MASTER DEVELOPMENT DRAINAGE PLAN

Villages at Waterview North Colorado Springs, CO

Prepared for:

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Prepared by:

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Project #: 096955000

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Kimley »Horn



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CERTIFICATION

ENGINEERS STATEMENT

"This report and plan for the drainage design of the Villages at Waterview North project was prepared by me (or under my direct supervision) and is correct to the best of my knowledge and belief. Said report and plan has been prepared in accordance with the provisions of the City of Colorado Springs Drainage Criteria Manual and is in conformity with the master plan of the drainage basin. I understand that City of Colorado Springs does not and will not assume liability for drainage facilities designed by others. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report."



SIGNATURE:

01/12/2023

Date

Jessica J. McCallum, P.E. Colorado P.E. No. 59054

DEVELOPER'S STATEMENT

CPR Entitlements, LLC. hereby certifies that the drainage facilities for the Villages at Waterview North development shall be constructed according to the design presented in this report. I understand that the City of Colorado Springs does not and will not assume liability for the drainage facilities designed and/or certified by my engineer and that are submitted to the City of Colorado Springs pursuant to section 7.7.906 of the City Code; and cannot, on behalf of the Villages at Waterview North development guarantee that final drainage design review will absolve CPR Entitlements, LLC. and/or their successors and/or assigns of future liability for improper design. I further understand that approval of the final plat does not imply approval of my engineer's drainage design.

Name of Developer Authorized Signature

Printed Name

Title

Address: 🧹

CITY OF COLORADO SPRINGS STATEMENT

Filed in accordance with Section 7.7.906 of the Code of the City of Colorado Springs, 2001, as amended.

For City Engineer

2023/01/19

Date

Conditions:

INTRODUCTION

PURPOSE AND SCOPE OF STUDY

The purpose of this report is to outline the Master Development Drainage Plan (the "MDDP") associated with the Villages at Waterview North Concept Plan (the "Concept Plan") and annexation/ zone change into the City of Colorado Springs (the "City"). The Project is located on three parcels at the northeast corner of S. Powers Blvd and Bradley Rd (the "Site"), City of Colorado Springs, Colorado.

This MDDP identifies on-site and offsite drainage patterns, areas tributary to the site and proposes to safely route developed storm water to adequate outfalls at or less than historic flow rates. A Final Drainage Report for the master development roadways and infrastructure and for each individual lot and use containing detailed proposed site stormwater infrastructure design will be submitted at a later date and prior to construction of the individual lots and roadways. The Project will be processed through the City of Colorado Springs and is currently going through the annexation process with the City. Additional outside agency review or processing is not anticipated as part of the Project.

DBPS INVESTIGATIONS

This Site is located within West Fork Jimmy Camp Creek and Jimmy Camp Creek Drainage Basins per the "West Fork Jimmy Camp Creek Drainage Basin Planning Study" prepared by Kiowa Engineering Corporation, dated October 2003, and "Jimmy Camp Creek Drainage Basin Planning Study" prepared by Wilson & Company, dated 1987. The Site is also located in the Big Johnson Drainage Basin per the "Big Johnson Reservoir/Crews Gulch Drainage Basin Planning Study" prepared by Kiowa Engineering Corporation, dated September 1991. These reports serve as the current, approved DBPS for these basins. The proposed development will comply with the standards and required improvements set by the DBPS's.

GENERAL PROJECT DESCRIPTION

The Project is located on three parcels at the northeast corner of S. Powers Blvd and Bradley Rd within a portion of Section 8 and Section 9, both in Township 15 South, Range 65 West of the 6th P.M. El Paso County, Colorado. The Site is located within the Jimmy Camp Creek and Big Johnson Drainage Basins which are mostly vacant land. The Site is surrounded by:

- North: Peak Innovation Parkway, Lot 7 Colorado Springs Airport Filing No. 1D
- South: Bradley Road
- East: Colorado Centre Metro District, Lot 4 Colorado Centre Foreign Trade Zone & Business Park Filing No. 1
- West: S. Powers Boulevard

DESCRIPTION OF PROPERTY

The proposed improvements consist of community commercial, regional commercial, and medium and high to very high residential uses within the Site. The Project will also include construction of internal roadways and utility infrastructure which will be detailed in the infrastructure Final Drainage Report submitted at a later date.

The total Site is approximately 116.5 acres and consists of vacant land with native vegetation



within the Jimmy Camp Creek Basin and Big Johnson Basin. There is a ridge located in the western portion of the Site that splits the site into the two basins. The Jimmy Camp Creek Basin portion of the Site drains approximately west to east at grades that vary from 3% to 9%. The Big Johnson Basin portion of the Site drains approximately northeast to southwest at grades that vary from 3% to 10%.

There are no major irrigation facilities within the Site. The Site does not currently provide on-site water quality or detention for the Project area. There is no regional detention pond for the Project Site.

There is an existing gas main that runs along the east side of the property.

PROJECT CHARACTERISTICS

The Project Site is 116.5 acres and the proposed improvements consist of community commercial, regional commercial, and medium and high to very high residential uses within the Site.

The proposed project will route stormwater to the private temporary sediment basins ("TSB's") via the proposed temporary drainage swales. It is intended that the temporary sediment basins in the northwest corner, southwest corner, and southeast corner of the Site will be upgraded to full spectrum detention basins. The Full Spectrum Detention Basins will be designed and further discussed in the infrastructure Final Drainage Report.

There are no major irrigation facilities within the Site. The Site does not currently provide on-site water quality or detention for the Project area. There is no regional detention pond for the Project Site. The existing land use is vacant land.

DBPS COMPLIANCE

The proposed development will comply with the requirements, recommendations, and design intent set forth by West Fork Jimmy Camp Creek, Jimmy Camp Creek, and Big Johnson Reservoir DBPS's. The Project is not adjacent to any major drainage ways located within West Fork Jimmy Camp Creek, Jimmy Camp Creek, Jimmy Camp Creek or Big Johnson Reservoir.

SOIL CONDITIONS

NRCS soil data is available for this Site and it has been noted that soils onsite are generally USCS Type A and B. The NRSC Soils map is provided in **Appendix A**.

MAJOR DRAINAGEWAYS & STRUCTURES

Jimmy Camp Creek is located approximately 3,000 feet east of the Site. The Big Johnson Reservoir is located approximately 3,700 feet southwest of the Site.

EXISTING AND PROPOSED LAND USES

The existing use of the Site is vacant land. The proposed uses will consist of community commercial, regional commercial, and medium and high to very high residential uses within the Site.



HYDROLOGIC ANALYSIS

REGULATIONS

Water quality and detention are required for this Project per the City of Colorado Springs Drainage Criteria Manual (the "DCM"), dated May 2014, and revised January 2021. The Site proposes private temporary sediment basins to accompany the initial erosion control measures, concept plan, zone change, and annexation into the City of Colorado Springs. The infrastructure Drainage Report will provided detailed information and design for the permanent full spectrum detention ponds proposed on Site.

DESIGN CRITERIA REFERENCE AND CONSTRAINTS

The Project follows the City of Colorado Springs Storm Drainage Criteria Manual, Volumes 1 and 2 (the "DCM") and the MHFD Urban Storm Drainage Criteria Manual Volumes 1, 2, and 3 (the "MANUAL"). Project area drainage is not significantly impacted by such constraints as utilities or existing development. Further detail regarding on-site drainage patterns is provided in the Proposed Drainage Conditions Section.

HYDROLOGIC CRITERIA

The 5-year and 100-year design storm events were used in determining rainfall and runoff for the proposed drainage system per Section 6 of the DCM. Table 6-2 of the DCM is the source for rainfall data for the 5-year and 100-year design storm events. Design runoff was calculated using the Rational Method for developed conditions as established in the DCM and the USDCM. Runoff coefficients for the proposed development were determined using Table 6-6 of the DCM by calculating weighted impervious values for each specific site basin.

Temporary sediment basins were provided for the Site for the overlot grading construction associated with the initial erosion control permit. Temporary sediment basins were sized per the MANUAL fact sheet on sediment basins which is provided in **Appendix C**.

EXISTING DRAINAGE BASIN

The Project Site is a part of the Amendment to the Master Drainage Development Plan for Waterview, Waterview North prepared by Dakota Springs Engineering, dated February 2021 (the "MDDP Amendment"). The MDDP Amendment defines 9 basins on the Pre-Development Basin Map provided in **Appendix F.** The Site consists of the MDDP Amendment existing basins BJD-12c, BJDEX14, JCDEX3.1, JCDEX3.2, and JCDEX3.3.

MAJOR DRAINAGE BASIN DESCRIPTION

The Site is located in the Jimmy Camp Creek and Big Johnson Drainage Basins. Currently, the site consists of natural vegetation. The existing runoff from the Site is captured by existing storm sewer within S. Powers Boulevard and Bradley Road. The runoff eventually outfalls to either Jimmy Camp Creek or the Big Johnson Reservoir. The Pre-Development Basin Map from the MDDP Amendment with respective runoffs and calculations is provided in **Appendix F**.

The Project Site is split between the Big Johnson Drainage Basin and the Jimmy Camp Creek Drainage Basin. The release rate from the future full spectrum detention ponds will release flows

at or below the historic runoff values for each major drainage basin. The platted lots will pay fees to the respective drainage basins. A Major Basin Exhibit with calculations was provided in **Appendix G.**

PROPOSED BASIN DESCRIPTIONS

The proposed Site was divided into eleven sub-basins. Each of these sub-basins sheet flows to a temporary sediment basin in the overlot graded condition. Hydrologic calculations are provided in **Appendix B**. A Drainage Exhibit is provided in **Appendix F**.

SPECIFIC DETAILS

Sub-Basin 1

Sub-basin 1 is 19.06 acres and is anticipated to be developed primarily into a regional commercial use with a portion to be community commercial use per the Villages at Waterview North Master Plan. The runoff within this sub-basin will be captured by the basin 1 temporary swale and routed to the private temporary sediment basin 1. The 5-year and 100-year storm event runoffs are 66.15 cfs and 120.65 cfs, respectively. The runoff developed within this sub-basin ultimately discharges into the Big Johnson Drainage Basin.

Sub-Basin 2

Sub-basin 2 is 20.77 acres and is anticipated to be developed into a community commercial use per the Villages at Waterview North Master Plan. The runoff within this sub-basin will be captured by the basin 2 east and 2 south temporary swales and routed to the private temporary sediment basin 2. The 5-year and 100-year storm event runoffs are 72.34 cfs and 131.96 cfs, respectively. The runoff within this sub-basin is split with ultimate outfalls to Big Johnson and Jimmy Camp Creek.

Sub-Basin 3

Sub-basin 3 is 8.16 acres and is anticipated to be developed into a regional commercial use and residential high and very high use. The runoff within this sub-basin will be captured by the basin 3 temporary swale and routed to the private temporary sediment basin 3A. The 5-year and 100-year storm event runoffs are 33.27 cfs and 60.69 cfs, respectively. The runoff developed within this sub-basin ultimately discharges into the Jimmy Camp Creek Drainage Basin.

Sub-Basin 4

Sub-basin 3 is 7.86 acres and is anticipated to be developed into a regional commercial use and residential high and very high use. The runoff within this sub-basin will be captured by the basin 4 temporary swale and routed to the private temporary sediment basin 4A. The 5-year and 100-year storm event runoffs are 16.46 cfs and 34.97 cfs, respectively. The runoff developed within this sub-basin ultimately discharges into the Jimmy Camp Creek Drainage Basin.

Sub-Basin 5

Sub-basin 5 is 9.73 acres and is anticipated to be developed into a residential high and very high use. The runoff within this sub-basin will be captured by the basin 5 temporary swale and routed to the private temporary sediment basin 5. The 5-year and 100-year storm event runoffs are 21.15 cfs and 44.93 cfs, respectively. The runoff developed within this sub-basin ultimately discharges into the Jimmy Camp Creek Drainage Basin.



Sub-Basin 6

Sub-basin 6 is 26.44 acres and is anticipated to be developed into a residential high and very high use. The runoff within this sub-basin will be captured by the basin 6 north, 6 south, and 6 east temporary swales and routed to the private temporary sediment basin 6. The 5-year and 100-year storm event runoffs are 49.21 cfs and 104.53 cfs, respectively. The runoff developed within this sub-basin ultimately discharges into the Jimmy Camp Creek Drainage Basin.

Sub-Basin 7

Sub-basin 7 is 22.41 acres and is anticipated to be developed into a residential medium use. The runoff within this sub-basin will be captured by the basin 7 temporary swale and routed to the private temporary sediment basin 6. The 5-year and 100-year storm event runoffs are 41.88 cfs and 88.96 cfs, respectively. The runoff developed within this sub-basin ultimately discharges into the Jimmy Camp Creek Drainage Basin.

Sub-Basin RW-1 through RW-5

Sub-Basins RW-1 through RW-5 consist of the main shared access roads that connect each phase of the development. The roads traverse from Bradley Road to the north adjacent parcel and east to tie back into Bradley Road. Sub-Basins RW-1 through RW-5 are 1.61 acres, 1.33 acres, 0.60 acres, 0.65 acres, and 0.47 acres respectively. The 5-year storm event runoffs are 6.02 cfs, 5.72 cfs, 2.69 cfs, 2.79 cfs, and 2.16 cfs respectively. The 100-year storm event runoffs are 10.77 cfs, 10.25 cfs, 4.83 cfs, 5.01 cfs, and 3.87 cfs respectively.

HYDRAULIC ANALYSIS

The proposed private temporary sediment basins are designed in accordance with the MANUAL and the fact sheet provided in **Appendix C**.

The proposed temporary sediment basins are designed to capture and slow runoff during construction to allow time for the settling of sediment prior to discharge downstream. The temporary sediment basins were sized with at least 3,600 cubic feet per acre of drainage area upstream of the basin. The orifice plate or riser pipes were designed to accommodate an emptying time of approximately 72 hours. Temporary sediment basins 1, 2, and 6 have orifice plates and spillways sized utilizing the MHFCD UD Detention spreadsheet due to the drainage area going to these basins exceeding 15 acres. Temporary sediment basins 3A, 3B, 4A, 4B, and 5 are sized utilizing Table SB-1 for the Temporary Sediment Basin detail in the City of Colorado Springs Stormwater Construction Manual.

Hydraulic calculations for the temporary drainage swales were computed using Flowmaster. Hydraulic calculations are included in **Appendix D**.

The inlet, storm sewer sizing, and full spectrum detention designs will be complete with the infrastructure Drainage Report.

OUTLET REQUIREMENTS

The water quality standards established by the CRITERIA will be met by the proposed full spectrum extended detention basins designed by the infrastructure Final Drainage Report. The orifice plates will allow the WQCV to be drained from the structure in at least 40 hours and the EURV in 68-72 hours.

FEMA INFORMATION

The Federal Emergency Management Agency (FEMA), Flood Insurance Rate Map (FIRM) No. 80841C0768G, effective date December 7, 2018, indicated the Site is located in Zone X (Areas determined outside the 500-year floodplain).

ENVIRONMENTAL EVALUATIONS

FOUR-STEP PROCESS

The four-step process per the MANUAL provides guidance and requirements for the selection of siting of structural Best Management Practices (BMPs) for new development and significant redevelopment.

Step 1: Employ Runoff Reduction Practices

Temporary drainage swales and temporary sediment basins are provided to help reduce runoff and promote infiltration. The Colorado Springs Green Infrastructure Guidance Manual, dated March 2022, will be implemented with individual lot Final Drainage Reports.

Step 2: Implement BMPs That Provide a Water Quality Capture Volume with Slow Release

This MDDP is associated with the initial erosion control permit, Concept Plan, Master Plan, zone change, and annexation process which does not require the capture and treatment of the water quality capture volume at this time. Erosion control techniques are implemented throughout the development in the form of temporary drainage swales and temporary sediment basins. The temporary sediment basins provide risers pipes that provide an emptying time of approximately 72 hours. Permanent extended detention basins will be designed and constructed with the infrastructure Final Drainage Report for the infrastructure improvements for the development.

Step 3: Stabilize Drainageways

The Project Site is located more than 500' away from any major drainageways and there are no open channels located on or adjacent to the Site. The Project outfall is ultimately to Jimmy Camp Creek and Big Johnson.

All new and re-development projects are required to construct or participate in the funding of channel stabilization measures. Drainage basin fees paid, at the time of platting, go toward channel stabilization within the drainage basin.

Step 4: Implement Site Specific and Other Source Control BMPs

The Site does not require "Covering of Storage/Handling Areas" or "Spill Containment and Control" (specialized BMPs) in the final constructed condition. There is no proposed material storage or other site operations that would introduce contaminants to the County's MS4 that would require site specific control or source control BMP for the proposed project.

All flows leaving the Site will be released at the historic rates and are not anticipated to cause adverse impact to downstream facilities and additional off-site improvements are not required by this Project at this time.

OUTLET REQUIREMENTS

The water quality standards established by the CRITERIA will be met by the proposed full spectrum extended detention basins. The water quality outlet structures will be designed per the specifications in the CRITERIA. The outlet structure for the extended detention basin will meet the micro-pool requirement that it be integrated into the design of the structure with an additional surcharge volume. The orifice plates of the structures will be designed based on the CRITERIA. The orifice plates will allow the WQCV to be drained from the structure in at least 40 hours and the EURC in 72 hours.

GRADING AND EROSION CONTROL PLAN

Erosion Control Plans will be submitted separately as a standalone construction document.

OFFSITE DRAINAGE ANALYSIS

Per the MDDP Amendment, sub-basins BJD-12a, BJD-12b, JCD OS-1.A, and JCD OS-1.B on the offsite northern property surface flow south towards the Project Site. In the Final Drainage Report a 20' wide berm with a height of 2' will be designed spanning the portion of the northern property where the offsite drainage sheet flows south to the Project Site. This berm will then direct flow east following historical drainage patterns. If the north adjacent parcel is in construction for their proposed project, the berm will not be required as it is the responsibility of the north adjacent owner to capture and treat their on-site storm runoff.

Temporary sediment basin 3 discharges east to the east property line and eventually discharges to an existing drainage channel along Bradley Road. A proposed riprap pad was provided at the outfall of this discharge pipe. The riprap sizing will be re-evaluated during final design of the extended detention basin and these calculations will be provided in that Final Drainage Report.

DEVELOPMENT FEES

DRAINAGE AND BRIDGE FEES

The Project Site is located in the Big Johnson, West Fork Jimmy Camp Creek, and Jimmy Camp Creek Basins. Fees are not applicable with the Concept Plan. Fees will be calculated with each subsequent subdivision plat's final drainage report and the drainage fees will be paid at the time of final plat recordation.

CONSTRUCTION COST OPINION

An opinion of probable construction cost for the construction of the private and public drainage facilities for the Project will be included in the infrastructure Final Drainage Report. Each individual lot will provide their own construction cost opinion in the Final Drainage Report for their specific development.

SUMMARY

COMPLIANCE WITH STANDARDS

The drainage design presented within this report for Villages at Waterview North conforms to the CRITERIA and MANUAL. Site runoff and storm drain facilities are not anticipated to adversely affect the downstream and surrounding developments.



This report and findings are in general conformance with all previously approved reports and/or studies which include this Site. The proposed Project does not adversely impact the peak flows downstream within Jimmy Camp Creek or Big Johnson.

REFERENCES

- 1. City of Colorado Springs Drainage Criteria Manual, January 2021.
- 2. Mile High Flood District Drainage Criteria Manual Vol. 1, prepared by Wright-McLaughlin Engineers, June 2001, with latest revisions.
- 3. Flood Insurance Rate Map, El Paso County, Colorado and Incorporated Areas, Map Number 08041C0768G, Effective Date December 7, 2018, prepared by the Federal Emergency Management Agency (FEMA).
- 4. Amendment to Master Drainage Development Plan for Waterview, Waterview North, prepared by Dakota Springs Engineering, February 2021.
- 5. Big Johnson Reservoir/Crews Gulch Drainage Basin Planning Study, prepared by Kiowa Engineering Corporation, September 1991.
- 6. Jimmy Camp Creek Drainage Basin Planning Study, prepared by Kiowa Engineering Corporation, dated March 9, 2015.

APPENDIX A – SOILS MAP AND FEMA FIRM PANEL

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Conservation Service



USDA Natural Resources Conservation Service

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
8	Blakeland loamy sand, 1 to 9 percent slopes	A	38.3	33.1%
31	Fort Collins loam, 3 to 8 percent slopes	В	30.6	26.5%
56	Nelson-Tassel fine sandy loams, 3 to 18 percent slopes	В	30.0	26.0%
86	Stoneham sandy loam, 3 to 8 percent slopes	В	14.6	12.6%
95	Truckton loamy sand, 1 to 9 percent slopes	A	0.0	0.0%
108	Wiley silt loam, 3 to 9 percent slopes	В	2.0	1.7%
Totals for Area of Intere	st	115.6	100.0%	

Hydrologic Soil Group

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



National Flood Hazard Layer FIRMette



Legend

104°41'8"W 38°46'1"N SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT Without Base Flood Elevation (BFE) With BFE or Depth Zone AE, AO, AH, VE, AR SPECIAL FLOOD HAZARD AREAS **Regulatory Floodway** 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X Future Conditions 1% Annual Chance Flood Hazard Zone X Area with Reduced Flood Risk due to Levee. See Notes. Zone X OTHER AREAS OF FLOOD HAZARD Area with Flood Risk due to Levee Zone D NO SCREEN Area of Minimal Flood Hazard Zone X Effective LOMRs OTHER AREAS Area of Undetermined Flood Hazard Zone D - - - Channel, Culvert, or Storm Sewer GENERAL STRUCTURES Levee, Dike, or Floodwall 20.2 Cross Sections with 1% Annual Chance 17.5 Water Surface Elevation Coastal Transect Mase Flood Elevation Line (BFE) Limit of Study Jurisdiction Boundary **Coastal Transect Baseline** OTHER Profile Baseline 08041C0768G FEATURES Hydrographic Feature eff. 12/7/2018 Digital Data Available No Digital Data Available MAP PANELS Unmapped The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location. This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 7/7/2021 at 3:45 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time. This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for 104°40'31"W 38°45'33"N Feet 1:6,000 unmapped and unmodernized areas cannot be used for regulatory purposes. 0 250 500 1,000 1,500 2,000

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

APPENDIX B – HYDROLOGIC CALCULATIONS

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IDF Equations:

$I_{100} = -2.52 \ln(D) + 12.735$
l₅₀ = -2.25ln(D) + 11.375
l ₂₅ -2.00ln(D) + 10.111
l₁₀ -1.75ln(D) + 8.847
l₅ -1.50In(D) + 7.583
l₂ -1.19In(D) + 6.035

Where:

I = Rainfall Intensity (in/hr)
D= Duration (minutes)

	<u>2-yr</u>	<u>5-yr</u>	<u>10-yr</u>	<u>100-yr</u>
P1 =	1.19	1.5	1.75	2.52

*The Design Point Rainfall Values and Time Intensity Frequency Tabulation are found in Table 6-2 and Figure 6-5, respectively of the Colorado Springs Drainage Criteria Manual, Volume1

Weighted Imperviousness Calculations

SUB-	AREA	AREA	BASIN	SOIL GROUP	WEIGHTED	WEIGHTED COEFFICIENTS			S
BASIN	(SF)	(Acres)	DESIGNATION	DESIGNATION	IMPERVIOUSNESS	C2	C5	C10	C100
1	830,188	19.06	COMMERCIAL	А	95.0%	0.79	0.81	0.83	0.88
2	904,811	20.77	COMMERCIAL	В	95.0%	0.79	0.81	0.83	0.88
3	355,415	8.16	COMMERCIAL	А	95.0%	0.79	0.81	0.83	0.88
4	342,309	7.86	RESIDENTIAL	А	70.0%	0.45	0.49	0.53	0.62
5	423,625	9.73	RESIDENTIAL	А	70.0%	0.45	0.49	0.53	0.62
6	1,151,520	26.44	RESIDENTIAL	В	70.0%	0.45	0.49	0.53	0.62
7	976,336	22.41	RESIDENTIAL	В	70.0%	0.45	0.49	0.53	0.62
TOTAL	4,984,204	114.42							

10/19/2022 Calculated by: MGS

<u>ROADWAYS</u>

SUB-	AREA	AREA	BASIN	WEIGHTED	WEIG			
BASIN	(SF)	(Acres)	DESIGNATION	IMPERVIOUSNESS	C2	C5	C10	C100
RW-1	70025	1.60755	ROADWAY	100.0%	0.89	0.9	0.92	0.96
RW-2	57797	1.32684	ROADWAY	100.0%	0.89	0.9	0.92	0.96
RW-3	26088	0.5989	ROADWAY	100.0%	0.89	0.9	0.92	0.96
RW-4	28224	0.64793	ROADWAY	100.0%	0.89	0.9	0.92	0.96
RW-5	20293	0.46586	ROADWAY	100.0%	0.89	0.9	0.92	0.96
TOTAL	202,427	4.65			0.89	0.9	0.92	0.96

10/19/2022 Calculated by: MGS

Watervie	w North - D	rainage Rep	oort							Watercou	rse Coeffici	ent				
Proposed	Runoff Calc	ulations			Forest	& Meadow	2.50	Short G	rass Pastur	e & Lawns	7.00			Grassed	d Waterway	15.00
Time of C	Concentratio	n			Fallow or Cultivation 5.00			Nearly Bare Ground 10.00				Paved Area & Shallow Gut		llow Gutter	20.00	
	SUB-BASIN				INITIAL / OVERLAND			TRAVEL TIME				(110	T(c) CHECK		FINAL	
DESIGN	DRAIN	AREA	AREA	C(5)	Length	Slope	T(i)	Length	Slope	Coeff.	Velocity	T(t)	COMP.	TOTAL	L/180+10	1(C)
POINT	BASIN	sq. ft.	ac.		ft.	%	min	ft.	%		fps	min.	T(c)	LENGTH		min.
1	1	830,188	19.06	0.81	100	2.0%	4.2	817	2.0%	20.00	2.8	4.8	9.0	917	15.1	9.0
2	2	904,811	20.77	0.81	100	4.0%	3.3	1350	4.0%	20.00	4.0	5.6	8.9	1450	18.1	8.9
3	3	355,415	8.16	0.81	100	6.0%	2.9	690	5.0%	20.00	4.5	2.6	5.5	790	14.4	5.5
4	4	342,309	7.86	0.49	100	5.0%	6.5	690	5.0%	20.00	4.5	2.6	9.1	790	14.4	9.1
5	5	423,625	9.73	0.49	100	5.0%	6.5	440	5.0%	20.00	4.5	1.6	8.1	540	13.0	8.1
6	6	1,151,520	26.44	0.49	100	5.0%	6.5	1600	5.0%	20.00	4.5	6.0	12.5	1700	19.4	12.5
7	7	976,336	22.41	0.49	100	3.9%	7.1	1700	7.3%	20.00	5.4	5.2	12.3	1800	20.0	12.3
				1						1						
RW-1	RW-1	70,025	1.61	0.90	50	1.0%	2.6	1368	2.5%	20.00	3.2	7.2	9.8	1418	17.9	9.8
RW-2	RW-2	57,797	1.33	0.90	50	1.0%	2.6	920	4.0%	20.00	4.0	3.8	6.4	970	15.4	6.4
RW-3	RW-3	26,088	0.60	0.90	50	1.0%	2.6	720	4.0%	20.00	4.0	3.0	5.6	770	14.3	5.6
RW-4	RW-4	28,224	0.65	0.90	50	1.0%	2.6	795	3.0%	20.00	3.5	3.8	6.4	845	14.7	6.4
RW-5	RW-5	20,293	0.47	0.90	50	1.0%	2.6	550	3.5%	20.00	3.7	2.4	5.0	600	13.3	5.0

Waterview North - Drainage Report												
Proposed R	unoff Calculati	ons			Desi	gn Storm	5 Year					
(Rational Met	hod Procedure)				-	-						
B	ASIN INFORMATIC	N			DIRECT	RUNOFF		CL	IMMULAT	IVE RUNC	DFF	
DESIGN	DRAIN	AREA	RUNOFF	T(c)	CxA	Ι	Q	T(c)	CxA	-	Q	NOTES
POINT	BASIN	ac.	COEFF	min		in/hr	cfs	min		in/hr	cfs	
1	1	19.06	0.81	9.0	15.44	4.28	66.15					
2	2	20.77	0.81	8.9	16.82	4.30	72.34					
3	3	8.16	0.81	5.5	6.61	5.03	33.27					
4	4	7.86	0.49	9.1	3.85	4.28	16.46					
5	5	9.73	0.49	8.1	4.77	4.44	21.15					
6	6	26.44	0.49	12.5	12.95	3.80	49.21					
7	7	22.41	0.49	12.3	10.98	3.81	41.88					
	r											
RW-1	RW-1	1.61	0.90	9.8	1.45	4.16	6.02					
RW-2	RW-2	1.33	0.90	6.4	1.19	4.79	5.72					
RW-3	RW-3	0.60	0.90	5.6	0.54	5.00	2.69					
RW-4	RW-4	0.65	0.90	6.4	0.58	4.79	2.79					
RW-5	RW-5	0.47	0.90	5.0	0.42	5.15	2.16					

Waterview North - Drainage Report Proposed Runoff Calculations Design Storm 100 Year (Rational Method Procedure)												
	,											
E	BASIN INFORMATION	1		DIR	ECT RUNC	DFF		C	UMMULAT	IVE RUNO	FF	
DESIGN	DRAIN	AREA	RUNOFF	T(c)	CxA	 :/\	Q	T(c)	CxA	 :/\	Q	NOTES
PUINT	BASIN	ac.	CUEFF	min		in/nr	CTS	min		in/nr	CTS	
1	1	19.06	0.88	9.0	16.77	7.19	120.65					
2	2	20.77	0.88	8.9	18.28	7.22	131.96					
3	3	8.16	0.88	5.5	7.18	8.45	60.69					
4	4	7.86	0.62	9.1	4.87	7.18	34.97					
5	5	9.73	0.62	8.1	6.03	7.45	44.93					
6	6	26.44	0.62	12.5	16.39	6.38	104.53					
7	7	22.41	0.62	12.3	13.90	6.40	88.96					
RW-1	RW-1	1.61	0.96	9.8	1.54	6.98	10.77					
RW-2	RW-2	1.33	0.96	6.4	1.27	8.04	10.25					
RW-3	RW-3	0.60	0.96	5.6	0.57	8.39	4.83					
RW-4	RW-4	0.65	0.96	6.4	0.62	8.05	5.01					
RW-5	RW-5	0.47	0.96	5.0	0.45	8.65	3.87					

SUMMARY - PROPOSED RUNOFF TABLE											
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	IMPERVIOUSNESS (%)						
1	1	19.06	66.15	120.65	0.95						
2	2	20.77	72.34	131.96	0.95						
3	3	8.16	33.27	60.69	0.95						
4	4	7.86	16.46	34.97	0.70						
5	5	9.73	21.15	44.93	0.70						
6	6	26.44	49.21	104.53	0.70						
7	7	22.41	41.88	88.96	0.70						
RW-1	RW-1	1.61	6.02	10.77	100.00						
RW-2	RW-2	1.33	5.72	10.25	100.00						
RW-3	RW-3	0.60	2.69	4.83	100.00						
RW-4	RW-4	0.65	2.79	5.01	100.00						
RW-5	RW-5	0.47	2.16	3.87	100.00						

APPENDIX C – SEDIMENT BASIN FACT SHEET

Kimley **»Horn**

Description

A sediment basin is a temporary pond built on a construction site to capture eroded or disturbed soil transported in storm runoff prior to discharge from the site. Sediment basins are designed to capture site runoff and slowly release it to allow time for settling of sediment prior to discharge. Sediment basins are often constructed in locations that will later be modified to serve as post-construction stormwater basins.

Appropriate Uses

Most large construction sites (typically greater than 2 acres) will require one or more sediment basins for effective

Photograph SB-1. Sediment basin at the toe of a slope. Photo courtesy of WWE.

management of construction site runoff. On linear construction projects, sediment basins may be impractical; instead, sediment traps or other combinations of BMPs may be more appropriate.

Sediment basins should not be used as stand-alone sediment controls. Erosion and other sediment controls should also be implemented upstream.

When feasible, the sediment basin should be installed in the same location where a permanent postconstruction detention pond will be located.

Design and Installation

The design procedure for a sediment basin includes these steps:

- Basin Storage Volume: Provide a storage volume of at least 3,600 cubic feet per acre of drainage area. To the extent practical, undisturbed and/or off-site areas should be diverted around sediment basins to prevent "clean" runoff from mixing with runoff from disturbed areas. For undisturbed areas (both on-site and off-site) that cannot be diverted around the sediment basin, provide a minimum of 500 ft³/acre of storage for undeveloped (but stable) off-site areas in addition to the 3,600 ft³/acre for disturbed areas. For stable, developed areas that cannot be diverted around the sediment basin, storage volume requirements are summarized in Table SB-1.
- Basin Geometry: Design basin with a minimum length-to-width ratio of 2:1 (L:W). If this cannot be achieved because of site space constraints, baffling may be required to extend the effective distance between the

inflow point(s) and the outlet to minimize short-circuiting.

• **Dam Embankment**: It is recommended that embankment slopes be 4:1 (H:V) or flatter and no steeper than 3:1 (H:V) in any location.

Sediment Basins			
Functions			
Erosion Control	No		
Sediment Control	Yes		
Site/Material Management	No		

• **Inflow Structure**: For concentrated flow entering the basin, provide energy dissipation at the point of inflow.

Imperviousness (%)	Additional Storage Volume (ft ³) Per Acre of Tributary Area
Undeveloped	500
10	800
20	1230
30	1600
40	2030
50	2470
60	2980
70	3560
80	4360
90	5300
100	6460

Table SB-1. Additional Volume Requirements for Undisturbed and Developed Tributary Areas Draining through Sediment Basins

- **Outlet Works**: The outlet pipe shall extend through the embankment at a minimum slope of 0.5 percent. Outlet works can be designed using one of the following approaches:
 - **Riser Pipe (Simplified Detail):** Detail SB-1 provides a simplified design for basins treating no more than 15 acres.
 - **Orifice Plate or Riser Pipe**: Follow the design criteria for Full Spectrum Detention outlets in the EDB Fact Sheet provided in Chapter 4 of this manual for sizing of outlet perforations with an emptying time of approximately 72 hours. In lieu of the trash rack, pack uniformly sized 1¹/₂ to 2-inch gravel in front of the plate or surrounding the riser pipe. This gravel will need to be cleaned out frequently during the construction period as sediment accumulates within it. The gravel pack will need to be removed and disposed of following construction to reclaim the basin for use as a permanent detention facility. If the basin will be used as a permanent extended detention basin for the site, a trash rack will need to be installed once contributing drainage areas have been stabilized and the gravel pack and accumulated sediment have been removed.
 - Floating Skimmer: If a floating skimmer is used, install it using manufacturer's recommendations. Illustration SB-1 provides an illustration of a Faircloth Skimmer Floating Outlet[™], one of the more commonly used floating skimmer outlets. A skimmer should be designed to release the design volume in no less than 48 hours. The use of a floating skimmer outlet can increase the sediment capture efficiency of a basin significantly. A floating outlet continually decants cleanest water off the surface of the pond and releases cleaner water than would discharge from a perforated riser pipe or plate.



Illustration SB-1. Outlet structure for a temporary sediment basin - Faircloth Skimmer Floating Outlet. Illustration courtesy of J. W. Faircloth & Sons, Inc., FairclothSkimmer.com.

- **Outlet Protection and Spillway:** Consider all flow paths for runoff leaving the basin, including protection at the typical point of discharge as well as overtopping.
 - **Outlet Protection:** Outlet protection should be provided where the velocity of flow will exceed the maximum permissible velocity of the material of the waterway into which discharge occurs. This may require the use of a riprap apron at the outlet location and/or other measures to keep the waterway from eroding.
 - **Emergency Spillway:** Provide a stabilized emergency overflow spillway for rainstorms that exceed the capacity of the sediment basin volume and its outlet. Protect basin embankments from erosion and overtopping. If the sediment basin will be converted to a permanent detention basin, design and construct the emergency spillway(s) as required for the permanent facility. If the sediment basin will not become a permanent detention basin, it may be possible to substitute a heavy polyvinyl membrane or properly bedded rock cover to line the spillway and downstream embankment, depending on the height, slope, and width of the embankments.

SC-7

Maintenance and Removal

Maintenance activities include the following:

- Dredge sediment from the basin, as needed to maintain BMP effectiveness, typically when the design storage volume is no more than one-third filled with sediment.
- Inspect the sediment basin embankments for stability and seepage.
- Inspect the inlet and outlet of the basin, repair damage, and remove debris. Remove, clean and replace the gravel around the outlet on a regular basis to remove the accumulated sediment within it and keep the outlet functioning.
- Be aware that removal of a sediment basin may require dewatering and associated permit requirements.
- Do not remove a sediment basin until the upstream area has been stabilized with vegetation.

Final disposition of the sediment basin depends on whether the basin will be converted to a permanent post-construction stormwater basin or whether the basin area will be returned to grade. For basins being converted to permanent detention basins, remove accumulated sediment and reconfigure the basin and outlet to meet the requirements of the final design for the detention facility. If the sediment basin is not to be used as a permanent detention facility, fill the excavated area with soil and stabilize with vegetation.



TABLE SB-1. SIZING INFORMATION FOR STANDARD SEDIMENT BASIN			
Upstream Drainage Area (rounded to nearest acre), (ac)	Basin Bottom Width (W), (ft)	Spillway Crest Length (CL), (ft)	Hole Diameter (HD), (in)
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	12 ½ 21 28 33 ½ 43 47 ¼ 51 55 58 ¼ 61 64 67 ½ 70 ½ 73 ¼	2 3 5 6 8 9 11 12 13 15 16 18 19 21 22	932 ¹ ¥ 6 ½ 2 ½ 2 2 ⅓ 3 2 ⅓ 3 1 ∬ 6 1 ∬ 7 6 1 ∬ 7 7 6 1 ∬ 7 6 1 ∬ 7 7 8 1 1 1 1 1 1 1 1 1 1 1 1 1

SEDIMENT BASIN INSTALLATION NOTES

1. SEE PLAN VIEW FOR:

-LOCATION OF SEDIMENT BASIN.

-TYPE OF BASIN (STANDARD BASIN OR NONSTANDARD BASIN).

-FOR STANDARD BASIN, BOTTOM WIDTH W, CREST LENGTH CL, AND HOLE DIAMETER, HD. -FOR NONSTANDARD BASIN, SEE CONSTRUCTION DRAWINGS FOR DESIGN OF BASIN

INCLUDING RISER HEIGHT H, NUMBER OF COLUMNS N, HOLE DIAMETER HD AND PIPE DIAMETER D.

2. FOR STANDARD BASIN, BOTTOM DIMENSION MAY BE MODIFIED AS LONG AS BOTTOM AREA IS NOT REDUCED.

3. SEDIMENT BASINS SHALL BE INSTALLED PRIOR TO ANY OTHER LAND-DISTURBING ACTIVITY THAT RELIES ON ON BASINS AS AS A STORMWATER CONTROL.

4. EMBANKMENT MATERIAL SHALL CONSIST OF SOIL FREE OF DEBRIS, ORGANIC MATERIAL, AND ROCKS OR CONCRETE GREATER THAN 3 INCHES AND SHALL HAVE A MINIMUM OF 15 PERCENT BY WEIGHT PASSING THE NO. 200 SIEVE.

5. EMBANKMENT MATERIAL SHALL BE COMPACTED TO AT LEAST 95 PERCENT OF MAXIMUM DENSITY IN ACCORDANCE WITH ASTM D698.

6. PIPE SCH 40 OR GREATER SHALL BE USED.

7. THE DETAILS SHOWN ON THESE SHEETS PERTAIN TO STANDARD SEDIMENT BASIN(S) FOR DRAINAGE AREAS LESS THAN 15 ACRES. SEE CONSTRUCTION DRAWINGS FOR EMBANKMENT, STORAGE VOLUME, SPILLWAY, OUTLET, AND OUTLET PROTECTION DETAILS FOR ANY SEDIMENT BASIN(S) THAT HAVE BEEN INDIVIDUALLY DESIGNED FOR DRAINAGE AREAS LARGER THAN 15 ACRES.

SEDIMENT BASIN MAINTENANCE NOTES

1. INSPECT BMPs EACH WORKDAY, AND MAINTAIN THEM IN EFFECTIVE OPERATING CONDITION. MAINTENANCE OF BMPs SHOULD BE PROACTIVE, NOT REACTIVE. INSPECT BMPs AS SOON AS POSSIBLE (AND ALWAYS WITHIN 24 HOURS) FOLLOWING A STORM THAT CAUSES SURFACE EROSION, AND PERFORM NECESSARY MAINTENANCE.

2. FREQUENT OBSERVATIONS AND MAINTENANCE ARE NECESSARY TO MAINTAIN BMPs IN EFFECTIVE OPERATING CONDITION. INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE DOCUMENTED THOROUGHLY.

3. WHERE ${\sf BMPs}$ have failed, Repair or Replacement should be initiated upon discovery of the failure.

4. SEDIMENT ACCUMULATED IN BASIN SHALL BE REMOVED AS NEEDED TO MAINTAIN BMP EFFECTIVENESS, TYPICALLY WHEN SEDIMENT DEPTH REACHES ONE FOOT (I.E., TWO FEET BELOW THE SPILLWAY CREST).

5. SEDIMENT BASINS ARE TO REMAIN IN PLACE UNTIL THE UPSTREAM DISTURBED AREA IS STABILIZED AND GRASS COVER IS ACCEPTED BY THE LOCAL JURISDICTION.

6. WHEN SEDIMENT BASINS ARE REMOVED, ALL DISTURBED AREAS SHALL BE COVERED WITH TOPSOIL, SEEDED AND MULCHED OR OTHERWISE STABILIZED AS APPROVED BY LOCAL JURISDICTION.

(DETAILS ADAPTED FROM DOUGLAS COUNTY, COLORADO)

NOTE: MANY JURISDICTIONS HAVE BMP DETAILS THAT VARY FROM UDFCD STANDARD DETAILS. CONSULT WITH LOCAL JURISDICTIONS AS TO WHICH DETAIL SHOULD BE USED WHEN DIFFERENCES ARE NOTED.

TEMPORARY SEDIMENT BASIN TSB



City of Colorado Springs Stormwater Enterprise



Construction Control Measures December 2020
1.0 DESCRIPTION

• Temporary sediment basins are small impoundments of water with a small outlet structure built on a construction site.

2.0 PURPOSE

• Used to capture and slowly release runoff prior to discharge from a construction site to allow sediment to settle out.

3.0 IMPLEMENTATION

- Temporary sediment basins for drainage areas larger than 15 acres must be individually designed by engineer.
- Erosion and other sediment controls should be implemented upstream of temporary sediment basins.

4.0 TIMING

- Install prior to upstream land disturbance.
- Remove temporary sediment basin after upstream area has been stabilized. Permanently stabilize area after basin has been removed.

5.0 MAINTENANCE

- Remove sediment from basin as needed to maintain the effectiveness of the temporary sediment basin. This is typically when sediment depth reaches one foot.
- Inspect sediment basin embankments for stability and seepage.
- Inspect the inlet and outlet of the basin, repair damage, and remove debris.



Construction Control Measures December 2020



	TABLE SB-1, SIZING INFORMATION FOR STANDARD SEDIMENT BASIN											
and the second se	UPSTREAM DRAINAGE AREA (ROUNDED TO NEAREST ACRE), (AC)	HOLE DIAMETER (HD), (IN)										
	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	12½" 21 28 33½ 38½ 43 47¼ 51 55 58¼ 61 64 67½ 70½ 73¼	2 3 5 6 8 9 11 12 13 15 16 18 19 21 22	952 1376 1376 2552 2552 2552 2552 2552 2552 2552 25								

INSTALLATION NOTES

- FOR STANDARD BASIN, BOTTOM DIMENSION MAY BE MODIFIED AS LONG AS BOTTOM AREA IS NOT REDUCED.
- 2. EMBANKMENT MATERIAL SHALL CONSIST OF SOIL FREE OF DEBRIS, ORGANIC MATERIAL, AND ROCKS OR CONCRETE GREATER THAN 3 INCHES, AND SHALL HAVE A MINIMUM OF 15 PERCENT BY WEIGHT PASSING THE No. 200 SIEVE
- EMBANKMENT MATERIAL SHALL BE COMPACTED TO AT LEAST 95 PERCENT OF MAXIMUM DENSITY IN ACCORDANCE WITH ASTM D-698.
- 4. PIPE SCHEDULE 40 OR GREATER SHALL BE USED.
- 5. THE DETAILS SHOWN ON THESE SHEETS PERTAIN TO STANDARD SEDIMENT BASIN(S) FOR DRAINAGE AREAS LESS THAN 15 ACRES. SEE CONSTRUCTION DRAWINGS FOR EMBANKMENT, STORAGE VOLUME, SPILLWAY, OUTLET, AND OUTLET PROTECTION DETAILS FOR ANY SEDIMENT BASIN(S) THAT HAVE BEEN INDIVIDUALLY DESIGNED FOR DRAINAGE AREAS LARGER THAN 15 ACRES. DESIGN
- CALCULATIONS MUST BE APPROVED PRIOR TO IMPLEMENTATION.

TSB

MAINTENANCE NOTES

- FREQUENT OBSERVATIONS AND MAINTENANCE ARE NECESSARY TO MAINTAIN CONTROL MEASURES IN EFFECTIVE OPERATING CONDITION. INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE DOCUMENTED THOROUGHLY.
- 2. SEDIMENT ACCUMULATED IN BASIN SHALL BE REMOVED AS NEEDED TO MAINTAIN CONTROL MEASURE EFFECTIVENESS, TYPICALLY WHEN SEDIMENT DEPTH REACHES ONE FOOT (I.E. TWO FEET BELOW SPILLWAY CREST).
- SEDIMÉNT BASINS ARE TO REMAIN IN PLACE UNTIL THE UPSTREAM DISTURBED AREA IS PERMANENTLY STABILIZED.
- 4. PERMANENTLY STABILIZE AREA AFTER SEDIMENT BASIN REMOVAL.



APPENDIX D – SEDIMENT BASIN SIZING

Kimley **»Horn**

MHFD-Detention, Version 4.06 (July 2022)

	Project:	Temporary S	Sediment B	Basin 1				., 2022)							
Basin ID: 1															
	VOLUME EURY WOCY														
		1 410 2	100-YEA	AR E		Depth Increment =		ft							
	PERMANENT ORIFIC POOL ExampleZone	Configurat	ion (Reten	tion Pond)		Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume	Volume
		oomgulu		luon i onu,		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft ²)	(acre)	(ft ³)	(ac-ft)
	Watershed Information	EDR	1			Top of Micropool		0.00				39,339	0.903	41.254	0.047
	Waterched Area -	19.06	acree					2.00		-	-	43,170	1.093	91,259	1 984
	Watershed Length =	1,750	ft					3.00				51,161	1.174	135,590	3.113
	Watershed Length to Centroid =	840	ft					4.00	-	-		55,268	1.269	188,805	4.334
	Watershed Slope =	0.010	ft/ft												
	Percentage Hydrologic Soil Group A =	100.0%	percent												
	Percentage Hydrologic Soil Group B =	0.0%	percent							-	-				
	Percentage Hydrologic Soil Groups C/D =	0.0%	percent	Dupin Time	Teelong										
DRAIN TIME MATCHES	Location for 1-hr Rainfall Depthe	User Input		Drain Time	Too Long				-	-	-				
MHFCD TEMP SEDIMENT	After providing required inputs above inc	luding 1-hour	rainfall							-	-				
BASIN REQUIREMENTS	depths, click 'Run CUHP' to generate run the embedded Colorado Urban Hydro	off hydrograph graph Procedu	s using ıre.	Ontional Lise	ar Querridec										
	Water Quality Capture Volume (WQCV) =	0.024	acre-feet	Optional Ose	acre-feet										
	Excess Urban Runoff Volume (EURV) =	0.018	acre-feet		acre-feet				-						
	2-yr Runoff Volume (P1 = 1.19 in.) =	0.010	acre-feet	1.19	inches										
	10-yr Runoff Volume (P1 = 1.75 in.) =	0.027	acre-feet	1.75	inches					-					
	25-yr Runoff Volume (P1 = 2 in.) =	0.240	acre-feet	2.00	inches										
	50-yr Runoff Volume (P1 = 2.25 in.) = 100-yr Runoff Volume (P1 = 2.52 in.) =	0.482	acre-feet	2.25	inches										
	500-yr Runoff Volume (P1 = 3.14 in.) =	1.593	acre-feet	2.52	inches		-		-	-	-				
	Approximate 2-yr Detention Volume =	0.010	acre-feet		-						-				
	Approximate 5-yr Detention Volume = Approximate 10-yr Detention Volume =	0.014	acre-feet												
CALCULATED PER	Approximate 25-yr Detention Volume =	0.030	acre-feet												
REQUIREMENTS OF	Approximate 50-yr Detention Volume =	0.075	acre-feet												
3,600 CF PER -	Approximate 100-yr Detention Volume =	0.206	acre-feet												
DRAINAGE AREA (19.06*3.600 = 68.616.CE	Define Zones and Basin Geometry														
= 1.575 ACRE-FEET)	Zone 1 Volume (User Defined)	1.575	acre-feet						-						
	Select Zone 2 Storage Volume (Optional) = Select Zone 3 Storage Volume (Optional) =		acre-feet												
	Total Detention Basin Volume =	1.575	acre-feet						-						
	Initial Surcharge Volume (ISV) =	user	ft ³							-	-				
	Initial Surcharge Depth (ISD) = Total Available Detention Depth (Hum) =	user	ft ft										-	┟────┦	
	Depth of Trickle Channel (H_{TC}) =	user	ft						-						
	Slope of Trickle Channel (S _{TC}) =	user	ft/ft						-						
	Basin Length-to-Width Ratio (R _{1.00}) =	user	H:V												
											-				
	Initial Surcharge Area $(A_{ISV}) =$	user	ft²												
	Surcharge Volume Length (LESV) =	user	ft								-				
	Depth of Basin Floor (H _{FLOOR}) =	user	ft												
	Length of Basin Floor (L _{FLOOR}) =	user	ft ft												
	Area of Basin Floor (A _{FLOOR}) =	user	ft²												
	Volume of Basin Floor (V _{FLOOR}) =	user	ft ³						-						
	Length of Main Basin (HMAIN) =	user	ft ft												
	Width of Main Basin (W _{MAIN}) =	user	ft												
	Area of Main Basin (A _{MAIN}) =	user	ft 2												
	Calculated Total Basin Volume (V _{total}) =	user	π - acre-feet								-				
			4												
							-			-	-				
									-	-	-				
										-	-				
									-	-	-				
							-			-	-				
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							-			-	-				
							-			-	-				
											-				

MHFD-Detention, Version 4.06 (July 2022)



	J	LIENTION						
Project:	Temporary Sedime	nt Basin 1	MHFD-Detention, Ve	ersion 4.06 (July 20	022)			
Basin ID:	1							
ZONE 3				Estimated	Estimated			
				Stage (ft)	Volume (ac-ft)	Outlet Type	1	
VOLUME_ EURV WQCV			Zone 1 (User)	1.62	1.575	Orifice Plate		
ZONE 1 AND 2	100-YEAR ORIFICE		Zone 2					
PERMANENT ORIFICES POOL Example Zone	Configuration (Ret	ention Pond)	Zone 3					
				Total (all zones)	1.575			<i>.</i>
User Input: Orifice at Underdrain Outlet (typically i	N/A	In a Filtration BMP) ft (distance below t	he filtration media si	urface)	Under	drain Orifice Area =		ers for Underdrain
Underdrain Orifice Diameter =	N/A	inches			Underdrai	n Orifice Centroid =	N/A	feet
	•	1						
User Input: Orifice Plate with one or more orifices	or Elliptical Slot We	eir (typically used to	drain WQCV and/or	EURV in a sediment	ation BMP)		Calculated Paramet	ers for Plate
Centroid of Lowest Orifice =	0.00	ft (relative to basin	bottom at Stage = 0	ft)	WQ Orif	ice Area per Row =	1.542E-02	ft ⁻
Orifice Plate: Orifice Vertical Spacing =	6.50	inches	bottom at Stage = u	π)	Ell	iptical Hait-Width =	N/A N/A	feet
Orifice Plate: Orifice Area per Row =	2.22	sa, inches (diamete	r = 1-11/16 inches)		Empl	Elliptical Slot Area =	N/A N/A	ft ²
			, ,				,	
User Input: Stage and Total Area of Each Orifice R	Row (numbered from	n lowest to highest)						
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orlifice Centroid (it)	2.00	2 22	2.22					
	<i>L.LL</i>	<i>L.LL</i>	LILL	1				
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)								
Orifice Area (sq. inches)								
User Input: Vertical Orifice (Circular or Rectangula	ar)						Calculated Paramet	ers for Vertical Orific
	Not Selected	Not Selected]				Not Selected	Not Selected
Invert of Vertical Orifice =			ft (relative to basin	bottom at Stage = 0) ft) Ve	rtical Orifice Area =		
Depth at top of Zone using Vertical Orifice =			ft (relative to basin	bottom at Stage = 0) ft) Vertica	I Orifice Centroid =		
Vertical Orifice Diameter =			inches					
User Input: Overflow Weir (Dropbox with Flat or S	Sloped Grate and Ou	itlet Pipe OR Rectan	gular/Trapezoidal W	eir and No Outlet Pi	pe)		Calculated Paramet	ers for Overflow Wei
<u></u>	Not Selected	Not Selected					Not Selected	Not Selected
Overflow Weir Front Edge Height, Ho =			ft (relative to basin bo	ottom at Stage = 0 ft)	Height of Grat	e Upper Edge, H _t =		
				·····	5			
Overflow Weir Front Edge Length =			feet		Overflow V	Veir Slope Length =		
Overflow Weir Front Edge Length = Overflow Weir Grate Slope =			feet H:V foot	(Overflow V Grate Open Area / 10	Veir Slope Length = 00-yr Orifice Area =		
Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type =			feet H:V feet	((Overflow V Grate Open Area / 10 Overflow Grate Oper Overflow Grate Oper	Veir Slope Length = 00-yr Orifice Area = 1 Area w/o Debris = 2 Area w/ Debris =		
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Overflow Weir Front Edge Length = Overflow Weir Grate Slope = Horiz. Length of Weir Sides = Overflow Grate Type = Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate (Depth to Invert of Outlet Pipe = Circular Orifice Diameter = User Input: Emergency Spillway (Rectangular or T Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = Net-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = Predevelopment Peak Q (cfs) = Predevelopment Peak Q (cfs) = Preak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	Circular Orifice, Res Not Selected The user can overn WQCV N/A 0.024 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	trictor Plate, or Rect Not Selected ft (relative to basin feet H:V feet EURV N/A 0.018 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet H:V feet % angular Orifice) ft (distance below base inches bottom at Stage = 0 2 hydrographs and ru 2 Year 1.19 0.010 0.010 0.11 0.00 0.1 0.0 N/A Plate N/A N/A 53 60	in bottom at Stage = Half-Cer Half-Cer I ft) I f	Overflow V Grate Open Area / 10 Overflow Grate Open Overflow Grate Open State of Comparison Spillway D Stage at Basin Area at Basin Volume at Comparison Basin Volume at Comparison Comparison Comparison Overflow Grate Open Overflow Grate Open Ove	Veir Slope Length = 00-yr Orifice Area = A Area w/o Debris = an Area w/ Debris = alculated Parameter butlet Orifice Area = tt Orifice Centroid = ttor Plate on Pipe = Design Flow Depth= Top of Freeboard = Top of Freeboard = Top of Freeboard = Top of Freeboard = Con 0 0.240 0.223 0.00 0.12 0.00 0.12 0.00 0.12 0.00 0.12 0.00 0.12 0.00 0.12 0.00 0.12 0.00 0.12 0.00 0.12 0.00 0.00 0.00 0.12 0.00 0.0	s for Outlet Pipe w/ Not Selected N/A Calculated Paramet Calculated Pa	Flow Restriction Plate Not Selected N/A ers for Spillway feet feet acres acre-ft W through AF). 100 Year 2.52 0.814 0.814 7.8 0.1 0.814 7.8 0.1 0.0 Plate N/A N/A N/A >120
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DETENTION BASIN STAGE-STORAGE TABLE BUILDER MHFD-Detention, Version 4.04 (February 2021)

Project:	Waterview I	North Pone	d 1 Spillway Calcs					
Basin ID:	1							
ZONE 3	2							
100-YR		T						
VOLUME EURY WOCV		-						
	- /	100-YE	AR	Donth Incromont -		A		
ZONE	1 AND 2	ORIFIC		Depth Increment =		Optional		
POOL ExampleZone	Configurat	ion (Reter	ntion Pond)	Stage - Storage	Stage	Override	Length	Width
	5			Description	(ft)	Stage (ft)	(ft)	(ft)
Watershed Information				Top of Micropool		0.00		
Selected BMP Type =	EDB	1				1.00		
Meteorie and Arres	10.00		Assumed			2.00		
watershed Area =	19.06	acres	imperviousness		-	2.00		
Watershed Length =	1,750	î.	for Basin 1			3.00		
Watershed Length to Centroid =	840	ft	development			4.00		
Watershed Slope =	0.010	ft/ft	dorolopilioni		-			-
Watershed Imperviousness =	95.00%	percent						
Percentage Hydrologic Soil Group A =	100.0%	percent						
Porcontago Hudrologic Soil Crown R -	0.00%	norcont						
Percentage Hydrologic Soll Group B -	0.0%	percent						
Percentage Hydrologic Soli Groups C/D =	0.0%	percent						
Target WQCV Drain Time =	40.0	hours						
Location for 1-hr Rainfall Depths =	User Input							
After providing required inputs above inc	luding 1-hour	rainfall						
depths, dick 'Run CUHP' to generate run	off hydrograph	s using						
the embedded Colorado Urban Hydro	graph Procedu	re.	Optional User Override	S				
Water Quality Capture Volume (WOCV) =	0.710	acre-feet	acre-feet					
Excess Urban Runoff Volume (FURV) -	2,499	acre-feet	acre-feet					-
2-vr Runoff Volume (P1 = 1.10 in) =	1 799	acre-foot	1 19 inches					
2. yr Kunoff Volume (F1 = 1.19 III.) =	2 200	acre-feet	1.15 inches		-			
5-yr Runon Volume (P1 = 1.5 lh.) =	2.298	acrenteet	1.50 incres					
10-yr Kunott Volume (P1 = 1.75 in.) =	2./09	acre-feet	1./5 inches					-
25-yr Runoff Volume (P1 = 2 in.) =	3.136	acre-feet	2.00 inches					
50-yr Runoff Volume (P1 = 2.25 in.) =	3.559	acre-feet	2.25 inches					
100-yr Runoff Volume (P1 = 2.52 in.) =	4.025	acre-feet	2.52 inches					
500-yr Runoff Volume (P1 = 3.14 in.) =	5.083	acre-feet	inches					
Approximate 2-yr Detention Volume =	1.653	acre-feet						
Approximate 5-yr Detention Volume =	2 140	acre-feet						
Approximate 10-yr Detention Volume -	2 534	acro-foot						
Approximate 10 yr Detention Volume -	2.037	acre feet						
Approximate 25-yr Detention Volume =	2.977	acre-leet						
Approximate 50-yr Detenuon volume =	3.233	acre-reet			-			-
Approximate 100-yr Detention Volume =	3.449	acre-feet						
Define Zones and Basin Geometry		-						
Select Zone 1 Storage Volume (Required) =	0.710	acre-feet						
Zone 2 Volume (EURV - Zone 1) =	1.788	acre-feet						
Zone 3 Volume (100-year - Zones 1 & 2) =	0.951	acre-feet		-				
Total Detention Basin Volume -	3 449	acre-feet						
Initial Surshares Volume (ISV) =	3.115	a 3						
inicial Suichaige Volume (13V) -	usei				-		-	-
Initial Surcharge Depth (ISD) =	user	π						
Total Available Detention Depth (H _{total}) =	user	ft						
Depth of Trickle Channel (H _{TC}) =	user	ft						
Slope of Trickle Channel (STC) =	user	ft/ft			-		-	-
Slopes of Main Basin Sides (Smain) =	user	H:V						
Basin Length-to-Width Ratio (RL/W) =	user				-		-	-
Initial Surcharge Area (Arcu) =	user	ft 2		-				
Surcharge Volume Length (Liss) =	user	Ĥ						
Surcharge Volume Width (14) -	LICON	e.						
Dopth of Deale Volume Wildli (WISV) =	user	н. Ф			<u> </u>		<u> </u>	
Deput or Basin Floor (H _{FLOOR}) =	user				-		-	-
Length of Basin Floor (L _{FLOOR}) =	user	ní o						-
Width of Basin Floor (W _{FLOOR}) =	user	π						
Area of Basin Floor (A _{FLOOR}) =	user	ft í						
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³			-			-
Depth of Main Basin (H _{MAIN}) =	user	ft						
Length of Main Basin $(L_{MAIN}) =$	user	ft						
Width of Main Basin (WMAIN) =	user	ft						
Area of Main Basin (A) =	User	ft 2						
Volume of Main Pasis (V) -	LICON	⊕ 3						
Calculated Total Paris Values 01	usei	ncro 6						
calculated Total Basin Volume (V _{total}) =	user	acre-feet		-				
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		1.00				43,170	0.991	41,254	0.947
		2.00		-		47,171	1.083	86,425	1.984
		3.00				51,161	1.174	135,590	3.113
		4.00				55 268	1 260	188 805	4 334
		4.00				55,200	1.205	100,005	1.551
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Area (acre)

Override

Volume (ft³)

Volume (ac-ft)

Area (ft²)

MHFD-Detention, Version 4.04 (February 2021)



DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.04 (February 2021) Project: Waterview North Pond 1 Spillway Calcs Basin ID: 1 Estimated Estimated Stage (ft) Volume (ac-ft) Outlet Type LUME EURV WOCV Zone 0.76 0.710 Orifice Plate Orifice Plate ZONE 1 AND 2 Zone 2 (EURV) 2.47 1 788 100-YEAF Zone 3 (100-year) 0.951 3 29 Example Zone Configuration (Retention Pond) Total (all zones 3.449 User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP) Calculated Parameters for Underdrain Underdrain Orifice Invert Depth = ft (distance below the filtration media surface) Underdrain Orifice Area N/A N/A ft² Underdrain Orifice Diameter = N/A inches Underdrain Orifice Centroid = N/A User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP). Calculated Parameters for Plate Invert of Lowest Orifice : 0.00 ft (relative to basin bottom at Stage = 0 ft) WO Orifice Area per Row N/A ft² Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft) Elliptical Half-Width feet 2.47 N/A Orifice Plate: Orifice Vertical Spacing = Elliptical Slot Centroid = 9.90 inches feet N/A ft² Orifice Plate: Orifice Area per Row = sa. inches Elliptical Slot Area = N/Δ User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest Row 1 (required) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 5 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional) Stage of Orifice Centroid (ft) 0.00 0.82 1.65 Orifice Area (sg. inches) 0.00 0.00 0.00 Row 9 (optional) Row 10 (optional) Row 11 (optional) Row 12 (optional) Row 13 (optional) Row 14 (optional) Row 15 (optional) Row 16 (optional) Stage of Orifice Centroid (ft) Orifice Area (sq. inches) User Input: Vertical Orifice (Circular or Rectangular) Calculated Parameters for Vertical Orific Not Selected Not Selected Not Selected Not Selected Invert of Vertical Orifice ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area Depth at top of Zone using Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid = Vertical Orifice Diameter inches User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe) Calculated Parameters for Overflow We Not Selected Not Selected Not Selected Not Selected Overflow Weir Front Edge Height, Ho Height of Grate Upper Edge, Ht ft (relative to basin bottom at Stage = 0 ft) Overflow Weir Front Edge Length = Overflow Weir Slope Length = feet Grate Open Area / 100-yr Orifice Area H:V Overflow Weir Grate Slope = Horiz. Length of Weir Sides = feet Overflow Grate Open Area w/o Debris : Overflow Grate Type Overflow Grate Open Area w/ Debris = Debris Clogging % = % User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plat Not Selected Not Selected Not Selected Not Selected Depth to Invert of Outlet Pipe Outlet Orifice Area ft (distance below basin bottom at Stage = 0 ft) Outlet Orifice Centroid : Circular Orifice Diameter = inches Half-Central Angle of Restrictor Plate on Pipe N/A N/A User Input: Emergency Spillway (Rectangular or Trape Iculated Parameters for Spillway oidal) ft (relative to basin bottom at Stage = 0 ft) Spillway Invert Stage= 3.30 Spillway Design Flow Depth= 0.39 feet Spillway Crest Length = 75.00 feet Stage at Top of Freeboard = 4.69 feet Basin Area at Top of Freeboard Spillway End Slopes = 4.00 H:V 1.27 acres Freeboard above Max Water Surface = Basin Volume at Top of Freeboard = 4.33 1.00 feet acre-ft es in the Inflow Hydrogra Routed Hydrograph Results The user can override the default CUHP hs table (Columns W through AF) raphs and runoff volumes by a new valı Design Storm Return Period WQCV EURV 2 Year 10 Yea 25 Yea 50 Year 5 Year One-Hour Rainfall Depth (in) N/A 0.710 N/A 1.19 1.50 2.298 1.75 2.709 2.00 2.25 2.52 CLIHP Runoff Volume (acre-ft) 2,499 1.789 3.136 Inflow Hydrograph Volume (acre-ft) N/A N/A 1.789 2.298 2.709 3.136 3.559 4.025 CUHP Predevelopment Peak Q (cfs) N/A N/A 0.1 0.2 0.3 4.6 2.3 7.8 N/A OPTIONAL Override Predevelopment Peak Q (cfs) N/A 0.00 0.01 0.12 0.01 0.24 0.41 Predevelopment Unit Peak Flow, g (cfs/acre) N/A N/A Peak Inflow Q (cfs) N/A N/A 25.7 32.2 37.0 44.3 50.3 57.8 Peak Outflow Q (cfs) 8.0 1.4 Ratio Peak Outflow to Predevelopment Q 03 1.0 Structure Controlling Flow Spillway Spillway Max Velocity through Grate 1 (fps) N/A N/A Max Velocity through Grate 2 (fps) N/A N/A Time to Drain 97% of Inflow Volume (hours) >120 >120 Time to Drain 99% of Inflow Volume (hours) >120 >120

Maximum Ponding Depth (ft) :

Maximum Volume Stored (acre-ft) =

Area at Maximum Ponding Depth (acres)

3.41

1.21

3.33

1.21

MHFD-Detention, Version 4.06 (July 2022)

	Project:	Temporary S	Sediment I	Basin 2				.,,							
	Basin ID:	2													
		2 SONE 1													
		1		_				-							
	ZONE	1 AND 2	ORIFIC	AR CE		Depth Increment =		ft Ontional	1	1	1	Ontional	1	1	
	POOL ExampleZone	e Configurat	ion (Reter	ntion Pond)	Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
	Watershed Information					Top of Micropool		0.00				24,667	0.566	(IC)	(ac-it)
	Selected BMP Type =	EDB						1.00				27,384	0.629	26,025	0.597
	Watershed Area =	20.77	acres					2.00				30,245	0.694	54,840	1.259
	Watershed Length =	1,800	ft A					3.00				33,339	0.765	86,632	1.989
	Watershed Eength to Centrold = Watershed Slope =	0.040	ft/ft												
	Watershed Imperviousness =	2.00%	percent							-					
	Percentage Hydrologic Soil Group A = Percentage Hydrologic Soil Group B =	0.0%	percent												
	Percentage Hydrologic Soil Groups C/D =	0.0%	percent												
	Target WQCV Drain Time =	72.0	hours	Drain Tim	e Too Long										
	After providing required inputs at the loss	Deriver - Cap	rainfall												
DRAIN TIME MATCHES	depths, dick regulated to generate run	off hydrograph	s using												
BASIN REQUIREMENTS	Water Quality Canture Volume (WOCV) =	0.026	acre-feet	Optional Us	er Overrides										
Brownegowenerro	Excess Urban Runoff Volume (EURV) =	0.020	acre-feet		acre-feet										
	2-yr Runoff Volume (P1 = 1.19 in.) =	0.158	acre-feet	1.19	inches					-					
	5-yr Runoff Volume (P1 = 1.5 in.) = 10-yr Runoff Volume (P1 = 1.75 in.) =	0.455	acre-feet	1.50	inches										
	25-yr Runoff Volume (P1 = 2 in.) =	1.386	acre-feet	2.00	inches										
CALCULATED PER	50-yr Runoff Volume (P1 = 2.25 in.) =	1.780	acre-feet	2.25	inches										
MHFCD REQUIREMENTS OF	100-yr Runoff Volume (P1 = 2.52 in.) = 500-vr Runoff Volume (P1 = 3.14 in.) =	3.421	acre-feet	2.52	inches										
3,600 CF PER	Approximate 2-yr Detention Volume =	0.019	acre-feet												
DRAINAGE AREA	Approximate 5-yr Detention Volume =	0.033	acre-feet												
(20.77*3,600 = 74,772 CF = 1 717 ACRE-FEET)	Approximate 25-yr Detention Volume =	0.191	acre-feet								-				
in the force in EET)	Approximate 50-yr Detention Volume =	0.283	acre-feet												
	Approximate 100-yr Detention Volume =	0.388	acre-feet								-				
	Define Zones and Basin Geometry	\$													
	Zone 1 Volume (User Defined) =	1.717	acre-feet												
	Select Zone 2 Storage Volume (Optional) = Select Zone 3 Storage Volume (Optional) =		acre-feet acre-feet												
	Total Detention Basin Volume =	1.717	acre-feet												
	Initial Surcharge Volume (ISV) =	user	ft ³												
	Total Available Detention Depth (ISD) =	user	π ft												
	Depth of Trickle Channel (H _{TC}) =	user	ft												
	Slope of Trickle Channel (S _{TC}) =	user	ft/ft												
	Basin Length-to-Width Ratio (R _{L/W}) =	user	n.v								-				
		· /	•												
	Initial Surcharge Area (A _{ISV}) = Surcharge Volume Length (L _{ISV}) =	user	ft² ft												
	Surcharge Volume Width (W_{ISV}) =	user	ft												
	Depth of Basin Floor (H _{FLOOR}) =	user	ft												
	Length of Basin Floor (L _{FLOOR}) = Width of Basin Floor (W _{FLOOR}) =	user	π ft												
	Area of Basin Floor (A _{FLOOR}) =	user	ft²												
	Volume of Basin Floor (V _{FLOOR}) =	user	ft ³												
	Length of Main Basin (L _{MAIN}) =	user	ft												
	Width of Main Basin (W _{MAIN}) =	user	ft							-					
	Area of Main Basin (A _{MAIN}) = Volume of Main Basin (V _{MAIN}) =	user	ft ⁴ ft ³												
	Calculated Total Basin Volume (V _{total}) =	user	acre-feet												
											-				
										-					
										-	-				
										-	-				
										-	-				
										-					
						1						1			

MHFD-Detention, Version 4.06 (July 2022)



DETENTION BASIN OUTLET STRUCTURE DESIGN

Project:	Temporary Sedime	ent Basin 2	nn D-Detention, V	ersion 4.0	0 (<i>July</i> 2)	022)			
Basin ID:	2								
ZONE 3	_			Estim	ated	Estimated			
100-YR				Stage	e (ft)	Volume (ac-ft)	Outlet Type		
VOLUME EURV WOCV			Zone 1 (User)	2.0	54	1.717	Orifice Plate		
	100-YEAR ORIFICE		Zone 2						
PERMANENT ORIFICES			Zone 3					1	
Example Zone	Configuration (Rete	ention Pond)		Total (all zones)	1.717			
User Input: Orifice at Underdrain Outlet (typically u	used to drain WQCV	in a Filtration BMP)						Calculated Parameter	ers for Underdrain
Underdrain Orifice Invert Depth =	N/A	ft (distance below t	he filtration media s	urface)		Under	drain Orifice Area =	N/A	ft²
Underdrain Orifice Diameter =	N/A	inches				Underdraii	n Orifice Centroid =	N/A	feet
User Input: Orifice Plate with one or more orifices	or Elliptical Slot We	pir (typically used to	drain WOCV and/or	FLIRV in a	sediment	ation BMP)		Calculated Paramet	arc for Plato
Centroid of Lowest Orifice =	0.00	ft (relative to basin	bottom at Stage = () ft)	Scannen	WO Orif	ice Area per Row =	1.063E-02	ft ²
Depth at top of Zone using Orifice Plate =	2.64	ft (relative to basin	bottom at Stage = () ft)		Ell	iptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	10.60	inches				Ellipt	tical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	1.53	sq. inches (diamete	er = 1-3/8 inches)			E	Elliptical Slot Area =	N/A	ft ²
Licer Inputs Stage and Total Area of Each Orifice I	Dow (numbered from	n lowest to highest)							
User Input: Stage and Total Area of Each Onlice P	Row 1 (required)	Pow 2 (ontional)	Pow 3 (ontional)	Pow 4 (ntional)	Pow 5 (optional)	Pow 6 (optional)	Pow 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.88	1.76	1000 4 (0	ptional)	Kow 5 (optional)	Kow o (optional)	(optional)	Row o (optional)
Orifice Area (sq. inches)	1.53	1.53	1.53						
		-	-						
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)								<u> </u>	
User Input: Vertical Orifice (Circular or Rectangula	ar)							Calculated Paramet	ers for Vertical Orific
User input. Vertical Onnee (circular of Rectangua	Not Selected	Not Selected	1					Not Selected	Not Selected
Invert of Vertical Orifice =			ft (relative to basin	bottom at	Stage = 0) ft) Ve	rtical Orifice Area =		
Depth at top of Zone using Vertical Orifice =			ft (relative to basin	bottom at	Stage = 0) ft) Vertica	al Orifice Centroid =		
Vertical Orifice Diameter =			inches						
Licer Input: Overflow Weir (Drephov with Elst or 9	Slanad Crata and Or	itlat Dina OB Bactan	aular/Transzoidal W	oir and No	Outlot Di	20)		Calculated Daramet	are for Overflow We
Oser Input: Overnow Weir (Dropbox with Flat or s	Not Selected	Not Selected		eir and ind	Outlet Pi	<u>pe)</u>		Not Selected	Not Selected
Overflow Weir Front Edge Height, Ho =	Not Sciected	Not Sciected	ft (relative to basin b	ottom at St	aae = 0 ft	Height of Grat	e Upper Edge, H. =	Not Selected	NOL Selected
Overflow Weir Front Edge Length =			feet		, j	Overflow V	Veir Slope Length =		
Overflow Weir Grate Slope =			H:V		0	Grate Open Area / 10	00-yr Orifice Area =		
Horiz. Length of Weir Sides =			feet		C	Overflow Grate Open	Area w/o Debris =		
Overflow Grate Type =						Overflow Grate Ope	en Area w/ Debris =		
Debris Clogging % =			%						
User Input: Outlet Pipe w/ Flow Postriction Plate (Circular Orifica Boo	trictor Plata or Pact	angular Orifico)			C	alculated Parameter	c for Outlat Pipa w/	Elow Postriction Plat
	Not Selected	Not Selected				<u> </u>	alculated Farameter.	Not Selected	Not Selected
Depth to Invert of Outlet Pipe =			ft (distance below ba	sin bottom	at Stage =	0 ft) C	outlet Orifice Area =		
Circular Orifice Diameter =			inches			Outle	t Orifice Centroid =		
			-		Half-Cer	ntral Angle of Restric	ctor Plate on Pipe =	N/A	N/A
User Input: Emergency Spillway (Rectangular or T	rapezoidal)	a (hattan at Chana (C ill		Calculated Paramete	ers for Spillway
Spillway Croct Longth -		relative to basin	portoni at stage = () IL)		Spillway L	Top of Freeboard -	┟──────┘	feet
Spillway End Slopes =		H:V				Basin Area at	Top of Freeboard =		acres
Freeboard above Max Water Surface =		feet				Basin Volume at	Top of Freeboard =		acre-ft
Doutod Hydrograph Doculto	The user can over	ida tha dafault CUU	budrographs and r	upoff volu	noc hu on	toring now values in	the Inflow Hydroar	anha tabla (Column)	M through AE
Design Storm Return Period =	WOCV	FURV	2 Year	5 Y	ear	10 Year	25 Year	50 Year	100 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1.	50	1.75	2.00	2.25	2.52
CUHP Runoff Volume (acre-ft) =	0.026	0.034	0.158	0.4	55	0.769	1.386	1.780	2.374
Innow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak () (cfs) =	N/A N/A	N/A N/A	2.0	0.4	55 7	0.769	1.386	1.780	2.3/4 24.9
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.10	0.2	27	0.42	0.75	0.94	1.20
Peak Inflow Q (cfs) = Peak Outflow O (cfs) =	IN/A 0.0	N/A 0.0	2.0	5.	/ 0	8.6 0.1	0.2	19.5 0.2	0,2
Ratio Peak Outflow to Predevelopment $Q =$	N/A	N/A	N/A	0.	0	0.0	0.0	0.0	0.0
Structure Controlling Flow =	Plate	Plate	Plate	Pla	ite	Plate	Plate	Plate	N/A
Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) =	N/A N/A	N/A N/A	N/A N/A	N/	A A	N/A N/A	N/A N/A	N/A N/A	N/A N/A
Time to Drain 97% of Inflow Volume (hours) =	57	62	118	>1	20	>120	>120	>120	>120
Time to Drain 99% of Inflow Volume (hours) =	72	77	>120	>1	20	>120	>120	>120	>120
Maximum Ponding Depth (ft) =	0.05	0.06	0.27	0.	/b 51	1.24	2.14	2.68	3.00 0.77
Maximum Volume Stored (acre-ft) =	0.028	0.034	0.149	0.4	42	0.750	1.357	1.740	1.989

		DEI	ENTIO	N DAS. MHFD-L	Detention, Version	4.04 (Feb.	GE TAL ruary 2021,		ILDER		
Project: Basin ID:	Waterview I	North Pon	d 2 Spillway (Calcs							
(ZONE 3 ZONE 3	2										
100-178		T									
VOLUME EURY WOCY	\sim	1. Con 11					n				
	1 AND 2	ORIFI	CE		Depth Increment =		ft Optional				0
POOL ExampleZone	e Configurat	ion (Rete	ntion Pond)		Stage - Storage Description	Stage (ft)	Override Stage (ft)	Length (ft)	Width (ft)	Area (ft ²)	O' An
Watershed Information		-			Top of Micropool		0.00			-	2
Selected BMP Type =	EDB		Assumed			-	1.00	-	-		2
Watershed Area =	20.77	acres	imperviou	isness			2.00				3
Watershed Length = Watershed Length to Centroid =	1,800	π A	for Basin	1			3.00				3
Watershed Slope =	0.040	ft/ft	developm	ient							+
Watershed Imperviousness =	95.00%	percent							-		
Percentage Hydrologic Soil Group A =	0.0%	percent									_
Percentage Hydrologic Soil Groups C/D =	0.0%	percent				-			-	-	1
Target WQCV Drain Time =	40.0	hours									
Location for 1-hr Rainfall Depths =	User Input										_
After providing required inputs above in depths, dick 'Run CUHP' to generate run	cluding 1-hour off hydrograph	rainfall s using									-
the embedded Colorado Urban Hydro	ograph Procedu	ire.	Optional Use	r Overrides		-				-	
Water Quality Capture Volume (WQCV) =	0.774	acre-feet		acre-feet							_
Excess Urban Runoff Volume (EURV) = 2-vr Runoff Volume (P1 = 1.19 in) =	2.221	acre-feet	1 19	acre-feet							+
5-yr Runoff Volume (P1 = 1.5 in.) =	2.491	acre-feet	1.50	inches							1
10-yr Runoff Volume (P1 = 1.75 in.) =	2.946	acre-feet	1.75	inches					-		
25-yr Runoff Volume (P1 = 2 in.) =	3.409	acre-feet	2.00	inches							_
100-yr Runoff Volume (P1 = 2.25 in.) =	4.368	acre-feet	2.25	inches					-	-	-
500-yr Runoff Volume (P1 = 3.14 in.) =	5.507	acre-feet		inches							
Approximate 2-yr Detention Volume =	1.791	acre-feet									
Approximate 5-yr Detention Volume = Approximate 10-yr Detention Volume =	2.326	acre-feet							-	-	-
Approximate 25-yr Detention Volume =	3.037	acre-feet									+
Approximate 50-yr Detention Volume =	3.151	acre-feet									
Approximate 100-yr Detention Volume =	3.251	acre-feet									+
Define Zones and Basin Geometry									-	-	+
Select Zone 1 Storage Volume (Required) =		acre-feet									
Select Zone 2 Storage Volume (Optional) =	1 000	acre-feet									_
20ne 3 Volume (User Defined - 20nes 1 & 2) = Total Detention Basin Volume =	1.988	acre-feet							-	-	+
Initial Surcharge Volume (ISV) =	user	ft ³								-	
Initial Surcharge Depth (ISD) =	user	ft									
Total Available Detention Depth (H _{total}) =	user	ft ft									+
Slope of Trickle Channel (STC) =	user	ft/ft									1
Slopes of Main Basin Sides (S _{main}) =	user	H:V									
Basin Length-to-Width Ratio (R _{L/W}) =	user]									+
Initial Surcharge Area (A _{1SV}) =	user	ft ²							-	-	+
Surcharge Volume Length (L _{ISV}) =	user	ft									
Surcharge Volume Width (W _{ISV}) =	user	ft									_
Length of Basin Floor (H _{FLOOR}) =	user	π A									+
Width of Basin Floor (W _{FLOOR}) =	user	ft									+
Area of Basin Floor (A _{FLOOR}) =	user	ft²									
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³									_
Length of Main Basin (LMAIN) =	user	ft				-			-	-	1
Width of Main Basin (W _{MAIN}) =	user	ft									Г
Area of Main Basin (A _{MAIN}) =	user	ft ²									_
VOLUME OF Main Basin (VMAIN) = Calculated Total Basin Volume (VMAIN) =	user user	it acre-feet									\vdash
(- (dial)		-								-	F
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Optional Override Area Area (ft²) (acre) 24,667 0.566
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Volume (ft³)

Volume (ac-ft)

MHFD-Detention, Version 4.04 (February 2021)



DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.04 (February 2021) Project: Waterview North Pond 2 Spillway Calcs Basin ID: 2 Estimated Ectimated Stage (ft) Volume (ac-ft) Outlet Type O-YR EURV WOCV Zone #N/A Orifice Plate Zone 2 Weir&Pipe (Rect.) 100-YEAF ZONE 1 AND 2 ORIFICES 1 988 Weir (No Pipe) Zone 3 (User) 3 00 Example Zone Configuration (Retention Pond) Total (all zones) User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP) Calculated Parameters for Underdrain ft (distance below the filtration media surface) Underdrain Orifice Area Underdrain Orifice Invert Depth : N/A N/A ft² Underdrain Orifice Diameter = N/A inches Underdrain Orifice Centroid = N/A User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WOCV and/or EURV in a sedimentation BMP). Calculated Parameters for Plate Invert of Lowest Orifice : 0.00 ft (relative to basin bottom at Stage = 0 ft) WO Orifice Area per Row N/A ft² Depth at top of Zone using Orifice Plate = ft (relative to basin bottom at Stage = 0 ft) Elliptical Half-Width feet N/A Orifice Plate: Orifice Vertical Spacing = Elliptical Slot Centroid = feet inches N/A ft² Orifice Plate: Orifice Area per Row = sa. inches Elliptical Slot Area N/Δ User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest Row 1 (required) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 5 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional) Stage of Orifice Centroid (ft) Orifice Area (sg. inches) Row 9 (optional) Row 10 (optional) Row 11 (optional) Row 12 (optional) Row 13 (optional) Row 14 (optional) Row 15 (optional) Row 16 (optional) Stage of Orifice Centroid (ft) Orifice Area (sq. inches) User Input: Vertical Orifice (Circular or Rectangular) Calculated Parameters for Vertical Orific Not Selected Not Selected Not Selected Not Selected Invert of Vertical Orifice ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area N/A N/A N/A N/A Depth at top of Zone using Vertical Orifice = ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid = N/A N/A N/A N/A Vertical Orifice Diameter N/A N/A inches User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe) Calculated Parameters for Overflow Wei Zone 3 Weir Zone 2 Weir Zone 2 Weir Zone 3 Weir Overflow Weir Front Edge Height, Ho Height of Grate Upper Edge, Ht 0.00 t (relative to basin bottom at Stage = 0 ft) N/A Weir Front Edge Length OR Weir Bottom Length feet Overflow Weir Slope Length : N/A Grate Open Area / 100-yr Orifice Area Weir Grate Slope OR Weir Side Slopes H:V N/A Horiz. Length of Weir Sides = N/A feet Overflow Grate Open Area w/o Debris : N/A Overflow Grate Open Area w/ Debris = Overflow Grate Type N/A N/A Debris Clogging % = N/A % User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plat Zone 2 Rectangular Not Selected Zone 2 Rectangula Not Selected Depth to Invert of Outlet Pipe N/A Outlet Orifice Area ft (distance below basin bottom at Stage = 0 ft) N/A Rectangular Orifice Width = Outlet Orifice Centroid inches N/A N/A Rectangular Orifice Height = inches Half-Central Angle of Restrictor Plate on Pipe N/A N/A User Input: Emergency Spillway (Rectangular or Trapez lated Parameters for Spillway oidal) ft (relative to basin bottom at Stage = 0 ft) Spillway Invert Stage 2.60 Spillway Design Flow Depth= 0.83 feet Spillway Crest Length = 30.00 feet Stage at Top of Freeboard = 4.43 feet Spillway End Slopes = 4.00 H:V Basin Area at Top of Freeboard 0.77 acres Freeboard above Max Water Surface Basin Volume at Top of Freeboard = 1.99 1.00 feet acre-ft es in the Inflow Hydrogra Routed Hydrograph Results hs table (Columns W through AF) The user can override the default CUHP araphs and runoff volumes by a new valı Design Storm Return Period WQCV EURV 2 Yea 10 Yea 25 Yea 50 Year 100 Yea 5 Year One-Hour Rainfall Depth (in) N/A 0.774 N/A 1.19 1.50 2.491 1.75 2.946 2.00 2.25 3.867 2.52 CLIHP Runoff Volume (acre-ft) 2.221 1.930 Inflow Hydrograph Volume (acre-ft) N/A N/A 1.930 2.491 2.946 3.409 3.867 4.368 CUHP Predevelopment Peak Q (cfs) N/A N/A 8.6 15.5 19.5 24.9 2.0 5.7 OPTIONAL Override Predevelopment Peak Q (cfs) N/A N/A 0.27 0.75 0.10 0.42 0.94 1.20 Predevelopment Unit Peak Flow, g (cfs/acre) N/A N/A Peak Inflow Q (cfs) N/A N/A 33.7 42.2 48.3 57.2 64.8 75.0 Peak Outflow Q (cfs) 3.9 14.8 23.7 23.7 23.7 9.2 Ratio Peak Outflow to Predevelopment Q N/A N/A 10 Structure Controlling Flow Spillway Spillway Spillway Spillway N/A N/A N/A Max Velocity through Grate 1 (fps) N/A N/A N/A N/A N/A N/A N/A N/A N/A Max Velocity through Grate 2 (fps) N/A N/A N/A N/A N/A Time to Drain 97% of Inflow Volume (hours) >120 >120 >120 >120 >120 >120 Time to Drain 99% of Inflow Volume (hours) >120 >120 >120 >120 >120 >120 >120 2.72 2.82 2.89 Maximum Ponding Depth (ft) : 2.99 3.00 3.00 3.00

0.75

0.75

1.84

0.76

1.905

0.77

1.989

0.77

1.989

0.76

1.974

Area at Maximum Ponding Depth (acres) = Maximum Volume Stored (acre-ft) =

0.77

DETENTION BASIN STAGE-STORAGE TABLE BUILDER MHFD-Detention, Version 4.06 (July 2022)

	Project: Ter	mporary S	ediment B	asin 6		,	•								
	Basin ID: <u>6 a</u>	and 7													
	(ZONE 3 (ZONE 2 (ZONE 2)		_												
	100-YR		T												
	VOLUME EURY WOOV	4	<u>k</u>					•							
	ZONE 1 ANI	10 2	ORIFICI	UR E		Depth Increment =		ft	1	1	1	Ontional			
	PERMANENT ORIFICES POOL ExampleZone Co	onfigurati	on (Reten	tion Pond)		Stage - Storage	Stage	Override	Length	Width	Area	Override	Area	Volume	Volume
		-				Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft ²)	(acre)	(ft ³)	(ac-ft)
	Watershed Information					Top of Micropool		0.00				61,013	1.401		
	Selected BMP Type =	EDB						1.00				65,222	1.497	63,117	1.449
	Watershed Area =	48.85	acres					2.00			-	69,563	1.597	130,510	2.996
	Watershed Length to Centroid -	2,300	n. A					4.00		-	-	79,621	1.099	202,305	6 306
	Watershed Length to Centrold =	0.020	ft/ft					5.00				83,340	1.913	359.610	8.256
	Watershed Imperviousness =	2.00%	percent					6.00				88,189	2.025	445,375	10.224
	Percentage Hydrologic Soil Group A =	35.0%	percent					7.00		-	-	93,164	2.139	536,051	12.306
	Percentage Hydrologic Soil Group B =	65.0%	percent					8.00			-	98,266	2.256	631,766	14.503
	Percentage Hydrologic Soil Groups C/D =	0.0%	percent										<u> </u>		
	location for 1-br Painfall Denths - Lise	72.0 ar Input	nours	Drain Time	Too Long						-		<u> </u>		
	After any idles as when is the standard in the		- in fail								-				
DRAIN TIME MATCHES	depths, dick 'Run Comp' to generate runoff h	hydrographs	annan Susing												
MHFCD TEMP SEDIMENT	the embedded Colorado Urban Hydrogra	ph Procedur	re.	Optional Use	r Overrides										
BASIN REQUIREMENTS	Water Quality Capture Volume (WQCV) =	0.062	acre-feet		acre-feet										
	Excess Urban Runoff Volume (EURV) =	0.068	acre-feet		acre-feet								<u> </u>		
	2-yr Runoff Volume (P1 = 1.19 in.) =	0.059	acre-feet	1.19	inches					-	-		<u> </u>		
MHECD	10-vr Runoff Volume (P1 = 1.75 in.) =	1.049	acre-feet	1.75	inches						-				
REQUIREMENTS OF	25-yr Runoff Volume (P1 = 2 in.) =	2.422	acre-feet	2.00	inches										
3,600 CF PER -	50-yr Runoff Volume (P1 = 2.25 in.) =	3.311	acre-feet	2.25	inches										
DRAINAGE AREA	100 yr Runoff Volume (P1 = 2.52 in.) =	4.741	acre-feet	2.52	inches					-			\vdash		
(48.85*3,600 = 175,860	500-yr Runoff Volume (P1 = 3.14 in.) =	7.085	acre-feet		inches					-			└───		
CF = 4.037 ACRE-FEET)	Approximate 2-yr Detention Volume =	0.064	acre-feet										┝───	\vdash	
	Approximate 5 or Detenuon volume =	0.310	acre-feet				-			-			<u> </u>	┝───┦	
	Approximate 25-yr Detention Volume =	0.479	acre-feet												
	Approximate 50-yr Detention Volume =	0.500	acre-feet												
	Approximate 100-yr Detention Volume =	0.779	acre-feet							-	-				
	Define Zones and Basin Geometry	4 027	acro fact										<u> </u>		
	Select Zone 2 Storage Volume (Ontional) =	4.037	acre-feet							-	_				
	Select Zone 3 Storage Volume (Optional) =		acre-feet												
	Total Detention Basin Volume =	4.037	acre-feet												
	Initial Surcharge Volume (ISV) =	user	ft ³							-	-				
	Initial Surcharge Depth (ISD) =	user	ft										L		
	Total Available Detention Depth (H _{total}) =	user	ft e										<u> </u>		
	Shope of Trickle Channel $(R_{TC}) =$	user	n. A/A							-	_				
	Slopes of Main Basin Sides (Smain) =	user	H:V			-									
	Basin Length-to-Width Ratio (R _{L/W}) =	user									-				
	_						-			-	-				
	Initial Surcharge Area (A _{ISV}) =	user	ft²							-			L		
	Surcharge Volume Length (LISV) =	user	π n				-			-			<u> </u>		
	Depth of Basin Floor (HFLOOR) =	user	ft				-			-	-				
	Length of Basin Floor (L _{FLOOR}) =	user	ft												
	Width of Basin Floor (W _{FLOOR}) =	user	ft							-	-				
	Area of Basin Floor (A _{FLOOR}) =	user	ft²												
	Volume of Basin Floor (V _{FLOOR}) =	user	ft' A										<u> </u>		
	Length of Main Basin (IMAIN) =	user	ft.							-	-				
	Width of Main Basin (WMAIN) =	user	ft												
	Area of Main Basin (A _{MAIN}) =	user	ft ²												
	Volume of Main Basin (V _{MAIN}) =	user	ft ³										\vdash		
	Calculated Total Basin Volume (V _{total}) =	user	acre-feet										┝───	───	
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MHFD-Detention, Version 4.06 (July 2022)



DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.06 (July 2022)

Project:	Temporary Sedime	nt Basin 6			.00 (July 2)	022)			
Basin ID:	6 and 7								
ZONE 3 ZONE 2 ZONE 1				Esti	mated	Estimated			
100-YR				Sta	ge (ft)	Volume (ac-ft)	Outlet Type		
VOLUME_EURV Wacv			Zone 1 (User)	2	2.64	4.037	Orifice Plate		
T ZONE 1 AND 2	100-YEAR ORIFICE		Zone 2						
PERMANENT ORIFICES	0 fi (D - t-		Zone 3						
Example zone	Configuration (Rete	ention Pond)		Total	(all zones)	4.037			
User Input: Orifice at Underdrain Outlet (typically i	used to drain WQCV	in a Filtration BMP)		<i>c</i> ,				Calculated Paramet	ers for Underdrain
Underdrain Orifice Invert Depth =	N/A	ft (distance below t	the filtration media s	urface)		Under	drain Orifice Area =	N/A	ft ^e
	N/A	inches				Underdia		N/A	ieet
User Input: Orifice Plate with one or more orifices	or Elliptical Slot We	eir (typically used to	drain WOCV and/or	EURV in	a sediment	tation BMP)		Calculated Paramet	ers for Plate
Centroid of Lowest Orifice =	0.00	ft (relative to basin	bottom at Stage = 0) ft)		WQ Orif	fice Area per Row =	2.604E-02	ft ²
Depth at top of Zone using Orifice Plate =	2.64	ft (relative to basin	bottom at Stage = 0) ft)		El	iptical Half-Width =	N/A	feet
Orifice Plate: Orifice Vertical Spacing =	10.60	inches				Ellip	tical Slot Centroid =	N/A	feet
Orifice Plate: Orifice Area per Row =	3.75	sq. inches (use rect	tangular openings)			1	=lliptical Slot Area =	N/A	ft
User Input: Stage and Total Area of Each Orifice I	Row (numbered fror	n lowest to hiahest)							
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4	(optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)
Stage of Orifice Centroid (ft)	0.00	0.88	1.76						
Orifice Area (sq. inches)	3.75	3.75	3.75						
	Dow O (and a	Dow 10 (coli)	Dow 11 (coling)	D 4*	(anti 1)	Pour 12 (Dow 14 (coli 1	Dow 15 (and a	Dow 16 (and the
Stago of Orifico Controid (ft)	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	ROW 12	(optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)
Orifice Area (sg. inches)									
User Input: Vertical Orifice (Circular or Rectangula	ar)		•					Calculated Paramet	ers for Vertical Orific
	Not Selected	Not Selected						Not Selected	Not Selected
Invert of Vertical Orifice =			ft (relative to basin	bottom a	at Stage = (Dft) Ve	rtical Orifice Area =		
Depth at top of Zone using Vertical Onnice =			It (relative to basin	bottom a	it Stage = (UTC) Vertica	al Orifice Centrold =		
		1	inches						
User Input: Overflow Weir (Dropbox with Flat or S	Sloped Grate and Ou	Itlet Pipe OR Rectan	gular/Trapezoidal W	eir and N	lo Outlet Pi	pe)		Calculated Paramet	ers for Overflow We
	Not Selected	Not Selected						Not Selected	Not Selected
Overflow Weir Front Edge Height, Ho =			ft (relative to basin be	ottom at S	Stage = 0 ft)	Height of Grat	te Upper Edge, $H_t =$		
Overflow Weir Grate Slope =			H·V		C	Grate Open Area / 1	00-vr Orifice Area =		
Horiz, Length of Weir Sides =			feet		(Overflow Grate Oper	Area w/o Debris =		
Overflow Grate Type =						Overflow Grate Ope	en Area w/ Debris =		
Debris Clogging % =			%						
User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Rest	trictor Plate, or Rect	angular Orifice)			<u>C</u>	alculated Parameters	s for Outlet Pipe w/	Flow Restriction Plat
Depth to Invert of Outlet Pipe =	NOL Selected	NOL Selected	ft (distance below ba	sin hotton	n at Stage =	0 ft))utlet Orifice Area =	Not Selected	Not Selected
Circular Orifice Diameter =			inches		n at Stage –	Outle	t Orifice Centroid =		
					Half-Cer	ntral Angle of Restri	ctor Plate on Pipe =	N/A	N/A
User Input: Emergency Spillway (Rectangular or T	rapezoidal)	la						Calculated Paramet	ers for Spillway
Spillway Invert Stage=		ft (relative to basin	bottom at Stage = 0) ft)		Spillway [Design Flow Depth=		feet
Spillway Crest Length =		feet				Stage at Basin Area at	Top of Freeboard =		reet
Freeboard above Max Water Surface =		feet				Basin Volume at	Top of Freeboard =		acre-ft
Bouted Hydrograph Besults	The user can over	ide the default (199	budrographs and -	unoff vel	umos bu ca	toring new values in	the Inflow Hydrocs	anhs tahla (Column	M through AE
<u>Rouleu Ayurograpii Results</u> Design Storm Return Period =	WOCV	FLIRV	2 Year	5	Year	10 Year	25 Year	50 Year	100 Year
One-Hour Rainfall Depth (in) =	N/A	N/A	1.19	1	.50	1.75	2.00	2.25	2.52
CUHP Runoff Volume (acre-ft) =	0.062	0.068	0.059	0.	.535	1.049	2.422	3.311	4.741
Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak O (cfs) =	N/A N/A	N/A N/A	0.059	0.	.535 6.9	1.049	2.422	3.311	4./41
OPTIONAL Override Predevelopment Peak Q (cfs) =	N/A	N/A							
Predevelopment Unit Peak Flow, q (cfs/acre) =	N/A	N/A	0.01	0	0.14	0.27	0.59	0.78	1.04
Peak Inflow Q (cfs) = Peak Outflow O (cfs) =	0.0	0.0	0.7		0.9	0.1	<u>26.8</u> 0.3	0.4	0.5
Ratio Peak Outflow to Predevelopment $Q =$	N/A	N/A	N/A	1	0.0	0.0	0.0	0.0	0.0
Structure Controlling Flow =	Plate	Plate	Plate	Ρ,	late	Plate	Plate	Plate	Plate
Max Velocity through Grate 2 (fps) =	N/A	N/A	N/A	1	N/A	N/A	N/A	N/A	N/A N/A
Time to Drain 97% of Inflow Volume (hours) =	57	59	57	>	120	>120	>120	>120	>120
Time to Drain 99% of Inflow Volume (hours) =	72	74	72	>	120	>120	>120	>120	>120
maximum Ponding Depth (ת) = Area at Maximum Ponding Depth (acres) =	1.41	1.41	1.40	1		1.47	1.56	1.61	1.70
Maximum Volume Stored (acre-ft) =	0.070	0.070	0.042	0.	.511	1.019	2.365	3.237	4.644

Maximum Ponding Depth (ft) = Area at Maximum Ponding Depth (acres) = Maximum Volume Stored (acre-ft) =

MHFD-Detention, Version 4.04 (February 2021)

Project:	Waterview I	North Pon	d 3 (Temp. Se	diment Ba	sin 6)
Basin ID:	6 and 7				
	2 ONE 1	-	~		
VOLUME EURY WOCV		1		~	
		100-11	AR	-	Darth In
PERMANENT ORIF	1 AND 2	ORIFI	CE		Depth In
POOL ExampleZone	Configurat	ion (Rete	ntion Pond)		Stage -
Watershed Information					Top of M
Selected BMP Type =	EDB	1			100 01 11
Watershed Area -	49.95	acros	Assumed		
Watershed Length =	2 300	ft ft	imperviou	sness	
Watershed Length to Centroid =	1.150	ft	for Basin	1	
Watershed Slope =	0.020	ft/ft	developm	ent	
Watershed Imperviousness =	70.00%	percent			
Percentage Hydrologic Soil Group A =	35.0%	percent			
Percentage Hydrologic Soil Group B =	65.0%	percent			
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			
Target WQCV Drain Time =	40.0	hours			
Location for 1-hr Rainiaii Depuis =	user input				
After providing required inputs above inc depths, dick 'Run CUHP' to generate run	luding 1-hour	raintall s using			
the embedded Colorado Urban Hydro	graph Procedu	re.	Optional Use	r Overrides	
Water Quality Capture Volume (WQCV) =	1.120	acre-feet		acre-feet	
Excess Urban Runoff Volume (EURV) =	3.957	acre-feet		acre-feet	
2-yr Runoff Volume (P1 = 1.19 in.) =	3.315	acre-feet	1.19	inches	
5-yr Runoff Volume (P1 = 1.5 in.) =	4.424	acre-feet	1.50	inches	
10-yr Runoff Volume (P1 = 1.75 in.) =	5.378	acre-feet	1.75	inches	
25-yr Runoff Volume (P1 = 2 in.) =	6.568	acre-feet	2.00	inches	
50-yr Runoff Volume (P1 = 2.25 in.) =	7.606	acre-feet	2.25	inches	
100-yr Runoff Volume (P1 = 2.52 in.) =	0.001	acre-leet	2.52	inches	
Approximate 2-vr Detention Volume =	2.897	acre-feet		inches	
Approximate 5-vr Detention Volume =	3.833	acre-feet			
Approximate 10-yr Detention Volume =	4.759	acre-feet			
Approximate 25-yr Detention Volume =	5.305	acre-feet			
Approximate 50-yr Detention Volume =	5.627	acre-feet			
Approximate 100-yr Detention Volume =	6.064	acre-feet			
Defension and Desire Comments					
Zone 1 Volume (WOCV) -	1 1 2 0	acro-foot			
Zone 2 Volume (FURV - Zone 1) =	2.838	acre-feet			
Zone 3 Volume (100-year - Zones 1 & 2) =	2.107	acre-feet			
Total Detention Basin Volume =	6.064	acre-feet			
Initial Surcharge Volume (ISV) =	user	ft ³			
Initial Surcharge Depth (ISD) =	user	ft			
Total Available Detention Depth (H _{total}) =	user	ft			
Depth of Trickle Channel (H_{TC}) =	user	ft o. /o			
Slope of Trickle Channel (S _{TC}) =	user	ft/ft			
Basin Length-to-Width Patio (P) =	user	n.v			
basin bengunto-widen Kato (KE/W) =	user	J			
Initial Surcharge Area (A _{ISV}) =	user	ft ²			
Surcharge Volume Length $(L_{ISV}) =$	user	ft			
Surcharge Volume Width (W_{ISV}) =	user	ft			
Depth of Basin Floor (H _{FLOOR}) =	user	ft			
Length of Basin Floor (L _{FLOOR}) =	user	ft			
Width of Basin Floor (W _{FLOOR}) =	user	ft			
Area of Basin Floor (A _{FLOOR}) =	user	π- α3			
Denth of Main Basin (Humu) =	user	n e			
Length of Main Basin (LMAIN) =	user	ft			
Width of Main Basin (WMAIN) =	user	ft			
Area of Main Basin (A _{MAIN}) =	user	ft ²			
Volume of Main Basin (V _{MAIN}) =	user	ft ³			
Calculated Total Basin Volume (V_{total}) =	user	acre-feet			

	Depth Increment =		ft							
	Charles Charles	0	Optional	Laurable	AND JUL	A 1000	Optional	A	Volumo	Malana
	Stage - Storage Description	Stage (ft)	Overnde Stage (ft)	Length (ft)	(作)	(ft ²)	Area (ft ²)	(acre)	(ft 3)	(ac-ft)
	Top of Micropool		0.00				61,013	1.401	(10)	(de it)
			1.00				65 222	1 497	78 370	1 799
			2.00				60 562	1 507	161 492	2 707
s		-	2.00		-	-	74.029	1.557	240 462	5.707
		-	4.00		_	_	78,621	1.055	342 445	7.861
			4.00 5.00		-	-	93 340	1.003	440 556	10 114
			5.00		-	-	03,340	2.025	F42 022	10.114
			7.00				03 164	2.025	602 647	12,407
		-	8.00		_	_	08 266	2.155	666.937	15 308
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MHFD-Detention, Version 4.04 (February 2021)



	L		DAJIN OUI	LLIJIKO	JIOKE DES		DETENTION BASIN OUTLET STRUCTURE DESIGN					
MHFD-Detention, Version 4.04 (February 2021)												
Project: Waterview North Pond 3 (Temp. Sediment Basin 6)												
ZONE 3	o and 7			Ectimated	Ectimated							
				Stage (ft)	Volume (ac-ft)	Outlet Type						
VOLUME EURV WOCV			Zone 1 (WOCV)	0.63	1 120	Orifice Plate	1					
± ±			Zone 1 (WQCV)	0.03	2 020	Orifice Plate						
ZONE 1 AND 2	ORIFICE		ZUIIE Z (EURV)	2.13	2.030							
POOL Example Zone	Configuration (Ret	ention Pond)	Zone 3 (100-year)	3.1/	2.107	Weir (No Pipe)						
	used to dusin WOCU	in a Filtration DMD		lotal (all zones)	6.064	l	Calculated Davament	ana fan Lindaudusin				
Underdrain Orifice Invert Denth -		ft (distance below t	he filtration media s	urface)	Under	drain Orifice Area –		ers for Underdrain				
Underdrain Orifice Diameter =	N/A	inches		undee)	Underdrai	n Orifice Centroid =	N/A	feet				
	,,,	inditeb			ondorardi							
User Input: Orifice Plate with one or more orifice	or Elliptical Slot We	eir (typically used to	drain WOCV and/or	EURV in a sediment	tation BMP)		Calculated Paramete	ers for Plate				
Invert of Lowest Orifice =	0.00	ft (relative to basin	bottom at Stage = 0) ft)	WQ Orif	fice Area per Row =	N/A	ft ²				
Depth at top of Zone using Orifice Plate =	2.13	ft (relative to basin	bottom at Stage = 0) ft)	El	iptical Half-Width =	N/A	feet				
Orifice Plate: Orifice Vertical Spacing =	8.50	inches			Ellip	tical Slot Centroid =	N/A	feet				
Orifice Plate: Orifice Area per Row =		sq. inches			E	Elliptical Slot Area =	N/A	ft ²				
User Input: Stage and Total Area of Each Orifice	Row (numbered from	n lowest to highest)		-								
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)				
Stage of Orifice Centroid (ft)	0.00	0.71	1.42									
Orifice Area (sq. inches)	0.00	0.00	0.00									
	Row 0 (optional)	Pow 10 (optional)	Pow 11 (ontional)	Pow 12 (optional)	Pow 12 (optional)	Pow 14 (optional)	Row 15 (optional)	Row 16 (optional)				
Stage of Orifice Controid (ff)	ROW 9 (Optional)	ROW 10 (Optional)	Row II (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	ROW 15 (Optional)	ROW 16 (Optional)				
Orifice Area (sq. inches)												
Office Area (34. inclies)												
User Input: Vertical Orifice (Circular or Rectangul	ar)						Calculated Paramete	ers for Vertical Orific				
	Not Selected	Not Selected	1				Not Selected	Not Selected				
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	0 ft) Ve	rtical Orifice Area =	N/A	N/A				
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	0 ft) Vertica	al Orifice Centroid =	N/A	N/A				
Vertical Orifice Diameter =	N/A	N/A	inches									
			-									
User Input: Overflow Weir (Dropbox with Flat or	Sloped Grate and Ou	utlet Pipe OR Rectan	gular/Trapezoidal W	eir (and No Outlet F	Pipe)		Calculated Parameter	ers for Overflow Wei				
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected				
Overflow Weir Front Edge Height, Ho =	2.13	N/A	ft (relative to basin be	ottom at Stage = 0 ft) Height of Grat	te Upper Edge, $H_t =$	N/A	N/A				
Overflow Weir Front Edge Height, Ho = Overflow Weir Bottom Length =	2.13	N/A N/A	ft (relative to basin be feet	ottom at Stage = 0 ft) Height of Grat Overflow V	te Upper Edge, $H_t =$ Veir Slope Length =	N/A N/A	N/A N/A				
Overflow Weir Front Edge Height, Ho = Overflow Weir Bottom Length = Overflow Weir Side Slopes =	2.13	N/A N/A N/A	ft (relative to basin be feet H:V	ottom at Stage = 0 ft) Height of Grat Overflow V Grate Open Area / 1	te Upper Edge, $H_t =$ Veir Slope Length = 00-yr Orifice Area =	N/A N/A N/A	N/A N/A N/A				
Overflow Weir Front Edge Height, Ho = Overflow Weir Bottom Length = Overflow Weir Side Slopes = Horiz. Length of Weir Sides =	2.13	N/A N/A N/A N/A	ft (relative to basin be feet H:V feet	ottom at Stage = 0 ft (() Height of Grai Overflow V Grate Open Area / 1 Overflow Grate Oper	te Upper Edge, $H_t =$ Veir Slope Length = 00-yr Orifice Area = n Area w/o Debris =	N/A N/A N/A N/A	N/A N/A N/A N/A				
Overflow Weir Front Edge Height, Ho = Overflow Weir Bottom Length = Overflow Weir Side Slopes = Horiz. Length of Weir Sides = Overflow Grate Type =	2.13	N/A N/A N/A N/A N/A	ft (relative to basin be feet H:V feet	bttom at Stage = 0 ft	Height of Grat Overflow V Grate Open Area / 1 Overflow Grate Oper Overflow Grate Oper	te Upper Edge, H _t = Veir Slope Length = 00-yr Orifice Area = 0 Area w/o Debris = en Area w/ Debris =	N/A N/A N/A N/A N/A	N/A N/A N/A N/A N/A				
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Worksheet for Outfall 6" PVC Riser Pipe for Southeast temporary sediment basin

Project Description		
Friction Method	Manning	
Cables Fam	Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.010	
Channel Slope	0.020 ft/ft	
Normal Depth	5.8 in	
Diameter	6.0 in	
Results		
Discharge	1.11 cfs	
How Area	0.2 ft ²	
Wetted Perimeter	1.4 ft	
Hydraulic Radius	1.7 in	
Top Width	0.20 ft	
Critical Depth	5.8 in	
Percent Full	95.8 %	
Critical Slope	0.020 ft/ft	
Velocity	5.71 ft/s	
Velocity Head	0.51 ft	
Specific Energy	0.99 ft	
Froude Number	1.023	
Maximum Discharge	1.11 cfs	
Discharge Full	1.03 cfs	
Slope Full	0.023 ft/ft	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Unstream Denth	0.0 in	
Profile Description	N/A	
Profile Headloss	0 00 ft	
Average End Denth Over Pice	0.00 10	
Normal Depth Over Rise	96.7 %	
Downstream Velocity	Infinity ft/s	
Unstream Velocity	Infinity ft/c	
Normal Depth	EQ in	
Critical Depth	5.0 iii	
Channel Slope	0.020 ft/ft	
Critical Slope	0.020 ft/ft	
citucal slope	0.020 10/1	

Temporary Drainage Swales.fm8 7/20/2022 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Rip-Rap Calculation TEMPORARY SEDIMENT BASIN 6

Applicable Equations:

$L_p = (1/2tan\Theta)(A_t/Y_t-D)$	Equation 9-11 per USCDM
$A_t = Q/V$	Equation 9-12 per USDCM
$\Theta = \tan^{-1}(1/(2*ExpansionFactor))$	Equation 9-13 per USDCM
$W = 2(L_p tan \Theta) + D$	Equation 9-14 per USDCM
$T = 2D_{50}$	Equation 9-15 per USDCM

Assumptions

Maximum Major Event Velocity is 5fps for FES outletting into grass channel

Input parameters:		
Description	Variable	Input Unit
Width of the conduit (use diameter for circular conduits),	D:	0.50 ft
HGL Elevation		0.48 ft
Invert Elevation		0.00 ft
Tailwater depth (ft),	Y _t :	0.48 ft
Expansion angle of the culvert flow	Θ:	0.12 radians
Design discharge (cfs)*	Q:	1.11 cfs
Froude Number	F _r	1.43 Supercritical
Unitless Variables for Tables:		
	For Figure 9-35 Q/D ^{2.5}	6.28
	For Figure 9-35 Yt/D	0.97
	For Figure 9-38 Q/D ^{1.5}	3.14
	For Figure 9-38 Yt/D	0.97
Allowable non-eroding velocity in the downstream channel	el (ft/sec) V:	5 ft/sec
Expansion Factor (Figure 9-35), 1/(2tan(θ))		4.2

Solve for:

Description	Variable	Output Unit
1. Required area of flow at allowable velocity (ft ²)	A _t :	0.22 ft ²
2. Length of Protection	L _p :	-0.17 ft
	$L_p < 3D?$	Yes
	L _{pmin} :	1.50 ft
3. Width of downstream riprap protection	W:	1.00 ft
4. Rip Rap Type (Figure 9-38)	-	VL
5. Rip Rap Size (Figure 8-34)	D ₅₀ :	6 inches
Rip Rap Summary		
Length	Lp	2.00 ft
Width	W	1.00 ft
Size	D ₅₀	6 inches
Туре	-	VL -
Thickness	Т	12 inches

APPENDIX E – TEMPORARY SWALE SIZING

Kimley **»Horn**

Description

Earth dikes and drainage swales are temporary storm conveyance channels constructed either to divert runoff around slopes or to convey runoff to additional sediment control BMPs prior to discharge of runoff from a site. Drainage swales may be lined or unlined, but if an unlined swale is used, it must be well compacted and capable of resisting erosive velocities.

Appropriate Uses

Earth dikes and drainage swales are typically used to control the flow path of runoff at a construction site by diverting runoff around areas prone to erosion, such as steep slopes. Earth dikes and drainage swales may also be constructed as temporary conveyance features. This will direct runoff to additional sediment control treatment BMPs, such as sediment traps or basins.



Photograph ED/DS-1. Example of an earth dike used to divert flows at a construction site. Photo courtesy of CDOT.

Design and Installation

When earth dikes are used to divert water for slope protection, the earth dike typically consists of a horizontal ridge of soil placed perpendicular to the slope and angled slightly to provide drainage along the contour. The dike is used in conjunction with a swale or a small channel upslope of the berm to convey the diverted water. Temporary diversion dikes can be constructed by excavation of a V-shaped trench or ditch and placement of the fill on the downslope side of the cut. There are two types of placement for temporary slope diversion dikes:

- A dike located at the top of a slope to divert upland runoff away from the disturbed area and convey it in a temporary or permanent channel.
- A diversion dike located at the base or mid-slope of a disturbed area to intercept runoff and reduce the effective slope length.

Depending on the project, either an earth dike or drainage swale may be more appropriate. If there is a

need for cut on the project, then an excavated drainage swale may be better suited. When the project is primarily fill, then a conveyance constructed using a berm may be the better option.

All dikes or swales receiving runoff from a disturbed area should direct stormwater to a sediment control BMP such as a sediment trap or basin.

Earth Dikes and Drainage Swales		
Functions		
Erosion Control Yes		
Sediment Control Moderate		
Site/Material Management No		

EC-10 Earth Dikes and Drainage Swales (ED/DS)

Unlined dikes or swales should only be used for intercepting sheet flow runoff and are not intended for diversion of concentrated flows.

Details with notes are provided for several design variations, including:

- ED-1. Unlined Earth Dike formed by Berm
- DS-1. Unlined Excavated Swale
- DS-2. Unlined Swale Formed by Cut and Fill
- DS-3. ECB-lined Swale
- DS-4. Synthetic-lined Swale
- DS-5. Riprap-lined Swale

The details also include guidance on permissible velocities for cohesive channels if unlined approaches will be used.

Maintenance and Removal

Inspect earth dikes for stability, compaction, and signs of erosion and repair. Inspect side slopes for erosion and damage to erosion control fabric. Stabilize slopes and repair fabric as necessary. If there is reoccurring extensive damage, consider installing rock check dams or lining the channel with riprap.

If drainage swales are not permanent, remove dikes and fill channels when the upstream area is stabilized. Stabilize the fill or disturbed area immediately following removal by revegetation or other permanent stabilization method approved by the local jurisdiction.

15" MIN

<u>_</u>23



ED-1. COMPACTED UNLINED EARTH DIKE FORMED BY BERM





DS-2. COMPACTED UNLINED SWALE FORMED BY CUT AND FILL



DS-3. ECB LINED SWALE (CUT AND FILL OR BERM)



EARTH DIKE AND DRAINAGE SWALE INSTALLATION NOTES

- 1. SEE SITE PLAN FOR:
 - LOCATION OF DIVERSION SWALE
 - TYPE OF SWALE (UNLINED, COMPACTED AND/OR LINED).
 - LENGTH OF EACH SWALE.
 - DEPTH, D, AND WIDTH, W DIMENSIONS.
 - FOR ECB/TRM LINED DITCH, SEE ECB DETAIL.
 - FOR RIPRAP LINED DITCH, SIZE OF RIPRAP, D50.

2. SEE DRAINAGE PLANS FOR DETAILS OF PERMANENT CONVEYANCE FACILITIES AND/OR DIVERSION SWALES EXCEEDING 2-YEAR FLOW RATE OR 10 CFS.

3. EARTH DIKES AND SWALES INDICATED ON SWMP PLAN SHALL BE INSTALLED PRIOR TO LAND-DISTURBING ACTIVITIES IN PROXIMITY.

4. EMBANKMENT IS TO BE COMPACTED TO 90% OF MAXIMUM DENSITY AND WITHIN 2% OF OPTIMUM MOISTURE CONTENT ACCORDING TO ASTM D698.

5. SWALES ARE TO DRAIN TO A SEDIMENT CONTROL BMP.

6. FOR LINED DITCHES, INSTALLATION OF ECB/TRM SHALL CONFORM TO THE REQUIREMENTS OF THE ECB DETAIL.

7. WHEN CONSTRUCTION TRAFFIC MUST CROSS A DIVERSION SWALE, INSTALL A TEMPORARY CULVERT WITH A MINIMUM DIAMETER OF 12 INCHES.

EARTH DIKE AND DRAINAGE SWALE MAINTENANCE NOTES

1. INSPECT BMPs EACH WORKDAY, AND MAINTAIN THEM IN EFFECTIVE OPERATING CONDITION. MAINTENANCE OF BMPs SHOULD BE PROACTIVE, NOT REACTIVE. INSPECT BMPs AS SOON AS POSSIBLE (AND ALWAYS WITHIN 24 HOURS) FOLLOWING A STORM THAT CAUSES SURFACE EROSION, AND PERFORM NECESSARY MAINTENANCE.

2. FREQUENT OBSERVATIONS AND MAINTENANCE ARE NECESSARY TO MAINTAIN BMPs IN EFFECTIVE OPERATING CONDITION. INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE DOCUMENTED THOROUGHLY.

3. WHERE BMPs HAVE FAILED, REPAIR OR REPLACEMENT SHOULD BE INITIATED UPON DISCOVERY OF THE FAILURE.

4. SWALES SHALL REMAIN IN PLACE UNTIL THE END OF CONSTRUCTION; IF APPROVED BY LOCAL JURISDICTION, SWALES MAY BE LEFT IN PLACE.

5. WHEN A SWALE IS REMOVED, THE DISTURBED AREA SHALL BE COVERED WITH TOPSOIL, SEEDED AND MULCHED OR OTHERWISE STABILIZED IN A MANNER APPROVED BY LOCAL JURISDICTION.

(DETAIL ADAPTED FROM DOUGLAS COUNTY, COLORADO AND THE CITY OF COLORADO SPRINGS, COLORADO, NOT AVAILABLE IN AUTOCAD)

NOTE: MANY JURISDICTIONS HAVE BMP DETAILS THAT VARY FROM UDFCD STANDARD DETAILS. CONSULT WITH LOCAL JURISDICTIONS AS TO WHICH DETAIL SHOULD BE USED WHEN DIFFERENCES ARE NOTED.

Project Description		
Friction Method	Manning Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.020 ft/ft	
Normal Depth	28.0 in	
Left Side Slope	3.000 H:V	
Right Side Slope	3.000 H:V	
Results		
Discharge	122.42 cfs	
Flow Area	16.3 ft ²	
Wetted Perimeter	14.8 ft	
Hydraulic Radius	13.3 in	
Top Width	14.00 ft	
Critical Depth	30.4 in	
Critical Slope	0.013 ft/ft	
Velocity	7.49 ft/s	
Velocity Head	0.87 ft	
Specific Energy	3.21 ft	
Froude Number	1.223	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	28.0 in	
Critical Depth	30.4 in	
Channel Slope	0.020 ft/ft	
Critical Slope	0.013 ft/ft	

Worksheet for Basin 1 Temp Drainage Swale

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Project Description		
Friction Method	Manning Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.030 ft/ft	
Normal Depth	27.0 in	
Left Side Slope	3.000 H:V	
Right Side Slope	3.000 H:V	
Results		
Discharge	136.07 cfs	
Flow Area	15.2 ft ²	
Wetted Perimeter	14.2 ft	
Hydraulic Radius	12.8 in	
Top Width	13.50 ft	
Critical Depth	31.7 in	
Critical Slope	0.013 ft/ft	
Velocity	8.96 ft/s	
Velocity Head	1.25 ft	
Specific Energy	3.50 ft	
Froude Number	1.489	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	27.0 in	
Critical Depth	31.7 in	
Channel Slope	0.030 ft/ft	
Critical Slope	0.013 ft/ft	

Worksheet for Basin 2 Temp Drainage Swale

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Project Description		
Friction Method	Manning Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.020 ft/ft	
Normal Depth	22.0 in	
Left Side Slope	3.000 H:V	
Right Side Slope	3.000 H:V	
Results		
Discharge	64.35 cfs	
Flow Area	10.1 ft ²	
Wetted Perimeter	11.6 ft	
Hydraulic Radius	10.4 in	
Top Width	11.00 ft	
Critical Depth	23.5 in	
Critical Slope	0.014 ft/ft	
Velocity	6.38 ft/s	
Velocity Head	0.63 ft	
Specific Energy	2.47 ft	
Froude Number	1.175	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	22.0 in	
Critical Depth	23.5 in	
Channel Slope	0.020 ft/ft	
Critical Slope	0.014 ft/ft	

Worksheet for Basin 3 Temp Drainage Swale

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Project Description		
Friction Method	Manning	
	Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.020 ft/ft	
Normal Depth	18.0 in	
Left Side Slope	3.000 H:V	
Right Side Slope	3.000 H:V	
Results		
Discharge	37.68 cfs	
Flow Area	6.8 ft ²	
Wetted Perimeter	9.5 ft	
Hydraulic Radius	8.5 in	
Top Width	9.00 ft	
Critical Depth	18.9 in	
Critical Slope	0.015 ft/ft	
Velocity	5.58 ft/s	
Velocity Head	0.48 ft	
Specific Energy	1.98 ft	
Froude Number	1.136	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Lenath	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	18.0 in	
Critical Depth	18.9 in	
Channel Slope	0.020 ft/ft	
Critical Slope	0.015 ft/ft	

Worksheet for Basin 4 Temp Drainage Swale

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Project Description		
Friction Method	Manning	
Calva Far	Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.008 ft/ft	
Normal Depth	24.0 in	
Left Side Slope	3.000 H:V	
Right Side Slope	3.000 H:V	
Results		
Discharge	49.70 cfs	
Flow Area	12.0 ft ²	
Wetted Perimeter	12.6 ft	
Hydraulic Radius	11.4 in	
Top Width	12.00 ft	
Critical Depth	21.2 in	
Critical Slope	0.015 ft/ft	
Velocity	4.14 ft/s	
Velocity Head	0.27 ft	
Specific Energy	2.27 ft	
Froude Number	0.730	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	24.0 in	
Critical Depth	21.2 in	
Channel Slope	0.008 ft/ft	
Critical Slope	0.015 ft/ft	

Worksheet for Basin 5 Temp Drainage Swale

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Project Description		
Friction Method	Manning Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.020 ft/ft	
Normal Depth	27.0 in	
Left Side Slope	3.000 H:V	
Right Side Slope	3.000 H:V	
Results		
Discharge	111.10 cfs	
Flow Area	15.2 ft ²	
Wetted Perimeter	14.2 ft	
Hydraulic Radius	12.8 in	
Top Width	13.50 ft	
Critical Depth	29.2 in	
Critical Slope	0.013 ft/ft	
Velocity	7.32 ft/s	
Velocity Head	0.83 ft	
Specific Energy	3.08 ft	
Froude Number	1.216	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	, 0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	27.0 in	
Critical Depth	29.2 in	
Channel Slope	0.020 ft/ft	
Critical Slope	0.013 ft/ft	

Worksheet for Basin 6 North Temp Drainage Swale

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666
Project Description		
Friction Method	Manning	
Calua Fau	Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.035 ft/ft	
Normal Depth	23.0 in	
Left Side Slope	3.000 H:V	
Right Side Slope	3.000 H:V	
Results		
Discharge	95.84 cfs	
Flow Area	11.0 ft ²	
Wetted Perimeter	12.1 ft	
Hydraulic Radius	10.9 in	
Top Width	11.50 ft	
Critical Depth	27.5 in	
Critical Slope	0.013 ft/ft	
Velocity	8.70 ft/s	
Velocity Head	1.18 ft	
Specific Energy	3.09 ft	
Froude Number	1.566	
Flow Type	Supercritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	23.0 in	
Critical Depth	27.5 in	
Channel Slope	0.035 ft/ft	
Critical Slope	0.013 ft/ft	

Worksheet for Basin 7 Temp Drainage Swale

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Project Description		
Friction Method	Manning Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.013 ft/ft	
Normal Depth	29.0 in	
Left Side Slope	3.000 H:V	
Right Side Slope	3.000 H:V	
Results		
Discharge	108.38 cfs	
Flow Area	17.5 ft ²	
Wetted Perimeter	15.3 ft	
Hydraulic Radius	13.8 in	
Top Width	14.50 ft	
Critical Depth	28.9 in	
Critical Slope	0.013 ft/ft	
Velocity	6.19 ft/s	
Velocity Head	0.59 ft	
Specific Energy	3.01 ft	
Froude Number	0.992	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Lenath	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0 0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	29.0 in	
Critical Depth	28.9 in	
Channel Slope	0.013 ft/ft	
Critical Slope	0.013 ft/ft	

Worksheet for Basin 6 East Temp Drainage Swale

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Project Description		
Friction Method	Manning Formula	
Solve For	Discharge	
Input Data		
Roughness Coefficient	0.030	
Channel Slope	0.013 ft/ft	
Normal Depth	29.0 in	
Left Side Slope	3.000 H:V	
Right Side Slope	3.000 H:V	
Results		
Discharge	108.38 cfs	
Flow Area	17.5 ft ²	
Wetted Perimeter	15.3 ft	
Hydraulic Radius	13.8 in	
Top Width	14.50 ft	
Critical Depth	28.9 in	
Critical Slope	0.013 ft/ft	
Velocity	6.19 ft/s	
Velocity Head	0.59 ft	
Specific Energy	3.01 ft	
Froude Number	0.992	
Flow Type	Subcritical	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	29.0 in	
Critical Depth	28.9 in	
Channel Slope	0.013 ft/ft	
Critical Slope	0.013 ft/ft	

Worksheet for Basin 6 South Temp Drainage Swale

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

APPENDIX F – OFFSITE DRAINAGE ANALYSIS

Kimley **»Horn**

Project Description				
Friction Method	Manning			_
Solve For	Discharge			
Input Data	-			-
Channel Slone	0 019 ft/ft			-
Normal Depth	12.0 in			
	Se	ction Definitions		-
Statio	n		Elevation	
(π)		-0+85	(π)	1.00
		-0+85		0.00
		0+20		0.00
		0+26		2.00
		0+46		2.00
	Rouahne	ss Seament Definitions		
Start Station	y	Ending Station	Poughnoss Coofficient	
(-0+85, 1.00)		(0+46, 2.00)	Roughness coencient	0.030
(0 . 00) 2.00)		(0 + 10) _100)		_
Options				_
Current Roughness Weighted Method	Pavlovskii's Method			
Open Channel Weighting Method	Pavlovskii's Method			
Closed Channel Weighting	Pavlovskii's Method			
Method	Method			-
Results				
Discharge	306.33 cfs			-
Roughness Coefficient	0.030			
Elevation Range	0.0 to 2.0 ft			
Flow Area	64.0 ft ²			
Wetted Perimeter	108.2 ft			
Hydraulic Radius	7.1 in			
Top Width	108.00 ft			
Normal Depth	12.0 in			
Critical Depth	12.5 in			
Critical Slope	0.015 ft/ft			
Velocity	4.79 ft/s			
	0.36 ft			
Specific Energy	1.36 ft			
	1.096			
ном туре	Supercritical			-
GVF Input Data				-
	Bentley Syste	ems, Inc. Haestad Methods Solution		– FlowMast

Temporary Drainage Swales.fm8 6/29/2022 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	12.0 in	
Critical Depth	12.5 in	
Channel Slope	0.019 ft/ft	
Critical Slope	0.015 ft/ft	

Temporary Drainage Swales.fm8 6/29/2022 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Project Description				
Friction Method	Manning			_
Solve For	Discharge			
Input Data	-			-
Channel Slone	0 019 ft/ft			-
Normal Depth	12.0 in			
	Se	ction Definitions		-
Statio	n		Elevation	
(π)		-0+85	(π)	1.00
		-0+85		0.00
		0+20		0.00
		0+26		2.00
		0+46		2.00
	Rouahne	ss Seament Definitions		
Start Station	y	Ending Station	Poughnoss Coofficient	
(-0+85, 1.00)		(0+46, 2.00)	Roughness coencient	0.030
(0 . 00) 2.00)		(0 · · · · · · · · · · · · · · · · · · ·		_
Options				_
Current Roughness Weighted Method	Pavlovskii's Method			
Open Channel Weighting Method	Pavlovskii's Method			
Closed Channel Weighting	Pavlovskii's Method			
Method	Method			-
Results				
Discharge	306.33 cfs			-
Roughness Coefficient	0.030			
Elevation Range	0.0 to 2.0 ft			
Flow Area	64.0 ft ²			
Wetted Perimeter	108.2 ft			
Hydraulic Radius	7.1 in			
Top Width	108.00 ft			
Normal Depth	12.0 in			
Critical Depth	12.5 in			
Critical Slope	0.015 ft/ft			
Velocity	4.79 ft/s			
	0.36 ft			
Specific Energy	1.36 ft			
	1.096			
ном туре	Supercritical			-
GVF Input Data				-
	Bentley Syste	ems, Inc. Haestad Methods Solution		– FlowMast

Temporary Drainage Swales.fm8 3/29/2022

27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	12.0 in	
Critical Depth	12.5 in	
Channel Slope	0.019 ft/ft	
Critical Slope	0.015 ft/ft	

Temporary Drainage Swales.fm8 3/29/2022

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Project Description	
Friction Method	Manning Formula
Solve For	Discharge
Input Data	
Channel Slope	0.019 ft/ft
Normal Depth	12.0 in
Discharge	306.33 cfs
	2.20
	2.00
	1.80
	1.60
	1.40
	5 1.20
	₩ 1.00 × · · · · · · · · · · · · · · · · · ·
	÷ 0.80
	0.60
	0.40
	0.20
	0.00
	-0.20
	-0+50 0+00 Station

Cross Section for North Offsite Drainage Berm

Temporary Drainage Swales.fm8 6/29/2022

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APPENDIX G – DRAINAGE EXHIBITS

Kimley **»Horn**



BASIN ID	BASIN		RATIONAL ANALYSIS RESULTS	
	(Ac.)		Q₅ (CFS)	Q100 (CFS)
BJD—12a	54.28		8	61
BJD-12b	9.54		2	15
BJD-12c	18.23		3	21
		BJD-K	4	31
JCD OS-1A	36.0		5	38
JCD OS-1B	20.7		5	33
JCDEX-3.1	68.6		9	69
JCDEX-3.2	13.21		3	22
		JCD-D	12	84
JCDEX-3.3	10.0		3	19
BJDEX14	6.16		2	14
		A	3	19
		A*	5	25

A* – MODELLED AS BASIN OS–1 IN THE FINAL DRAINAGE REPORT FOR FILING 1 OF TRAILS AT ASPEN RIDGE, APP'D ON FEBRUARY 13, 2020.



PROPOSED PRIVATE TEMPORARY SEDIMENT. BASIN 1 BASIN BOTTOM WIDTH AVERAGE: 120' BASIN BOTTOM LENGTH: 325' 54.28 <u>80.0</u> DEPTH 4' 61 SPILLWAY CREST LENGTH: 75' SPILLWAY CREST HEIGHT: 3.30' RISER PIPE HOLE DIAMETER: (3) 1 11/16" RISER PIPE HEIGHT: 1.62' RISER PIPE HOLE SEPARATIONS: 6.50" REQUIRED VOLUME: 68,616 CF PROPOSED VOLUME: 188,805 CF (BASIN TO BE CONVERTED TO A FULL PROPOSED PRIVATE TEMPORARY SEDIMENT BASIN 3B-SPECTRUM DETENTION BASIN AT FINAL BASIN BOTTOM WIDTH: 50' DESIGN AND DEVELOPMENT) BASIN BOTTOM LENGTH: 345' SPILLWAY CREST LENGTH: 12' RISER PIPE HOLE DIAMETER: $\frac{27}{33}$ " – D – REQUIRED VOLUME: 2,075 CF PROPOSED VOLUME: 45,000 CF 80.0 9.54 RW-100 1.61 10.77 BIG / JOHNSON BASIN 19.06 95.0 . 120.65 OUTLET/STANDPIPE --5989_ EX. PUBLIC 10'X6' REINFORCED-CONCRETE BOX CULVERT BASIN 1 TEMP SWALE PROPOSED UDFCD DS-2 COMPACTED UNLINED TEMPORARY DRAINAGE SWALE 1 FORMED BY CUT AND FILL TOP WIDTH: 14' V-SWALE PROPOSED PRIVATE TEMPORARY SEDIMENT BASIN 4B-BASIN BOTTOM WIDTH: 50' BASIN BOTTOM LENGTH: 345' DEPTH 2' SPILLWAY CREST LENGTH: 12' RISER PIPE HOLE DIAMETER: 27" REQUIRED VOLUME: 28,296 CF \ PROPOSED VOLUME: 45,000 CF PROPOSED PRIVATE TEMPORARY SEDIMENT BASIN 4A 5995-BASIN BOTTOM WIDTH: 60' BASIN BOTTOM LENGTH: 355' DEPTH: 2'\ SPILLWAY CREST LENGTH: 12' RISER PIPE DIAMETER: 27 REQUIRED VOLUME: 28,296 PROPOSED VOLUME: 45,333 PROPERTY LINE BASIN 4 TEMP SWALE PROPOSED UDFCD DS-1 COMPACTED EXCAVATED UNLINED TEMPORARY DRAINAGE SWALE TOP WIDTH: 9.0' 3:1 SIDE SLOPES BASIN 2 EAST TEMP SWALE PROPOSED UDFCD DS-21 COMPACTED UNLINED TEMPORARY DRAINAGE SWALE 2 FORMED BY CUT AND FILL TOP WIDTH: 13.5' V-SWALE BASIN 2 SOUTH TEMP SWALE -PROPOSED UDFCD DS-2 COMPACTED UNLINED TEMPORARY DRAINAGE SWALE 2 FORMED BY CUT AND FILL DRAINAGE EXHIBIT - WATERVIEW NORTH COLORADO SPRINGS, CO



Kimley»Horn

	SU	MMARY - PR	OPOSED RU	NOFF TABLE	
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	IMPERVIOUSNESS (%)
1	1	19.06	66.15	120.65	0.95
2	2	20.77	72.34	131.96	0.95
3	3	8.16	33.27	60.69	0.95
4	4	7.86	16.46	34.97	0.70
5	5	9.73	21.15	44.93	0.70
6	6	26.44	49.21	104.53	0.70
7	7	22.41	41.88	88.96	0.70
RW-1	RW-1	1.61	6.02	10.77	100.00
RW-2	RW-2	1.33	5.72	10.25	100.00
RW-3	RW-3	0.60	2.69	4.83	100.00
RW-4	RW-4	0.65	2.79	5.01	100.00
RW-5	RW-5	0.47	2.16	3.87	100.00

-20' LONG X 10' WIDE TYPE VL (6-IN-DIAMETER), 12-IN THICK RIPRAP

400

PROPOSED VOLUME: 666.837 CF (BASIN TO BE CONVERTED TO A FULL SPECTRUM DETENTION BASIN AT FINAL DESIGN AND DEVELOPMENT -PROPERTY LINE

3:1 SIDE SLOPES PROPOSED PRIVATE TEMPORARY SEDIMENT BASIN BOTTOM WIDTH: 210' BASIN BOTTOM LENGTH: 400' SPILLWAY CREST LENGTH: 75' SPILLWAY CREST HEIGHT: 3' RISER PIPE HOLE SIZE: (3) 1"X 3 $\frac{3}{4}$ " RECTANGULAR HOLES RISER PIPE HEIGHT: 2.64' RISER PIPE HOLE SEPARATIONS: 10.60" REQUIRED VOLUME: 175,860 CF

TOP WIDTH: 16' 3:1 SIDE SLOPES BASIN 6 SOUTH TEMP SWALE PROPOSED UDFCD DS-2 COMPACTED UNLINED TEMPORARY DRAINAGE SWALE FORMED BY CUT AND FILL TOP WIDTH: 14.5'

-BASIN 6 EAST TEMP SWALE PROPOSED UDFCD DS-2 COMPACTED UNLINED TEMPORARY DRAINAGE SWALE 6 FORMED BY CUT AND FILL

OS-80.0 20.7 33

LEGEND A = BASIN DESIGNATIONА B = AREA (ACRES)C = BASIN IMPERVIOUSNESSB

---- --- EASEMENT

– XXXX ——

0

— XXXX — _ ____

FLOW DIRECTION

PROPERTY BOUNDARY

EXISTING STORM SEWER

RIPRAP

SPILLWAY

- --- XXXX - --- EXISTING MINOR CONTOUR

MAJOR FEE BASIN DELINEATION

DRAINAGE BASIN BOUNDARY

----- PROPOSED MAJOR CONTOUR

EXISTING MAJOR CONTOUR

PROPOSED STORM SEWER

PROPOSED STORM INLET

= DESIGN POINT

D = 100YR DESIGN STORM RUNOFF (CFS)

APPENDIX H – MASTER DRAINAGE BASIN EXHIBIT AND CALCULATIONS

Kimley **»Horn**



LEGEND



SUMMARY - PROPOSED RUNOFF TABLE					
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	IMPERVIOUSNESS (%)
BJB	BJB	26.20	7.18	48.21	0.02
JCCB	JCCB	90.34	22.74	152.69	0.02

BJB JCCB

JIMMY CAMP CREEK BASIN

BIG JOHNSON BASIN

→ PROPERTY LINE

Kimley»Horn

096955000

IDF Equations:

I ₁₀₀ =	-2.52ln(D) + 12.735
l ₅₀ =	-2.25ln(D) + 11.375
₂₅	-2.00ln(D) + 10.111
I_{10}	-1.75ln(D) + 8.847
I۶	-1.50ln(D) + 7.583
l ₂	-1.19ln(D) + 6.035

Where:

I = Rainfall Intensity (in/hr)
D= Duration (minutes)

	<u>2-yr</u>	<u>5-yr</u>	<u>10-yr</u>	<u>100-yr</u>
P1 =	1.19	1.5	1.75	2.52

*The Design Point Rainfall Values and Time Intensity Frequency Tabulation are found in Table 6-2 and Figure 6-5, respectively of the Colorado Springs Drainage Criteria Manual, Volume1

Waterview North (Major Basins) Drainage Report Colorado Springs, CO

Weighted Imperviousness Calculations

SUB-	AREA	AREA	SOIL GROUP	WEIGHTED	WEIGHTED COEFFICIENT			S
BASIN	(SF)	(Acres)	DESIGNATION	IMPERVIOUSNESS	C2	C5	C10	C100
BJB	1,141,190	26.20	A/B	2.0%	0.03	0.09	0.17	0.36
JCCB	3,935,162	90.34	A/B	2.0%	0.03	0.09	0.17	0.36
TOTAL	5,076,352	116.54						

9/29/22 Calculated by: JJM



Watervie	Waterview North - Drainage Report Watercourse Coefficient															
Proposed	l Runoff Cal	culations			Forest	& Meadow	2.50	Short G	rass Pastur	e & Lawns	7.00			Grasse	d Waterway	15.00
Time of Concentration						Cultivation	5.00		Nearly Ba	re Ground	10.00		Paveo	d Area & Sha	allow Gutter	20.00
		SUB-BASIN			INIT	IAL / OVERL	AND	T	RAVEL TIN	IE				T(c) CHECK		FINAL
DATA						TIME		T(t)					(URE	BANIZED BA	SINS)	T(c)
DESIGN	DRAIN	AREA	AREA	C(5)	Length	Slope	T(i)	Length	Slope	Coeff.	Velocity	T(t)	COMP.	TOTAL	L/180+10	
POINT	BASIN	sq. ft.	ac.		ft.	%	min	ft.	%		fps	min.	T(c)	LENGTH		min.
BJB	BJB	1,141,190	26.20	0.09	100	3.0%	12.8	1811	10.0%	2.50	0.8	38.2	51.0	1911	20.6	20.6
JCCB	JCCB	3,935,162	90.34	0.09	100	5.0%	10.8	2466	9.5%	2.50	0.8	53.3	64.1	2566	24.3	24.3

Waterview North - Drainage Report Proposed Runoff Calculations Design Storm 5 Year (Rational Method Procedure)												
B	ASIN INFORMATIO	N			DIRECT	RUNOFF		CL	IMMULAT	IVE RUNC)FF	
DESIGN	DRAIN	AREA	RUNOFF	T(c)	СхА	1	Q	T(c)	СхА	I	Q	NOTES
POINT	BASIN	ac.	COEFF	min		in/hr	cfs	min		in/hr	cfs	
BJB	BJB	26.20	0.09	20.6	2.36	3.05	7.18					
JCCB	JCCB	90.34	0.09	24.3	8.13	2.80	22.74					

Waterview North - Drainage Report Proposed Runoff Calculations Design Storm 100 Year (Rational Method Procedure)												
E	BASIN INFORMATION	1		DIR	ECT RUNG	DFF		C	UMMULAT	IVE RUNO	-F	
DESIGN	DRAIN	AREA	RUNOFF	T(c)	CxA	I	Q	T(c)	СхА	I	Q	NOTES
POINT	BASIN	ac.	COEFF	min		in/hr	cfs	min		in/hr	cfs	
BJB	BJB	26.20	0.36	20.6	9.43	5.11	48.21					
JCCB	JCCB	90.34	0.36	24.3	32.52	4.69	152.69					

SUMMARY - PROPOSED RUNOFF TABLE											
DESIGN POINT	BASIN DESIGNATION	BASIN AREA (ACRES)	DIRECT 5-YR RUNOFF (CFS)	DIRECT 100-YR RUNOFF (CFS)	IMPERVIOUSNESS (%)						
BJB	BJB	26.20	7.18	48.21	0.02						
JCCB	JCCB	90.34	22.74	152.69	0.02						