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#### Engineer's Statement:

This report and plan for the drainage design of True North Commons was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the City of Colorado Springs Drainage Criteria Manual and is in conformity with the master plan of the drainage basin. I understand that the City of Colorado Springs does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Nicole M. Schanel

Date

02 JAN 2019

Registered Professional Engineer

Blue & Silver Development Partners, LLC

State of Colorado

No. 52434



## **Developer's Statement:**

Blue & Silver Development Partners, LLC hereby certifies that the drainage facilities for True North Commons shall be constructed according to the design presented in this report. I understand that the City of Colorado Springs does not and will not assume liability for the drainage facilities designed and/or certified by my engineer and that are submitted to the City of Colorado Springs pursuant to section 7.7.906 of the City Code; and cannot, on behalf of True North Commons, guarantee that final drainage design review will absolve Blue & Silver Development Partners, LLC and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the final plat does not imply approval of my engineer's drainage design.

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|---|---|
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|   | 01/11/2019                                |
| For the City Engineer                                   | Date                                      |
|   |   |
| Conditions:   |   |



## I. Introduction

True North Commons is comprised of 57.8 acres of undeveloped land located on the west side of Interstate 25 at the North Gate exit. The site is owned by the United States Air Force Academy (USAFA) and is currently being annexed into the City of Colorado Springs. The site has not been platted and will remain unplatted through the development process.

The 57-acre piece of land will be portioned off into two separate parcels. Parcel 1 (approximately 36 acres) will contain about 20 acres of land to be developed at a later time, as well as approximately 16 acres comprised of a combination of retail and commercial development, including a new Visitor's Center for USAFA. Parcel 2 (approximately 21 acres) is to encompass a mix of retail, office space as well as hotel and conference uses. Blue & Silver Development Partners, LLC will be entering into a long-term lease agreement with USAFA in order to develop the land. The Project location is shown in Figure 1.

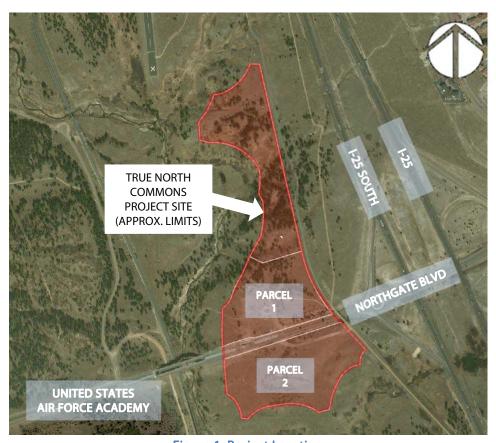


Figure 1. Project Location

True North Commons is located in both Sections 1 and 12, Township 12 South, Range 67 West of the 6<sup>th</sup> P.M. in the City of Colorado Springs, County of El Paso, State of Colorado. The site is bound on the east by the Interstate 25 corridor and on the west side by Monument Creek. Undeveloped USAFA property lies to the north and south of the overall site. The proposed property is divided into two parcels by



Northgate Boulevard. The northern extends approximately 3,000 feet north of Northgate Boulevard. The second parcel extends about 1,000 feet to the south, with the existing roadway providing the northerly boundary.

Topographical information for the site was found using *United States Geological Survey* (USGS) mapping. The *Web Soil Survey*, created by the *Natural Resources Conservation Service* was utilized to investigate the existing general soil types within the site. As previously mentioned, this report has been prepared in accordance to the standards set forth in the DCM. In addition, the *Urban Storm Drainage Criteria Manuals, Volumes 1 through 3*, dated 2016 have been used to supplement the City Criteria Manual.

The purpose of this Master Development Drainage Plan is to identify and evaluate the offsite and onsite drainage patterns associated with the undeveloped land and to provide hydrologic and hydraulic analyses of the area to ensure compliance with the City of Colorado Springs Drainage Criteria Manual Volumes 1 & 2 (DCM) as well as provide safe, effective routing to the downstream outfalls. In addition to the reviews by the City of Colorado Springs, USAFA will also serve as a jurisdiction for the project and will evaluate this MDDP.

This parcel currently discharges into Monument Creek and Smith Creek (a tributary of Monument Creek) and, eventually, Fountain Creek. A Restoration Study was completed by Matrix Design Group titled "Monument Creek Watershed Restoration Master Plan", dated October 31, 2016 that analyzed the creek and its tributaries and outlined the framework needed for rehabilitation of the creek from recent fire and flood damages but a detailed drainage planning study of this area has not yet been completed (refer to Figure 2 below). As such, this MDDP will analyze the existing drainage patterns and use these calculations to ensure the developed condition has no adverse impacts to any downstream infrastructure.



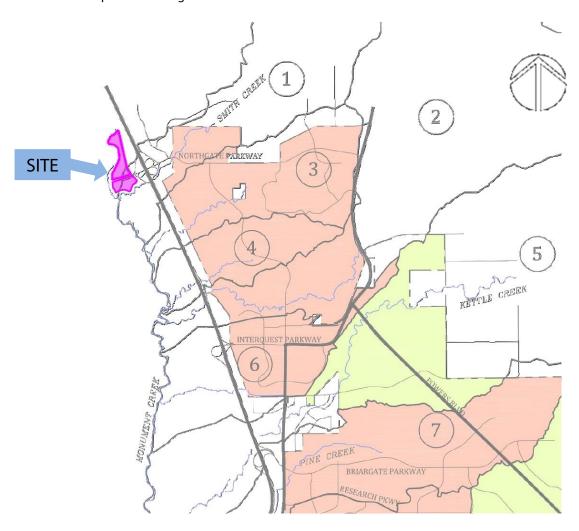


Figure 2. Drainage Basin Planning Study Map

# II. Project Characteristics

The Monument Creek watershed reaches north to approximately County Line Road and is the receiving waters for the True North Commons development, though this region has not previously been included in any DBPS. The site is presently undeveloped and covered with natural vegetation with the exception of Northgate Boulevard and a gravel parking lot associated with the Santa Fe Trail.

Soils can be classified in four different hydrologic groups, A, B, C, or D to help predict the stormwater runoff rates. Hydrologic group "A" is characterized by deep, well-drained coarse-grained soils with a rapid infiltration rate when thoroughly wet and having a low runoff potential. Group "D" typically has a clay layer at or near to the surface, or a very shallow depth to impervious bedrock and has a very slow infiltration rate and a high runoff potential. Refer to the Soil Map provided in Appendix C for a detailed description of the soils for the site. The following soil types are present in the development area:



Table 1. NRCS Soil Survey for El Paso County

| Soil ID | Soil                                   | Hydrologic     | Runoff | Percent on |
|---------|--|----------------|--------|------------|
| Number  |  | Classification | Class  | Site       |
| 42      | Kettle-Rock outcrop complex            | В              | Medium | 36.9%      |
| 71      | Pring coarse sandy loam (3%-8% slopes) | В              | Low    | 31.0%      |
| 93      | Tomah-Crowfoot complex (8%-15% slopes  | В              | Medium | 32.1%      |

The ultimate receiving waters for the entirety of the site is Monument Creek. The proposed development drains in a general northeast to southwest pattern until being collected by existing, natural swales which convey the flows offsite and into Monument Creek. With the exception of a southeastern portion of the site, these swales discharge the collected flows directly into Monument Creek, including the flows captured in Northgate Boulevard. The remaining piece of land also runs in a general northeast to southwest drainage pattern and is collected in an existing swale. However, this swale discharges into Smith Creek. Smith Creek is a tributary of Monument Creek and the two creeks converge approximately 600 feet southwest of the site's southern boundary.

The 57-acre parcel will be annexed into the City of Colorado Springs and zoned as a Planned Unit Development (PUD). Specifically, the site is planned for uses consisting of office, retail, commercial, hotel, and governmental. The proposed condition of the site will include modifications to the existing Northgate Boulevard, 8 acres for the new USAFA Visitor's Center, 8 acres of retail and commercial space, 10.5 acres of office space, and 10.5 acres of hotel and conferences uses.

# III. Hydrologic Analysis

The hydrology for this project uses the Rational Method as recommended by the DCM (Volume 1, Chapter 6, Section 3) for the minor and major storms. The Rational Method is used for drainage basins less than 100 acres in size.

Rational Method coefficients from Table 6-6 of the DCM were utilized in the calculations. Refer to Appendix B for the aforementioned table. The time of concentration consists of the initial time of overland flow combined with the travel time of concentrated flow until reaching a point of discharge. A minimum time of concentration of 5 minutes is utilized for urban area. The hypothetical rainfall depths for the 24-hour storm duration utilized were taken from the DCM with the minor and major storm event depths listed in the table below.



Table 2. DCM 1-Hour Rainfall Depths

| Storm Recurrence Interval | Rainfall Depth (inches) |  |  |  |  |  |  |  |
|---------------------------|-------------------------|--|--|--|--|--|--|--|
| 5-year                    | 1.50                    |  |  |  |  |  |  |  |
| 100-year                  | 2.52                    |  |  |  |  |  |  |  |

The rainfall intensity equation for the Rational Method was taken from the DCM Figure 6-5 (Appendix B).

## **Existing Drainage Conditions**

The undeveloped site runs in a general northeast to southwest pattern before draining offsite and eventually into Monument Creek. The existing calculations have been summarized:

**Table 3. Existing Conditions Basin & Design Point Summary** 

| Basin ID | Acreage | Q <sub>5</sub> | Q <sub>100</sub> |  |  |
|----------|---------|----------------|------------------|--|--|
| OS1      | 28.4    | 7.6            | 51.4             |  |  |
| OS2      | 10.7    | 2.5            | 17.1             |  |  |
| OS3      | 10.4    | 35.7           | 65.8             |  |  |
| Α        | 20.2    | 6.5            | 43.9             |  |  |
| В        | 16.4    | 4.4            | 29.6             |  |  |
| С        | 3.4     | 7.1            | 13.2             |  |  |
| D        | 11.3    | 3.5            | 23.4             |  |  |
| Е        | 10.0    | 2.3            | 15.4             |  |  |
| DP1      | 48.6    | 12.2           | 81.9             |  |  |
| DP2      | 27.1    | 5.7            | 38.0             |  |  |
| DP3      | 13.9    | 35.4           | 65.3             |  |  |
| DP4      | 11.3    | 3.5            | 23.4             |  |  |
| DP5      | 10.0    | 2.3            | 15.4             |  |  |

More specifically, the *existing conditions* for the site have been analyzed and are presented by design point as follows:



Existing Design Point 1 ( $Q_5 = 12.2 \text{ cfs}$ ,  $Q_{100} = 89.1 \text{ cfs}$ ) is located at the western boundary of the site where the runoff discharges into Monument Creek. The contributing sub-basins for this design point include offsite Sub-basin OS1 (28.4 acres;  $Q_5 = 7.6 \text{ cfs}$ ,  $Q_{100} = 51.4 \text{ cfs}$ ) which includes the runoff that flows onto the site from the northeast and continues to travel in a general northeast to southwest direction until combining with the runoff from onsite Sub-basin A (20.2 acres;  $Q_5 = 6.5 \text{ cfs}$ ,  $Q_{100} = 43.9 \text{ cfs}$ ). The combined flows are collected through natural drainage swales until they leave the site. The graphic below depicts the area encompassed by this design point and has been added for a visual reference only. Please refer to the Existing Conditions Drainage Map for more detailed information (Appendix C).

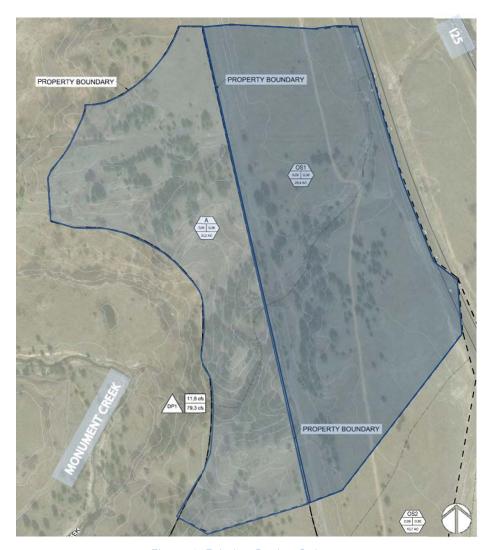


Figure 3. Existing Design Point 1



**Existing Design Point 2** ( $Q_5 = 5.7$  cfs,  $Q_{100} = 38.0$  cfs) is composed of the offsite Sub-basin OS2 (10.7 acres;  $Q_5 = 35.7$  cfs,  $Q_{100} = 17.1$  cfs) which sheet flows from the northeast to the southwest until converging into shallow concentrated flows and which continue in their current pattern onto onsite Sub-basin B (16.4 acres;  $Q_5 = 4.4$  cfs,  $Q_{100} = 29.6$  cfs). This combined runoff exits the proposed site and releases into Monument Creek.



Figure 4. Existing Design Point 2



**Existing Design Point 3** ( $Q_5 = 35.4$  cfs,  $Q_{100} = 65.3$  cfs) accounts for runoff created by offsite Sub-basin OS3 (10.4 acres;  $Q_5 = 2.5$  cfs,  $Q_{100} = 65.8$  cfs) and onsite Sub-basin C (3.43 acres;  $Q_5 = 7.1$  cfs,  $Q_{100} = 13.2$  cfs). The majority of these basins consist of the exist paved Northgate Boulevard ramps and roadway corridor. Runoff from offsite Sub-basin OS3 drains to roadside swales that continue onto onsite Sub-basin C until releasing into Monument Creek at the bridge crossing.

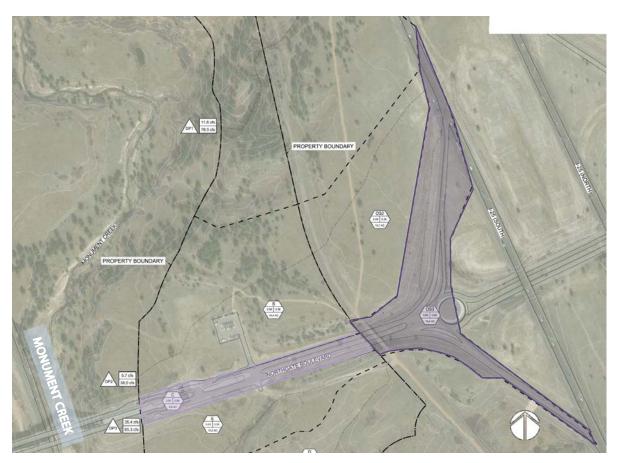


Figure 5. Existing Design Point 3



**Existing Design Point 4** consists of a singular onsite sub-basin, Sub-basin D (11.3 acres;  $Q_5 = 3.5$  cfs,  $Q_{100} = 23.4$  cfs). Drainage generated in this existing area sheet flows to an existing natural drainage swale in the middle of the sub-basin. Once collected in the swale, the runoff is conveyed to the southwest, continuing offsite and eventually discharging into Smith Creek, a tributary of Monument Creek. Similarly, **Existing Design Point 5** includes only onsite Subbasin E (10.0 acres;  $Q_5 = 2.3$  cfs,  $Q_{100} = 15.4$  cfs). Runoff from this area flows from the northeast to southwest until leaving the site and draining into Monument Creek.

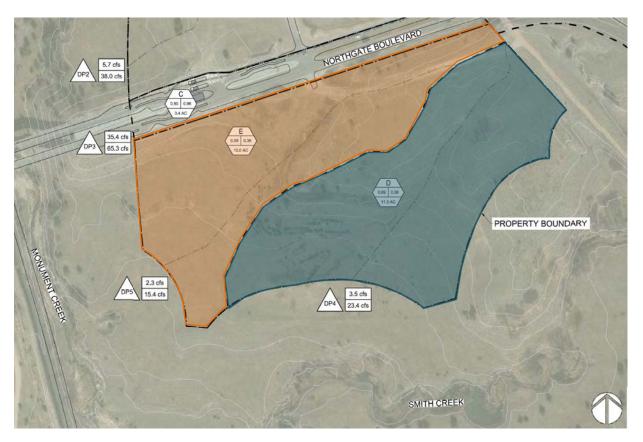


Figure 6. Existing Design Points 4 & 5



## **Developed Drainage Conditions**

The drainage pattern for the developed conditions will continue to travel to the southwest as in the undeveloped conditions. The drainage from the parcels will be split by Northgate Boulevard and treated by two separate Full Spectrum Detention Ponds prior to releasing the flows outside of the property lines. From there, the treated discharge will flow overland into Monument Creek. The developed calculations have been summarized:

Table 4. Developed Conditions Basin & Design Point Summary

| Basin ID | Acreage | Q <sub>5</sub> | Q <sub>100</sub> |
|----------|---------|----------------|------------------|
| OS1      | 28.4    | 7.6            | 51.4             |
| OS2      | 10.7    | 2.5            | 17.1             |
| OS3      | 10.4    | 35.7           | 65.8             |
| Α        | 20.2    | 6.5            | 43.9             |
| B1       | 8.3     | 33.2           | 60.6             |
| B2       | 8.2     | 31.5           | 57.4             |
| С        | 3.4     | 7.1            | 13.2             |
| D        | 10.5    | 40.7           | 74.2             |
| Е        | 10.0    | 37.2           | 67.9             |
| DP1      | 48.6    | 12.2           | 81.9             |
| DP2      | 19.0    | 23.1           | 50.5             |
| DP3      | 13.9    | 35.4           | 65.3             |
| DP4      | 22.0    | 56.9           | 104.8            |
| DP5      | 20.5    | 55.3           | 100.8            |

More specifically, the developed conditions for the site have been analyzed and are presented by design point as follows:

**Design Point 1** in the developed condition is to remain unchanged from **Existing Design Point 1**. At this time, onsite Sub-basin A is to remain undeveloped and the flows from this basin as well as offsite Sub-basin OS1 will continue to drain as they have historically, as previously discussed. When future development occurs, a final drainage report and Full Spectrum Detention Pond will be required.



**Design Point 2** ( $Q_5 = 23.1$  cfs,  $Q_{100} = 50.5$  cfs) is the convergence of offsite Sub-basin OS2 as well as onsite Sub-basin B1 (8.3 acres;  $Q_5 = 33.2$  cfs,  $Q_{100} = 60.6$  cfs). Sub-basin B1 is planning to contain the proposed USAFA Visitor's Center and associated parking and has been modeled using coefficients utilized for commercial development. At this time, offsite Sub-basin OS2 is anticipated to remain undeveloped. The combined flows will be conveyed by curb and gutter and directed to proposed storm infrastructure located at **Design Point 2**. From here, the runoff will be conveyed to the west until releasing into the northern Full Spectrum Detention Pond at **Design Point 4**.

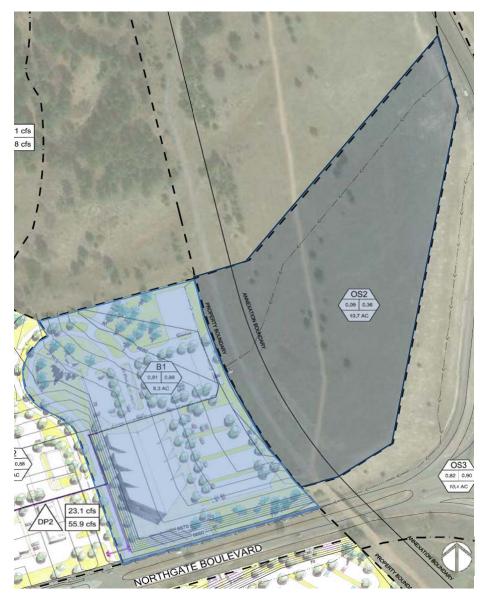


Figure 7. Proposed Design Point 2



**Design Point 3**, similarly to **Design Point 1**, will also remain unchanged from its existing condition and will continue to contribute the flows analyzed presented earlier in this report.

**Design Point 4** ( $Q_5 = 56.9$  cfs,  $Q_{100} = 104.8$  cfs) is located at the Full Spectrum Detention Pond (North Pond) that will be required to treat the runoff generated for the developed site north of Northgate Boulevard. This will include the abovementioned **Design Points 2 and 3**, as well as flows from onsite Sub-basin B2 (8.2 acres;  $Q_5 = 31.5$  cfs,  $Q_{100} = 57.4$  cfs). Sub-basin B2 has an anticipated use of commercial and has been evaluated based on the corresponding coefficients for this use provided in the DCM.



Figure 8. Proposed Design Point 4



**Design Point 5** ( $Q_5 = 55.3$  cfs,  $Q_{100} = 100.8$  cfs) is located at the southern detention facility (South Pond) that will be required, located at the southwest corner of the site. This design point will encompass onsite flows from Sub-basin D (10.5 acres;  $Q_5 = 40.7$  cfs,  $Q_{100} = 74.2$  cfs) which will be directed by proposed curb, gutter, and storm infrastructure to the southwest, combining with flows from Sub-basin E (10.0 acres;  $Q_5 = 37.2$  cfs,  $Q_{100} = 67.9$  cfs). This Full Spectrum Detention Basin has been designed to accommodate 20.5 acres of developed runoff, which will require a pond volume of approximately 3.2 acre-feet of storage. In previous conditions, portions of these two sub-basins would have released into Smith Creek prior to its convergence with Monument Creek. In the proposed conditions, all flows from these sub-basins will be directed into the detention basin before releasing directly to Monument Creek.

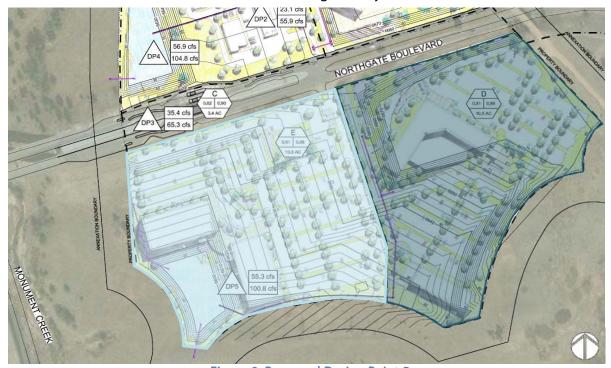


Figure 9. Proposed Design Point 5

## **Detention and Water Quality**

In accordance with the City of Colorado Springs drainage criteria, the proposed True North Commons will provide onsite Full Spectrum Detention Facilities to mitigate the developed drainage impacts. Both proposed facilities for the development will be Extended Detention Basins (EDB) that will discharge just to the west of the property boundary, allowing the treated runoff to flow overland into Monument Creek at the approved unit release rate stated in Table 13-2 of the DCM, included in Appendix B. The calculated release rates for each pond are stated in the Table 6, below.



**Table 5. Pond Releases** 

| Design Return | NRCS Hydrologic Soil | Contributin | g Area     | Total Allowable Release |                        |  |  |  |
|---------------|----------------------|-------------|------------|-------------------------|------------------------|--|--|--|
| Period        | Group                | (Acres      | s)         | (cfs)                   |                        |  |  |  |
| (Years)       | В                    | North Pond  | South Pond | North Pond              | South Pond             |  |  |  |
| 5             | 0.04                 | 40.0        | 20.5       | Q <sub>5</sub> = 1.6    | $Q_5 = 0.8$            |  |  |  |
| 100           | 0.30                 |             |            | Q <sub>100</sub> = 12   | Q <sub>100</sub> = 6.2 |  |  |  |

The North Pond EDB has a total watershed area of 40.0 acres with an imperviousness of 50% to include the developed onsite sub-basins as well as the offsite, undeveloped acreage of Sub-basin OS2. This results in the following volumes:

Water Quality Capture Volume (WQCV): 0.705 acre-feet Excess Urban Runoff Volume (EURV): 2.192 acre-feet 5-YR Detention Volume: 2.267 acre-feet 100-YR Detention Volume: 3.835 acre-feet

The South Pond EDB has been designed to accommodate 20.5 acres of developed runoff with an approximate imperviousness of 95%. The required volumes calculated:

Water Quality Capture Volume (WQCV): 0.764 acre-feet Excess Urban Runoff Volume (EURV): 2.192 acre-feet 5-YR Detention Volume: 2.296 acre-feet 100-YR Detention Volume: 3.208 acre-feet

The Final Drainage Reports that will be required for the development will provide detailed pond routing calculations using UD-Detention from the Urban Drainage Flood Control District for final design.



## IV. Hydraulic Analysis

In accordance with the DCM, major drainage will be conveyed through a combination of open channels, underground storm sewer capacity, and allowable street capacity. Calculations have been completed per the DCM Volume 1, Chapter 9, Section 7.

As previously stated, the entire site is located within the Monument Creek Drainage Basin, and all drainage that exits the site will ultimately release into Monument Creek. In the developed conditions, Design Points 4 and 5 represent the two site exit points for the drainage of True North Commons.

The storm systems as well as both proposed full spectrum detention ponds will be privately owned and maintained by the business improvement district that is currently being established for the property.

A hydraulic analysis using the Manning's equation has been completed to determine the pipe capacity of the trunk mains for the site, refer to Appendix A for calculations. **Pipe Run 1** includes the trunk main located in the proposed road that extends to the north from Northgate Boulevard. Because the site is at a preliminary design stage, this pipe has been designed to accommodate the entirety of the flow reaching DP1, resulting in a 36" storm drain. This pipe will connect to an inlet and extend west to **Pipe Run 2** (48"), which has been designed to capture the DP4 design flows and will discharge into the northern detention pond. **Pipe Run 3** (42") will convey the runoff generated in Sub-Basin D to the south and then west where it will connect to **Pipe Run 4**, a 48" storm drain that will carry the DP5 flows to the west and discharge into the south pond. A more detailed analysis of the roadways, storm sewers, swales, and inlets will be required to be completed at the time of development of the parcels. At this time, no improvements to any existing infrastructure are anticipated.





Figure 10. Pipe Run Summary

Per the *Flood Insurance Rate Maps (FIRM) 08041CO290 F and 08041CO290 F*, effective dates March 17, 1997, published by the Federal Emergency Management Agency (FEMA), the entirety of the site is located within Zone D, which is specified as an area in which flood hazards are undetermined. However, the site does not lie within the 100-year floodplain as delineated from the GIS provided by USAFA.

## V. Environmental Evaluations

Concurrent with this MDDP, an Environmental Assessment is being completed for the property. There are wetlands located on the site which are currently being delineated as either jurisdictional or non-jurisdictional in coordination with the United States Army Corp of Engineers (USCOE). Prebles Meadow Jumping Mouse has been located within the annexation boundary, but not within the developable



area. The project will coordinate with US Fish and Wildlife Service, USAFA, and the US COE for any impact mitigation that may be required.

All onsite detention facilities shall be designed to accommodate water quality requirements. As the development of each parcel progresses, the detention guidelines in this report are to be upheld.

Per the DCM Chapter 1, Section 4, the City of Colorado Springs requires the UDFCD Four Step Process for receiving water protection that focuses on reducing runoff volumes, treating the water quality capture volume (WQCV), stabilizing drainageways, and implementing long-term source controls.

# Step 1: Reduce runoff by disconnecting impervious area, eliminating "unnecessary" impervious area and encouraging infiltration into soils that are suitable.

Site specific landscaping will be done on each lot to decrease the connectivity of impervious areas. Grass-lined swales will be used where possible to allow ground infiltration.

## Step 2: Treat and slowly release the WQCV.

Each pond will meet the DCM standards for the release rates of Full Spectrum Detention Ponds for Water Quality Capture Volumes.

#### Step 3: Stabilize stream channels.

The two Full Spectrum Detention Ponds that will treat the developed site for water quality and detention will release at the City of Colorado Springs maximum release rate of 0.30 cfs/acre, resulting in a much lower release rate than the present conditions. At the location of each outfall, outside of the property boundary, a permanent low tailwater basin will be installed to mitigate any erosion created by the point discharge. These factors will eliminate any adverse impacts that could occur from the development, therefore no creek improvements are required.

#### Step 4: Implement source controls.

During construction, the contractor will have designated concrete washout areas and will implement sediment control logs and inlet protection in order to control pollutants at their source.

# VI. Fee Development

Monument Creek continues to run south after leaving the True North Commons property. At the intersection of I-25 and Cimarron, Monument Creek converges with (and continues on as) Fountain Creek. Per the *2018 Drainage, Bridge and Pond Fees* released by Colorado Springs, fees vary based on the associated basin study within the Fountain Creek watershed. This fee schedule (found in Appendix B) states that "Pursuant to the recommendation of the Subdivisions Storm Drainage Board adopted at its meeting of September 15, 1977, there are exempted and excluded from the provisions of this part construction of the main Fountain Creek Channel from the confluence of Fountain Creek with Monument Creek northwest to the City limits. Land development taking place adjacent to Fountain Creek shall remain responsible for dedicating rights of way necessary for the channelization



of Fountain Creek, and the developers shall continue to pay to the City as a condition of subdivision plat approval the applicable drainage fees. Drainage fees are required in accordance with the appropriate basin study."

As previously stated in this report, True North Commons is not located within any existing basin study and fees have not been established. If the site were to be platted in the future, fees will be required.

## VII. References

- City of Colorado Springs, Colorado. 2014. Drainage Criteria Manual, Volumes 1 & 2.
- Matrix Design Group, Inc. 2016. Monument Creek Watershed Restoration Master Plan.
- NRCS. 1981. Soil Survey of El Paso County, Colorado. U.S. Department of Agriculture Soil Conservation Service, now the Natural Resource Conservation Service.
- Urban Drainage and Flood Control District. 2001 (Rev. 2016). Urban Storm Drainage Criteria
   Manual. Volumes 1-3



# Appendix A – Hydrologic and Hydraulic Calculations



Project Name:True North CommonsProject Location:Colorado SpringsDesignerNMSNotes:Existing Conditions

Average Channel Velocity Average Slope for Initial Flow 5 ft/s (If specific channel vel is used, this will be ignored)
0.04 ft/ft (If Elevations are used, this will be ignored)

|       |                     | Area      |       |      |          |           |      | Ratio     | onal 'C' Values |      |            |      |      |        | Flow Lengths Initial Flow |         |         | Flow     | Channel Flow |          | Tc    | Minor Storm Flow Rate | Major Storm Flow Rate |
|-------|---------------------|-----------|-------|------|----------|-----------|------|-----------|-----------------|------|------------|------|------|--------|---------------------------|---------|---------|----------|--------------|----------|-------|-----------------------|-----------------------|
|       |                     |           |       | S    | urface T | Type 1    | Su   | ırface Ty | pe 2            | Su   | rface Type | 3    | Com  | oosite | Initial                   | Channel | Average | Initial  | Average      | Velocity | Total | Q5                    | Q100                  |
| Basin | Contributing Basins | sf        | acres | C5   | C100     | Area (SF) | C5   | C100      | Area (SF)       | C5   | C100       | Area | C5   | C100   | ft                        | ft      | Slope   | Tc (min) | Slope        | (ft/s)   | (min) | cfs                   | cfs                   |
| OS1   |                     | 1,238,609 | 28.44 | 0.09 | 0.36     | 1,238,609 | 0.90 | 0.96      | 0               | 0.81 | 0.88       | 0    | 0.09 | 0.36   | 179                       | 1013    | 0.067   | 13.0     | 0.036        | 2.2      | 20.7  | 7.6                   | 51.4                  |
| OS2   |                     | 466,760   | 10.72 | 0.09 | 0.36     | 466,760   | 0.90 | 0.96      | 0               | 0.81 | 0.88       | 0    | 0.09 |        | 120                       | 948     | 0.017   | 16.9     | 0.019        | 1.7      |       | 2.5                   | 17.1                  |
| OS3   |                     | 454,202   | 10.43 | 0.09 | 0.36     | 45,420    | 0.90 | 0.96      | 408,782         | 0.81 | 0.88       | 0    | 0.82 | 0.90   | 136                       | 1290    | 0.029   | 4.1      | 0.037        | 3.8      | 9.8   | 35.7                  | 65.8                  |
| Α     |                     | 878,699   | 20.18 | 0.09 | 0.36     | 878,699   | 0.90 | 0.96      | 0               | 0.81 | 0.88       | 0    | 0.09 |        | 150                       | 428     | 0.067   | 11.9     | 0.068        | 3.4      |       | 6.5                   | 43.9                  |
| В     |                     | 714,832   | 16.42 |      | 0.36     | 714,832   | 0.90 | 0.96      | 0               | 0.81 | 0.88       | 0    | 0.09 |        | 138                       | 1024    | 0.036   | 14.0     | 0.046        | 2.5      |       | 4.4                   | 29.6                  |
| C     |                     | 149,267   | 3.43  | 0.09 | 0.36     | 14,927    | 0.90 | 0.96      | 134,340         | 0.81 | 0.88       | 0    | 0.82 |        | 48                        | 1214    | 0.021   | 2.7      | 0.003        | 0.8      |       | 7.1                   | 13.2                  |
| D     |                     | 490,256   | 11.26 |      | 0.36     | 490,256   | 0.90 | 0.96      | 0               | 0.81 | 0.88       | 0    | 0.09 |        | 124                       | 881     | 0.073   |          | 0.061        | 3.0      |       | 3.5                   | 23.4                  |
| E     |                     | 435,392   | 10.00 | 0.09 | 0.36     | 435,392   | 0.90 | 0.96      | 0               | 0.81 | 0.88       | 0    | 0.09 | 0.36   | 157                       | 1110    | 0.013   | 21.1     | 0.056        | 2.8      | 27.7  | 2.3                   | 15.4                  |
| DP1   | DP1 & A             | 2,117,308 | 48.61 | 0.09 | 0.36     | 2,117,308 | 0.90 | 0.96      | 0               | 0.81 | 0.88       | 0    | 0.09 | 0.36   | 179                       | 1591    | 0.067   | 13.0     | 0.047        | 2.5      | 23.6  | 12.2                  | 81.9                  |
| DP2   | OS2 & B             | 1,181,592 | 27.13 | 0.09 | 0.36     | 1,181,592 | 0.90 | 0.96      | 0               | 0.81 | 0.88       | 0    | 0.09 | 0.36   | 120                       | 2110    | 0.017   | 16.9     | 0.036        | 2.2      | 32.9  | 5.7                   | 38.0                  |
| DP3   | OS3 & C             | 603,469   | 13.86 | 0.09 | 0.36     | 60,347    | 0.90 | 0.96      | 543,122         | 0.81 | 0.88       | 0    | 0.82 | 0.90   | 136                       | 2504    | 0.029   | 4.1      | 0.021        | 2.8      | 19.0  | 35.4                  | 65.3                  |
| DP4   | D                   | 490,256   | 11.26 | 0.09 | 0.36     | 490,256   | 0.90 | 0.96      | 0               | 0.81 | 0.88       | 0    | 0.09 | 0.36   | 124                       | 881     | 0.073   | 10.6     | 0.061        | 3.0      | 15.5  | 3.5                   | 23.4                  |
| DP5   | E                   | 435,392   | 10.00 | 0.09 | 0.36     | 435,392   | 0.90 | 0.96      | 0               | 0.81 | 0.88       | 0    | 0.09 | 0.36   | 157                       | 1110    | 0.013   | 21.1     | 0.056        | 2.8      | 27.7  | 2.3                   | 15.4                  |

Project Name:True North CommonsProject Location:Colorado SpringsDesignerNMSNotes:Proposed Condition

Average Channel Velocity 5 ft/s (If specific chan Average Slope for Initial Flow 0.04 ft/ft (If Elevations are

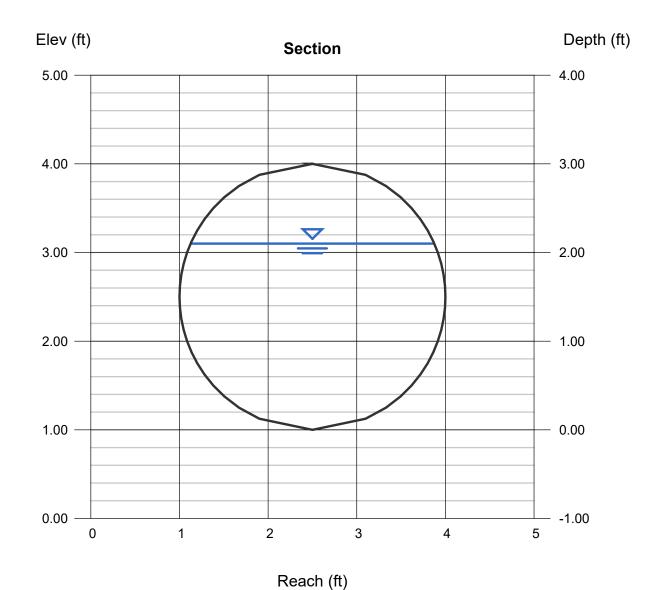
5 ft/s (If specific channel vel is used, this will be ignored)
.04 ft/ft (If Elevations are used, this will be ignored)

|           |                     | Area      |       |      |          |           |      |            | Rationa   | l 'C' Valu | es          |         |           |        |      |        | Flow Lei  | ngths   | Initial Flow |           | Channel | l Flow   |          | Tc    | Minor Storm Flow Rate | Major Storm Flow Rate |
|-----------|---------------------|-----------|-------|------|----------|-----------|------|------------|-----------|------------|-------------|---------|-----------|--------|------|--------|-----------|---------|--------------|-----------|---------|----------|----------|-------|-----------------------|-----------------------|
|           |                     |           |       | Su   | rface Ty | pe 1      | Su   | rface Type | 2         | Sı         | urface Type | 3       | Surface   | Type 4 | Comp | oosite | Initial ( | Channel | Initial      | Low Point | Average | Velocity | Channel  | Total | Q5                    | Q100                  |
| Basin     | Contributing Basins | sf        | acres | C5 ( | 100      | Area (SF) | C5   | C100       | Area (SF) | C5         | C100        | Area    | C5 C100   | Area   | C5   | C100   | ft        | ft      | Tc (min)     | Elevation | Slope   | (ft/s)   | Tc (min) | (min) | cfs                   | cfs                   |
| OS1       |                     | 1,238,609 | 28.44 | 0.09 | 0.36     | 1,238,609 | 0.90 | 0.96       | 0         | 0.81       | 0.88        | 0       | 0.12 0.39 | 0      | 0.09 | 0.36   | 179       | 1013    | 13.0         | 6678      | 0.036   | 2.2      | 7.7      | 20.7  | 7.6                   | 51.4                  |
| OS2       |                     | 466,760   | 10.72 | 0.09 | 0.36     | 466,760   | 0.90 | 0.96       | 0         | 0.81       | 0.88        | 0       | 0.12 0.39 | 0      | 0.09 | 0.36   | 120       | 948     | 16.9         | 6692      | 0.019   | 1.7      | 9.3      | 26.2  |                       | 17.1                  |
| OS3       |                     | 454,202   | 10.43 | 0.09 | 0.36     | 45,420    | 0.90 | 0.96       | 408,782   | 0.81       | 0.88        |         | 0.12 0.39 |        | 0.82 |        | 136       | 1290    | 4.1          | 6658      | 0.037   | 3.8      | 5.7      | 9.8   |                       | 65.8                  |
| A         |                     | 878,699   | 20.18 | 0.09 | 0.36     | 878,699   | 0.90 | 0.96       | 0         | 0.81       | 0.88        | 0       | 0.12 0.39 | 0      | 0.09 | 0.36   | 150       | 426     | 11.9         | 6639      | 0.068   | 3.4      | 2.1      | 14.0  |                       | 43.9                  |
| <i>B1</i> |                     | 360,108   | 8.27  | 0.09 |          | 0         | 0.90 | 0.96       | 0         | 0.81       |             |         |           |        | 0.81 | 0.88   | 40        | 871     | 1.9          | 6658      | 0.037   | 3.8      | 3.8      | 5.8   |                       | 60.6                  |
| B2        |                     | 354,728   | 8.15  | 0.09 | 0.36     | 0         | 0.90 | 0.96       | 0         | 0.81       | 0.88        |         | 0.12 0.39 |        | 0.81 | 0.88   | 28        | 1033    | 2.3          | 6630      | 0.040   | 4.0      | 4.3      | 6.6   |                       | 57.4                  |
| C         |                     | 149,267   | 3.43  | 0.09 | 0.36     | 14,927    | 0.90 | 0.96       | 134,340   | 0.81       | 0.88        | 0       | 0.12 0.39 | 0      | 0.82 | 0.90   | 48        | 1214    | 2.7          | 6653      | 0.003   | 0.8      | 25.3     | 28.0  | 7.1                   | 13.2                  |
| D         |                     | 456,750   | 10.49 | 0.09 | 0.36     | 0         | 0.90 | 0.96       | 0         | 0.81       | 0.88        | 456,750 | 0.12 0.39 | 0      | 0.81 | 0.88   | 17        | 1228    | 1.5          | 6600      | 0.041   | 4.1      | 5.0      | 6.5   |                       | 74.2                  |
| E         |                     | 434,099   | 9.97  | 0.09 | 0.36     | 0         | 0.90 | 0.96       | 0         | 0.81       | 0.88        | 434,099 | 0.12 0.39 | 0      | 0.81 | 0.88   | 83        | 1086    | 2.8          | 6626      | 0.040   | 4.0      | 4.5      | 7.4   | 37.2                  | 67.9                  |
| DP1       | OS1 & A             | 2,117,308 | 48.61 | 0.09 | 0.36     | 2,117,308 | 0.90 | 0.96       | 0         | 0.81       | 0.88        | 0       | 0.12 0.39 | 0      | 0.09 | 0.36   | 179       | 1591    | 13.0         | 6639      | 0.047   | 2.5      | 10.6     | 23.6  | 12.2                  | 81.9                  |
| DP2       | OS2 & B1            | 826,868   | 18.99 | 0.09 | 0.36     | 466,760   | 0.90 | 0.96       | 0         | 0.81       | 0.88        | 360,108 | 0.12 0.39 | 0      | 0.41 | 0.59   | 179       | 2167    | 8.9          | 6639      | 0.035   | 2.2      | 16.4     | 25.3  | 20.9                  | 50.5                  |
| DP3       | OS3 & C             | 603,469   | 13.86 | 0.09 | 0.36     | 60,347    | 0.90 | 0.96       | 543,122   | 0.81       | 0.88        | 0       | 0.12 0.39 | 0      | 0.82 | 0.90   | 136       | 2504    | 4.1          | 6653      | 0.021   | 2.8      | 14.9     | 19.0  | 35.4                  | 65.3                  |
| DP4       | DP3 & B2            | 958,197   | 22.00 | 0.09 | 0.36     | 60,347    | 0.90 | 0.96       | 543,122   | 0.81       | 0.88        | 354,728 | 0.12 0.39 | 0      | 0.82 | 0.90   | 136       | 3125    | 4.1          | 6658      | 0.015   | 3.6      | 14.5     | 18.6  | 56.9                  | 104.8                 |
| DP5       | D&E                 | 890,849   | 20.46 | 0.09 | 0.36     | 0         | 0.90 | 0.96       | 0         | 0.81       | 0.88        | 890,849 | 0.12 0.39 | 0      | 0.81 | 0.88   | 136       | 2504    | 4.3          | 6653      | 0.021   | 3.4      | 12.3     | 16.6  | 55.3                  | 100.8                 |

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, Oct 1 2018

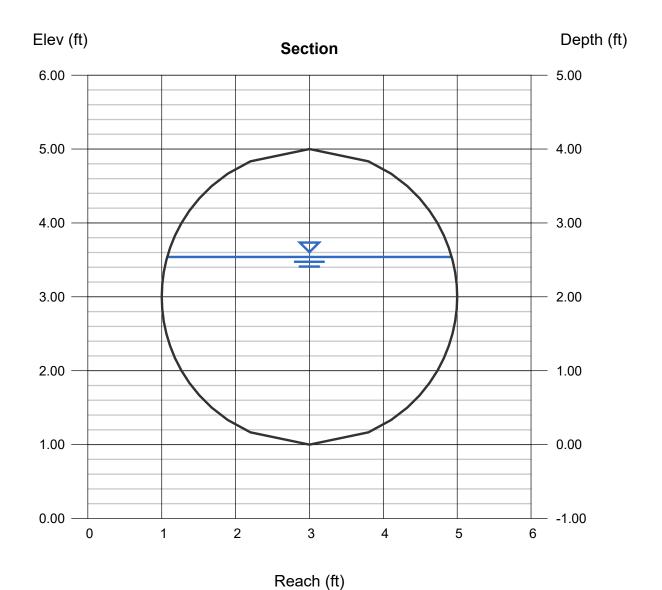
| Circular         |         | Highlighted         |         |
|------------------|---------|---------------------|---------|
| Diameter (ft)    | = 3.00  | Depth (ft)          | = 2.10  |
|                  |         | Q (cfs)             | = 55.90 |
|                  |         | Area (sqft)         | = 5.30  |
| Invert Elev (ft) | = 1.00  | Velocity (ft/s)     | = 10.56 |
| Slope (%)        | = 1.00  | Wetted Perim (ft)   | = 5.95  |
| N-Value          | = 0.013 | Crit Depth, Yc (ft) | = 2.43  |
|                  |         | Top Width (ft)      | = 2.75  |
| Calculations     |         | EGL (ft)            | = 3.83  |
| Compute by:      | Known Q |                     |         |
| Known Q (cfs)    | = 55.90 |                     |         |
|                  |         |                     |         |



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Monday, Oct 1 2018

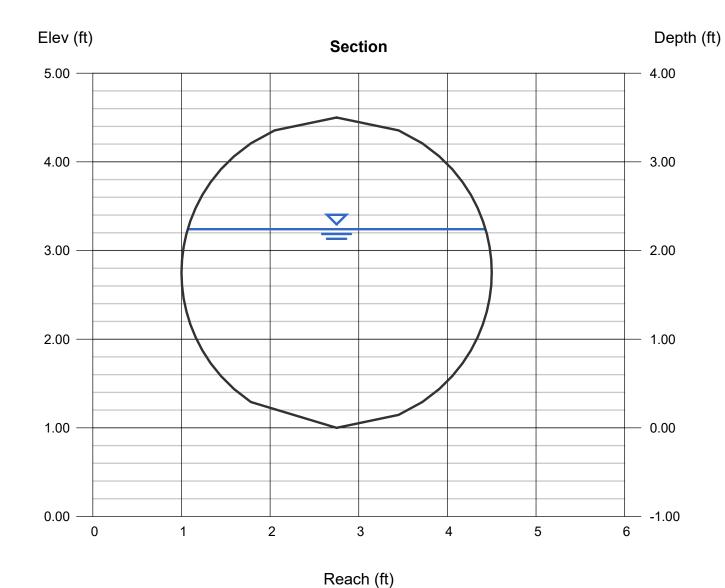
| Circular         |          | Highlighted         |          |
|------------------|----------|---------------------|----------|
| Diameter (ft)    | = 4.00   | Depth (ft)          | = 2.54   |
|                  |          | Q (cfs)             | = 104.80 |
|                  |          | Area (sqft)         | = 8.42   |
| Invert Elev (ft) | = 1.00   | Velocity (ft/s)     | = 12.44  |
| Slope (%)        | = 1.00   | Wetted Perim (ft)   | = 7.38   |
| N-Value          | = 0.013  | Crit Depth, Yc (ft) | = 3.10   |
|                  |          | Top Width (ft)      | = 3.85   |
| Calculations     |          | EGL (ft)            | = 4.95   |
| Compute by:      | Known Q  |                     |          |
| Known Q (cfs)    | = 104.80 |                     |          |
|                  |          |                     |          |



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Monday, Oct 1 2018

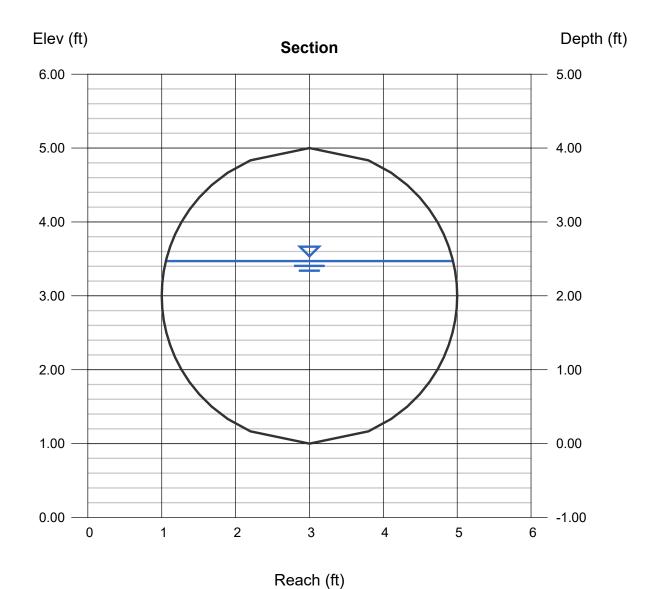
| Circular         |         | Highlighted         |         |
|------------------|---------|---------------------|---------|
| Diameter (ft)    | = 3.50  | Depth (ft)          | = 2.24  |
|                  |         | Q (cfs)             | = 74.20 |
|                  |         | Area (sqft)         | = 6.51  |
| Invert Elev (ft) | = 1.00  | Velocity (ft/s)     | = 11.41 |
| Slope (%)        | = 1.00  | Wetted Perim (ft)   | = 6.49  |
| N-Value          | = 0.013 | Crit Depth, Yc (ft) | = 2.70  |
|                  |         | Top Width (ft)      | = 3.36  |
| Calculations     |         | EGL (ft)            | = 4.26  |
| Compute by:      | Known Q |                     |         |
| Known Q (cfs)    | = 74.20 |                     |         |
|                  |         |                     |         |



Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

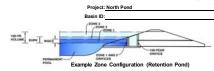
Monday, Oct 1 2018

| Circular         |          | Highlighted         |          |
|------------------|----------|---------------------|----------|
| Diameter (ft)    | = 4.00   | Depth (ft)          | = 2.47   |
|                  |          | Q (cfs)             | = 100.80 |
|                  |          | Area (sqft)         | = 8.16   |
| Invert Elev (ft) | = 1.00   | Velocity (ft/s)     | = 12.35  |
| Slope (%)        | = 1.00   | Wetted Perim (ft)   | = 7.24   |
| N-Value          | = 0.013  | Crit Depth, Yc (ft) | = 3.04   |
|                  |          | Top Width (ft)      | = 3.89   |
| Calculations     |          | EGL (ft)            | = 4.84   |
| Compute by:      | Known Q  |                     |          |
| Known Q (cfs)    | = 100.80 |                     |          |
|                  |          |                     |          |



#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)



| quired Volume Calculation               |        |         |
|---|--------|---------|
| Selected BMP Type =                     | EDB    |         |
| Watershed Area =                        | 41.00  | acres   |
| Watershed Length =                      | 2,240  | ft      |
| Watershed Slope =                       | 0.035  | ft/ft   |
| Watershed Imperviousness =              | 50.00% | percent |
| Percentage Hydrologic Soil Group A =    | 0.0%   | percent |
| Percentage Hydrologic Soil Group B =    | 100.0% | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0%   | percent |
| Desired WQCV Drain Time =               | 40.0   | hours   |

| Desired WQCV Drain Time =              | 40.0       | hours    |
|--|------------|----------|
| Location for 1-hr Rainfall Depths =    | User Input |          |
| Water Quality Capture Volume (WQCV) =  | 0.705      | acre-fee |
| Excess Urban Runoff Volume (EURV) =    | 2.192      | acre-fee |
| 2-yr Runoff Volume (P1 = 1.19 in.) =   | 1.767      | acre-fee |
| 5-yr Runoff Volume (P1 = 1.5 in.) =    | 2.413      | acre-fee |
| 10-yr Runoff Volume (P1 = 1.75 in.) =  | 3.265      | acre-fee |
| 25-yr Runoff Volume (P1 = 2 in.) =     | 4.551      | acre-fee |
| 50-yr Runoff Volume (P1 = 2.25 in.) =  | 5.443      | acre-fee |
| 100-yr Runoff Volume (P1 = 2.52 in.) = | 6.612      | acre-fee |
| 500-yr Runoff Volume (P1 = 0 in.) =    | 0.000      | acre-fee |
| Approximate 2-yr Detention Volume =    | 1.653      | acre-fee |
| Approximate 5-yr Detention Volume =    | 2.267      | acre-fee |
| Approximate 10-yr Detention Volume =   | 3.002      | acre-fee |
| Approximate 25-yr Detention Volume =   | 3.286      | acre-fee |
| Approximate 50-yr Detention Volume =   | 3.436      | acre-fee |
| Approximate 100-yr Detention Volume =  | 3.835      | acre-fee |
|  |            | •        |

| Stann-Storago | Calculation |
|---------------|-------------|

| tage-Storage Calculation                                |       |       |
|---|-------|-------|
| Zone 1 Volume (WQCV) =                                  | 0.705 | acre- |
| Zone 2 Volume (EURV - Zone 1) =                         | 1.487 | acre- |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 1.643 | acre- |
| Total Detention Basin Volume =                          | 3.835 | acre- |
| Initial Surcharge Volume (ISV) =                        | 92    | ft/3  |
| Initial Surcharge Depth (ISD) =                         | 0.50  | ft    |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00  | ft    |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | 1.00  | ft    |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | 0.005 | ft/ft |
| Slopes of Main Basin Sides (Smain) =                    | 4     | H:V   |
| Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =       | 2     |       |
|   |       | _     |
|   |       |       |

| Initial Surcharge Area (A <sub>ISV</sub> ) =  | 184     | ft^2     |
|---|---------|----------|
| Surcharge Volume Length (L <sub>ISV</sub> ) = | 13.6    | ft       |
| Surcharge Volume Width (W <sub>ISV</sub> ) =  | 13.6    | ft       |
| Depth of Basin Floor (H <sub>FLOOR</sub> ) =  | 1.31    | ft       |
| Length of Basin Floor (L <sub>FLOOR</sub> ) = | 281.1   | ft       |
| Width of Basin Floor (W <sub>FLOOR</sub> ) =  | 144.7   | ft       |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =   | 40,689  | ft^2     |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) = | 19,067  | ft/3     |
| Depth of Main Basin (H <sub>MAIN</sub> ) =    | 3.19    | ft       |
| Length of Main Basin (L <sub>MAIN</sub> ) =   | 306.6   | ft       |
| Width of Main Basin (W <sub>MAIN</sub> ) =    | 170.2   | ft       |
| Area of Main Basin (A <sub>MAIN</sub> ) =     | 52,203  | ft^2     |
| Volume of Main Basin (V <sub>MAIN</sub> ) =   | 147,708 | ft/3     |
| Calculated Total Basin Volume (Vtotal) =      | 3.835   | acre-fee |
|   |         | _        |

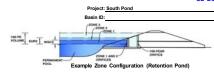
| Depth Increment =              |    |
|--------------------------------|----|
| Stage - Storage<br>Description | ** |
| Ton of Missonsol               |    |

| Stage - Storage<br>Description | Stage<br>(ft) | Override<br>Stage (ft) | Length<br>(ft) | Width<br>(ft)  | Area<br>(ft*2)   | Override<br>Area (ft/2) | Area<br>(acre) | Volume<br>(ft'3)   | Volume<br>(ac-ft) |
|--------------------------------|---------------|------------------------|----------------|----------------|------------------|-------------------------|----------------|--------------------|-------------------|
| Top of Micropool               | 0.00          | g_ (,                  | 13.6           | 13.6           | 184              |                         | 0.004          | ()                 | (== 1.7)          |
| ISV                            | 0.50          |                        | 13.6           | 13.6           | 184              |                         | 0.004          | 90                 | 0.002             |
|                                | 0.60          |                        | 13.6           | 13.6           | 184              |                         | 0.004          | 109                | 0.002             |
|                                | 0.70          |                        | 13.6           | 13.6           | 184              |                         | 0.004          | 127                | 0.003             |
|                                | 0.80          |                        | 13.6           | 13.6           | 184              |                         | 0.004          | 145                | 0.003             |
|                                | 0.90          |                        | 13.6           | 13.6           | 184              |                         | 0.004          | 164                | 0.004             |
|                                | 1.00          |                        | 13.6           | 13.6           | 184              |                         | 0.004          | 182                | 0.004             |
|                                | 1.10          |                        | 13.6           | 13.6           | 184              |                         | 0.004          | 201                | 0.005             |
|                                | 1.20          |                        | 13.6<br>13.6   | 13.6<br>13.6   | 184<br>184       |                         | 0.004          | 219<br>238         | 0.005             |
|                                | 1.40          |                        | 13.6           | 13.6           | 184              |                         | 0.004          | 256                | 0.006             |
|                                | 1.50          |                        | 13.6           | 13.6           | 184              |                         | 0.004          | 274                | 0.006             |
|                                | 1.60          |                        | 31.9           | 22.6           | 721              |                         | 0.017          | 315                | 0.007             |
|                                | 1.70          |                        | 52.3           | 32.6           | 1,704            |                         | 0.039          | 432                | 0.010             |
|                                | 1.80          |                        | 72.7           | 42.6           | 3,096            |                         | 0.071          | 669                | 0.015             |
|                                | 1.90          |                        | 93.1           | 52.6           | 4,896            |                         | 0.112          | 1,065              | 0.024             |
|                                | 2.00          |                        | 113.5          | 62.6           | 7,104            |                         | 0.163          | 1,662              | 0.038             |
|                                | 2.10          |                        | 136.0<br>156.4 | 73.6           | 10,004           |                         | 0.230          | 2,598<br>3,748     | 0.060             |
|                                | 2.20          |                        | 176.8          | 83.6<br>93.6   | 16,541           |                         | 0.300          | 5,225              | 0.086             |
|                                | 2.40          |                        | 197.2          | 103.6          | 20,421           |                         | 0.469          | 7,070              | 0.162             |
|                                | 2.50          |                        | 217.6          | 113.6          | 24,710           |                         | 0.567          | 9,323              | 0.214             |
|                                | 2.60          |                        | 238.0          | 123.6          | 29,406           |                         | 0.675          | 12,026             | 0.276             |
|                                | 2.70          |                        | 258.4          | 133.6          | 34,511           |                         | 0.792          | 15,218             | 0.349             |
|                                | 2.80          |                        | 278.8          | 143.6          | 40,024           |                         | 0.919          | 18,941             | 0.435             |
| Floor                          | 2.81          |                        | 280.8          | 144.6          | 40,597           |                         | 0.932          | 19,345             | 0.444             |
|                                | 2.90          |                        | 281.8          | 145.4          | 40,991           |                         | 0.941          | 23,019             | 0.528             |
|                                | 3.00          |                        | 282.6          | 146.2          | 41,334           |                         | 0.949          | 27,136             | 0.623             |
| Zone 1 (WQCV)                  | 3.09          |                        | 283.4          | 147.0          | 41,643           |                         | 0.956          | 30,870             | 0.709             |
|                                | 3.10<br>3.20  |                        | 283.4<br>284.2 | 147.0<br>147.8 | 41,677<br>42,022 |                         | 0.957<br>0.965 | 31,286<br>35,471   | 0.718<br>0.814    |
|                                | 3.20          |                        | 284.2          | 147.8          | 42,022           |                         | 0.965          | 39,691             | 0.814             |
|                                | 3.40          |                        | 285.8          | 149.4          | 42,716           |                         | 0.973          | 43,945             | 1.009             |
|                                | 3.50          |                        | 286.6          | 150.2          | 43,065           |                         | 0.989          | 48,234             | 1.107             |
|                                | 3.60          |                        | 287.4          | 151.0          | 43,415           |                         | 0.997          | 52,558             | 1.207             |
|                                | 3.70          |                        | 288.2          | 151.8          | 43,767           |                         | 1.005          | 56,917             | 1.307             |
|                                | 3.80          |                        | 289.0          | 152.6          | 44,119           |                         | 1.013          | 61,311             | 1.408             |
|                                | 3.90          |                        | 289.8          | 153.4          | 44,473           |                         | 1.021          | 65,741             | 1.509             |
|                                | 4.00          |                        | 290.6          | 154.2          | 44,829           |                         | 1.029          | 70,206             | 1.612             |
|                                | 4.10<br>4.20  |                        | 291.4<br>292.2 | 155.0<br>155.8 | 45,185<br>45,543 |                         | 1.037          | 74,707<br>79,243   | 1.715<br>1.819    |
|                                | 4.20          |                        | 292.2          | 156.6          | 45,902           |                         | 1.054          | 83,815             | 1.924             |
|                                | 4.40          |                        | 293.8          | 157.4          | 46,262           |                         | 1.062          | 88,424             | 2.030             |
|                                | 4.50          |                        | 294.6          | 158.2          | 46,624           |                         | 1.070          | 93,068             | 2.137             |
| Zone 2 (EURV)                  | 4.56          |                        | 295.1          | 158.7          | 46,842           |                         | 1.075          | 95,872             | 2.201             |
|                                | 4.60          |                        | 295.4          | 159.0          | 46,987           |                         | 1.079          | 97,748             | 2.244             |
|                                | 4.70          |                        | 296.2          | 159.8          | 47,351           |                         | 1.087          | 102,465            | 2.352             |
|                                | 4.80          |                        | 297.0          | 160.6          | 47,717           |                         | 1.095          | 107,219            | 2.461             |
|                                | 4.90          |                        | 297.8          | 161.4          | 48,084           |                         | 1.104          | 112,009            | 2.571             |
|                                | 5.00<br>5.10  |                        | 298.6<br>299.4 | 162.2<br>163.0 | 48,452<br>48,821 |                         | 1.112          | 116,836<br>121,699 | 2.682<br>2.794    |
|                                | 5.10          |                        | 300.2          | 163.8          | 49,192           |                         | 1.121          | 126,600            | 2.906             |
|                                | 5.30          |                        | 301.0          | 164.6          | 49,564           |                         | 1.138          | 131,538            | 3.020             |
|                                | 5.40          |                        | 301.8          | 165.4          | 49,937           |                         | 1.146          | 136,513            | 3.134             |
|                                | 5.50<br>5.60  |                        | 302.6<br>303.4 | 166.2<br>167.0 | 50,311<br>50,687 |                         | 1.155<br>1.164 | 141,525<br>146,575 | 3.249<br>3.365    |
|                                | 5.70          |                        | 304.2          | 167.8          | 51,064           |                         | 1.172          | 151,662            | 3.482             |
|                                | 5.80<br>5.90  |                        | 305.0          | 168.6<br>169.4 | 51,442<br>51,822 |                         | 1.181          | 156,788<br>161,951 | 3.599<br>3.718    |
| Zone 3 (100-year)              | 6.00          |                        | 305.8<br>306.6 | 170.2          | 52,203           |                         | 1.198          | 167,152            | 3.837             |
|                                | 6.10<br>6.20  |                        | 307.4<br>308.2 | 171.0<br>171.8 | 52,585<br>52,968 |                         | 1.207          | 172,391<br>177,669 | 3.958<br>4.079    |
|                                | 6.30          |                        | 309.0          | 172.6          | 53,353           |                         | 1.225          | 182,985            | 4.201             |
|                                | 6.40<br>6.50  |                        | 309.8<br>310.6 | 173.4<br>174.2 | 53,739<br>54,126 |                         | 1.234          | 188,340<br>193,733 | 4.324<br>4.447    |
|                                | 6.60          |                        | 311.4          | 175.0          | 54,515           |                         | 1.251          | 199,165            | 4.572             |
|                                | 6.70<br>6.80  |                        | 312.2<br>313.0 | 175.8<br>176.6 | 54,905<br>55,296 |                         | 1.260<br>1.269 | 204,636<br>210,146 | 4.824             |
|                                | 6.90<br>7.00  |                        | 313.8<br>314.6 | 177.4<br>178.2 | 55,688<br>56,082 |                         | 1.278          | 215,695<br>221,284 | 4.952<br>5.080    |
|                                | 7.10          |                        | 315.4          | 179.0          | 56,477           |                         | 1.297          | 226,912            | 5.209             |
|                                | 7.20<br>7.30  |                        | 316.2<br>317.0 | 179.8<br>180.6 | 56,873<br>57,270 |                         | 1.306<br>1.315 | 232,579<br>238,286 | 5.339<br>5.470    |
|                                | 7.40          |                        | 317.8          | 181.4          | 57,669           |                         | 1.324          | 244,033            | 5.602             |
|                                | 7.50<br>7.60  |                        | 318.6<br>319.4 | 182.2<br>183.0 | 58,069<br>58,471 |                         | 1.333          | 249,820<br>255,647 | 5.735<br>5.869    |
|                                | 7.70          |                        | 320.2          | 183.8          | 58,873           |                         | 1.352          | 261,514            | 6.004             |
|                                | 7.80<br>7.90  |                        | 321.0<br>321.8 | 184.6<br>185.4 | 59,277<br>59,682 |                         | 1.361<br>1.370 | 267,422<br>273,370 | 6.139<br>6.276    |
|                                | 8.00          |                        | 322.6          | 186.2<br>187.0 | 60,089<br>60,497 |                         | 1.379          | 279,358            | 6.413             |
|                                | 8.10<br>8.20  |                        | 323.4          | 187.8          | 60,906           |                         | 1.389          | 285,388            | 6.552             |
| -                              | 8.30          |                        | 325.0          | 188.6          | 61,316<br>61,728 |                         | 1.408          | 297,569<br>303,721 | 6.831             |
|                                | 8.40<br>8.50  |                        | 325.8<br>326.6 | 189.4<br>190.2 | 62,140           |                         | 1.417<br>1.427 | 309,914            | 6.972<br>7.115    |
| -                              | 8.60<br>8.70  |                        | 327.4<br>328.2 | 191.0<br>191.8 | 62,555<br>62,970 |                         | 1.436          | 316,149<br>322,425 | 7.258<br>7.402    |
|                                | 8.80          |                        | 329.0          | 192.6          | 63,387           |                         | 1.455          | 328,743            | 7.547             |
|                                | 8.90<br>9.00  |                        | 329.8<br>330.6 | 193.4<br>194.2 | 63,805<br>64,224 |                         | 1.465          | 335,103<br>341,504 | 7.693<br>7.840    |
|                                | 9.10          |                        | 331.4          | 195.0          | 64,644           |                         | 1.484          | 347,947            | 7.988             |
|                                | 9.20<br>9.30  |                        | 332.2<br>333.0 | 195.8<br>196.6 | 65,066<br>65,489 |                         | 1.494<br>1.503 | 354,433<br>360,961 | 8.137<br>8.287    |
|                                | 9.40          |                        | 333.8          | 197.4          | 65,914           |                         | 1.513          | 367,531            | 8.437             |
|                                | 9.50<br>9.60  |                        | 334.6<br>335.4 | 198.2<br>199.0 | 66,339<br>66,766 |                         | 1.523          | 374,143<br>380 799 | 8.589<br>8.742    |
|                                | 9.70          |                        | 336.2          | 199.8          | 67,195           |                         | 1.543          | 387,497            | 8.896             |
|                                | 9.80<br>9.90  |                        | 337.0<br>337.8 | 200.6<br>201.4 | 67,624<br>68.055 |                         | 1.552<br>1.562 | 394,238<br>401.022 | 9.050<br>9.206    |
|                                | 9.90          |                        | 33/.8          | 201.4          | 550,55           |                         | 1.562          | 401,022            | 9.206             |

North Pond.xlsm, Basin 10/3/2018, 2:59 PM

#### DETENTION BASIN STAGE-STORAGE TABLE BUILDER

UD-Detention, Version 3.07 (February 2017)



| quired Volume Calculation               |        |         |
|---|--------|---------|
| Selected BMP Type =                     | EDB    |         |
| Watershed Area =                        | 20.50  | acres   |
| Watershed Length =                      | 1,730  | ft      |
| Watershed Slope =                       | 0.035  | ft/ft   |
| Watershed Imperviousness =              | 95.00% | percent |
| Percentage Hydrologic Soil Group A =    | 0.0%   | percent |
| Percentage Hydrologic Soil Group B =    | 100.0% | percent |
| Percentage Hydrologic Soil Groups C/D = | 0.0%   | percent |
| Desired WQCV Drain Time =               | 40.0   | hours   |

| hours     | 40.0       | Desired WQCV Drain Time =              |
|-----------|------------|--|
| _         | User Input | Location for 1-hr Rainfall Depths =    |
| acre-feet | 0.764      | Water Quality Capture Volume (WQCV) =  |
| acre-feet | 2.192      | Excess Urban Runoff Volume (EURV) =    |
| acre-fee  | 1.883      | 2-yr Runoff Volume (P1 = 1.19 in.) =   |
| acre-fee  | 2.442      | 5-yr Runoff Volume (P1 = 1.5 in.) =    |
| acre-fee  | 2.940      | 10-yr Runoff Volume (P1 = 1.75 in.) =  |
| acre-fee  | 3.438      | 25-yr Runoff Volume (P1 = 2 in.) =     |
| acre-fee  | 3.842      | 50-yr Runoff Volume (P1 = 2.25 in.) =  |
| acre-fee  | 4.376      | 100-yr Runoff Volume (P1 = 2.52 in.) = |
| acre-fee  | 0.000      | 500-yr Runoff Volume (P1 = 0 in.) =    |
| acre-fee  | 1.768      | Approximate 2-yr Detention Volume =    |
| acre-fee  | 2.296      | Approximate 5-yr Detention Volume =    |
| acre-fee  | 2.796      | Approximate 10-yr Detention Volume =   |
| acre-fee  | 2.997      | Approximate 25-yr Detention Volume =   |
| acre-fee  | 3.110      | Approximate 50-yr Detention Volume =   |
| acre-fee  | 3.208      | Approximate 100-yr Detention Volume =  |
|           |            |  |

#### ge Calculatio

| age-Storage Calculation                                 |       |         |
|---|-------|---------|
| Zone 1 Volume (WQCV) =                                  | 0.764 | acre-fe |
| Zone 2 Volume (EURV - Zone 1) =                         | 1.428 | acre-fe |
| Zone 3 Volume (100-year - Zones 1 & 2) =                | 1.017 | acre-fe |
| Total Detention Basin Volume =                          | 3.208 | acre-fe |
| Initial Surcharge Volume (ISV) =                        | 100   | ft/3    |
| Initial Surcharge Depth (ISD) =                         | 0.50  | ft      |
| Total Available Detention Depth (H <sub>total</sub> ) = | 6.00  | ft      |
| Depth of Trickle Channel (H <sub>TC</sub> ) =           | 1.00  | ft      |
| Slope of Trickle Channel (S <sub>TC</sub> ) =           | 0.005 | ft/ft   |
| Slopes of Main Basin Sides (Smain) =                    | 4     | H:V     |
| Basin Length-to-Width Ratio (R <sub>L/W</sub> ) =       | 2     |         |
|   |       | _       |

|   |         | _       |
|---|---------|---------|
| Initial Surcharge Area (A <sub>ssv</sub> ) =  | 200     | ft^2    |
| Surcharge Volume Length (L <sub>ISV</sub> ) = | 14.1    | ft      |
| Surcharge Volume Width (W <sub>ISV</sub> ) =  | 14.1    | ft      |
| Depth of Basin Floor (H <sub>FLOOR</sub> ) =  | 1.15    | ft      |
| Length of Basin Floor (L <sub>FLOOR</sub> ) = | 249.6   | ft      |
| Width of Basin Floor (W <sub>FLOOR</sub> ) =  | 129.6   | ft      |
| Area of Basin Floor (A <sub>FLOOR</sub> ) =   | 32,350  | ft^2    |
| Volume of Basin Floor (V <sub>FLOOR</sub> ) = | 13,504  | ft/3    |
| Depth of Main Basin (H <sub>MAIN</sub> ) =    | 3.35    | ft      |
| Length of Main Basin (L <sub>MAIN</sub> ) =   | 276.4   | ft      |
| Width of Main Basin (W <sub>MAIN</sub> ) =    | 156.3   | ft      |
| Area of Main Basin (A <sub>MAIN</sub> ) =     | 43,216  | ft^2    |
| Volume of Main Basin (V <sub>MAIN</sub> ) =   | 125,964 | ft/3    |
| Calculated Total Basin Volume (Vtotal) =      | 3.209   | acre-fi |
| •   |         | _       |

| Stage - Storage<br>Description | Stage<br>(ft) | Optional<br>Override<br>Stage (ft) | Length<br>(ft) | Width<br>(ft)  | Area<br>(ft'2)   | Optional<br>Override<br>Area (ft'2) | Area<br>(acre) | Volume<br>(ft/3)   | Volume<br>(ac-ft) |
|--------------------------------|---------------|------------------------------------|----------------|----------------|------------------|-------------------------------------|----------------|--------------------|-------------------|
| Top of Micropool               | 0.00          | otage (II)                         | 14.1           | 14.1           | 200              | Area (IC2)                          | 0.005          | (103)              | (ac-it)           |
| ISV                            | 0.50          |                                    | 14.1           | 14.1           | 200              |                                     | 0.005          | 00                 | 0.000             |
| 15.V                           |               |                                    |                |                |                  |                                     |                | 98                 | 0.002             |
|                                | 0.60          |                                    | 14.1           | 14.1           | 200              |                                     | 0.005          | 118                | 0.003             |
|                                | 0.70          |                                    | 14.1           | 14.1           | 200              |                                     | 0.005          | 138                | 0.003             |
|                                | 0.80          |                                    | 14.1           | 14.1           | 200              |                                     | 0.005          | 158                | 0.004             |
|                                | 0.90          |                                    | 14.1           | 14.1           | 200              |                                     | 0.005          | 178                | 0.004             |
|                                | 1.00          |                                    | 14.1           | 14.1           | 200              |                                     | 0.005          | 198                | 0.005             |
|                                | 1.10          |                                    | 14.1           | 14.1           | 200              |                                     | 0.005          | 218                | 0.005             |
|                                | 1.20          |                                    | 14.1           | 14.1           | 200              |                                     | 0.005          | 238                | 0.005             |
|                                | 1.30          |                                    | 14.1           | 14.1           | 200              |                                     | 0.005          | 258                | 0.006             |
|                                | 1.40          |                                    | 14.1           | 14.1           | 200              |                                     | 0.005          | 278                | 0.006             |
|                                | 1.50          |                                    | 14.1           | 14.1           | 200              |                                     | 0.005          | 298                | 0.007             |
|                                | 1.60          |                                    | 32.5           | 23.1           | 752              |                                     | 0.017          | 340                | 0.008             |
|                                | 1.70          |                                    | 52.9           | 33.1           | 1,752            |                                     | 0.040          | 462                | 0.011             |
|                                | 1.80          |                                    | 73.3           | 43.1           | 3,161            |                                     | 0.073          | 704                | 0.016             |
|                                | 1.90          |                                    | 93.7           | 53.1           | 4,978            |                                     | 0.114          | 1,107              | 0.025             |
|                                | 2.00          |                                    | 114.1          | 63.1           | 7,203            |                                     | 0.165          | 1,713              | 0.039             |
|                                | 2.10          |                                    | 136.5          | 74.1           | 10,121           |                                     | 0.232          | 2,661              | 0.061             |
|                                | 2.20          |                                    | 156.9          | 84.1           | 13,203           |                                     | 0.303          | 3,824              | 0.088             |
|                                | 2.30          |                                    | 177.3          | 94.1           | 16,692           |                                     | 0.383          | 5,316              | 0.122             |
|                                | 2.40          |                                    | 197.7          | 104.1          | 20,590           |                                     | 0.473          | 7,176              | 0.165             |
|                                | 2.50          |                                    | 218.1          | 114.1          | 24,896           |                                     | 0.572          | 9,447              | 0.217             |
|                                | 2.60          |                                    | 238.5          | 124.1          | 29,609           |                                     | 0.680          | 12,169             | 0.279             |
| Floor                          | 2.65          |                                    | 248.7          | 129.1          | 32,119           |                                     | 0.737          | 13,712             | 0.315             |
|                                | 2.70          |                                    | 250.0          | 129.9          | 32,488           |                                     | 0.746          | 15,331             | 0.352             |
|                                | 2.80          |                                    | 250.8          | 130.7          | 32,793           |                                     | 0.753          | 18,595             | 0.427             |
|                                | 2.90          |                                    | 251.6          | 131.5          | 33,098           |                                     | 0.760          | 21,890             | 0.503             |
|                                | 3.00          |                                    | 252.4          | 132.3          | 33,406           |                                     | 0.767          | 25,215             | 0.503             |
|                                | 3.10          |                                    | 253.2          | 133.1          | 33,714           |                                     | 0.774          | 28,571             | 0.656             |
|                                | 3.10          |                                    | 253.2          | 133.1          | 34,024           |                                     | 0.774          | 31,958             | 0.734             |
| Zone 1 (WQCV)                  | 3.20          |                                    | 254.0          | 133.9          | 34,024           |                                     | 0.781          | 33,321             | 0.765             |
| Zone i (wqcv)                  |               |                                    |                |                | 34,335           |                                     |                |                    |                   |
|                                | 3.30          |                                    | 254.8          | 134.7          |                  |                                     | 0.788          | 35,376<br>38,825   | 0.812             |
|                                | 3.40          |                                    | 255.6          | 135.5          | 34,647           |                                     | 0.795          |                    | 0.891             |
|                                | 3.50          |                                    | 256.4          | 136.3          | 34,961           |                                     | 0.803          | 42,305             | 0.971             |
|                                | 3.60          |                                    | 257.2          | 137.1          | 35,275           |                                     | 0.810          | 45,817             | 1.052             |
|                                | 3.70          |                                    | 258.0          | 137.9          | 35,592           |                                     | 0.817          | 49,360             | 1.133             |
|                                | 3.80          |                                    | 258.8          | 138.7          | 35,909           |                                     | 0.824          | 52,935             | 1.215             |
|                                | 3.90          |                                    | 259.6          | 139.5          | 36,228           |                                     | 0.832          | 56,542             | 1.298             |
|                                | 4.00          |                                    | 260.4          | 140.3          | 36,548           |                                     | 0.839          | 60,181             | 1.382             |
|                                | 4.10          |                                    | 261.2          | 141.1          | 36,869           |                                     | 0.846          | 63,852             | 1.466             |
|                                | 4.20          |                                    | 262.0          | 141.9          | 37,191           |                                     | 0.854          | 67,555             | 1.551             |
|                                | 4.30          |                                    | 262.8          | 142.7          | 37,515           |                                     | 0.861          | 71,290             | 1.637             |
|                                | 4.40          |                                    | 263.6          | 143.5          | 37,840           |                                     | 0.869          | 75,058             | 1.723             |
|                                | 4.50          |                                    | 264.4          | 144.3          | 38,167           |                                     | 0.876          | 78,858             | 1.810             |
|                                | 4.60          |                                    | 265.2          | 145.1          | 38,494           |                                     | 0.884          | 82,691             | 1.898             |
|                                | 4.70          |                                    | 266.0          | 145.9          | 38,823           |                                     | 0.891          | 86,557             | 1.987             |
|                                | 4.80          |                                    | 266.8          | 146.7          | 39,153           |                                     | 0.899          | 90,456             | 2.077             |
|                                | 4.90          |                                    | 267.6          | 147.5          | 39,485           |                                     | 0.906          | 94,388             | 2.167             |
| Zone 2 (EURV)                  | 4.93          |                                    | 267.9          | 147.8          | 39,585           |                                     | 0.909          | 95,574             | 2.194             |
|                                | 5.00          |                                    | 268.4          | 148.3          | 39,818           |                                     | 0.914          | 98,353             | 2.258             |
|                                | 5.10          |                                    | 269.2          | 149.1          | 40,152           |                                     | 0.922          | 102,351            | 2.350             |
|                                | 5.20          |                                    | 270.0          | 149.9          | 40,487           |                                     | 0.929          | 106,383            | 2.442             |
|                                | 5.30          |                                    | 270.8          | 150.7          | 40,824           |                                     | 0.937          | 110,449            | 2.536             |
|                                | 5.40          |                                    | 271.6          | 151.5          | 41,162           |                                     | 0.945          | 114,548            | 2.630             |
|                                | 5.50          |                                    | 272.4          | 152.3          | 41,501           |                                     | 0.953          | 118,681            | 2.725             |
|                                | 5.60          |                                    | 273.2          | 153.1          | 41,841           |                                     | 0.961          | 122,848            | 2.820             |
|                                | 5.70<br>5.80  |                                    | 274.0<br>274.8 | 153.9<br>154.7 | 42,183<br>42,526 |                                     | 0.968          | 127,050<br>131,285 | 2.917<br>3.014    |
|                                | 5.90          |                                    | 275.6          | 155.5          | 42,870           |                                     | 0.984          | 135,555            | 3.112             |
| Zone 3 (100-year)              | 6.00          |                                    | 276.4          | 156.3          | 43,216<br>43,563 |                                     | 0.992          | 139,859<br>144,198 | 3.211             |
|                                | 6.10          |                                    | 277.2          | 157.1<br>157.9 | 43,563           |                                     | 1.000          | 144,198            | 3.310             |
|                                | 6.30          |                                    | 278.8          | 158.7          | 44,260           |                                     | 1.016          | 152,980            | 3.512             |
|                                | 6.40          |                                    | 279.6<br>280.4 | 159.5<br>160.3 | 44,611<br>44,963 |                                     | 1.024          | 157,424<br>161.902 | 3.614             |
|                                | 6.60          |                                    | 280.4          | 160.3          | 45,316           |                                     | 1.032          | 161,902<br>166,416 | 3.820             |
|                                | 6.70          |                                    | 282.0          | 161.9          | 45,671           |                                     | 1.048          | 170,966            | 3.925             |
|                                | 6.80          |                                    | 282.8<br>283.6 | 162.7<br>163.5 | 46,026           |                                     | 1.057<br>1.065 | 175,551<br>180,171 | 4.030<br>4.136    |
|                                | 7.00          |                                    | 284.4          | 164.3          | 46,384<br>46,742 |                                     | 1.065          | 184,827            | 4.136             |
|                                | 7.10          |                                    | 285.2          | 165.1          | 47,102           |                                     | 1.081          | 189,519            | 4.351             |
|                                | 7.20<br>7.30  |                                    | 286.0<br>286.8 | 165.9<br>166.7 | 47,462<br>47.825 |                                     | 1.090          | 194,248<br>199,012 | 4.459<br>4.569    |
|                                | 7.40          |                                    | 286.8          | 166.7          | 47,825<br>48,188 |                                     | 1.106          | 199,012<br>203,813 | 4.569             |
|                                | 7.50          |                                    | 288.4          | 168.3          | 48,553           |                                     | 1.115          | 208,650            | 4.790             |
|                                | 7.60          |                                    | 289.2          | 169.1<br>169.9 | 48,919<br>49,286 |                                     | 1.123          | 213,523            | 4.902             |
|                                | 7.70          |                                    | 290.0          | 170.7          | 49,286           |                                     | 1.131          | 218,434 223,381    | 5.015             |
|                                | 7.90          |                                    | 291.6          | 171.5          | 50,025           |                                     | 1.148          | 228,365            | 5.243             |
|                                | 8.00          |                                    | 292.4<br>293.2 | 172.3<br>173.1 | 50,396           |                                     | 1.157          | 233,386            | 5.358<br>5.474    |
|                                | 8.10<br>8.20  |                                    | 293.2          | 1/3.1          | 50,768<br>51.142 |                                     | 1.165          | 238,444            | 5.474             |
|                                | 8.30          |                                    | 294.8          | 174.7          | 51,517           |                                     | 1.183          | 248,672            | 5.709             |
|                                | 8.40<br>8.50  |                                    | 295.6<br>296.4 | 175.5<br>176.3 | 51,893<br>52,271 |                                     | 1.191          | 253,843            | 5.827<br>5.947    |
|                                | 8.60          |                                    | 297.2          | 176.3          | 52,271           |                                     | 1.209          | 259,051<br>264,297 | 5.947             |
|                                | 8.70          |                                    | 298.0          | 177.9          | 53,030           |                                     | 1.217          | 269,581            | 6.189             |
|                                | 8.80<br>8.90  |                                    | 298.8<br>299.6 | 178.7<br>179.5 | 53,411<br>53,794 |                                     | 1.226          | 274,903<br>280,263 | 6.311             |
|                                | 9.00          |                                    | 300.4          | 180.3          | 54,178           |                                     | 1.244          | 285,662            | 6.558             |
|                                | 9.10          |                                    | 301.2          | 181.1          | 54,563           |                                     | 1.253          | 291,099            | 6.683             |
|                                | 9.20<br>9.30  |                                    | 302.0<br>302.8 | 181.9<br>182.7 | 54,950<br>55,338 |                                     | 1.261          | 296,575<br>302,089 | 6.808<br>6.935    |
|                                | 9.40          |                                    | 303.6          | 183.5          | 55,727           |                                     | 1.279          | 302,089            | 7.062             |
|                                | 9.50          |                                    | 304.4          | 184.3          | 56,117           |                                     | 1.288          | 313,234            | 7.191             |
|                                | 9.60          |                                    | 305.2<br>306.0 | 185.1<br>185.9 | 56,509<br>56,902 |                                     | 1.297          | 318,866<br>324,536 | 7.320<br>7.450    |
|                                |               |                                    |                |                |                  |                                     |                |                    |                   |

South Pond.xlsm, Basin 12/7/2018, 8:12 AM

# Appendix B – Standard Design Charts and Tables



Chapter 6 Hydrology

Table 6-6. Runoff Coefficients for Rational Method

(Source: UDFCD 2001)

| Land Use or Surface<br>Characteristics            | Percent<br>Impervious | Runoff Coefficients |         |         |         |         |         |         |         |         |         |          |         |
|---|-----------------------|---------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|---------|
|   |                       | 2-year              |         | 5-year  |         | 10-year |         | 25-year |         | 50-year |         | 100-year |         |
|   |                       | HSG A&B             | HSG C&D | HSG A&B | HSG C&D | HSG A&B | HSG C&D | HSG A&B | HSG C&D | HSG A&B | HSG C&D | HSG A&B  | HSG C&D |
| Business  |                       |                     |         |         |         |         |         |         |         |         |         |          |         |
| Commercial Areas                                  | 95                    | 0.79                | 0.80    | 0.81    | 0.82    | 0.83    | 0.84    | 0.85    | 0.87    | 0.87    | 0.88    | 0.88     | 0.89    |
| Neighborhood Areas                                | 70                    | 0.45                | 0.49    | 0.49    | 0.53    | 0.53    | 0.57    | 0.58    | 0.62    | 0.60    | 0.65    | 0.62     | 0.68    |
| Residential                                       |                       |                     |         |         |         |         |         |         |         |         |         |          |         |
| 1/8 Acre or less                                  | 65                    | 0.41                | 0.45    | 0.45    | 0.49    | 0.49    | 0.54    | 0.54    | 0.59    | 0.57    | 0.62    | 0.59     | 0.65    |
| 1/4 Acre  | 40                    | 0.23                | 0.28    | 0.30    | 0.35    | 0.36    | 0.42    | 0.42    | 0.50    | 0.46    | 0.54    | 0.50     | 0.58    |
| 1/3 Acre  | 30                    | 0.18                | 0.22    | 0.25    | 0.30    | 0.32    | 0.38    | 0.39    | 0.47    | 0.43    | 0.52    | 0.47     | 0.57    |
| 1/2 Acre  | 25                    | 0.15                | 0.20    | 0.22    | 0.28    | 0.30    | 0.36    | 0.37    | 0.46    | 0.41    | 0.51    | 0.46     | 0.56    |
| 1 Acre  | 20                    | 0.12                | 0.17    | 0.20    | 0.26    | 0.27    | 0.34    | 0.35    | 0.44    | 0.40    | 0.50    | 0.44     | 0.55    |
| Industrial  |                       |                     |         |         |         |         |         |         |         |         |         |          |         |
| Light Areas                                       | 80                    | 0.57                | 0.60    | 0.59    | 0.63    | 0.63    | 0.66    | 0.66    | 0.70    | 0.68    | 0.72    | 0.70     | 0.74    |
| Heavy Areas                                       | 90                    | 0.71                | 0.73    | 0.73    | 0.75    | 0.75    | 0.77    | 0.78    | 0.80    | 0.80    | 0.82    | 0.81     | 0.83    |
| Parks and Cemeteries                              | 7                     | 0.05                | 0.09    | 0.12    | 0.19    | 0.20    | 0.29    | 0.30    | 0.40    | 0.34    | 0.46    | 0.39     | 0.52    |
| Playgrounds                                       | 13                    | 0.07                | 0.13    | 0.16    | 0.23    | 0.24    | 0.31    | 0.32    | 0.42    | 0.37    | 0.48    | 0.41     | 0.54    |
| Railroad Yard Areas                               | 40                    | 0.23                | 0.28    | 0.30    | 0.35    | 0.36    | 0.42    | 0.42    | 0.50    | 0.46    | 0.54    | 0.50     | 0.58    |
| Undeveloped Areas                                 |                       |                     |         |         |         |         |         |         |         |         |         |          |         |
| Historic Flow Analysis<br>Greenbelts, Agriculture | 2                     | 0.03                | 0.05    | 0.09    | 0.16    | 0.17    | 0.26    | 0.26    | 0.38    | 0.31    | 0.45    | 0.36     | 0.51    |
| Pasture/Meadow                                    | 0                     | 0.02                | 0.04    | 0.08    | 0.15    | 0.15    | 0.25    | 0.25    | 0.37    | 0.30    | 0.44    | 0.35     | 0.50    |
| Forest  | 0                     | 0.02                | 0.04    | 0.08    | 0.15    | 0.15    | 0.25    | 0.25    | 0.37    | 0.30    | 0.44    | 0.35     | 0.50    |
| Exposed Rock                                      | 100                   | 0.89                | 0.89    | 0.90    | 0.90    | 0.92    | 0.92    | 0.94    | 0.94    | 0.95    | 0.95    | 0.96     | 0.96    |
| Offsite Flow Analysis (when landuse is undefined) | 45                    | 0.26                | 0.31    | 0.32    | 0.37    | 0.38    | 0.44    | 0.44    | 0.51    | 0.48    | 0.55    | 0.51     | 0.59    |
| Streets   |                       |                     |         |         |         |         |         |         |         |         |         |          |         |
| Paved   | 100                   | 0.89                | 0.89    | 0.90    | 0.90    | 0.92    | 0.92    | 0.94    | 0.94    | 0.95    | 0.95    | 0.96     | 0.96    |
| Gravel  | 80                    | 0.57                | 0.60    | 0.59    | 0.63    | 0.63    | 0.66    | 0.66    | 0.70    | 0.68    | 0.72    | 0.70     | 0.74    |
| Drive and Walks                                   | 100                   | 0.89                | 0.89    | 0.90    | 0.90    | 0.92    | 0.92    | 0.94    | 0.94    | 0.95    | 0.95    | 0.96     | 0.96    |
| Roofs   | 90                    | 0.71                | 0.73    | 0.73    | 0.75    | 0.75    | 0.77    | 0.78    | 0.80    | 0.80    | 0.82    | 0.81     | 0.83    |
| Lawns   | 0                     | 0.02                | 0.04    | 0.08    | 0.15    | 0.15    | 0.25    | 0.25    | 0.37    | 0.30    | 0.44    | 0.35     | 0.50    |

#### 3.2 Time of Concentration

One of the basic assumptions underlying the Rational Method is that runoff is a function of the average rainfall rate during the time required for water to flow from the hydraulically most remote part of the drainage area under consideration to the design point. However, in practice, the time of concentration can be an empirical value that results in reasonable and acceptable peak flow calculations.

For urban areas, the time of concentration  $(t_c)$  consists of an initial time or overland flow time  $(t_i)$  plus the travel time  $(t_i)$  in the storm sewer, paved gutter, roadside drainage ditch, or drainage channel. For non-urban areas, the time of concentration consists of an overland flow time  $(t_i)$  plus the time of travel in a concentrated form, such as a swale or drainageway. The travel portion  $(t_i)$  of the time of concentration can be estimated from the hydraulic properties of the storm sewer, gutter, swale, ditch, or drainageway. Initial time, on the other hand, will vary with surface slope, depression storage, surface cover, antecedent rainfall, and infiltration capacity of the soil, as well as distance of surface flow. The time of concentration is represented by Equation 6-7 for both urban and non-urban areas.

Hydrology Chapter 6

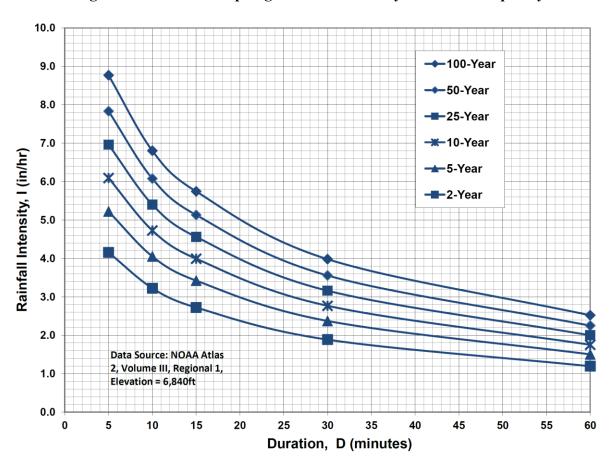


Figure 6-5. Colorado Springs Rainfall Intensity Duration Frequency

## **IDF Equations**

$$I_{100} = -2.52 \ln(D) + 12.735$$

$$I_{50} = -2.25 \ln(D) + 11.375$$

$$I_{25} = -2.00 \ln(D) + 10.111$$

$$I_{10} = -1.75 \ln(D) + 8.847$$

$$I_5 = -1.50 \ln(D) + 7.583$$

$$I_2 = -1.19 \ln(D) + 6.035$$

Note: Values calculated by equations may not precisely duplicate values read from figure. Hydrology Chapter 6

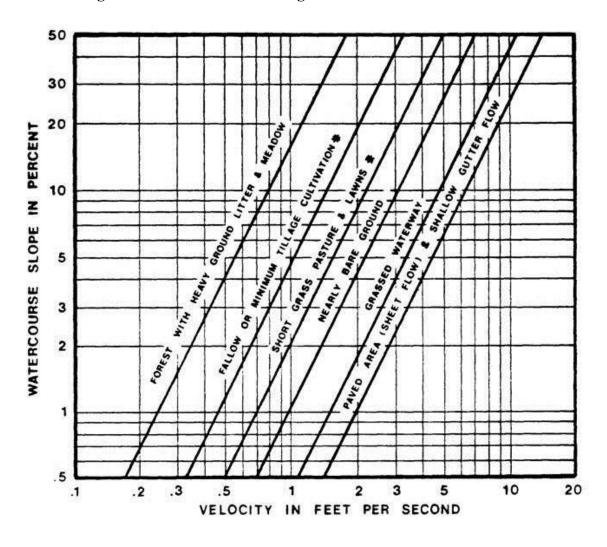


Figure 6-25. Estimate of Average Concentrated Shallow Flow

Table 13-2. Allowable Unit Release Rates (cfs/ac) (For 2-hour Design Storm w/ARC I CNs)

| Design Return  | NRCS Hydrologic Soil Group |      |      |  |  |  |  |  |
|----------------|----------------------------|------|------|--|--|--|--|--|
| Period (years) | A                          | В    | C&D  |  |  |  |  |  |
| 2              | 0.00                       | 0.01 | 0.04 |  |  |  |  |  |
| 5              | 0.00                       | 0.04 | 0.30 |  |  |  |  |  |
| 100            | 0.10                       | 0.30 | 0.50 |  |  |  |  |  |

# 2018 DRAINAGE, BRIDGE AND POND FEES CITY OF COLORADO SPRINGS

Effective January 1, 2018

|   |      |          | oandary 1, 20 |           | Pond        |            |  |
|---|------|----------|---------------|-----------|-------------|------------|--|
|   | DBPS | Drainage | Bridge        | Pond Land | Facility    | Surcharge/ |  |
| Basin Name                                | Year | Fee/Acre | Fee/Acre      | Fee/Acre  | Fee/Acre    | Acre       |  |
| 19th Street                               | 1964 | \$3,777  |               |           |             |            |  |
| 21st Street                               | 1977 | \$5,765  |               |           |             |            |  |
| Bear Creek                                | 1980 | \$3,710  | \$350         |           |             |            |  |
| Big Johnson, Crews                        | 1991 | \$14,354 | \$1,180       | \$241     |             |            |  |
| Black Squirrel Creek                      | 1989 | \$13,151 | \$1,502       | \$789     |             |            |  |
| Camp Creek                                | 1964 | \$2,127  |               |           |             |            |  |
| Cottonwood Creek <sup>1</sup>             | 2000 | \$13,241 | \$1,059       |           |             | \$678      |  |
| Douglas Creek                             | 1981 | \$11,929 | \$267         |           |             |            |  |
| Dry Creek <sup>2</sup>                    | 1966 | \$0.00   | ·             |           |             |            |  |
| Elkhorn Basin <sup>3</sup>                | n/a  | \$0.00   |               |           |             |            |  |
| Fishers Canyon⁴                           | 1991 | \$0.00   |               |           |             |            |  |
| Fountain Creek <sup>5</sup>               | n/a  | VAR      |               |           |             |            |  |
| Jimmy Camp Creek                          | 2015 | \$7,474  |               |           | \$2,436     |            |  |
| Kettle Creek <sup>6</sup> Old Ranch Trib. | 2001 | \$0.00   |               |           | ·           |            |  |
| Little Johnson                            | 1988 | \$12,528 |               | \$1,227   |             |            |  |
| Mesa                                      | 1986 | \$10,027 |               |           |             |            |  |
| Middle Tributary                          | 1987 | \$6,556  |               | \$1,121   |             |            |  |
| Miscellaneous <sup>7</sup>                | n/a  | \$11,157 |               |           |             |            |  |
| Monument Branch <sup>12</sup>             | 1987 | \$0.00   |               |           |             |            |  |
| North Rockrimmon                          | 1973 | \$5,766  |               |           |             |            |  |
| Park Vista (MDDP)                         | 2004 | \$16,059 |               |           |             |            |  |
| Peterson Field                            | 1984 | \$12,113 | \$558         |           |             |            |  |
| Pine Creek <sup>8</sup>                   | 1988 | \$0.00   |               |           |             |            |  |
| Pope's Bluff                              | 1976 | \$3,839  | \$657         |           |             |            |  |
| Pulpit Rock                               | 1968 | \$6,358  |               |           |             |            |  |
| Sand Creek <sup>9</sup>                   | 1996 | \$11,851 | \$713         | \$1,070   | \$3,445     | \$1,249    |  |
| Shooks Run <sup>10</sup>                  | 1994 | \$0.00   |               |           |             |            |  |
| Smith Creek <sup>11</sup>                 | 2002 | \$0.00   |               |           |             |            |  |
| South Rockrimmon                          | 1976 | \$4,508  |               |           |             |            |  |
| Southwest Area                            | 1984 | \$12,621 |               |           |             |            |  |
| Spring Creek                              | 1968 | \$9,943  |               |           |             |            |  |
| Templeton Gap                             | 1977 | \$6,558  | \$72          |           |             |            |  |
| Windmill Gulch                            | 1992 | \$13,678 | \$268         | \$3,055   | and the AFT |            |  |

All Drainage, Bridge and Detention Pond Facilities Fees adjusted by 5.7% over 2017 by City Council Resolution No. 157-17 on December 12, 2017 to be effective on January 1, 2018. \$58/acre increase to Sand Creek Drainage Fee approved by Board July 13, 2017. Land Fees are based on the Park Land Dedication Fee which is currently \$76,602/acre (0% change for inflation in 2017).

<sup>&</sup>lt;sup>1</sup> The 2018 Cottonwood Creek drainage fee consists of a capital improvement fee of \$10,172 per acre and land fee of \$3,069 per acre for a total of \$13,241 per acre. These fees are adjusted annually using different procedures but are combined for collection purposes. The surcharge fee of \$678/ac is due in cash; credits for prior facility construction cannot be used to offset this fee, which is deposited into a separate City fund known as the "Cottonwood Creek Surcharge" fund.

<sup>&</sup>lt;sup>2</sup> Dry Creek is a closed basin per City Council Resolution No. 118-08 on June 24, 2008

<sup>&</sup>lt;sup>3</sup> Elkhorn Basin is a closed basin per the Annexation Agreements for the area.

<sup>&</sup>lt;sup>4</sup> Fishers Canyon is a closed basin per City Council Resolution No. 74-08 on April 22, 2008.

<sup>&</sup>lt;sup>5</sup>Pursuant to the recommendation of the Subdivision Storm Drainage Board adopted at its meeting of September 15, 1977, there are exempted and excluded from the provisions of this part construction of the main Fountain Creek Channel from the confluence of Fountain Creek with Monument Creek northwest to the City limits. Land developments taking place adjacent to Fountain Creek shall remain responsible for dedicating rights of way necessary for the channelization of Fountain Creek, and the developers shall continue to pay to the City as a condition of subdivision plat approval the applicable drainage fees. Drainage fees are required in accordance with the appropriate basin study.

<sup>&</sup>lt;sup>6</sup> Kettle Creek Old Ranch Tributary is a closed basin per City Council Resolution 139-02 on August 27, 2002.

<sup>&</sup>lt;sup>7</sup> Miscellaneous fee is assessed on unstudied areas and the Roswell and Westside Basins.

<sup>&</sup>lt;sup>8</sup> Pine Creek is a closed basin per City Council Resolution No.236-88 on December 13, 1988.

<sup>&</sup>lt;sup>9</sup>Sand Creek Detention Pond #2 Surcharge (Ridgeview and Indigo Ranch) = \$1,249/ac. for 2018. Sand Creek Pond fees include two components, one for facility construction costs (\$4,515) and one for land dedication costs (\$1,070), the total Pond fee within Sand Creek is \$4,329/ac.

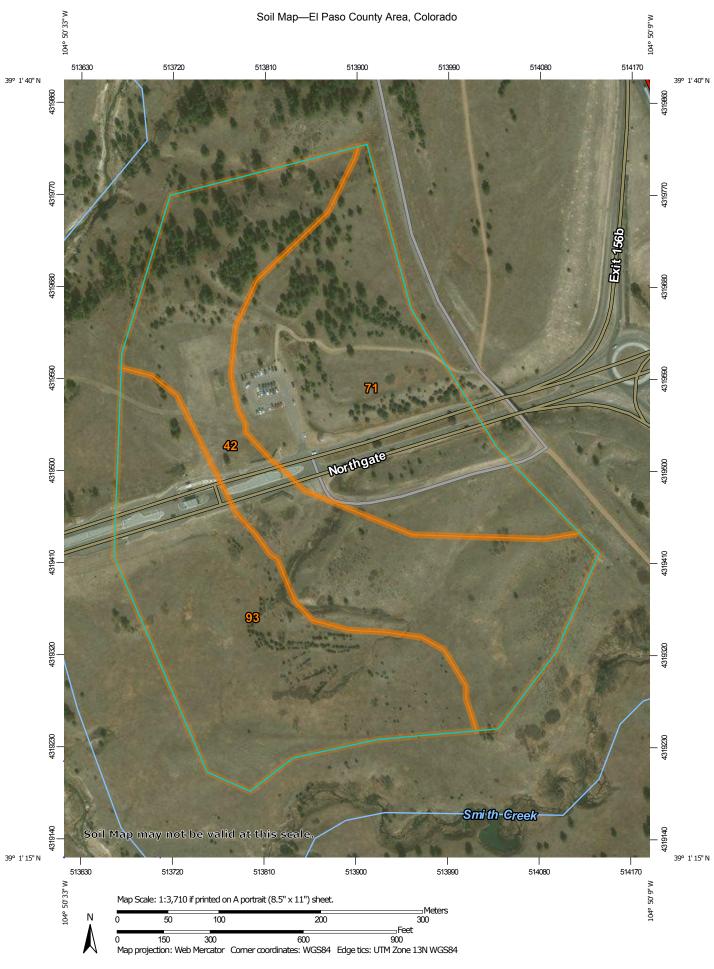
<sup>&</sup>lt;sup>10</sup> Shooks Run is a closed basin pursuant to the recommendation of the Drainage Board, adopted at its meeting on October 15, 1963.

<sup>&</sup>lt;sup>11</sup> Smith Creek is a closed basin per City Council Resolution 140-02 on August 27, 2002

<sup>&</sup>lt;sup>12</sup> Monument Branch Basin is a closed basin per City Council Res. 177-10 on October 12, 2010

# Appendix C – Maps





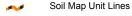
#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons



Soil Map Unit Points

#### Special Point Features

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Sandy Spot

Severely Eroded Spot

Saline Spot

Sinkhole

Slide or Slip

Sodic Spot

#### CLIND

Spoil Area

Stony Spot

Very Stony Spot

Wet Spot
Other

#### Water Features

Streams and Canals

#### Transportation

+++ Rails

Interstate Highways

US Routes

Major Roads

Local Roads

#### Background

Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Feb 22, 2014—Mar 9, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

# **Map Unit Legend**

| Map Unit Symbol             | Map Unit Name                                  | Acres in AOI | Percent of AOI |  |
|-----------------------------|--|--------------|----------------|--|
| 42                          | Kettle-Rock outcrop complex                    | 17.8         | 36.9%          |  |
| 71                          | Pring coarse sandy loam, 3 to 8 percent slopes | 15.0         | 31.0%          |  |
| 93                          | Tomah-Crowfoot complex, 8 to 15 percent slopes | 15.5         | 32.1%          |  |
| Totals for Area of Interest | 1  | 48.2         | 100.0%         |  |

# El Paso County Area, Colorado

## 42—Kettle-Rock outcrop complex

## **Map Unit Setting**

National map unit symbol: 368j Elevation: 6,800 to 7,700 feet Frost-free period: 110 to 130 days

Farmland classification: Not prime farmland

### **Map Unit Composition**

Kettle and similar soils: 60 percent

Rock outcrop: 20 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

### **Description of Kettle**

#### Setting

Landform: Hills

Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Sandy alluvium derived from arkose

### Typical profile

E - 0 to 16 inches: gravelly loamy sand Bt - 16 to 40 inches: gravelly sandy loam

C - 40 to 60 inches: extremely gravelly loamy sand

#### **Properties and qualities**

Slope: 8 to 40 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Somewhat excessively drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): High

(2.00 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

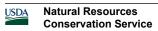
Land capability classification (nonirrigated): 7e

Hydrologic Soil Group: B Hydric soil rating: No

#### **Description of Rock Outcrop**

#### Typical profile

R - 0 to 60 inches: unweathered bedrock



## **Properties and qualities**

Slope: 8 to 60 percent

Depth to restrictive feature: 0 inches to lithic bedrock

Available water storage in profile: Very low (about 0.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydrologic Soil Group: D Hydric soil rating: No

## **Minor Components**

#### Other soils

Percent of map unit: Hydric soil rating: No

## **Data Source Information**

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017

# El Paso County Area, Colorado

## 71—Pring coarse sandy loam, 3 to 8 percent slopes

## **Map Unit Setting**

National map unit symbol: 369k Elevation: 6,800 to 7,600 feet

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Pring and similar soils: 85 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

## **Description of Pring**

#### Setting

Landform: Hills

Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Arkosic alluvium derived from sedimentary rock

#### Typical profile

A - 0 to 14 inches: coarse sandy loam
C - 14 to 60 inches: gravelly sandy loam

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High

(2.00 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 6.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: B

Ecological site: Loamy Park (R048AY222CO)

Hydric soil rating: No

#### **Minor Components**

#### Other soils

Percent of map unit: Hydric soil rating: No

### **Pleasant**

Percent of map unit: Landform: Depressions Hydric soil rating: Yes

# **Data Source Information**

Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017

# El Paso County Area, Colorado

## 93—Tomah-Crowfoot complex, 8 to 15 percent slopes

## **Map Unit Setting**

National map unit symbol: 36bb Elevation: 7,300 to 7,600 feet

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Tomah and similar soils: 50 percent Crowfoot and similar soils: 30 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

### **Description of Tomah**

#### Setting

Landform: Alluvial fans, hills

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Alluvium derived from arkose and/or residuum

weathered from arkose

## **Typical profile**

A - 0 to 10 inches: loamy sand E - 10 to 22 inches: coarse sand C - 48 to 60 inches: coarse sand

#### **Properties and qualities**

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat):

Moderately high to high (0.60 to 2.00 in/hr) Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Very low (about 2.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: B

Ecological site: Sandy Divide (R049BY216CO)

Hydric soil rating: No

#### **Description of Crowfoot**

#### Setting

Landform: Hills, alluvial fans

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium

### Typical profile

A - 0 to 12 inches: loamy sand E - 12 to 23 inches: sand

Bt - 23 to 36 inches: sandy clay loam C - 36 to 60 inches: coarse sand

# Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat):

Moderately high to high (0.60 to 2.00 in/hr) Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 4.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: B

Ecological site: Sandy Divide (R049BY216CO)

Hydric soil rating: No

#### **Minor Components**

## Other soils

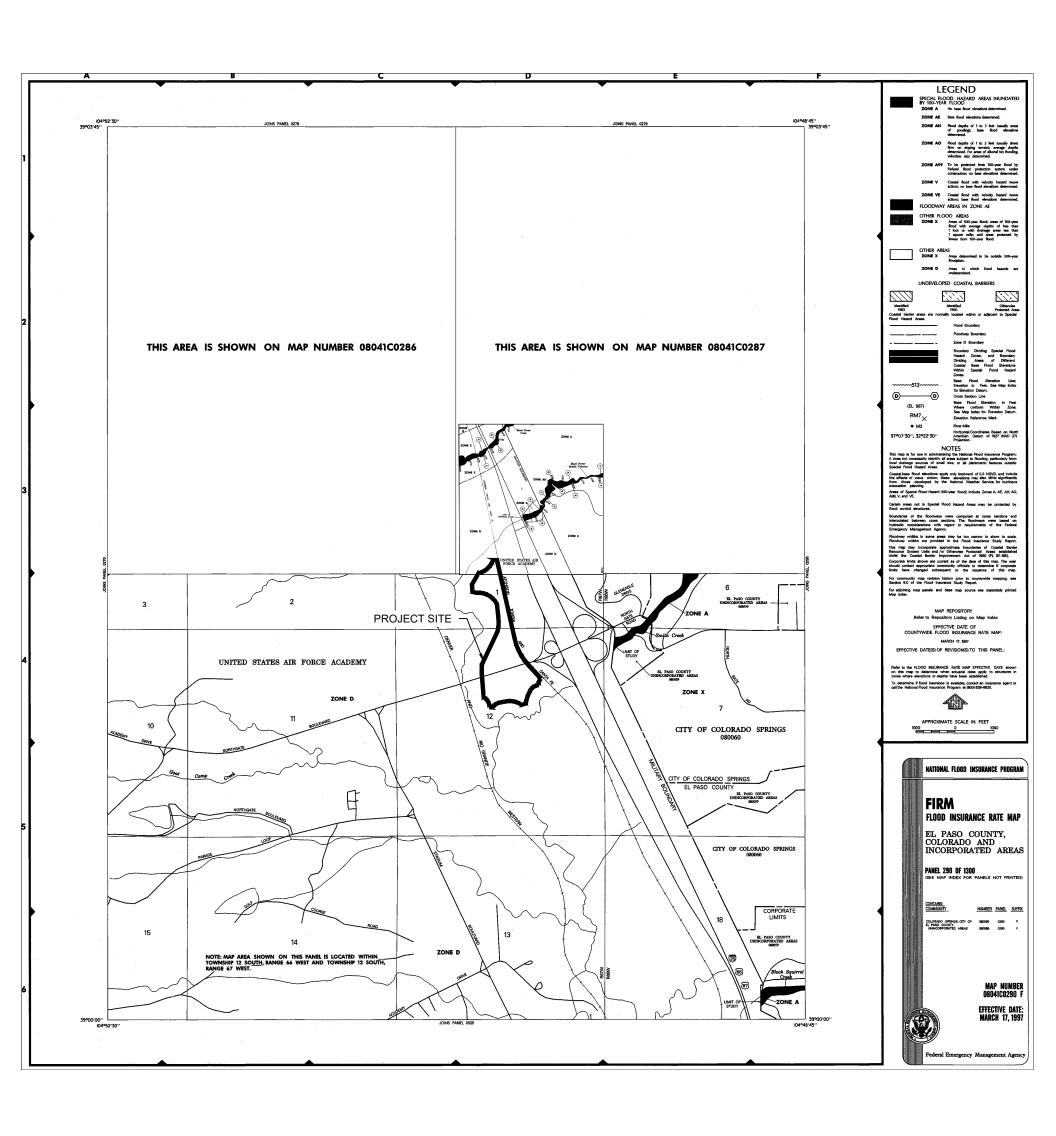
Percent of map unit: Hydric soil rating: No

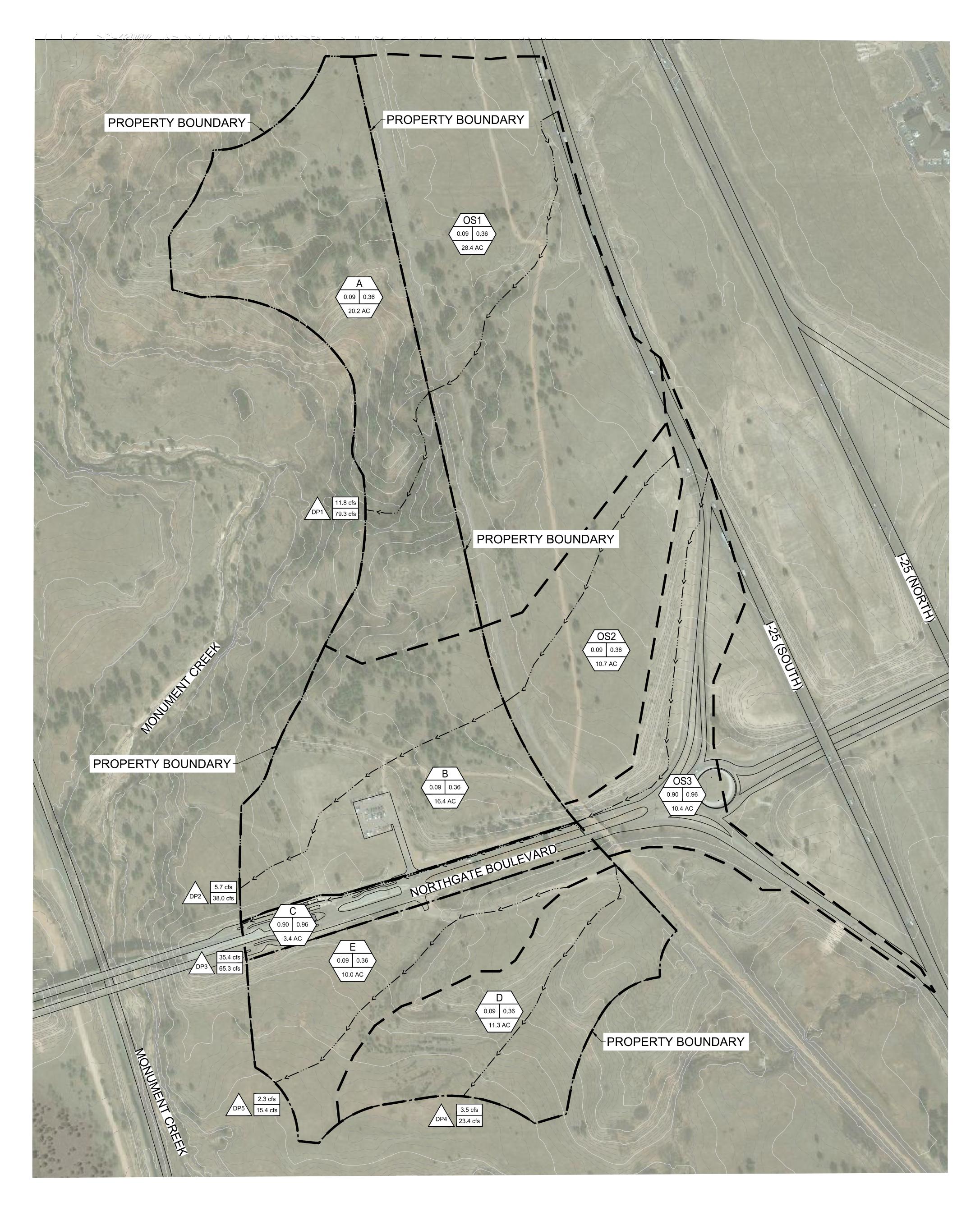
#### **Pleasant**

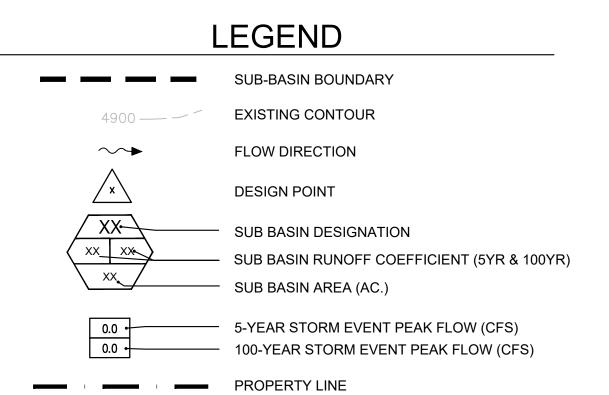
Percent of map unit: Landform: Depressions Hydric soil rating: Yes

### **Data Source Information**

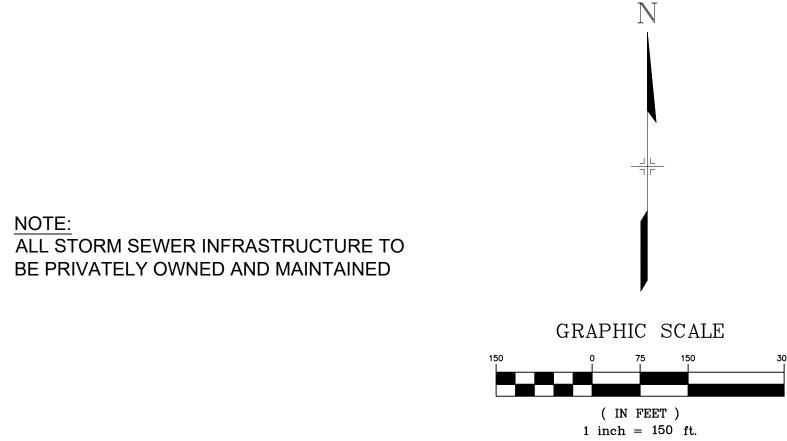
Soil Survey Area: El Paso County Area, Colorado Survey Area Data: Version 15, Oct 10, 2017

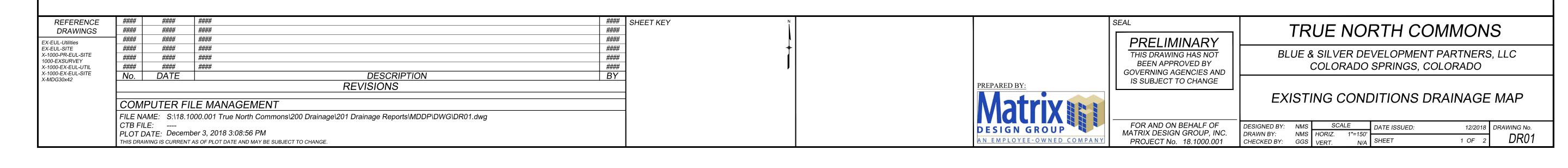




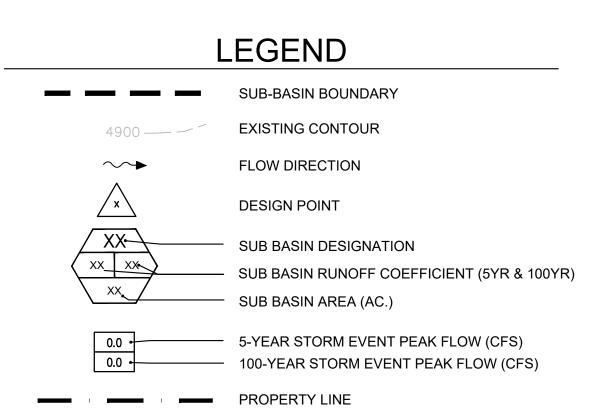


| Design Point Summa |            |  |  |  |
|--------------------|------------|--|--|--|
| ID                 | Q100 (cfs) |  |  |  |
| OS1                | 51.4       |  |  |  |
| OS2                | 17.1       |  |  |  |
| OS3                | 65.8       |  |  |  |
| Α                  | 43.9       |  |  |  |
| В                  | 29.6       |  |  |  |
| С                  | 13.2       |  |  |  |
| D                  | 23.4       |  |  |  |
| E                  | 15.4       |  |  |  |
| DP1                | 81.9       |  |  |  |
| DP2                | 38.0       |  |  |  |
| DP3                | 65.3       |  |  |  |
| DP4                | 23.4       |  |  |  |
| DP5                | 15.4       |  |  |  |

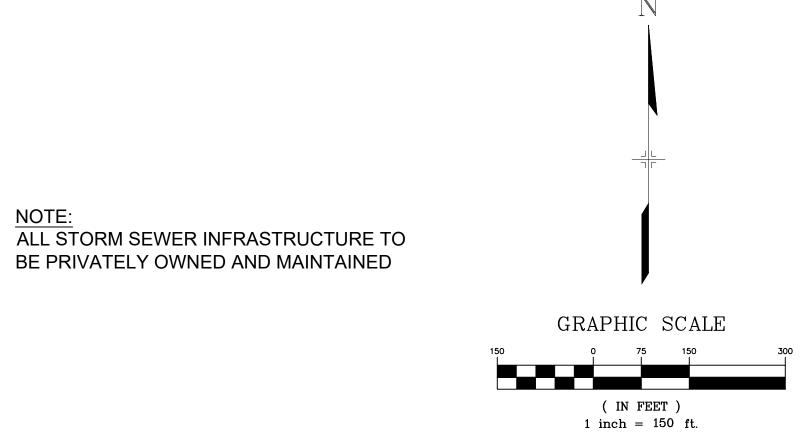


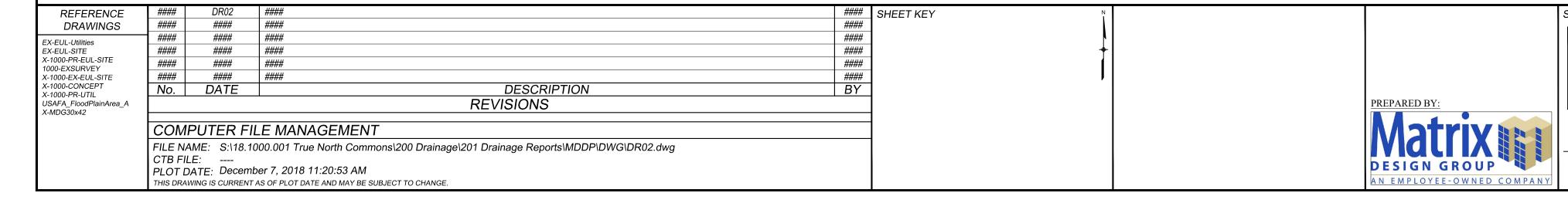


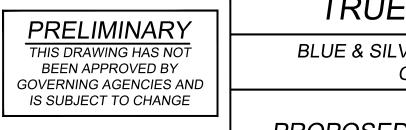




| ID  | Design Poir |      | Q100 (cfs) |
|-----|-------------|------|------------|
| OS1 | 28.44       | 7.6  | 51.4       |
| OS2 | 10.72       | 2.5  | 17.1       |
| OS3 | 10.43       | 35.7 | 65.8       |
| А   | 20.18       | 6.5  | 43.9       |
| B1  | 8.27        | 33.2 | 60.6       |
| B2  | 8.15        | 31.5 | 57.4       |
| С   | 3.43        | 7.1  | 13.2       |
| D   | 10.49       | 40.7 | 74.2       |
| E   | 9.97        | 37.2 | 67.9       |
| DP1 | 48.61       | 12.2 | 81.9       |
| DP2 | 18.99       | 20.9 | 50.5       |
| DP3 | 13.86       | 35.4 | 65.3       |
| DP4 | 22.00       | 56.9 | 104.8      |
| DP5 | 20.46       | 55.3 | 100.8      |







PROJECT No. 18.1000.001

TRUE NORTH COMMONS BLUE & SILVER DEVELOPMENT PARTNERS, LLC COLORADO SPRINGS, CO

2 OF 2

PROPOSED CONDITIONS DRAINAGE MAP DESIGNED BY: NMS SCALE DATE ISSUED:
DRAWN BY: NMS HORIZ. 1"=150'
CHECKED BY: GGS VERT. N/A SHEET FOR AND ON BEHALF OF MATRIX DESIGN GROUP, INC. 12/2018 DRAWING No. DR02