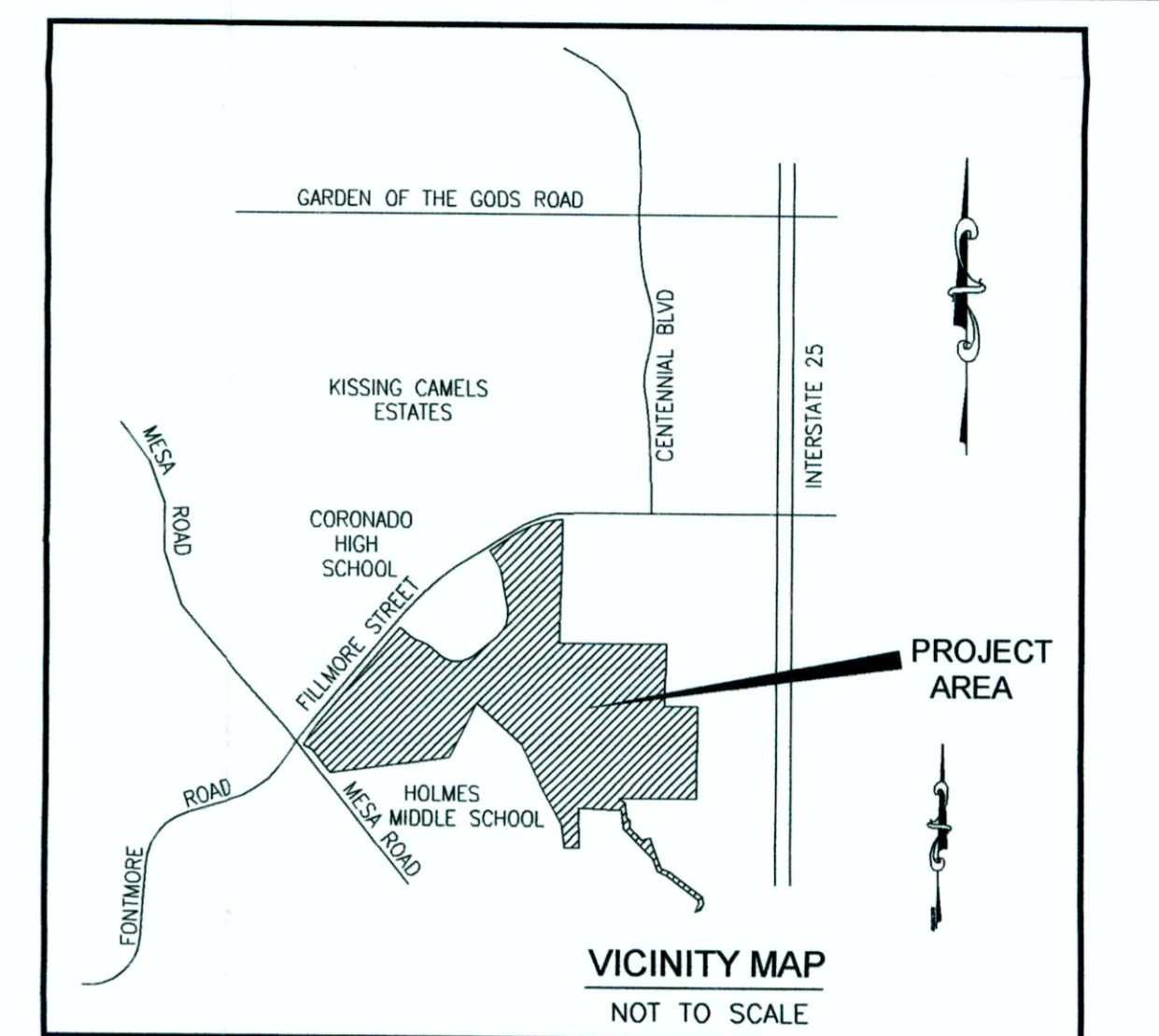
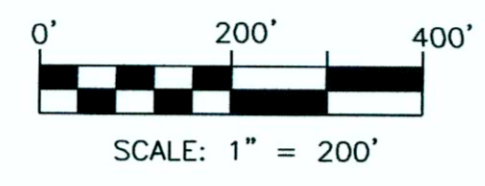
Project No.: 07028
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SHEET
EXH 1
OF X SHEETS



LEGEND

- R — SUB-BASIN DESIGNATION
- 10.4 ac — SUB-BASIN AREA
- △ — DESIGN POINT
- DRAINAGE BASIN BOUNDARY
- STREAM INVERT
- R17.2 — HEC-1 ROUTING ELEMENT



DESIGN POINT DISCHARGES W/O PROPOSED DETENTION

DESIGN POINT	5-YEAR FLOW	100-YEAR FLOW
5B	106	168
10	20	68
13	30	155
13.1	32	161
14 (1)	54	245
14.1	26	85
14.2	31	100
17.1	107	171
17.2	111	245
18.1 (2)	111	261
18.2	145	378

(1) DP 14=DP 26 DBPS
 (2) DP 18.1=DP 12 DBPS

SUB-BASIN DISCHARGES

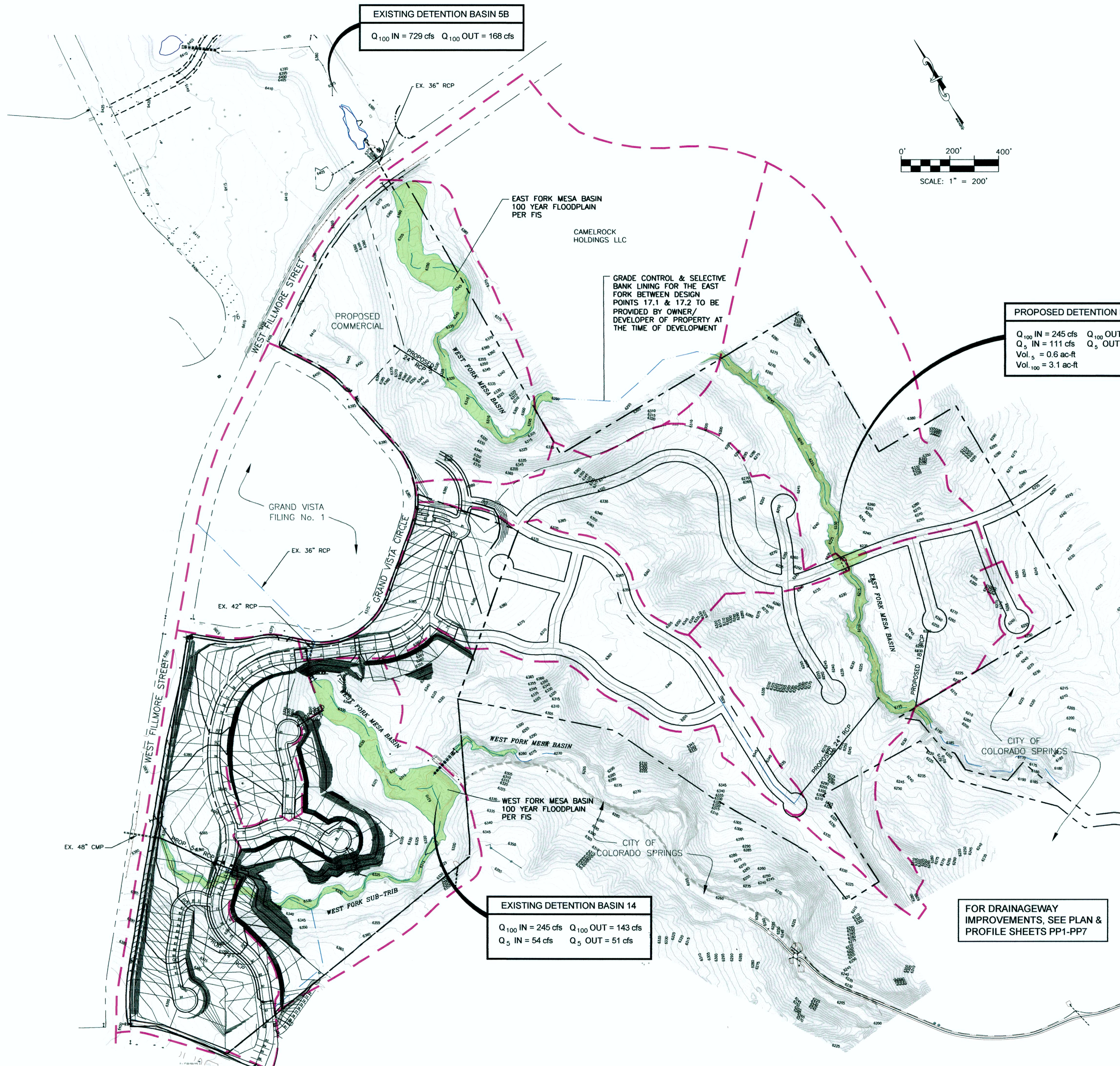
BASIN	Q ₅	Q ₁₀₀
M14.1	12	30
M14A	1	13
M14C	7	31
M14D	6	19
M17A	40	91
M17B	24	64
M18A	1	6
M18B	1	12
M18C	18	53
M18D	28	78

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MASTER DEVELOPMENT DRAINAGE PLAN
 SUB-BASIN MAP
 PROPOSED BASIN CONDITIONS
 COLORADO SPRINGS, COLORADO

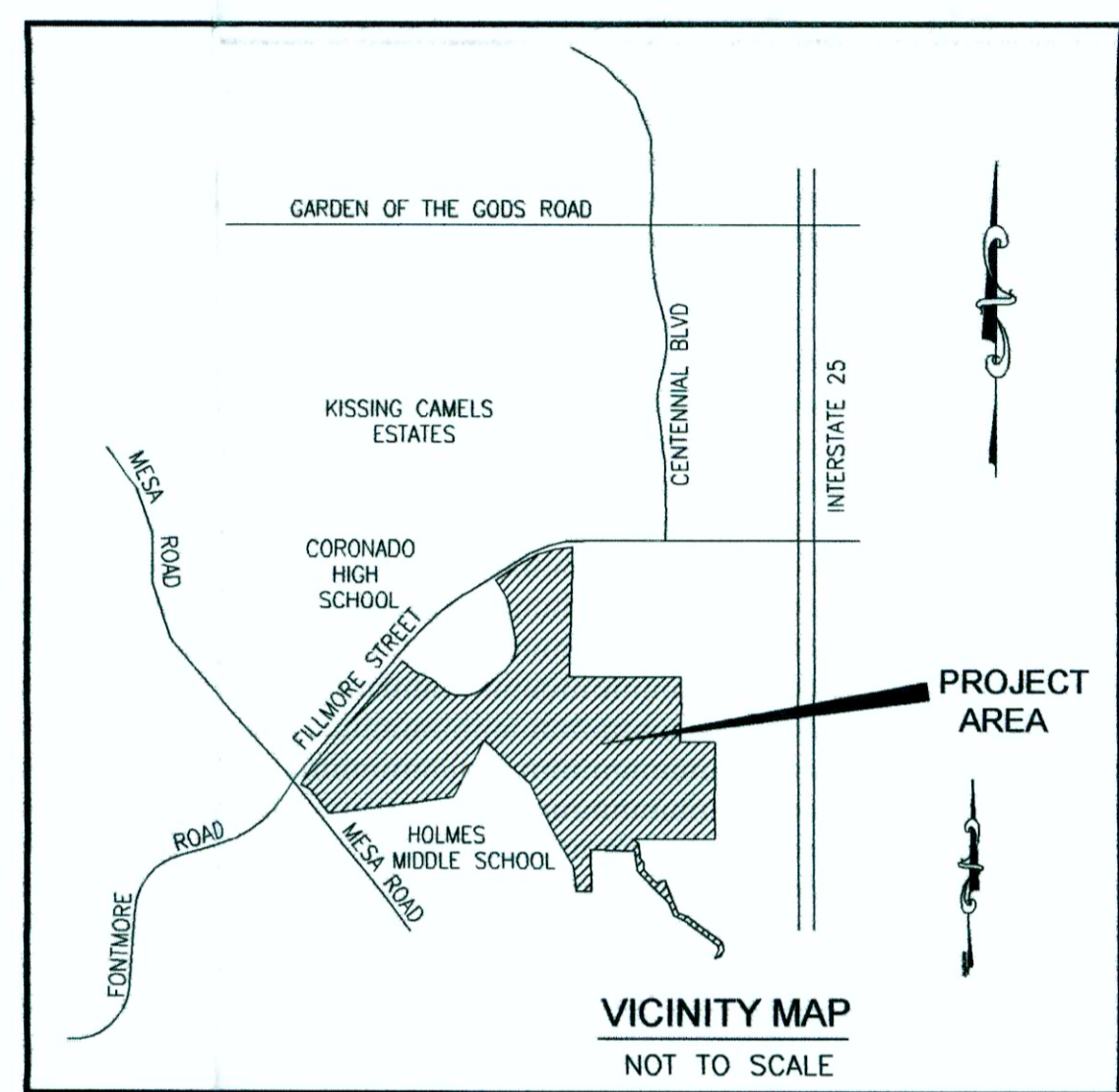
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SHEET
EXH 2
 OF X SHEETS



LEGEND

- SUB-BASIN DESIGNATION
- SUB-BASIN AREA
- DESIGN POINT
- DRAINAGE BASIN BOUNDARY
- STREAM INVERT
- HEC-1 ROUTING ELEMENT



**DESIGN POINT FLOWS
W/O PROPOSED DETENTION**

DESIGN POINT	5-YEAR FLOW	100-YEAR FLOW
5B	106	168
10	20	68
13	30	155
13.1	32	161
14 (1)	54	245
14.1	26	85
14.2	31	100
17.1	107	171
17.2	111	245
18.1	111	261
18.2	145	378

**DESIGN POINT FLOWS
WITH DETENTION**

DESIGN POINT	5-YEAR FLOW	100-YEAR FLOW
18.1	111	261
18 (1)	110	176
18.2	127	280

(1) OUTFLOW FROM EXISTING DETENTION BASIN

(1) OUTFLOW FROM PROPOSED DETENTION BASIN @ DP 18.1

FOR DRAINAGEWAY IMPROVEMENTS, SEE PLAN & PROFILE SHEETS PP1-PP7

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SENTINEL RIDGE
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PROPOSED FACILITIES
COLORADO SPRINGS, COLORADO

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EXH 3
OF X SHEETS