

RICH,

We do need to get the fee issue resolved, so that the DBPS can be updated & the MDDP approved. Has Nor'wood decided how they want to proceed? Do they want me to set up a

Master Development Drainage Plan  
Wolf Ranch Development

City of Colorado Springs, Colorado

meeting with  
Dave L. &  
Cam?

Does the Stormwater  
Enterprise have  
any impact on  
how they want  
to proceed?

Prepared For:

Nor'wood Development Group  
4065 Sinton Road Suite 200  
Colorado Springs, CO 80907

Prepared By:

Kiowa Engineering Corporation  
1604 South 21<sup>st</sup> Street  
Colorado Springs, Colorado 80904

Project Number 03094  
July 2004  
Revised November 2004  
Revised February 15, 2005

MRM  
1/16/06

	<u>Page</u>
<b>TABLE OF CONTENTS</b> .....	ii
<b>ENGINEERING STATEMENT</b> .....	iii
<b>PROJECT AREA DESCRIPTION</b> .....	1
<b>PREVIOUS REPORTS</b> .....	1
<b>HYDROLOGY</b> .....	3
<b>EXISTING MAJOR SUB-WATERSHED DESCRIPTIONS</b> .....	4
<b>DEVELOPED MAJOR SUB-WATERSHEDS</b> .....	9
<b>HYDROLOGY RESULTS</b> .....	9
<b>REGIONAL DETENTION HYDROLOGY</b> .....	11
<b>HYDRAULICS</b> .....	13
<b>FLOODPLAIN STATEMENT</b> .....	14
<b>PROPOSED FACILITIES</b> .....	14
Detention .....	14
Drainageways.....	16
Drop and Check structures .....	17
Roadway Crossings.....	17
Trails .....	18
Maintenance.....	18
Right-of-way.....	19
<b>DRAINAGE BASIN FEES</b> .....	20
 <b>LIST OF TABLES</b>	
Table 1 Comparison of 100-year Peak Discharges.....	10
Table 2 Comparison of Existing, Future and Detained Condition Peak Discharges .....	12
 <b>LIST OF FIGURES</b>	
Figure 1            Vicinity Map.....	2
Figure 2            Hydrologic Soils Map .....	5
Figure 3            Hydrologic Land Use Map .....	6
Figure 4            Existing Condition Sub-basin Map .....	MP
Figure 5            Proposed Condition Sub-basin Map .....	MP
Figure 6            Proposed Facilities.....	MP
Figure 7            Floodplain Information .....	15
 Appendix A – Hydrologic Calculations	
Appendix B – Hydraulic Calculations	
Appendix C – Plan and Profiles	

**ENGINEER'S STATEMENT:**

The attached master development drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City/County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Kiowa Engineering Corporation, 1604 South 21<sup>st</sup> Street, Colorado Springs, Colorado 80904

\_\_\_\_\_  
Richard N. Wray  
Registered Engineer # 19310

\_\_\_\_\_  
Date

**DEVELOPER'S STATEMENT:**

I, the Developer, have read and will comply with all of the requirements specified in this drainage report and plan.

BY: \_\_\_\_\_  
Date

ADDRESS: Nor'wood Development Group  
Plaza of the Rockies  
102 South Tejon Suite 200  
Colorado Springs, CO 80903

**CITY OF COLORADO SPRINGS**

Filed in accordance with Section 7-7-906 of the Code of the City of Colorado Springs, 2001, as amended.

\_\_\_\_\_  
**City Engineer**

\_\_\_\_\_  
**Dated**

## **PROJECT DESCRIPTION**

Wolf Ranch Development is a master planned community located in northeast Colorado Springs. The master development plan includes open space, parks, drainage, residential, office and commercial uses. The development covers approximately 1800 acres. The development is located bordered by Black Forest Road on the east, Old Ranch Road on the north, the Cordera development on the west and Cowpoke Road on the south. The location of the site is presented on Figure 1.

The property subject to development is located in portions of Sections 30 and 31 Township 12 South, Range 65 West of the 6th Principal Meridian and Section 6 Township 13 South Range 65 West of the 6<sup>th</sup> Principal Meridian. The development subject to master drainage planning has a segment of Cottonwood Creek that passes through the southern portion of the site as well as a major sub-tributary designated as Tributary Four in this report. The property lies completely within the Cottonwood Creek basin.

## **PREVIOUS REPORTS**

The following reports and plans were reviewed in the process of preparing this master development drainage plan:

1. Soil Survey for El Paso County, Colorado, dated June 1981.
2. "City of Colorado Springs/El Paso County Drainage Criteria Manual", prepared by City of Colorado Springs, El Paso County, dated May 1987, revised 1996.
3. Cottonwood Creek Drainage Basin Planning Study (DBPS) prepared by URS, Inc., dated 1994.
4. Cottonwood Creek Drainage Basin Planning Study prepared by Ayres Associates, Inc. dated June 2000.
5. Westcreek at Wolf Ranch Subdivision Master Development Drainage Plan and Final Drainage Report for Westcreek at Wolf Ranch Filings Nos. 1, 2, 3, 4 and 5, prepared by Rockwell Consulting, dated September 2003.
6. Westcreek at Wolf Ranch Subdivision Master Development Drainage Plan and Final Drainage Report for Westcreek at Wolf Ranch Filings Nos. 6, 7, 8, 9, 10, 11 and 12 and Research Parkway at Wolf Ranch Filings 1, 2, and 3, prepared by Rockwell Consulting, dated December 2003.
7. HEC-1 Flood Hydrograph Package User's Manual, prepared by US Army Corps of Engineers Hydrologic Engineering Center, dated June 1998.
8. Prudent Line for Rural Areas in El Paso County Criteria prepared by Ayres Associates dated June 2000.



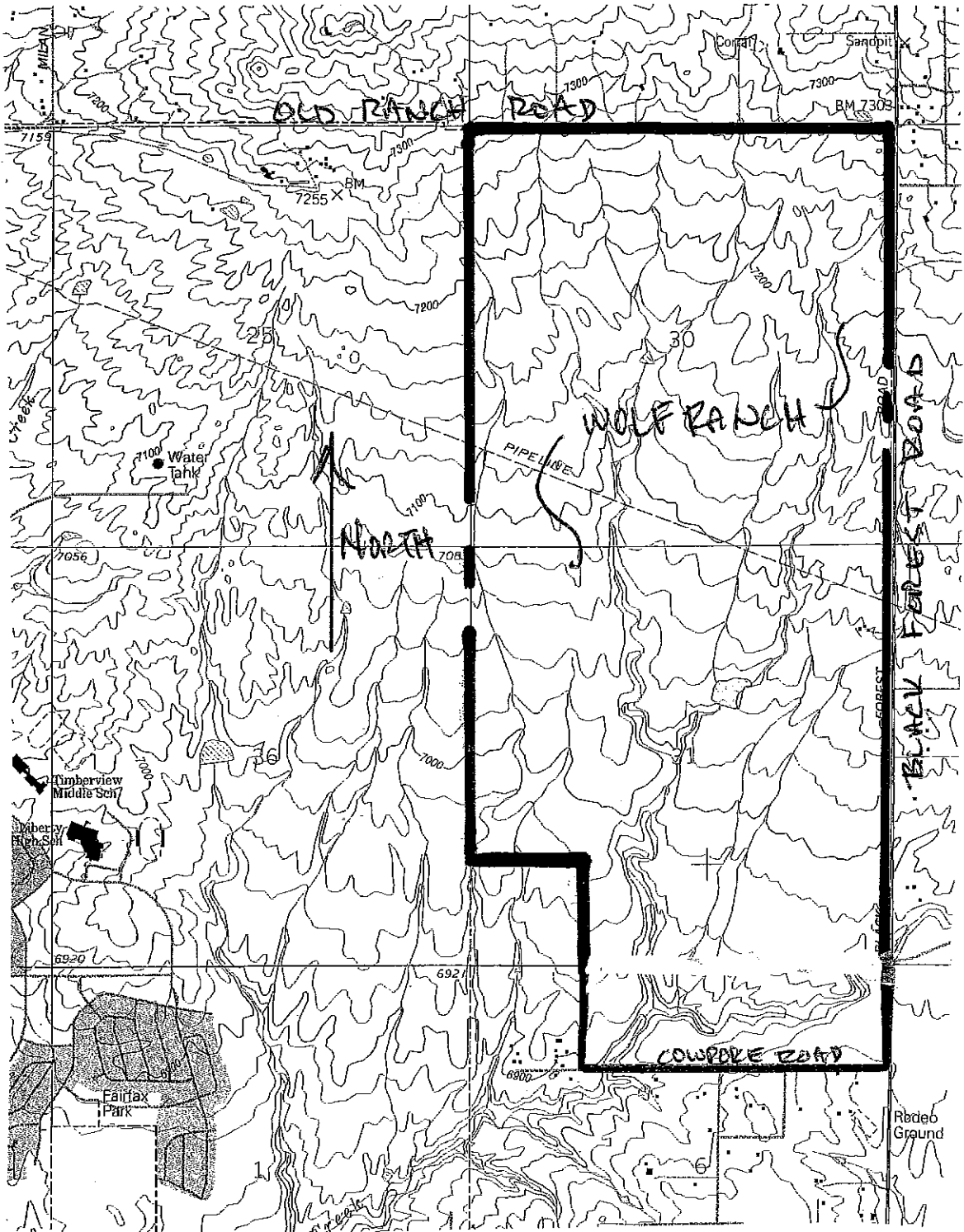


FIGURE 1  
VICINITY MAP

References 3 and 4 were prepared for the overall Cottonwood Creek Drainage basin and were used to establish the selected drainageway improvements for the basin. The City adopted the studies and used them in the establishment of the drainage and bridge fees for the basin. The primary difference between these two studies was that in Reference 4 the prudent line concept was incorporated into the DBPS as the preferred alternative channel design for the upper portions of Cottonwood Creek and for Tributary Four as well. The drainage fee was modified in Reference 4 to account for the land costs associated with the creation of a prudent line setback. No channel improvements other than grade control structures were recommended for Cottonwood Creek and Tributary Four for the reaches within the Wolf Ranch development. The peak discharges summarized in Reference 4 were applied in the design of bank improvements and grade controls for the portion of Cottonwood Creek that passes through the southern portion of the development.

References 5 and 6 were used to establish the proposed major drainage structures within the Filings covered by these master development drainage plans and final drainage reports. Storm sewer outfall sewers and detention basins shown recommended in these studies were considered when the hydrologic models were developed for this MDDP.

The purpose of this MDDP is to develop the hydrologic model of the onsite and offsite watersheds related to the Master Planned area. It is also the focus of this MDDP to evaluate the storm sewer infrastructure to be constructed as part of the Westcreek and greater Wolf Ranch developments, and to establish the size, type, and location of the major drainageway facilities for Wolf Ranch. It should however be expected that modifications in the size and location of the major drainageway facilities as shown herein might occur depending upon the actual development of the land within the Wolf Ranch property. In particular the location of the regional detention basins may be shifted as alternatives are analyzed as part of the land development process.

## **HYDROLOGY**

The offsite and onsite hydrology for the site was estimated using the methods outlined in the City/County Storm Drainage Criteria Manual. Topography for the site was compiled at a two-foot contour interval and a horizontal scale of one inch to 400-feet. This topography was used to verify the onsite sub-basin boundaries. Offsite sub-basin boundaries were determined using the above referenced reports, the City of Colorado Springs FIMS mapping base, and the USGS quadrangle maps for the area. Field inspections were also carried out in order to confirm or refine subdivision limits.

Existing and developed condition peak discharges for the sub-basins and design points along the major drainageway associated with Tributary Four and Cottonwood Creek shown on the Hydrologic Sub-basin Map were determined for the 5-year and 100-year recurrence intervals. The 24-hour storm duration was modeled using a Type IIA rainfall distribution. The total 24-hour rainfall depth was 2.5 and 4.4 inches for the 5- and 100-year frequencies, respectively. No area reduction factor was applied to the rainfall distribution and total depths.

Soils within the Wolf Ranch are mostly classified into hydrologic soils group B as shown in Reference 1. A small amount of hydrologic soil group A exists along the west-bank of Tributary Four in the southern portion of the development. For the purposes of modeling the developed conditions, all soils within the development were assumed to be hydrologic soil group B. Presented on Figure 2 are the hydrologic soil types that can be found within the Wolf Ranch development.

Land uses within the development were determined using the master development plan for Wolf Ranch. The development land will be of mixed uses. The land uses were used in the establishment of the curve numbers (CN values) that were input to the HEC-1 model. For the existing development condition and CN value of 61 was used for all of existing sub-basins within the development. Presented on Figure 3 is the hydrologic land use map for Wolf Ranch and their associated CN-values.

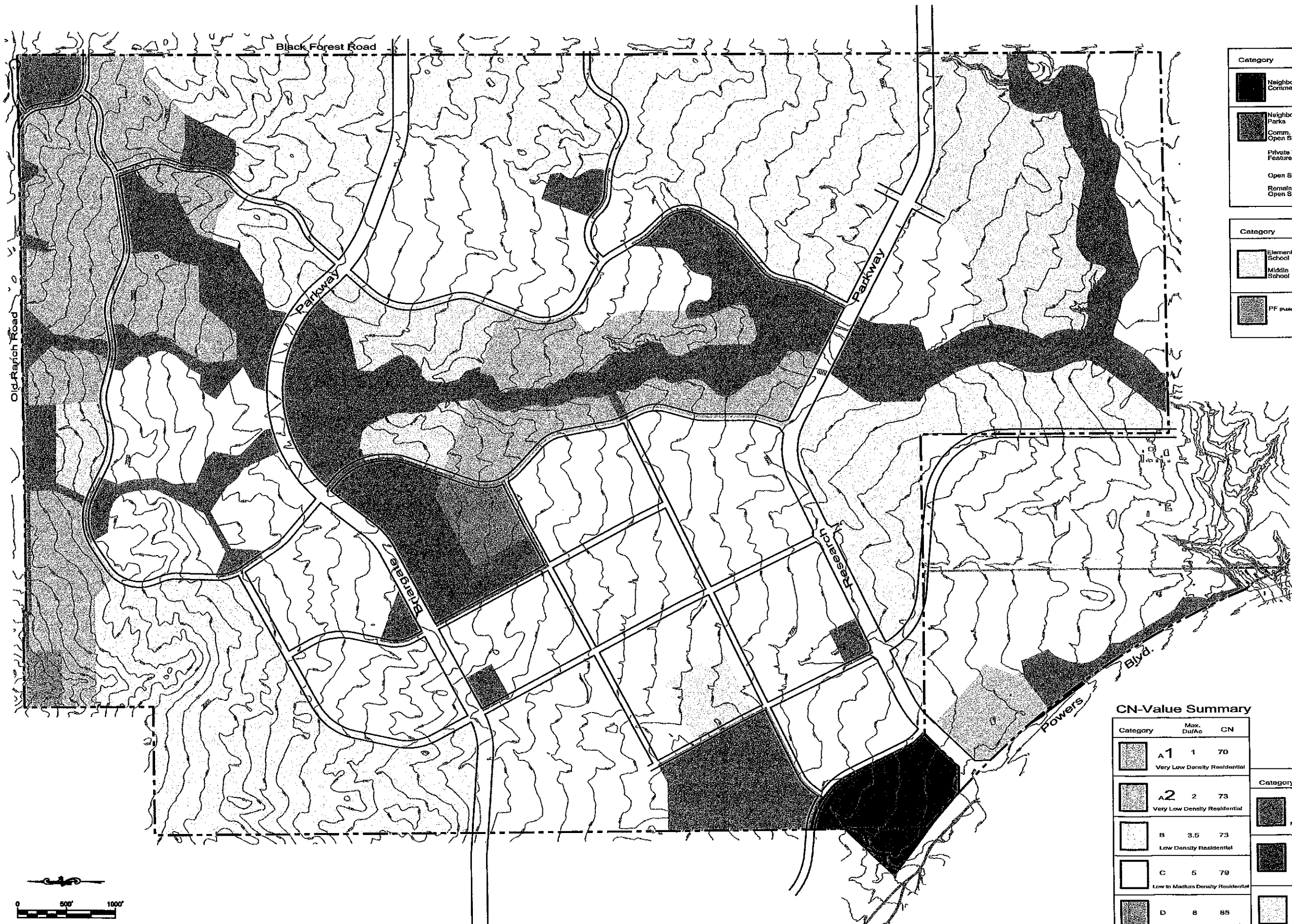
The time of concentration for each of the sub-basins modeled was estimated. The time of concentration was computed from a combination of overland flow, channel and pipe flow for each sub-basin. The time lag for each sub-basin was computed by reducing the time of concentration by 60 percent. The time lag was input to the HEC-1 model.

The Muskingum-Cunge routing technique was used to route the sub-basin hydrographs between design points. The majority of the routing elements were trapezoidal channel sections. Within the Westcreek portion of the development storm sewers were modeled. The longitudinal slope of each routing element was determined using the topographic mapping described above.

Hydrologic flow charts were prepared and are contained within Appendix A of this report. These flow charts were used to compile the HEC-1 model.

## **EXISTING MAJOR SUB-WATERSHED DESCRIPTIONS**

The study area was divided into eight major sub-watersheds. These sub-watersheds are noted in the hydrologic analysis by using the designations A through H. The sub-basins were coded accordingly (i.e., A-1, A-2, B-1, etc). The sub-basins for the existing condition are presented on Figure 4.



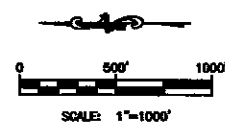
Category	CN
Neighborhood Commercial	92
Neighborhood Parks Comm. Parks/ Open Space	61
Private Entry Features	
Open Space	
Remaining Open Space	

Category	CN
Elementary School	75
Middle School	80
PF (Inaccessibility)	70

CN-Value Summary

Category	Max. Du/Ac	CN
A1 Very Low Density Residential	1	70
A2 Very Low Density Residential	2	73
B Low Density Residential	3.5	73
C Low to Medium Density Residential	5	79
D Medium Density Residential	8	85

Category	Max. Du/Ac	CN
E Medium to High Density Residential	12	88
F High Density Residential	25	92
Mixed Use Up to 25.00	25.00	92



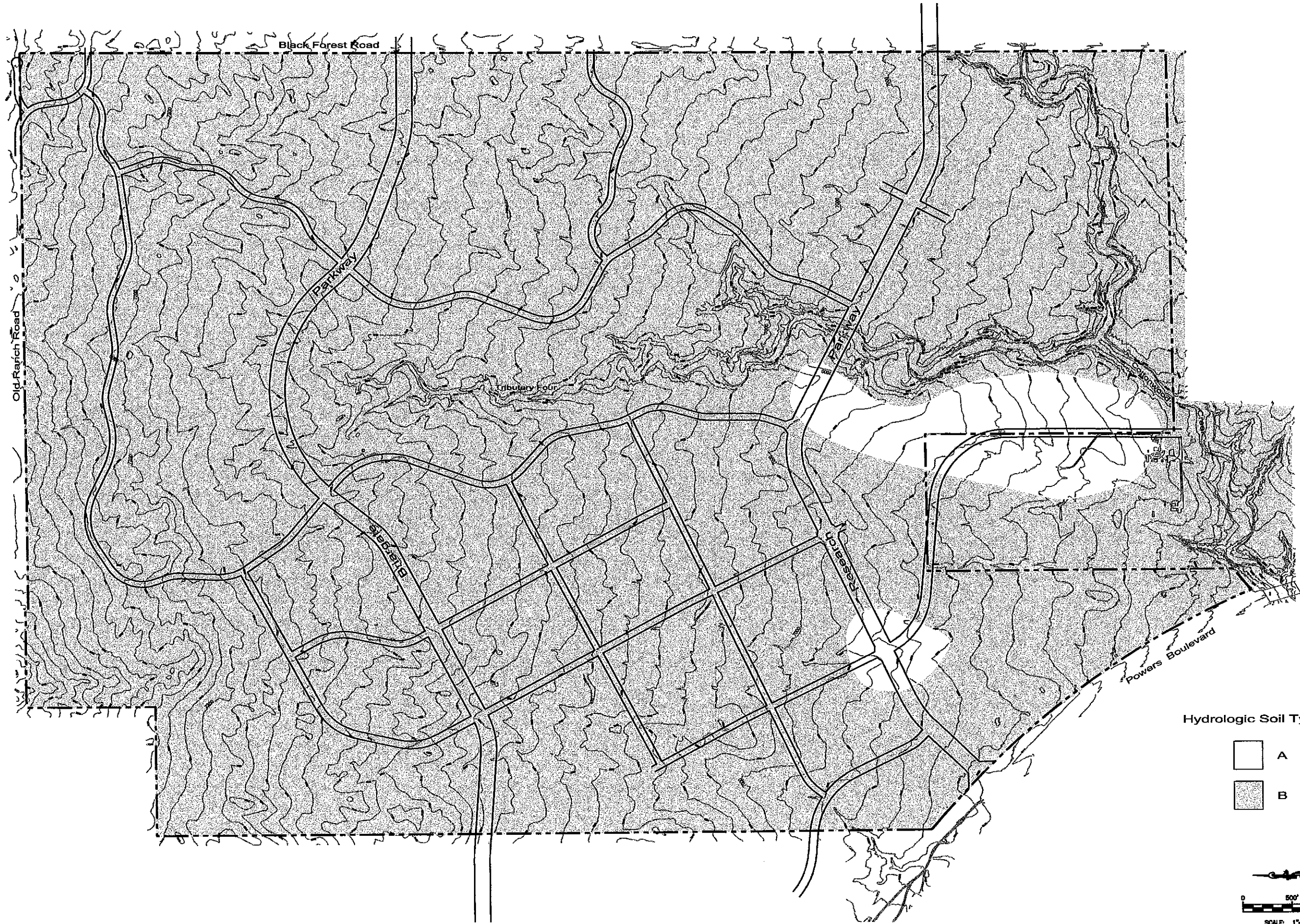
**Kiowa Engineering Corporation**  
 1604 South 21st Street  
 Colorado Springs, Colorado  
 80904  
 (719) 630-7342

**WOLF RANCH**  
**MASTER DEVELOPMENT DRAINAGE PLAN**  
**HYDROLOGIC LANDUSE MAP**  
 COLORADO SPRINGS, COLORADO

Project No.: 03084  
 Date: 01-04  
 Design: RNW  
 Drawn: EAK  
 Check: RNW  
 Revisions:

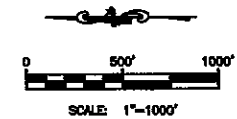
SHEET  
**Fig. 3**





Hydrologic Soil Type

- A
- B



**Kiowa Engineering Corporation**  
 1604 South 21st Street  
 Colorado Springs, Colorado  
 80904  
 (719) 630-7342

**WOLF RANCH**  
**MASTER DEVELOPMENT DRAINAGE PLAN**  
**HYDROLOGIC SOILS MAP**  
 COLORADO SPRINGS, COLORADO

Project No.: 03084  
 Date: 01-04  
 Design: RNW  
 Drawn: EAK  
 Check: RNW  
 Revisions:

SHEET  
**Fig. 2**

As shown on Figure 4 the "A" basins discharge to an existing concrete box culvert under Powers Boulevard. The sub-watershed drains a total of .42 square miles at its outfall point along the west boundary of the development. Slopes along the major drainageway range from 3 to 5 percent. Soils are entirely hydrologic soil group B. There is a portion of sub-basin A-1 that lies offsite from Wolf Ranch. The offsite portion of sub-basin A-1 is presently developed into large rural lots ranging in size from 5 to 40 acres. The watershed is well vegetated with native grasses. A small portion of sub-basin A-1 is forested.

The "B" basins discharge to an existing 54-inch reinforced concrete storm sewer that is within Research Parkway west of Powers Boulevard. The sub-watershed drains a total of .15 square miles at its outfall point at Powers Boulevard. Slopes along the major drainageway range from 2 to 5 percent. Soils are entirely hydrologic soil group B. Sub-watershed B lies entirely within Wolf Ranch. The watershed is well vegetated with native grasses.

The "C" basins discharge to an existing 72-inch reinforced concrete storm sewer that is under Powers Boulevard near the southwest corner of the property. The sub-watershed drains a total of .25 square miles at its outfall point at Powers Boulevard. Slopes along the major drainageway range from 2 to 5 percent. Soils are predominantly hydrologic soil group B however a small portion of type A soil exists within sub-basin C-1. Sub-watershed C lies entirely within Wolf Ranch. Most of sub-basin C-2 lies within the Westcreek subdivision Filings 1 through 3. The watershed is well vegetated with native grasses.

The "D" basins discharge to Cottonwood Creek within an offsite property just upstream of Powers Boulevard. The sub-watershed drains a total of .36 square miles at its outfall point at Cottonwood Creek. Slopes along the major drainageway range from 2 to 5 percent. Soils are predominantly hydrologic soil group B. Sub-watershed D lies mostly within Wolf Ranch however sub-basin D-3 lies within the Goetsch property that lies south of Wolf Ranch. The watershed is well vegetated with native grasses. The major drainageway within sub-basin D-3 is stable and has no improvements such as grade controls or bank lining. The drainageway is poorly defined where it enters Cottonwood Creek.

The "E" basins discharge to the Cottonwood Creek drainageway through an offsite property just upstream of Powers Boulevard. The sub-watershed drains a total of .32 square miles at its outfall point at Cottonwood Creek. Slopes along the major drainageway range from 2 to 5 percent. Soils are entirely hydrologic soil group B.

Approximately 60-percent of sub-watershed E lies within Wolf Ranch however 40 percent lies within the Goetsch property south of Wolf Ranch. The watershed is well vegetated with native grasses. The major drainageway within sub-basin E-2 is stable and has no improvements such as grade controls or bank lining. A stock pond exists along the drainageway within the Goetsch property.

“F” basins discharge to Cottonwood Creek approximately 4,000 feet upstream of the bridge over Powers Boulevard. The sub-watershed drains a total of 2 square miles at its outfall point. Slopes along the major drainageway range from 2 to 4 percent. Soils are mostly classified as hydrologic soil group B however a small area of Type A soil exist along the west overbank of Tributary Four south of Research Parkway. There is a portion of sub-watershed F that is offsite from Wolf Ranch. The offsite portion of the sub-watershed (i.e., sub-basins F-1 though F-7) is presently developed into large rural lots ranging in size from 5 to 40 acres. The watershed is well vegetated with native grasses. A small portion of the upper watershed is forested. The major drainageway in the F sub-watershed is Tributary 4. There are presently no improvements along the drainageway in the form of bank lings or grade controls. The low flow channel and some segments of the 100-year floodplain that have cross-section that is well incised.

The “G” basins discharge to Cottonwood Creek approximately 500 feet upstream of the outfall of sub-watershed F. The sub-watershed drains a total of .32 square miles at its outfall point. Slopes along the major drainageway range from 2 to 3 percent. Soils are entirely hydrologic soil group B. A portion of sub-watershed G lies offsite from Wolf Ranch. The offsite portion of the sub-watershed (i.e., sub-basin G-1) is presently developed into large rural lots ranging in size from 2.5 to 5 acres. The watershed is well vegetated with native grasses.

The “H” basin discharges to Cottonwood Creek just downstream of Black Forest Road. This sub-watershed drains a total of .093 square miles at its outfall point. Slopes along the watershed range from 2 to 6 percent. Soils are entirely hydrologic soil group B. The sub-watershed is well vegetated with native grasses.

It was assumed in this report that the portions of the A- and F-basins that lie north of Old Ranch Road will not develop to any higher land use densities than exist today. If denser development occurs north of Old Ranch Road, it has been further assumed that detention would be required so that the peak discharges flowing onto the Wolf Ranch development would not be increased over the existing condition rates calculated in this report.

## **DEVELOPED MAJOR SUB-WATERSHEDS**

The study area was divided into nine major sub-watersheds. These sub-watersheds are noted in the hydrologic analysis by using the designations A through J. The sub-basins were coded accordingly (i.e., A-1, A-2, B-1, etc). The sub-basins for the developed condition existing condition are presented on Figure 5. For the most part the developed condition sub-watershed boundaries cover similar areas as compared to existing sub-watersheds. The sub-basin divides were determined using the master development plan so that basin divides and key design points could be evaluated at future major roads. Some minor sub-basin rerouting and diversions have occurred. The curve-numbers were revised for the developed conditions. The developed curve numbers ranged from 61 to 90. The time of concentration values and resulting time lags were evaluating using developed flow paths and storm sewers where applicable.

## **HYDROLOGY RESULTS**

Presented of Figures 4 and 5 are the peak discharges that resulted from the hydrology analysis for sub-basins as well as at key design points within the development. Presented on Table 1 is a comparison of the DBPS discharges summarized in Reference 4 at each common design point. The variances in the peak discharges are largely the result of the differences between the HEC-1 model developed in the Reference 4 and this MDDP. A greater degree of sub-basin delineation has been applied in this MDDP that can cause differences in peak discharges. Differences if the sub-basin area can also produce variances between this MDDP and the DBPS. The input and output for the HEC-1 computer model for the existing and developed hydrologic analyses are contained within Appendix A of this report. There was no analysis conducted in this MDDP for the main stem of Cottonwood Creek. Peak discharges data shown on Table 1 that was obtained derived from the DBPS were applied in this MDDP for the estimation of the 100-year flood plain for Cottonwood Creek and the sizing selective of bank linings.

At design point A the primary difference between the 100-year peak discharge reported in Reference 4 and this MDDP is due to the larger basin area applied in this MDDP for the developed condition. A modestly lower curve number was applied in this MDDP compared to Reference 4. The lower curve number yields a lower unit discharge at design point A for the MDDP hydrology (i.e., 1,490 cubic feet per second/square mile (DBPS) versus 1,280 cubic feet per second/square mile (MDDP)). This result is consistent with the application of a lower curve number.

At design point F located at the confluence of Tributary Four and Cottonwood Creek the variance in the peak discharges is also the result of a larger area applied in the



**TABLE 1:**  
**COMPARISON OF 100-YEAR PEAK DISCHARGES**  
**DEVELOPED CONDITION WITHOUT DETENTION**  
**WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN**

DESIGN POINT (cfs)	DBPS (REFERENCE 4)		MDDP (KIOWA)	
	Q5 (cfs)	Q100 (cfs)	Q5 (cfs)	Q100 (cfs)
A	n/r	553	270	930
F	n/r	1,450	310	1,650
COTTONWOOD CREEK AT POWERS BOULEVARD	n/r	2,730 (1)	ne	ne
COTTONWOOD CREEK UPSTREAM OF TRIBUTARY FOUR	n/r	860 (1)	ne	ne

(1) Source: Cottonwood Creek DBPS, Ayres Associates, June 2000 (reference 4)

n/r = not reported in this MDDP

ne = no estimate made in this MDDP

MDDP and differing curve number. The unit discharges compare well between the DBPS and this MDDP, (i.e., 760 cubic feet per second/square mile (DBPS) versus 810 cubic feet per second/square (MDDP)).

### **REGIONAL DETENTION HYDROLOGY**

Detention storage was determined through an iterative process where an initial volume was calculated based on the changes of SCS curve numbers between the existing and developed condition. The initial volume was refined using the HEC-1 model resulting in the storage volumes summarized in this report. The proposed development condition was modeled with sufficient detention storage so that the flow rates were maintained to historic levels at each outfall point along the development's southern and western boundaries. The implementation of detention storage will have the affect of reducing the size of major drainageway facilities that may lie downstream of a detention basin. Detention will extend the time and duration of peak discharges but significantly reduce the magnitude of the peak flow rates for the 5- and 100-year recurrence intervals.

Presented on Figure 6 are the locations and hydraulic characteristics of six detention basins that are proposed within the Wolf Ranch development. Each detention basin would be built with an outlet structure that would control the 5-year and 100-year discharges from the detention basin to historic levels at the discharge points from the property. Detention basins within sub-watershed A, E/D, DB18, DB19 and G will have additional storage attributed to water quality. Onsite detention is recommended for the development that may occur within sub-watersheds H and J since no site with the physical attributes for a detention basin exists. Detention basins A, DB18, DB19 and DB28 have been sited to take into account a roadway embankment that could be integrated into the design of the detention basin. Presented on Table 2 are peak flow comparisons at the discharge point of each sub-watershed for the existing, developed and detained hydrologic conditions.

At design point A an "allowable" discharge of 553 cubic feet per second was determined in Reference 4. The allowable discharge at Design Point A represents the maximum release rate from a developed A watershed and would be within the hydraulic capacity of the Fairfax Detention Basin. The Fairfax detention basin lies downstream of Powers Boulevard and is a regional detention basin that receives runoff from sub-watershed A. The discharge in the detained condition at design point A is 165 cubic feet per second well below the allowable discharge stated in Reference 4. The existing condition peak discharge as estimated herein is 160 cubic feet per second.

**TABLE 2:**  
**COMPARISON OF EXISTING, FUTURE AND DETAINED CONDITIONS PEAK DISCHARGES**  
**WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN**

DESIGN POINT	LOCATION	EXISTING CONDITION		FUTURE CONDITION		DETAINED CONDITION	
		Q5 (cfs)	Q100 (cfs)	Q5 (cfs)	Q100 (cfs)	Q5 (cfs)	Q100 (cfs)
A	at West Property Line	11	157	270	933	37	138
A5	at Cross Creek Drive	N/A	N/A	273	935	273	935
A6	at existing stock pond	12	142	225	723	225	723
A3	at Briargate Boulevard	N/A	N/A	89	330	89	330
C	at Cottonwood Creek	8	94	104	314	104	314
D	at Cottonwood Creek	10	107	47	162	N/A	N/A
D2 (1)	at south property line	10	103	48	158	33	151
E	at Cottonwood Creek	11	124	94	304	N/A	N/A
E2 (1)	at south property line	6	66	98	309	33	151
F	Tributary 4 at Cottonwood Creek	49	661	307	1,654	102	565
F28	Tributary 4 at Research Parkway	55	664	304	1,659	101	554
F22	Tributary 4 1,000' south of Briargate	49	570	126	850	52	245
G	at Cottonwood Creek	13	155	129	502	40	134
H-1	at Research Parkway	5	41	17	63	17	63
H-2	at Cottonwood Creek	3	36	25	96	25	96

(1) Detained design points D2 and E2 combine the discharges for existing basins E-1 and design point D2

The input and output for the HEC-1 computer model for the detained hydrologic analysis is contained within Appendix A of this report.

## HYDRAULICS

The sizing of the major drainageway conveyances, storm sewer outfall lines and roadway culverts was accomplished using the discharge data produced for the detained hydrologic condition. Presented on Figure 6 are the sizes for each of the major roadway crossings. Roadway culverts were determined using the Federal Highways Administration HY-8 Culvert Analysis program. The input and output for the culvert analyses are contained within Appendix B. Storm sewers shown on Figure 6 were determined using normal flow equations and a minimum slope of 2 percent. The major storm sewers were modeled in the HEC-1 analysis.

With the exception of the Cottonwood Creek and Tributary Four drainageways the open channels shown on Figure 6 were sized using normal depth equations. For grass-lined channels a maximum 100-year velocity of five feet per second was assumed. For channels lined with riprap a maximum 100-year design velocity of nine feet per second was applied. The spacing of grade control along open channels, including Cottonwood Creek and Tributary Four was determined using an assumption that the longitudinal slope would degrade to one-half of the existing longitudinal slope.

Presented on plan and profiles PP1 through PP6 contained within Appendix C are the proposed drainageway improvements for the segments of Tributary Four and Cottonwood Creek within the development. Grade controls would be sloping boulder or soil cement drops with a maximum drop height of six vertical feet. A typical section of a boulder sloping drop is included with the plan and profiles. The drop structure would provide for the control of the 5-year as well as the 100-year discharge through the drop. Selective riprap bank lining is proposed along Cottonwood Creek and Tributary Four. The locations proposed for bank lining are shown on the plan and profiles. A typical bank section and sloping drop has been provided for on the detail sheet PP7 as well.

Presented on the plan and profile drawings is the 100-year floodplain and profile for Cottonwood Creek and Tributary Four. The 100-year water surface was determined using the U. S. Army Corps of Engineers HEC-2 water surface profile program. The hydrology used to determine the floodplain and profile was the developed condition without detention. The 100-year velocity along Cottonwood Creek through the Wolf Ranch development ranges 4 to 10 feet per second. The 100-year velocity for Tributary Four ranges from 6 to 10 feet per second. These velocity ranges were used when determining the average riprap size needed for the selective linings.

Also presented on the plan and profiles is a proposed erosion setback for Cottonwood Creek and Tributary Four. This setback was determined using the “prudent line” methodology for erosion resistant banks conditions as outlined in Reference 8. This setback was determined in order to define the location of the encroachment limits for the Cottonwood Creek and Tributary Four corridors. This setback was determined since the banks will only be selectively lined and therefore some allowance for lateral migration of the stream channel could occur. Using the methodology outlined in Reference 8, the calculated setback ranges from 60 to 140 feet for Tributary Four. The location of the erosion setback denotes the limits of encroachment fill that would be associated with land development activities with the exception of roadway and utility crossings. The potential for vertical degradation will be limited by the drop structures. The use of the prudent line criteria is appropriate for the segments of Tributary Four and Cottonwood Creek within the property and is consistent with the Cottonwood Creek Drainage Basin Planning Study (Reference 4). The calculations associated with determining the location of the erosion setback are included within Appendix B.

### **FLOODPLAIN STATEMENT**

Floodplains for the 100-year existing condition have been delineated for Cottonwood Creek within the Colorado Springs and El Paso County Flood Insurance Study (FIS). Cottonwood Creek is the only drainageway within the Wolf Ranch development that has been studied by FEMA.

Shown on Figure 7 is the project site superimposed on the Flood Insurance Study FIRM panel for this area of El Paso County. Portions of the Wolf Creek property lie within a 100-year floodplain and floodway as depicted in the in the City of Colorado Springs and El Paso County Flood Insurance Study (FIS), prepared by the Federal Emergency Management Agency (FEMA).

### **PROPOSED FACILITIES**

#### **Detention**

The primary conclusion of this MDDP is that regional detention will be required to maintain the historic flow conditions at the development’s west and south property lines. It is proposed to construct six detention basins within the development. Three of the detention basins lie within the Tributary Four watershed. The remaining three lie within sub-watersheds A, E/D and G. Onsite detention is recommended for sub-watersheds G-5, H and J. As discussed above, the detention basins shown on Figure 6 collectively act to reduce the 100-year peak discharge to at or below historic conditions. Detention basin

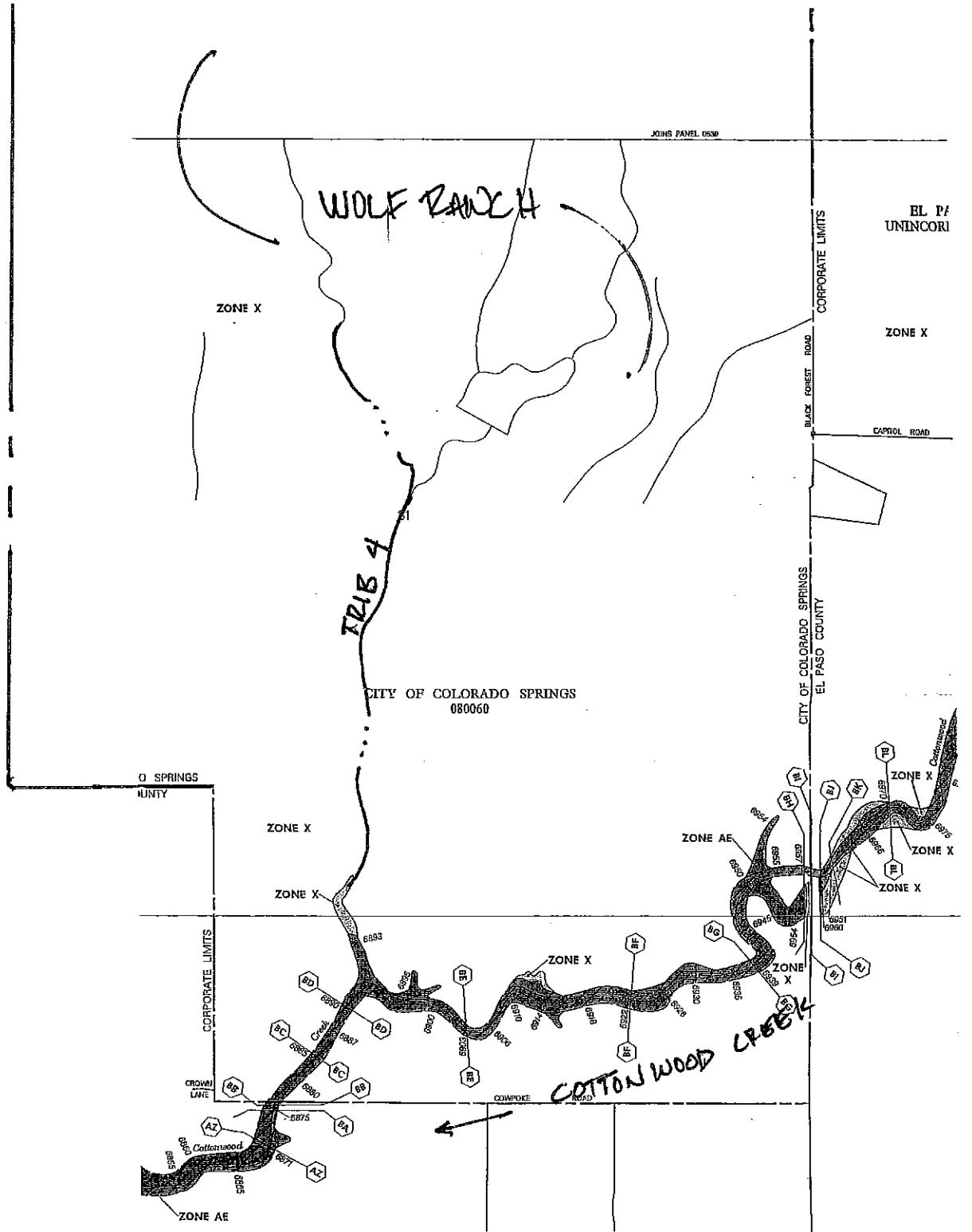


FIGURE 7  
FLOODLAIN INFORMATION

E/D has been constructed with the Westcreek II subdivision. Detention basin E/D was design to function as a wetland bottom extended duration detention basin in conformance with Volume 2 of the City's Drainage Criteria Manual. It is the intent of this MDDP to incorporate water quality storage and discharge control features for all of the detention basins except detention basin F28 that lies upstream of proposed Research Parkway embankment. The HEC-1 models incorporating these storage facilities are contained within Appendix A of this report. The storage and outflow data for each of the detention basins are presented on Figure 6. Each detention basin will be designed to be in conformance with the City/County storm drainage technical criteria. Each detention basin will be required to have an emergency spillway. Easements or tracts dedicated for access and maintenance will be established at each detention basin site through the platting process.

### **Drainageways**

The City of Colorado Springs, El Paso County Drainage Criteria Manual was used in the development of the typical sections and plans for the major drainageways within the Cross Creek Development. The City/County storm drainage criteria manual was supplemented by other criteria with more specific application. These were:

1. Urban Storm Drainage Criteria Manual, Volumes I, II, and III prepared by the Urban Drainage and Flood Control District.

The recommended channel sections for each reach of drainageway have been presented on Figure 6 at the rear of this report and on the preliminary plan and profiles of Tributary Four.

The City of Colorado Springs adopted a streamside overlay zone for many of the natural watercourses that lie within the City in 2001. This zone was established in order to restrict encroachment of fill associated with development into the natural flood zones of a particular drainageway and to promote the preservation of the natural floodplain zones that may exist. Because of the prudent line assumption that has been advanced for Cottonwood Creek, Cottonwood Creek was exempted from the streamside overlay regulations and criteria. Tributary Four does not lie within a designated streamside overlay zone.

### Drop and Check Structures

Drop structures have been sited along the Cottonwood Creek, and Tributary Four drainageways in order to maintain the channel invert at a stable gradient or to reduce the slope of the channel gradient so that lower velocities result along the drainageways. When determining the location of drop structures a degraded slope of no more than one-half of the existing slope was assumed. In the case of Cottonwood Creek the design slope ranged from 1.5 percent to 2 percent. In the case of Tributary Four the design slope applied was 1.25 percent. This assumption allows for the design to accommodate future channel degradation without modifying the existing channel section. The drops are designed to allow for a maximum drop of six feet and will have a sloping face of four to one.

Check structures are needed along the invert of some of the natural and smaller improved drainageways shown on Figure 6. The check will allow for a three-foot degradation of the invert prior to undermining a given check. These checks will be constructed of either riprap or concrete. A typical check structure detail has been presented on detail sheet PP7. The interval between checks is shown for each drainageway on Figure 6.

### Roadway Crossings

Summarized on Figure 6 are the size, type and location of roadway crossings along the major drainageways. The location of future arterials and collector streets was obtained from the development plan for Wolf Ranch. A 100-year headwater to depth ratio of 1.1 was assumed in the sizing of the major roadway culverts.

The existing crossings at Cowpoke Road and Black Forest Road are proposed to remain as they have sufficient capacity to pass the 100-year discharge without overtopping. These crossings are maintained by the El Paso County Department of Transportation. El Paso County recently repaired the wingwalls on the bridge at Black Forest Road and installed some additional riprap outlet protection. The bridge at Cowpoke Road will be removed when Tutt Boulevard is extended across Cottonwood Creek and Cowpoke Road is realigned.

As part of the annexation agreement for the Wolf Ranch property the Black Forest Road bridge will be required to be rebuilt by the developer of Wolf Ranch when traffic levels on Black Forest Road warrant the widening of the roadway. The hydraulic capacity of the new structure when built should be able to convey the discharges estimated in this MDDP.

Several culverts exist under Old Ranch Road at this time. These culverts range in size from 18-inches to 48-inches and are all corrugated metal pipe. The culverts have

*to be removed when  
Tutt is realigned*

*to be rebuilt by  
Wolf Ranch Heights  
per their  
annexation  
agreement*



adequate capacity to convey the existing five-year flow under the roadway without overtopping. Some of the culverts have a 100-year capacity. It was assumed in the hydrologic analysis that the areas north of Old Ranch Road will not produce runoff greater than the existing condition rates calculated in this report. The majority of the area north of Old Ranch Road is developed. If a denser land use takes place in the future, stormwater detention would be required so that an increase the rates of runoff to the Wolf Ranch property does not occur. There is however no intention to replace the existing crossing under Old Ranch Road as part of the development of the Wolf Ranch property.

### **Trails**

Trails for access to the detention basins and major drainageways need to be incorporated into the design of the improvements. For the Wolf Ranch a multi-purpose trail is proposed that is aligned along the Tributary Four. This trail will have to be accommodated at each of the roadway crossings by either an at grade or sub-grade crossing. Where practical, this trail can accommodate maintenance access to the channel and the detention basins. If the trail encroaches into a 100-year floodplain, the trail design should take into account hydraulic considerations, utilities in the area and access to dedicated parks and roadway crossings. Maintenance access to the drainageway and to existing utilities within the drainageway corridor can offer a multiple use aspect to a trail project.

### **Maintenance**

Maintenance of drainageway facilities is essential in preventing long term degradation of the drainageway and overbank areas. Along the drainageway, clearing of debris and dead vegetation should be considered within the low flow area of the creek and its tributaries. On the overbanks, limited maintenance of the existing vegetative cover is recommended. Yearly clearing of trash and debris at roadway crossings is also recommended to ensure the design capacity of the crossing, and to enhance the crossings for trail users if a trail exists. Caution should be taken when clearing culverts of sediment so as not to leave the dredged soil within the channel or overbank area. This disturbs the native vegetation and creates a potential water quality concern if the dredged material is subsequently washed into the drainageway by natural erosion. For those reaches of drainageways that are designated for selective lining and the floodplain preservation, maintenance activities should be carried out while minimizing the disturbances to native vegetation.

The proposed detention basins will also require annual maintenance. The outlet structures will need to be cleared and the entry channel and forebays cleared of debris or silt. For those detention basin where water quality storage has been incorporated into the design, the clearing of sediment from the water quality pools will need to be carried out on a yearly basis as well, minimum.

At the present time a metropolitan district is in existence that will serve the Wolf Ranch property. The metropolitan district will be responsible for the construction and maintenance of various public facilities within the Wolf Ranch property including but not necessarily limited to common open spaces and landscaped medians, parks, roadways, major drainageways, detention basin and community centers. The exact scope of the maintenance responsibilities of the metropolitan district is still subject to refinement. Agreements between the City of Colorado Springs and the metropolitan district may need to be developed that will define the exact maintenance responsibility for the public infrastructure within Wolf Ranch. At this time it is envisioned that the major drainageway facilities shown in this MDDP along Tributary Four and drainageway A, as well as the detention basins would be subject to maintenance by the metropolitan district. If the portion of the Cottonwood Creek that lies within Wolf Ranch is closed to fee assessment and reimbursement of facilities (see discussion below), it is envisioned that the district would take over maintenance responsibilities of the major drainageway facilities and detention basin shown in this MDDP.

Has this been refined?

You will need to update DBPS & go to Drainage Board for fee adjustment

#### **Right-of-Way**

It will be required for the main drainageways that pass through the development to be located within dedicated tracts, easements or right-of-ways. Access to these tracts or easement will be granted to the metropolitan district so that routine maintenance activities can be conducted. In the case of right-of-ways and tracts, these lands would be dedicated to the metropolitan district. For those segments of the drainageway where floodplain preservation is the recommended plan, a combination of open space dedication (such as park-land and greenbelts), in combination with a more narrow dedicated maintenance right-of-way along the low flow area of the drainageway should be obtained through the land development process. Land dedication will be required for the detention basins. The dedication of easements and right-of-way for the drainageways and detention basins would be accomplished at the time of development planning and/or platting of the parcels that lie adjacent to or upstream of the stormwater facility.

### **DRAINAGE BASIN FEES**

It is the intent of the developer to request that the developable land within the Wolf Ranch property be exempted from the assessment of drainage fees associated with the Cottonwood Creek basin and in essence "close" the basin. As such the developable acreage subject to fee assessment that has been is estimated at 1,484 acres would be removed from the Cottonwood basin. Additionally, the drainageway improvements identified in the DBPS for the portion of Cottonwood Creek within the property and for Tributary Four would not be subject to reimbursement. The estimated cost for these facilities as presented in the DBPS was approximately \$400,000. The land associated with the erosion control setback will also not be subject to reimbursement through the Cottonwood Creek basin fee system.

A formal presentation to the Drainage Board will be conducted wherein the recalculation of the basins fees will be discussed and revised accordingly based upon the recommendation of the Drainage Board. It is understood that the City will not provide a final approval of the MDDP until the revised fees for the basin have been reestablished. Should the closing of the basin be approved by the Drainage Board, the Cottonwood Creek DBPS would have to be updated to reflect the changes to the Cottonwood Creek basin fees and the elimination of major drainageway facilities that will be constructed within the Wolf Ranch property.

What is the latest?

**APPENDIX A**  
**HYDROLOGIC CALCULATIONS**

WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN  
 WEIGHTED CN-VALUES  
 FUTURE DEVELOPMENT CONDITIONS

A-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
A-1	38.2	61	0	0	0	38.2	0	0	0	61.0
A-3	96.0	73	0	0	0	96	0	0	0	73.0
A-4	55.1	79	73	0	0	36.9	18.2	0	0	77.0
A-5	71.3	79	61	75	0	39.2	28.5	3.6	0	71.6
A-6	23.7	79	0	0	0	23.7	0	0	0	79.0
A-7	32.0	61	79	0	0	2.7	29.3	0	0	77.5
A-8	50.6	85	88	61	0	15	30	5.6	0	84.1
A-9	43.1	79	75	0	0	32.3	10.3	0	0	77.1
A-10	5.5	92	61	0	0	3.3	2.2	0	0	79.6
A-11	51.8	61	73	79	0	3	14.1	34.7	0	76.3

Wolf Ranch Master Development Drainage Plan  
Time of Concentration  
A-basins

Basin	Slope			Length			Run Coef. (5-year)	Velocity			T <sub>c</sub>			Basin	
	O'land	Chan. 1	Chan. 2	O'land	Chan. 1	Chan. 2		O'land	Chan. 1	Chan. 2	O'land	Chan. 1	Chan. 2		
A-1	9.0 %	6.1 %	0 %	1,000 lf	1,650 lf	0 lf	0.20	8.0 ft/sec	8.0 ft/sec	0.0 ft/sec	1536 sec.	206 sec.	0 sec.	29.0 min.	A-1
A-3	6.0 %	2.1 %	0 %	300 lf	3,200 lf	0 lf	0.45	8.0 ft/sec	5.0 ft/sec	0.0 ft/sec	696 sec.	640 sec.	0 sec.	22.3 min.	A-3
A-4	2.0 %	4.1 %	3 %	300 lf	850 lf	1,650 lf	0.50	2.0 ft/sec	8.0 ft/sec	8.0 ft/sec	926 sec.	106 sec.	206 sec.	20.6 min.	A-4
A-5	2.0 %	3.1 %	1 %	300 lf	2,050 lf	1,120 lf	0.60	2.0 ft/sec	8.0 ft/sec	5.0 ft/sec	771 sec.	256 sec.	224 sec.	20.9 min.	A-5
A-6	2.0 %	1.6 %	0 %	300 lf	1,550 lf	0 lf	0.50	2.0 ft/sec	5.0 ft/sec	5.0 ft/sec	926 sec.	310 sec.	0 sec.	20.6 min.	A-6
A-7	2.0 %	2.0 %	0 %	100 lf	2,000 lf	0 lf	0.50	2.0 ft/sec	4.0 ft/sec	10.0 ft/sec	534 sec.	500 sec.	0 sec.	17.2 min.	A-7
A-8	3.3 %	2.3 %	0 %	300 lf	2,420 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	914 sec.	605 sec.	0 sec.	25.3 min.	A-8
A-9	2.0 %	2.0 %	0 %	300 lf	2,300 lf	0 lf	0.45	2.0 ft/sec	4.0 ft/sec	10.0 ft/sec	1003 sec.	575 sec.	0 sec.	26.3 min.	A-9
A-10	5.0 %	0.0 %	0 %	550 lf	0 lf	0 lf	0.20	5.0 ft/sec	4.0 ft/sec	10.0 ft/sec	1386 sec.	0 sec.	0 sec.	23.1 min.	A-10
A-11	4.7 %	3.4 %	0 %	300 lf	1,252 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	813 sec.	313 sec.	0 sec.	18.8 min.	A-11

Equations:

$$\text{Time of Concentration (Overland)} = 1.87(1.1 - C_x)L^{0.5} S^{-0.333}$$

$C_x$  = Runoff coefficient for five-year flow

L = Length of overland flow in feet

S = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{0.5 \log S + 0.2})$$

S = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_n^{2/3} S^{1/2}$$

Slope (S) = Slope of the channel

n = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN  
 WEIGHTED CN-VALUES  
 FUTURE DEVELOPMENT CONDITIONS

B-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
B-1	25.6	92	85	73	0	25.6	0	0	0	92.0

Wolf Ranch Master Development Drainage Plan  
Time of Concentration  
B-basins

Basin	Slope			Length			Run Coef. (5-year)	Velocity			T <sub>c</sub>			Basin	
	Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		T <sub>c</sub>
B-1	2.0 %	2.0 %	0 %	100 lf	1,850 lf	0 lf	0.90	2.0 ft/sec	4.0 ft/sec	0.0 ft/sec	178 sec.	463 sec.	0 sec.	10.7 min.	B-1

Equations:

$$\text{Time of Concentration (Overland)} = 1.87(1.1 - C_s)L^{0.5} S^{-0.333}$$

$C_s$  = Runoff coefficient for five-year flow

$L$  = Length of overland flow in feet

$S$  = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{0.5\log S + 0.3})$$

$S$  = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_m^{2/3} S^{1/2}$$

Slope ( $S$ ) = Slope of the channel

$n$  = Manning's number

$R_m$  = Hydraulic Radius (Reynold's Number)



WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN  
 WEIGHTED CN-VALUES  
 FUTURE DEVELOPMENT CONDITIONS

C-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
C-1	29.4	79	0	0	0	29.4	0	0	0	79.0
C-2	70.4	79	92	61	0	35.0	21	14.4	0	79.2
C-3	35.2	79	0	0	0	35.2	0	0	0	79.0

Wolf Ranch Master Development Drainage Plan  
Time of Concentration  
C-basins

Basin	Slope			Length			Rin Coef. (5-year)	Velocity			T <sub>c</sub>			Basin	
	Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		T <sub>c</sub>
C-1	2.0%	3.0%	0%	100 lf	1,950 lf	0 lf	0.60	2.0 ft/sec	4.0 ft/sec	0.0 ft/sec	445 sec.	488 sec.	0 sec.	15.5 min.	C-1
C-2	3.0%	4.0%	0%	100 lf	650 lf	3,450 lf	0.55	2.0 ft/sec	4.0 ft/sec	6.0 ft/sec	428 sec.	163 sec.	0 sec.	9.8 min.	C-2
C-3	2.5%	2.0%	0%	100 lf	2,650 lf	0 lf	0.55	2.0 ft/sec	4.0 ft/sec	0.0 ft/sec	455 sec.	663 sec.	0 sec.	18.6 min.	C-3

Equations:

Time of Concentration (Overland) =  $1.87(1.1 - C_s)L^{0.5} S^{-0.333}$

C<sub>s</sub> = Runoff coefficient for five-year flow

L = Length of overland flow in feet

S = Slope of flow path in percent

Velocity (Road) =  $10(10^{(0.51 \log S + 0.3)})$

S = Slope of flow path in percent

Velocity (Channel) =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN  
 WEIGHTED CN-VALUES  
 FUTURE DEVELOPMENT CONDITIONS

D-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
D-1	39.4	79	61	0	0	36.5	2.9	0	0	77.7
D-2	23.0	73	0	0	0	23.0	0	0	0	73.0
D-3	15.4	61	0	0	0	15.4	0	0	0	61.0

Wolf Ranch Master Development Drainage Plan  
Time of Concentration  
D-basins

Basin	Slope			Length			Run Coef. (5-year)	Velocity			T <sub>c</sub>			Basin	
	O'land	Chan. 1	Chan. 2	O'land	Chan. 1	Chan. 2		O'land	Chan. 1	Chan. 2	O'land	Chan. 1	Chan. 2		
D-1	2.0 %	2.0 %	0 %	100 lf	2,350 lf	0 lf	0.55	2.0 ft/sec	4.0 ft/sec	0.0 ft/sec	490 sec.	588 sec.	0 sec.	18.0 min.	D-1
D-2	2.0 %	3.0 %	0 %	100 lf	1,350 lf	0 lf	0.55	2.0 ft/sec	6.0 ft/sec	0.0 ft/sec	490 sec.	225 sec.	0 sec.	11.9 min.	D-2
D-3	4.0 %	2.6 %	0 %	800 lf	1,920 lf	0 lf	0.20	7.0 ft/sec	4.0 ft/sec	0.0 ft/sec	1800 sec.	480 sec.	0 sec.	38.0 min.	D-3

Equations:

$$\text{Time of Concentration (Overland)} = 1.87(1.1 - C_p)L^{0.5} S^{-0.583}$$

$C_p$  = Runoff coefficient for five-year flow

L = Length of overland flow in feet

S = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{(0.5 \log S + 0.3)})$$

S = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_h^{2/3} S^{1/2}$$

Slope (S) = Slope of the channel

n = Manning's number

$R_h$  = Hydraulic Radius (Reynold's Number)

WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN  
 WEIGHTED CN-VALUES  
 FUTURE DEVELOPMENT CONDITIONS

E-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
E-1	25.8	79	0	0	0	25.8	0	0	0	79.0
E-2	33.3	73	0	0	0	33.3	0	0	0	73.0
E-3	63.7	61	0	0	0	63.7	0	0	0	61.0
E-4	27.1	73	0	0	0	27.1	0	0	0	73.0
E-5	25.6	79	0	0	0	25.6	0	0	0	79.0
E-6	30.6	79	0	0	0	30.6	0	0	0	79.0

Wolf Ranch Master Development Drainage Plan  
Time of Concentration  
E-basins

Basin	Slope			Length			Run Coef.		Velocity			T <sub>c</sub>			Basin
	O'land	Chan. 1	Chan. 2	O'land	Chan. 1	Chan. 2	(5-year)	O'land	Chan. 1	Chan. 2	O'land	Chan. 1	Chan. 2	T <sub>c</sub>	
E-1	2.0 %	2.0 %	0 %	100 lf	1,700 lf	0 lf	0.60	2.0 ft/sec	4.0 ft/sec	0.0 ft/sec	445 sec.	425 sec.	0 sec.	14.5 min.	E-1
E-2	3.0 %	3.0 %	0 %	100 lf	2,250 lf	0 lf	0.55	2.0 ft/sec	6.0 ft/sec	0.0 ft/sec	428 sec.	375 sec.	0 sec.	13.4 min.	E-2
E-3	3.0 %	2.0 %	0 %	700 lf	3,150 lf	0 lf	0.25	2.0 ft/sec	5.0 ft/sec	0.0 ft/sec	1750 sec.	630 sec.	0 sec.	39.7 min.	E-3
E-4	2.0 %	2.0 %	0 %	100 lf	2,150 lf	0 lf	0.55	2.0 ft/sec	6.0 ft/sec	0.0 ft/sec	490 sec.	358 sec.	0 sec.	14.1 min.	E-4
E-5	3.0 %	3.0 %	0 %	100 lf	1,700 lf	0 lf	0.55	2.0 ft/sec	6.0 ft/sec	0.0 ft/sec	428 sec.	283 sec.	0 sec.	11.9 min.	E-5
E-6	2.0 %	2.0 %	0 %	100 lf	2,200 lf	0 lf	0.50	2.0 ft/sec	4.0 ft/sec	0.0 ft/sec	534 sec.	550 sec.	0 sec.	18.1 min.	E-6

Equations:

$$\text{Time of Concentration (Overland)} = 1.87(1.1 - C_s)L^{0.5} S^{-0.333}$$

$C_s$  = Runoff coefficient for five-year flow

$L$  = Length of overland flow in feet

$S$  = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{(1.5 \log S + 0.3)})$$

$S$  = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_n^{2/3} S^{1/2}$$

Slope ( $S$ ) = Slope of the channel

$n$  = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN  
 WEIGHTED CN-VALUES  
 FUTURE DEVELOPMENT CONDITIONS

F-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
F-1 to F-7										data taken from prior program compilations
F-8	57.8	70	73	0	0	28.9	28.9	0	0	71.5 ✓
F-9	27.5	70	0	0	0	27.5	0	0	0	70.0 ✓
F-10	11.5	61	75	0	0	6.6	4.9	0	0	67.0 ✓
F-11	29.4	61	70	0	0	5.9	23.5	0	0	68.2 ✓
F-12	37.2	61	70	0	0	3.1	34.1	0	0	69.3 ✓
F-13	9	61	0	0	0	9.0	0	0	0	61.0 ✓
F-14	82.6	61	70	73	0	0.0	0	82.6	0	73.0 ✓
F-15	13.4	61	70	73	0	2.7	6.7	4	0	69.1 ✓
F-16	17.3	70	73	0	0	0.9	16.4	0	0	72.8 ✓
F-17	24.9	61	70	73	0	23.1	0	1.2	0	60.1 ✓
F-18	63	61	70	79	0	9.5	22.1	31.4	0	73.1 ✓

F-19	65.3	61	73	79	0	20.9	0	44.4	0	73.2
F-22	41	61	92	0	0	36.9	4.1	0	0	64.1
F-23	19.8	0	73	0	0	0.0	19.8	0	0	73.0
F-24	57	79	0	0	0	57.0	0	0	0	79.0
F-25	57	61	73	79	0	6.0	29	22	0	74.1
F-26	34	0	79	0	0	0.0	34	0	0	79.0
F-27	129	61	73	92	0	26.0	65	38	0	76.2
F-28	24	61	73	79	0	13.0	5	6	0	68.0
F-29	16	61	79	0	0	8.0	8	0	0	70.0
F-30	14	79	73	0	0	11.0	3	0	0	77.7
F-31	60	61	73	79	65	33.0	6	18	3	67.8



Wolf Ranch Master Development Drainage Plan  
Time of Concentration  
F-basins

Basin	Slope			Length			Run Coef. (5-year)	Velocity			T			Basin	
	O'land	Chan. 1	Chan. 2	O'land	Chan. 1	Chan. 2		O'land	Chan. 1	Chan. 2	O'land	Chan. 1	Chan. 2		
F-8	6.7 %	4.4 %	0 %	298 lf	2,323 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	720 sec.	581 sec.	0 sec.	21.7 min.	F-8
F-9	6.3 %	4.0 %	0 %	300 lf	927 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	737 sec.	232 sec.	0 sec.	16.1 min.	F-9
F-10	6.7 %	5.0 %	0 %	300 lf	600 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	722 sec.	150 sec.	0 sec.	14.5 min.	F-10
F-11	5.7 %	4.1 %	0 %	300 lf	918 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	762 sec.	230 sec.	0 sec.	16.5 min.	F-11
F-12	4.0 %	3.3 %	0 %	300 lf	1,290 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	857 sec.	323 sec.	0 sec.	19.7 min.	F-12
F-13	7.3 %	5.2 %	0 %	300 lf	498 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	702 sec.	125 sec.	0 sec.	13.8 min.	F-13
F-14	3.7 %	3.1 %	3 %	300 lf	1,081 lf	1,730 lf	0.40	4.0 ft/sec	4.0 ft/sec	8.0 ft/sec	880 sec.	270 sec.	216 sec.	22.8 min.	F-14
F-15	5.8 %	3.7 %	0 %	300 lf	931 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	758 sec.	233 sec.	0 sec.	16.5 min.	F-15
F-16	2.6 %	2.6 %	0 %	300 lf	1,085 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	990 sec.	271 sec.	0 sec.	21.0 min.	F-16
F-17	3.7 %	3.4 %	3 %	300 lf	945 lf	990 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	880 sec.	236 sec.	124 sec.	20.7 min.	F-17
F-18	3.3 %	3.5 %	0 %	300 lf	1,465 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	914 sec.	366 sec.	0 sec.	21.3 min.	F-18
F-19	4.5 %	5.9 %	4 %	300 lf	634 lf	1,155 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	824 sec.	159 sec.	144 sec.	18.8 min.	F-19
F-22	4.1 %	3.5 %	0 %	300 lf	1,705 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	850 sec.	426 sec.	0 sec.	21.3 min.	F-22
F-23	4.0 %	4.8 %	2 %	300 lf	414 lf	890 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	857 sec.	104 sec.	111 sec.	17.9 min.	F-23
F-24	4.0 %	2.1 %	0 %	300 lf	2,765 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	857 sec.	691 sec.	0 sec.	25.8 min.	F-24
F-25	2.0 %	2.8 %	0 %	300 lf	2,270 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	1080 sec.	568 sec.	0 sec.	27.5 min.	F-25
F-26	4.7 %	2.7 %	0 %	300 lf	1,250 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	813 sec.	313 sec.	0 sec.	18.8 min.	F-26
F-27	2.7 %	3.8 %	2 %	300 lf	1,650 lf	4,150 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	977 sec.	413 sec.	519 sec.	31.8 min.	F-27
F-28	3.3 %	4.7 %	0 %	300 lf	1,950 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	914 sec.	488 sec.	0 sec.	23.4 min.	F-28
F-29	2.7 %	4.3 %	0 %	300 lf	655 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	977 sec.	164 sec.	0.0 ft/sec	19.0 min.	F-29
F-30	3.3 %	4.1 %	0 %	300 lf	680 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	914 sec.	170 sec.	0.0 ft/sec	18.1 min.	F-30
F-31	3.3 %	5.0 %	3 %	300 lf	1,600 lf	1,110 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	914 sec.	400 sec.	139 sec.	24.2 min.	F-31

Equations:

$$\text{Time of Concentration (Overland)} = 1.87(1.1 - C_c)L^{0.5} S^{-0.333}$$

$C_c$  = Runoff coefficient for five-year flow

L = Length of overland flow in feet

S = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{(0.5 \log S + 0.3)})$$

S = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_n^{2/3} S^{1/2}$$

Slope (S) = Slope of the channel

n = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

Wolf Ranch Master Development Drainage Plan  
Time of Concentration  
F-basins

Basin	Slope			Length			Run Coef. (S-year)	Velocity			T <sub>c</sub>			Basin	
	Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		
F-8	6.7 %	4.4 %	0 %	298 lf	2,323 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	720 sec.	581 sec.	0 sec.	21.7 min.	F-8
F-9	6.3 %	4.0 %	0 %	300 lf	927 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	737 sec.	232 sec.	0 sec.	16.1 min.	F-9
F-10	6.7 %	5.0 %	0 %	300 lf	600 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	722 sec.	150 sec.	0 sec.	14.5 min.	F-10
F-11	5.7 %	4.1 %	0 %	300 lf	918 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	762 sec.	230 sec.	0 sec.	16.5 min.	F-11
F-12	4.0 %	3.3 %	0 %	300 lf	1,290 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	857 sec.	323 sec.	0 sec.	19.7 min.	F-12
F-13	7.3 %	5.2 %	0 %	300 lf	498 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	702 sec.	125 sec.	0 sec.	13.8 min.	F-13
F-14	3.7 %	3.1 %	3 %	300 lf	1,081 lf	1,730 lf	0.40	4.0 ft/sec	4.0 ft/sec	8.0 ft/sec	880 sec.	270 sec.	216 sec.	22.8 min.	F-14
F-15	5.8 %	3.7 %	0 %	300 lf	931 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	758 sec.	233 sec.	0 sec.	16.5 min.	F-15
F-16	2.6 %	2.6 %	0 %	300 lf	1,085 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	990 sec.	271 sec.	0 sec.	21.0 min.	F-16
F-17	3.7 %	3.4 %	3 %	300 lf	945 lf	990 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	880 sec.	236 sec.	124 sec.	20.7 min.	F-17
F-18	3.3 %	3.5 %	0 %	300 lf	1,465 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	914 sec.	366 sec.	0 sec.	21.3 min.	F-18
F-19	4.5 %	5.9 %	4 %	300 lf	634 lf	1,155 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	824 sec.	159 sec.	144 sec.	18.8 min.	F-19
F-21	3.3 %	2.3 %	0 %	300 lf	2,420 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	914 sec.	605 sec.	0 sec.	25.3 min.	F-21
F-22	4.1 %	3.5 %	0 %	300 lf	1,705 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	850 sec.	426 sec.	0 sec.	21.3 min.	F-22
F-23	4.0 %	4.8 %	2 %	300 lf	414 lf	890 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	857 sec.	104 sec.	111 sec.	17.9 min.	F-23
F-24	4.0 %	2.1 %	0 %	300 lf	2,765 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	857 sec.	691 sec.	0 sec.	25.8 min.	F-24
F-25	2.0 %	2.8 %	0 %	300 lf	2,270 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	1080 sec.	568 sec.	0 sec.	27.5 min.	F-25
F-26	4.7 %	2.7 %	0 %	300 lf	1,250 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	813 sec.	313 sec.	0 sec.	18.8 min.	F-26
F-27	2.7 %	3.8 %	2 %	300 lf	1,650 lf	4,150 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	977 sec.	413 sec.	519 sec.	31.8 min.	F-27
F-28	3.3 %	4.7 %	0 %	300 lf	1,950 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	914 sec.	488 sec.	0 sec.	23.4 min.	F-28
F-29	2.7 %	4.3 %	0 %	300 lf	655 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	977 sec.	164 sec.	0.0 ft/sec	19.0 min.	F-29
F-30	3.3 %	4.1 %	0 %	300 lf	680 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	914 sec.	170 sec.	0.0 ft/sec	18.1 min.	F-30
F-31	3.3 %	5.0 %	3 %	300 lf	1,600 lf	1,110 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	914 sec.	400 sec.	139 sec.	24.2 min.	F-31

Equations:

$$\text{Time of Concentration (Overland)} = 1.87(1.1 - C_p)L^{0.5} S^{-0.333}$$

$C_p$  = Runoff coefficient for five-year flow

$L$  = Length of overland flow in feet

$S$  = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{(0.5 \log S + 0.3)})$$

$S$  = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_n^{2/3} S^{1/2}$$

Slope ( $S$ ) = Slope of the channel

$n$  = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN  
 WEIGHTED CN-VALUES  
 FUTURE DEVELOPMENT CONDITIONS

G-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
G-1										data taken from prior program compilations
G-2	22.4	73	0	0	0	22.4	0	0	0	73.0
G-3	113.3	73	0	0	0	113.3	0	0	0	73.0
G-5	43.5	80	79	0	0	33.0	10.5	0	0	79.8

Wolf Ranch Master Development Drainage Plan  
Time of Concentration  
G-basins

Basin	Slope			Length			Run. Coef. (5-year)	Velocity			T <sub>c</sub>			Basin	
	Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		
G-2	3.5 %	2.9 %	0 %	284 lf	1,796 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	872 sec.	449 sec.	0 sec.	22.0 min.	G-2
G-3	3.0 %	2.6 %	0 %	263 lf	3,376 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	883 sec.	844 sec.	0 sec.	28.8 min.	G-3
G-5	2.7 %	4.1 %	0 %	300 lf	1,900 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	977 sec.	475 sec.	0 sec.	24.2 min.	G-5

Equations:

$$\text{Time of Concentration (Overland)} = 1.87(1.1 - C_s)L^{0.5} S^{-0.333}$$

$C_s$  = Runoff coefficient for five-year flow

$L$  = Length of overland flow in feet

$S$  = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{0.5 \log S + 0.3})$$

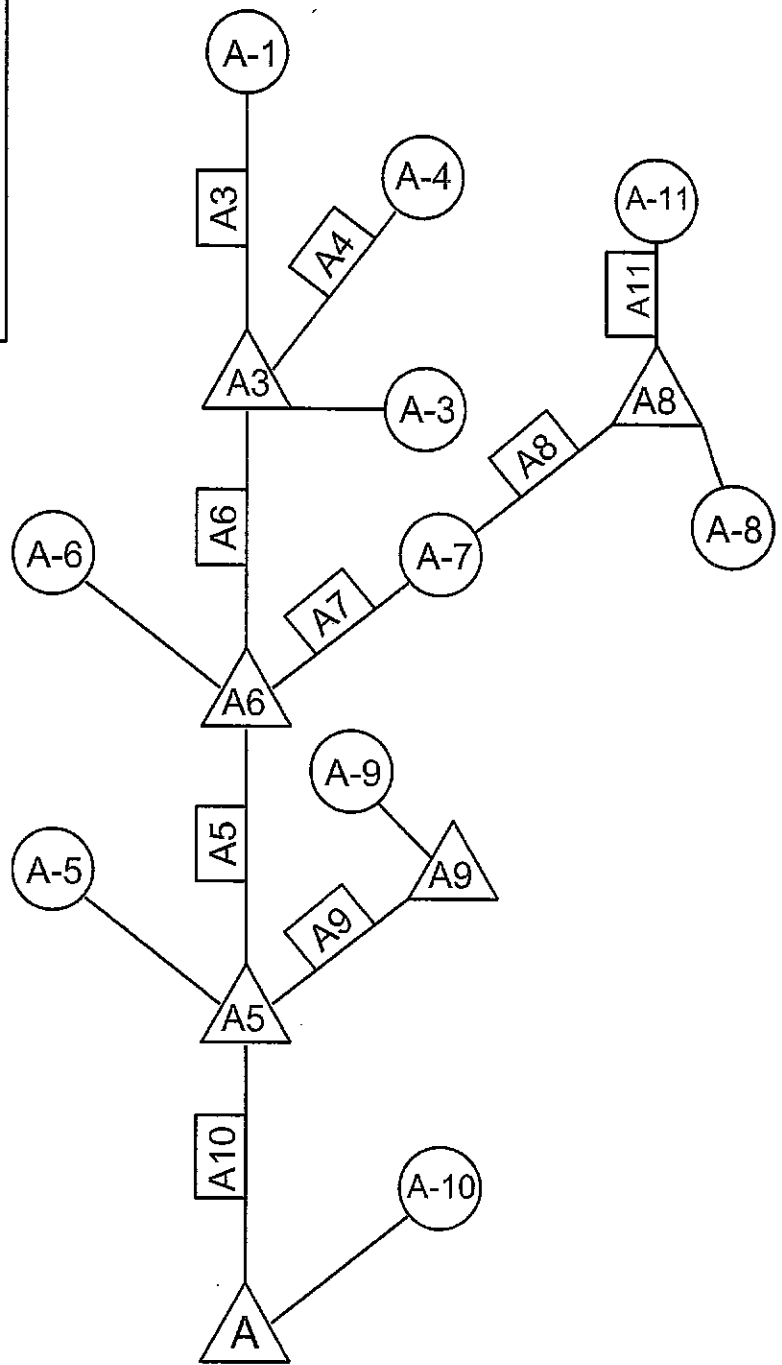
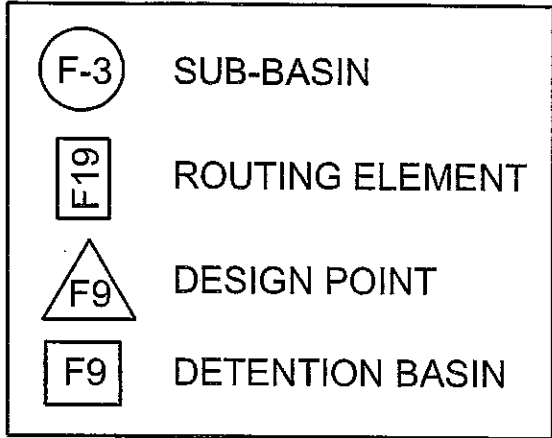
$S$  = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_n^{2/3} S^{1/2}$$

Slope ( $S$ ) = Slope of the channel

$n$  = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)



HEC1 FLOW SCHEMATIC  
DEVELOPED CONDITION 'A' BASINS

Kiowa Engineering Corporation

1604 South 21st Street  
 Colorado Springs, Colorado  
 80904-4208  
 (719) 630-7342

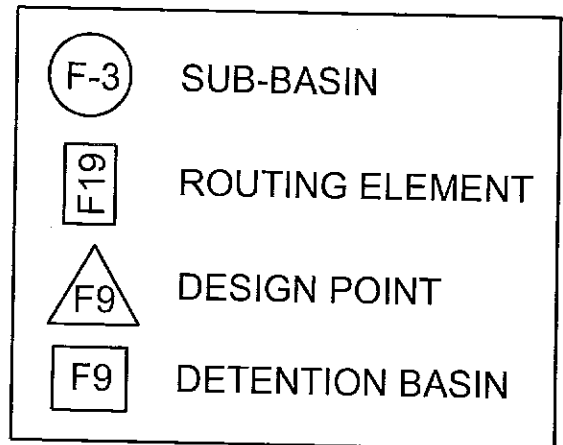
WOLF RANCH  
 HYDROLOGIC MODEL SCHEMATIC  
 COLORADO SPRINGS, COLORADO

FIGURE A

PROJECT NO.: 03094  
 DATE: 01/29/04  
 DESIGN: RNW  
 REVISIONS:



HEC1 FLOW SCHEMATIC  
DEVELOPED CONDITION 'B' BASINS



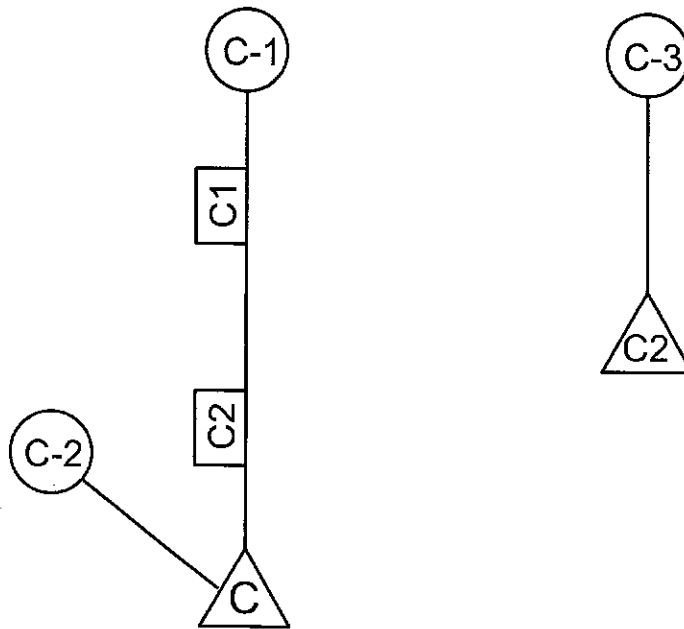
Kiowa Engineering Corporation

1604 South 21st Street  
Colorado Springs, Colorado  
80904-4208  
(719) 630-7342

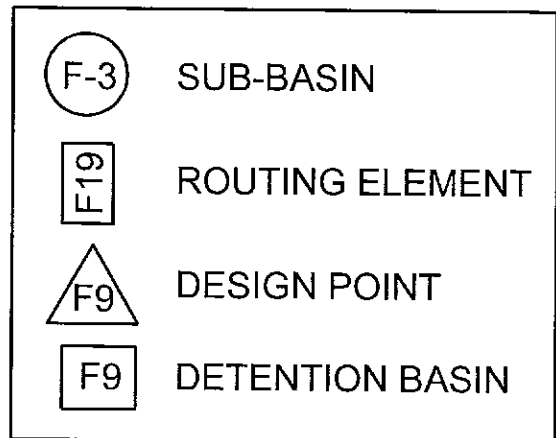
WOLF RANCH  
HYDROLOGIC MODEL SCHEMATIC  
COLORADO SPRINGS, COLORADO

FIGURE B

PROJECT NO.: 03094  
DATE: 01/29/04  
DESIGN: RNW  
REVISIONS:



HEC1 FLOW SCHEMATIC  
DEVELOPED CONDITION 'C' BASINS



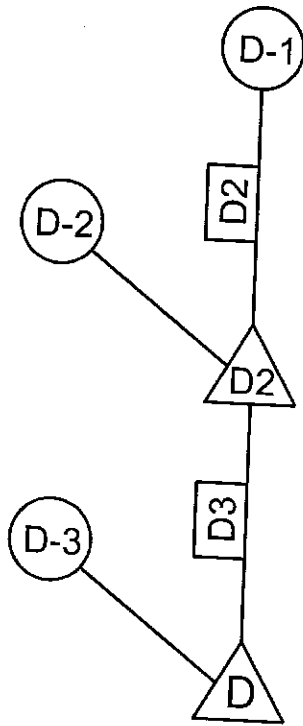
Kiowa Engineering Corporation

1604 South 21st Street  
 Colorado Springs, Colorado  
 80904-4208  
 (719) 630-7342

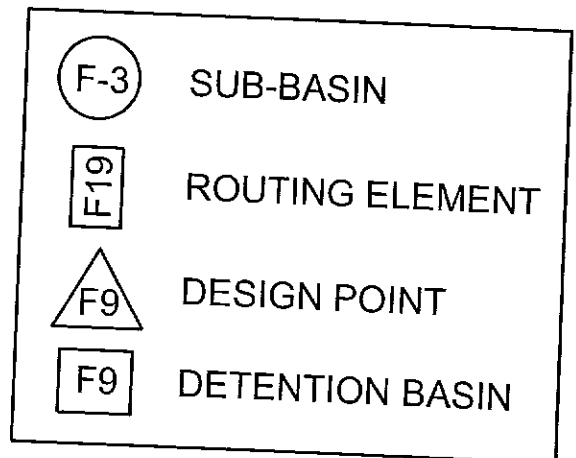
WOLF RANCH  
 HYDROLOGIC MODEL SCHEMATIC  
 COLORADO SPRINGS, COLORADO

FIGURE C

PROJECT NO.: 03094  
 DATE: 01/29/04  
 DESIGN: RNW  
 REVISIONS:



HEC1 FLOW SCHEMATIC  
DEVELOPED CONDITION 'D' BASINS



Kiowa Engineering Corporation

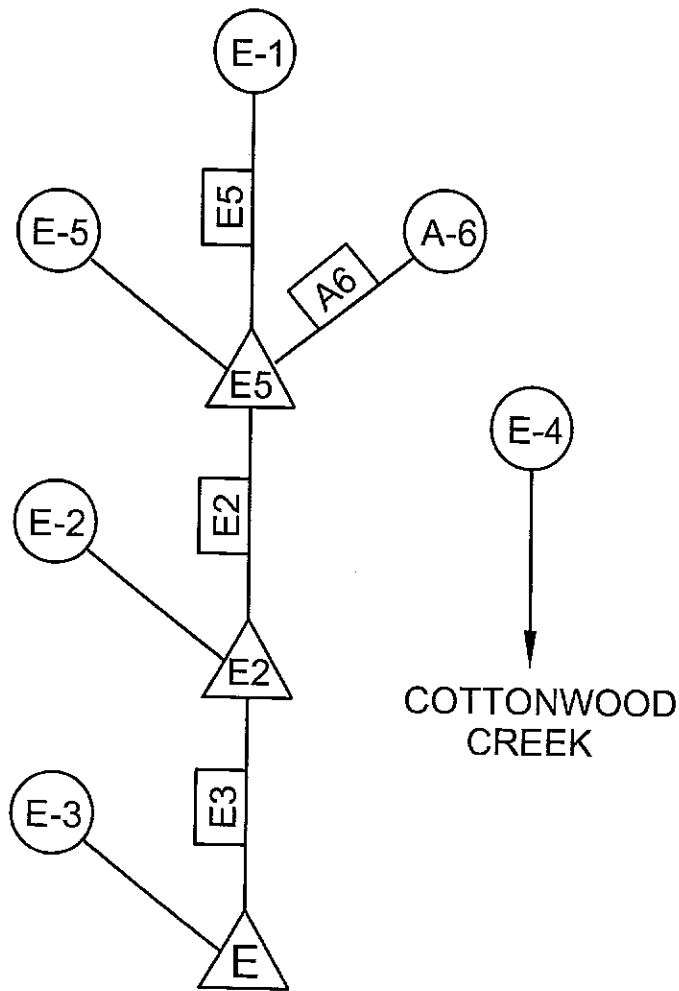
1604 South 21st Street  
 Colorado Springs, Colorado  
 80904-4208  
 (719) 630-7342

WOLF RANCH  
 HYDROLOGIC MODEL SCHEMATIC  
 COLORADO SPRINGS, COLORADO

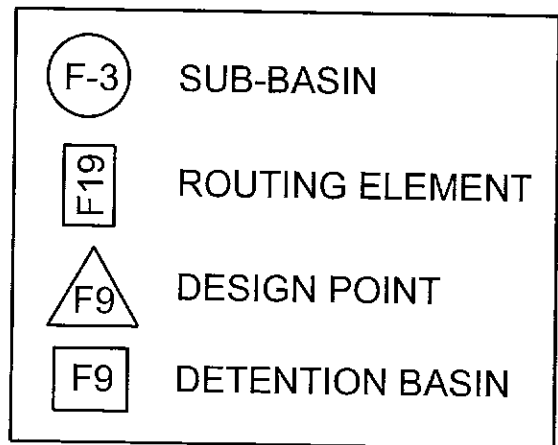
FIGURE D

PROJECT NO.: 03094  
 DATE: 01/29/04  
 DESIGN: RNW  
 REVISIONS:





HEC1 FLOW SCHEMATIC  
DEVELOPED CONDITION 'E' BASINS



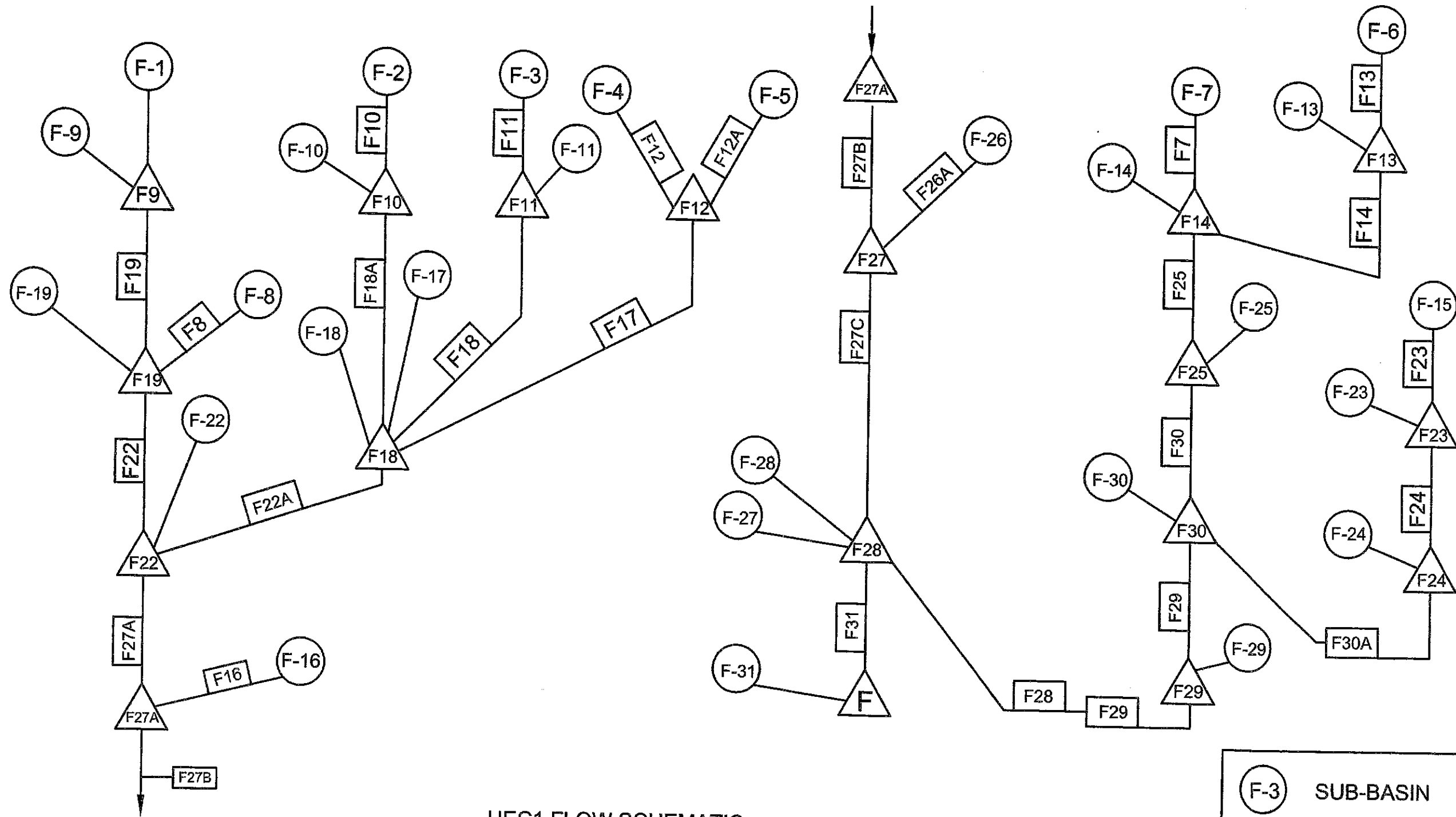
Kiowa Engineering Corporation

1604 South 21st Street  
 Colorado Springs, Colorado  
 80904-4208  
 (719) 630-7342

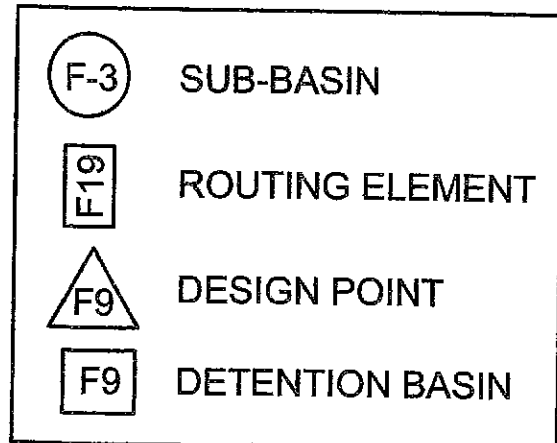
WOLF RANCH  
 HYDROLOGIC MODEL SCHEMATIC  
 COLORADO SPRINGS, COLORADO

FIGURE E

PROJECT NO.: 03094  
 DATE: 01/29/04  
 DESIGN: RNW  
 REVISIONS:



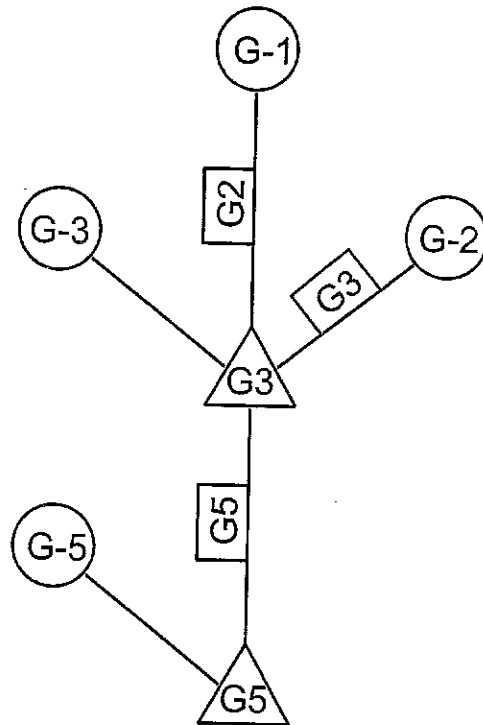
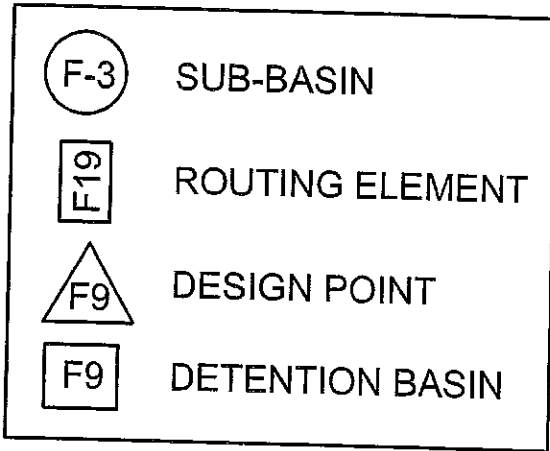
**HEC1 FLOW SCHEMATIC  
DEVELOPED CONDITION 'F' BASINS**



Kiowa Engineering Corporation  
 1604 South 21st St.  
 Colorado Springs, Colorado  
 80904 - 4208  
 (719) 630-7342

**WOLF RANCH  
 HYDROLOGIC MODEL SCHEMATIC  
 FIGURE F  
 COLORADO SPRINGS, COLORADO**

Project No.:	03004
Scale:	
Date:	03/06/04
Design:	RAW
Drawn:	JUN
Check:	RAW
Revisions:	



HEC1 FLOW SCHEMATIC  
DEVELOPED CONDITION 'G' BASINS

<p><u>Kiowa Engineering Corporation</u> 1604 South 21st Street Colorado Springs, Colorado 80904-4208 (719) 630-7342</p>	<p align="center">WOLF RANCH HYDROLOGIC MODEL SCHEMATIC COLORADO SPRINGS, COLORADO  FIGURE G</p>	<p>PROJECT NO.: 03094 DATE: 02/17/04 DESIGN: RNW REVISIONS:</p>
---	--	---

**HEC-1 INPUT & OUTPUT**  
**EXISTING DEVELOPMENT CONDITIONS**

```

*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* U.S. ARMY CORPS OF ENGINEERS
* JUN 1998
* HYDROLOGIC ENGINEERING CENTER
* VERSION 4.1
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
* RUN DATE 25FEB04 TIME 18:18:07
* (916) 756-1104
*
*****
*****

```

A-BASINS  
EXISTING

```

X      X  XXXXXXXX  XXXXX      X
X      X  X        X      X      XX
X      X  X        X        X      X
XXXXXXXX XXXX      X          XXXXX  X
X      X  X        X        X      X
X      X  X        X      X      X
X      X  XXXXXXXX  XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1  
PAGE 1

HEC-1 INPUT

LINE  
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1 ID Wolf Ranch Master Development Drainage Plan  
2 ID A Basins, existing development condition PN

J3094

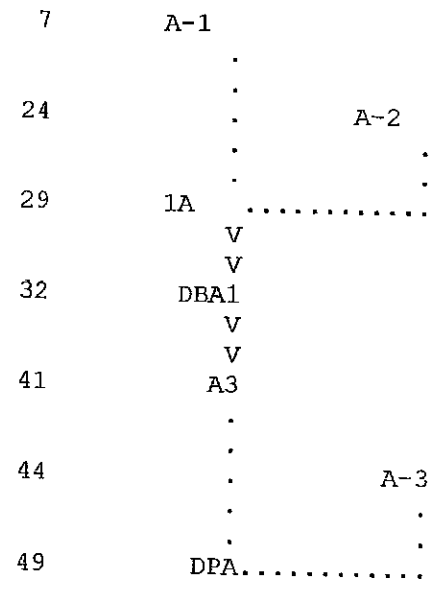
ABASINE.DAT	3	ID	5-year and 100 Year, 24 hr Type IIA Storm					fn			
		*DIAGRAM									
	4	IT	5	0	0	300					
	5	IO	5	0							
	6	JR	PREC	.56	1.0						
	7	KK	A-1								
	8	KM	SCS RUNOFF FOR SUB-BASIN A-1								
	9	BA	.1819								
	10	IN	15								
	11	PB	4.4								
0.0100	0.0120	0.0143	12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080
0.0390	0.0460	0.0530	13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320
0.7650	0.7800	0.7900	14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500
0.8450	0.8500	0.8550	15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400
0.8863	0.8900	0.8938	16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825
0.9210	0.9240	0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180
0.9475	0.9500	0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450
0.9725	0.9750	0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700
0.9888	0.9900	0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875
			21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000
			22	LS	0	61					
			23	UD	0.36						
			24	KK	A-2						
			25	KM	RUNOFF FOR SUB-BASIN A-2						
			26	BA	.1098						
			27	LS	0	61					
			28	UD	.29						
			29	KK	1A						
			30	KM	DESIGN POINT 1A COMBINE RUNOFF FROM A-1 AND A-2						
			31	HC	2						
			32	KK	DBA1						
			33	KM	ROUTE DP 1A THROUGH EXISTING STOCK POND DBA1						
			34	RS	1	ELEV	7040			1	
			35	SA	0.16	0.34	0.56	0.77			
			36	SE	7040	7041	7042	7043			
			37	SS	7041	60	0.49	1.5			
			38	ST	7041	60	0.49	1.5			
			39	SW	0	10	70	90			
			40	SE	7043	7041	7041	7043			
			41	KK	A3						
BASIN A-3			42	KM	ROUTE OUTFLOW FROM EXISTING STOCK POND DBA1 THROUGH SUB-						

LINE  
 ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

44	KK	A-3		
45	KM	RUNOFF FOR SUB-BASIN A-3		
46	BA	.1318		
47	LS	0	61	
48	UD	0.28		
49	KK	DPA		
50	KM	DESIGN POINT A COMBINE RUNOFF from A3 AND SUB-BASIN A-3		
51	HC	2		
52	ZZ			

1  
 SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW



(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
* HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
* 609 SECOND STREET *
  
```

```

*
* DAVIS, CALIFORNIA 95616 *
* RUN DATE 25FEB04 TIME 18:18:07 *
* (916) 756-1104 *
*
*
*****
*****

```

Wolf Ranch Master Development Drainage Plan  
 A Basins, existing development condition PN 03094  
 5-year and 100 Year, 24 hr Type IIA Storm fn

ABASINE.DAT

```

5 IO      OUTPUT CONTROL VARIABLES
          IPRNT      5  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

```

```

IT        HYDROGRAPH TIME DATA
          NMIN      5  MINUTES IN COMPUTATION INTERVAL
          IDATE     1  0  STARTING DATE
          ITIME     0000 STARTING TIME
          NQ        300 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE    2  0  ENDING DATE
          NDTIME    0055 ENDING TIME
          ICENT     19  CENTURY MARK

```

```

          COMPUTATION INTERVAL    .08 HOURS
          TOTAL TIME BASE        24.92 HOURS

```

ENGLISH UNITS

```

          DRAINAGE AREA      SQUARE MILES
          PRECIPITATION DEPTH INCHES
          LENGTH, ELEVATION  FEET
          FLOW                CUBIC FEET PER SECOND
          STORAGE VOLUME     ACRE-FEET
          SURFACE AREA       ACRES
          TEMPERATURE        DEGREES FAHRENHEIT

```

```

JP        MULTI-PLAN OPTION
          NPLAN            1  NUMBER OF PLANS

```

```

JR        MULTI-RATIO OPTION
          RATIOS OF PRECIPITATION
          .56      1.00

```

1

ECONOMIC COMPUTATIONS

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS



PRECIPITATION OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO			
				RATIO 1	RATIO 2		
				.56	1.00		
HYDROGRAPH AT +	A-1	.18	1	FLOW TIME	7. 6.33	85. 6.25	
HYDROGRAPH AT +	A-2	.11	1	FLOW TIME	5. 6.25	59. 6.17	
2 COMBINED AT +	DPA1	.29	1	FLOW TIME	12. 6.33	142. 6.25	
ROUTED TO +	DBA1	.29	1	FLOW TIME	8. 6.75	116. 6.33	
				** PEAK STAGES IN FEET **			
				1	STAGE	7041.41	7043.50
					TIME	6.75	6.33
ROUTED TO +	A3	.29	1	FLOW TIME	8. 6.92	113. 6.42	
HYDROGRAPH AT +	A-3	.13	1	FLOW TIME	6. 6.25	72. 6.17	
2 COMBINED AT +	DPA	.42	1	FLOW TIME	11. 6.75	157. 6.42	

1  
STATION DBA1  
BREACH FORMATION)

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING

PLAN 1 .....	INITIAL VALUE	SPILLWAY CREST	TOP
OF DAM			
7041.00	ELEVATION	7040.00	7041.00
0.	STORAGE	0.	0.
0.	OUTFLOW	0.	0.

TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS
6.75	.00	.56	7041.41	.41	0.	8.	18.58
6.33	.00	1.00	7043.50	2.50	2.	116.	19.00

\*\*\* NORMAL END OF HEC-1 \*\*\*

EIE CONDITIONS  
B - BASINS

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
* HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
* 609 SECOND STREET *
* *
* DAVIS, CALIFORNIA 95616 *
* RUN DATE 16JAN04 TIME 15:41:35 *
* (916) 756-1104 *
*
*****
*****

```

```

X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION.

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY.

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1  
PAGE 1

HEC-1.INPUT

```

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Wolf Ranch Master Development Drainage Plan
2 ID B basins existing development condition PN 03094
3 ID 5-year and 100 Year, 24 hr Type IIA Storm FN bbas-e.dat
*DIAGRAM
4 ET 5 0 0 300
5 IO 4 0
6 JR PREC .56 1.0
7 KK B-1
8 RM NOTE FOR SUB-BASIN B1
9 BA .1505
10 IN 15
11 PB 4.4
12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120
0.0143
13 PC 0.0165 0.0188 0.0210 0.0233 0.0255 0.0278 0.0320 0.0390 0.0460
0.0530

```

0.7900	14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800
0.8550	15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500
0.8938	16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900
0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240
0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500
0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750
0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900
	21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000		
	22	LS	0	61							
	23	UD	0.50								
	24	ZZ									

1.

SCHMATIC DIAGRAM OF STREAM NETWORK

INPUT  
LINE

(V) ROUTING (--->) DIVERSION OR PUMP FLOW

NO.

(.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

7 B-1

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
U.S. ARMY CORPS OF ENGINEERS
* JUN 1998
HYDROLOGIC ENGINEERING CENTER
* VERSION 4.1
609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
* RUN DATE 16JAN04 TIME 15:41:35
(916) 756-1104
*
*****
*****

```

Wolf Ranch Master Development Drainage Plan  
 B basins existing development condition PN 03094  
 5-year and 100 Year, 24 hr Type IIA Storm FN bbas-e.dat

5 IO

OUTPUT CONTROL VARIABLES

FRONT 4 FRONT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0 HYDROGRAPH PLOT SCALE

IT

HYDROGRAPH TIME DATA

NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 2 0 ENDING DATE  
 NDTIME 0055 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS





EXISTING CONDITIONS  
C-BASINS

```

1*****
*****
*
*
*   FLOOD HYDROGRAPH PACKAGE (HEC-1)
U.S. ARMY CORPS OF ENGINEERS
*   JUN 1998
HYDROLOGIC ENGINEERING CENTER
*   VERSION 4.1
609 SECOND STREET
*
DAVIS, CALIFORNIA 95616
*   RUN DATE 16JAN04 TIME 15:41:52
(916) 756-1104
*
*****
*****

```

```

X   X XXXXXXXX XXXXX      X
X   X X      X      X    XX
X   X X      X      X    X
XXXXXXX XXXX      X      XXXXX X
X   X X      X      X    X
X   X X      X      X    X
X   X XXXXXXXX XXXXX      XXXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE. NEW FINITE DIFFERENCE ALGORITHM

1  
PAGE 1

HEC-1 INPUT

```

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1          ID          Wolf Ranch Master Development Drainage Plan
2          ID          C Basins existing development condition PN 03094
3          TD          5-year and 100 Year, 24 hr Type IIA Storm FN cbas-e.dat
          *DIAGRAM
4          TA          5          ~          ~          ~
5          IO          4          0
6          JR          PREC          .56          1.0

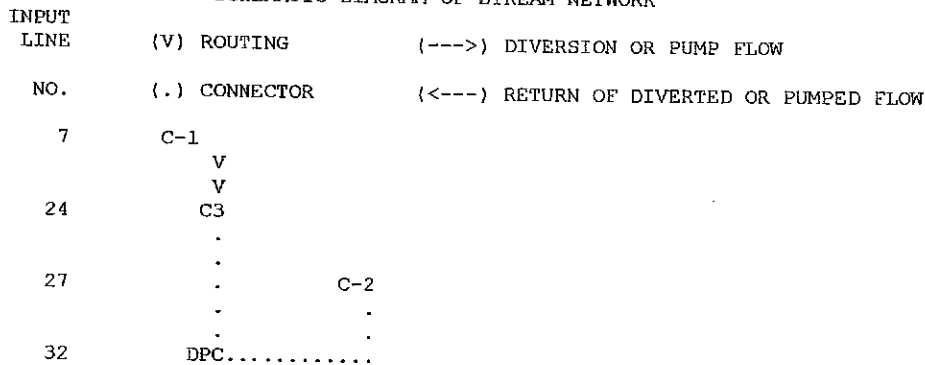
7          KK          C-1
8          KA          RUNOFF FOR SUBBASIN C1
9          BA          .1508
10         IN          15
11         PB          4.4
12         PC          0.0000  0.0005  0.0015  0.0030  0.0045  0.0060  0.0080  0.0100  0.0120
0.0143
13         PC          0.0165  0.0188  0.0210  0.0233  0.0255  0.0278  0.0320  0.0390  0.0460
0.0530

```

0.7900	14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800
0.8550	15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500
0.8938	16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900
0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240
0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500
0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750
0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900
	21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000		
	22	LS	0	61							
	23	UD	0.46								
	24	KK	C3								
	25	RM	ROUTE SUB-BASIN C-1 TO DF C								
	26	RD	.3700	.032	.004		TRAP	.10		.4	
	27	KK	C-2								
	28	KM	RUNOFF FOR SUB-BASIN C-2								
	29	BA	.0991								
	30	LS	0	61							
	31	UD	0.43								
	32	KK	DPC								
	33	KM	COMBINE RUNOFF FROM C3 AND C-2								
	34	HC	2								
	35	ZZ									

1

SCHEMATIC DIAGRAM OF STREAM NETWORK



(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
* HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* RUN DATE 16JAN04 TIME 15:41:52 *
* (916) 756-1104 *
*
*****
*****

```



Wolf Ranch Master Development Drainage Plan  
 C Basins existing development condition PN 03094  
 5-year and 100 Year, 24 hr Type IIA Storm FN cbas-e.dat

5 IO            OUTPUT CONTROL VARIABLES  
                  IPRNT            4    PRINT CONTROL  
                  IPLOT            0    PLOT CONTROL  
                  QSCAL            0.    HYDROGRAPH PLOT SCALE

IT             HYDROGRAPH TIME DATA  
                  NMIN            5    MINUTES IN COMPUTATION INTERVAL  
                  IDATE           1    0    STARTING DATE  
                  ITIME           0000 STARTING TIME  
                  NQ               300. NUMBER OF HYDROGRAPH ORDINATES  
                  NDDATE          2    0    ENDING DATE  
                  NDTIME          0055 ENDING TIME  
                  ICENT           19    CENTURY MARK

                 COMPUTATION INTERVAL    .08 HOURS  
                  TOTAL TIME BASE        24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA            SQUARE MILES  
 PRECIPITATION DEPTH     INCHES  
 LENGTH, ELEVATION       FEET  
 FLOW                      CUBIC FEET PER SECOND  
 STORAGE VOLUME          ACRES-FEET  
 SURFACE AREA             ACRES  
 TEMPERATURE             DEGREES FAHRENHEIT

JP             MULTI-PLAN OPTION  
                  NPLAN            1    NUMBER OF PLANS

JR             MULTI-RATIO OPTION  
                  RATIOS OF PRECIPITATION  
                  .56        1.00

\*\*\* \*\*  
 \*\*\* \*\*

\*\*\*\*\*  
 \*            \*  
 7 KK        \*    C-1    \*  
 \*            \*  
 \*\*\*\*\*

RUNOFF FOR SUBIBASN C1

10 IN           TIME DATA FOR INPUT TIME SERIES  
                  JXMIN            15    TIME INTERVAL IN MINUTES  
                  JXDATE          1    0    STARTING DATE  
                  JXTIME          0    STARTING TIME

SUBBASIN RUNOFF DATA

9 BA            SUBBASIN CHARACTERISTICS  
                  TAREA            .15    SUBBASIN AREA

PRECIPITATION DATA

11 PB           STORM            4.40    BASIN TOTAL PRECIPITATION

12 PI           INCREMENTAL PRECIPITATION PATTERN

.00            .00            .00            .00            .00            .00            .00            .00







COMBINE RUNOFF from C3 AND C-1

34 HC HYDROGRAPH COMBINATION  
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\*

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC  
 COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	C-1	.15	1	FLOW	58.
				TIME	6.50
ROUTED TO					
+	C3	.15	1	FLOW	59.
				TIME	6.50
HYDROGRAPH AT					
+	C-2	.10	1	FLOW	41.
				TIME	6.33
2 COMBINED AT					
+	DPC	.25	1	FLOW	94.
				TIME	6.50

1

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

VOLUME (IN)	ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO COMPUTATION INTERVAL	
								PEAK (CFS)	TIME TO PEAK (MIN)
		FOR PLAN = 1	RATIO= .00						
.19		C3 MANE	2.00	5.79	406.00	.18	5.00	5.43	410.00

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1490E+01 EXCESS= .0000E+00 OUTFLOW= .1481E+01 BASIN STORAGE=  
 .1603E-01 PERCENT ERROR= -.5

		FOR PLAN = 1	RATIO= .00						
1.02		C3 MANE	2.50	58.59	390.00	1.02	5.00	58.59	390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8231E+01 EXCESS= .0000E+00 OUTFLOW= .8223E+01 BASIN STORAGE=  
 .2816E-01 PERCENT ERROR= -.2

\*\*\* NORMAL END OF HEC-1 \*\*\*

*Eastfield  
D Basins  
2-1002R*

```

*****
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
CORPS OF ENGINEERS
* JUN 1998
ENGINEERING CENTER
* VERSION 4.1
SECOND STREET
*
CALIFORNIA 95616
* RUN DATE 11MAR04 TIME 12:41:53
(916) 756-1104
*
*****
*****

```

```

*
* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,
*
*

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND ECL1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

1  
PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10	
1	ID	Wolf Ranch Master Development Drainage Plan										
2	ID	D Basins existing development conditions PN 03094										
3	ID	5-year and 100 Year, 24 hr Type IIA Storm FN dbas-e.dat										
	*DIAGRAM											
4	IT	5	0	0	300							
5	IO	4	0									
6	JR	PREC	.48	.61	.70	.93	1.0					
7	KK	D-1										
8	KM	RUNOFF FOR Sub-basin D-1										
9	EA	.1503										
10	IN	15										
11	PB	4.4										
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143	
13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530	
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900	
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550	
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938	
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270	

18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	61								
23	UD	0.44									
24	KK	D2									
25	KM	ROUTE FLOW FROM SUB-BASIN D-1 TP DP D2									
26	RD	5470	0.027	0.04			TRAP	10	10		
27	KK	D-2									
28	KM	RUNOFF FROM Sub-basin D-2									
29	BA	.1660									
30	LS	0	61								
31	UD	0.37									
32	KK	DPD2									
33	KM	COMBINE RUNOFF from D-2 AND D2									
34	HC	2									
35	KK	D3									
36	KM	ROUTE FLOW FROM DP D2 TO DP D									
37	RD	3000	0.035	0.04			TRAP	10	10		
38	KK	D-3									
39	KM	RUNOFF FROM Sub-basin D-3									
40	BA	.0450									
41	LS	0	61								
42	UD	0.12									

HEC-1 INPUT

1  
PAGE 2

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
43	KK DPD2
44	KM COMBINE RUNOFF from D-3 AND D3
45	HC 2
46	ZZ

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
7	D-1	
	V	
	V	
24	D2	
	.	
	.	
27	D-2	
	.	
	.	
32	DPD2.....	
	V	
	V	
35	D3	
	.	
	.	
38	D-3	
	.	
	.	
43	DPD2.....	

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

1\*\*\*\*\*  
\*\*\*\*\*

```

*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
*
CALIFORNIA 95616 *
* RUN DATE 11MAR04 TIME 12:41:53 *
(916) 756-1104 *
*
*
*****
*****

```

Wolf Ranch Master Development Drainage Plan  
 D Basins existing development conditions PN 03094  
 5-year and 100 Year, 24 hr Type IIA Storm FN dbas-e.dat

```

5 IO      OUTPUT CONTROL VARIABLES
          IPRNT      4  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

```

```

IT        HYDROGRAPH TIME DATA
          NMIN       5  MINUTES IN COMPUTATION INTERVAL
          IDATE      1  0  STARTING DATE
          ITIME      0000 STARTING TIME
          NQ         300 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE     2  0  ENDING DATE
          NDDTIME    0055 ENDING TIME
          ICENT      19  CENTURY MARK

```

```

          COMPUTATION INTERVAL .08 HOURS
          TOTAL TIME BASE     24.92 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME    ACRE-FEET
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

```

JP        MULTI-PLAN OPTION
          NPLAN      1  NUMBER OF PLANS

```

```

JR        MULTI-RATIO OPTION
          RATIOS OF PRECIPITATION
          .48      .61      .70      .93      1.00

```

```

*** **
*** **

```

```

*****
*
7 KK    * D-1 *
*
*****

```

RUNOFF FOR Sub-basin D-1





.00 .00 .00 .00 .00 .00 .00 .00

22 LS SCS LOSS RATE  
STRTL 1.28 INITIAL ABSTRACTION  
CRVNBR 61.00 CURVE NUMBER  
RTIMP .00 PERCENT IMPERVIOUS AREA

23 UD SCS DIMENSIONLESS UNITGRAPH  
TLAG .44 LAG

\*\*\*

UNIT HYDROGRAPH  
28 END-OF-PERIOD ORDINATES

66.	12.	37.	76.	122.	146.	150.	139.	120.	92.
4.	50.	38.	29.	22.	16.	12.	9.	7.	5.
	3.	2.	2.	1.	1.	1.	0.	0.	

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
24 KK \* D2 \*  
\* \*  
\*\*\*\*\*

ROUTE FLOW FROM SUB-BASIN D-1 TP DP D2

HYDROGRAPH ROUTING DATA

26 RD MUSKINGUM-CUNGE CHANNEL ROUTING  
L 5470. CHANNEL LENGTH  
S .0270 SLOPE  
N .040 CHANNEL ROUGHNESS COEFFICIENT  
CA .00 CONTRIBUTING AREA  
SHAPE TRAP CHANNEL SHAPE  
WD 10.00 BOTTOM WIDTH OR DIAMETER  
Z 10.00 SIDE SLOPE

\*\*\*

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
27 KK \* D-2 \*  
\* \*  
\*\*\*\*\*

RUNOFF FROM Sub-basin D-2

SUBBASIN RUNOFF DATA

29 BA SUBBASIN CHARACTERISTICS  
TAREA .17 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.40 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN  
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00

.00



39. 28. 20. 14. 10. 7. 5. 4. 3.  
 2. 1. 1. 0.

\*\*\* \*\*  
 \*\*\* \*\*

32 KK  
 \*\*\*\*\*  
 \* \*  
 \* DPD2 \*  
 \* \*  
 \*\*\*\*\*

COMBINE RUNOFF from D-2 AND D2

34 HC HYDROGRAPH COMBINATION  
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\*

\*\*\* \*\*  
 \*\*\* \*\*

35 KK  
 \*\*\*\*\*  
 \* \*  
 \* D3 \*  
 \* \*  
 \*\*\*\*\*

ROUTE FLOW FROM DP D2 TO DP D

HYDROGRAPH ROUTING DATA

37 RD MUSKINGUM-CUNGE CHANNEL ROUTING  
 L 3000. CHANNEL LENGTH  
 S .0350 SLOPE  
 N .040 CHANNEL ROUGHNESS COEFFICIENT  
 CA .00 CONTRIBUTING AREA  
 SHAPE TRAP CHANNEL SHAPE  
 WD 10.00 BOTTOM WIDTH OR DIAMETER  
 Z 10.00 SIDE SLOPE

\*\*\*

\*\*\* \*\*  
 \*\*\* \*\*

38 KK  
 \*\*\*\*\*  
 \* \*  
 \* D-3 \*  
 \* \*  
 \*\*\*\*\*

RUNOFF FROM Sub-basin D-3

SUBBASIN RUNOFF DATA

40 BA SUBBASIN CHARACTERISTICS  
 TAREA .05 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.40 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN



\*\*\* \*\*

\*\*\*\*\*  
 \*  
 43 KK \* DPD2 \*  
 \*  
 \*\*\*\*\*

COMBINE RUNOFF from D-3 AND D3

45 HC HYDROGRAPH COMBINATION  
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\*

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION					
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	
				.48	.61	.70	.93	1.00	
HYDROGRAPH AT									
+	D-1	.15	1	FLOW	2.	9.	18.	49.	60.
				TIME	6.58	6.42	6.42	6.33	6.33
ROUTED TO									
+	D2	.15	1	FLOW	2.	9.	20.	49.	59.
				TIME	7.33	7.00	6.67	6.67	6.67
HYDROGRAPH AT									
+	D-2	.17	1	FLOW	2.	11.	22.	61.	75.
				TIME	6.50	6.33	6.33	6.25	6.25
2 COMBINED AT									
+	DPD2	.32	1	FLOW	4.	14.	33.	84.	103.
				TIME	7.33	6.92	6.67	6.50	6.50
ROUTED TO									
+	D3	.32	1	FLOW	3.	15.	31.	88.	103.
				TIME	7.67	7.17	6.92	6.67	6.67
HYDROGRAPH AT									
+	D-3	.05	1	FLOW	1.	6.	12.	30.	36.
				TIME	6.08	6.08	6.08	6.08	6.08
2 COMBINED AT									
+	DPD2	.36	1	FLOW	4.	16.	32.	92.	107.
				TIME	7.67	7.17	6.92	6.67	6.67

\*\*\* NORMAL END OF HEC-1 \*\*\*

*Ea Condition*  
*E Basins*  
*2 -> 100yr*

```

*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
*
CALIFORNIA 95616 *
* RUN DATE 11MAR04 TIME 12:43:42 *
(916) 756-1104 *
*
*****
*****

```

```

*
*
* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,
*
*

```

```

X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1  
PAGE 1

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Wolf Ranch master Development Drainage Plan									
2	ID	E Basins existing development condition PN 03094									
3	ID	5-year and 100 Year, 24 hr Type IIA Storm FN ebas-e.dat									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	4	0								
6	JR	PREC	.48	.61	.70	.93	1.0				
7	KK	E-1									
8	KM	RUNOFF FOR SUB-BASIN E-1									
9	BA	.1640									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143
13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270

18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	61								
23	UD	0.44									
24	KK	E2									
25	KM	ROUTE FLOW FROM SUB-BASIN E-1 TO DP E									
26	RD	3050	.035	0.04		TRAP	10	5			
27	KK	E-2									
28	KM	RUNOFF FOR SUB-BASIN E-2									
29	BA	.1520									
30	LS	0	61								
31	UD	0.44									
32	KK	DPE									
33	KM	COMBINE RUNOFF FROM E2 AND E-2									
34	HC	2									
35	ZZ										

1

SCHMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE NO.	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW	
7	E-1	
	V	
	V	
24	E2	
	.	
	.	
27	.	E-2
	.	.
	.	.
32	DPE.....	

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
* CALIFORNIA 95616 *
* RUN DATE 11MAR04 TIME 12:43:42 *
(916) 756-1104 *
*
*****
*****

```

Wolf Ranch master Development Drainage Plan  
E Basins existing development condition FN 03094  
5-year and 100 Year, 24 hr Type IIA Storm FN ebas-e.dat

5 IO OUTPUT CONTROL VARIABLES

IPRNT	4	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE









.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

30 LS SCS LOSS RATE  
STRTL 1.28 INITIAL ABSTRACTION  
CRVNER 61.00 CURVE NUMBER  
RTIMP .00 PERCENT IMPERVIOUS AREA

31 UD SCS DIMENSIONLESS UNITGRAPH  
TLAG .44 LAG

\*\*\*

	UNIT HYDROGRAPH									
	28 END-OF-PERIOD ORDINATES									
67.	12.	37.	77.	123.	148.	152.	141.	121.	93.	
4.	50.	38.	29.	22.	16.	12.	9.	7.	5.	
	3.	2.	2.	1.	1.	1.	1.	0.		

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
32 KK \* DPE \*  
\* \*  
\*\*\*\*\*

COMBINE RUNOFF FROM E2 AND E-2

34 HC HYDROGRAPH COMBINATION  
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\*

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
FLOWS IN CURTIC FEET PER SECOND, AREA IN SQUARE MILES  
TIME TO PEAK IN HOURS

RATIOS APPLIED TO PRECIPITATION

OPERATION	STATION	AREA	PLAN		RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5
					.48	.61	.70	.93	1.00
HYDROGRAPH AT									
+	E-1	.16	1	FLOW	2.	10.	19.	53.	66.
				TIME	6.58	6.42	6.42	6.33	6.33
ROUTED TO									
+	E2	.16	1	FLOW	2.	10.	19.	53.	66.
				TIME	6.92	6.67	6.58	6.50	6.50
HYDROGRAPH AT									
+	E-2	.15	1	FLOW	2.	9.	18.	49.	61.
				TIME	6.58	6.42	6.42	6.33	6.33
2 COMBINED AT									
+	DPE	.32	1	FLOW	3.	18.	35.	99.	124.
				TIME	6.92	6.58	6.50	6.42	6.42
1									
*** NORMAL END OF HEC-1 ***									

Ex-Conditions

"F" Basins

```

*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
* HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
* 609 SECOND STREET *
*
* DAVIS, CALIFORNIA 95616 *
* RUN DATE 16JAN04 TIME 17:45:26 *
* (916) 756-1104 *
*
*****
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1  
PAGE 1

HEC-1 INPUT

```

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Wolf-Ranch Master Development Drainage Plan
2 ID F Basins Existing Development Condition PN 03094
3 ID 5-year and 100 Year, 24 hr Type IIA Storm FN fbas-e.dat
*DIAGRAM
4 XT 5 0 0 300
5 IO 4 0
6 JR PREC -.56 1.0
7 KK F-1
8 KM RUNOFF SUB-BASIN F-1
9 BA .1659
10 IN 1b
11 PFP 4.4
12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120
0.0143
13 PC 0.0165 0.0188 0.0210 0.0233 0.0255 0.0278 0.0320 0.0390 0.0460
0.0530

```

0.7900	14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800
0.8550	15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500
0.8938	16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900
0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240
0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500
0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750
0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900
	21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000		
	22	LS	0	61							
	23	UD	0.20								
	24	KK	1-8								
	25	KM	ROUTE FLOW FROM F-1 THROUGH F-8								
	26	RD	4620	0.04	0.04		TRAP	6		3	
	27	KK	F-8								
	28	KM	SCS RUNOFF F-8								
	29	BA	.1499								
	30	LS	0	61							
	31	UD	.22								
	32	KK	1F								
	33	KM	COMBINE RUNOFF FROM F-1 AND F-8								
	34	HC	2								
	35	KK	F-2								
	36	KM	SCS RUNOFF F-2								
	37	BA	.0424								
	38	LS	0	61							
	39	UD	.19								
	40	KK	F-3								
	41	KM	SCS RUNOFF F-3								
	42	BA	.0942								
	43	LS	0	61							
	44	UD	.22								

1  
PAGE 2

HEC-1 INPUT

LINE  
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

45	KK	2F									
46	KM	COMBINE RUNOFF FROM F-2 AND F-3									
47	HC	2									
48	KK	2F-5F									
49	KM	ROUTE FLOW FROM 2F THROUGH F-9									
50	RD	3087	0.036	0.04		TRAP	6			3	
51	KK	F-9									
52	KM	SCS RUNOFF F-9									
53	BA	.1953									
54	LS	0	61								
55	UD	.27									
56	KK	5F									
57	KM	COMBINE RUNOFF FROM 2F AND F-9									
58	HC	2									
59	KK	POND1									
60	KM	ROUTE FLOW THROUGH POND1									
61	RS	1	ELEV	7133							

62	SA	0.41	0.58	0.76	0.86				
63	SE	7133	7134	7135	7136				
64	ST	7133	10	0.50	1.5				
65	SS	7133	10	0.50	1.5				
66	SW	0	50	60	70	125			
67	SE	7136	7135	7133	7133	7136			
68	KK	F-4							
69	KM	SCS RUNOFF F-4							
70	BA	.2681							
71	LS	0	61						
72	UD	.28							
73	KK	F-5							
74	KM	SCS RUNOFF F-5							
75	BA	.1073							
76	LS	0	61						
77	UD	.28							
78	KK	3F							
79	KM	COMBINE RUNOFF FROM F-4 AND F-5							
80	HC	2							
81	KK	3F-6F							
82	KM	ROUTE FLOW FROM 3F THROUGH F-10							
83	RD	3790	0.034	0.04		TRAP	10	10	
84	KK	F-10							
85	KM	SCS RUNOFF F-10							
86	BA	.0883							
87	LS	0	61						
88	UD	.28							

1  
PAGE 3

HEC-1 INPUT

LINE  
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

89	KK	6F							
90	KM	COMBINE RUNOFF FROM 3F AND F-10							
91	HC	2							
92	KK	8F							
93	KM	COMBINE RUNOFF FROM 5F AND 6F							
94	HC	2							
95	KK	8F-9F							
96	KM	ROUTE FLOW FROM 8F TO 9F							
97	RD	1706	0.034	0.04		TRAP	6	2	
98	KK	F9							
99	KM	COMBINE RUNOFF FROM 1F AND 8F							
100	HC	2							
101	KK	F12							
102	KM	ROUTE FLOW FROM 5F 8F TO DF F12							
103	RC	.04	0.035	0.04	5200	0.022			
104	RX	0	20	33	37	43	47	60	80
105	RY	7014	7004	7004	7000	7000	7004	7004	7014
106	KK	F-6							
107	KM	SCS RUNOFF F-6							
108	BA	.0310							
109	LS	0	61						
110	UD	.19							
111	KK	F-7							
112	KM	SCS RUNOFF F-7							
113	BA	.0782							
114	LS	0	61						



115 UD .19  
 116 KK 4F  
 117 KM COMBINE RUNOFF FROM F-6 AND F-7  
 118 HC 2  
 119 KK 4F-7F  
 120 KM ROUTE FLOW FROM 4F THROUGH F-11  
 121 RD 3610 0.06 0.04 TRAP 10 10  
 122 KK F-11  
 123 KM SCS RUNOFF F-11  
 124 BA .1136  
 125 LS 0 61  
 126 UD .16  
 127 KK 7F  
 128 KM COMBINE RUNOFF FROM 4F AND F-11  
 129 HC 2

1  
PAGE 4

HEC-1 INPUT

LINE  
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

130 KK 7F-10F  
 131 KM ROUTE FLOW FROM 7F THROUGH F-14  
 132 RD 4970 0.023 0.04 TRAP 6 3  
 133 KK F-14  
 134 KM SCS RUNOFF F-14  
 135 BA .1493  
 136 LS 0 61  
 137 UD .30  
 138 KK F-13 1  
 139 KM RUNOFF SUB-BASIN F-13  
 140 BA .1169  
 141 LS 0 61  
 142 UD .44  
 143 KK F14  
 144 KM COMBINE RUNOFF FROM 7F, F-13, AND F-14  
 145 HC 3  
 146 KK DBF13  
 147 KM ROUTE FLOW FROM DP F14 THROUGH POND DBF13  
 148 RS 1 ELEV 7026 1  
 149 SA 1.97 2.35 2.83 3.21 3.66 4.0 4.33  
 150 SE 7026 7027 7028 7029 7030 7031 7032  
 151 ST 7029 40 0.50 1.5  
 152 SS 7029 40 0.50 1.5  
 153 SW 0 0 1.20 1.50  
 154 SE 7032 7029 7029 7032  
 155 KK F15  
 156 KM ROUTE FLOW FROM POND DB F13 TO DP F15  
 157 RS 1 STOR. -1  
 158 RC .04 0.035 0.04 1194 0.5  
 159 RX 0 20 33 37 43 47 60 80  
 160 RY 7014 7004 7004 7000 7000 7004 7004 7014  
 161 KK F-15  
 162 KM RUNOFF SUB-BASIN F-15  
 163 BA .0321  
 164 LS 0 61  
 165 UD .11  
 166 KK DPF15  
 167 KM COMBINE RUNOFF FROM F15 AND SUB-BASIN F-15

168 HC 2  
 169 KK F-12  
 170 KM SCS RUNOFF F-12  
 171 BA .2471  
 172 LS 0 61  
 173 UD .33

1  
 PAGE 5

HEC-1 INPUT

LINE  
 ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

174 KK F12  
 175 KM COMBINE RUNOFF FROM F12, DP F15 AND F16  
 176 HC 3  
 177 KK F16  
 178 KM ROUTE FLOW FROM DP F12 TO DP F16  
 179 RC .04 0.035 0.04 2091 0.02  
 180 RX 0 20 33 37 43  
 181 RY 7014 7004 7004 7000 7000 7004 7004 7014  
 182 KK F-16  
 183 KM RUNOFF SUB-BASIN F-16  
 184 BA .0570  
 185 LS 0 61  
 186 UD .09  
 187 KK DPF16 1  
 188 KM COMBINE RUNOFF FROM F16 AND F-16  
 189 HC 2  
 190 KK F17  
 191 KM ROUTE FLOW FROM DP F16 TO DP F ,  
 192 RD 1950 0.025 0.04 TRAP 20 3  
 193 KK F-17  
 194 KM RUNOFF SUB-BASIN F-17  
 195 BA .0520  
 196 LS 0 61  
 197 UD .37  
 198 KK DPF  
 199 KM COMBINE RUNOFF FROM F17 AND SUB-BASIN F-17  
 200 HC 2  
 201 ZZ

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

7 F-1  
 V  
 V  
 24 1-8  
 .  
 27 . F-8  
 .  
 32 1F.....  
 .  
 35 . F-2  
 .  
 40 . F-3

45	.	.	.
	.	2F.....	.
	.	∇	.
	.	V	.
48	.	2F-5F	.
	.	.	.
51	.	.	F-9
	.	.	.
56	.	5F.....	.
	.	∇	.
	.	V	.
59	.	POND1	.
	.	.	.
68	.	.	F-4
	.	.	.
73	.	.	F-5
	.	.	.
78	.	.	3F.....
	.	.	∇
	.	.	V
81	.	.	3F-6F
	.	.	.
84	.	.	F-10
	.	.	.
89	.	.	6F.....
	.	.	.
92	.	8F.....	.
	.	∇	.
	.	V	.
95	.	8F-9F	.
	.	.	.
98	F9.....	.	.
	V	.	.
	V	.	.
101	F12	.	.
	.	.	.
106	.	F-6	.
	.	.	.
111	.	.	F-7
	.	.	.
116	.	4F.....	.
	.	∇	.
	.	V	.
119	.	4F-7F	.
	.	.	.
122	.	.	F-11
	.	.	.
127	.	7F.....	.
	.	∇	.
	.	V	.
130	.	7F-10F	.
	.	.	.
133	.	.	F-14
	.	.	.

```

138      .           .           .           F-13
      .           .           .           .
143      .           F14.....
      .           V
      .           V
146      .           DBF13
      .           V
      .           V
155      .           F15
      .           .
161      .           .           F-15
      .           .           .
166      .           DPF15.....
      .           .
169      .           .           F-12
      .           .           .
174      .           F12.....
      .           V
      .           V
177      .           F16
      .           .
182      .           .           F-16
      .           .           .
187      .           DPF16.....
      .           V
      .           V
190      .           F17
      .           .
193      .           .           F-17
      .           .           .
198      .           DPF.....

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	F-1	.17	1	FLOW	10.
				TIME	6.17
					110.
					6.08
ROUTED TO					
+	1-8	.17	1	FLOW	9.
				TIME	6.42
					110.
					6.25
HYDROGRAPH AT					
+	F-8	.15	1	FLOW	9.
				TIME	6.17
					93.
					6.17
2 COMBINED AT					
+	1F	.32	1	FLOW	14.
				TIME	6.42
					186.
					6.17
HYDROGRAPH AT					

+	F-2	.04	1	FLOW TIME	3. 6.17	29. 6.08
	HYDROGRAPH AT					
+	F-3	.09	1	FLOW TIME	5. 6.17	59. 6.17
	2 COMBINED AT					
+	2F	.14	1	FLOW TIME	8. 6.17	87. 6.08
	ROUTED TO					
+	2F-5F	.14	1	FLOW TIME	9. 6.33	85. 6.25
	HYDROGRAPH AT					
+	F-9	.20	1	FLOW TIME	10. 6.25	111. 6.17
	2 COMBINED AT					
+	5F	.33	1	FLOW TIME	18. 6.33	192. 6.17
	ROUTED TO					
+	POND1	.33	1	FLOW TIME	18. 6.33	192. 6.17
	** PEAK STAGES IN FEET **					
	1			STAGE TIME	7134.09 7.17	7136.25 6.17
	HYDROGRAPH AT					
+	F-4	.27	1	FLOW TIME	13. 6.25	147. 6.17
	HYDROGRAPH AT					
+	F-5	.11	1	FLOW TIME	5. 6.33	52. 6.25
	2 COMBINED AT					
+	3F	.38	1	FLOW TIME	17. 6.25	196. 6.17
	ROUTED TO					
+	3F-6F	.38	1	FLOW TIME	18. 6.42	196. 6.33
	HYDROGRAPH AT					
+	F-10	.09	1	FLOW TIME	4. 6.25	49. 6.17
	2 COMBINED AT					
+	6F	.46	1	FLOW TIME	22. 6.42	235. 6.33
	2 COMBINED AT					
+	8F	.80	1	FLOW TIME	37. 6.42	407. 6.25
	ROUTED TO					
+	8F-9F	.80	1	FLOW TIME	36. 6.50	398. 6.33
	2 COMBINED AT					
+	F9	1.11	1	FLOW TIME	49. 6.50	570. 6.25
	ROUTED TO					
+	F12	1.11	1	FLOW TIME	48. 6.75	566. 6.42

HYDROGRAPH AT						
+	F-6	.03	1	FLOW TIME	2. 6.17	21. 6.08
HYDROGRAPH AT						
+	F-7	.08	1	FLOW TIME	5. 6.17	54. 6.08
2 COMBINED AT						
+	4F	.11	1	FLOW TIME	7. 6.17	75. 6.08
ROUTED TO						
+	4F-7F	.11	1	FLOW TIME	6. 6.50	74. 6.25
HYDROGRAPH AT						
+	F-11	.11	1	FLOW TIME	8. 6.08	86. 6.08
2 COMBINED AT						
+	7F	.22	1	FLOW TIME	10. 6.42	133. 6.17
ROUTED TO						
+	7F-10F	.22	1	FLOW TIME	11. 6.50	130. 6.33
HYDROGRAPH AT						
+	F-14	.15	1	FLOW TIME	7. 6.25	77. 6.17
HYDROGRAPH AT						
+	F-13	.12	1	FLOW TIME	4. 6.50	47. 6.33
3 COMBINED AT						
+	F14	.49	1	FLOW TIME	20. 6.50	244. 6.33
ROUTED TO						
+	DBF13	.49	1	FLOW TIME	0. .00	29. 7.67
** PEAK STAGES IN FEET **						
1 STAGE 7027.97 7030.28						
TIME 24.92 7.67						
ROUTED TO						
+	F15	.49	1	FLOW TIME	0. .00	29. 7.75
** PEAK STAGES IN FEET **						
1 STAGE 7000.00 7000.20						
TIME .00 7.67						
HYDROGRAPH AT						
+	F-15	.03	1	FLOW TIME	3. 6.08	27. 6.00
2 COMBINED AT						
+	DPF15	.52	1	FLOW TIME	3. 6.08	31. 7.75
HYDROGRAPH AT						
+	F-12	.25	1	FLOW TIME	11. 6.33	123. 6.25
3 COMBINED AT						
+	F12	1.88	1	FLOW TIME	55. 6.75	664. 6.42

ROUTED TO  
+ F16 1.88 1 FLOW 48. 643.  
TIME 6.83 6.42

\*\* PEAK STAGES IN FEET \*\*  
1 STAGE 7001.13 7004.59  
TIME 6.83 6.42

HYDROGRAPH AT  
+ F-16 .06 1 FLOW 5. 53.  
TIME 6.08 6.00

2 COMBINED AT  
+ DPF16 1.94 1 FLOW 49. 650.  
TIME 6.83 6.42

ROUTED TO  
+ F17 1.94 1 FLOW 48. 644.  
TIME 7.00 6.50

HYDROGRAPH AT  
+ F-17 .05 1 FLOW 2. 24.  
TIME 6.42 6.25

2 COMBINED AT  
+ DPF 1.99 1 FLOW 49. 661.  
TIME 7.00 6.50

1  
1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION POND1  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1 .....

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	7133.00	7133.00	7133.00
STORAGE	0.	0.	0.
OUTFLOW	0.	0.	0.

TIME OF FAILURE HOURS	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
.00	.56	7134.09	1.09	1.	6.	19.08	7.17
.00	1.00	7136.25	3.25	2.	29.	19.25	6.17

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DBF13  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1 .....

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	7026.00	7029.00	7029.00
STORAGE	0.	8.	8.
OUTFLOW	0.	0.	0.

TIME OF FAILURE HOURS	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
.00	.56	7027.97	.00	5.	0.	.00	.00

.00	1.00	7030.28	1.28	12.	29.	18.42	7.67
-----	------	---------	------	-----	-----	-------	------

\*\*\* NORMAL END OF HEC-1 \*\*\*



G-BASINS  
Existing Condition

```

1*****
*****
*
*
*   FLOOD HYDROGRAPH PACKAGE (HEC-1)
U.S. ARMY CORPS OF ENGINEERS
*   JUN 1998
HYDROLOGIC ENGINEERING CENTER
*   VERSION 4.1
609 SECOND STREET
*
DAVIS, CALIFORNIA 95616
* RUN DATE 19JAN04 TIME 09:36:27
(916) 756-1104
*
*****
*****

```

```

X   X  XXXXXXXX  XXXXX      X
X   X X          X   X      XX
X   X X          X          X
XXXXXXX XXXX    X          XXXXX X
X   X X          X          X
X   X X          X   X      X
X   X  XXXXXXXX  XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION.

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 PAGE 1 HEC-1 INPUT

ID	LINE	1	2	3	4	5	6	7	8	9	10	
	1	ID	Wolf Ranch Master Development Drainage Plan									
	2	ID	G Basins Existing development conditions PN 03094									
	3	ID	5-year and 100 Year, 24 hr Type IIA Storm FN Gbas-e.dat									
		*DIAGRAM										
	4	IT	5	0	0	300						
	5	IO	4	0								
	6	JR	PREC	.56	1.0							
	7	KK	G-1									
	8	KM	RUNOFF -- Sub-basin G-1									
	9	BA	.0808									
	10	IN	15									
	11	PB	4.4									
0.0143	12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	
0.0530	13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	

0.7900	14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800
0.8550	15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500
0.8938	16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900
0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240
0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500
0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750
0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900
	21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000		
	22	LS	0	61							
	23	UD	0.22								
	24	KK	G2								
	25	KM	ROUTE FLOW from SUB-BASIN G-1 TO DP G2								
	26	RD	3700	0.029	0.04		TRAP	10		10	
	27	KK	G-2								
	28	KM	RUNOFF - Sub-basin G-2								
	29	BA	.171								
	30	LS	0	61							
	31	UD	0.31								
	32	KK	DPG2								
	33	KM	COMBINE RUNOFF from G2 AND SUB-BASIN G-2								
	34	HC	2								
	35	KK	G3								
	36	KM	ROUTE FLOW from DP G2 TO DP G3								
	37	RD	1850	0.028	0.04		TRAP	10		10	
	38	KK	G-3								
	39	KM	RUNOFF - Sub-basin G-3								
	40	BA	.068								
	41	LS	0	61							
	42	UD	0.44								

1  
PAGE 2

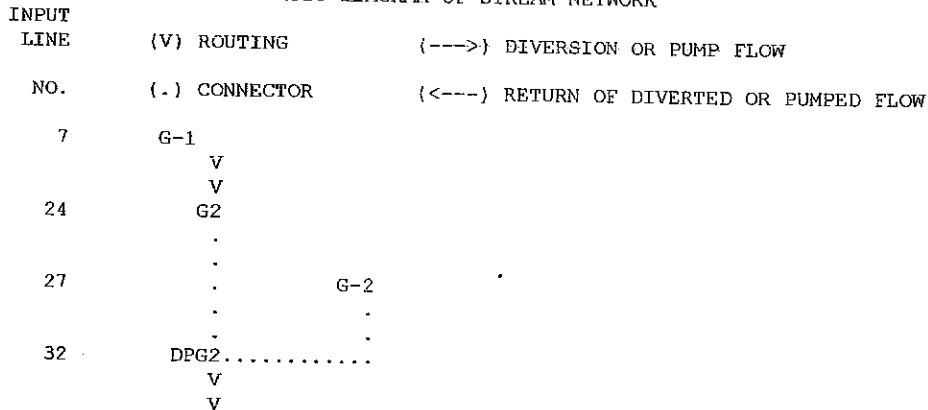
HEC-1 INPUT

LINE  
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43	KK	DPG									
44	KM	COMBINE RUNOFF from G3 AND SUB-BASIN G-3									
45	HC	2									
46	ZZ										

1

SCHEMATIC DIAGRAM OF STREAM NETWORK



```

35      G3
      .
38      .      G-3
      .
43      DPG.....

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
*****
*
*
*   FLOOD HYDROGRAPH PACKAGE (HEC-1) *
U.S. ARMY CORPS OF ENGINEERS *
*   JUN 1998 *
HYDROLOGIC ENGINEERING CENTER *
*   VERSION 4.1 *
609 SECOND STREET *
*
DAVIS, CALIFORNIA 95616 *
* RUN DATE 19JAN04 TIME 09:36:27 *
(916) 756-1104 *
*
*****
*****

```

Wolf Ranch Master Development Drainage Plan  
G Basins Existing development conditions PN 03094  
5-year and 100 Year, 24 hr Type IIA Storm FN Gbas-e.dat

```

5 IO      OUTPUT CONTROL VARIABLES
          IPRNT      4  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0.  HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMIN      5  MINUTES IN COMPUTATION INTERVAL
          IDATE     1  0  STARTING DATE
          ITIME     0000 STARTING TIME
          NQ        300 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE    2  0  ENDING DATE
          NDTIME    0055 ENDING TIME
          ICENT     .19 CENTURY MARK

          COMPUTATION INTERVAL .08 HOURS
          TOTAL TIME BASE 24.92 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME    ACRES-FEET
SURFACE AREA      ACRES
TEMPERATURE       DEGREES FAHRENHEIT

```

```

JP        MULTI-PLAN OPTION
          NPLAN      1  NUMBER OF PLANS

JR        MULTI-RATIO OPTION
          RATIOS OF PRECIPITATION
          .56      1.00

```



.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

22 LS           SCS LOSS RATE  
                   STRTL           1.28   INITIAL ABSTRACTION  
                   CRVNBR          61.00   CURVE NUMBER  
                   RTIMP           .00     PERCENT IMPERVIOUS AREA

23 UD           SCS DIMENSIONLESS UNITGRAPH  
                   TLAG            .22   LAG

\*\*\*

UNIT HYDROGRAPH  
 15 END-OF-PERIOD ORDINATES

6.	32.	108.	149.	131.	85.	49.	30.	18.	10.
	4.	2.	1.	1.	0.				

\*\*\* \*\*  
 \*\*\* \*\*

\*\*\*\*\*  
 \*                   \*  
 24 KK           \*           G2   \*  
 \*                   \*  
 \*\*\*\*\*

ROUTE FLOW from SUB-BASIN G-1 TO DP G2

HYDROGRAPH ROUTING DATA

26 RD           MUSKINGUM-CUNGE CHANNEL ROUTING  
                   L           3700.   CHANNEL LENGTH  
                   S           .0290   SLOPE  
                   N           .040   CHANNEL ROUGHNESS COEFFICIENT  
                   CA          .00   CONTRIBUTING AREA  
                   SHAPE       TRAP   CHANNEL SHAPE  
                   WD          10.00  BOTTOM WIDTH OR DIAMETER  
                   Z           10.00  SIDE SLOPE

\*\*\*

\*\*\* \*\*  
 \*\*\* \*\*

\*\*\*\*\*  
 \*                   \*  
 27 KK           \*           G-2   \*  
 \*                   \*  
 \*\*\*\*\*

RUNOFF - Sub-basin G-2

SUBBASIN RUNOFF DATA



31 UD

SCS DIMENSIONLESS UNITGRAPH  
TLAG .31 LAG

\*\*\*

UNIT HYDROGRAPH  
21 END-OF-PERIOD ORDINATES

37.	31.	101.	196.	234.	221.	178.	118.	78.	54.
1.	25.	17.	12.	8.	5.	4.	3.	2.	1.
	0.								

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
32 KK \* DPG2 \*  
\* \*  
\*\*\*\*\*

COMBINE RUNOFF from G2 AND SUB-BASIN G-2

34 HC

HYDROGRAPH COMBINATION  
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\*

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
35 KK \* G3 \*  
\* \*  
\*\*\*\*\*

ROUTE FLOW from DP G2 TOA DP G

HYDROGRAPH ROUTING DATA

37 RD

MUSKINGUM-CUNGE CHANNEL ROUTING  
L 1850. CHANNEL LENGTH  
S .0280 SLOPE  
N .040 CHANNEL ROUGHNESS COEFFICIENT  
CA .00 CONTRIBUTING AREA  
SHAPE TRAP CHANNEL SHAPE  
WD 10.00 BOTTOM WIDTH OR DIAMETER  
Z 10.00 SIDE SLOPE

\*\*\*

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
38 KK \* G-3 \*  
\* \*  
\*\*\*\*\*

RUNOFF - Sub-basin G-3

SUBBASIN RUNOFF DATA





42 UD

SCS DIMENSIONLESS UNITGRAPH  
TLAG .44 LAG

\*\*\*

		UNIT HYDROGRAPH 28 END-OF-PERIOD ORDINATES							
30.	6.	17.	35.	55.	66.	68.	63.	54.	42.
2.	22.	17.	13.	10.	7.	6.	4.	3.	2.
	1.	1.	1.	1.	0.	0.	0.	0.	

\*\*\* \*\*

\*\*\*\*\*  
\* \*  
43 KK \* DPG \*  
\* \*  
\*\*\*\*\*

COMBINE RUNOFF from G3 AND SUB-BASIN G-3

45 HC HYDROGRAPH COMBINATION  
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\*

1

COMPUTATIONS PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	G-1	.08	1	FLOW TIME	5. 6.17
					50. 6.17
ROUTED TO					
+	G2	.08	1	FLOW TIME	6. 6.58
					51. 6.33
HYDROGRAPH AT					
+	G-2	.17	1	FLOW TIME	8. 6.33
					87. 6.25
2 COMBINED AT					
+	DPG2	.25	1	FLOW TIME	11. 6.58
					130. 6.25
ROUTED TO					
+	G3	.25	1	FLOW TIME	11. 6.75
					127. 6.33
HYDROGRAPH AT					
+	G-3	.07	1	FLOW TIME	2. 6.50
					27. 6.33
2 COMBINED AT					
+	DPG	.32	1	FLOW TIME	13. 6.75
					155. 6.33

\*\*\* NORMAL END OF HEC-1 \*\*\*

*H-Basins  
Existing Conditions*

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
609 SECOND STREET *
*
DAVIS, CALIFORNIA 95616 *
* RUN DATE. 19JAN04 TIME 10:16:18 *
(916) 756-1104 *
*
*****
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1  
PAGE 1

HEC-1 INPUT

```

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Wolf Ranch master Development Drainage Plan
2 ID H Basins Existing Development Conditions PN 03094
3 ID 5-year and 100 Year, 24 hr Type IIA Storm FN hbas-e.dat
*DIAGRAM
4 YI 5 0 0 000
5 IO 4 0
6 JR PREC .56 1.0
7 KK H-1
8 RM
9 BA .0370 RUNOFF FROM SUB-BASIN H-1
10 IN 15
11 TF 4 4
12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120
0.0143
13 PC 0.0165 0.0188 0.0210 0.0233 0.0255 0.0278 0.0320 0.0390 0.0460
0.0530

```

0.7900	14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800
0.8550	15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500
0.8938	16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900
0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240
0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500
0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750
0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900
	21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000		
	22	LS	0	61							
	23	UD	0.05								
	24	KK	H-2								
	25	RM									
	26	BA	.0931								
	27	LS	0	61							
	28	UD	.47								
	29	EE									

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW  
 7 H-1  
 .  
 .  
 24 . H-2

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* U.S. ARMY CORPS OF ENGINEERS
* JUN 1998
* HYDROLOGIC ENGINEERING CENTER
* VERSION 4.1
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* RUN DATE 19JAN04 TIME 10:16:18
* (916) 756-1104
*
*****
*****

```

Wolf Ranch master Development Drainage Plan  
 H Basins Existing Development Conditions PN 03094  
 5-year and 100 Year, 24 hr Type IIA Storm FN hbas-e.dat

5 IO OUTPUT CONTROL VARIABLES  
 IPRNT 4 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL

IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 2 0 ENDING DATE  
 NDTIME 0055 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME TONE-Feet  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION  
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION  
 RATIOS OF PRECIPITATION  
 .56 1.00

\*\*\* \*\*  
 \*\*\* \*\*

\*\*\*\*\*  
 \* \*  
 7 KK \* H-1 \*  
 \* \*  
 \*\*\*\*\*

RUNOFF FROM SUB-BASIN H-1

10 IN TIME DATA FOR INPUT TIME SERIES  
 JXMIN 15 TIME INTERVAL IN MINUTES  
 JXDATE 1 0 STARTING DATE  
 JXTIME 0 STARTING TIME

SUBBASIN RUNOFF DATA

9 BA SUBBASIN CHARACTERISTICS  
 PAREA .04 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.40 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.10	.10	.00	.01	.01	.01	.01	.01	.10	.10
.00	.00	.10	.10	.01	.01	.01	.01	.01	.01





28 UD

SCS DIMENSIONLESS UNITGRAPH  
TLAG .47 LAG

\*\*\*

UNIT HYDROGRAPH									
30 END-OF-PERIOD ORDINATES									
47.	7.	19.	40.	65.	83.	88.	85.	75.	63.
3.	35.	27.	21.	16.	12.	9.	7.	5.	4.
0.	2.	2.	1.	1.	1.	1.	1.	0.	0.
1									

COMPUTATIONS

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	H-1	.04	1	FLOW TIME	5. 41. 6.00 6.00
HYDROGRAPH AT					
+	H-2	.09	1	FLOW TIME	3. 36. 6.50 6.42

\*\*\* NORMAL END OF HEC-1 \*\*\*

**HEC-1 INPUT & OUTPUT  
DEVELOPED CONDITIONS**



```

*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
*   VERSION 4.1
*
* RUN DATE 11FEB05 TIME 10:15:24
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

```

A-BASINS DEVELOPED

```

X   X   XXXXXXXX   XXXXX   X
X   X   X           X       XX
X   X   X           X       X
XXXXXXX XXXX       X       XXXXX X
X   X   X           X       X
X   X   X           X       X
X   X   XXXXXXXX   XXXXX   XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW. THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

```

                                HEC-1 INPUT
LINE  ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1     ID      Wolf Ranch, Master Developed Drainage Plan
2     ID      A Basins, future development condition ABAS-F.DAT
3     ID      5-year and 100 Year, 24 hr Type IIA Storm
4     *DIAGRAM
5     IT      5          0          0          300
6     IO      5          0
7     JR      PREC      .56          1.0
8     KK      A-1
9     KM      RUNOFF FROM SUB-BASIN A-1
10    BA      .060
11    IN      15
12    PB      4.4
12    PC      0.0000  0.0005  0.0015  0.0030  0.0045  0.0060  0.0080  0.0100  0.0120  0.0143

```

13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270
18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	61								
23	UD	.292									
24	KK	A3									
25	KM	ROUTE FLOW FROM SUB-BASIN A-1 TO DP A3									
26	RD	3500	.021	0.04		TRAP	10	4			
27	KK	A-4									
28	KM	RUNOFF FROM SUB-BASIN A-4									
29	BA	.0861									
30	LS	0	77								
31	UD	0.21									
32	KK	A4									
33	KM	ROUTE FLOW FROM SB A-4 TO DP A3									
34	RD	450	.02	.013		CIRC	3.5				
35	KK	A-3									
36	KM	RUNOFF FROM SUB-BASIN A-3									
37	BA	.1500									
38	LS	0	73								
39	UD	.221									
40	KK	DPA3									
41	KM	DESIGN POINT A3 COMBINE RUNOFF FROM SUB-BASIN A-3, A3 AND A4									
42	HC	3									

HEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43	KK	A6									
44	KM	ROUTE FLOW FROM DP A3 TO DP A6									
45	RD	1550	.016	0.04		TRAP	10	4			
46	KK	A-11									
47	KM	RUNOFF FROM SUB-BASIN A-11									
48	BA	.081									
49	LS	0	76.3								
50	UD	.19									
51	KK	A11									
52	KM	ROUTE RUNOFF FROM SB A-11 TO DPA8									



91	UD	.263				
92	KK	A9				
93	KM	ROUTE FLOW FROM SUB-BASIN A-9 TO DESIGN POINT A5				
94	RD	500	.02	.016	CIRC	3.5
95	KK	A-5				
96	KM	RUNOFF FROM SUB-BASIN A-5				
97	BA	.1114				
98	LS	0	71.6			
99	UD	.209				
100	KK	DPA5				
101	KM	DESIGN POINT A5 COMBINE RUNOFF FROM SUB-BASIN A-5, A5 AND A9				
102	HC	3				
103	KK	A10				
104	KM	ROUTE FLOW FROM DESIGN POINT A5 TO DESIGN POINT A				
105	RD	720	.021	.04	TRAP	15 4
106	KK	A-10				
107	KM	RUNOFF FROM SUB-BASIN A-10				
108	BA	.0086				
109	LS	0	79.6			
110	UD	.231				
111	KK	DPA				
112	KM	DESIGN POINT A COMBINE RUNOFF SUB-BASIN A-10 AND A10				
113	HC	2				
114	ZZ					

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
7	A-1	
	V	
	V	
24	A3	
	.	
	.	
27	A-4	
	V	
	V	
32	A4	
	.	
	.	
35	.	A-3
	.	.
	.	.

40	DPA3.....		
	V		
	V		
43	A6		
	.		
46	.	A-11	
	.	V	
	.	V	
51	.	A11	
	.	.	
54	.	.	A-8
	.	.	.
59	.	DP A8.....	
	.	V	
	.	V	
62	.	A8	
	.	.	
65	.	.	A-7
	.	.	.
70	.	DP A7.....	
	.	V	
	.	V	
73	.	A7	
	.	.	
76	.	.	A-6
	.	.	.
81	DPA6.....		
	V		
	V		
84	A5		
	.		
87	.	A-9	
	.	V	
	.	V	
92	.	A9	
	.	.	
95	.	.	A-5
	.	.	.
100	DPA5.....		
	V		
	V		
103	A10		

106

A-10

111

DPA.....

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*       JUN 1998                *
*       VERSION 4.1              *
*
* RUN DATE 11FEB05 TIME 10:15:24 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET            *
* DAVIS, CALIFORNIA 95616      *
* (916) 756-1104              *
*
*****

```

Wolf Ranch, Master Developed Drainage Plan  
 A Basins, future development condition ABAS-F.DAT  
 5-year and 100 Year, 24 hr Type IIA Storm

5 IO

OUTPUT CONTROL VARIABLES

```

IPRNT      5 PRINT CONTROL
IPLOT      0 PLOT CONTROL
QSCAL     0. HYDROGRAPH PLOT SCALE

```

IT

HYDROGRAPH TIME DATA

```

NMIN      5 MINUTES IN COMPUTATION INTERVAL
IDATE     1 0 STARTING DATE
ITIME     0000 STARTING TIME
NQ        300 NUMBER OF HYDROGRAPH ORDINATES
NDDATE    2 0 ENDING DATE
NDTIME    0055 ENDING TIME
ICENT     19 CENTURY MARK

```

```

COMPUTATION INTERVAL .06 HOURS
TOTAL TIME BASE     24.92 HOURS

```

ENGLISH UNITS

```

DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME     ACRE-FEET
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

JP MULTI-PLAN OPTION  
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION  
 RATIOS OF PRECIPITATION  
 .56 1.00

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	A-1	.06	1	FLOW	32.
				TIME	6.25
ROUTED TO					
+	A3	.06	1	FLOW	31.
				TIME	6.42
HYDROGRAPH AT					
+	A-4	.09	1	FLOW	137.
				TIME	6.08
ROUTED TO					
+	A4	.09	1	FLOW	136.
				TIME	6.08
HYDROGRAPH AT					
+	A-3	.15	1	FLOW	194.
				TIME	6.17
3 COMBINED AT					
+	DPA3	.30	1	FLOW	330.
				TIME	6.17
ROUTED TO					
+	A6	.30	1	FLOW	322.
				TIME	6.17
HYDROGRAPH AT					
+	A-11	.08	1	FLOW	131.
				TIME	6.08
ROUTED TO					
+	A11	.08	1	FLOW	128.
				TIME	6.08

HYDROGRAPH AT						
+	A-8	.08	1	FLOW	58.	154.
				TIME	6.17	6.08
2 COMBINED AT						
+	DP A8	.16	1	FLOW	94.	282.
				TIME	6.08	6.08
ROUTED TO						
+	A8	.16	1	FLOW	94.	276.
				TIME	6.17	6.08
HYDROGRAPH AT						
+	A-7	.05	1	FLOW	28.	87.
				TIME	6.08	6.08
2 COMBINED AT						
+	DP A7	.21	1	FLOW	119.	364.
				TIME	6.08	6.08
ROUTED TO						
+	A7	.21	1	FLOW	117.	359.
				TIME	6.17	6.08
HYDROGRAPH AT						
+	A-6	.04	1	FLOW	21.	64.
				TIME	6.08	6.08
3 COMBINED AT						
+	DPA6	.54	1	FLOW	225.	723.
				TIME	6.17	6.08
ROUTED TO						
+	A5	.54	1	FLOW	221.	713.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	A-9	.07	1	FLOW	29.	96.
				TIME	6.17	6.17
ROUTED TO						
+	A9	.07	1	FLOW	29.	95.
				TIME	6.17	6.17
HYDROGRAPH AT						
+	A-5	.11	1	FLOW	33.	139.
				TIME	6.17	6.08
3 COMBINED AT						
+	DPA5	.72	1	FLOW	273.	935.
				TIME	6.25	6.17



ROUTED TO

+	A10	.72	1	FLOW TIME	266. 6.25	919. 6.17
---	-----	-----	---	--------------	--------------	--------------

HYDROGRAPH AT

+	A-10	.01	1	FLOW TIME	5. 6.08	15. 6.08
---	------	-----	---	--------------	------------	-------------

2 COMBINED AT

+	DPA	.73	1	FLOW TIME	270. 6.25	933. 6.17
---	-----	-----	---	--------------	--------------	--------------

1

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME (IN)	
						DT (MIN)	PEAK (CFS)		
FOR PLAN = 1 RATIO= .00									
A3	MANE	1.25	4.28	397.50	.18	5.00	3.12	405.00	.18

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5932E+00 EXCESS= .0000E+00 OUTFLOW= .5910E+00 BASIN STORAGE= .9858E-02 PERCENT ERROR= -1.3

FOR PLAN = 1 RATIO= .00									
A3	MANE	1.75	32.23	383.25	1.02	5.00	31.41	385.00	1.03

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3276E+01 EXCESS= .0000E+00 OUTFLOW= .3277E+01 BASIN STORAGE= .1004E-01 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00									
A4	MANE	.49	41.51	365.63	.72	5.00	40.75	365.00	.72

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3296E+01 EXCESS= .0000E+00 OUTFLOW= .3296E+01 BASIN STORAGE= .3985E-04 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00									
A4	MANE	.38	136.75	365.55	2.13	5.00	136.13	365.00	2.13

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9780E+01 EXCESS= .0000E+00 OUTFLOW= .9780E+01 BASIN STORAGE= .3901E-04 PERCENT ERROR= .0

FOR PLAN = 1 RATIO= .00									
A6	MANE	2.00	89.81	372.00	.52	5.00	87.95	370.00	.52

*B' BASINS  
FUTURE CONDITIONS*

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* U.S. ARMY CORPS OF ENGINEERS
* JUN 1998
* HYDROLOGIC ENGINEERING CENTER
* VERSION 4.1
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
* RUN DATE 03FEB04 TIME 11:18:38
* (916) 756-1104
*
*****
*****

```

```

X X XXXXXXX XXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT  
PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Wolf Ranch Master Development Drainage Plan									
2	ID	B basins future development condition PN 03094									
3	ID	5-year and 100 Year, 24 hr Type IIA Storm FN bbas-f.dat									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	5	0								
6	JR	PREC	.56	1.0							
7	KK	B-1									
8	KM	RUNOFF FOR SUB-BASIN B-1									
9	BA	.0400									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100		
0.0120	0.0143										
13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390		
0.0460	0.0530										
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650		
0.7800	0.7900										
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450		
0.8500	0.8550										
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863		
0.8900	0.8938										

0.9240	0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210
0.9500	0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475
0.9750	0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725
0.9900	0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888
		21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000	
		22	LS	0	92						
		23	UD	.1070							
		24	ZZ								

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT  
 LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW  
 7 B-1

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
609 SECOND STREET *
*
DAVIS, CALIFORNIA 95616 *
* RUN DATE 03FEB04 TIME 11:18:38 *
(916) 756-1104 *
*
*****
*****

```

Wolf Ranch Master Development Drainage Plan  
 B basins future development condition PN 03094  
 5-year and 100 Year, 24 hr Type IIA Storm FN bbas-f.dat

5 IO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 2 0 ENDING DATE  
 NDTIME 0055 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION  
 NPLAN 1 NUMBER OF PLANS



```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
*
* RUN DATE 24JAN05 TIME 09:53:48 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE ; SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
1	ID	Wolf Ranch Master Development Drainage Plan									
2	ID	C basins future development condition PN 03094									
3	ID	5-year and 100 year, 24 hr Type IIA Storm									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	5	0								
6	JR	PREC	.56	1.0							
7	KK	C-1									
8	KM	RUNOFF FOR SUB-BASIN C-1									
9	BA	.0460									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143

C-BASIN DEVELOPER

13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9088	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270
18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	79								
23	UD	.1550									
24	KK	C1									
25	KM	ROUTE FLOW FROM SUB-BASIN C-1 TO C2									
26	RD	2500	0.02	.013			CIRC	4.0			
27	KK	C2									
28	KM	ROUTE FLOW FROM C1 TO DP C									
29	RD	1450	0.02	.013			CIRC	6.0			
30	KK	C-2									
31	KM	RUNOFF FROM SUB-BASIN C-2									
32	BA	.1110									
33	LS	0	79.2								
34	UD	.098									
35	KK	DPC									
36	KM	DESIGN POINT C COMBINE RUNOFF FROM SUB-BASIN C-2 AND C2									
37	HC	2									
38	KK	C-3									
39	KM	RUNOFF FROM SUB-BASIN C-3									
40	BA	.0550									
41	LS	0	79								
42	UD	.185									
43	ZZ										

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

7 C-1  
 V  
 V  
 24 C1  
 V  
 V  
 27 C2  
 .  
 .

```

30      .      C-2
      .
      .
35      DPC.....
      .
      .
38      .      C-3

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*      JUN 1998                    *
*      VERSION 4.1                 *
* RUN DATE 24JAN05 TIME 09:53:48 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET            *
* DAVIS, CALIFORNIA 95616      *
* (916) 756-1104               *
*
*****

```

Wolf Ranch Master Development Drainage Plan  
 C basins future development condition PN 03094  
 5-year and 100 year, 24 hr Type IIA Storm

```

5 IO      OUTPUT CONTROL VARIABLES
          IPRNT      5 PRINT CONTROL
          IPLOT      0 PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

```

```

IT        HYDROGRAPH TIME DATA
          NMIN      5 MINUTES IN COMEUTATION INTERVAL
          IDATE     1 0 STARTING DATE
          ITIME     0000 STARTING TIME
          NQ        300 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE    2 0 ENDING DATE
          NDTIME    0055 ENDING TIME
          ICENT     19 CENTURY MARK

```

```

          COMPUTATION INTERVAL .08 HOURS
          TOTAL TIME BASE      24.92 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME    ACRE-FEET
SURFACE AREA      ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

JP MULTI-PLAN OPTION  
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION  
RATIOS OF PRECIPITATION  
.56 1.00

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN		RATIOS APPLIED TO PRECIPITATION	
					RATIO 1	RATIO 2
HYDROGRAPH AT +	C-1	.05	1	FLOW TIME	30. 6.08	86. 6.08
ROUTED TO +	C1	.05	1	FLOW TIME	29. 6.08	86. 6.08
ROUTED TO +	C2	.05	1	FLOW TIME	27. 6.08	84. 6.08
HYDROGRAPH AT +	C-2	.11	1	FLOW TIME	84. 6.00	240. 6.00
2 COMBINED AT +	DPC	.16	1	FLOW TIME	104. 6.00	314. 6.00
HYDROGRAPH AT +	C-3	.05	1	FLOW TIME	33. 6.08	100. 6.08

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

INTERPOLATED TO  
COMPUTATION INTERVAL  
PEAK TIME TO  
PEAK

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
FOR PLAN = 1 RATIO = .00									

12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120 0.0143





```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 24JAN05 TIME 10:06:30
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Wolf Ranch Master Development Drainage Plan									
2	ID	D Basins future development condition pn 03094									
3	ID	5-year and 100 Year, 24 hr Type IIA Storm									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	5	0								
6	JR	PREC	.56	1.0							
7	KK	D-1									
8	KM	RUNOFF FOR SUB-BASIN D-1									
9	BA	.0620									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143

D-BASINS  
 DEVELOPED

13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270
18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	77.7								
23	UD	.180									
24	KK	D2									
25	KM	ROUTE FLOW FROM SUB-BASIN D-1 TO DP D2									
26	RD	1230	0.01	.013			CIRC	4.5			
27	KK	D-2									
28	KM	RUNOFF FROM SUB-BASIN D-2									
29	BA	.0360									
30	LS	0	73								
31	UD	.119									
32	KK	DPD2									
33	KM	DESIGN POINT D2 COMBINE RUNOFF FROM SUB-BASIN D-2 AND D2									
34	HC	2									
35	KK	D3									
36	KM	ROUTE FLOW FROM DP D2 TO DP D									
37	RD	3100	.026	.040			TRAP	4			
38	KK	D-3									
39	KM	RUNOFF FROM SUB-BASIN D-3									
40	BA	.0240									
41	LS	0	61								
42	UD	.380									

HEC-1 INPUT

PAGE 2

1  
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43	KK	DPD									
44	KM	DESIGN POINT D COMBINE RUNOFF FROM SUB-BASINS D-3 AND D2									
45	HC	2									
46	ZZ										

1  
 SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

7 D-1

```

      V
      V
24    D2
      .
      .
27    .          D-2
      .
      .
32    DPD2.....
      V
      V
35    D3
      .
      .
38    .          D-3
      .
      .
43    DPD.....

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   JUN 1998                   *
*   VERSION 4.1                 *
*
* RUN DATE  24JAN05  TIME 10:06:30 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
*   609 SECOND STREET          *
*   DAVIS, CALIFORNIA 95616    *
*   (916) 756-1104            *
*
*****

```

Wolf Ranch Master Development Drainage Plan  
 D Basins future development condition pn 03094  
 5-year and 100 Year, 24 hr Type IIA Storm

```

5 IO      OUTPUT CONTROL VARIABLES
          IPRNT      5  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

```

```

IT        HYDROGRAPH TIME DATA
          NMIN      5  MINUTES IN COMPUTATION INTERVAL
          IDATE     1  0  STARTING DATE
          ITIME     0000 STARTING TIME
          NQ        300 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE    2  0  ENDING DATE
          NDTIME    0055 ENDING TIME
          ICENT     19  CENTURY MARK

```

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION  
 NPLAN 1 NUMBER OF PLANS  
 JR MULTI-RATIO OPTION  
 RATIOS OF PRECIPITATION  
 .56 1.00

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION		
				RATIO 1 .56	RATIO 2 1.00	
HYDROGRAPH AT +	D-1	.06	1	FLOW TIME	35. 6.08	108. 6.08
ROUTED TO +	D2	.06	1	FLOW TIME	33. 6.08	105. 6.08
HYDROGRAPH AT +	D-2	.04	1	FLOW TIME	15. 6.08	57. 6.00
2 COMBINED AT +	DPD2	.10	1	FLOW TIME	48. 6.08	158. 6.08
ROUTED TO +	D3	.10	1	FLOW TIME	47. 6.17	155. 6.08
HYDROGRAPH AT +	D-3	.02	1	FLOW TIME	1. 6.42	11. 6.25

2 COMBINED AT	DPD	.12	1	FLOW	47.	162.
+				TIME	6.17	6.08

1

\*\*\* NORMAL END OF HEC-1 \*\*\*

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
*
* RUN DATE 24JAN05 TIME 10:25:27 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
1	ID	Wolf Ranch Master Development Drainage Plan									
2	ID	E basins future development condition PN 03094									
3	ID	5-year and 100 year, 24hr Type IIA Storm									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	5	0								
6	JR	PREC	.56	1.0							
7	KK	E-1									
8	KM	RUNOFF FOR SUB-BASIN E-1									
9	BA	.0403									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143

E-BASINS DEVELOPMENT

13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270
18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	79								
23	UD	.1450									

24 KK E5  
25 KM ROUTE FLOW FROM SUB-BASIN E-1 TO DP E5  
26 RD 360 0.010 .035 TRAP 10 4

27 KK E-6  
28 KM RUNOFF FROM SUB-BASIN E-6  
29 BA .0478  
30 LS 0 79  
31 UD .181

32 KK E6  
33 KM ROUTE FLOW FROM SUB-BASIN E-6 TO DP E5  
34 RD 1450 .010 .013 CIRC 3

35 KK E-5  
36 KM RUNOFF FROM SUB-BASIN E-5  
37 BA .0400  
38 LS 0 79  
39 UD .119

40 KK DPE5  
41 KM DESIGN POINT E5 COMBINE RUNOFF FROM SUB-BASIN E-5, E6 AND E5  
42 HC 3

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43 KK E2  
44 KM ROUTE FLOW FROM DESIGN POINT E5 TO DP E2  
45 RD 1850 .010 .013 CIRC 4.5

46 KK E-2  
47 KM RUNOFF FROM SUB-BASIN E-2  
48 BA .0520  
49 LS 0 73  
50 UD .134

51 KK DPE2  
52 KM DESIGN POINT E2 COMBINE RUNOFF FROM SUB-BASIN E-2 AND E2

53	HC	2				
54	KK	E3				
55	KM	ROUTE FLOW FROM DP E2 TO DP E				
56	RD	3150 .010 .040	TRAP	10	4	
57	KK	E-3				
58	KM	RUNOFF FROM SUB-BASIN E-3				
59	BA	.0095				
60	LS	0 61				
61	UD	.397				
62	KK	DPE				
63	KM	DESIGN POINT E COMBINE RUNOFF FROM SUB-BASIN E-3 AND E3				
64	HC	2				
65	KK	E-4				
66	KM	RUNOFF FROM SUB-BASIN E-4				
67	BA	.0423				
68	LS	0 73				
69	UD	.141				
70	ZZ					

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

```

  7      E-1
        V
        V
  24     E5
        .
        .
  27     .      E-6
        .      V
        .      V
  32     .      E6
        .      .
        .      .
  35     .      .      E-5
        .      .      .
        .      .      .
  40     DPES.....
        V
        V
  43     E2
        .
        .
  46     .      E-2
        .
  
```



```

51     DPE2.....
      V
      V
54     E3
      .
57     .           E-3
      .
62     DPE.....
      .
65     .           E-4

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   JUN 1998                 *
*   VERSION 4.1              *
*
* RUN DATE 24JAN05 TIME 10:25:27 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
*   609 SECOND STREET          *
*   DAVIS, CALIFORNIA 95616    *
*   (916) 756-1104            *
*
*****

```

Wolf Ranch Master Development Drainage Plan  
E basins future development condition EN 03094  
5-year and 100 year, 24hr Type IIA Storm

```

5 IO      OUTPUT CONTROL VARIABLES
          IPRNT      5 PRINT CONTROL
          IPLOT      0 PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMIN       5 MINUTES IN COMPUTATION INTERVAL
          IDATE      1 0 STARTING DATE
          ITIME      0000 STARTING TIME
          NQ         300 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE     2 0 ENDING DATE
          NDTIME     0055 ENDING TIME
          ICENT      19 CENTURY MARK

          COMPUTATION INTERVAL .08 HOURS
          TOTAL TIME BASE 24.92 HOURS

```

ENGLISH UNITS

DRAINAGE AREA            SQUARE MILES  
 PRECIPITATION DEPTH    INCHES  
 LENGTH, ELEVATION      FEET  
 FLOW                      CUBIC FEET PER SECOND  
 STORAGE VOLUME        ACRE-FEET  
 SURFACE AREA            ACRES  
 TEMPERATURE            DEGREES FAHRENHEIT

JP            MULTI-PLAN OPTION  
                   NPLAN            1    NUMBER OF PLANS

JR            MULTI-RATIO OPTION  
                   RATIOS OF PRECIPITATION  
                   .56            1.00

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	E-1	.04	1	FLOW	26.    77.5
				TIME	6.08   6.00
ROUTED TO					
+	E5	.04	1	FLOW	26.    76.
				TIME	6.08   6.08
HYDROGRAPH AT					
+	E-6	.05	1	FLOW	29.    87.5
				TIME	6.08   6.08
ROUTED TO					
+	E6	.05	1	FLOW	28.    85.
				TIME	6.08   6.08
HYDROGRAPH AT					
+	E-5	.04	1	FLOW	28.    82.
				TIME	6.00   6.00
3 COMBINED AT					
+	DPE5	.13	1	FLOW	80.    233.
				TIME	6.08   6.08
ROUTED TO					
+	E2	.13	1	FLOW	76.    232.
				TIME	6.08   6.08

HYDROGRAPH AT						
+	E-2	.05	1	FLOW	22.	79.
				TIME	6.08	6.00
2 COMBINED AT						
+	DPE2	.18	1	FLOW	98.	309.
				TIME	6.08	6.08
ROUTED TO						
+	E3	.18	1	FLOW	94.	301.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	E-3	.01	1	FLOW	0.	4.
				TIME	6.42	6.33
2 COMBINED AT						
+	DPE	.19	1	FLOW	94.	304.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	E-4	.04	1	FLOW	18.	63.
				TIME	6.08	6.08

1  
 \*\*\* NORMAL END OF HEC-1 \*\*\*

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 24JAN05 TIME 16:15:22
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

```

```

X X XXXXXXX XXXXX X
X X X X XX
X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Wolf Ranch Master Development Drainage Plan
2 ID F basins future development conditions PN 03094
3 ID 5-year and 100 year, 24hr Type IIA Storm FN: FBAS-F.DAT
*DIAGRAM
4 IT 5 0 0 300
5 IO 5 0
6 JR PREC .56 1.0
7 KK F-8
8 KM RUNOFF FOR SUB-BASIN F-8
9 BA .0630
10 IN 15
11 PE 4.4
12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120 0.0143

```

F. BASINS Developed

13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270
18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	71.5								
23	UD	0.22									

24 KK RF-8  
 25 KM ROUTE FLOW FROM SUB-BASIN F-8 TO DESIGN POINT F19  
 26 RD 1800 0.033 0.04 TRAP 10 6

27 KK F-1  
 28 KM RUNOFF FOR BASIN F-1  
 29 BA .1659  
 30 LS 0 61  
 31 UD .20

32 KK RF-9  
 33 KM ROUTE FLOW FROM SUB-BASIN F-1 TO DESIGN POINT F9  
 34 RD 700 0.037 0.04 TRAP 10 6

35 KK F-9  
 36 KM RUNOFF FOR BASIN F-9  
 37 BA .0430  
 38 LS 0 70  
 39 UD .16

40 KK DPF9  
 41 KM COMBINE FLOW FROM SUB-BASIN F-9 AND RF-9  
 42 HC 2

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43 KK RF-19  
 44 KM ROUTE FLOW FROM DESIGN POINT DP F9 TO DESIGN POINT F19  
 45 RD 2300 0.035 0.04 TRAP 20 6

46 KK F-19  
 47 KM RUNOFF FOR BASIN F-19  
 48 BA .1020  
 49 LS 0 73.2  
 50 UD .19

51 KK DPF19  
 52 KM COMBINE FLOW FROM SUB-BASIN F-19, RF-8 AND RF19

53	HC	3					
54	KK	RF-22					
55	KM	ROUTE FLOW FROM DESIGN POINT DP F19 TO DESIGN POINT F22					
56	RD	1800	0.033	0.04	TRAP	20	3
57	KK	F-2					
58	KM	RUNOFF FOR BASIN F-2					
59	BA	.0424					
60	LS	0	61				
61	UD	.19					
62	KK	RF-10					
63	KM	ROUTE FLOW FROM SUB-BASIN F-2 TO DESIGN POINT F10					
64	RD	850	0.059	0.04	TRAP	10	6
65	KK	F-10					
66	KM	RUNOFF FOR BASIN F-10					
67	BA	.0180					
68	LS	0	67				
69	UD	.15					
70	KK	DPF10					
71	KM	COMBINE FLOW FROM SUB-BASIN F-10 AND RF10					
72	HC	2					
73	KK	RF-18A					
74	KM	ROUTE FLOW FROM DESIGN POINT DP F10 TO DESIGN POINT F18					
75	RD	1800	0.037	0.04	TRAP	10	6
76	KK	F-3					
77	KM	RUNOFF FOR SUB-BASIN F-3					
78	BA	.0942					
79	LS	0	61				
80	UD	.22					
81	KK	RF-11					
82	KM	ROUTE FLOW FROM SUB-BASIN F-3 TO DESIGN POINT F11					
83	RD	950	0.038	0.04	TRAP	10	6
					HEC-1 INPUT		
	LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10					
84	KK	F-11					
85	KM	RUNOFF FOR SUB-BASIN F-11					
86	BA	.0460					
87	LS	0	68.2				
88	UD	.17					
89	KK	DPF11					
90	KM	COMBINE FLOW FROM SUB-BASIN F-11 AND RF-11					

```

91      HC      2
92      KK      RF-18
93      KM      ROUTE FLOW FROM DESIGN POINT F11 TO DESIGN POINT F18
94      RD      1800  0.037  0.04      TRAP      10      6

95      KK      F-4
96      KM      RUNOFF FOR SUB-BASIN F-4
97      BA      .2681
98      LS      0      61
99      UD      .28

100     KK      RF-12
101     KM      ROUTE FLOW FROM SUB-BASIN F-4 TO DESIGN POINT F12
102     RD      1150  0.044  0.04      TRAP      10      6

103     KK      F-5
104     KM      RUNOFF FOR SUB-BASIN F-5
105     BA      .1073
106     LS      0      61
107     UD      .34

108     KK      RF-12A
109     KM      ROUTE FLOW FROM SUB-BASIN F-5 TO DESIGN POINT F12
110     RD      1600  0.035  0.04      TRAP      10      6

111     KK      F-12
112     KM      RUNOFF FOR SUB-BASIN F-12
113     BA      .0590
114     LS      0      69.3
115     UD      .20

116     KK      DPF12
117     KM      COMBINE FLOW FROM SUB-BASIN RF-12, RF-12A, AND F-12
118     HC      3

119     KK      RF-17
120     KM      ROUTE FLOW FROM DESIGN POINT F-12 TO DESIGN POINT F18
121     RD      1900  0.028  0.04      TRAP      10      6

122     KK      F-17
123     KM      RUNOFF FOR SUB-BASIN F-17
124     BA      .0380
125     LS      0      60.1
126     UD      .21

```

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

127     KK      F-18
128     KM      RUNOFF FOR SUB-BASIN F-18

```

129	BA	.0980					
130	LS	0	73.1				
131	UD	.21					
132	KK	DPF18					
133	KM	COMBINE FLOW FROM SUB-BASINS F-18 AND F17, AND RF-18A, RF-18 AND RF-17					
134	HC	5					
135	KK	RF-22A					
136	KM	ROUTE FLOW FROM DESIGN POINT F-18 TO DESIGN POINT F22					
137	RD	1800	0.027	0.04	TRAP	10	6
138	KK	F-22					
139	KM	RUNOFF FOR SUB-BASIN F-22					
140	BA	.0640					
141	LS	0	64.1				
142	UD	.21					
143	KK	DPF22					
144	KM	COMBINE FLOW FROM SUB-BASIN F-22, RF-22 AND RF-22A					
145	HC	3					
146	KK	RF-27A					
147	KM	ROUTE FLOW FROM DESIGN POINT F-22 TO DESIGN POINT F27A					
148	RD	500	0.029	0.04	TRAP	10	6
149	KK	F-16					
150	KM	RUNOFF FOR SUB-BASIN F-16					
151	BA	.0270					
152	LS	0	72.8				
153	UD	.21					
154	KK	RF-16					
155	KM	ROUTE FLOW FROM SUB-BASIN F-16 TO DESIGN POINT F27A					
156	RD	2000	0.030	0.04	TRAP	10	6
157	KK	DPF27A					
158	KM	COMBINE FLOW FROM RF-16 AND RF-27A					
159	HC	2					
160	KK	RF-27B					
161	KM	ROUTE FLOW FROM DESIGN POINT F27A TO DESIGN POINT F27					
162	RD	3150	0.020	0.04	TRAP	10	6
163	KK	F-26					
164	KM	RUNOFF FOR SUB-BASIN F-26					
165	BA	.0520					
166	LS	0	79				
167	UD	.19					

HEC-1 INPUT

PAGE 5

1

LINE

ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10



168	KK	RF-26A					
169	KM	ROUTE FLOW FROM SUB-BASIN F-26 TO DESIGN POINT F27					
170	RD	1250	0.013	0.04	TRAP	10	6
171	KK	DPF27					
172	KM	COMBINE FLOW FROM RF-27B AND RF-26A					
173	HC	2					
174	KK	RF-27C					
175	KM	ROUTE FLOW FROM DESIGN POINT F27 TO DESIGN POINT F28					
176	RD	1400	0.019	0.04	TRAP	50	3
177	KK	F-7					
178	KM	RUNOFF FOR SUB-BASIN F-7					
179	BA	.0782					
180	LS	0	61				
181	UD	.19					
182	KK	RF-7					
183	KM	ROUTE FLOW FROM SUB-BASIN F-7 TO DESIGN POINT F14					
184	RD	1200	0.033	0.04	TRAP	10	6
185	KK	F-14					
186	KM	RUNOFF FOR SUB-BASIN F-14					
187	BA	.1290					
188	LS	0	73.0				
189	UD	.23					
190	KK	F-6					
191	KM	RUNOFF FOR SUB-BASIN F-6					
192	BA	.0310					
193	LS	0	61				
194	UD	.19					
195	KK	RF-13					
196	KM	ROUTE FLOW FROM SUB-BASIN F-6 TO DESIGN POINT F13					
197	RD	800	0.038	0.04	TRAP	10	6
198	KK	F-13					
199	KM	RUNOFF FOR SUB-BASIN F-13					
200	BA	.0140					
201	LS	0	61				
202	UD	.14					
203	KK	DPF13					
204	KM	COMBINE FLOW FROM RF-13 AND F-13					
205	HC	2					
206	KK	RF-14					
207	KM	ROUTE FLOW FROM DESIGN POINT F13 TO DESIGN POINT F14					

LINE	ID	1	2	3	4	5	6	7	8	9	10
208	RD	3600	0.027	0.04				TRAP	20	6	
								HEC-1 INPUT			
209	KK	DPF14									
210	KM	COMBINE FLOW FROM RF-7, F-14, AND RF-14									
211	HC	3									
212	KK	RF-25									
213	KM	ROUTE FLOW FROM DESIGN POINT F14 TO DESIGN POINT F25							TRAP	20	6
214	RD	2600	0.023	0.04							
215	KK	F-25									
216	KM	RUNOFF FOR SUB-BASIN F-25									
217	BA	.0890									
218	LS	0	74.1								
219	UD	.28									
220	KK	DPF25									
221	KM	COMBINE FLOW FROM RF-25 AND RF-14									
222	HC	2									
223	KK	RF-30									
224	KM	ROUTE FLOW FROM DESIGN POINT F25 TO DESIGN POINT F30							TRAP	20	6
225	RD	900	0.027	0.024							
226	KK	F-15									
227	KM	RUNOFF FOR SUB-BASIN F-15									
228	BA	.021									
229	LS	0	69.1								
230	UD	.16									
231	KK	RF-23									
232	KM	ROUTE FLOW FROM SUB-BASIN F15 TO DESIGN POINT F23							TRAP	10	3
233	RD	1200	0.023	0.04							
234	KK	F-23									
235	KM	RUNOFF FOR SUB-BASIN F-23									
236	BA	.0310									
237	LS	0	73.0								
238	UD	.18									
239	KK	DPF23									
240	KM	COMBINE FLOW FROM RF-23 AND F-23									
241	HC	2									
242	KK	RF-24									
243	KM	ROUTE FLOW FROM DESIGN POINT F23 TO DESIGN POINT F24							TRAP	10	6
244	RD	2250	0.026	0.04							

1

245 KK F-24  
 246 KM RUNOFF FOR SUB-BASIN F-24  
 247 BA .0890  
 248 LS 0 79  
 249 UD .26

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

250 KK DFF24  
 251 KM COMBINE FLOW FROM RF-24 AND F-24  
 252 HC 2

253 KK RF-30A  
 254 KM ROUTE FLOW FROM DESIGN POINT F24 TO DESIGN POINT F30  
 255 RD 1100 0.033 0.04 TRAP 10 6

256 KK F-30  
 257 KM RUNOFF FOR SUB-BASIN F-30  
 258 BA .0220  
 259 LS 0 77.7  
 260 UD .18

261 KK DFF30  
 262 KM COMBINE FLOW FROM RF-30, RF-30A, AND F-30  
 263 HC 3

264 KK RF-29  
 265 KM ROUTE FLOW FROM DESIGN POINT F30 TO DESIGN POINT F29  
 266 RD 2350 0.027 0.04 TRAP 6 3

267 KK F-29  
 268 KM RUNOFF FOR SUB-BASIN F-29  
 269 BA .0250  
 270 LS 0 70  
 271 UD .19

272 KK DFF29  
 273 KM COMBINE FLOW FROM RF-29 AND F-29  
 274 HC 2

275 KK RF-28  
 276 KM ROUTE FLOW FROM DESIGN POINT F29 TO DESIGN POINT F28  
 277 RD 750 0.015 0.04 TRAP 20 3

278 KK F-28  
 279 KM RUNOFF FOR SUB-BASIN F-28  
 280 BA .042  
 281 LS 0 68  
 282 UD .23

283 KK F-27  
 284 KM RUNOFF FOR SUB-BASIN F-27  
 285 BA .213  
 286 LS 0 76.2  
 287 UD .32  
  
 288 KK DPF28  
 289 KM COMBINE FLOW FROM RF-27C, RF-28, F-28 AND F-27  
 290 HC 4

1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

291 KK RF-31  
 292 KM ROUTE FLOW FROM DESIGN POINT F28 TO DESIGN POINT F  
 293 RD 3500 0.023 0.04 TRAP 100 3  
  
 294 KK F-31  
 295 KM RUNOFF FOR SUB-BASIN F-31  
 296 BA .0810  
 297 LS 0 67.8  
 298 UD .24  
  
 299 KK DP F  
 300 KM COMBINE FLOW FROM RF-31 AND F-31  
 301 HC 2  
 302 ZZ

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW  
  
 7 F-8  
 V  
 V  
 24 RF-8  
 .  
 .  
 27 . F-1  
 . V  
 . V  
 32 . RF-9  
 .  
 .  
 35 . F-9  
 .  
 .  
 40 . DPF9.....  
 . V

43	.	V		
	.	RF-19		
	.	.		
46	.	.	F-19	
	.	.	.	
51	DPF19	.....		
	V			
	V			
54	RF-22			
	.			
57	.	F-2		
	.	V		
	.	V		
62	.	RF-10		
	.	.		
65	.	.	F-10	
	.	.	.	
70	.	DPF10	.....	
	.	V		
	.	V		
73	.	RF-18A		
	.	.		
76	.	.	F-3	
	.	.	V	
	.	.	V	
81	.	.	RF-11	
	.	.	.	
84	.	.	.	F-11
	.	.	.	.
89	.	.	DPF11	.....
	.	.	V	
	.	.	V	
92	.	.	RF-18	
	.	.	.	
95	.	.	.	F-4
	.	.	.	V
	.	.	.	V
100	.	.	.	RF-12
	.	.	.	.
103	.	.	.	.
	.	.	.	F-5
	.	.	.	V
	.	.	.	V

108	.	.	.	.	RF-12A	.
	.	.	.	.	.	.
111	.	.	.	.	.	F-12
	.	.	.	.	.	.
116	.	.	.	DPF12	.....	.
	.	.	.	V		.
	.	.	.	V		.
119	.	.	.	RF-17		.
	.	.	.	.		.
122	.	.	.	.	F-17	.
	.	.	.	.	.	.
127	.	.	.	.	.	F-18
	.	.	.	.	.	.
132	.	DPF18	.....	.	.	.
	.	V		.	.	.
	.	V		.	.	.
135	.	RF-22A		.	.	.
	.	.		.	.	.
138	.	.	F-22	.	.	.
	.	.	.	.	.	.
143	DPF22	.....	.	.	.	.
	V		.	.	.	.
	V		.	.	.	.
146	RF-27A		.	.	.	.
	.		.	.	.	.
149	.	F-16	.	.	.	.
	.	V	.	.	.	.
	.	V	.	.	.	.
154	.	RF-16	.	.	.	.
	.	.	.	.	.	.
157	DPF27A	.....	.	.	.	.
	V		.	.	.	.
	V		.	.	.	.
160	RF-27B		.	.	.	.
	.		.	.	.	.
163	.	F-26	.	.	.	.
	.	V	.	.	.	.
	.	V	.	.	.	.
168	.	RF-26A	.	.	.	.
	.	.	.	.	.	.
171	DPF27	.....	.	.	.	.

174	V			
	V			
	RF-27C			
177	.	F-7		
	.	V		
	.	V		
182	.	RF-7		
	.	.		
185	.	.	F-14	
	.	.	.	
190	.	.	.	F-6
	.	.	.	V
	.	.	.	V
195	.	.	.	RF-13
	.	.	.	.
198	.	.	.	F-13
	.	.	.	.
	.	.	.	.
203	.	.	.	DPF13.....
	.	.	.	V
	.	.	.	V
206	.	.	.	RF-14
	.	.	.	.
	.	.	.	.
209	.	DPF14.....	.	.
	.	V	.	.
	.	V	.	.
212	.	RF-25	.	.
	.	.	.	.
215	.	.	F-25	.
	.	.	.	.
	.	.	.	.
220	.	DPF25.....	.	.
	.	V	.	.
	.	V	.	.
223	.	RF-30	.	.
	.	.	.	.
226	.	.	F-15	.
	.	.	V	.
	.	.	V	.
231	.	.	RF-23	.
	.	.	.	.
	.	.	.	.
234	.	.	.	F-23
	.	.	.	.

239	.	.	.	DPF23.....	.
	.	.	.	V	.
	.	.	.	V	.
242	.	.	.	RF-24	.
	.	.	.	.	.
245	.	.	.	.	F-24
	.	.	.	.	.
250	.	.	.	DPF24.....	.
	.	.	.	V	.
	.	.	.	V	.
253	.	.	.	RF-30A	.
	.	.	.	.	.
256	.	.	.	.	F-30
	.	.	.	.	.
261	.	.	.	DPF30.....	.
	.	.	.	V	.
	.	.	.	V	.
264	.	.	.	RF-29	.
	.	.	.	.	.
267	.	.	.	.	F-29
	.	.	.	.	.
272	.	.	.	DPF29.....	.
	.	.	.	V	.
	.	.	.	V	.
275	.	.	.	RF-28	.
	.	.	.	.	.
278	.	.	.	.	F-28
	.	.	.	.	.
283	.	.	.	.	F-27
	.	.	.	.	.
288	.	.	.	DPF28.....	.
	.	.	.	V	.
	.	.	.	V	.
291	.	.	.	RF-31	.
	.	.	.	.	.
294	.	.	.	.	F-31
	.	.	.	.	.
299	.	.	.	DP F.....	.

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION



```

*****
+
+ FLOOD HYDROGRAPH PACKAGE (HEC-1) +
+ JUN 1998 +
+ VERSION 4.1 +
+ RUN DATE 24JAN05 TIME 16:15:22 +
+
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

Wolf Ranch Master Development Drainage Plan  
 F basins future development conditions PN 03094  
 5-year and 100 year, 24hr Type IIA Storm FN: FBAS-F.DAT

```

5 IO OUTPUT CONTROL VARIABLES
      IPRNT      5 PRINT CONTROL
      IPLOT      0 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE

```

```

IT HYDROGRAPH TIME DATA
      NMIN      5 MINUTES IN COMPUTATION INTERVAL
      IDATE      1 0 STARTING DATE
      ITIME      0000 STARTING TIME
      NQ         300 NUMBER OF HYDROGRAPH ORDINATES
      NDDATE     2 0 ENDING DATE
      NDTIME     0055 ENDING TIME
      ICENT      19 CENTURY MARK

```

```

      COMPUTATION INTERVAL .08 HOURS
      TOTAL TIME BASE 24.92 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

```

```

JP MULTI-PLAN OPTION
      NPLAN      1 NUMBER OF PLANS

```

```

JR MULTI-RATIO OPTION
      RATIOS OF PRECIPITATION
      .56      1.00

```

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN		RATIOS APPLIED TO PRECIPITATION	
					RATIO 1 .56	RATIO 2 1.00
HYDROGRAPH AT +	F-8	.06	1	FLOW TIME	18. 6.17	76. 6.08
ROUTED TO +	RF-8	.06	1	FLOW TIME	18. 6.25	74. 6.17
HYDROGRAPH AT +	F-1	.17	1	FLOW TIME	10. 6.17	110. 6.08
ROUTED TO +	RF-9	.17	1	FLOW TIME	10. 6.25	106. 6.17
HYDROGRAPH AT +	F-9	.04	1	FLOW TIME	13. 6.08	55. 6.08
2 COMBINED AT +	DFF9	.21	1	FLOW TIME	20. 6.17	157. 6.08
ROUTED TO +	RF-19	.21	1	FLOW TIME	19. 6.33	153. 6.17
HYDROGRAPH AT +	F-19	.10	1	FLOW TIME	38. 6.08	144. 6.08
3 COMBINED AT +	DPF19	.37	1	FLOW TIME	61. 6.25	350. 6.17
ROUTED TO +	RF-22	.37	1	FLOW TIME	59. 6.25	338. 6.17
HYDROGRAPH AT +	F-2	.04	1	FLOW TIME	3. 6.17	29. 6.08

ROUTED TO						
+	RF-10	.04	1	FLOW TIME	3. 6.25	28. 6.17
HYDROGRAPH AT						
+	F-10	.02	1	FLOW TIME	4. 6.08	20. 6.08
2 COMBINED AT						
+	DPF10	.06	1	FLOW TIME	6. 6.17	46. 6.08
ROUTED TO						
+	RF-18A	.06	1	FLOW TIME	5. 6.33	45. 6.17
HYDROGRAPH AT						
+	F-3	.09	1	FLOW TIME	5. 6.17	59. 6.17
ROUTED TO						
+	RF-11	.09	1	FLOW TIME	5. 6.25	58. 6.17
HYDROGRAPH AT						
+	F-11	.05	1	FLOW TIME	11. 6.08	53. 6.08
2 COMBINED AT						
+	DPF11	.14	1	FLOW TIME	13. 6.17	102. 6.08
ROUTED TO						
+	RF-18	.14	1	FLOW TIME	13. 6.25	102. 6.17
HYDROGRAPH AT						
+	F-4	.27	1	FLOW TIME	13. 6.25	147. 6.17
ROUTED TO						
+	RF-12	.27	1	FLOW TIME	13. 6.33	144. 6.25
HYDROGRAPH AT						
+	F-5	.11	1	FLOW TIME	5. 6.33	52. 6.25
ROUTED TO						
+	RF-12A	.11	1	FLOW TIME	5. 6.50	51. 6.33

HYDROGRAPH AT						
+	F-12	.06	1	FLOW TIME	14. 6.08	67. 6.08
3 COMBINED AT						
+	DPF12	.43	1	FLOW TIME	24. 6.25	236. 6.25
ROUTED TO						
+	RF-17	.43	1	FLOW TIME	24. 6.42	234. 6.25
HYDROGRAPH AT						
+	F-17	.04	1	FLOW TIME	2. 6.17	23. 6.08
HYDROGRAPH AT						
+	F-18	.10	1	FLOW TIME	33. 6.08	131. 6.08
5 COMBINED AT						
+	DPF18	.77	1	FLOW TIME	64. 6.25	490. 6.17
ROUTED TO						
+	RF-22A	.77	1	FLOW TIME	62. 6.33	486. 6.25
HYDROGRAPH AT						
+	F-22	.06	1	FLOW TIME	7. 6.17	51. 6.08
3 COMBINED AT						
+	DPF22	1.21	1	FLOW TIME	126. 6.33	850. 6.25
ROUTED TO						
+	RF-27A	1.21	1	FLOW TIME	125. 6.33	846. 6.25
HYDROGRAPH AT						
+	F-16	.03	1	FLOW TIME	9. 6.08	36. 6.08
ROUTED TO						
+	RF-16	.03	1	FLOW TIME	9. 6.25	34. 6.17
2 COMBINED AT						
+	DPF27A	1.24	1	FLOW TIME	133. 6.33	880. 6.25

ROUTED TO +	RF-27B	1.24	1	FLOW TIME	131. 6.42	864. 6.33
HYDROGRAPH AT +	F-26	.05	1	FLOW TIME	31. 6.08	94. 6.08
ROUTED TO +	RF-26A	.05	1	FLOW TIME	30. 6.17	90. 6.17
2 COMBINED AT +	DPF27	1.29	1	FLOW TIME	145. 6.42	916. 6.33
ROUTED TO +	RF-27C	1.29	1	FLOW TIME	142. 6.50	913. 6.33
HYDROGRAPH AT +	F-7	.08	1	FLOW TIME	5. 6.17	54. 6.08
ROUTED TO +	RF-7	.08	1	FLOW TIME	5. 6.25	53. 6.17
HYDROGRAPH AT +	F-14	.13	1	FLOW TIME	42. 6.17	162. 6.08
HYDROGRAPH AT +	F-6	.03	1	FLOW TIME	2. 6.17	21. 6.08
ROUTED TO +	RF-13	.03	1	FLOW TIME	2. 6.25	21. 6.17
HYDROGRAPH AT +	F-13	.01	1	FLOW TIME	1. 6.08	11. 6.08
2 COMBINED AT +	DPF13	.05	1	FLOW TIME	3. 6.17	30. 6.08
ROUTED TO +	RF-14	.05	1	FLOW TIME	4. 6.75	30. 6.33

+ 3 COMBINED AT	DPF14	.25	1	FLOW TIME	45. 6.17	210. 6.17
ROUTED TO						
+ ROUTED TO	RF-25	.25	1	FLOW TIME	44. 6.33	209. 6.25
HYDROGRAPH AT						
+ HYDROGRAPH AT	F-25	.09	1	FLOW TIME	29. 6.17	108. 6.17
2 COMBINED AT						
+ 2 COMBINED AT	DPF25	.34	1	FLOW TIME	67. 6.25	306. 6.17
ROUTED TO						
+ ROUTED TO	RF-30	.34	1	FLOW TIME	67. 6.33	305. 6.25
HYDROGRAPH AT						
+ HYDROGRAPH AT	F-15	.02	1	FLOW TIME	6. 6.08	26. 6.08
ROUTED TO						
+ ROUTED TO	RF-23	.02	1	FLOW TIME	5. 6.17	25. 6.17
HYDROGRAPH AT						
+ HYDROGRAPH AT	F-23	.03	1	FLOW TIME	12. 6.08	44. 6.08
2 COMBINED AT						
+ 2 COMBINED AT	DPF23	.05	1	FLOW TIME	16. 6.17	68. 6.08
ROUTED TO						
+ ROUTED TO	RF-24	.05	1	FLOW TIME	15. 6.25	65. 6.17
HYDROGRAPH AT						
+ HYDROGRAPH AT	F-24	.09	1	FLOW TIME	45. 6.17	137. 6.17
2 COMBINED AT						
+ 2 COMBINED AT	DPF24	.14	1	FLOW TIME	55. 6.25	202. 6.17
ROUTED TO						
+ ROUTED TO	RF-30A	.14	1	FLOW TIME	54. 6.25	196. 6.17

HYDROGRAPH AT						
+	F-30	.02	1	FLOW TIME	12. 6.08	38. 6.08
3 COMBINED AT						
+	DPF30	.50	1	FLOW TIME	124. 6.25	517. 6.17
ROUTED TO						
+	RF-29	.50	1	FLOW TIME	122. 6.33	514. 6.25
HYDROGRAPH AT						
+	F-29	.03	1	FLOW TIME	7. 6.08	30. 6.08
2 COMBINED AT						
+	DPF29	.53	1	FLOW TIME	125. 6.33	532. 6.25
ROUTED TO						
+	RF-28	.53	1	FLOW TIME	123. 6.42	519. 6.25
HYDROGRAPH AT						
+	F-28	.04	1	FLOW TIME	8. 6.17	40. 6.08
HYDROGRAPH AT						
+	F-27	.21	1	FLOW TIME	75. 6.25	264. 6.17
4 COMBINED AT						
+	DPF28	2.07	1	FLOW TIME	304. 6.42	1659. 6.33
ROUTED TO						
+	RF-31	2.07	1	FLOW TIME	302. 6.58	1622. 6.42
HYDROGRAPH AT						
+	F-31	.08	1	FLOW TIME	15. 6.17	75. 6.17
2 COMBINED AT						
+	DP F	2.15	1	FLOW TIME	307. 6.58	1654. 6.42

1

\*\*\* NORMAL END OF HEC-1 \*\*\*

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 27JAN05 TIME 10:00:05
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Wolf Ranch Master Development Drainage Plan									
2	ID	G Basins Future developed condition								PN 03094	
3	ID	5-year and 100 Year, 24 hr Type IIA Storm FN Gbas-f.dat									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	4	0								
6	JR	PREC	.56	1.0							
7	KK	G-1									
8	KM	RUNOFF - Sub-basin G-1									
9	BA	.0808									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143

G-BASINS DEVELOPED



13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270
18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	61								
23	UD	0.22									

24	KK	G2									
25	KM		ROUTE FLOW from SUB-BASIN G-1 TO DP G3								
26	RD	3200	0.027	0.04		TRAP	10		4		

27	KK	G-2									
28	KM		RUNOFF - Sub-basin G-2								
29	BA	.035									
30	LS	0	73								
31	UD	0.22									

32	KK	G3									
33	KM		ROUTE FLOW from SUB-BASIN G-2 TO DP G3								
34	RD	2730	0.024	0.04		TRAP	10		4		

35	KK	G-3									
36	KM		RUNOFF - Sub-basin G-3								
37	BA	.177									
38	LS	0	73								
39	UD	0.29									

40	KK	DPG3									
41	KM		COMBINE RUNOFF from G2, G3 AND SUB-BASIN G-3								
42	HC	3									

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43	KK	G5									
44	KM		ROUTE FLOW from DP G3 TO DP G5								
45	RD	2200	0.02	.013		CIRC	4.5				

46	KK	G-5									
47	KM		RUNOFF - Sub-basin G-5								
48	BA	.153									
49	LS	0	79.8								
50	UD	0.26									

51	KK	DPG									
52	KM		COMBINE RUNOFF from G5 AND SUB-BASIN G-5								

53 HC 2  
54 ZZ

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

7	G-1		
	V		
	V		
24	G2		
	.		
27	.	G-2	
	.	V	
	.	V	
32	.	G3	
	.	.	
	.	.	
35	.	.	G-3
	.	.	.
	.	.	.
40	DPG3.....		
	V		
	V		
43	G5		
	.		
	.		
46	.	G-5	
	.	.	
	.	.	
51	DPG.....		

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

1\*\*\*\*\*  
\*  
\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
\* JUN 1998 \*  
\* VERSION 4.1 \*  
\*  
\* RUN DATE 27JAN05 TIME 10:00:05 \*  
\*  
\*\*\*\*\*

\*\*\*\*\*  
\*  
\* U.S. ARMY CORPS OF ENGINEERS \*  
\* HYDROLOGIC ENGINEERING CENTER \*  
\* 609 SECOND STREET \*  
\* DAVIS, CALIFORNIA 95616 \*  
\* (916) 756-1104 \*  
\*\*\*\*\*

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS.

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT +	G-1	.08	1	FLOW TIME	5. 6.17
					50. 6.17
ROUTED TO +	G2	.08	1	FLOW TIME	4. 6.58
					50. 6.25
HYDROGRAPH AT +	G-2	.04	1	FLOW TIME	12. 6.17
					45. 6.08
ROUTED TO +	G3	.04	1	FLOW TIME	12. 6.33
					44. 6.25
HYDROGRAPH AT +	G-3	.18	1	FLOW TIME	50. 6.17
					200. 6.17
3 COMBINED AT +	DPG3	.29	1	FLOW TIME	57. 6.25
					278. 6.25
ROUTED TO +	G5	.29	1	FLOW TIME	55. 6.33
					277. 6.25
HYDROGRAPH AT +	G-5	.15	1	FLOW TIME	83. 6.17
					243. 6.17
2 COMBINED AT +	DPG	.45	1	FLOW TIME	129. 6.17
					502. 6.17

1

\*\*\* NORMAL END OF HEC-1 \*\*\*

H-J Basins Developed

```

*****
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
*
CALIFORNIA 95616 *
* RUN DATE 21MAY04 TIME 15:11:47 *
756-1104 *
*
*****
*****

```

```

*
* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,
* (916)
*

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

HEC1KW. THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1  
PAGE 1

HEC-1 INPUT

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Wolf Ranch master Development Drainage Plan
2 ID H AND J Basins developed conditions PN 03094
3 ID 5-year and 100 Year, 24 hr Type IIA Storm FN hjbas-f.dat
4 *DIAGRAM
IT 5 0 0 300
5 IO 4 0
6 JR PREC .56 1.0
7 KK H-1
8 KM
9 BA .0370 RUNOFF FROM SUB-BASIN H-1
10 IN 15
11 PB 4.4
12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120 0.0143
13 PC 0.0165 0.0188 0.0210 0.0233 0.0255 0.0278 0.0320 0.0390 0.0460 0.0530
14 PC 0.0600 0.0750 0.1000 0.4000 0.7000 0.7250 0.7500 0.7650 0.7800 0.7900
15 PC 0.8000 0.8100 0.8200 0.8250 0.8300 0.8350 0.8400 0.8450 0.8500 0.8550
16 PC 0.8600 0.8638 0.8675 0.8713 0.8750 0.8788 0.8825 0.8863 0.8900 0.8938
17 PC 0.8975 0.9013 0.9050 0.9083 0.9115 0.9148 0.9180 0.9210 0.9240 0.9270

```



5 IO            OUTPUT CONTROL VARIABLES  
                 IPRNT            4    PRINT CONTROL  
                 IPLOT            0    PLOT CONTROL  
                 QSCAL            0.    HYDROGRAPH PLOT SCALE

IT            HYDROGRAPH TIME DATA  
                 NMIN            5    MINUTES IN COMPUTATION INTERVAL  
                 IDATE            1    0    STARTING DATE  
                 ITIME            0000 STARTING TIME  
                 NQ                300    NUMBER OF HYDROGRAPH ORDINATES  
                 NDDATE           2    0    ENDING DATE  
                 NDTIME           0055 ENDING TIME  
                 ICENT            19    CENTURY MARK  
  
                 COMPUTATION INTERVAL    .08 HOURS  
                 TOTAL TIME BASE        24.92 HOURS

ENGLISH UNITS  
   DRAINAGE AREA            SQUARE MILES  
   PRECIPITATION DEPTH      INCHES  
   LENGTH, ELEVATION        FEET  
   FLOW                      CUBIC FEET PER SECOND  
   STORAGE VOLUME            ACRE-FEET  
   SURFACE AREA              ACRES  
   TEMPERATURE                DEGREES FAHRENHEIT

JP            MULTI-PLAN OPTION  
                 NPLAN            1    NUMBER OF PLANS

JR            MULTI-RATIO OPTION  
                 RATIOS OF PRECIPITATION  
                 .56            1.00

\*\*\* \*\*  
 : \*\* \*\*

\*\*\*\*\*  
 \*            \*

RATIOS APPLIED TO PRECIPITATION						
OPERATION	STATION	AREA	PLAN		RATIO 1	RATIO 2
					.56	1.00
HYDROGRAPH AT						
+	H-1	.04	1	FLOW	17.	63.
				TIME	6.00	6.00
HYDROGRAPH AT						
+	H-2	.07	1	FLOW	25.	96.
				TIME	6.08	6.08
HYDROGRAPH AT						
+	J-1	.03	1	FLOW	19.	53.
				TIME	6.00	6.00
HYDROGRAPH AT						
+	J-2	.05	1	FLOW	30.	92.
				TIME	6.08	6.08

\*\*\* NORMAL END OF HEC-1 \*\*\*

**HEC-1 INPUT & OUTPUT  
DEVELOPED CONDITIONS WITH DETENTION**

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 11FEB05 TIME 10:13:10 *
*****
*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

```

```

X X XXXXXXXX XXXXX X
X X X X XX
X X X X X
XXXXXXXX XXXX XXXXX X
X X X X X X
X X X X X X
X X XXXXXXXX XXXXX XXXX

```

*A-Break Determined*

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DE, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION. NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPRT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Wolf Ranch, Master Developed Drainage Plan pn 03094
2 ID A Basins, future development condition w/detention a-det.dat
3 ID 5-year and 100 Year, 24 hr Type IIA Storm
  *DIAGRAM
4 IT 5 0 0 300
5 IO 5 0
6 JR PREC .56 1.0
7 KK A-1
8 KM RUNOFF FROM SUB-BASIN A-1
9 BA .060
10 IN 15
11 PB 4.4
12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120 0.0143

```



13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270
18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	61								
23	UD	.292									

24	KK	A3									
25	KM	ROUTE FLOW FROM SUB-BASIN A-1 TO DP A3									
26	RD	3500	.021	0.04		TRAP	10		4		

27	KK	A-4									
28	KM	RUNOFF FROM SUB-BASIN A-4									
29	BA	.0861									
30	LS	0	77								
31	UD	0.21									

32	KK	A4									
33	KM	ROUTE RUNOFF FROM A-4 TO TO DP A3									
34	RD	450	.02	.013		CIRC	3.5				

35	KK	A-3									
36	KM	RUNOFF FROM SUB-BASIN A-3									
37	BA	.1500									
38	LS	0	73								
39	UD	.221									

40	KK	DPA3									
41	KM	DESIGN POINT A3 COMBINE RUNOFF FROM SUB-BASIN A-3, A3 AND A4									
42	HC	3									

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43	KK	A6									
44	KM	ROUTE FLOW FROM DP A3 TO DP A6									
45	RD	1550	.016	0.04		TRAP	10		4		

46	KK	A-11									
47	KM	RUNOFF FROM SUB-BASIN A-11									
48	BA	.081									
49	LS	0	76.3								
50	UD	.19									

51	KK	A11									
52	KM	ROUTE SUB-BASIN A-11 TO DP A8									

53	RD	1400	.02	.013	CIRC	3.5
54	KK	A-8				
55	KM	RUNOFF FROM BASIN A-8				
56	BA	.079				
57	LS	0	84.1			
58	UD	.250				
59	KK	DP A8				
60	KM	COMBINE RUNOFF FROM SB A-8 AND A11				
61	HC	2				
62	KK	A8				
63	KM	ROUTE FLOW FROM SUB-BASIN A-8 TO DP A7				
64	RD	1100	.02	.013	CIRC	4.5
65	KK	A-7				
66	KM	RUNOFF FROM SUB-BASIN A-7				
67	BA	.0500				
68	LS	0	77.5			
69	UD	.172				
70	KK	DP A7				
71	KM	COMBINE RUNOFF FROM SUB-BASIN A-7 AND A8				
72	HC	2				
73	KK	A7				
74	KM	ROUTE FLOW FROM DP A7 TO DP A6				
75	RD	800	0.02	0.013	CIRC	5
76	KK	A-6				
77	KM	RUNOFF FROM SUB-BASIN A-6				
78	BA	.037				
79	LS	0	79			
80	UD	.21				
81	KK	DPA6				
82	KM	DESIGN POINT A6 COMBINE RUNOFF FROM SUB-BASIN A-6, A6 AND A7				
83	HC	3				

HEC-1 INPUT

1

LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
84	KK	A5									
85	KM	ROUTE FLOW FROM DESIGN POINT A6 TO DP A5									
86	RD	2200	.011	.04	TRAP	10	4				
87	KK	A-9									
88	KM	RUNOFF FROM SUB-BASIN A-9									
89	BA	.0673									
90	LS	0	77.1								

91	UD	.263					
92	KK	A9					
93	KM	ROUTE FLOW FROM SUB-BASIN A-9 TO DESIGN POINT A5					
94	RD	500	.02	.016	CIRC	3.5	
95	KK	A-5					
96	KM	RUNOFF FROM SUB-BASIN A-5					
97	BA	.1114					
98	LS	0	71.6				
99	UD	.209					
100	KK	DPA5					
101	KM	DP A5 COMBINE RUNOFF FROM SUB-BASIN A-5, A5 AND A9 THIS IS INFLOW					
102	KM	TO DETENTION BASIN A					
103	HC	3					
104	KK	DBA					
105	KM	ROUTE DP A5 THROUGH DETENTION BASIN A					
106	RS	1	ELEV	100			
107	SV	0	4	10	25	45	60
108	SE	100	102	104	106	108	110
109	SQ	0	10	35	80	180	500
110	KK	A10					
111	KM	ROUTE FLOW FROM DESIGN POINT A5 TO DESIGN POINT A					
112	RD	720	.021	.04	TRAP	15	4
113	KK	A-10					
114	KM	RUNOFF FROM SUB-BASIN A-10					
115	BA	.0096					
116	LS	0	79.6				
117	UD	.231					
118	KK	DPA					
119	KM	DESIGN POINT A COMBINE RUNOFF SUB-BASIN A-10 AND A10					
120	HC	2					
121	ZZ						

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT			
LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW	
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW	
7	A-1		
	V		
	V		
24	A3		
	.		
	.		
27	.	A-4	

	.	V	
	.	V	
32	.	A4	
	.	.	
	.	.	
35	.	.	A-3
	.	.	.
	.	.	.
40	DPA3	.....	.
	V		
	V		
43	A6		
	.		
	.		
46	.	A-11	
	.	V	
	.	V	
51	.	A11	
	.	.	
	.	.	
54	.	.	A-8
	.	.	.
	.	.	.
59	.	DP A8	.....
	.	V	
	.	V	
62	.	A8	
	.	.	
	.	.	
65	.	.	A-7
	.	.	.
	.	.	.
70	.	DP A7	.....
	.	V	
	.	V	
73	.	A7	
	.	.	
	.	.	
76	.	.	A-6
	.	.	.
	.	.	.
81	DPA6	.....	.
	V		
	V		
84	A5		
	.		
	.		
87	.	A-9	
	.	V	
	.	V	
92	.	A9	
	.	.	

```

95      .      .      A-5
      .      .      .
      .      .      .
100     DPAS .....
      V
      V
104     DBA
      V
      V
110     A10
      .
      .
113     .      A-10
      .      .
      .      .
118     DPA.....

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*      JUN 1998 *
*      VERSION 4.1 *
* RUN DATE 11FEB05 TIME 10:13:10 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

Wolf Ranch, Master Developed Drainage Plan pn 03094  
A Basins, future development condition w/detention a-det.dat  
5-year and 100 Year, 24 hr Type IIA Storm

```

5 IO      OUTPUT CONTROL VARIABLES
      IPRNT      5 PRINT CONTROL
      IPLOT      0 PLOT CONTROL
      QSCAL      0. HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
      NMIN      5 MINUTES IN COMPUTATION INTERVAL
      IDATE      1 0 STARTING DATE
      ITIME      0000 STARTING TIME
      NQ         300 NUMBER OF HYDROGRAPH ORDINATES
      NDDATE     2 0 ENDING DATE
      NDDTIME    0055 ENDING TIME
      ICENT      19 CENTURY MARK

      COMPUTATION INTERVAL .08 HOURS

```

TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION  
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION  
 RATIOS OF PRECIPITATION  
 .56 1.00

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	A-1	.06	1	FLOW TIME	3. 6.25 32. 6.17
ROUTED TO					
+	A3	.06	1	FLOW TIME	3. 6.75 31. 6.42
HYDROGRAPH AT					
+	A-4	.09	1	FLOW TIME	42. 6.08 137. 6.08
ROUTED TO					
+	A4	.09	1	FLOW TIME	41. 6.08 136. 6.08
HYDROGRAPH AT					
+	A-3	.15	1	FLOW TIME	49. 6.17 194. 6.08
3 COMBINED AT					
+	DPA3	.30	1	FLOW TIME	89. 6.17 330. 6.08

ROUTED TO						
+	A6	.30	1	FLOW TIME	88. 6.17	322. 6.17
HYDROGRAPH AT						
+	A-11	.08	1	FLOW TIME	40. 6.08	131. 6.08
ROUTED TO						
+	A11	.08	1	FLOW TIME	37. 6.08	128. 6.08
HYDROGRAPH AT						
+	A-8	.08	1	FLOW TIME	58. 6.17	154. 6.08
2 COMBINED AT						
+	DP A8	.16	1	FLOW TIME	94. 6.08	282. 6.08
ROUTED TO						
+	A8	.16	1	FLOW TIME	94. 6.17	276. 6.08
HYDROGRAPH AT						
+	A-7	.05	1	FLOW TIME	28. 6.08	87. 6.08
2 COMBINED AT						
+	DP A7	.21	1	FLOW TIME	119. 6.08	364. 6.08
ROUTED TO						
+	A7	.21	1	FLOW TIME	117. 6.17	359. 6.08
HYDROGRAPH AT						
+	A-6	.04	1	FLOW TIME	21. 6.08	64. 6.08
3 COMBINED AT						
+	DPA6	.54	1	FLOW TIME	225. 6.17	723. 6.08
ROUTED TO						
+	A5	.54	1	FLOW TIME	221. 6.25	713. 6.17
HYDROGRAPH AT						
+	A-9	.07	1	FLOW TIME	29. 6.17	96. 6.17

ROUTED TO  
+ A9 .07 1 FLOW 29. 95.  
TIME 6.17 6.17

HYDROGRAPH AT  
+ A-5 .11 1 FLOW 33. 139.  
TIME 6.17 6.08

3 COMBINED AT  
+ DPAS .72 1 FLOW 273. 935.  
TIME 6.25 6.17

ROUTED TO  
+ DBA .72 1 FLOW 36. 137.  
TIME 7.25 6.92

\*\* PEAK STAGES IN FEET \*\*  
1 STAGE 104.05 107.14  
TIME 7.25 6.92

ROUTED TO  
+ A10 .72 1 FLOW 36. 137.  
TIME 7.25 7.00

HYDROGRAPH AT  
+ A-10 .01 1 FLOW 5. 16.  
TIME 6.08 6.08

2 COMBINED AT  
+ DPA .73 1 FLOW 37. 138.  
TIME 7.17 6.92

1  
\*\*\* NORMAL END OF HEC-1 \*\*\*



```

*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 24JAN05 TIME 14:10:15
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Wolf Ranch Master Development Drainage Plan pn 03094
2 ID E basins future development condition with detention
3 ID 5-year and 100 year, 24hr Type IIA Storm fn:eddet.dat
*DIAGRAM
4 IT 5 0 0 300
5 IO 5 0
6 JR PREC .56 1.0
7 KK E-1
8 KM RUNOFF FOR SUB-BASIN E-1
9 BA .0403
10 IN 15
11 PE 4.4
12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120 0.0143

```

E/D ISAAC DET



53	HC	2								
54	KK	D-1								
55	KM	SUB-BASIN D-1								
56	EA	.062								
57	LS	0	78.1							
58	UD	.180								
59	KK	D2								
60	KM	ROUTE RUNOFF FROM SUB-BASIN D-1 TO DP D2								
61	RD	1230	.01	.013		CIRC	4.5			
62	KK	D-2								
63	KM	RUNOFF FROM SUB-BASIN D-2								
64	EA	.036								
65	LS	0	73							
66	UD	.119								
67	KK	DPD2								
68	KM	COMBINE RUNOFF FROM SUB-BASIN D-2 AND DP D2								
69	HC	2								
70	KK	DPE-D								
71	KM	COMBINE RUNOFF FROM DP D2 AND DP E2								
72	HC	2								
73	KK	DBE-D								
74	KM	DETENTION BASIN E-D								
75	KM	THIS OUTFLOW FROM DETENTION BASIN E-D								
76	RS	1	ELEV	-1						
77	SQ	0	2.2	11	15	109.2	162.9	179.9	509	
78	SE	6952	6954.25	6954.5	6956.33	6957	6958	6959	6960	
79	SA	0	1.5	2.08	3.04	3.59	3.86	4	4.2	
80	SE	6952	6953	6954	6955	6957	6959	6960	6961	
81	ZZ									

I

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
LINE		
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
7	E-1	
	V	
	V	
24	E5	
	.	
	.	
27	E-6	
	V	
	V	
32	E6	





HYDROGRAPH AT						
+	E-6	.05	1	FLOW TIME	29. 6.08	87. 6.08
ROUTED TO						
+	E6	.05	1	FLOW TIME	28. 6.08	85. 6.08
HYDROGRAPH AT						
+	E-6	.04	1	FLOW TIME	28. 6.00	82. 6.00
3 COMBINED AT						
+	DPE5	.13	1	FLOW TIME	85. 6.08	241. 6.08
ROUTED TO						
+	E2	.13	1	FLOW TIME	82. 6.08	240. 6.08
HYDROGRAPH AT						
+	E-2	.05	1	FLOW TIME	34. 6.08	102. 6.00
2 COMBINED AT						
+	DPE2	.18	1	FLOW TIME	116. 6.08	336. 6.08
HYDROGRAPH AT						
+	D-1	.06	1	FLOW TIME	36. 6.08	109. 6.08
ROUTED TO						
+	D2	.06	1	FLOW TIME	34. 6.08	107. 6.08
HYDROGRAPH AT						
+	D-2	.04	1	FLOW TIME	15. 6.08	57. 6.00
2 COMBINED AT						
+	DPD2	.10	1	FLOW TIME	49. 6.08	160. 6.08
2 COMBINED AT						
+	DPE-D	.28	1	FLOW TIME	165. 6.08	496. 6.08
ROUTED TO						
+	DDE-D	.28	1	FLOW TIME	13. 7.17	151. 6.33

\*\* PEAK STAGES IN FEET \*\*  
1 STAGE 6955.24 6957.78  
TIME 7.17 6.33

1

\*\*\* NORMAL END OF HEC-1 \*\*\*

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 14FEB05 TIME 13:10:37
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Wolf Ranch Master Development Drainage plan									
2	ID	F-Basins future developed condition with detention									FN 03094
3	ID	5-year and 100 Year, 24 hr Type IIA Storm FN: f-DET.dat									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	5	0								
6	JR	PREC	.56	1.0							
7	KK	F-8									
8	KM	RUNOFF FOR SUB-BASIN F-8									
9	BA	.0630									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143

F BASINS DESTROYED



13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270
18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	71.5								
23	UD	0.22									

24	KK	RF-8									
25	KM		ROUTE FLOW FROM SUB-BASIN F-8 TO DETENTION BASIN DB 19								
26	RD	1800	0.037	0.04		TRAP	15		4		

27	KK	F-1									
28	KM		RUNOFF FOR BASIN F-1								
29	BA	.1659									
30	LS	0	61								
31	UD	.20									

32	KK	RF-9									
33	KM		ROUTE FLOW FROM SUB-BASIN F-1 TO DESIGN POINT F9								
34	RD	700	0.037	0.04		TRAP	10		6		

35	KK	F-9									
36	KM		RUNOFF FOR BASIN F-9								
37	BA	.0430									
38	LS	0	70								
39	UD	.16									

40	KK	DPF9									
41	KM		COMBINE FLOW FROM SUB-BASIN F-9 AND RF-9								
42	HC	2									

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43	KK	RF-19									
44	KM		ROUTE FLOW FROM DESIGN POINT DP F9 TO DETENTION BASIN DB 19								
45	RD	2000	0.018	0.04		TRAP	20		4		

46	KK	F-19									
47	KM		RUNOFF FOR BASIN F-19								
48	BA	.1020									
49	LS	0	73.2								
50	UD	.19									

51	KK	DPF19									
52	KM		COMBINE FLOW FROM SUB-BASIN F-19, RF-8 AND RF19								

53 KM THIS IS INFLOW TO DETENTION BASIN F-19  
54 HC 3

55 KK DBF19  
56 KM ROUTE DPF19 THROUGH DETENTION BASIN F19  
57 KM THIS OUTFLOW FROM DETENTION BASIN F-19  
58 RS 1 ELEV 7140  
59 SV 0 1 4 11 23.5 41  
60 SE 7140 7142 7144 7146 7148 7150  
61 SQ 0 10 55 100 200 300

62 KK RF-22  
63 KM ROUTE FLOW FROM DESIGN POINT DPF19 TO DESIGN POINT F22  
64 RD 1800 0.033 0.04 TRAP 20 3

65 KK F-2  
66 KM RUNOFF FOR BASIN F-2  
67 BA .0424  
68 LS 0 61  
69 UD .19

70 KK RF-10  
71 KM ROUTE FLOW FROM SUB-BASIN F-2 TO DESIGN POINT F10  
72 RD 850 0.059 0.04 TRAP 10 6

73 KK F-10  
74 KM RUNOFF FOR BASIN F-10  
75 BA .0180  
76 LS 0 67  
77 UD .15

78 KK DPF10  
79 KM COMBINE FLOW FROM SUB-BASIN F-10 AND RF10  
80 HC 2

81 KK RF-18A  
82 KM ROUTE FLOW FROM DESIGN POINT DP F10 TO DETENTION BASIN DB 18  
83 RD 1600 0.050 0.04 TRAP 15 4

1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

84 KK F-3  
85 KM RUNOFF FOR SUB-BASIN F-3  
86 BA .0942  
87 LS 0 61  
88 UD .22

89 KK RF-11  
90 KM ROUTE FLOW FROM SUB-BASIN F-3 TO DESIGN POINT F11  
91 RD 950 0.038 0.04 TRAP 10 6

```

92      KK      F-11
93      KM      RUNOFF FOR SUB-BASIN F-11
94      BA      .0460
95      LS      0      68.2
96      UD      .17

97      KK      DPF11
98      KM      COMBINE FLOW FROM SUB-BASIN F-11 AND RF-11
99      HC      2

100     KK      RF-18
101     KM      ROUTE FLOW FROM DESIGN POINT F11 TO DETENTION BASIN DB 18
102     RD      1600  0.029  0.04      TRAP      15      4

103     KK      F-4
104     KM      RUNOFF FOR SUB-BASIN F-4
105     BA      .2681
106     LS      0      61
107     UD      .28

108     KK      RF-12
109     KM      ROUTE FLOW FROM SUB-BASIN F-4 TO DESIGN POINT F12
110     RD      1150  0.044  0.04      TRAP      10      6

111     KK      F-5
112     KM      RUNOFF FOR SUB-BASIN F-5
113     BA      .1073
114     LS      0      61
115     UD      .34

116     KK      RF-12A
117     KM      ROUTE FLOW FROM SUB-BASIN F-5 TO DESIGN POINT F12
118     RD      1600  0.035  0.04      TRAP      10      6

119     KK      F-12
120     KM      RUNOFF FOR SUB-BASIN F-12
121     BA      .0590
122     LS      0      69.3
123     UD      .20

```

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

124     KK      DPF12
125     KM      COMBINE FLOW FROM SUB-BASIN RF-12 RF-12A, AND F-12
126     HC      3

127     KK      RF-17
128     KM      ROUTE FLOW FROM DESIGN POINT F-12 TO DETENTION BASIN DB 18
129     RD      1600  0.020  0.04      TRAP      15      4

```

```

130      KK      F-17
131      KM      RUNOFF FOR SUB-BASIN F-17
132      BA      .0380
133      LS      0      60.1
134      UD      .21

135      KK      F-18
136      KM      RUNOFF FOR SUB-BASIN F-18
137      BA      .0980
138      LS      0      73.1
139      UD      .21

140      KK      F-16
141      KM      RUNOFF FOR SUB-BASIN F-16
142      BA      .0270
143      LS      0      72.8
144      UD      .21

145      KK      RF-16
146      KM      ROUTE FLOW FROM SUB-BASIN F-16 TO DETENTION BASIN DB 18
147      RD      600  0.020  .013      CIRC      2

148      KK      DPF18
149      KM      COMBINE FLOW FROM SUB-BASINS F-18, F17, RF-18A, RF-18, RF-17, AND RF-16
150      KM      THIS IS INFLOW TO DETENTION BASIN F-18
151      HC      6

152      KK      DBF18
153      KM      ROUTE DPF18 THROUGH DETENTION BASIN F-18
154      KM      THIS IS OUTFLOW FROM DETENTION BASIN F-18
155      RS      1      ELEV      7140
156      SV      0      1      4      11      23.5      41
157      SE      7140      7142      7144      7146      7148      7150
158      SQ      0      10      55      100      200      300

159      KK      RF-22A
160      KM      ROUTE FLOW FROM DESIGN POINT DPF18 TO DESIGN POINT F22
161      RD      1800  0.027  0.04      TRAP      10      6

162      KK      F-22
163      KM      RUNOFF FOR SUB-BASIN F-22
164      BA      .0640
165      LS      0      64.1
166      UD      .21

```

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

167      KK      DPF22
168      KM      COMBINE FLOW FROM SUB-BASIN F-22, RF-22 AND RF-22A

```

169	HC	3							
170	KK	RF-27							
171	KM	ROUTE FLOW FROM DESIGN POINT DPF22 TO DESIGN POINT F27							
172	RD	3700	0.020	0.04	TRAP	50	3		
173	KK	F-26							
174	KM	RUNOFF FOR SUB-BASIN F-26							
175	BA	.0520							
176	LS	0	79						
177	UD	.19							
178	KK	RF-26A							
179	KM	ROUTE FLOW FROM SUB-BASIN F26 TO DESIGN POINT F27							
180	RD	1150	0.020	.013	CIRC	2			
181	KK	DPF27							
182	KM	COMBINE FLOW FROM RF-27 AND RF-26A							
183	HC	2							
184	KK	RF-27C							
185	KM	ROUTE FLOW FROM DESIGN POINT F27 TO DESIGN POINT F28							
186	RD	1400	0.019	0.04	TRAP	50	3		
187	KK	F-7							
188	KM	RUNOFF FOR SUB-BASIN F-7							
189	BA	.0782							
190	LS	0	61						
191	UD	.19							
192	KK	RF-7							
193	KM	ROUTE FLOW FROM SUB-BASIN F-7 TO DESIGN POINT F14							
194	RD	1200	0.033	0.04	TRAP	10	6		
195	KK	F-14							
196	KM	RUNOFF FOR SUB-BASIN F-14							
197	BA	.1290							
198	LS	0	73.0						
199	UD	.23							
200	KK	F-6							
201	KM	RUNOFF FOR SUB-BASIN F-6							
202	BA	.0310							
203	LS	0	61						
204	UD	.19							
205	KK	RF-13							
206	KM	ROUTE FLOW FROM SUB-BASIN F-6 TO DESIGN POINT F13							
207	RD	800	0.038	0.04	TRAP	10	6		

HEC-1 INPUT

PAGE 6

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

208	KK	F-13								
209	KM		RUNOFF FOR SUB-BASIN F-13							
210	BA	.0140								
211	LS	0	61							
212	UD	.14								
213	KK	DPF13								
214	KM		COMBINE FLOW FROM RF-13 AND F-13							
215	HC	2								
216	KK	RF-14								
217	KM		ROUTE FLOW FROM DESIGN POINT F13 TO DESIGN POINT F14							
218	RD	3600	0.027	0.04	TRAP	20	6			
219	KK	DPF14								
220	KM		COMBINE FLOW FROM RF-7, F-14, AND RF-14							
221	HC	3								
222	KK	RF-25								
223	KM		ROUTE FLOW FROM DESIGN POINT F14 TO DESIGN POINT F25							
224	RD	2600	0.023	0.04	TRAP	20	6			
225	KK	F-25								
226	KM		RUNOFF FOR SUB-BASIN F-25							
227	BA	.0890								
228	LS	0	74.1							
229	UD	.28								
230	KK	DPF25								
231	KM		COMBINE FLOW FROM RF-25 AND RF-14							
232	HC	2								
233	KK	RF-30								
234	KM		ROUTE FLOW FROM DESIGN POINT F25 TO DESIGN POINT F30							
235	RD	900	0.027	0.04	TRAP	20	6			
236	KK	F-15								
237	KM		RUNOFF FOR SUB-BASIN F-15							
238	BA	.0210								
239	LS	0	69.1							
240	UD	.15								
241	KK	RF-23								
242	KM		ROUTE FLOW FROM SUB-BASIN F15 TO DESIGN POINT F23							
243	RD	1200	0.023	0.04	TRAP	10	3			
244	KK	F-23								
245	KM		RUNOFF FOR SUB-BASIN F-23							
246	BA	.0310								
247	LS	0	73.0							

248

UD .18

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

249 KK DPF23  
250 KM COMBINE FLOW FROM RF-23 AND F-23  
251 HC 2

252 KK RF-24  
253 KM ROUTE FLOW FROM DESIGN POINT F23 TO DESIGN POINT F24  
254 RD 2250 0.026 0.04 TRAP 10 6

255 KK F-24  
256 KM RUNOFF FOR SUB-BASIN F-24  
257 BA .0890  
258 LS 0 79  
259 UD .26

260 KK DPF24  
261 KM COMBINE FLOW FROM RF-24 AND F-24  
262 HC 2

263 KK RF-30A  
264 KM ROUTE FLOW FROM DESIGN POINT F24 TO DESIGN POINT F30  
265 RD 1100 0.033 0.04 TRAP 10 6

266 KK F-30  
267 KM RUNOFF FOR SUB-BASIN F-30  
268 BA .0220  
269 LS 0 77.7  
270 UD .18

271 KK DPF30  
272 KM COMBINE FLOW FROM RF-30, RF-30A AND F-30  
273 HC 3

274 KK RF-29  
275 KM ROUTE FLOW FROM DESIGN POINT F30 TO DESIGN POINT F29  
276 RD 2350 0.027 0.04 TRAP 6 3

277 KK F-29  
278 KM RUNOFF FOR SUB-BASIN F-29  
279 BA .0250  
280 LS 0 70  
281 UD .19

282 KK DPF29  
283 KM COMBINE FLOW FROM RF-29 AND F-29  
284 HC 2

285 KK RF-28  
 286 KM ROUTE FLOW FROM DESIGN POINT F29 TO DESIGN POINT F28  
 287 RD 750 0.015 0.04 TRAP 20 3  
 HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

288 KK F-28  
 289 KM RUNOFF FOR SUB-BASIN F-28  
 290 BA .042  
 291 LS 0 68  
 292 UD .23

293 KK F-27  
 294 KM RUNOFF FOR SUB-BASIN F-27  
 295 BA .213  
 296 LS 0 76.2  
 297 UD .32

298 KK DPF28  
 299 KM COMBINE FLOW FROM RF-27C, RF-28, F-28 AND F-27  
 300 KM THIS IS INFLOW TO DETENTION BASIN F-28  
 301 HC 4

302 KK DBF28  
 303 KM ROUTE DPF28 THROUGH DETENTION BASIN F-28  
 304 KM THIS IS OUTFLOW FROM DETENTION BASIN F-28

RS	1	ELEV	6960								
SV	0	.74	2.72	6.20	10.81	15.88	21.44	27.56	34.39	42.08	
SV	50.72	60.39	71.09	82.91	95.94	110.43					
SE	6960	6962	6964	6966	6968	6970	6972	6974	6976	6978	
SE	6980	6982	6984	6986	6988	6990					
SQ	0	10	55	100	200	300	550	560	570	580	
SQ	590	600	610	620	630	640					

312 KK RF-31  
 313 KM ROUTE FLOW FROM DPF TO DESIGN POINT F  
 314 RD 3500 0.023 0.04 TRAP 20 3

315 KK F-31  
 316 KM RUNOFF FOR SUB-BASIN F-31  
 317 BA .069  
 318 LS 0 61  
 319 UD .24

320 KK DP F  
 321 KM COMBINE FLOW FROM RF-31 AND F-31  
 322 HC 2  
 323 ZZ

1

SCHEMATIC DIAGRAM OF STREAM NETWORK



INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
7	F-8	
	V	
	V	
24	RF-8	
	.	
	.	
27	.	F-1
	V	
	V	
32	RF-9	
	.	
	.	
35	.	F-9
	.	.
	.	.
40	DPF9.....	
	V	
	V	
43	RF-19	
	.	
	.	
46	.	F-19
	.	.
	.	.
51	DPF19.....	
	V	
	V	
55	DBF19	
	V	
	V	
62	RF-22	
	.	
	.	
65	.	F-2
	V	
	V	
70	RF-10	
	.	
	.	
73	.	F-10
	.	.
	.	.
78	DPF10.....	
	V	
	V	
81	RF-18A	
	.	

84	.	.	F-3	.	.	.	.
	.	.	V	.	.	.	.
	.	.	V	.	.	.	.
89	.	.	RF-11	.	.	.	.
	.	.	.	.	.	.	.
92	.	.	.	F-11	.	.	.
	.	.	.	.	.	.	.
97	.	.	DPF11	.....	.	.	.
	.	.	V	.	.	.	.
	.	.	V	.	.	.	.
100	.	.	RF-18	.	.	.	.
	.	.	.	.	.	.	.
103	.	.	.	F-4	.	.	.
	.	.	.	V	.	.	.
	.	.	.	V	.	.	.
108	.	.	RF-12	.	.	.	.
	.	.	.	.	.	.	.
111	.	.	.	.	F-5	.	.
	.	.	.	.	V	.	.
	.	.	.	.	V	.	.
116	.	.	.	.	RF-12A	.	.
	.	.	.	.	.	.	.
119	.	.	.	.	.	F-12	.
	.	.	.	.	.	.	.
124	.	.	.	DPF12	.....	.	.
	.	.	.	V	.	.	.
	.	.	.	V	.	.	.
127	.	.	RF-17	.	.	.	.
	.	.	.	.	.	.	.
130	.	.	.	.	F-17	.	.
	.	.	.	.	.	.	.
135	.	.	.	.	.	F-18	.
	.	.	.	.	.	.	.
140	.	.	.	.	.	.	F-16
	.	.	.	.	.	.	V
	.	.	.	.	.	.	V
145	.	.	.	.	.	.	RF-16
	.	.	.	.	.	.	.
	.	.	.	.	.	.	.
148	.	.	DPF18	.....	.	.	.
	.	.	V	.	.	.	.
	.	.	V	.	.	.	.

152	.	DBF18		
	.	V		
	.	V		
159	.	RF-22A		
	.	.		
162	.	.	F-22	
	.	.		
167	DPF22	.....		
	V			
	V			
170	RF-27			
	.			
173	.	F-26		
	.	V		
	.	V		
178	.	RF-26		
	.	.		
181	DPF27	.....		
	V			
	V			
184	RF-27C			
	.			
187	.	F-7		
	.	V		
	.	V		
192	.	RF-7		
	.	.		
195	.	.	F-14	
	.	.	.	
200	.	.	F-6	
	.	.	V	
	.	.	V	
205	.	.	RF-13	
	.	.	.	
208	.	.	.	F-13
	.	.	.	.
213	.	.	DPF13	.....
	.	.	V	
	.	.	V	
216	.	.	RF-14	
	.	.	.	
219	.	DPF14	.....	

222	.	V		
	.	V		
	.	RF-25		
	.	.		
225	.	.	F-25	
	.	.		
	.	.		
230	.	DPF25	.....	
	.	V		
	.	V		
233	.	RF-30		
	.	.		
	.	.		
236	.	.	F-15	
	.	.	V	
	.	.	V	
241	.	.	RF-23	
	.	.		
	.	.		
244	.	.		F-23
	.	.		
	.	.		
249	.	.	DPF23	.....
	.	.	V	
	.	.	V	
252	.	.	RF-24	
	.	.		
	.	.		
255	.	.		F-24
	.	.		
	.	.		
260	.	.	DPF24	.....
	.	.	V	
	.	.	V	
263	.	.	RF-30	
	.	.		
	.	.		
266	.	.		F-30
	.	.		
	.	.		
271	.	.	DPF30	.....
	.	.	V	
	.	.	V	
274	.	.	RF-29	
	.	.		
	.	.		
277	.	.		F-29
	.	.		
	.	.		
282	.	.	DPF29	.....
	.	.	V	

```

      .           V
285   .           RF-28
      .           .
      .           .
288   .           .           F-28
      .           .           .
      .           .           .
293   .           .           .           F-27
      .           .           .           .
      .           .           .           .
298   DFF28.....
      V
      V
302   DBF28
      V
      V
312   RF-31
      .
      .
315   .           F-31
      .           .
      .           .
320   DP F.....

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   JUN 1998 *
*   VERSION 4.1 *
*
* RUN DATE 14FEB05 TIME 13:10:37 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
*   609 SECOND STREET *
*   DAVIS, CALIFORNIA 95616 *
*   (916) 756-1104 *
*
*****

```

Wolf Ranch Master Development Drainage plan  
 F-Basins future developed condition with detention PN 03094  
 5-year and 100 Year, 24 hr Type IIA Storm FN: f-DET.dat

```

5 IO      OUTPUT CONTROL VARIABLES
          IPRNT      5 PRINT CONTROL
          IPLOT      0 PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMIN      5 MINUTES IN COMPUTATION INTERVAL
          IDATE     1 0 STARTING DATE
          ITIME     0000 STARTING TIME

```

NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 2 0 ENDING DATE  
 NDTIME 0055 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION  
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION  
 RATIOS OF PRECIPITATION  
 .56 1.00

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	F-8	.06	1	FLOW	18.
				TIME	6.17
					76.
					6.08
ROUTED TO					
+	RF-8	.06	1	FLOW	18.
				TIME	6.25
					74.
					6.17
HYDROGRAPH AT					
+	F-1	.17	1	FLOW	10.
				TIME	6.17
					110.
					6.08
ROUTED TO					
+	RF-9	.17	1	FLOW	10.
				TIME	6.25
					106.
					6.17
HYDROGRAPH AT					
+	F-9	.04	1	FLOW	13.
					55.

				TIME	6.08	6.08
2 COMBINED AT						
+	DPF9	.21	1	FLOW	20.	157.
				TIME	6.17	6.08
ROUTED TO						
+	RF-19	.21	1	FLOW	19.	152.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-19	.10	1	FLOW	38.	144.
				TIME	6.08	6.08
3 COMBINED AT						
+	DPF19	.37	1	FLOW	61.	349.
				TIME	6.25	6.17
ROUTED TO						
+	DBF19	.37	1	FLOW	21.	91.
				TIME	6.67	6.58
				** PEAK STAGES IN FEET **		
			1	STAGE	7142.51	7145.62
				TIME	6.67	6.58
ROUTED TO						
+	RF-22	.37	1	FLOW	21.	91.
				TIME	6.83	6.67
HYDROGRAPH AT						
+	F-2	.04	1	FLOW	3.	29.
				TIME	6.17	6.08
ROUTED TO						
+	RF-10	.04	1	FLOW	3.	28.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-10	.02	1	FLOW	4.	20.
				TIME	6.08	6.08
2 COMBINED AT						
+	DPF10	.06	1	FLOW	6.	46.
				TIME	6.17	6.08
ROUTED TO						
+	RF-18A	.06	1	FLOW	5.	45.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-3	.09	1	FLOW	5.	59.

				TIME	6.17	6.17
ROUTED TO						
+	RF-11	.09	1	FLOW	5.	58.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-11	.05	1	FLOW	11.	53.
				TIME	6.08	6.08
2 COMBINED AT						
+	DPF11	.14	1	FLOW	13.	102.
				TIME	6.17	6.08
ROUTED TO						
+	RF-18	.14	1	FLOW	13.	102.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-4	.27	1	FLOW	13.	147.
				TIME	6.25	6.17
ROUTED TO						
+	RF-12	.27	1	FLOW	13.	144.
				TIME	6.33	6.25
HYDROGRAPH AT						
+	F-5	.11	1	FLOW	5.	52.
				TIME	6.33	6.25
ROUTED TO						
+	RF-12A	.11	1	FLOW	5.	51.
				TIME	6.50	6.33
HYDROGRAPH AT						
+	F-12	.06	1	FLOW	14.	67.
				TIME	6.08	6.08
3 COMBINED AT						
+	DPF12	.43	1	FLOW	24.	236.
				TIME	6.25	6.25
ROUTED TO						
+	RF-17	.43	1	FLOW	24.	235.
				TIME	6.42	6.25
HYDROGRAPH AT						
+	F-17	.04	1	FLOW	2.	23.
				TIME	6.17	6.08
HYDROGRAPH AT						
+	F-18	.10	1	FLOW	33.	131.



				TIME	6.08	6.08
HYDROGRAPH AT						
+	F-16	.03	1	FLOW	9.	36.
				TIME	6.08	6.08
ROUTED TO						
+	RF-16	.03	1	FLOW	9.	35.
				TIME	6.17	6.08
6 COMBINED AT						
+	DPF18	.80	1	FLOW	72.	527.
				TIME	6.25	6.17
ROUTED TO						
+	DBF18	.80	1	FLOW	29.	147.
				TIME	6.75	6.75
** PEAK STAGES IN FEET **						
			1	STAGE	7142.85	7146.93
				TIME	6.75	6.75
ROUTED TO						
+	RF-22A	.80	1	FLOW	29.	146.
				TIME	6.92	6.83
HYDROGRAPH AT						
+	F-22	.06	1	FLOW	7.	51.
				TIME	6.17	6.08
3 COMBINED AT						
+	DPF22	1.24	1	FLOW	52.	245.
				TIME	6.83	6.75
ROUTED TO						
+	RF-27	1.24	1	FLOW	52.	245.
				TIME	7.08	6.83
HYDROGRAPH AT						
+	F-26	.05	1	FLOW	31.	94.
				TIME	6.08	6.08
ROUTED TO						
+	RF-26	.05	1	FLOW	30.	92.
				TIME	6.08	6.08
2 COMBINED AT						
+	DPF27	1.29	1	FLOW	55.	254.
				TIME	7.08	6.83
ROUTED TO						
+	RF-27C	1.29	1	FLOW	55.	254.

				TIME	7.00	6.83
HYDROGRAPH AT						
+	F-7	.08	1	FLOW	5.	54.
				TIME	6.17	6.08
ROUTED TO						
+	RF-7	.08	1	FLOW	5.	53.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-14	.13	1	FLOW	42.	162.
				TIME	6.17	6.08
HYDROGRAPH AT						
+	F-6	.03	1	FLOW	2.	21.
				TIME	6.17	6.08
ROUTED TO						
+	RF-13	.03	1	FLOW	2.	21.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-13	.01	1	FLOW	1.	11.
				TIME	6.08	6.08
2 COMBINED AT						
+	DPF13	.05	1	FLOW	3.	30.
				TIME	6.17	6.08
ROUTED TO						
+	RF-14	.05	1	FLOW	4.	30.
				TIME	6.75	6.33
3 COMBINED AT						
+	DPF14	.25	1	FLOW	45.	210.
				TIME	6.17	6.17
ROUTED TO						
+	RF-25	.25	1	FLOW	44.	209.
				TIME	6.33	6.25
HYDROGRAPH AT						
+	F-25	.09	1	FLOW	29.	108.
				TIME	6.17	6.17
2 COMBINED AT						
+	DPF25	.34	1	FLOW	67.	306.
				TIME	6.25	6.17
ROUTED TO						
+	RF-30	.34	1	FLOW	68.	305.

				TIME	6.33	6.25
HYDROGRAPH AT						
+	F-15	.02	1	FLOW	6.	26.
				TIME	6.08	6.08
ROUTED TO						
+	RF-23	.02	1	FLOW	6.	25.
				TIME	6.17	6.08
HYDROGRAPH AT						
+	F-23	.03	1	FLOW	12.	44.
				TIME	6.08	6.08
2 COMBINED AT						
+	DPF23	.05	1	FLOW	16.	69.
				TIME	6.17	6.08
ROUTED TO						
+	RF-24	.05	1	FLOW	15.	66.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-24	.09	1	FLOW	45.	137.
				TIME	6.17	6.17
2 COMBINED AT						
+	DPF24	.14	1	FLOW	55.	203.
				TIME	6.25	6.17
ROUTED TO						
+	RF-30	.14	1	FLOW	55.	197.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-30	.02	1	FLOW	12.	38.
				TIME	6.08	6.08
3 COMBINED AT						
+	DPF30	.50	1	FLOW	124.	515.
				TIME	6.33	6.25
ROUTED TO						
+	RF-29	.50	1	FLOW	122.	517.
				TIME	6.33	6.25
HYDROGRAPH AT						
+	F-29	.03	1	FLOW	7.	30.
				TIME	6.08	6.08
2 COMBINED AT						
+	DPF29	.53	1	FLOW	125.	535.

				TIME	6.33	6.25
ROUTED TO						
+	RF-28	.53	1	FLOW	124.	519.
				TIME	6.42	6.25
HYDROGRAPH AT						
+	F-28	.04	1	FLOW	8.	40.
				TIME	6.17	6.08
HYDROGRAPH AT						
+	F-27	.21	1	FLOW	75.	264.
				TIME	6.25	6.17
4 COMBINED AT						
+	DPF28	2.07	1	FLOW	210.	903.
				TIME	6.33	6.25
ROUTED TO						
+	DBF28	2.07	1	FLOW	101.	554.
				TIME	7.08	6.67
				** PEAK STAGES IN FEET **		
			1	STAGE	6966.02	6972.79
				TIME	7.08	6.67
ROUTED TO						
+	RF-31	2.07	1	FLOW	101.	555.
				TIME	7.25	6.83
HYDROGRAPH AT						
+	F-31	.07	1	FLOW	4.	42.
				TIME	6.25	6.17
2 COMBINED AT						
+	DP F	2.14	1	FLOW	102.	565.
				TIME	7.25	6.58
1						

\*\*\* NORMAL END OF HEC-1 \*\*\*

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
*
* RUN DATE 14FEB05 TIME 13:40:24 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

```

X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Wolf Ranch Master Development Drainage Plan
2 ID G Basins Future developed condition with detention PN 03094
3 ID 5-year and 100 Year, 24 hr Type IIA Storm FN G-det.dat
*DIAGRAM
4 IT 5 0 0 300
5 IO 4 0
6 JR PREC .56 1.0

7 KK G-1
8 KM RUNOFF - Sub-basin G-1
9 BA .0808
10 IN 15
11 PB 4.4
12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120 0.0143

```

G-BASINS  
 DETAILED



53	KM	RUNOFF FROM SUB-BASIN G-4
54	BA	.043
55	LS	0        79
56	UD	.212
57	KK	DP G
58	KM	COMBINE RUNOFF FROM G-4 AND G4
59	HC	2
60	KK	G-5
61	KM	RUNOFF - Sub-basin G-5
62	BA	.073
63	LS	0        76.2
64	UD	0.26
65	ZZ	

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
LINE		
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
7	G-1	
	V	
	V	
24	G2	
	.	
	.	
27	.	G-2
	.	V
	.	V
32	.	G3
	.	.
	.	.
35	.	G-3
	.	.
	.	.
40	DPG3.....	
	V	
	V	
43	DB G	
	V	
	V	
49	G4	
	.	
	.	
52	.	G-4
	.	.
	.	.
57	DP G.....	
	.	
	.	

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 14FEB05 TIME 13:40:24 *
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

Wolf Ranch Master Development Drainage Plan  
 G Basins Future developed condition with detention FN 03094  
 5-year and 100 Year, 24 hr Type IIA Storm FN G-det.dat

5 IO

## OUTPUT CONTROL VARIABLES

```

IPRNT      4  PRINT CONTROL
IPLOT      0  PLOT CONTROL
QSCAL     0.  HYDROGRAPH PLOT SCALE

```

IT

## HYDROGRAPH TIME DATA

```

NMIN      5  MINUTES IN COMPUTATION INTERVAL
IDATE     1  0  STARTING DATE
ITIME     0000 STARTING TIME
NQ        300 NUMBER OF HYDROGRAPH ORDINATES
NDDATE    2  0  ENDING DATE
NDTIME    0055 ENDING TIME
ICENT     19  CENTURY MARK

```

```

COMPUTATION INTERVAL .08 HOURS
TOTAL TIME BASE     24.92 HOURS

```

## ENGLISH UNITS

```

DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME     ACRE-FEET
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS



OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION		
				RATIO 1	RATIO 2	
				.56	1.00	
HYDROGRAPH AT +	G-1	.08	1	FLOW TIME	5. 6.17	50. 6.17
ROUTED TO +	G2	.08	1	FLOW TIME	4. 6.58	50. 6.25
HYDROGRAPH AT +	G-2	.04	1	FLOW TIME	12. 6.17	45. 6.08
ROUTED TO +	G3	.04	1	FLOW TIME	12. 6.33	44. 6.25
HYDROGRAPH AT +	G-3	.18	1	FLOW TIME	50. 6.17	200. 6.17
3 COMBINED AT +	DPG3	.29	1	FLOW TIME	57. 6.25	278. 6.25
ROUTED TO +	DB G	.29	1	FLOW TIME	34. 6.58	111. 6.58
				** PEAK STAGES IN FEET **		
			1	STAGE TIME	4.14 6.58	7.04 6.58
ROUTED TO +	G4	.29	1	FLOW TIME	34. 6.58	111. 6.58
HYDROGRAPH AT +	G-4	.04	1	FLOW TIME	24. 6.08	74. 6.08
2 COMBINED AT +	DP G	.34	1	FLOW TIME	40. 6.42	134. 6.25
HYDROGRAPH AT +	G-5	.07	1	FLOW	30.	100.

1

TIME

6.17

6.17

\*\*\* NORMAL END OF HEC-1 \*\*\*

1071

**APPENDIX B**

**HYDRAULIC CALCULATIONS**

# BASIN 'A' HYDRAULICS

## Preliminary Detention Basin Sizing

### - Detention Basin "A"

- historic data  $Q_5 = \frac{11}{39}$   $Q_{100} = \frac{157}{244}$   
 $TBA = .42 \text{ SM} = 270 \text{ Ac}$   
 $CN = 61$  Runoff  $5 \text{ yr} = .2''$   
 $100 \text{ yr} = 1.02''$

- "Developed":  $Q_5 = \frac{206}{221} \text{ cfs}$   $Q_{100} = \frac{722}{584} \text{ cfs}$   
 $TBA = .57 \text{ SM} = 365 \text{ Ac}$

Wtd CN =  $[.6(.62) + .15(.76) + .026(.79) + .05(.782) + .03(.718)$   
 $+ .067(.721) + .111(.772) + .008(.61)]$   
 $+ (.57) = 73.9 \text{ } \approx 74$   
 Runoff:  $5 \text{ yr} = .6''$   
 $100 \text{ yr} = 1.90''$

- RAINFALL 5-year = 2.5"  
 100-year = 4.4"

### - Existing 'A' BASIN VOLUME

$Vol(5) = 270 \text{ Ac} (.2/12) = 4.5 \text{ AF}$   
 $Vol(100) = 270 \text{ Ac} (1.02/12) = 23.0 \text{ AF}$

### - DEVELOPED 'A' BASIN VOLUME

$Vol(5) = 365 (.6/12) = 18.6 \text{ AF}$   
 $Vol(100) = 365 (1.90/12) = 57.8 \text{ AF}$

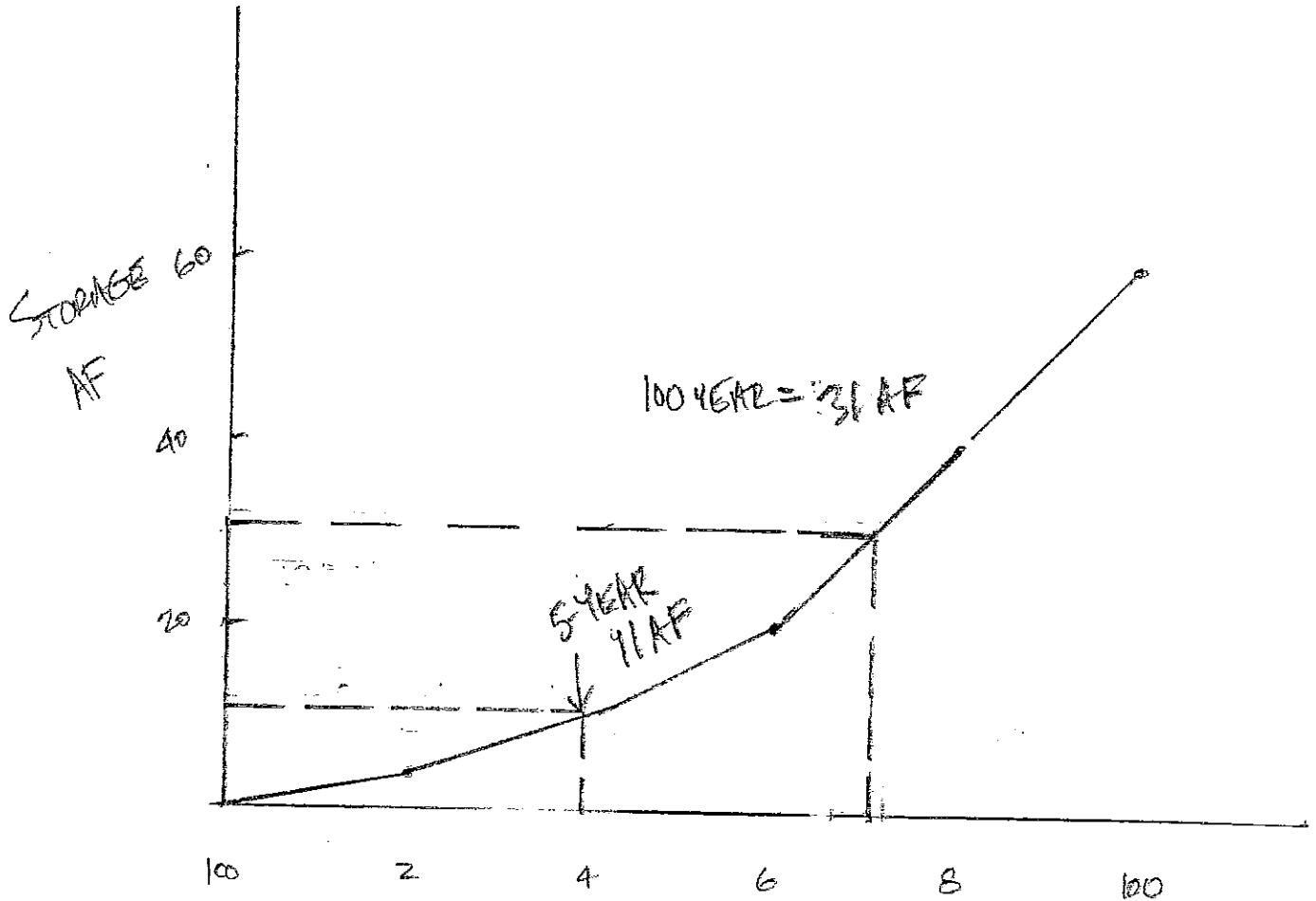
$\Delta = 14.1 \text{ AF } 5 \text{ YEAR}$   
 $34.8 \text{ AF} = 100 \text{ YR}$

Detention Basin "A"

RESTRAINED FLOW

$Q_r = 28 \text{ cfs}$

$Q_{100} = 165 \text{ cfs}$



w/wq  $\approx$  5-YEAR

TOTAL  $V_{av} = 31 \text{ AF} + 11 = \frac{42 \text{ AF}}{2}$

OUTLET CULVERT FROM  
DET. BASIN A Q = 166 cfs<sup>1</sup>

CURRENT DATE: 05-14-2004  
CURRENT TIME: 14:35:17

FILE DATE: 05-14-2004  
FILE NAME: A5

\*\*\*\*\*  
\*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
\*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
\*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	97.00	200.02	1 RCB	5.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*  
\*\*\*\*\*  
\*\*\*\*\* SUMMARY OF CULVERT FLOWS (CFS) FILE: A5 DATE: 05-14-2004 \*\*\*\*\*

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
101.21	17	17	0	0	0	0	0	0	1
101.91	34	34	0	0	0	0	0	0	1
102.49	51	51	0	0	0	0	0	0	1
103.01	68	68	0	0	0	0	0	0	1
103.49	85	85	0	0	0	0	0	0	1
103.95	102	102	0	0	0	0	0	0	1
104.42	119	119	0	0	0	0	0	0	1
104.91	136	136	0	0	0	0	0	0	1
105.43	153	153	0	0	0	0	0	0	1
105.86	166	166	0	0	0	0	0	0	1
110.00	261	261	0	0	0	0	0	0	1

\*\*\*\*\*  
\*\*\*\*\* SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: A5 DATE: 05-14-2004 \*\*\*\*\*

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
101.21	0.00	17	0	0.00
101.91	0.00	34	0	0.00
102.49	0.00	51	0	0.00
103.01	0.00	68	0	0.00
103.49	0.00	85	0	0.00
103.95	0.00	102	0	0.00
104.42	0.00	119	0	0.00
104.91	0.00	136	0	0.00
105.43	0.00	153	0	0.00
105.86	0.00	166	0	0.00

\*\*\*\*\*  
<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000  
\*\*\*\*\*



CURRENT DATE: 05-14-2004  
CURRENT TIME: 14:35:17

FILE DATE: 05-14-2004  
FILE NAME: A5

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 4.0  
CHANNEL SLOPE V/H (FT/FT) 0.025  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 97.00  
CULVERT NO.1 OUTLET INVERT ELEVATION 97.00 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	97.00	0.000	0.00	0.00
17.00	97.42	0.931	3.44	0.66
34.00	97.63	0.962	4.33	0.98
51.00	97.79	0.977	4.92	1.23
68.00	97.92	0.987	5.38	1.44
85.00	98.04	0.994	5.76	1.63
102.00	98.15	0.999	6.08	1.79
119.00	98.25	1.003	6.36	1.95
136.00	98.34	1.007	6.61	2.09
153.00	98.42	1.010	6.84	2.22
166.00	98.49	1.012	7.00	2.32

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE GRAVEL  
EMBANKMENT TOP WIDTH (FT) 20.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*



BASIN 'A'

OUTFALL CHANNELS.

- Try to achieve Velocity 5-year 5fps or less
- 100 year Velocity < 7 fps for grassed

OUTFALL  
- Channel A3

$$Q_5 = 3 + 64 = 67 \text{ cfs}$$

$$Q_{100} = SB A1 + SB A3$$

$$Q_{100} = 32 + 223 = 255 \text{ cfs}$$

conservative

- Existing Slope DP A1 → A3

$$L = 3700' \quad \Delta H = 7228 - 7086 = 142'$$

$$\text{Slope} = 142/3700 = 3.8\%$$

$$\text{@ Slope} = 3.8\% \quad V_5 = 6.5 \text{ fps no good.}$$

$$\text{if Slope} = 1.7\% \quad V_5 = 4.9 \text{ cfs}$$

$$V_{100} = 7.0 \text{ (ps. : : ck)} \left. \begin{array}{l} V_5 = 4.9 \text{ cfs} \\ V_{100} = 7.0 \text{ (ps. : : ck)} \end{array} \right\} \text{SEE 2+3 of 3}$$

Required grade control:

$$L = 3700' \quad \Delta S = .038 - .017 = .021$$

$$H = 77.7' \quad \text{Seq 78}$$

$$\text{w/ 3' each check / drop} = 26 \text{ checks}$$

$$\text{Specify} = 3700/26 = \underline{\underline{142'}}$$

20F3

**Wolf Ranch MDDP**  
**Swale Capacity Calculation**

Structure A3: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	67 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	1.7 %
Depth of Flow	1.10 ft	Manning's Roughness Coef.	0.035

Channel Area	15.8 sf
Channel Wetted Perimeter	19.1 ft
Hydraulic Radius	0.83 ft

Channel Flow Velocity	4.9 ft/sec
Channel Flow Capacity	78 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	2.2 ft
Top Width	27.8 ft

Equations:

Area (A) = b(d)  
 b = width  
 d = depth  
 Perimeter (P) = b + 2d\*(1+z<sup>2</sup>)<sup>0.5</sup>  
 z = side slope  
 Hydraulic Radius = A/P

Velocity = (1.49/n)R<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>  
 Slope (S) = Slope of the channel  
 n = Manning's number  
 R<sub>n</sub> = Hydraulic Radius (Reynold's Number)  
 Flow = (1.49/n)AR<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>  
 Freeboard = 1.0 + 0.025(v)d<sup>0.33</sup>

30F3

# Wolf Ranch MDDP

## Swale Capacity Calculation

Structure A3: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	255 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	1.7 %
Depth of Flow	2.10 ft	Manning's Roughness Coef.	0.035

Channel Area	38.6 sf
Channel Wetted Perimeter	27.3 ft
Hydraulic Radius	1.41 ft

Channel Flow Velocity	7.0 ft/sec
Channel Flow Capacity	270 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	3.3 ft
Top Width	36.6 ft

### Equations:

$$\text{Area (A)} = b(d)$$

$$b = \text{width}$$

$$d = \text{depth}$$

$$\text{Perimeter (P)} = b + 2d(1+z^2)^{0.5}$$

$$z = \text{side slope}$$

$$\text{Hydraulic Radius} = A/P$$

$$\text{Velocity} = (1.49/n)R_n^{2/3} S^{1/2}$$

$$\text{Slope (S)} = \text{Slope of the channel}$$

$$n = \text{Manning's number}$$

$$R_n = \text{Hydraulic Radius (Reynold's Number)}$$

$$\text{Flow} = (1.49/n)AR_n^{2/3} S^{1/2}$$

$$\text{Freeboard} = 1.0 + 0.025(v)d^{0.33}$$

OUTFALL CHANNEL A6.

Flow ranges  $\Delta$  A3  $\rightarrow$  A6

$$Q_s = 89 + 21 = 110 \text{ cfs}$$

$$Q_{100} = 390 + 64 = 394 \text{ cfs}$$

Existing Slope A3  $\rightarrow$  A6

$$L = 1600' \quad \Delta H = 7086 - 7036 = 50'$$

$$S = 50/1600 = .03125 \%$$

$$V_s @ S = .03125 \%/ 64 \text{ is no good}$$

$$@ \text{ Slope} = 1.4\%$$

$$V_s = 4.9 \text{ fps is ok}$$

$$V_{100} = 7.1 \text{ fps, close, is ok}$$

Required grade control.

$$L = 1600' \quad \Delta S = .03125 - .014 = .01725$$

$$H \& \text{ drops} = 1600(.01725) = 27.6', \text{ say } 27$$

w/ 3' each, need 9 drops/checks

$$\text{Spacing } 1600/27 = 60'$$

Spacing is way to close.

if sloping boulder drops used, 6' drop each

$\therefore$  spacing increased to 120'  
 need 14 drops

Still to do:

go to riprap side slopes.

make  $V_s = 7$  fps

w/  $BW = 10'$ , slope = 2.790

Success  $\left\{ \begin{array}{l} V_c = 6.9 \text{ fps.} \\ V_{100} = 9.3 \\ d_{100} = 3.7 \text{ (w/ FB)} \end{array} \right.$   
 3+484

Riprap size

$$\frac{V_s^{1.7}}{1.36} = \frac{9.3(.027)^{1.7}}{1.36} = 3.8 \text{ TYPE 'L', close to 'M' use M.}$$

Required grade control

$$\Delta S = .03125 - .027 = .00425$$

$$\text{Total H} = .00425(1600) = 6.8, \text{ say } 6$$

$\therefore$  need 2 x 3' drops

$$\text{Spacing} = 1600 / 2 = 800'$$

Wolf Ranch MDDP  
Swale Capacity Calculation

3/4

Structure A6: Riprap channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	110 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	2.7 %
Depth of Flow	1.20 ft	Manning's Roughness Coef.	0.035

Channel Area	17.8 sf
Channel Wetted Perimeter	19.9 ft
Hydraulic Radius	0.89 ft

Channel Flow Velocity	6.5 ft/sec
Channel Flow Capacity	115 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.37 ft
Top Width	29.0 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d \cdot (1+z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)d^{0.33}$

4/4

**Wolf Ranch MDDP**  
**Swale Capacity Calculation**

**Structure A6: Riprap channel 100-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	394 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	2.7 %
Depth of Flow	2.30 ft	Manning's Roughness Coef.	0.035

Channel Area	44.2 sf
Channel Wetted Perimeter	29.0 ft
Hydraulic Radius	1.52 ft

Channel Flow Velocity	9.3 ft/sec
Channel Flow Capacity	409 cfs
Capacity Check	Okay

Freeboard	1.3 ft
Swale Depth	3.60 ft
Top Width	38.8 ft

**Equations:**

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)d^{0.33}$

REV 2-10-05

OUTFALL CHANNEL A5

Flow range DRAG + SB A5

$Q_5 = 225 + 33 = 258 \text{ cfs}$

$Q_{100} = 723 + 139 = 862 \text{ cfs}$

Existing slope A6  $\rightarrow$  up of detection horizon A'

$\Delta H = 7036 - 6994 = 42' \quad L = 1750'$

$\text{Slope} = 42/1750 = .024/1$

Use riprap:

e Slope = 2.4%

$V_5 = 7.5 \text{ fps close or de) see } 245 \text{ cfs}$   
 $V_{100} = 11.0 \text{ fps}$

Riprap Size =  $\frac{10 \cdot (1.024)^{1.7}}{1.36} = 4.1$  use Type 'M'



2/3

### Wolf Ranch MDDP Swale Capacity Calculation

Structure A5: Riprap channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	258 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.4 %
Depth of Flow	1.60 ft	Manning's Roughness Coef.	0.035

Channel Area	34.2 sf
Channel Wetted Perimeter	28.2 ft
Hydraulic Radius	1.21 ft

Channel Flow Velocity	7.5 ft/sec
Channel Flow Capacity	257 cfs
Capacity Check	NO

Freeboard	1.2 ft
Swale Depth	2.82 ft
Top Width	37.6 ft

Equations:

$$\text{Area (A)} = b(d)$$

$$b = \text{width}$$

$$d = \text{depth}$$

$$\text{Perimeter (P)} = b + 2d \cdot (1 + z^2)^{0.5}$$

$$z = \text{side slope}$$

$$\text{Hydraulic Radius} = A/P$$

$$\text{Velocity} = (1.49/n)R_n^{2/3} S^{1/2}$$

$$\text{Slope (S)} = \text{Slope of the channel}$$

$$n = \text{Manning's number}$$

$$R_n = \text{Hydraulic Radius (Reynold's Number)}$$

$$\text{Flow} = (1.49/n)AR_n^{2/3} S^{1/2}$$

$$\text{Freeboard} = 1.0 + 0.025(v)d^{0.33}$$

**Wolf Ranch MDDP  
Swale Capacity Calculation**

3/3

**Structure A5: Riprap channel 100-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	862 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.4 %
Depth of Flow	3.00 ft	Manning's Roughness Coef.	0.035

Channel Area	81.0 sf
Channel Wetted Perimeter	39.7 ft
Hydraulic Radius	2.04 ft

Channel Flow Velocity	10.6 ft/sec
Channel Flow Capacity	859 cfs
Capacity Check	NO

Freeboard	1.4 ft
Swale Depth	4.38 ft
Top Width	50.0 ft

**Equations:**

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d\*(1+z<sup>2</sup>)<sup>0.5</sup>

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Freeboard = 1.0 + 0.025(v)d<sup>0.33</sup>

Channel #10

$Q_5 = 28 \text{ cfs}$   
 $Q_{100} = 165 \text{ cfs}$  } outlet side of detention basin 'A'

$L = 400'$  design slope =  $12/400 = 3.0\%$

design for  $Q_{100}$  only

$V_{100} = 7.6 \text{ fps}$  from swale calc (see 2/2)

$$VS^{1.47}/1.36 = \frac{7.6(603)^{1.47}}{1.36} = 3.07 \text{ use Type 'L'}$$

2/2

**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure A10: Riprap channel 100-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	165 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	3.0 %
Depth of Flow	1.45 ft	Manning's Roughness Coef.	0.035

Channel Area            22.9 sf  
 Channel Wetted Perimeter    22.0 ft  
 Hydraulic Radius            1.04 ft

Channel Flow Velocity	7.6 ft/sec
Channel Flow Capacity	174 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.66 ft
Top Width	31.3 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d\*(1+z<sup>2</sup>)<sup>0.5</sup>

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Freeboard = 1.0 + 0.025(v)d<sup>0.33</sup>

Outfall Storm Sewers

Assume all Storm Sewers @ 2.0%, RCP

Outfall Storm Sewer A4

$Q_{100} = 136 \text{ cfs (DP A3)}$

@ 2.0%,  $Q = 142 \text{ cfs for } 42" \text{ RCP} \therefore \text{ok}$

Storm Sewer A7

$Q_{100} = 360 \text{ cfs}$

@ 2.0%,  $Q = 368 \text{ cfs for } 60" \text{ RCP} \therefore \text{ok}$

Storm Sewer A9

$Q_{100} = 76 \text{ cfs}$

use 1.0% since grade may be a problem

$\therefore @ 1.3\%, Q = 73 \text{ cfs for } 36" \text{ RCP} \therefore \text{ok}$

Storm Sewer Branch 'A3' to Bridgegate Blvd.

$Q_{100} = 194 \text{ cfs}$

18" @ 2.0%  $Q_{100} = 203 \text{ cfs} \therefore \text{ok}$

Storm Sewer A4-1 @ DP A4-1

$Q_{100} = \text{DP A3} + \text{SBA4} = 194 + 137 = 331$

@ 2.6% 54" RCP  $Q_{100} = 317 \text{ cfs} \therefore \text{ok w/ lagging.}$

Storm Sewer A-11 e SB A-11

$$Q_{100} = 150 \text{ cfs}$$

$$42" \text{ RCP @ } 2.0\% \quad C_{up} = 142 \text{ cfs} \quad \therefore \underline{\underline{ok}}$$

Storm Sewer AB

$$Q_{100} = 262 \text{ cfs}$$

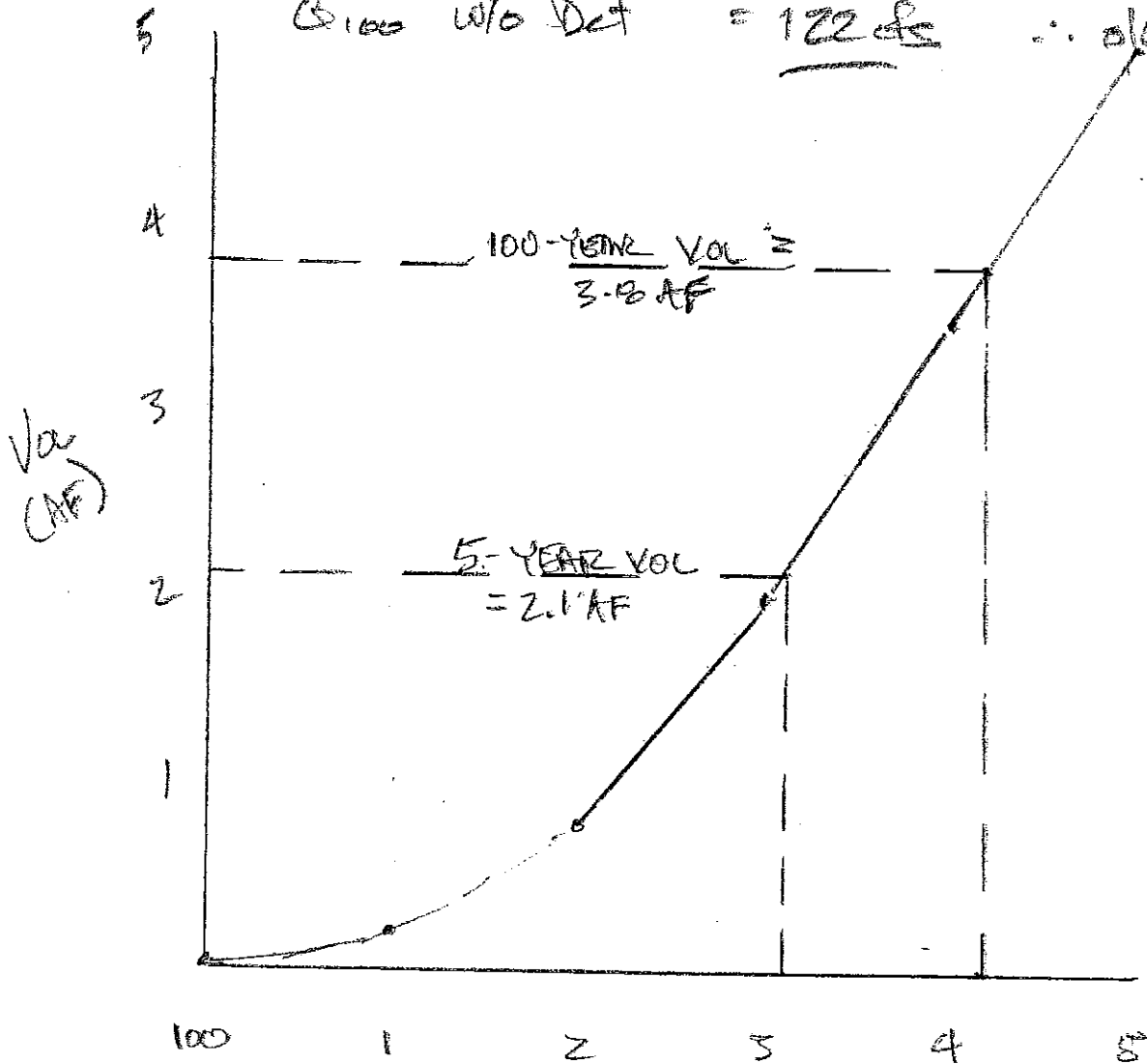
$$@ 2.0\% \quad 54" \text{ RCP} \quad Q = 278 \text{ cfs} \quad \therefore \underline{\underline{ok}}$$



May not need to detain because ex 54" rcp has adequate capacity to pickup 100 year developed flow:

Q<sub>cap</sub> 54" rcp @ 1.0% = 200 cfs

Q<sub>100</sub> w/o Det = 122 cfs ∴ ok.



w/ WQ = 5 YEAR VOL

TOTAL VOL = 3.8 + 2.1 = 5.9 AF



Detention "Basin" E/D

- Historic Data:

$$BA = .164 \text{ SM (SD'E')} + .32 \text{ SM (DP'D2)} = .48 \text{ SM} = 307 \text{ A}$$

$$CN = 61 \quad \text{Runoff } S_{5r} = .2'' \quad 100\text{-yr} = 1.02''$$

D Basin Ex  $Q_5 = 10$ ;  $Q_{100} = 103$  E-Basin Ex;  $Q_5 = 6$   $Q_{100} = 66$

- Developed Data:

$$\text{Total E/D: } Q_5 = 16 \text{ cfs } Q_{100} = 169$$

$$BA = .10 \text{ SM (DP'D2')} + .18 \text{ (DP'E2')} = .28 \text{ SM} = 179 \text{ Ac}$$

$$CN = \frac{[.048(79) + .04(81.8) + .04(79) + .062(78.1) + .052(79) + .036(79)]}{.28} = 79.2$$

- Existing E/D From Volume of Runoff

$$\text{Vol}(5) = 307 (.2/12) = 5.2 \text{ AF}$$

$$\text{Vol}(100) = 307 (1.02/12) = 26.1 \text{ AF}$$

- Developed E/D Volume of Runoff

$$\text{Runoff } S_{5\text{-year}} = .84'' \quad 100\text{-year} = 2.29''$$

$$\text{Vol } 5 = 179 (.84/12) = 12.5 \text{ AF}$$

$$\text{Vol } 100 = 179 (2.29/12) = 34.2 \text{ AF}$$

- Required Storage

$$\Delta \text{ Vol } 5 = 12.5 - 5.2 = 7.3 \text{ AF}$$

$$\Delta \text{ Vol } 100 = 34.2 - 26.1 = 8.1 \text{ AF}$$

- Required Storage Volumes

Vol 5-year =  $18.6 - 4.5 = 14.1$  AF

Vol 100-year =  $57.8 - 23.0 = 34.8$  AF

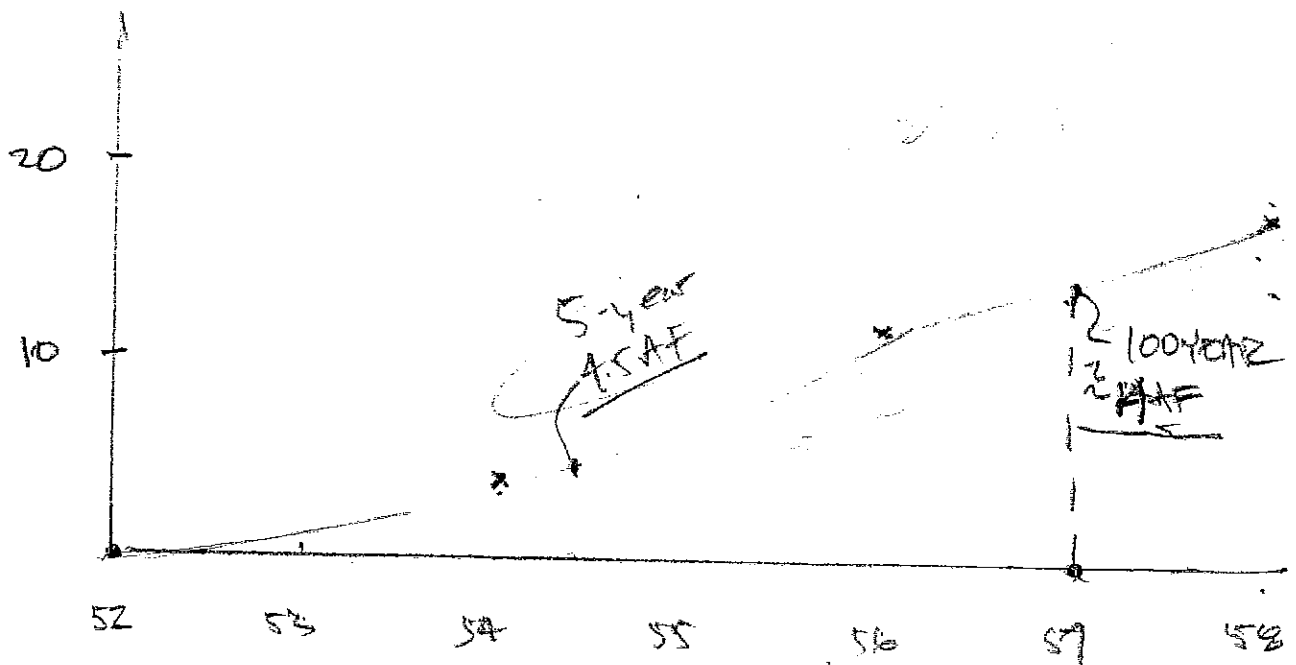
Above values are conservative & do not include channel storage due to routing.

- WFLOW TO DET. BASIN

$Q_5 = 173$  cfs  $Q_{100} = 509$  cfs

- Allowable Release Rates

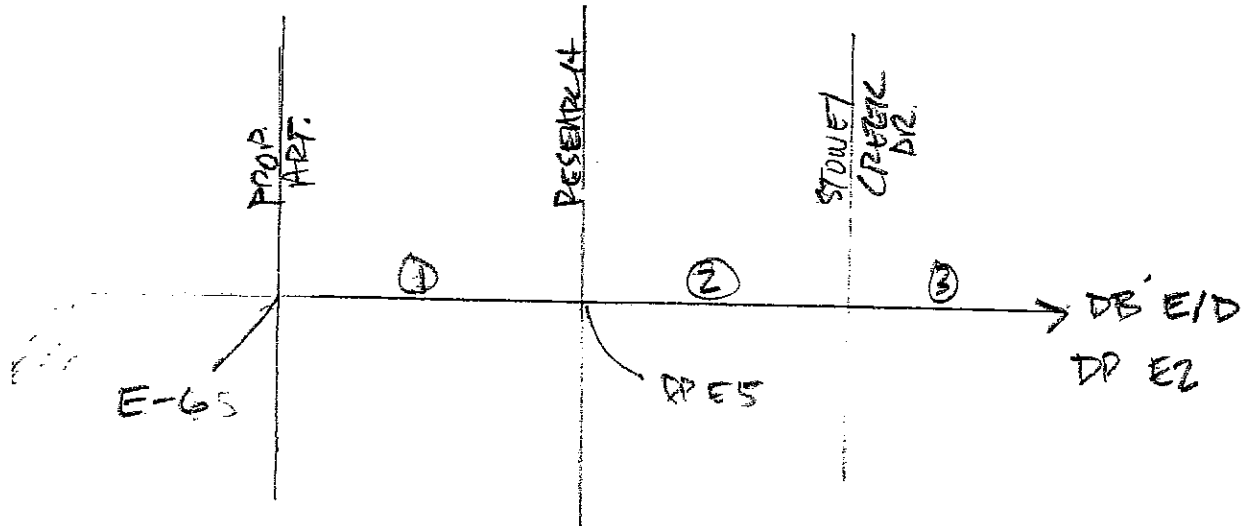
$Q_5 = 16$  cfs  $Q_{100} = 169$  cfs.



# 'E/D' BASIN HYDRAULICS

## Outfall Storm Sewer Sizing

East Outfall to Detention Basin 'E/D'



Flow Summary

	Q <sub>5</sub>	Q <sub>100</sub>
c E-6	29	87
c DP ES	85	241
c Stony Creek	95	270
c DB E/D	116	336

### Segment 1 EG to Research Parkway

Ex ground slope along prop Road =  $40/300 = .03\%$

use 2.5%  $\dot{i}$  pick up 100-year

$\therefore$  36" pipe @ 2% = 94 cfs  $\therefore$  OK

Segment 2 Research to Stony Creek  $Q_{100} = 241 \text{ cfs}$   
 use slope of Pony Creek Street  $4/140 = .029\%$   
 use slope of 2.4%

$\therefore$  48" rep @ 2.4% = 227 cfs. probably ok since slope can probably be made steeper than 2.4%

Segment 3 Stony Creek to D/B ED  
 $Q_{100} = 270$

• use slope from D/B to int of Abby Rd & Pony Creek,  
 elev @ D/B = 52.0 est. elev of int. intersection = 60  
 $\therefore$  slope =  $60 - 52 / 350 = .023\%$

• check Pony Creek  $6/330 = .019\%$  use .018%

60" rep @ .018 =  $Q = 349$ ; too much

54" rep @ .018 = 264 cfs, probably ok (Seg 3A)

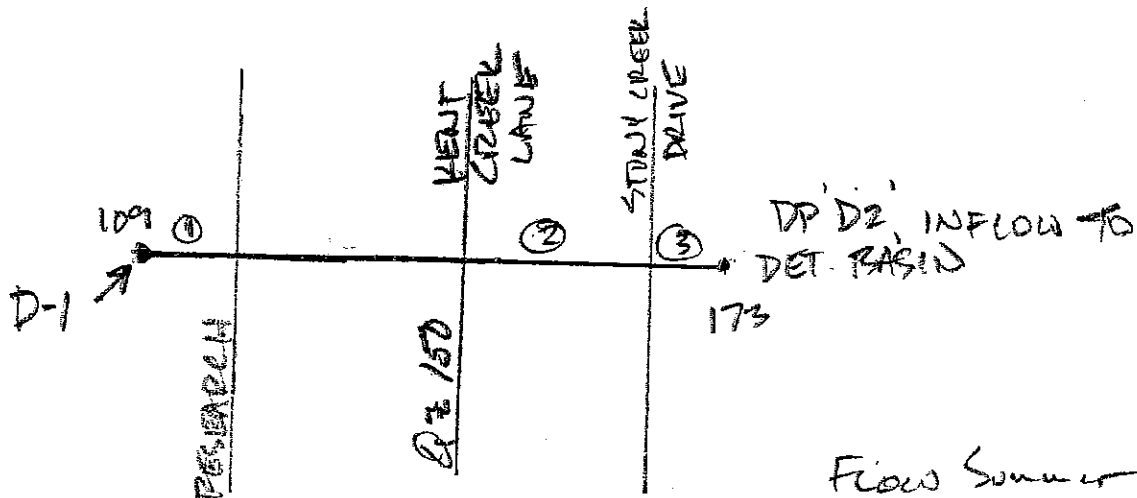
Seg 3b (Abby Road lanes)  $Q = 336$

54" @ 2.3%  $Q = 305 \text{ cfs}$  no good

60" @ 2.3%  $Q = 404$  ok

Outfall Storm Sewer Sizing,

Wet outfall to Detention Basin E/D



Flow Summary

e D-1	36	109
e DPD2	57	173

Segment 1 :  $Q = 109$  cfs

assume minimum slope of 2% across Research

$\therefore$  Need 42" RCP  $Q = 142$  cfs ←

36" RCP  $Q = 94$  cfs  $\therefore$  no good

Segment 2 : Kent Creek Drive to Stony Creek  $Q = 150$  cfs.

use slope of Connet Lane, 2%

48" RCP @ 2% = 203 cfs ; ample. ←

42" RCP @ 2% = 140  $\therefore$  no good

Segment 3:

Stoney Creek to Rd. Basin E/D

$$Q = 170 \text{ cfs}$$

Bottom of Pond @ 52 ± . L = 160'

appears the slope will be 2 2/120 = .0167% say  
.016

$$48'' \text{ dia } Q @ 1.8\% = 182 \text{ cfs } \therefore \text{ok.}$$

RAIN F HYDRAULICS

roadway culverts (See HFB results)

- DP F9  $Q_{100} = 152 \text{ cfs}$   $L = 80'$   
 $Hw/D = 42/4 = 1.05 \therefore \underline{\underline{4' \times 6' \text{ CEC}}}$

- SB F8  $Q_{100} = 161 \text{ cfs}$   $L = 80'$   
 $Hw/D = 3.8/4 = .95 \therefore \text{ok } 48" \text{ REP}$

DP F10  $Q_{100} = 48 \text{ cfs}$   $L = 80'$   
 $Hw/D = 3.3/3.5 = .94 \therefore \text{ok } 42" \text{ REP}$

DP F11  $Q_{100} = 102 \text{ cfs}$   $L = 80'$   
 $Hw/D = 4.25/4 = 1.06 \therefore \text{ok } 4' \times 4' \text{ CEC}$

DP F12  $Q_{100} = 236 \text{ cfs}$   $L = 80'$   
 $Hw/D = 4/4 = 1 \therefore \text{ok } 4' \times 10' \text{ CEC}$

SB F15  $Q_{100} = 4 \text{ cfs}$  use 18" REP

DP F13  $Q_{100} = 30 \text{ cfs}$   $L = 80'$   
 $Hw/D = 2.7/3 = .9 \therefore \text{ok use } 36" \text{ REP}$

~~SB F20 (Briarcliff Blvd)~~  $Q_{100} = 140 \text{ cfs}$   $L = 160'$   
 ~~$Hw/D = 3.97/4 = 1.0 \therefore \text{ok use } 4' \times 6' \text{ CEC}$~~

Roadway Culverts Contd.

DB 19: This is outlet of Det. Basin 19  $L = 240' \pm$   
 $Q_{100} \text{ out} = 89 \text{ cfs.}$

Assume Hw depth of 7' can be obtained  
 w/ 42" RCP,  $Hw/D = 6.6/3.5 = 1.9$

6.6' Hw depth consistent w/ DB 19 Hw requirements.

DB 18: This is outlet of Det. Basin 18,  $L = 240' \pm$   
 $Q_{100} \text{ out} = 141 \text{ cfs}$

Assume Hw depth  $\approx 7'$ , same as DB 19  
 w/ 48" RCP,  $Hw = 7.5' \therefore \text{OK.}$

$$Hw/D = 7.5/4 = 1.88$$

DP F23:  $Q_{100} = 69 \text{ cfs}$   $L = 160'$   
 (Briargate)

$$Hw/D = 3.8/4 = .95 \therefore \text{use } 48" \text{ RCP}$$

DP F14:  $Q_{100} = 210 \text{ cfs}$   $L = 160'$

$$Hw/D = 4.35/4 = 1.08 \therefore \text{OK use } 4' \times 8' \text{ CBC}$$

DP F24:  $Q_{100} = 181 \text{ cfs}$   $L = 80'$

$$Hw/D = 3.9/4 = .98 \therefore \text{OK use } 4' \times 8' \text{ CBC}$$



DP F25:  $Q_{100} = 303 \text{ cfs}$   $L = 80'$   
 $HW/D = 4.75/5 = .94$   $\therefore$  ok  $5' H \times 10' W \text{ CBC}$

DP F30:  $Q_{100} = 490 \text{ cfs}$   $L = 80'$   
 $HW/D = 6.6/6 = 1.10$   $\therefore$  ok use  $6' \times 10' \text{ CBC}$

DP F28: This is outlet from Det Basin DB 28 @  $L = 240' \pm$   
Research Parkway  
Assume HW depth of  $16'$  to match HEC-1  
 $Q_{100} = 563 \text{ cfs}$   
w/  $4' \times 8' \text{ CBC}$   $HW = 16.5' \therefore$  ok.  
use  $4' \times 8' \text{ CBC}$

CURRENT DATE: 05-19-2004  
 CURRENT TIME: 13:11:37

FILE DATE: 05-19-2004  
 FILE NAME: F9

\*\*\*\*\*  
 \*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
 \*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
 \*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCB	6.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*  
 \*\*\*\*\* SUMMARY OF CULVERT FLOWS (CFS) \*\*\*\*\*  
 \*\*\*\*\* FILE: F9 \*\*\*\*\*  
 \*\*\*\*\* DATE: 05-19-2004 \*\*\*\*\*

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
100.91	16	16	0	0	0	0	0	0	1
101.45	32	32	0	0	0	0	0	0	1
101.90	48	48	0	0	0	0	0	0	1
102.31	64	64	0	0	0	0	0	0	1
102.69	80	80	0	0	0	0	0	0	1
103.05	96	96	0	0	0	0	0	0	1
103.38	112	112	0	0	0	0	0	0	1
103.72	128	128	0	0	0	0	0	0	1
104.05	144	144	0	0	0	0	0	0	1
104.23	152	152	0	0	0	0	0	0	1
110.00	334	334	0	0	0	0	0	0	1

*How/D = 1005. : 06*

\*\*\*\*\*  
 \*\*\*\*\* SUMMARY OF ITERATIVE SOLUTION ERRORS \*\*\*\*\*  
 \*\*\*\*\* FILE: F9 \*\*\*\*\*  
 \*\*\*\*\* DATE: 05-19-2004 \*\*\*\*\*

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
100.91	0.00	16	0	0.00
101.45	0.00	32	0	0.00
101.90	0.00	48	0	0.00
102.31	0.00	64	0	0.00
102.69	0.00	80	0	0.00
103.05	0.00	96	0	0.00
103.38	0.00	112	0	0.00
103.72	0.00	128	0	0.00
104.05	0.00	144	0	0.00
104.23	0.00	152	0	0.00

\*\*\*\*\*  
 <1> TOLERANCE (FT) = 0.010  
 <2> TOLERANCE (%) = 1.000  
 \*\*\*\*\*



PRINT DATE: 05-19-2004  
CURRENT TIME: 13:11:37

FILE DATE: 05-19-2004  
FILE NAME: F9

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 98.40  
CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
16.00	98.83	0.808	2.99	0.53
32.00	99.03	0.830	3.72	0.78
48.00	99.18	0.840	4.21	0.97
64.00	99.31	0.847	4.58	1.13
80.00	99.42	0.852	4.88	1.27
96.00	99.52	0.856	5.14	1.40
112.00	99.61	0.859	5.36	1.51
128.00	99.69	0.862	5.57	1.62
144.00	99.77	0.865	5.75	1.71
152.00	99.81	0.866	5.83	1.76

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*

CURRENT DATE: 05-19-2004  
 CURRENT TIME: 13:20:42

FILE DATE: 05-19-2004  
 FILE NAME: SB8

\*\*\*\*\*  
 \*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
 \*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
 \*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCP	4.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*  
 \*\*\*\*\* SUMMARY OF CULVERT FLOWS (CFS) FILE: SB8 DATE: 05-19-2004 \*\*\*\*\*

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0		0 1
101.59	16	16	0	0	0	0	0		0 1
102.36	32	32	0	0	0	0	0		0 1
103.04	48	48	0	0	0	0	0		0 1
103.65	64	64	0	0	0	0	0		0 1
104.28	80	80	0	0	0	0	0		0 1
104.97	96	96	0	0	0	0	0		0 1
105.78	112	112	0	0	0	0	0		0 1
106.73	128	128	0	0	0	0	0		0 1
107.82	144	144	0	0	0	0	0		0 1
108.42	152	152	0	0	0	0	0		0 1
110.00	171	171	0	0	0	0	0	OVERTOPPING	

\*\*\*\*\*  
 \*\*\*\*\* SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: SB8 DATE: 05-19-2004 \*\*\*\*\*

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
101.59	0.00	16	0	0.00
102.36	0.00	32	0	0.00
103.04	0.00	48	0	0.00
103.65	0.00	64	0	0.00
104.28	0.00	80	0	0.00
104.97	0.00	96	0	0.00
105.78	0.00	112	0	0.00
106.73	0.00	128	0	0.00
107.82	0.00	144	0	0.00
108.42	0.00	152	0	0.00

\*\*\*\*\*  
 <1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000  
 \*\*\*\*\*



REPORT DATE: 05-19-2004  
REPORT TIME: 13:20:42

FILE DATE: 05-19-2004  
FILE NAME: SB8

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 98.40  
CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
16.00	98.83	0.808	2.99	0.53
32.00	99.03	0.830	3.72	0.78
48.00	99.18	0.840	4.21	0.97
64.00	99.31	0.847	4.58	1.13
80.00	99.42	0.852	4.88	1.27
96.00	99.52	0.856	5.14	1.40
112.00	99.61	0.859	5.36	1.51
128.00	99.69	0.862	5.57	1.62
144.00	99.77	0.865	5.75	1.71
152.00	99.81	0.866	5.83	1.76

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*

CURRENT DATE: 05-19-2004  
 CURRENT TIME: 13:25:46

FILE DATE: 05-19-2004  
 FILE NAME: F10

\*\*\*\*\*  
 \*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
 \*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
 \*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCP	3.50	3.50	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*

\*\*\*\*\*  
 SUMMARY OF CULVERT FLOWS (CFS) FILE: F10 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
100.99	6	6	0	0	0	0	0	0	1
101.43	12	12	0	0	0	0	0	0	1
101.77	18	18	0	0	0	0	0	0	1
102.13	24	24	0	0	0	0	0	0	1
102.45	30	30	0	0	0	0	0	0	1
102.74	36	36	0	0	0	0	0	0	1
103.02	42	42	0	0	0	0	0	0	1
103.30	48	48	0	0	0	0	0	0	1
103.58	54	54	0	0	0	0	0	0	1
103.88	60	60	0	0	0	0	0	0	1
110.00	134	134	0	0	0	0	0	0	OVERTOPPING

\*\*\*\*\*

\*\*\*\*\*  
 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F10 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
100.99	0.00	6	0	0.00
101.43	0.00	12	0	0.00
101.77	0.00	18	0	0.00
102.13	0.00	24	0	0.00
102.45	0.00	30	0	0.00
102.74	0.00	36	0	0.00
103.02	0.00	42	0	0.00
103.30	0.00	48	0	0.00
103.58	0.00	54	0	0.00
103.88	0.00	60	0	0.00

\*\*\*\*\*

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

\*\*\*\*\*





PRINT DATE: 05-19-2004  
PRINT TIME: 13:25:46

FILE DATE: 05-19-2004  
FILE NAME: F10

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 98.40  
CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
6.00	98.64	0.769	2.15	0.30
12.00	98.76	0.798	2.72	0.45
18.00	98.85	0.812	3.11	0.57
24.00	98.93	0.821	3.41	0.67
30.00	99.00	0.828	3.65	0.75
36.00	99.07	0.833	3.86	0.83
42.00	99.12	0.837	4.04	0.90
48.00	99.18	0.840	4.21	0.97
54.00	99.23	0.843	4.35	1.03
60.00	99.28	0.845	4.49	1.09

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*

CURRENT DATE: 05-19-2004  
 CURRENT TIME: 13:46:47

FILE DATE: 05-19-2004  
 FILE NAME: F11

\*\*\*\*\*  
 \*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
 \*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
 \*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCB	4.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*

\*\*\*\*\*  
 SUMMARY OF CULVERT FLOWS (CFS) FILE: F11 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
100.93	11	11	0	0	0	0	0	0	1
101.48	22	22	0	0	0	0	0	0	1
101.94	33	33	0	0	0	0	0	0	1
102.36	44	44	0	0	0	0	0	0	1
102.75	55	55	0	0	0	0	0	0	1
103.11	66	66	0	0	0	0	0	0	1
103.46	77	77	0	0	0	0	0	0	1
103.80	88	88	0	0	0	0	0	0	1
104.15	99	99	0	0	0	0	0	0	1
104.25	102	102	0	0	0	0	0	0	1
110.00	223	223	0	0	0	0	0	0	OVERTOPPING

\*\*\*\*\*

\*\*\*\*\*  
 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F11 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
100.93	0.00	11	0	0.00
101.48	0.00	22	0	0.00
101.94	0.00	33	0	0.00
102.36	0.00	44	0	0.00
102.75	0.00	55	0	0.00
103.11	0.00	66	0	0.00
103.46	0.00	77	0	0.00
103.80	0.00	88	0	0.00
104.15	0.00	99	0	0.00
104.25	0.00	102	0	0.00

\*\*\*\*\*

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

\*\*\*\*\*



C RENT DATE: 05-19-2004  
C RENT TIME: 13:46:47

FILE DATE: 05-19-2004  
FILE NAME: F11

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 98.40  
CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
11.00	98.74	0.795	2.65	0.43
22.00	98.91	0.819	3.31	0.63
33.00	99.04	0.830	3.76	0.79
44.00	99.14	0.838	4.10	0.93
55.00	99.24	0.843	4.38	1.04
66.00	99.32	0.848	4.62	1.15
77.00	99.40	0.851	4.83	1.25
88.00	99.47	0.854	5.01	1.33
99.00	99.54	0.857	5.18	1.42
102.00	99.55	0.857	5.23	1.44

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*





CURRENT DATE: 05-19-2004  
CURRENT TIME: 13:52:24

FILE DATE: 05-19-2004  
FILE NAME: F12

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 98.40  
CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
24.00	98.93	0.821	3.41	0.67
48.00	99.18	0.840	4.21	0.97
72.00	99.36	0.850	4.73	1.20
96.00	99.52	0.856	5.14	1.40
120.00	99.65	0.861	5.47	1.56
144.00	99.77	0.865	5.75	1.71
168.00	99.88	0.868	6.00	1.85
192.00	99.98	0.872	6.22	1.98
216.00	100.08	0.874	6.42	2.09
236.00	100.15	0.876	6.58	2.18

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*



DP F13 upper local roadway

RENT DATE: 05-19-2004  
 CURRENT TIME: 14:17:54

FILE DATE: 05-19-2004  
 FILE NAME: F13

\*\*\*\*\*  
 \*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
 \*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
 \*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCP	3.00	3.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*  
 SUMMARY OF CULVERT FLOWS (CFS) FILE: F13 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
100.78	4	4	0	0	0	0	0	0	1
101.12	7	7	0	0	0	0	0	0	1
101.39	11	11	0	0	0	0	0	0	1
101.66	14	14	0	0	0	0	0	0	1
101.91	18	18	0	0	0	0	0	0	1
102.14	21	21	0	0	0	0	0	0	1
102.35	25	25	0	0	0	0	0	0	1
102.56	28	28	0	0	0	0	0	0	1
102.67	30	30	0	0	0	0	0	0	1
102.96	35	35	0	0	0	0	0	0	1
110.00	100	100	0	0	0	0	0	0	1

HWID= .9

\*\*\*\*\*  
 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F13 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
100.78	0.00	4	0	0.00
101.12	0.00	7	0	0.00
101.39	0.00	11	0	0.00
101.66	0.00	14	0	0.00
101.91	0.00	18	0	0.00
102.14	0.00	21	0	0.00
102.35	0.00	25	0	0.00
102.56	0.00	28	0	0.00
102.67	0.00	30	0	0.00
102.96	0.00	35	0	0.00

\*\*\*\*\*  
 <1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000



CURRENT DATE: 05-19-2004  
CURRENT TIME: 14:17:54

FILE DATE: 05-19-2004  
FILE NAME: F13

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 98.40  
CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
3.50	98.58	0.744	1.78	0.22
7.00	98.67	0.776	2.27	0.33
10.50	98.74	0.793	2.61	0.42
14.00	98.79	0.804	2.87	0.49
17.50	98.85	0.811	3.08	0.56
21.00	98.90	0.817	3.27	0.62
24.50	98.94	0.822	3.43	0.67
28.00	98.98	0.826	3.57	0.73
30.00	99.00	0.828	3.65	0.75
35.00	99.06	0.832	3.83	0.82

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*

DB19 OUTLET OF  
DETENTION BASIN<sup>1</sup>

CURRENT DATE: 05-19-2004  
CURRENT TIME: 16:28:35

FILE DATE: 05-19-2004  
FILE NAME: DB19

\*\*\*\*\*  
 FHWA CULVERT ANALYSIS \*\*\*\*\*  
 HY-8, VERSION 3.2 \*\*\*\*\*  
 \*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	95.20	240.05	1 RCP	3.50	3.50	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*  
 SUMMARY OF CULVERT FLOWS (CFS) FILE: DB19 DATE: 05-19-2004  
 \*\*\*\*\*

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
101.29	10	10	0	0	0	0	0	0	1
101.90	20	20	0	0	0	0	0	0	1
102.45	30	30	0	0	0	0	0	0	1
102.93	40	40	0	0	0	0	0	0	1
103.39	50	50	0	0	0	0	0	0	1
103.88	60	60	0	0	0	0	0	0	1
104.42	70	70	0	0	0	0	0	0	1
105.05	80	80	0	0	0	0	0	0	1
105.76	90	90	0	0	0	0	0	0	1
106.57	100	100	0	0	0	0	0	0	1
110.00	134	134	0	0	0	0	0	0	1

\*\*\*\*\*  
 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: DB19 DATE: 05-19-2004  
 \*\*\*\*\*

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
101.29	0.00	10	0	0.00
101.90	0.00	20	0	0.00
102.45	0.00	30	0	0.00
102.93	0.00	40	0	0.00
103.39	0.00	50	0	0.00
103.88	0.00	60	0	0.00
104.42	0.00	70	0	0.00
105.05	0.00	80	0	0.00
105.76	0.00	90	0	0.00
106.57	0.00	100	0	0.00

\*\*\*\*\*  
 <1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000  
 \*\*\*\*\*



CURRENT DATE: 05-19-2004  
CURRENT TIME: 16:28:35

FILE DATE: 05-19-2004  
FILE NAME: DB19

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 95.20  
CULVERT NO.1 OUTLET INVERT ELEVATION 95.20 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	95.20	0.000	0.00	0.00
10.00	95.53	0.791	2.56	0.41
20.00	95.68	0.816	3.22	0.60
30.00	95.80	0.828	3.65	0.75
40.00	95.91	0.836	3.98	0.88
50.00	96.00	0.841	4.26	0.99
60.00	96.08	0.845	4.49	1.09
70.00	96.15	0.849	4.70	1.19
80.00	96.22	0.852	4.88	1.27
90.00	96.28	0.855	5.04	1.35
100.00	96.34	0.857	5.20	1.43

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*

DB18. outlet of  
detection basin 1

CURRENT DATE: 05-19-2004  
CURRENT TIME: 16:33:00

FILE DATE: 05-19-2004  
FILE NAME: DB18

\*\*\*\*\*  
\*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
\*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
\*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	95.20	240.05	1 RCP	4.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*  
\*\*\*\*\*

SUMMARY OF CULVERT FLOWS (CFS) FILE: DB18 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
101.53	15	15	0	0	0	0	0	0	1
102.27	30	30	0	0	0	0	0	0	1
102.92	45	45	0	0	0	0	0	0	1
103.50	60	60	0	0	0	0	0	0	1
104.08	75	75	0	0	0	0	0	0	1
104.70	90	90	0	0	0	0	0	0	1
105.41	105	105	0	0	0	0	0	0	1
106.24	120	120	0	0	0	0	0	0	1
107.19	135	135	0	0	0	0	0	0	1
107.53	140	140	0	0	0	0	0	0	1
110.00	171	171	0	0	0	0	0	0	1

\*\*\*\*\*  
\*\*\*\*\*

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: DB18 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
101.53	0.00	15	0	0.00
102.27	0.00	30	0	0.00
102.92	0.00	45	0	0.00
103.50	0.00	60	0	0.00
104.08	0.00	75	0	0.00
104.70	0.00	90	0	0.00
105.41	0.00	105	0	0.00
106.24	0.00	120	0	0.00
107.19	0.00	135	0	0.00
107.53	0.00	140	0	0.00

\*\*\*\*\*  
<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000  
\*\*\*\*\*

CURRENT DATE: 05-19-2004  
 RENT TIME: 16:33:00

FILE DATE: 05-19-2004  
 FILE NAME: DB18

\*\*\*\*\*  
 \*\*\*\*\* CULVERT # 1 \*\*\*\*\*  
 \*\*\*\*\*

PERFORMANCE CURVE FOR 1 BARREL(S)

Q (cfs)	HWE (ft)	TWE (ft)	ICH (ft)	OCH (ft)	FLOW TYPE	CCE (ft)	FCE (ft)	TCE (ft)	VO (fps)
0	100.00	95.20	0.00	-4.80	0-NF	0.00	100.00	0.00	0.00
15	101.53	95.61	1.53	-2.18	6-FF	0.00	0.00	0.00	10.30
30	102.27	95.80	2.27	-1.77	6-FF	0.00	0.00	0.00	12.46
45	102.92	95.95	2.92	-1.30	6-FF	0.00	0.00	0.00	13.15
60	103.50	96.08	3.50	-0.75	6-FF	0.00	0.00	0.00	14.37
75	104.08	96.18	4.08	-0.11	6-FF	0.00	0.00	0.00	15.08
90	104.70	96.28	4.70	0.63	6-FF	0.00	0.00	0.00	15.77
105	105.41	96.37	5.41	1.46	6-FF	0.00	0.00	0.00	16.38
120	106.24	96.45	6.24	2.38	6-FF	0.00	0.00	0.00	16.91
135	107.19	96.53	7.19	3.40	6-FF	0.00	0.00	0.00	17.34
140	107.53	96.55	7.53	3.77	6-FF	0.00	0.00	0.00	17.46

El. inlet face invert 100.00 ft El. outlet invert 95.20 ft  
 El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

\*\*\*\*\*

\* \*\* SITE DATA \*\*\*\*\* CULVERT INVERT \*\*\*\*\*  
 INLET STATION (FT) 100.00  
 INLET ELEVATION (FT) 100.00  
 OUTLET STATION (FT) 340.00  
 OUTLET ELEVATION (FT) 95.20  
 NUMBER OF BARRELS 1.00  
 SLOPE (V-FT/H-FT) 0.0200  
 CULVERT LENGTH ALONG SLOPE (FT) 240.05

\*\*\*\*\* CULVERT DATA SUMMARY \*\*\*\*\*  
 BARREL SHAPE CIRCULAR  
 BARREL DIAMETER 4.00 FT  
 BARREL MATERIAL CONCRETE  
 BARREL MANNING'S N 0.012  
 INLET TYPE CONVENTIONAL  
 INLET EDGE AND WALL SQUARE EDGE WITH HEADWALL  
 INLET DEPRESSION NONE

\*\*\*\*\*



CURRENT DATE: 05-19-2004  
PRINT TIME: 16:33:00

FILE DATE: 05-19-2004  
FILE NAME: DB18

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 95.20  
CULVERT NO.1 OUTLET INVERT ELEVATION 95.20 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	95.20	0.000	0.00	0.00
15.00	95.61	0.806	2.93	0.51
30.00	95.80	0.828	3.65	0.75
45.00	95.95	0.839	4.13	0.94
60.00	96.08	0.845	4.49	1.09
75.00	96.18	0.851	4.79	1.23
90.00	96.28	0.855	5.04	1.35
105.00	96.37	0.858	5.27	1.46
120.00	96.45	0.861	5.47	1.56
135.00	96.53	0.863	5.65	1.66
140.00	96.55	0.864	5.70	1.69

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*

F23 - BRIDGE BLDG 1

CURRENT DATE: 05-21-2004  
 CURRENT TIME: 09:22:08

FILE DATE: 05-19-2004  
 FILE NAME: F23

\*\*\*\*\*  
 \*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
 \*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
 \*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	96.80	160.03	1 RCP	4.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*  
 \*\*\*\*\* FILE: F23 CULVERT HEADWATER ELEVATION (FT) DATE: 05-19-2004 \*\*\*\*\*

DISCHARGE	1	2	3	4	5	6	ROADWAY
0	100.00	0.00	0.00	0.00	0.00	0.00	110.00
8	101.07	0.00	0.00	0.00	0.00	0.00	110.09
15	101.53	0.00	0.00	0.00	0.00	0.00	110.14
23	101.90	0.00	0.00	0.00	0.00	0.00	110.18
30	102.27	0.00	0.00	0.00	0.00	0.00	110.22
38	102.61	0.00	0.00	0.00	0.00	0.00	110.25
45	102.92	0.00	0.00	0.00	0.00	0.00	110.28
53	103.22	0.00	0.00	0.00	0.00	0.00	110.31
60	103.50	0.00	0.00	0.00	0.00	0.00	110.34
68	103.79	0.00	0.00	0.00	0.00	0.00	110.37
69	103.84	0.00	0.00	0.00	0.00	0.00	110.37

\*\*\*\*\*  
 \*\*\*\*\* HW/D = .95 \*\*\*\*\*



CURRENT DATE: 05-21-2004  
PRINT TIME: 09:22:08

FILE DATE: 05-19-2004  
FILE NAME: F23

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 96.80  
CULVERT NO.1 OUTLET INVERT ELEVATION 96.80 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	96.80	0.000	0.00	0.00
7.50	97.08	0.779	2.32	0.35
15.00	97.21	0.806	2.93	0.51
22.50	97.32	0.819	3.34	0.64
30.00	97.40	0.828	3.65	0.75
37.50	97.48	0.834	3.91	0.85
45.00	97.55	0.839	4.13	0.94
52.50	97.62	0.842	4.32	1.02
60.00	97.68	0.845	4.49	1.09
67.50	97.73	0.848	4.65	1.16
69.00	97.74	0.849	4.68	1.18

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*

REPORT DATE: 05-19-2004  
 CURRENT TIME: 17:00:28

FILE DATE: 05-19-2004  
 FILE NAME: F14

\*\*\*\*\*  
 \*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
 \*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
 \*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	96.80	160.03	1 RCB	8.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*  
 SUMMARY OF CULVERT FLOWS (CFS) FILE: F14 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
100.93	22	22	0	0	0	0	0	0	1
101.48	44	44	0	0	0	0	0	0	1
101.94	66	66	0	0	0	0	0	0	1
102.36	88	88	0	0	0	0	0	0	1
102.75	110	110	0	0	0	0	0	0	1
103.11	132	132	0	0	0	0	0	0	1
103.46	154	154	0	0	0	0	0	0	1
103.80	176	176	0	0	0	0	0	0	1
104.15	198	198	0	0	0	0	0	0	1
104.35	210	210	0	0	0	0	0	0	1
110.00	445	445	0	0	0	0	0	0	OVERTOPPING

\*\*\*\*\*  
 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F14 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
100.93	0.00	22	0	0.00
101.48	0.00	44	0	0.00
101.94	0.00	66	0	0.00
102.36	0.00	88	0	0.00
102.75	0.00	110	0	0.00
103.11	0.00	132	0	0.00
103.46	0.00	154	0	0.00
103.80	0.00	176	0	0.00
104.15	0.00	198	0	0.00
104.35	0.00	210	0	0.00

\*\*\*\*\*  
 <1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000  
 \*\*\*\*\*



CURRENT DATE: 05-19-2004  
CURRENT TIME: 17:00:28

FILE DATE: 05-19-2004  
FILE NAME: F14

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 96.80  
CULVERT NO.1 OUTLET INVERT ELEVATION 96.80 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	96.80	0.000	0.00	0.00
22.00	97.31	0.819	3.31	0.63
44.00	97.54	0.838	4.10	0.93
66.00	97.72	0.848	4.62	1.15
88.00	97.87	0.854	5.01	1.33
110.00	98.00	0.859	5.34	1.50
132.00	98.11	0.863	5.61	1.64
154.00	98.22	0.866	5.86	1.77
176.00	98.32	0.870	6.08	1.89
198.00	98.41	0.872	6.27	2.01
210.00	98.45	0.874	6.37	2.06

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*

CURRENT DATE: 05-21-2004  
CURRENT TIME: 09:29:06

FILE DATE: 05-19-2004  
FILE NAME: F24

\*\*\*\*\*  
\*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
\*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
\*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCB	8.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*  
\*\*\*\*\* SUMMARY OF CULVERT FLOWS (CFS) FILE: F24 DATE: 05-19-2004 \*\*\*\*\*

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
100.84	19	19	0	0	0	0	0	0	1
101.34	38	38	0	0	0	0	0	0	1
101.76	57	57	0	0	0	0	0	0	1
102.13	76	76	0	0	0	0	0	0	1
102.49	95	95	0	0	0	0	0	0	1
102.82	114	114	0	0	0	0	0	0	1
103.13	133	133	0	0	0	0	0	0	1
103.43	152	152	0	0	0	0	0	0	1
103.72	171	171	0	0	0	0	0	0	1
103.86	180	180	0	0	0	0	0	0	1
110.00	445	445	0	0	0	0	0	0	1

*Hw/D<sub>o</sub> = .98*

\*\*\*\*\*  
\*\*\*\*\* SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F24 DATE: 05-19-2004 \*\*\*\*\*

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
100.84	0.00	19	0	0.00
101.34	0.00	38	0	0.00
101.76	0.00	57	0	0.00
102.13	0.00	76	0	0.00
102.49	0.00	95	0	0.00
102.82	0.00	114	0	0.00
103.13	0.00	133	0	0.00
103.43	0.00	152	0	0.00
103.72	0.00	171	0	0.00
103.86	0.00	180	0	0.00

\*\*\*\*\*  
<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000  
\*\*\*\*\*





CURRENT DATE: 05-21-2004  
CURRENT TIME: 09:29:06

FILE DATE: 05-19-2004  
FILE NAME: F24

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 98.40  
CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
19.00	98.87	0.814	3.16	0.59
38.00	99.09	0.834	3.92	0.86
57.00	99.25	0.844	4.42	1.06
76.00	99.39	0.851	4.81	1.24
95.00	99.51	0.856	5.12	1.39
114.00	99.62	0.860	5.39	1.52
133.00	99.72	0.863	5.62	1.65
152.00	99.81	0.866	5.83	1.76
171.00	99.90	0.869	6.03	1.87
180.00	99.93	0.870	6.11	1.91

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*

CURRENT DATE: 05-21-2004  
 CURRENT TIME: 09:25:45

FILE DATE: 05-21-2004  
 FILE NAME: F25

\*\*\*\*\*  
 \*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
 \*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
 \*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCB	10.00	5.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*  
 SUMMARY OF CULVERT FLOWS (CFS) FILE: F25 DATE: 05-21-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
101.24	31	31	0	0	0	0	0	0	1
101.60	62	62	0	0	0	0	0	0	1
102.10	93	93	0	0	0	0	0	0	1
102.54	124	124	0	0	0	0	0	0	1
102.97	155	155	0	0	0	0	0	0	1
103.36	186	186	0	0	0	0	0	0	1
103.73	217	217	0	0	0	0	0	0	1
104.09	248	248	0	0	0	0	0	0	1
104.43	279	279	0	0	0	0	0	0	1
104.74	306	306	0	0	0	0	0	0	1
110.00	663	663	0	0	0	0	0	0	1

*Handwritten: 104.74*

\*\*\*\*\*

\*\*\*\*\*  
 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F25 DATE: 05-21-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
101.24	0.00	31	0	0.00
101.60	0.00	62	0	0.00
102.10	0.00	93	0	0.00
102.54	0.00	124	0	0.00
102.97	0.00	155	0	0.00
103.36	0.00	186	0	0.00
103.73	0.00	217	0	0.00
104.09	0.00	248	0	0.00
104.43	0.00	279	0	0.00
104.74	0.00	306	0	0.00

\*\*\*\*\*  
 <1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000  
 \*\*\*\*\*



CURRENT DATE: 05-21-2004  
START TIME: 09:25:45

FILE DATE: 05-21-2004  
FILE NAME: F25

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 98.40  
CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
31.00	99.01	0.829	3.69	0.77
62.00	99.29	0.846	4.53	1.11
93.00	99.50	0.855	5.09	1.37
124.00	99.67	0.861	5.52	1.59
155.00	99.82	0.866	5.87	1.78
186.00	99.96	0.871	6.17	1.95
217.00	100.08	0.874	6.43	2.10
248.00	100.19	0.877	6.67	2.24
279.00	100.30	0.880	6.88	2.37
306.00	100.38	0.882	7.05	2.47

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*

CURRENT DATE: 05-21-2004  
 CURRENT TIME: 09:33:34

FILE DATE: 05-19-2004  
 FILE NAME: F30

\*\*\*\*\*  
 \*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
 \*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
 \*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCB	10.00	6.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*  
 \*\*\*\*\* SUMMARY OF CULVERT FLOWS (CFS) FILE: F30 DATE: 05-19-2004 \*\*\*\*\*

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
101.88	50	50	0	0	0	0	0	0	1
102.20	100	100	0	0	0	0	0	0	1
102.88	150	150	0	0	0	0	0	0	1
103.52	200	200	0	0	0	0	0	0	1
104.09	250	250	0	0	0	0	0	0	1
104.63	300	300	0	0	0	0	0	0	1
105.15	350	350	0	0	0	0	0	0	1
105.66	400	400	0	0	0	0	0	0	1
106.18	450	450	0	0	0	0	0	0	1
106.60	490	490	0	0	0	0	0	0	1
110.00	753	753	0	0	0	0	0	0	OVERTOPPING

\*\*\*\*\*  
 \*\*\*\*\* SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F30 DATE: 05-19-2004 \*\*\*\*\*

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
101.88	0.00	50	0	0.00
102.20	0.00	100	0	0.00
102.88	0.00	150	0	0.00
103.52	0.00	200	0	0.00
104.09	0.00	250	0	0.00
104.63	0.00	300	0	0.00
105.15	0.00	350	0	0.00
105.66	0.00	400	0	0.00
106.18	0.00	450	0	0.00
106.60	0.00	490	0	0.00

\*\*\*\*\*  
 <1> TOLERANCE (FT) = 0.010      <2> TOLERANCE (%) = 1.000  
 \*\*\*\*\*



CURRENT DATE: 05-21-2004  
CURRENT TIME: 09:33:34

FILE DATE: 05-19-2004  
FILE NAME: F30

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*

BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 98.40  
CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
50.00	99.20	0.841	4.26	0.99
100.00	99.54	0.857	5.20	1.43
150.00	99.80	0.865	5.81	1.75
200.00	100.01	0.872	6.29	2.02
250.00	100.20	0.878	6.68	2.25
300.00	100.36	0.882	7.01	2.45
350.00	100.51	0.886	7.31	2.64
400.00	100.65	0.889	7.57	2.81
450.00	100.78	0.892	7.80	2.97
490.00	100.87	0.894	7.98	3.09

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 110.00

\*\*\*\*\*



DB 28 Reservoir Parkway  
 Outlet from det. basin

CURRENT DATE: 05-19-2004  
 CURRENT TIME: 18:03:27

FILE DATE: 05-19-2004  
 FILE NAME: DB28

\*\*\*\*\*  
 \*\*\*\*\* FHWA CULVERT ANALYSIS \*\*\*\*\*  
 \*\*\*\*\* HY-8, VERSION 3.2 \*\*\*\*\*  
 \*\*\*\*\*

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	95.20	240.05	1 RCB	8.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

\*\*\*\*\*  
 \*\*\*\*\*

SUMMARY OF CULVERT FLOWS (CFS) FILE: DB28 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
102.03	60	60	0	0	0	0	0	0	1
103.20	120	120	0	0	0	0	0	0	1
104.23	180	180	0	0	0	0	0	0	1
105.33	240	240	0	0	0	0	0	0	1
106.62	300	300	0	0	0	0	0	0	1
108.18	360	360	0	0	0	0	0	0	1
110.04	420	420	0	0	0	0	0	0	1
112.25	480	480	0	0	0	0	0	0	1
114.97	540	540	0	0	0	0	0	0	1
116.45	570	570	0	0	0	0	0	0	1
120.00	636	636	0	0	0	0	0	0	1

\*\*\*\*\*  
 \*\*\*\*\*

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: DB28 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
102.03	0.00	60	0	0.00
103.20	0.00	120	0	0.00
104.23	0.00	180	0	0.00
105.33	0.00	240	0	0.00
106.62	0.00	300	0	0.00
108.18	0.00	360	0	0.00
110.04	0.00	420	0	0.00
112.25	0.00	480	0	0.00
114.97	0.00	540	0	0.00
116.45	0.00	570	0	0.00

\*\*\*\*\*  
 <1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000  
 \*\*\*\*\*



CURRENT DATE: 05-19-2004  
RENT TIME: 18:03:27

FILE DATE: 05-19-2004  
FILE NAME: DB28

\*\*\*\*\*  
\*\*\*\*\* TAILWATER \*\*\*\*\*  
\*\*\*\*\*

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*  
BOTTOM WIDTH (FT) 10.00  
SIDE SLOPE H/V (X:1) 6.0  
CHANNEL SLOPE V/H (FT/FT) 0.020  
MANNING'S N (.01-0.1) 0.035  
CHANNEL INVERT ELEVATION (FT) 95.20  
CULVERT NO.1 OUTLET INVERT ELEVATION 95.20 FT

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	95.20	0.000	0.00	0.00
60.00	96.08	0.845	4.49	1.09
120.00	96.45	0.861	5.47	1.56
180.00	96.73	0.870	6.11	1.91
240.00	96.96	0.877	6.61	2.20
300.00	97.16	0.882	7.01	2.45
360.00	97.34	0.886	7.36	2.67
420.00	97.50	0.890	7.66	2.87
480.00	97.65	0.894	7.94	3.06
540.00	97.79	0.897	8.19	3.23
570.00	97.85	0.899	8.30	3.31

\*\*\*\*\*  
\*\*\*\*\* ROADWAY OVERTOPPING DATA \*\*\*\*\*  
\*\*\*\*\*

ROADWAY SURFACE PAVED  
EMBANKMENT TOP WIDTH (FT) 30.00  
CREST LENGTH (FT) 100.00  
OVERTOPPING CREST ELEVATION (FT) 120.00

\*\*\*\*\*

CUTANAL DESIGN - BASIN 'F'

Design guidelines

Side Tributaries : Try to get 5-year velocity  $\leq 5$  fps or less for grassland.  
 Try to get 100-year velocity  $\leq 7$  fps for grassland / w riprap invert.  $> 7$  fps, need  $\neq$  riprap sides.

- Since perimeter of Wolf Ranch is low density (i.e., 2.5 ac and greater lots), natural drainageways could be left as is. Check structures @ most along steep sections.

<u>"Nat. Drainageway"</u>	<u>Ex. Slope</u>	<u><math>\tau</math> @ 1' depth (lb)</u>
SB F-B	.04	2.5
<del>SB F-B</del>	<del>.031</del>	<del>1.5</del>
F9	.057	3.4
F10	.04	2.5
F11	.038	2.4
F12	.042	2.6
F12A	.034	2.2
F13	.05	3.1
F7	.031	1.9
F14	.042	2.6

$\tau = 8ds = 8s$  for  $d=1'$

- Channel SB F-8  $Q_{100} = 69 \text{ cfs}$   $T = 2.5 \text{ e } 12''$   
 $69 \text{ cfs}$  would be  $< 12''$  deep  $\therefore T < 2.5$   
recommend leave as is.

~~- Channel SB F-20  $T < 2.1$  allowable for gravel lined  
leave as is.~~

- Channel F9  $Q_{100} = 152 \text{ cfs}$   
drain-gully is very wide,  $> 50 \text{ BW}$   
 $\therefore T < 3.6$  leave as is.

- Channel F10:  $Q_{100} = 48 \text{ cfs}$   $T = 2.5 \text{ pcf}$   
low flows,  $T < 2.5$  leave as is.

- Channel F11:  $Q_{100} = 102 \text{ cfs}$   $T = 2.4 \text{ pcf}$   
 $d < 12''$   $\therefore T < 2.4$   
leave as is.

- Channel F12:  $Q_{100} = 144 \text{ cfs}$   $T = 2.6 \text{ pcf}$   
very broad flow path,  $>> 50'$   
 $\therefore d < 12''$ ,  $T < 2.6$  leave as is.

- Channel 12A:  $Q_{100} = 51 \text{ cfs}$   $T = 2.2 \text{ pcf}$   
very broad flow path;  $>> 50'$   
 $\therefore d < 12''$ ,  $T < 2.2 \text{ pcf}$   
leave as is.

- channel F13 :  $Q_{100} = 21 \text{ cfs}$   $T = 3.1$   
 very low flow; may be a roadside swale.  
 w/  $d = .5$  (dc for 21 cfs)  $\tau = 1.55 \text{ psf}$   
 $\therefore$  leave as is or grasslined swale.

Improved drainage ways

- FB (to conform w/ F13)  
 $Q_5$  range 15  $\rightarrow$  25 cfs  $\pm$   
 $Q_{100}$  range 6 cfs  $\rightarrow$  80 cfs  $\pm$   
 Slope = .037 %  
 - area has broad flow path; cutting through low density vegetation  
 $\therefore$  use BW 15'  
 Sys Velocity = 4.2 cfs  $\therefore$  dc for grassland  
 100 yr = 6.1 fps "need riprap" invert  
 No grade control proposed.

- F14  
 $Q_5 = 18 \rightarrow 56$   
 $Q_{100} = 152 \rightarrow 338 \text{ cfs}$   $S = .035 \%$   
 Fairly defined flow path. use BW = 20'  
 $e S = .035$ ,  $V_5 = 5.2 \text{ fps}$   $\therefore$  no good.  
 Flatten w/ grade control.  
 $e S = 2.5 \%$   $V_5 = 4.8 \text{ cfs}$ ,  $V_{100} = 8 \text{ fps}$   $\therefore$  no good  
 flatten to 1.8%  $V_5 = 4$   $V_{100} = 7.2 \text{ cfs}$   
 $\underline{\underline{3}}$

F19 cont'd.

Grade control. Design Slope =  $1.8\%$   $L = 1850'$   
 Ex Slope =  $3.5\%$

$\therefore \Delta H = 1850 (.035 - .018) = 31.5'$  See 32

Assume 6' of drop into DB forebay(s)

$\therefore 3.2 \cdot L = 26'$  9 drops / checks

Spacing @ 3' each  $1850 / 9 = 205'$

Spacing @ 200' int.

F18A :  $Q_5 = 16$   $L = 1100'$   
 $Q_{100} = 48$

wide flow path. max BW = 15'

Slope ex. =  $.05'/1'$

100 year velocity w/ 15' BW = 5.9 ft/s

5 year velocity = 3.1 ft/s

No grade control required

F18 :  $Q_5 = 13$  ,  $Q_{100} = 102$  cfs -  $L = 1500'$

$Q_5 = F10 + F11 = 6 + 13 = 19$  cfs  
 $Q_{100} = 48 + 102 = 150$  cfs.

Slope =  $50/1500 = .033'/1'$

Assume 6' of drop can be achieved in DB forebay(s)

$\therefore \Delta H = 50 - 6 = 44$

$\therefore S = 44/1500 = .029'/1'$   $V_5 = 3.7$  ft/s  
 $V_{100} = 6.9$  ft/s

F17

$$Q_s = 24 \text{ cfs} + 3 \text{ BFI7} = 24 + 3 = 27 \text{ cfs} \quad L = 1600'$$

$$Q_{100} = 236 \text{ cfs} + 25 \text{ cfs} = 261 \text{ cfs}$$

$$S = 54/1600 = .034\%$$

Assume 6' of drop into DB Forebay.

$$\therefore S_{\text{eff}} = 54 - 6 / 1600 = .03\%$$

@ Slope = .03%,  $V_{100}$  w/ 15' BW = 8.5 fpc.   
 no good.

Flatten with grade control:

$$@ S = .02\%, \quad V_{100} = 7.1 \text{ fpc} \therefore \frac{d_c}{2}$$

$$V_5 = 3.5 \text{ fpc} \therefore \frac{d_c}{2}$$

Required grade control:

$$\Delta S = .035 \cdot .02 = .01 \times L = 16'$$

@ 3' / drop, need 3.1 drops, say 3

$$L_{\text{seg}} = 1600/3 = 533'$$

F16

This would be piped to DB18

$$Q_{100} = 3 \text{ cfs}$$

w/ 2% storm sewer slope need 24" RCP.



Lower Portions, F14/F7

$$Q_5 = 2F14 + 2F7 = 5 + 2 = 7 \text{ cfs}$$

$$Q_{100} = 53 + 30 = 83 \text{ cfs} \quad L = 750'$$

$$S = 46.24 / 750' = .029' / 1'$$

w/ 10' BW,  $S = 2.9\%$   $V_5 = 3 \text{ fps} \therefore \text{ok}$

$$V_{100} = 7.1 \text{ fps} \therefore \text{ok}$$

No grade control required.

F23

$$Q_5 = 6 \rightarrow 16$$

$$Q_{100} = 26 \rightarrow 69$$

$$L = 1050'$$

$$S = 28 / 1050 = .027' / 1'$$

w/ 10' BW,  $V_5 = 3.5 \text{ fps} \therefore \text{ok}$

$$V_{100} = 5.7 \text{ fps} \therefore \text{ok}$$

no grade control req'd.

F24

$$Q_5 = 16 \rightarrow 44$$

$$Q_{100} = 69 \rightarrow 181$$

$$L = 2200'$$

$$S = 60 / 2200 = .027' / 1'$$

w/ 15' BW,  $V_5 = 4.5 \text{ fps}$   $V_{100} = 7.1 \therefore \text{ok}$

no grade control req'd.

F25

$Q_5 = 45 \rightarrow 66$

$L = 2400'$

$Q_{100} = 210 \rightarrow 303$

$S = 66/2400 = .028\%$

w/ BW = 20',  $S = .028$ ,  $V_{100} = 8.2$  is no good  
 Try  $S = .018$ ,  $V_{100} = 6.9$  is ok.  
 $V_5 =$

Need Grade control

$\Delta S = .028 - .018 = .01 \times L = 24'$

w/ 3' per GC, need 8 drop/dumps

Spacing @ 300' int.

F30

$Q_5 = 66$

$L = 900'$

$Q_{100} = 303$

$S = 66/900 = .073\%$

Use same section as F25

$S_{req'd} = 1.8\%$  for  $V_{100} < 7$  fps.

$\therefore (.073 - .018) 900 = 11.7'$  say 12

Need 4, 3' GC/drops

spacing  $900/4 = 225'$

F29  $Q_5 = 112$   $Q_{100} = 490$   $L = 750'$   
 $S = \frac{30 - 00}{750} = .04' / 1'$

try  $BW = 20'$ ,  $V_{100} = 10.5$  fps  $\therefore$  no good.  
 cut to 2%, still need riprap.  $V_{100} = 8.2$  fps.  
 go with riprap swale.

GC:  $\Delta S = .04 - .02 = .02 \times L = 15'$   
 $\therefore$  need 5, 3' drops @ 150' interval. to close.  
 use 2- 6' sloping drops.

$\therefore$  Slope of channel =  $750(.04 - X) = 12'$   
 $X = .024' / 1'$   
 Riprap Size:  $V S^{.17} / 1.36 = 8.8(.024)^{.17}$   
 $= 3.4$   
Type 'L'

~~F21  $Q_5 = 45 \rightarrow 120$   $L = 1750'$   
 $Q_{100} = 140 \rightarrow 313$   
 $S = 50 / 1750 = .029' / 1'$~~

~~Try  $BW = 20'$  @  $S = .029$ ,  $V_{100} = 8.2$   $\therefore$  no good  
 w/  $S = 1.8\%$   $V_{100} = 6.9$  fps  $\therefore$  ok~~

~~GC:  $(.029 - .018) 1750 = .011(1750) = 19.25$~~

~~seg 21:~~

~~w/ 3'/66, need 7 drops: Int =  $1750/3 = 250'$~~

F22  $Q_5 = 20 + \frac{1}{2} \overset{SB}{F22} = 20 + \frac{1}{2}(7) = 24 \text{ cfs}$   
 $Q_{100} = 89 + \frac{1}{2} \overset{SB}{F22} = 89 + \frac{1}{2}(5) = 115 \text{ cfs}$   
 $L = 1850' \quad S = 60/1850 = .032'$

Try  $BW = 15'$ ,  $S = .032'$ ,  $V_{100} = 6.5$  is ok  $V_5 =$   
 no qc required

F22A  $Q_5 = 26 + \frac{1}{2} \overset{SB}{F22} = 30 \text{ cfs}$   
 $Q_{100} = 141 + \frac{1}{2} \overset{SB}{F22} = 167 \text{ cfs}$   
 $L = 2050' \quad S = 60/2050 = .029'$

Try  $20'$  BW,  $S = .029'$   $V_{100} = 6.7$  is ok  
 $V_5 = 3.7$  is ok  
 No GC req'd.

**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure F8: Grasslined channel 5-year**

<b>Trapezoidal Channel Capacity Calculation (Values to be Input)</b>			
Design Flow	25 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	3.7 %
Depth of Flow	0.40 ft	Manning's Roughness Coef.	0.035

Channel Area	6.6 sf
Channel Wetted Perimeter	18.3 ft
Hydraulic Radius	0.36 ft

Channel Flow Velocity	4.2 ft/sec
Channel Flow Capacity	28 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.48 ft
Top Width	26.8 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d(1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)d^{0.33}$



**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure F8: Grasslined channel 100-year**

<b>Trapezoidal Channel Capacity Calculation (Values to be Input)</b>			
Design Flow	80 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	3.7 %
Depth of Flow	0.75 ft	Manning's Roughness Coef.	0.035

Channel Area	13.5 sf
Channel Wetted Perimeter	21.2 ft
Hydraulic Radius	0.64 ft

Channel Flow Velocity	6.1 ft/sec
Channel Flow Capacity	82 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.89 ft
Top Width	30.1 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP**  
**Swale Capacity Calculation**

**Structure F19: Grasslined channel 5-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	56 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	1.8 %
Depth of Flow	0.65 ft	Manning's Roughness Coef.	0.035

Channel Area      14.7 sf  
Channel Wetted Perimeter      25.4 ft  
Hydraulic Radius      0.58 ft

Channel Flow Velocity	4.0 ft/sec
Channel Flow Capacity	58 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.74 ft
Top Width	33.9 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d \sqrt{1+z^2}^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure F19: Grasslined channel 100-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	338 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	1.8 %
Depth of Flow	1.80 ft	Manning's Roughness Coef.	0.035

Channel Area	49.0 sf
Channel Wetted Perimeter	34.8 ft
Hydraulic Radius	1.41 ft

Channel Flow Velocity	7.2 ft/sec
Channel Flow Capacity	351 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	3.02 ft
Top Width	44.1 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d \cdot (1+z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)d^{0.33}$



**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure F18A: Grasslined channel 5-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	6 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	5.0 %
Depth of Flow	0.20 ft	Manning's Roughness Coef.	0.035

Channel Area	3.2 sf
Channel Wetted Perimeter	16.6 ft
Hydraulic Radius	0.19 ft

Channel Flow Velocity	3.1 ft/sec
Channel Flow Capacity	10 cfs
Capacity Check	Okay

Freeboard	1.0 ft
Swale Depth	1.25 ft
Top Width	25.0 ft

Equations:

$$\text{Area (A)} = b(d)$$

b = width

d = depth

$$\text{Perimeter (P)} = b + 2d(1 + z^2)^{0.5}$$

z = side slope

$$\text{Hydraulic Radius} = A/P$$

$$\text{Velocity} = (1.49/n)R_n^{2/3} S^{1/2}$$

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

$$\text{Flow} = (1.49/n)AR_n^{2/3} S^{1/2}$$

$$\text{Freeboard} = 1.0 + 0.025(v)^{0.33}$$

**Wolf Ranch MDDP**  
**Swale Capacity Calculation**

**Structure F18A: Grasslined channel 100-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	48 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	5.0 %
Depth of Flow	0.55 ft	Manning's Roughness Coef.	0.035

Channel Area	9.5 sf
Channel Wetted Perimeter	19.5 ft
Hydraulic Radius	0.48 ft

Channel Flow Velocity	5.9 ft/sec
Channel Flow Capacity	56 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.67 ft
Top Width	28.4 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d(1+z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure F18: Grasslined channel 5-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	19 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.9 %
Depth of Flow	0.40 ft	Manning's Roughness Coef.	0.035

Channel Area	6.6 sf
Channel Wetted Perimeter	18.3 ft
Hydraulic Radius	0.36 ft

Channel Flow Velocity	3.7 ft/sec
Channel Flow Capacity	24 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.47 ft
Top Width	26.7 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure F18: Grasslined channel 100-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	150 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.9 %
Depth of Flow	1.15 ft	Manning's Roughness Coef.	0.035

Channel Area	22.5 sf
Channel Wetted Perimeter	24.5 ft
Hydraulic Radius	0.92 ft

Channel Flow Velocity	6.9 ft/sec
Channel Flow Capacity	155 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.33 ft
Top Width	33.6 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n) R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n) A R_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP  
Swale Capacity Calculation**

Structure F17: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	27 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.0 %
Depth of Flow	0.50 ft	Manning's Roughness Coef.	0.035

Channel Area	8.5 sf
Channel Wetted Perimeter	19.1 ft
Hydraulic Radius	0.44 ft

Channel Flow Velocity	3.5 ft/sec
Channel Flow Capacity	30 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.57 ft
Top Width	27.6 ft

**Equations:**

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d(1+z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure F17: Grasslined channel 100-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	261 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.0 %
Depth of Flow	1.70 ft	Manning's Roughness Coef.	0.035

Channel Area	37.1 sf
Channel Wetted Perimeter	29.0 ft
Hydraulic Radius	1.28 ft

Channel Flow Velocity	7.1 ft/sec
Channel Flow Capacity	263 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.91 ft
Top Width	38.3 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n) R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n) A R_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)n^{0.33}$

**Wolf Ranch MDDP**  
**Swale Capacity Calculation**

Structure F14: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	7 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	2.9 %
Depth of Flow	0.30 ft	Manning's Roughness Coef.	0.035

Channel Area	3.4 sf
Channel Wetted Perimeter	12.5 ft
Hydraulic Radius	0.27 ft

Channel Flow Velocity	3.0 ft/sec
Channel Flow Capacity	10 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.35 ft
Top Width	20.8 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d\*(1+z<sup>2</sup>)<sup>0.5</sup>

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Freeboard = 1.0 + 0.025(v)d<sup>0.33</sup>

**Wolf Ranch MDDP  
Swale Capacity Calculation**

Structure F14: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	83 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	2.9 %
Depth of Flow	0.95 ft	Manning's Roughness Coef.	0.029

Channel Area      13.1 sf  
Channel Wetted Perimeter      17.8 ft  
Hydraulic Radius      0.74 ft

Channel Flow Velocity	7.1 ft/sec
Channel Flow Capacity	93 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.13 ft
Top Width	27.0 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)^{0.33}$



**Wolf Ranch MDDP**  
**Swale Capacity Calculation**

Structure F23: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	16 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	2.7 %
Depth of Flow	0.40 ft	Manning's Roughness Coef.	0.035

Channel Area            4.6 sf  
Channel Wetted Perimeter    13.3 ft  
Hydraulic Radius            0.35 ft

Channel Flow Velocity	3.5 ft/sec
Channel Flow Capacity	16 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.46 ft
Top Width	21.7 ft

**Equations:**

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d\*(1+z<sup>2</sup>)<sup>0.5</sup>

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Freeboard = 1.0 + 0.025(v)d<sup>0.33</sup>

**Wolf Ranch MDDP**  
**Swale Capacity Calculation**

Structure F23: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	69 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	2.7 %
Depth of Flow	0.95 ft	Manning's Roughness Coef.	0.035

Channel Area	13.1 sf
Channel Wetted Perimeter	17.8 ft
Hydraulic Radius	0.74 ft

Channel Flow Velocity	5.7 ft/sec
Channel Flow Capacity	75 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	2.09 ft
Top Width	26.7 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b+2d\*(1+z<sup>2</sup>)<sup>0.5</sup>

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Freeboard = 1.0+0.025(v)d<sup>0.33</sup>

**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure F24: Grasslined channel 5-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	44 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.7 %
Depth of Flow	0.60 ft	Manning's Roughness Coef.	0.035

Channel Area	10.4 sf
Channel Wetted Perimeter	19.9 ft
Hydraulic Radius	0.52 ft

Channel Flow Velocity	4.5 ft/sec
Channel Flow Capacity	47 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.70 ft
Top Width	28.6 ft

Equations:

$$\text{Area (A)} = b(d)$$

b = width

d = depth

$$\text{Perimeter (P)} = b + 2d(1 + z^2)^{0.5}$$

z = side slope

$$\text{Hydraulic Radius} = A/P$$

$$\text{Velocity} = (1.49/n)R_n^{2/3} S^{1/2}$$

Slope (S) = Slope of the channel

n = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

$$\text{Flow} = (1.49/n)AR_n^{2/3} S^{1/2}$$

$$\text{Freeboard} = 1.0 + 0.025(v)d^{0.33}$$

**Wolf Ranch MDDP**  
**Swale Capacity Calculation**

**Structure F24: Grasslined channel 100-year**

<b>Trapezoidal Channel Capacity Calculation (Values to be Input)</b>			
Design Flow	181 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.7 %
Depth of Flow	1.30 ft	Manning's Roughness Coef.	0.035

Channel Area	26.3 sf
Channel Wetted Perimeter	25.7 ft
Hydraulic Radius	1.02 ft

Channel Flow Velocity	7.1 ft/sec
Channel Flow Capacity	186 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.49 ft
Top Width	34.9 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

$R_n$  = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP**  
**Swale Capacity Calculation**

Structure F25: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	66 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	1.8 %
Depth of Flow	0.70 ft	Manning's Roughness Coef.	0.035

Channel Area	16.0 sf
Channel Wetted Perimeter	25.8 ft
Hydraulic Radius	0.62 ft

Channel Flow Velocity	4.1 ft/sec
Channel Flow Capacity	66 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.79 ft
Top Width	34.3 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d\*(1+z<sup>2</sup>)<sup>0.5</sup>

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Freeboard = 1.0 + 0.025(v)d<sup>0.33</sup>

**Wolf Ranch MDDP**  
**Swale Capacity Calculation**

Structure F25: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	303 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	1.8 %
Depth of Flow	1.70 ft	Manning's Roughness Coef.	0.035

Channel Area      45.6 sf  
Channel Wetted Perimeter      34.0 ft  
Hydraulic Radius      1.34 ft

Channel Flow Velocity	6.9 ft/sec
Channel Flow Capacity	316 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.91 ft
Top Width	43.3 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP**  
**Swale Capacity Calculation**

**Structure F29: Riprap channel 100-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	490 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	2.4 %
Depth of Flow	2.00 ft	Manning's Roughness Coef.	0.035

Channel Area	56.0 sf
Channel Wetted Perimeter	36.5 ft
Hydraulic Radius	1.53 ft

Channel Flow Velocity	8.8 ft/sec
Channel Flow Capacity	491 cfs
Capacity Check	Okay

Freeboard	1.3 ft
Swale Depth	3.28 ft
Top Width	46.2 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d\*(1+z<sup>2</sup>)<sup>0.5</sup>

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Freeboard = 1.0 + 0.025(v)d<sup>0.33</sup>

**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure F22: Grasslined channel 5-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	24 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	3.2 %
Depth of Flow	0.40 ft	Manning's Roughness Coef.	0.035

Channel Area	6.6 sf
Channel Wetted Perimeter	18.3 ft
Hydraulic Radius	0.36 ft

Channel Flow Velocity	3.9 ft/sec
Channel Flow Capacity	26 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.47 ft
Top Width	26.8 ft

Equations:

$$\text{Area (A)} = b(d)$$

$$b = \text{width}$$

$$d = \text{depth}$$

$$\text{Perimeter (P)} = b + 2d(1+z^2)^{0.5}$$

$$z = \text{side slope}$$

$$\text{Hydraulic Radius} = A/P$$

$$\text{Velocity} = (1.49/n)R_n^{2/3} S^{1/2}$$

$$\text{Slope (S)} = \text{Slope of the channel}$$

$$n = \text{Manning's number}$$

$$R_n = \text{Hydraulic Radius (Reynold's Number)}$$

$$\text{Flow} = (1.49/n)AR_n^{2/3} S^{1/2}$$

$$\text{Freeboard} = 1.0 + 0.025(v)d^{0.33}$$



**Wolf Ranch MDDP**  
**Swale Capacity Calculation**

Structure F22: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	115 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	3.2 %
Depth of Flow	0.95 ft	Manning's Roughness Coef.	0.035

Channel Area	17.9 sf
Channel Wetted Perimeter	22.8 ft
Hydraulic Radius	0.78 ft

Channel Flow Velocity	6.5 ft/sec
Channel Flow Capacity	115 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.11 ft
Top Width	31.9 ft

Equations:

$$\text{Area (A)} = b(d)$$

$$b = \text{width}$$

$$d = \text{depth}$$

$$\text{Perimeter (P)} = b + 2d(1+z^2)^{0.5}$$

$$z = \text{side slope}$$

$$\text{Hydraulic Radius} = A/P$$

$$\text{Velocity} = (1.49/n)R_n^{2/3} S^{1/2}$$

$$\text{Slope (S)} = \text{Slope of the channel}$$

$$n = \text{Manning's number}$$

$$R_n = \text{Hydraulic Radius (Reynold's Number)}$$

$$\text{Flow} = (1.49/n)AR_n^{2/3} S^{1/2}$$

$$\text{Freeboard} = 1.0 + 0.025(v)d^{0.33}$$

**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure F22A: Grasslined channel 5-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	30 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	2.9 %
Depth of Flow	0.40 ft	Manning's Roughness Coef.	0.035

Channel Area            8.6 sf  
Channel Wetted Perimeter    23.3 ft  
Hydraulic Radius            0.37 ft

Channel Flow Velocity	3.7 ft/sec
Channel Flow Capacity	32 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.47 ft
Top Width	31.8 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d\*(1+z<sup>2</sup>)<sup>0.5</sup>

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R<sub>a</sub><sup>2/3</sup> S<sup>1/2</sup>

Slope (S) = Slope of the channel

n = Manning's number

R<sub>a</sub> = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR<sub>a</sub><sup>2/3</sup> S<sup>1/2</sup>

Freeboard = 1.0 + 0.025(v)d<sup>0.33</sup>

**Wolf Ranch MDDP**  
**Swale Capacity Calculation**

Structure F22A: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	167 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	2.9 %
Depth of Flow	1.05 ft	Manning's Roughness Coef.	0.035

Channel Area	25.4 sf
Channel Wetted Perimeter	28.7 ft
Hydraulic Radius	0.89 ft

Channel Flow Velocity	6.7 ft/sec
Channel Flow Capacity	170 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.22 ft
Top Width	37.8 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d\*(1+z<sup>2</sup>)<sup>0.5</sup>

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Slope (S) = Slope of the channel

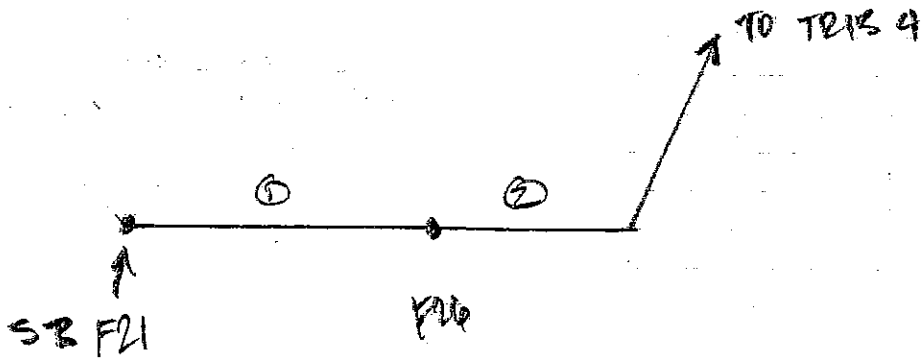
n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Freeboard = 1.0 + 0.025(v)d<sup>0.33</sup>

OUTFALL STORM SEWER, BASIN 'F'



Flow Summary

	$Q_{100}$	
c SB F21	184 cfs	→ 235
c DP F26		1/2 to DP F26
c DP F27	285 cfs	
Segment ①	$Q_{100} = 184$ cfs	

assume 1.8% Pipe Slope ∴ 48" RCP,  $Q_{full} = 193$  cfs

Segment ②  $Q_{100} = 294$  cfs → 285 c Trib 4  
 Should be able to steepen slope to 2.5 → 3%  
 ∴ 54" @ 2.2% ≈  $Q_{full} = 292$  cfs ∴ ok

~~Segment ③  $Q_{100} = 110$  → 813 cfs~~  
~~SB F21 @ 2.4%  $Q_{full}$  for 42" RCP = 1190 cfs ∴ ok~~  
~~SB to SB 20 1/2"  $Q = 70$  cfs. 36" RCP @ 2.0 = 91 cfs ∴ ok~~

Detection Basin G @ DP G3

Inflow to Det Basin =  $Q_5 = 57 \text{ cfs}$

$Q_{100} = 278 \text{ cfs}$

100yr Historic Flow @ DP G2 Figure 4 =  $130 \text{ cfs}$

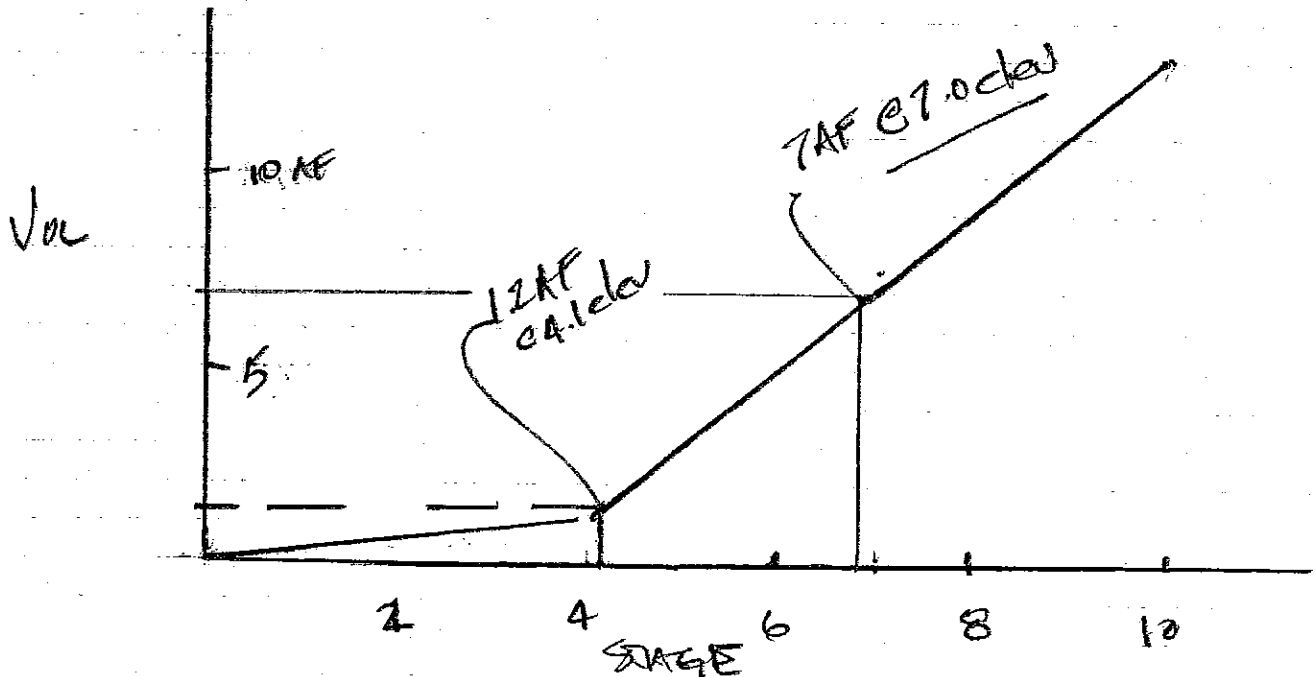
Make total flow to Tributary Four = G2 Historic.

$\therefore$  Flow @ outfall to Trib. Four = DB G + SB G4

Proposed Flow in SB G4 =  $Q_5 = 24 \text{ cfs}$

$Q_{100} = 74 \text{ cfs}$

Est. 100yr Discharge from detection basin G:  $130 - 74 = 56 \text{ cfs}$



G-Basin Hydraulics

Outfall Channels

Use same criteria as previous basins.

G3

$$Q_5 = 12 + 1/2(G3) = 12 + 25 = 37 \text{ cfs}$$

$$Q_{100} = 45 + 100 = 145 \text{ cfs}$$

$$L = 3150' \quad S = \frac{124 - 82}{3150} = .026'/1'$$

$$w/TSW = 15', S = .026 \quad V_{100} = 6.5 \text{ fps } \underline{\text{ok}}$$

$$V_5 = 4.2 \text{ fps } \underline{\text{ok}}$$

No grade control required.

G2

$$Q_5 = 5861 + 1/2 G3 = 5 + 25 = 30 \text{ cfs}$$

$$Q_{100} = 50 + 100 = 150 \text{ cfs}$$

$$L = 3250' \quad S = (166 - 82)/3250 = .026'/1'$$

$$w/ 15' TSW; S = .026'/1'$$

$$V_{100} = 6.7 \text{ fps } \underline{\text{ok}}$$

$$V_5 = 4.0 \text{ fps } \underline{\text{ok}}$$

No grade control Req'd.

**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure G2: Grasslined channel 5-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	30 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.6 %
Depth of Flow	0.50 ft	Manning's Roughness Coef.	0.035

Channel Area	8.5 sf
Channel Wetted Perimeter	19.1 ft
Hydraulic Radius	0.44 ft

Channel Flow Velocity	4.0 ft/sec
Channel Flow Capacity	34 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.58 ft
Top Width	27.6 ft

Equations:

$$\text{Area (A)} = b(d)$$

b = width

d = depth

$$\text{Perimeter (P)} = b + 2d(1 + z^2)^{0.5}$$

z = side slope

$$\text{Hydraulic Radius} = A/P$$

$$\text{Velocity} = (1.49/n)R_n^{2/3} S^{1/2}$$

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

$$\text{Flow} = (1.49/n)AR_n^{2/3} S^{1/2}$$

$$\text{Freeboard} = 1.0 + 0.025(v)d^{0.33}$$

**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure G2: Grasslined channel 100-year**

<b>Trapezoidal Channel Capacity Calculation (Values to be Input)</b>			
Design Flow	150 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.6 %
Depth of Flow	1.20 ft	Manning's Roughness Coef.	0.035

Channel Area      23.8 sf  
Channel Wetted Perimeter      24.9 ft  
Hydraulic Radius      0.95 ft

Channel Flow Velocity	6.7 ft/sec
Channel Flow Capacity	158 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.38 ft
Top Width	34.0 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) =  $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity =  $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow =  $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard =  $1.0 + 0.025(v)d^{0.33}$



**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure G3: Grasslined channel 5-year**

<b>Trapezoidal Channel Capacity Calculation (Values to be Input)</b>			
Design Flow	37 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.6 %
Depth of Flow	0.55 ft	Manning's Roughness Coef.	0.035

Channel Area      9.5 sf  
Channel Wetted Perimeter      19.5 ft  
Hydraulic Radius      0.48 ft

Channel Flow Velocity	4.2 ft/sec
Channel Flow Capacity	40 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.64 ft
Top Width	28.1 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b+2d\*(1+z<sup>2</sup>)<sup>0.5</sup>

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Slope (S) = Slope of the channel

n = Manning's number

R<sub>n</sub> = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR<sub>n</sub><sup>2/3</sup> S<sup>1/2</sup>

Freeboard = 1.0+0.025(v)d<sup>0.33</sup>

**Wolf Ranch MDDP  
Swale Capacity Calculation**

**Structure G3: Grasslined channel 100-year**

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	145 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.6 %
Depth of Flow	1.15 ft	Manning's Roughness Coef.	0.035

Channel Area	22.5 sf
Channel Wetted Perimeter	24.5 ft
Hydraulic Radius	0.92 ft

Channel Flow Velocity	6.5 ft/sec
Channel Flow Capacity	146 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.32 ft
Top Width	33.6 ft

Equations:

$$\text{Area (A)} = b(d)$$

$$b = \text{width}$$

$$d = \text{depth}$$

$$\text{Perimeter (P)} = b + 2d(1 + z^2)^{0.5}$$

$$z = \text{side slope}$$

$$\text{Hydraulic Radius} = A/P$$

$$\text{Velocity} = (1.49/n)R_n^{2/3} S^{1/2}$$

$$\text{Slope (S)} = \text{Slope of the channel}$$

$$n = \text{Manning's number}$$

$$R_n = \text{Hydraulic Radius (Reynold's Number)}$$

$$\text{Flow} = (1.49/n)AR_n^{2/3} S^{1/2}$$

$$\text{Freeboard} = 1.0 + 0.025(v)d^{0.33}$$

Pipe Alternation, Reach GA

$$Q_{100} = \frac{111 \text{ cfs out of DB 'G'}}{DR 'G'} = \dots$$

use RCP ;  $S = 2.8\%$

$$36'' \text{ RCP @ } 2.8\% \quad Q_{100} = \underline{112 \text{ cfs}} \therefore \text{ok}$$

CULVERT OUT OF DB 'G'

CURRENT DATE: 02-14-2005  
 CURRENT TIME: 13:58:44

FILE DATE: 02-14-2005  
 FILE NAME: DBGOUT

FHWA CULVERT ANALYSIS  
 HY-8, VERSION 6.1

C U L V E R T N O.	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (ft)	OUTLET ELEV. (ft)	CULVERT LENGTH (ft)	BARRELS SHAPE MATERIAL	SPAN (ft)	RISE (ft)	MANNING n	INLET TYPE
1	100.00	94.00	200.09	1 RCP	3.50	3.50	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (cfs)

FILE: DBGOUT

DATE: 02-14-2005

ELEV (ft)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	1
101.34	12.0	12.0	0.0	0.0	0.0	0.0	0.0	0.00	1
102.11	24.0	24.0	0.0	0.0	0.0	0.0	0.0	0.00	1
102.72	36.0	36.0	0.0	0.0	0.0	0.0	0.0	0.00	1
103.28	48.0	48.0	0.0	0.0	0.0	0.0	0.0	0.00	1
103.86	60.0	60.0	0.0	0.0	0.0	0.0	0.0	0.00	1
104.52	72.0	72.0	0.0	0.0	0.0	0.0	0.0	0.00	1
105.30	84.0	84.0	0.0	0.0	0.0	0.0	0.0	0.00	1
106.22	96.0	96.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.27	108.0	108.0	0.0	0.0	0.0	0.0	0.0	0.00	1
107.55	111.0	111.0	0.0	0.0	0.0	0.0	0.0	0.00	1
110.00	134.0	134.0	0.0	0.0	0.0	0.0	0.0	0.00	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS

FILE: DBGOUT

DATE: 02-14-2005

HEAD ELEV (ft)	HEAD ERROR (ft)	TOTAL FLOW (cfs)	FLOW ERROR (cfs)	% FLOW ERROR
100.00	0.000	0.00	0.00	0.00
101.34	0.000	12.00	0.00	0.00
102.11	0.000	24.00	0.00	0.00
102.72	0.000	36.00	0.00	0.00
103.28	0.000	48.00	0.00	0.00
103.86	0.000	60.00	0.00	0.00
104.52	0.000	72.00	0.00	0.00
105.30	0.000	84.00	0.00	0.00
106.22	0.000	96.00	0.00	0.00
107.27	0.000	108.00	0.00	0.00
107.55	0.000	111.00	0.00	0.00

<1> TOLERANCE (ft) = 0.010

<2> TOLERANCE (%) = 1.000

CURRENT DATE: 02-14-2005  
 START TIME: 13:58:44

FILE DATE: 02-14-2005  
 FILE NAME: DBGOUT

PERFORMANCE CURVE FOR CULVERT 1 - 1( 3.50 (ft) BY 3.50 (ft)) RCP

DIS- CHARGE FLOW (cfs)	HEAD- WATER ELEV. (ft)	INLET CONTROL DEPTH (ft)	OUTLET CONTROL DEPTH (ft)	FLOW TYPE <F4>	NORMAL DEPTH (ft)	CRIT. DEPTH (ft)	OUTLET DEPTH (ft)	TW DEPTH (ft)	OUTLET VEL. (fps)	TW VEL. (fps)
0.00	100.00	0.00	0.00	0-NF	0.00	0.00	0.00	0.00	0.00	0.00
12.00	101.34	1.34	1.34	1-S2n	0.57	1.05	0.59	0.29	10.86	3.76
24.00	102.11	2.11	2.11	1-S2n	0.83	1.50	0.85	0.43	13.25	4.78
36.00	102.72	2.72	2.72	1-S2n	1.03	1.85	0.95	0.54	16.82	5.48
48.00	103.28	3.28	3.28	1-S2n	1.19	2.16	1.23	0.64	15.87	6.02
60.00	103.86	3.86	3.86	5-S2n	1.35	2.42	1.40	0.72	16.62	6.46
72.00	104.52	4.52	4.52	5-S2n	1.49	2.65	1.57	0.80	17.24	6.84
84.00	105.30	5.30	5.30	5-S2n	1.63	2.85	1.72	0.87	17.90	7.18
96.00	106.22	6.22	6.22	5-S2n	1.77	3.00	1.87	0.93	18.38	7.48
108.00	107.27	7.27	7.27	5-S2n	1.89	3.15	2.01	1.00	18.88	7.75
111.00	107.55	7.55	7.55	5-S2n	1.93	3.19	2.05	1.01	18.96	7.82
El. inlet face invert					100.00 ft	El. outlet invert			94.00 ft	
El. inlet throat invert					0.00 ft	El. inlet crest			0.00 ft	

\*\* SITE DATA \*\*\*\*\* CULVERT INVERT \*\*\*\*\*

INLET STATION	100.00 ft
INLET ELEVATION	100.00 ft
OUTLET STATION	300.00 ft
OUTLET ELEVATION	94.00 ft
NUMBER OF BARRELS	1
SLOPE (V/H)	0.0300
CULVERT LENGTH ALONG SLOPE	200.09 ft

\*\*\*\*\* CULVERT DATA SUMMARY \*\*\*\*\*

BARREL SHAPE	CIRCULAR
BARREL DIAMETER	3.50 ft
BARREL MATERIAL	CONCRETE
BARREL MANNING'S n	0.012
INLET TYPE	CONVENTIONAL
INLET EDGE AND WALL	SQUARE EDGE WITH HEADWALL
INLET DEPRESSION	NONE

CURRENT DATE: 02-14-2005  
 RENT TIME: 13:58:44

FILE DATE: 02-14-2005  
 FILE NAME: DBGOUT

---



---

TAILWATER

---



---

\*\*\*\*\* REGULAR CHANNEL CROSS SECTION \*\*\*\*\*

BOTTOM WIDTH	10.00 ft
SIDE SLOPE H/V (X:1)	4.0
CHANNEL SLOPE V/H (ft/ft)	0.035
MANNING'S n (.01-0.1)	0.030
CHANNEL INVERT ELEVATION	94.00 ft
CULVERT NO.1 OUTLET INVERT ELEVATION	94.00 ft

\*\*\*\*\* UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (cfs)	W.S.E. (ft)	FROUDE NUMBER	DEPTH (ft)	VEL. (f/s)	SHEAR (psf)
0.00	94.00	0.000	0.00	0.00	0.00
12.00	94.29	1.237	0.29	3.76	0.63
24.00	94.43	1.286	0.43	4.78	0.94
36.00	94.54	1.313	0.54	5.48	1.18
48.00	94.64	1.330	0.64	6.02	1.39
60.00	94.72	1.341	0.72	6.46	1.57
72.00	94.80	1.350	0.80	6.84	1.74
84.00	94.87	1.357	0.87	7.18	1.90
96.00	94.93	1.363	0.93	7.48	2.04
108.00	95.00	1.368	1.00	7.75	2.18
111.00	95.01	1.369	1.01	7.82	2.21

---



---

ROADWAY OVERTOPPING DATA

---



---

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH	60.00 ft
CREST LENGTH	100.00 ft
OVERTOPPING CREST ELEVATION	110.00 ft

---



---

H/B Box Hydraulics

H-1 att'll to Cottonwood Creek

$$Q_{100} = 63 \text{ cfs}$$

Assume 2% of Storm Sewer

∴ Need 30" pipe @ 2.4%

H-2: direct discharge to creek via <sup>onsite</sup> detection basin outlet structure(s).

J-1: "

J-2: "

Product Line Estimation: Tributary 4

Per page 12 of the criteria, use method outlined in 3.3.

$$EROS \text{ Setback} = 2 (BH + ID) + VW$$

This is for erosion resistant materials. Our plan would be to line the outside ponds creating a "eros. resistant" bank.

Assume ID = 2' at all XSECC.

XSEC	Max BH	ID	VW	ESetback
1	22'	2	95	140'
2	36'	2	65	140
3	22	2	95	140
4	22'	2	70	115   20
5	12'	2	85	130   115
6	16	2	80	115
11	16	2	55	115
12	16	2	140	175
13	22	2	75	125
14	12	2	60	90
15	14	2	65	100
16	12	2	60	90
17	10	2	45	70
18	10	2	35	75
19	10	2	35	60
20	10	2	35	60



PROPOSED LINE: COTTONWOOD

Same "erosion-resistant" assumption as Trk 4

XSEC	MATH	ID (I)	VW	EROS. SB
10SD.1	8'	4'	55	80
50.2	16'	4'	95'	135
50.3	20'	4'	80'	130
50.4	16'	4'	85'	125
50.5	32"	4'	70	140
60.1	28	4	140'	200
60.2	10'	↓	80'	110
60.3	14		90'	125
60.4	32'		55'	130
60.5	18		70	115
60.6	24		90'	145
60.7	18		40'	85

(1) Assume constant 4' for Cottonwood; w/ grab central in place.

```

1*****
* WATER SURFACE PROFILES *
* VERSION OF SEPTEMBER 1988 *
* ERROR: 01,02 *
* UPDATED: 4 APRIL 1989 *
* RUN DATE 7/12/ 4 TIME 16:41:24 *
*****

```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* THE HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104, (916) 551-1748 *
*****

```

```

X X XXXXXXX XXXXX XXXXX
X X X X X X X
X X X X X X
XXXXXXXX XXXX X XXXXX XXXXX
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXXXXXX

```

END OF BANNER

1 7/12/ 4 16:41:24

PAGE 1

THIS RUN EXECUTED 7/12/ 4 16:41:24

```

*****
HEC2 RELEASE DATED SEP 88 UPDATED APR 1989

```

```

ERROR CORR - 01,02
MODIFICATION -

```

```

*****

```

```

T1 WOLF RANCH MDDP, KIOWA ENGINEERING 2004 PN 03094
T2 100-YEAR DISCHARGES FROM DBPS X-SECTIONS L TO R LOOKING UPSTREAM
T3 COTTONWOOD CREEK FILENAME CC.DAT

```

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	0	2	0	0	0	0	0	0	6810	0
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	1	0	-1	0	0	0	0	0	0	0

QT 1 3477

NC	0.020	0.020	0.045	0.100	0.300	0	0	0	0	0
POWERS BOULEVARD										
X1	1040.1	14	1120	1204	0	0	0	0	0	0
GR	6860	1000	6838	1055	6836	1072	6824	1100	6822	1108
GR	6820	1120	6814	1130	6814	1140	6816	1165	6818	1204
GR	6826	1240	6834	1276	6840	1310	6846	1350		

QT	1	2733								
X1	1040.2	10	1055	1078	550	550	550	0	0	0
GR	6864	1000	6824	1055	6822	1060	6824	1068	6826	1078
GR	6828	1105	6830	1118	6838	1165	6850	1198	6854	1210

X1	1040.3	14	1195	1333	675	675	675	0	0	0
GR	6870	1000	6862	1045	6854	1150	6852	1170	6840	1195
GR	6838	1222	6834	1230	6836	1240	6838	1262	6840	1333
GR	6842	1355	6850	1410	6860	1423	6870	1462		

X1	1040.4	10	1127	1250	525	525	525	0	0	0
GR	6878	1000	6870	1050	6862	1127	6850	1155	6848	1180
GR	6846	1238	6862	1250	6872	1295	6874	1310	6876	1380

X1	1040.5	12	1142	1195	550	550	550	0	0	0
GR	6884	1000	6878	1050	6862	1115	6858	1142	6856	1165
GR	6854	1170	6852	1172	6854	1180	6856	1195	6860	1215
GR	6876	1230	6880	1290						

COWPOKE ROAD										
X1	1050.1	12	1058	1160	785	785	785	0	0	0
GR	6898	1000	6890	1030	6880	1058	6874	1080	6868	1095
GR	6868	1105	6872	1112	6876	1140	6884	1160	6892	1200
GR	6894	1215	6896	1232						

1 7/12/ 4 16:41:24

X1	1050.2	11	1124	1215	400	400	400	0	0	0
GR	6904	1000	6894	1072	6886	1090	6884	1110	6880	1124
GR	6876	1148	6872	1162	6874	1178	6880	1215	6898	1230
GR	6910	1290								

X1	1050.3	8	1090	1175	405	405	405	0	0	0
GR	6910	1000	6882	1090	6880	1120	6878	1150	6880	1158
GR	6886	1175	6900	1195	6912	1275				

QT	1	857								
X1	1050.4	13	1100	1160	540	540	540	0	0	0
GR	6920	1000	6914	1035	6896	1050	6892	1075	6912	1090
GR	6912	1100	6892	1112	6890	1120	6890	1135	6892	1160
GR	6900	1205	6912	1228	6920	1278				

X1	1050.5	15	1262	1380	490	490	490	0	0	0
----	--------	----	------	------	-----	-----	-----	---	---	---

GR	6930	1000	6924	1045	6923	1065	6924	1080	6926	1110
GR	6926	1142	6920	1190	6912	1262	6904	1290	6902	1302
GR	6900	1318	6900	1358	6904	1366	6910	1380	6922	1405

CSAGRICULTURAL

X1	1060.1	11	1107	1275	580	580	580	0	0	0
GR	6934	1000	6924	1075	6922	1088	6922	1107	6910	1123
GR	6908	1130	6910	1140	6910	1253	6914	1275	6924	1293
GR	6934	1345								

X1	1060.2	11	1100	1215	428	428	428	0	0	0
GR	6940	1000	6930	1085	6922	1100	6916	1140	6912	1155
GR	6914	1160	6916	1180	6918	1205	6920	1215	6930	1228
GR	6934	1268								

X1	1060.3	15	1065	1245	562	562	562	0	0	0
GR	6944	1000	6942	1025	6940	1065	6922	1098	6920	1108
GR	6922	1118	6924	1152	6926	1192	6932	1220	6934	1245
GR	6934	1300	6936	1320	6942	1340	6944	1362	6950	1410

X1	1060.4	8	1052	1136	443	443	443	0	0	0
GR	6950	1000	6948	1018	6932	1052	6930	1082	6926	1092
GR	6928	1100	6940	1136	6950	1153				

X1	1060.5	9	1026	1115	517	517	517	0	0	0
GR	6960	1000	6958	1015	6950	1026	6938	1032	6936	1040
GR	6938	1048	6940	1097	6950	1115	6956	1150		

X1	1060.6	10	1070	1111	300	300	300	0	0	0
GR	6962	1000	6950	1030	6946	1045	6942	1070	6938	1076
GR	6937	1090	6938	1105	6940	1111	6954	1145	6960	1203

1 7/12/ 4 16:41:24

X1	1060.7	10	1103	1153	314	314	314	0	0	0
GR	6970	1000	6968	1060	6966	1078	6950	1103	6942	1118
GR	6941	1121	6942	1124	6948	1128	6950	1153	6966	1170

BLACK FOREST ROAD

X1	1070.1	9	1155	1167	196	196	196	0	0	0
GR	6976	1000	6974	1135	6972	1145	6950	1155	6946	1158
GR	6946	1162	6950	1167	6972	1184	6974	1219		

1 7/12/ 4 16:41:24

SECNO DEPTH CWSEL CRIWS WSELK EG HV HL CLOSS BANK ELEV

Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*PROF 1  
0

CCHV= .100 CEHV= .300

\*SECNO 1040.100

3720 CRITICAL DEPTH ASSUMED

POWERS BOULEVARD

1040.10	5.80	6819.80	6819.80	6810.00	6821.61	1.81	.00	.00	6820.00
3477.	0.	3409.	68.	0.	315.	7.	0.	0.	6818.00
.00	.00	10.82	9.35	.000	.045	.020	.000	6814.00	1120.34
.018826	0.	0.	0.	0	20	0	.00	91.76	1212.09

0

\*SECNO 1040.200

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

1040.20	7.85	6829.85	6829.85	.00	6831.81	1.96	6.92	.05	6824.00
2733.	283.	1332.	1118.	24.	138.	88.	4.	1.	6826.00
.01	12.02	9.68	12.67	.020	.045	.020	.000	6822.00	1046.95
.008293	550.	550.	550.	3	14	0	.00	70.09	1117.04

0

\*SECNO 1040.300

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

1040.30	6.59	6840.59	6840.59	.00	6841.66	1.07	8.34	.09	6840.00
2733.	2.	2723.	9.	0.	327.	2.	8.	3.	6840.00
.04	4.37	8.32	4.67	.020	.045	.020	.000	6834.00	1193.78
.020369	675.	675.	675.	16	10	0	.00	145.69	1339.46

0

\*SECNO 1040.400

1040.40	4.85	6850.85	6850.76	.00	6852.34	1.49	10.55	.12	6862.00
2733.	0.	2733.	0.	0.	279.	0.	12.	4.	6862.00
.05	.00	9.79	.00	.000	.045	.000	.000	6846.00	1153.02
.019828	525.	525.	525.	7	19	0	.00	88.62	1241.64

0

\*SECNO 1040.500

7185 MINIMUM SPECIFIC ENERGY

1

7/12/ 4 16:41:24

PAGE 5

SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	HL	CLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

3720 CRITICAL DEPTH ASSUMED  
 1040.50 7.75 6859.75 6859.75 .00 6861.39 1.64 8.82 .05 6858.00  
 2733. 80. 2203. 450. 10. 226. 35. 15. 5. 6856.00  
 .07 7.75 9.77 12.82 .020 .045 .020 .000 6852.00 1130.21  
 .013225 550. 550. 550. 5 14 0 .00 83.52 1213.73

0

\*SECNO 1050.100  
 7185 MINIMUM SPECIFIC ENERGY  
 3720 CRITICAL DEPTH ASSUMED  
 COWPOKE ROAD

1050.10 7.79 6875.79 6875.79 .00 6877.70 1.91 12.70 .08 6880.00  
 2733. 0. 2733. 0. 0. 246. 0. 20. 7. 6884.00  
 .09 .00 11.10 .00 .000 .045 .000 .000 6868.00 1073.45  
 .020229 785. 785. 785. 11 5 0 .00 65.06 1138.51

0

\*SECNO 1050.200

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 2.01

1050.20 8.75 6880.75 .00 .00 6881.40 .64 3.57 .13 6880.00  
 2733. 3. 2730. 0. 1. 424. 0. 23. 7. 6880.00  
 .10 2.67 6.44 2.04 .020 .045 .020 .000 6872.00 1121.36  
 .005004 400. 400. 400. 4 0 0 .00 94.27 1215.63

0

\*SECNO 1050.300

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = .53

1050.30 5.59 6883.59 .00 .00 6885.13 1.55 3.46 .27 6882.00  
 2733. 33. 2700. 0. 4. 270. 0. 26. 8. 6886.00  
 .11 8.24 10.00 .00 .020 .045 .000 .000 6878.00 1084.90  
 .017840 405. 405. 405. 3 0 0 .00 83.26 1168.16

0

1

7/12/ 4 16:41:24

PAGE 6

SECNO	DEPTH	CWSEL	CRIWS	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*SECNO 1050.400

3265 DIVIDED FLOW

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = .39

1050.40	3.23	6893.23	6892.88	.00	6893.89	.66	8.66	.09	6912.00
857.	30.	803.	25.	5.	123.	4.	29.	9.	6892.00
.14	5.62	6.55	5.79	.020	.045	.020	.000	6890.00	1067.31
.011827	540.	540.	540.	11	11	0	.00	64.28	1166.92

0

\*SECNO 1050.500

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

1050.50	2.19	6902.19	6902.19	.00	6903.11	.92	8.13	.08	6912.00
857.	0.	857.	0.	0.	111.	0.	30.	10.	6910.00
.16	.00	7.70	.00	.000	.045	.000	.000	6900.00	1300.88
.024976	490.	490.	490.	8	14	0	.00	61.49	1362.37

0

\*SECNO 1060.100

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 1.61

CSAGRICULTURAL

1060.10	3.40	6911.40	.00	.00	6911.68	.27	8.50	.06	6922.00
857.	0.	857.	0.	0.	205.	0.	32.	11.	6914.00
.19	.00	4.17	.00	.000	.045	.000	.000	6908.00	1121.14
.009631	580.	580.	580.	6	0	0	.00	139.55	1260.69

0

\*SECNO 1060.200

3301 HV CHANGED MORE THAN HVINS

1

7/12/ 4 16:41:24

PAGE 7

SECNO	DEPTH	CWSEL	GRIWS	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = .66

1060.20	4.98	6916.98	.00	.00	6917.87	.89	6.01	.18	6922.00
857.	0.	857.	0.	0.	113.	0.	34.	12.	6920.00
.21	.00	7.55	.00	.000	.045	.000	.000	6912.00	1133.46
.022335	428.	428.	428.	4	0	0	.00	58.80	1192.26

0  
\*SECNO 1060.300

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 1.58

1060.30	5.04	6925.04	.00	.00	6925.44	.40	7.52	.05	6940.00
857.	0.	857.	0.	0.	169.	0.	36.	13.	6934.00
.24	.00	5.07	.00	.000	.045	.000	.000	6920.00	1092.43
.008900	562.	562.	562.	5	0	0	.00	80.29	1172.72

0  
\*SECNO 1060.400

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

1060.40	5.44	6931.44	6931.44	.00	6932.51	1.07	6.19	.20	6932.00
857.	0.	857.	0.	0.	103.	0.	37.	14.	6940.00
.26	.00	8.30	.00	.000	.045	.000	.000	6926.00	1060.38
.025000	443.	443.	443.	4	8	0	.00	49.95	1110.32

0  
\*SECNO 1060.500

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 1.44

1060.50	4.70	6940.70	.00	.00	6941.24	.54	8.68	.05	6950.00
857.	0.	857.	0.	0.	145.	0.	38.	14.	6950.00
.28	.00	5.90	.00	.000	.045	.000	.000	6936.00	1030.65
.012051	517.	517.	517.	6	0	0	.00	67.63	1098.27

0  
1

7/12/ 4 16:41:24

PAGE 8

SECNO	DEPTH	CWSEL	CRISW	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*SECNO 1060.600

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 2.07

1060.60	5.48	6942.48	.00	.00	6942.80	.32	1.53	.02	6942.00
---------	------	---------	-----	-----	---------	-----	------	-----	---------



857.	1.	824.	32.	1.	180.	7.	40.	15.	6940.00
.30	1.50	4.57	4.31	.020	.045	.020	.000	6937.00	1067.01
.002806	300.	300.	300.	4	0	0	.00	50.01	1117.02

0

\*SECNO 1060.700

3301 HV CHANGED MORE THAN HVINS

3685 20 TRIALS ATTEMPTED WSEL,CWSEL  
 3693 PROBABLE MINIMUM SPECIFIC ENERGY  
 3720 CRITICAL DEPTH ASSUMED

1060.70	6.50	6947.50	6947.50	.00	6949.56	2.05	2.03	.52	6950.00
857.	0.	857.	0.	0.	75.	0.	41.	15.	6950.00
.31	.00	11.50	.00	.000	.045	.000	.000	6941.00	1107.68
.027701	314.	314.	314.	20	11	0	.00	19.99	1127.67

0

\*SECNO 1070.100

7185 MINIMUM SPECIFIC ENERGY  
 3720 CRITICAL DEPTH ASSUMED  
 BLACK FOREST ROAD

1070.10	6.81	6952.81	6952.81	.00	6955.14	2.33	4.62	.08	6950.00
857.	13.	814.	29.	2.	66.	3.	41.	15.	6950.00
.31	7.38	12.39	9.58	.020	.045	.020	.000	6946.00	1153.72
.020333	196.	196.	196.	1	8	0	.00	15.45	1169.17

0

1

7/12/ 4 16:41:24

PAGE 9

THIS RUN EXECUTED 7/12/ 4 16:41:24

\*\*\*\*\*  
 HEC2 RELEASE DATED SEP 88 UPDATED APR 1989

ERROR CORR - 01,02  
 MODIFICATION -

\*\*\*\*\*

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

COTTONWOOD CREEK FILENAM

SUMMARY PRINTOUT TABLE 150

SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRWS	EG	10*KS	VCH	AREA	.01K
* 1040.100	.00	.00	.00	6814.00	3477.00	6819.80	6819.80	6821.61	188.26	10.82	322.37	253.41

*	1040.200	550.00	.00	.00	6822.00	2733.00	6829.85	6829.85	6831.81	82.93	9.68	249.36	300.12
*	1040.300	675.00	.00	.00	6834.00	2733.00	6840.59	6840.59	6841.66	203.69	8.32	329.32	191.49
	1040.400	525.00	.00	.00	6846.00	2733.00	6850.85	6850.76	6852.34	198.28	9.79	279.09	194.09
*	1040.500	550.00	.00	.00	6852.00	2733.00	6859.75	6859.75	6861.39	132.25	9.77	270.96	237.65
*	1050.100	785.00	.00	.00	6868.00	2733.00	6875.79	6875.79	6877.70	202.29	11.10	246.24	192.16
*	1050.200	400.00	.00	.00	6872.00	2733.00	6880.75	.00	6881.40	50.04	6.44	424.93	386.36
*	1050.300	405.00	.00	.00	6878.00	2733.00	6883.59	.00	6885.13	178.40	10.00	274.10	204.62
*	1050.400	540.00	.00	.00	6890.00	857.00	6893.23	6892.88	6893.89	118.27	6.55	132.11	78.80
*	1050.500	490.00	.00	.00	6900.00	857.00	6902.19	6902.19	6903.11	249.76	7.70	111.33	54.23
*	1060.100	580.00	.00	.00	6908.00	857.00	6911.40	.00	6911.68	96.31	4.17	205.41	87.33
*	1060.200	428.00	.00	.00	6912.00	857.00	6916.98	.00	6917.87	223.35	7.55	113.46	57.34
*	1060.300	562.00	.00	.00	6920.00	857.00	6925.04	.00	6925.44	89.00	5.07	169.14	90.84
*	1060.400	443.00	.00	.00	6926.00	857.00	6931.44	6931.44	6932.51	250.00	8.30	103.29	54.20
*	1060.500	517.00	.00	.00	6936.00	857.00	6940.70	.00	6941.24	120.51	5.90	145.30	78.07
*	1060.600	300.00	.00	.00	6937.00	857.00	6942.48	.00	6942.80	28.06	4.57	188.29	161.79
*	1060.700	314.00	.00	.00	6941.00	857.00	6947.50	6947.50	6949.56	277.01	11.50	74.54	51.49

1 7/12/ 4 16:41:24

PAGE 10

SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRWS	EG	10*KS	VCH	AREA	.01K	
*	1070.100	196.00	.00	.00	6946.00	857.00	6952.81	6952.81	6955.14	203.33	12.39	70.59	60.10

1 7/12/ 4 16:41:24

PAGE 11

COTTONWOOD CREEK FILENAM  
SUMMARY PRINTOUT TABLE 150

SECNO	Q	CWSEL	DIFWSP	DIFWSX	DIFKWS	TOPWID	XLCH
-------	---	-------	--------	--------	--------	--------	------

*	1040.100	3477.00	6819.80	.00	.00	9.80	91.76	.00
*	1040.200	2733.00	6829.85	.00	10.05	.00	70.09	550.00
*	1040.300	2733.00	6840.59	.00	10.73	.00	145.69	675.00
	1040.400	2733.00	6850.85	.00	10.26	.00	88.62	525.00
*	1040.500	2733.00	6859.75	.00	8.90	.00	83.52	550.00
*	1050.100	2733.00	6875.79	.00	16.04	.00	65.06	785.00
*	1050.200	2733.00	6880.75	.00	4.97	.00	94.27	400.00
*	1050.300	2733.00	6883.59	.00	2.83	.00	83.26	405.00
*	1050.400	857.00	6893.23	.00	9.64	.00	64.28	540.00
*	1050.500	857.00	6902.19	.00	8.96	.00	61.49	490.00
*	1060.100	857.00	6911.40	.00	9.22	.00	139.55	580.00
*	1060.200	857.00	6916.98	.00	5.58	.00	58.80	428.00
*	1060.300	857.00	6925.04	.00	8.05	.00	80.29	562.00
*	1060.400	857.00	6931.44	.00	6.40	.00	49.95	443.00
*	1060.500	857.00	6940.70	.00	9.26	.00	67.63	517.00
*	1060.600	857.00	6942.48	.00	1.77	.00	50.01	300.00
*	1060.700	857.00	6947.50	.00	5.03	.00	19.99	314.00
*	1070.100	857.00	6952.81	.00	5.31	.00	15.45	196.00

1

7/12/ 4 16:41:24

PAGE 12

```

1*****
* WATER SURFACE PROFILES *
* VERSION OF SEPTEMBER 1988 *
* ERROR: 01,02 *
* UPDATED: 4 APRIL 1989 *
* RUN DATE 7/12/ 4 TIME 16:39:20 *
*****

```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* THE HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104, (916) 551-1748 *
*****

```

```

X X XXXXXXXX XXXXX XXXXX
X X X X X X X X
X X X X X X X X
XXXXXXXX XXXX X XXXXX XXXXX
X X X X X X X
X X X X X X X
X X XXXXXXXX XXXXX XXXXXXXX

```

END OF BANNER

1 7/12/ 4 16:39:20

PAGE 1

THIS RUN EXECUTED 7/12/ 4 16:39:20

```

*****
HEC2 RELEASE DATED SEP 88 UPDATED APR 1989

```

ERROR CORR - 01,02  
MODIFICATION -

```

*****

```

```

T1 TRIBUTARY FOUR WOLF RANCH MDDP KIOWA ENGINEERING PN 03094
T2 100-YEAR FREQUENCY DEVELOPED W/O DETETNION X-SECTIONS L TO R UPSTREA
T3 FILENAME TRIB4.DAT

```

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	0	2	0	0	.02	0	0	0	6878	0
J2	NPROF	IPLT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	1	0	-1	0	0	0	0	0	0	0
QT	1				1870					



QT 1 1830

NORTH RESEARCH PARKWAY

X1	9	23	1086	1149	162	162	162	0	0	0
GR	6983	1000	6982	1006	6980	1018	6978	1033	6976	1059
GR	6974	1076	6972	1081	6970	1086	6968	1090	6966	1095
GR	6964	1104	6963	1112	6964	1119	6966	1141	6968	1146
GR	6970	1149	6972	1151	6974	1154	6976	1156	6978	1159
GR	6980	1161	6982	1163	6983	1164				

X1	10	20	1017	1091	411	411	411	0	0	0
GR	6990	1000	6988	1005	6986	1008	6984	1012	6982	1014
GR	6980	1017	6978	1019	6976	1024	6974	1029	6972	1037
GR	6970	1048	6972	1055	6974	1070	6976	1076	6978	1083
GR	6980	1091	6982	1099	6986	1110	6988	1126	6990	1141

X1	11	31	1048	1132	407	407	407	0	0	0
GR	7004	1000	7002	1012	7000	1018	7002	1022	7004	1025
GR	7006	1033	7008	1038	6990	1048	6988	1056	6986	1064
GR	6984	1074	6982	1081	6980	1087	6980	1090	6981	1099
GR	6980	1107	6978	1115	6978	1118	6980	1123	6982	1124
GR	6984	1126	6986	1127	6988	1129	6990	1132	6992	1135
GR	6994	1139	6996	1143	6998	1146	7000	1153	7002	1164
GR	7004	1173								

QT 1 1160

X1	12	29	1077	1291	585	585	585	0	0	0
GR	7020	1000	7018	1015	7016	1034	7014	1048	7012	1061
GR	7010	1077	7008	1096	7006	1112	7004	1134	7004	1181
GR	7002	1198	7000	1216	7000	1238	7002	1268	7004	1275
GR	7006	1279	7008	1282	7010	1291	7012	1304	7014	1325

1

7/12/ 4 16:39:20

GR	7015	1332	7014	1340	7013	1345	7014	1346	7016	1351
GR	7018	1356	7020	1362	7021	1380	7020	1409		

X1	13	23	1018	1195	443	443	443	0	0	0
GR	7028	1000	7026	1003	7024	1008	7022	1013	7020	1018
GR	7018	1022	7016	1025	7014	1041	7012	1046	7010	1053
GR	7008	1063	7007	1077	7008	1093	7010	1119	7012	1157
GR	7014	1168	7016	1177	7018	1186	7020	1195	7022	1202
GR	7024	1213	7026	1224	7028	1237				

X1	14	22	1037	1135	634	634	634	0	0	0
GR	7042	1000	7040	1009	7038	1022	7036	1033	7034	1034
GR	7032	1036	7030	1037	7028	1038	7026	1041	7024	1048

GR	7022	1066	7023	1092	7024	1114	7026	1121	7028	1127
GR	7030	1135	7032	1144	7034	1176	7036	1191	7038	1201
GR	7040	1248	7042	1263						
X1	15	26	1112	1197	438	438	438	0	0	0
GR	7054	1000	7053	1017	7053	1043	7052	1068	7050	1070
GR	7048	1074	7046	1081	7044	1086	7044	1097	7042	1106
GR	7040	1112	7038	1118	7036	1127	7035	1139	7034	1154
GR	7035	1177	7036	1188	7038	1192	7040	1197	7042	1211
GR	7044	1225	7046	1246	7046	1291	7047	1310	7050	1358
GR	7054	1392								
X1	16	18	1161	1259	352	352	352	0	0	0
GR	7060	1000	7054	1057	7053	1104	7052	1159	7050	1161
GR	7042	1173	7040	1177	7041	1200	7042	1222	7044	1233
GR	7046	1244	7048	1252	7050	1259	7052	1267	7054	1280
GR	7056	1296	7058	1315	7060	1335				
X1	17	18	1067	1163	382	382	382	0	0	0
GR	7068	1000	7064	1034	7060	1067	7058	1079	7056	1087
GR	7054	1092	7052	1097	7050	1101	7049	1111	7048	1125
GR	7049	1137	7050	1144	7054	1152	7060	1163	7062	1180
GR	7064	1209	7066	1243	7068	1285				
X1	18	21	1165	1261	416	416	416	0	0	0
GR	7076	1000	7074	1020	7073	1042	7072	1080	7072	1136
GR	7072	1153	7070	1165	7068	1173	7060	1182	7058	1185
GR	7057	1189	7056	1195	7057	1214	7058	1228	7060	1232
GR	7066	1243	7068	1249	7070	1261	7072	1277	7074	1297
GR	7076	1307								
X1	19	27	1178	1337	480	480	480	0	0	0
GR	7088	1000	7086	1038	7084	1080	7083	1096	7083	1101
GR	7083	1140	7082	1175	7080	1178	7072	1190	7070	1198
GR	7069	1206	7068	1217	7069	1223	7070	1227	7074	1235
GR	7076	1240	7078	1248	7079	1277	7078	1314	7079	1326
GR	7080	1337	7084	1371	7085	1382	7086	1395	7086	1473
GR	7087	1505	7088	1531						

1

7/12/ 4 16:39:20

PAGE 4

TRIBUTARY FOUR LIMITS										
X1	20	19	1054	1085	363	363	363	0	0	0
GR	7094	1000	7090	1024	7086	1040	7084	1044	7076	1054
GR	7075	1057	7074	1060	7075	1074	7076	1085	7078	1089
GR	7080	1093	7082	1096	7084	1100	7086	1104	7088	1108
GR	7090	1116	7092	1128	7093	1140	7094	1153		

SECNO	DEPTH	CWSEL	CRISWS	WSELK	EG	HV	HL	CLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

## \*PROF 1

CCHV= .100 CEHV= .300

## \*SECNO 1.000

TRIBUTARY FOUR

1.00	5.35	6895.35	.00	6878.00	6896.62	1.27	.00	.00	6900.00
1870.	0.	1870.	0.	0.	207.	0.	0.	0.	6900.00
.00	.00	9.03	.00	.000	.045	.000	.000	6890.00	1017.65
.020013	0.	0.	0.	0	0	8	.00	75.20	1092.84

0

## \*SECNO 2.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

2.00	5.24	6905.24	6905.24	.00	6906.60	1.36	8.88	.03	6910.00
1870.	0.	1870.	0.	0.	200.	0.	2.	1.	6910.00
.01	.00	9.36	.00	.000	.045	.000	.000	6900.00	1094.85
.021833	425.	425.	425.	4	8	0	.00	73.82	1168.67

0

## \*SECNO 3.000

3.00	3.65	6913.65	.00	.00	6914.74	1.08	8.11	.03	6920.00
1870.	0.	1870.	0.	0.	224.	0.	4.	1.	6920.00
.03	.00	8.36	.00	.000	.045	.000	.000	6910.00	1013.17
.020447	384.	384.	384.	2	0	0	.00	93.63	1106.80

0

## \*SECNO 4.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

4.00	4.09	6924.09	6924.09	.00	6925.39	1.30	9.29	.07	6930.00
1870.	0.	1870.	0.	0.	204.	0.	6.	2.	6930.00
.04	.00	9.16	.00	.000	.045	.000	.000	6920.00	1041.68
.022526	433.	433.	433.	3	8	0	.00	79.41	1121.09

0

## \*SECNO 5.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

5.00	5.16	6933.16	6933.16	.00	6934.43	1.27	8.28	.00	6940.00
1870.	0.	1870.	0.	0.	207.	0.	8.	3.	6940.00
.05	.00	9.05	.00	.000	.045	.000	.000	6928.00	1056.89
.023082	363.	363.	363.	5	11	0	.00	83.68	1140.56

0

1



SECNO	DEPTH	CWSEL	CRISW	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*SECNO 6.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

6.00	4.69	6948.69	6948.69	.00	6950.17	1.47	15.16	.06	6960.00
1870.	0.	1870.	0.	0.	192.	0.	11.	4.	6960.00
.07	.00	9.74	.00	.000	.045	.000	.000	6944.00	1023.65
.022331	668.	668.	668.	3	11	0	.00	66.82	1090.47

0

\*SECNO 7.000

7.00	5.48	6957.48	6957.41	.00	6958.75	1.27	8.57	.02	6960.00
1870.	0.	1870.	0.	0.	206.	0.	13.	5.	6960.00
.08	.00	9.06	.00	.000	.045	.000	.000	6952.00	1218.02
.021726	389.	389.	389.	5	11	0	.00	77.88	1295.91

0

\*SECNO 8.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

SOUTH RESEARCH PARKWAY

8.00	4.33	6965.33	6965.33	.00	6966.89	1.56	6.86	.08	6970.00
1870.	0.	1870.	0.	0.	187.	0.	14.	5.	6970.00
.09	.00	10.01	.00	.000	.045	.000	.000	6961.00	1051.55
.021184	320.	320.	320.	3	15	0	.00	61.12	1112.67

0

\*SECNO 9.000

NORTH RESEARCH PARKWAY

9.00	5.51	6968.51	.00	.00	6969.82	1.31	2.90	.03	6970.00
1830.	0.	1830.	0.	0.	200.	0.	15.	6.	6970.00
.09	.00	9.17	.00	.000	.045	.000	.000	6963.00	1088.98
.015283	162.	162.	162.	2	0	0	.00	57.79	1146.77

0

\*SECNO 10.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

10.00	6.10	6976.10	6976.10	.00	6977.79	1.69	7.30	.12	6980.00
1830.	0.	1830.	0.	0.	175.	0.	16.	6.	6980.00
.11	.00	10.44	.00	.000	.045	.000	.000	6970.00	1023.75
.020892	411.	411.	411.	2	8	0	.00	52.61	1076.35

0

1

SECNO	DEPTH	CWSEL	CRISW	WSELK	EG	HV	HL	OLOSS	BANK ELEV
-------	-------	-------	-------	-------	----	----	----	-------	-----------

Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*SECNO 11.000

11.00	6.06	6984.06	.00	.00	6985.53	1.48	7.72	.02	6990.00
1830.	0.	1830.	0.	0.	188.	0.	18.	7.	6990.00
.12	.00	9.75	.00	.000	.045	.000	.000	6978.00	1073.69
.017284	407.	407.	407.	3	0	0	.00	52.34	1126.03

0

\*SECNO 12.000

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

12.00	2.75	7002.75	7002.75	.00	7003.71	.95	11.50	.05	7010.00
1160.	0.	1160.	0.	0.	148.	0.	20.	7.	7010.00
.14	.00	7.84	.00	.000	.045	.000	.000	7000.00	1191.61
.024520	585.	585.	585.	10	14	0	.00	79.02	1270.63

0

\*SECNO 13.000

13.00	3.97	7010.97	.00	.00	7011.57	.61	7.83	.03	7020.00
1160.	0.	1160.	0.	0.	185.	0.	22.	8.	7020.00
.16	.00	6.26	.00	.000	.045	.000	.000	7007.00	1049.61
.013353	443.	443.	443.	5	0	0	.00	87.76	1137.38

0

\*SECNO 14.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

14.00	3.09	7025.09	7025.09	.00	7026.10	1.00	11.19	.12	7030.00
1160.	0.	1160.	0.	0.	144.	0.	25.	9.	7030.00
.18	.00	8.04	.00	.000	.045	.000	.000	7022.00	1044.18
.024389	634.	634.	634.	10	15	0	.00	73.65	1117.82

0

\*SECNO 15.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

15.00	3.13	7037.13	7037.13	.00	7038.17	1.04	10.47	.01	7040.00
1160.	0.	1160.	0.	0.	142.	0.	26.	10.	7040.00
.19	.00	8.18	.00	.000	.045	.000	.000	7034.00	1121.90
.023422	438.	438.	438.	4	5	0	.00	68.37	1190.27

0

1

7/12/ 4 16:39:20

PAGE 8

SECNO	DEPTH	CWSEL	CRISW	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*SECNO 16.000

16.00	3.92	7043.92	.00	.00	7044.77	.86	6.58	.02	7050.00
1160.	0.	1160.	0.	0.	156.	0.	27.	11.	7050.00
.21	.00	7.42	.00	.000	.045	.000	.000	7040.00	1170.13
.015269	352.	352.	352.	5	0	0	.00	62.42	1232.54

0

\*SECNO 17.000

7185 MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

17.00	3.71	7051.71	7051.71	.00	7053.01	1.30	7.04	.13	7060.00
1160.	0.	1160.	0.	0.	127.	0.	28.	11.	7060.00
.22	.00	9.15	.00	.000	.045	.000	.000	7048.00	1097.58
.022673	382.	382.	382.	3	11	0	.00	49.84	1147.42

0

\*SECNO 18.000

18.00	4.00	7060.00	.00	.00	7061.07	1.07	8.04	.02	7070.00
1160.	0.	1160.	0.	0.	140.	0.	30.	12.	7070.00
.23	.00	8.31	.00	.000	.045	.000	.000	7056.00	1182.00
.016680	416.	416.	416.	5	0	0	.00	50.01	1232.00

0

\*SECNO 19.000

7185 MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

19.00	4.46	7072.46	7072.46	.00	7073.89	1.43	9.13	.11	7080.00
1160.	0.	1160.	0.	0.	121.	0.	31.	12.	7080.00
.25	.00	9.60	.00	.000	.045	.000	.000	7068.00	1189.31
.021908	480.	480.	480.	10	8	0	.00	42.62	1231.92

0

\*SECNO 20.000

TRIBUTARY FOUR LIMITS

20.00	4.78	7078.78	.00	.00	7080.09	1.31	6.18	.01	7076.00
1160.	18.	1108.	35.	5.	119.	8.	32.	13.	7076.00
.26	3.66	9.34	4.49	.050	.045	.050	.000	7074.00	1050.53
.013610	363.	363.	363.	4	0	0	.00	40.02	1090.55

0

1

7/12/ 4 16:39:20

PAGE 9

THIS RUN EXECUTED 7/12/ 4 16:39:20

\*\*\*\*\*  
HEC2 RELEASE DATED SEP 88 UPDATED APR 1989

ERROR CORR - 01,02  
MODIFICATION -

\*\*\*\*\*

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

FILENAME TRIB4.DAT

SUMMARY PRINTOUT TABLE 150

SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRIWS	EG	10*KS	VCH	AREA	.01K
1.000	.00	.00	.00	6890.00	1870.00	6895.35	.00	6896.62	200.13	9.03	207.07	132.18
* 2.000	425.00	.00	.00	6900.00	1870.00	6905.24	6905.24	6906.60	218.33	9.36	199.69	126.56
3.000	384.00	.00	.00	6910.00	1870.00	6913.65	.00	6914.74	204.47	8.36	223.76	130.78
* 4.000	433.00	.00	.00	6920.00	1870.00	6924.09	6924.09	6925.39	225.26	9.16	204.15	124.60
* 5.000	363.00	.00	.00	6928.00	1870.00	6933.16	6933.16	6934.43	230.82	9.05	206.68	123.08
* 6.000	668.00	.00	.00	6944.00	1870.00	6948.69	6948.69	6950.17	223.31	9.74	192.07	125.14
7.000	389.00	.00	.00	6952.00	1870.00	6957.48	6957.41	6958.75	217.26	9.06	206.48	126.87
* 8.000	320.00	.00	.00	6961.00	1870.00	6965.33	6965.33	6966.89	211.84	10.01	186.81	128.48
9.000	162.00	.00	.00	6963.00	1830.00	6968.51	.00	6969.82	152.83	9.17	199.56	148.03
* 10.000	411.00	.00	.00	6970.00	1830.00	6976.10	6976.10	6977.79	208.92	10.44	175.29	126.61
11.000	407.00	.00	.00	6978.00	1830.00	6984.06	.00	6985.53	172.84	9.75	187.74	139.20
* 12.000	585.00	.00	.00	7000.00	1160.00	7002.75	7002.75	7003.71	245.20	7.84	148.03	74.08
13.000	443.00	.00	.00	7007.00	1160.00	7010.97	.00	7011.57	133.53	6.26	185.37	100.39
* 14.000	634.00	.00	.00	7022.00	1160.00	7025.09	7025.09	7026.10	243.89	8.04	144.27	74.28
* 15.000	438.00	.00	.00	7034.00	1160.00	7037.13	7037.13	7038.17	234.22	8.18	141.84	75.80
16.000	352.00	.00	.00	7040.00	1160.00	7043.92	.00	7044.77	152.69	7.42	156.26	93.88
* 17.000	382.00	.00	.00	7048.00	1160.00	7051.71	7051.71	7053.01	226.73	9.15	126.83	77.04

1

7/12/ 4 16:39:20

PAGE 10

SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRIWS	EG	10*KS	VCH	AREA	.01K
18.000	416.00	.00	.00	7056.00	1160.00	7060.00	.00	7061.07	166.80	8.31	139.62	89.82

*	19.000	480.00	.00	.00	7068.00	1160.00	7072.46	7072.46	7073.89	219.08	9.60	120.83	78.37
	20.000	363.00	.00	.00	7074.00	1160.00	7078.78	.00	7080.09	136.10	9.34	131.11	99.43

1

7/12/ 4 16:39:20

PAGE 11

FILENAME TRIB4.DAT

SUMMARY PRINTOUT TABLE 150

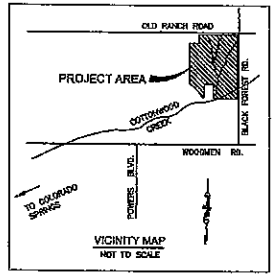
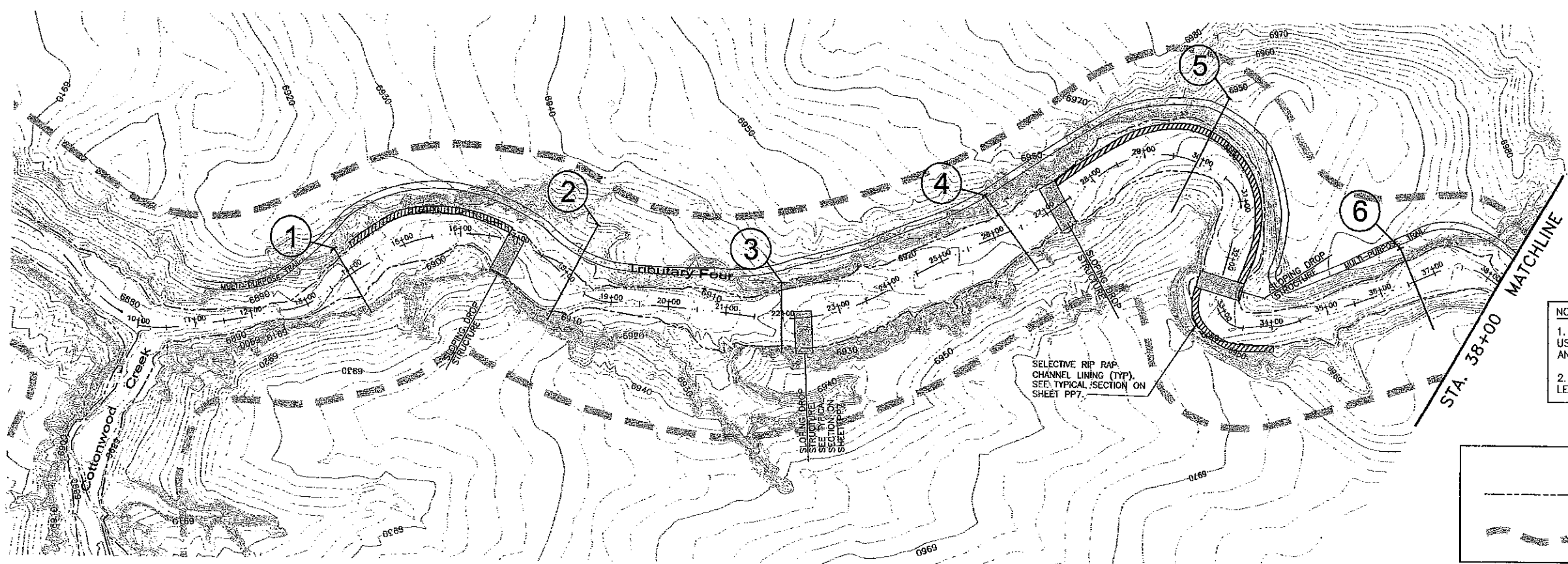
	SECNO	Q	CWSEL	DIFWSP	DIFWSX	DIFKWS	TOPWID	XLCH
	1.000	1870.00	6895.35	.00	.00	17.35	75.20	.00
*	2.000	1870.00	6905.24	.00	9.89	.00	73.82	425.00
	3.000	1870.00	6913.65	.00	8.42	.00	93.63	384.00
*	4.000	1870.00	6924.09	.00	10.44	.00	79.41	433.00
*	5.000	1870.00	6933.16	.00	9.07	.00	83.68	363.00
*	6.000	1870.00	6948.69	.00	15.53	.00	66.82	668.00
	7.000	1870.00	6957.48	.00	8.79	.00	77.88	389.00
*	8.000	1870.00	6965.33	.00	7.85	.00	61.12	320.00
	9.000	1830.00	6968.51	.00	3.18	.00	57.79	162.00
*	10.000	1830.00	6976.10	.00	7.59	.00	52.61	411.00
	11.000	1830.00	6984.06	.00	7.96	.00	52.34	407.00
*	12.000	1160.00	7002.75	.00	18.70	.00	79.02	585.00
	13.000	1160.00	7010.97	.00	8.21	.00	87.76	443.00
*	14.000	1160.00	7025.09	.00	14.13	.00	73.65	634.00
*	15.000	1160.00	7037.13	.00	12.04	.00	68.37	438.00
	16.000	1160.00	7043.92	.00	6.78	.00	62.42	352.00
*	17.000	1160.00	7051.71	.00	7.79	.00	49.84	382.00
	18.000	1160.00	7060.00	.00	8.29	.00	50.01	416.00

*	19.000	1160.00	7072.46	.00	12.46	.00	42.62	480.00
	20.000	1160.00	7078.78	.00	6.32	.00	40.02	363.00

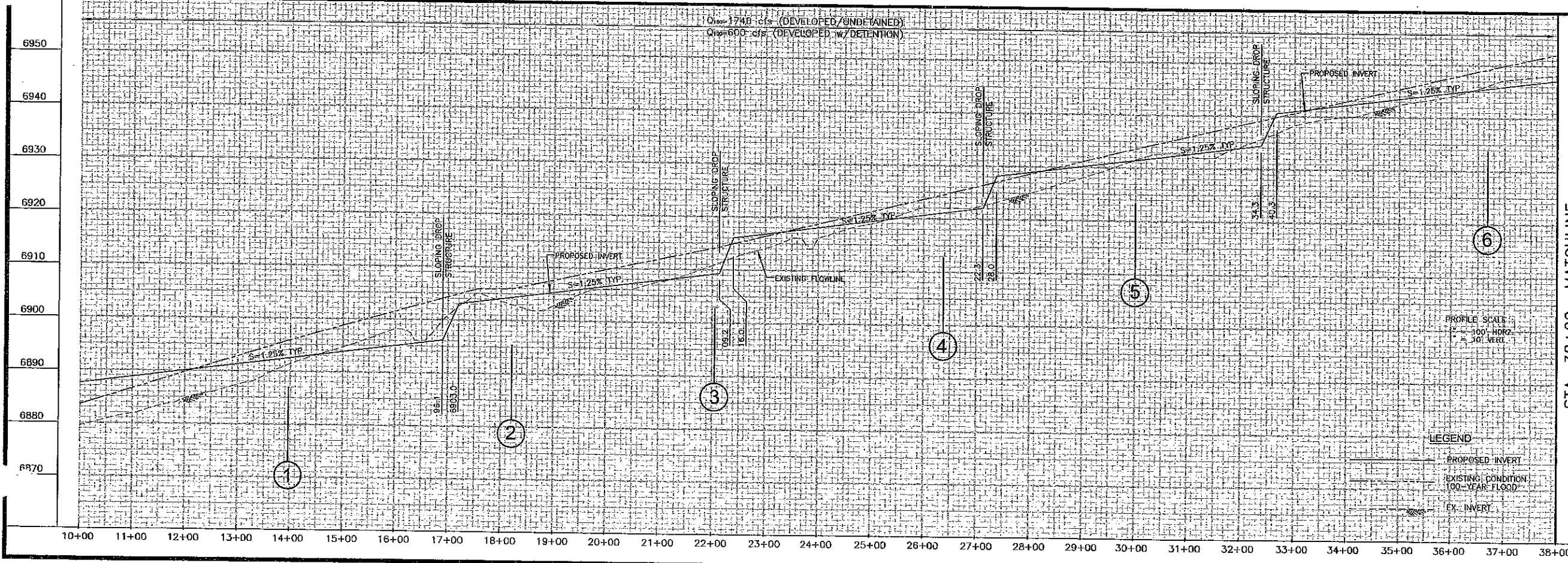
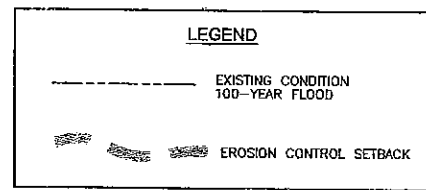
1

7/12/ 4      16:39:20

**APPENDIX C**  
**PLAN AND PROFILES**

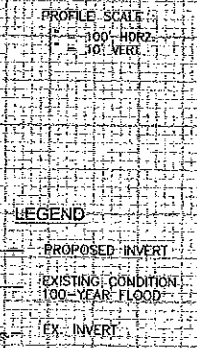


- NOTES :**
- FLOODPLAIN SHOWN DETERMINED USING THE 100-YEAR DEVELOPED AND UNDETAILED.
  - CROSS-SECTIONS ORIENTED LEFT-TO-RIGHT FACING UPSTREAM.



STA. 38+00 MATCHLINE

6950
6940
6930
6920
6910
6900
6890
6880
6870



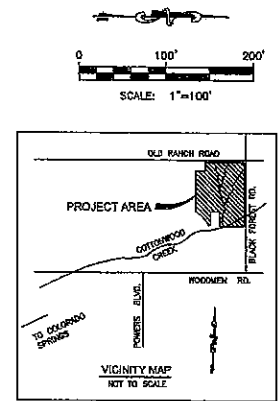
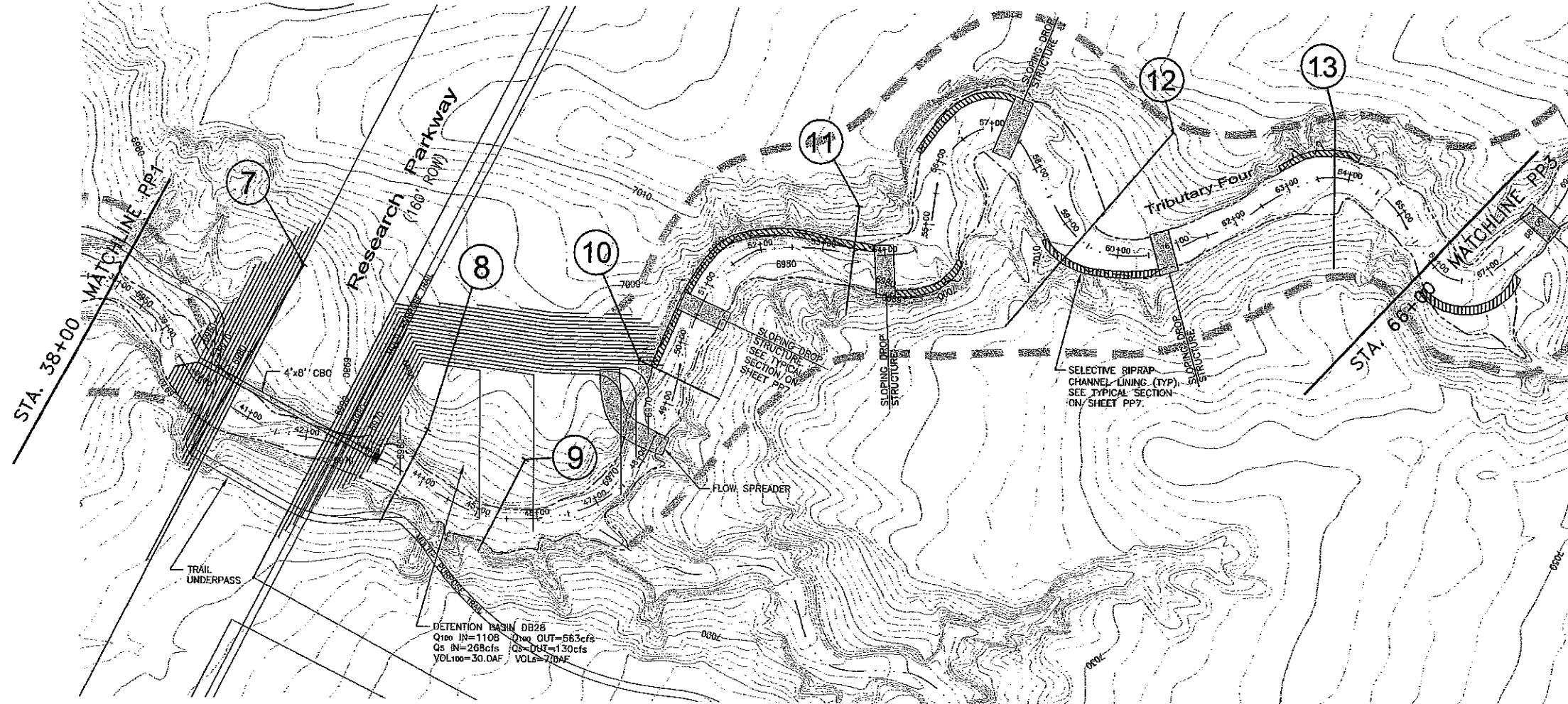
**Kiowa Engineering Corporation**  
 1604 South 21st St.  
 Colorado Springs, Colorado  
 80904 - 4208  
 (719) 630-7342

**WOLF RANCH**  
**MASTER DEVELOPMENT DRAINAGE PLAN**  
**TRIBUTARY FOUR**  
**PLAN & PROFILE**  
 COLORADO SPRINGS, COLORADO

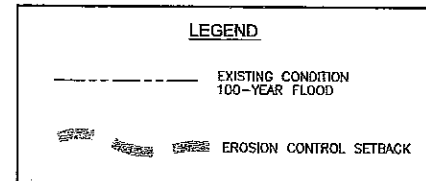
Project No.: 03094  
 Date: 02/13/04  
 Design: RNW  
 Drawn: JLN  
 Check: RNW  
 Revisions:

SHEET  
**PP1**

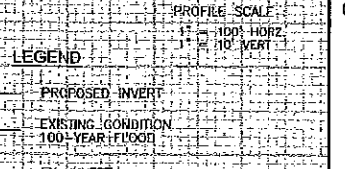
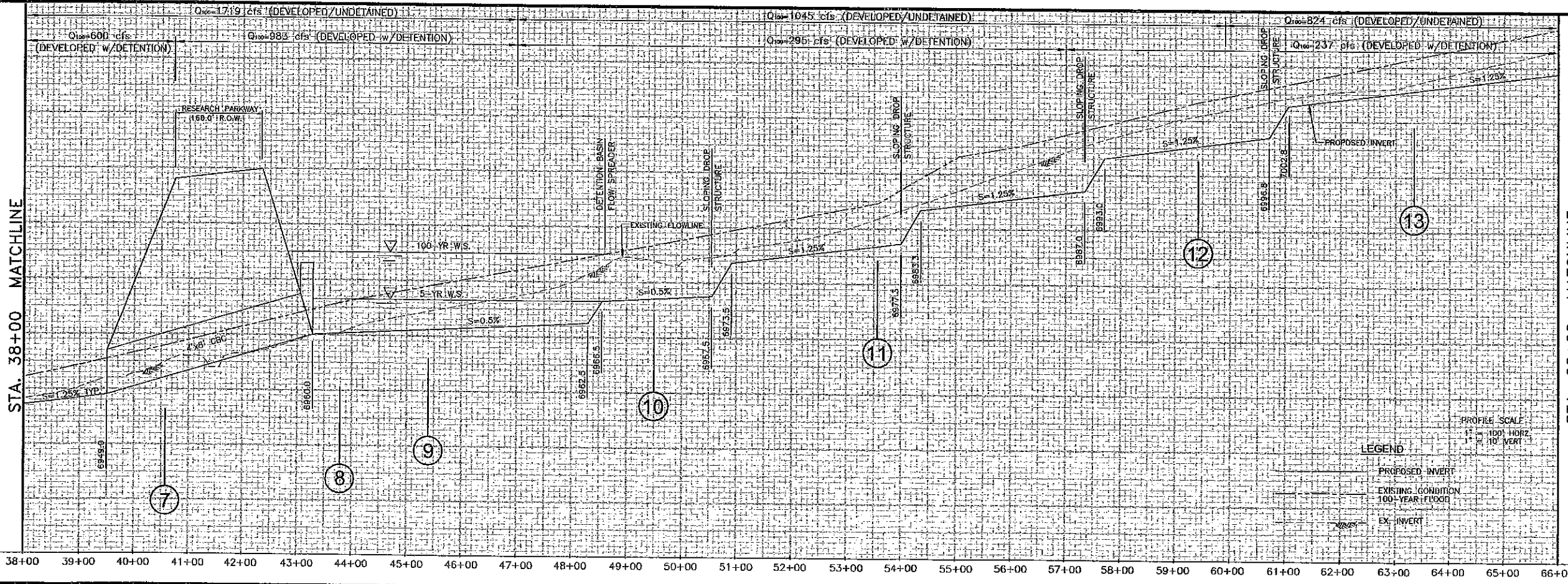




- NOTES:
- FLOODPLAIN SHOWN DETERMINED USING THE 100-YEAR DEVELOPED AND UNDETAINED.
  - CROSS-SECTIONS ORIENTED LEFT-TO-RIGHT FACING UPSTREAM.



DETENTION BASIN DB26  
 Q<sub>100</sub> IN=1108 Q<sub>100</sub> OUT=563cfs  
 Q<sub>5</sub> IN=268cfs Q<sub>5</sub> OUT=130cfs  
 VOL<sub>100</sub>=30.0AF VOL<sub>5</sub>=7.0AF

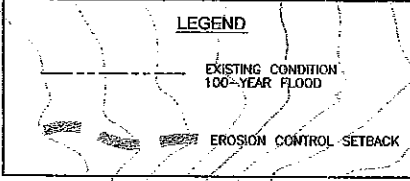
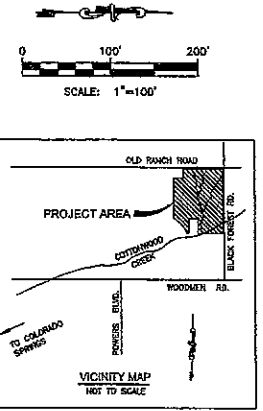
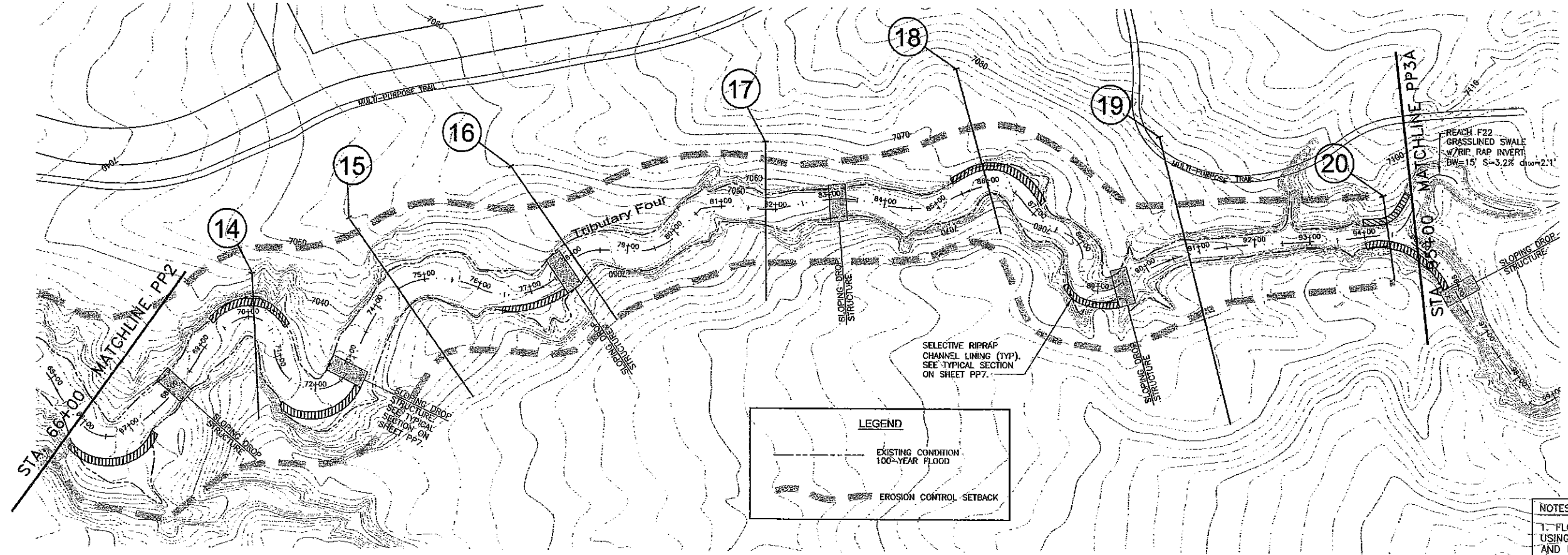


**WOLF RANCH**  
 MASTER DEVELOPMENT DRAINAGE PLAN  
 TRIBUTARY FOUR  
 PLAN & PROFILE  
 COLORADO SPRINGS, COLORADO

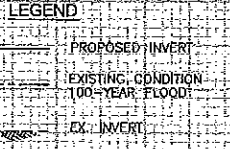
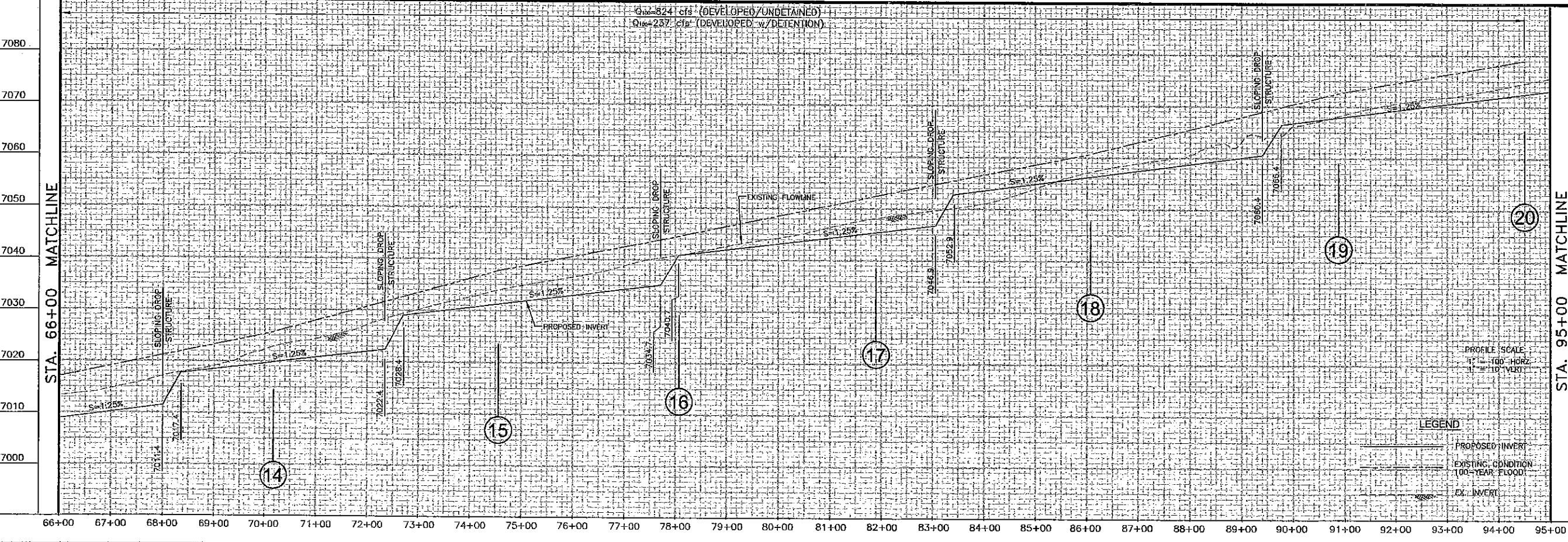
Project No.: 03094  
 Date: 02/13/04  
 Design: RNW  
 Drawn: JLN  
 Check: RNW  
 Revisions:

SHEET  
**PP2**

Kiowa Engineering Corporation  
 1604 South 21st St.  
 Colorado Springs, Colorado  
 80904-4208  
 (719) 690-7342



NOTES:  
 1. FLOODPLAIN SHOWN DETERMINED USING THE 100-YEAR DEVELOPED AND UNDETAINED.  
 2. CROSS-SECTIONS ORIENTED LEFT-TO-RIGHT FACING UPSTREAM.



WOLF RANCH  
 MASTER DEVELOPMENT DRAINAGE PLAN  
 TRIBUTARY FOUR  
 PLAN & PROFILE  
 COLORADO SPRINGS, COLORADO

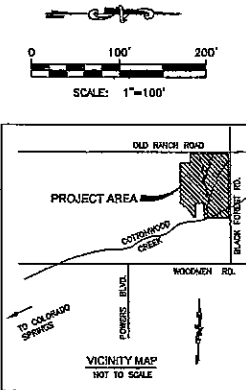
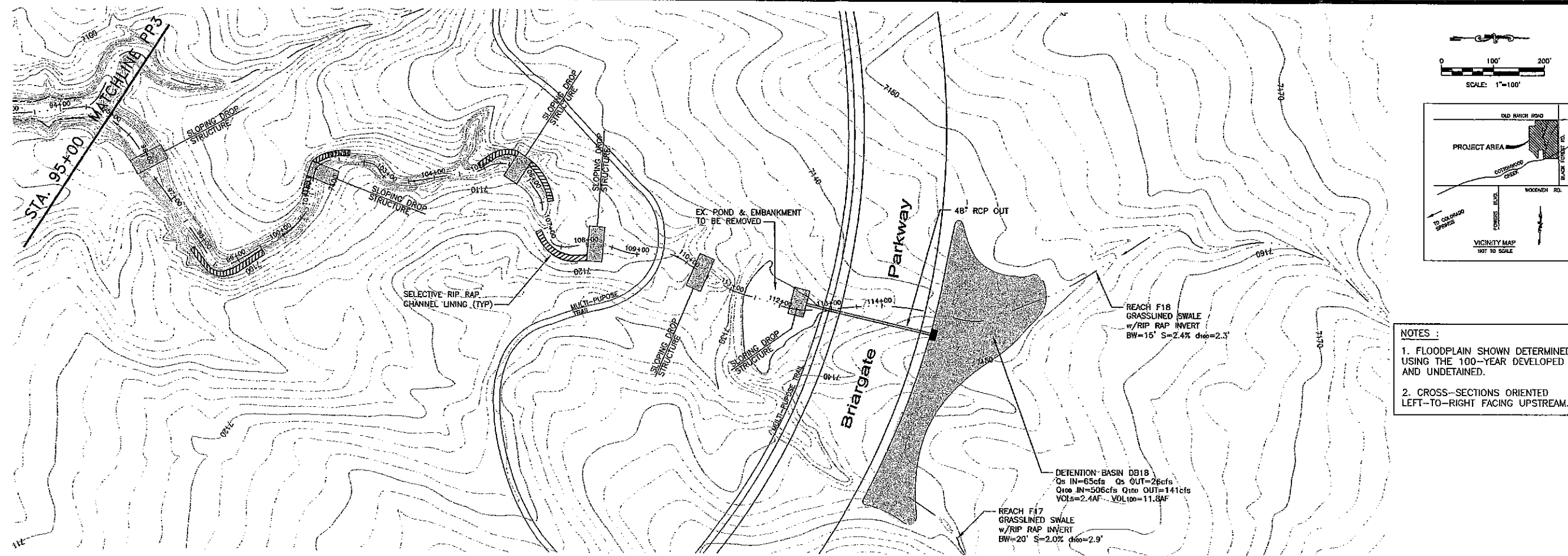
Project No.: 03094  
 Date: 02/13/04  
 Design: RNW  
 Drawn: JLN  
 Check: RNW  
 Revisions:

SHEET  
**PP3**  
 OF X SHEETS

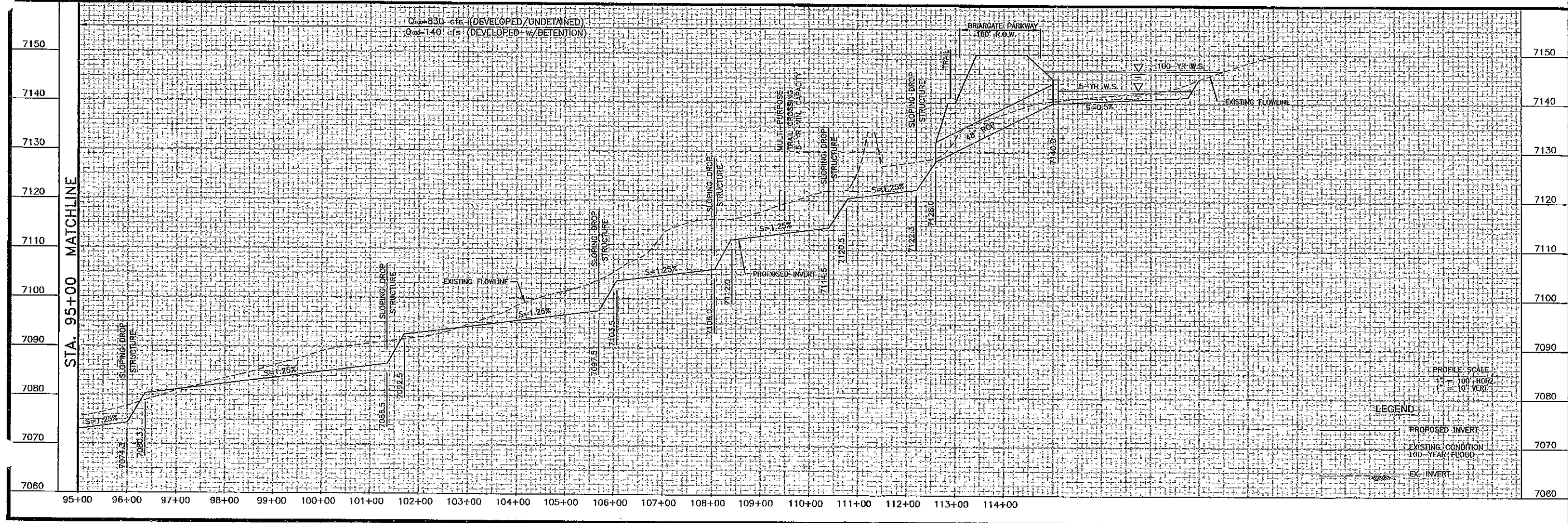
Kiowa Engineering Corporation  
 1604 South 21st St.  
 Colorado Springs, Colorado  
 80904 - 4208  
 (719) 630-7342

03094 pp1-3.dwg (Rev. 01, 2004)





- NOTES:**
- FLOODPLAIN SHOWN DETERMINED USING THE 100-YEAR DEVELOPED AND UNDETAINED.
  - CROSS-SECTIONS ORIENTED LEFT-TO-RIGHT FACING UPSTREAM.

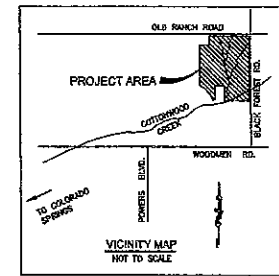
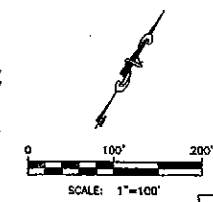
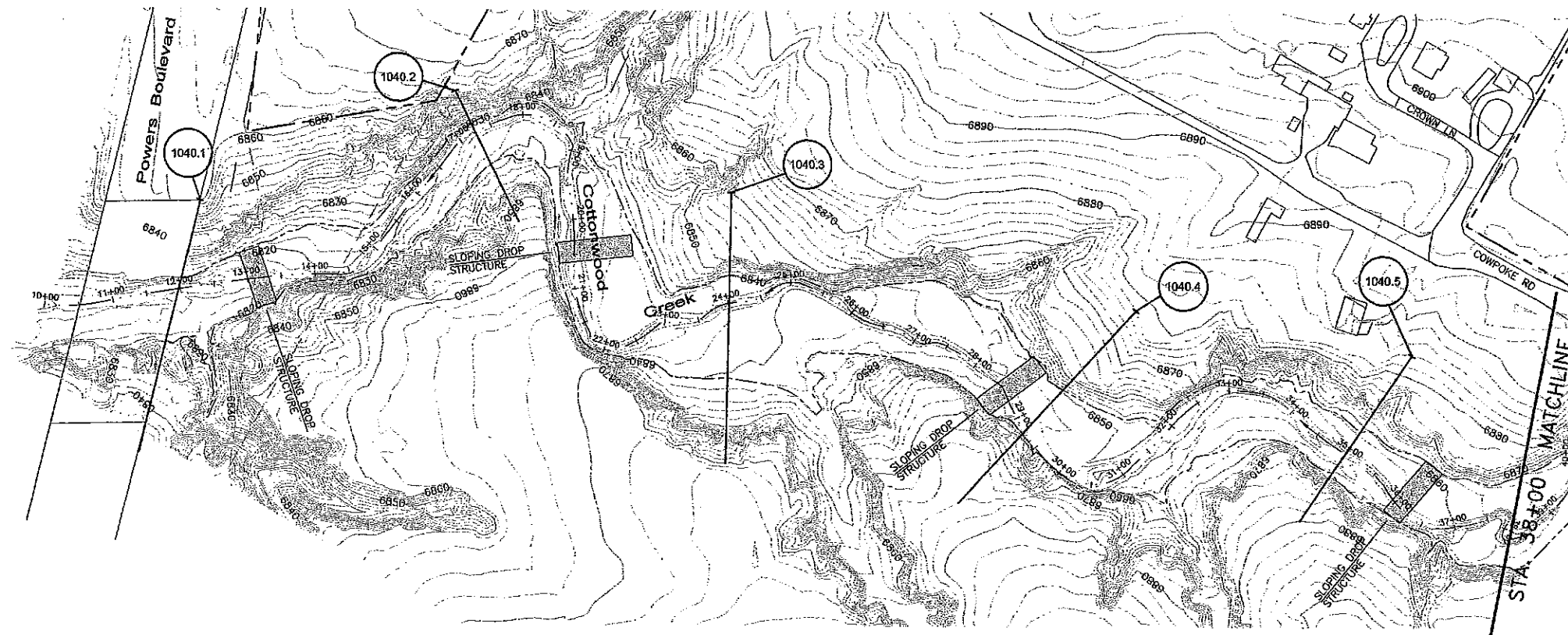


**WOLF RANCH  
MASTER DEVELOPMENT DRAINAGE PLAN  
TRIBUTARY FOUR  
PLAN & PROFILE  
COLORADO SPRINGS, COLORADO**

Project No.: 03094  
Date: 02/13/04  
Design: RNW  
Drawn: JLN  
Check: RNW  
Revisions:

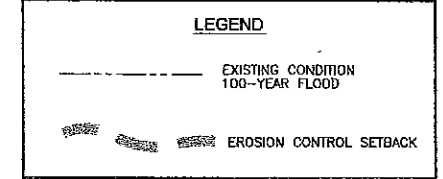
SHEET  
**PP3A**  
OF X SHEETS

**Kiowa Engineering Corporation**  
1604 South 21st St.  
Colorado Springs, Colorado  
80904 - 4208  
(719) 630-7342



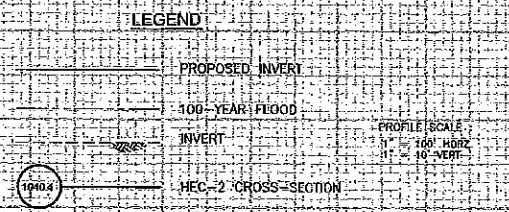
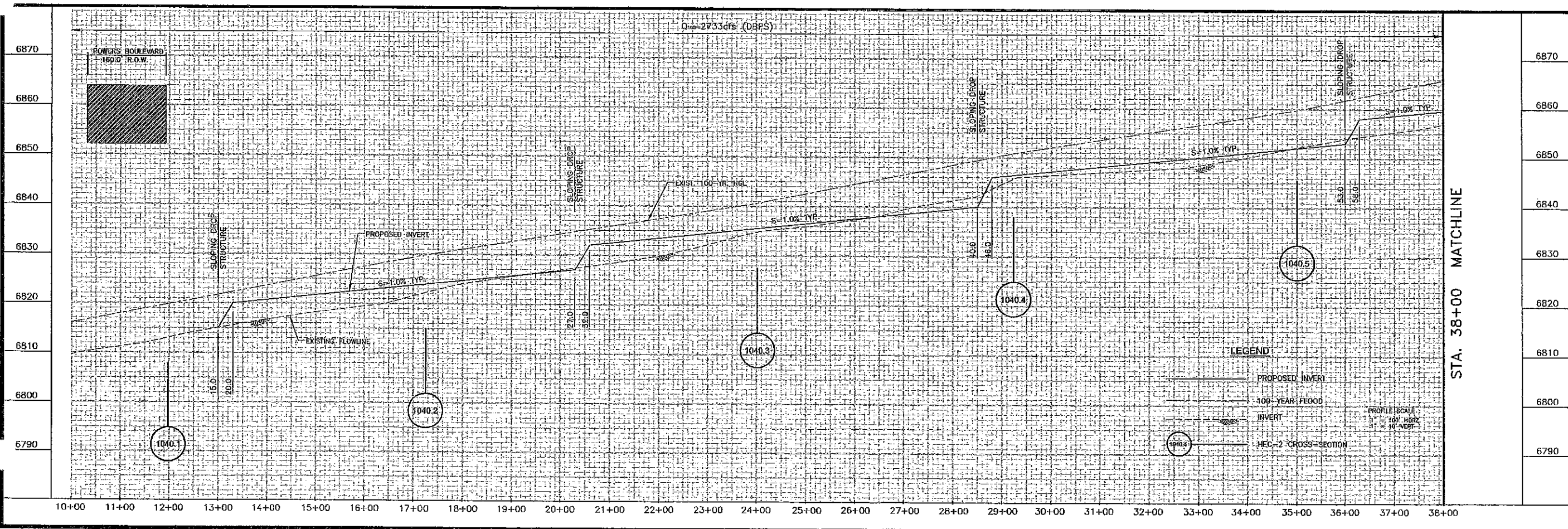
NOTES:

1. FLOODPLAIN SHOWN DETERMINED USING THE 100-YEAR DEVELOPED AND UNDETAINED.
2. CROSS-SECTIONS ORIENTED LEFT-TO-RIGHT FACING UPSTREAM.



**Kiowa Engineering Corporation**  
 1604 South 21st St.  
 Colorado Springs, Colorado  
 80904 - 4208  
 (719) 830-7342

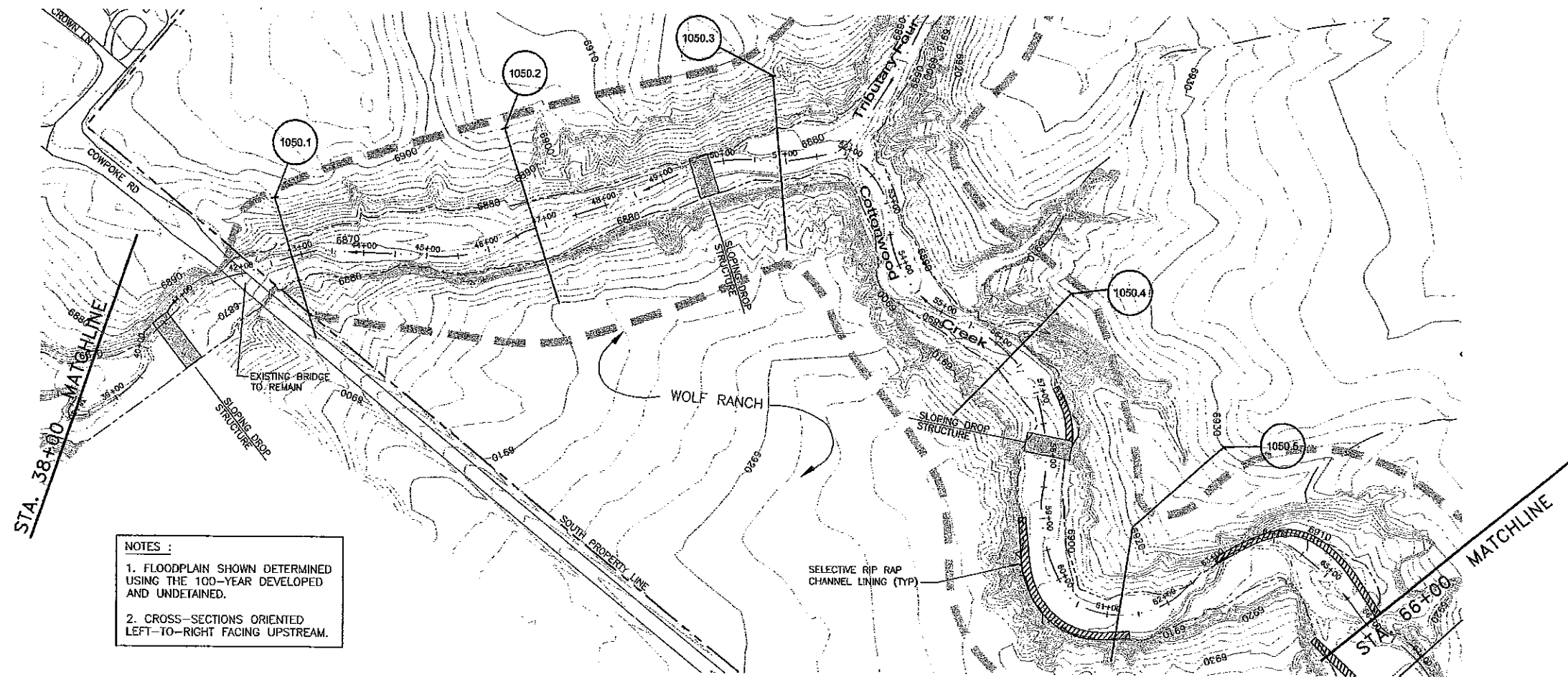
**WOLF RANCH**  
 MASTER DEVELOPMENT DRAINAGE PLAN  
 COTTONWOOD CREEK  
 PLAN & PROFILE  
 COLORADO SPRINGS, COLORADO



Project No.: 03094  
 Date: 02/09/04  
 Design: RNW  
 Drawn: JLN  
 Check: RNW  
 Revisions:

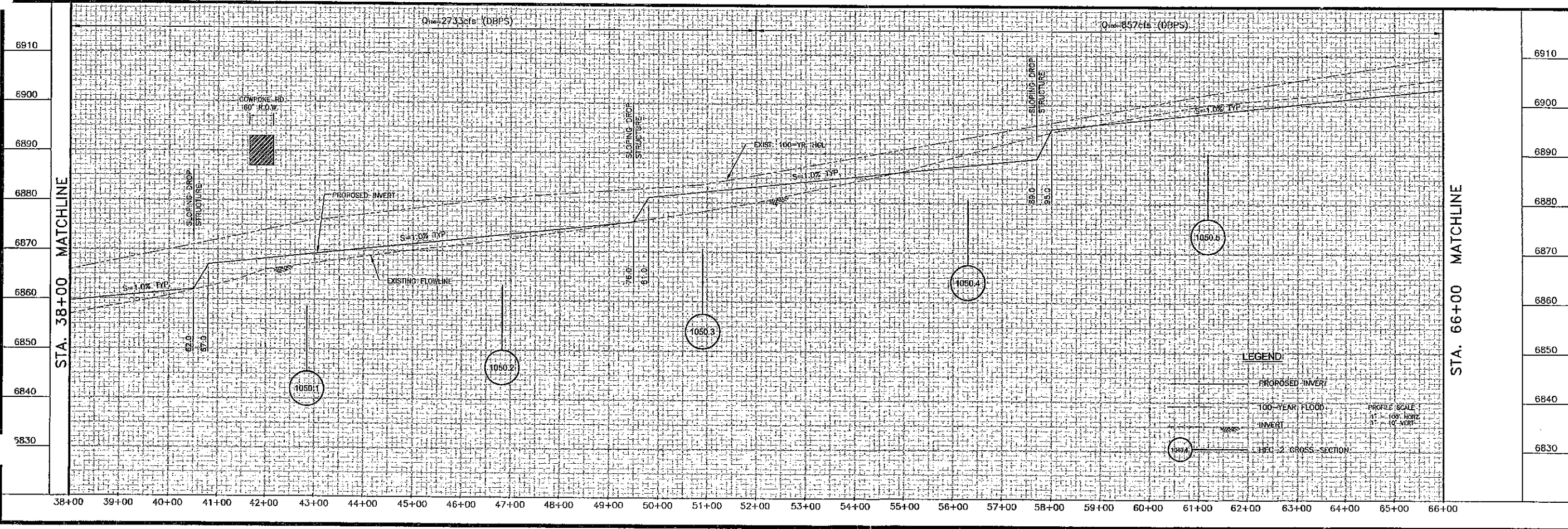
SHEET  
**PP4**  
 OF X SHEETS





**NOTES:**

1. FLOODPLAIN SHOWN DETERMINED USING THE 100-YEAR DEVELOPED AND UNDETAILED.
2. CROSS-SECTIONS ORIENTED LEFT-TO-RIGHT FACING UPSTREAM.

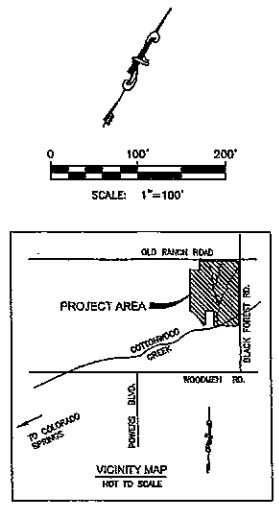
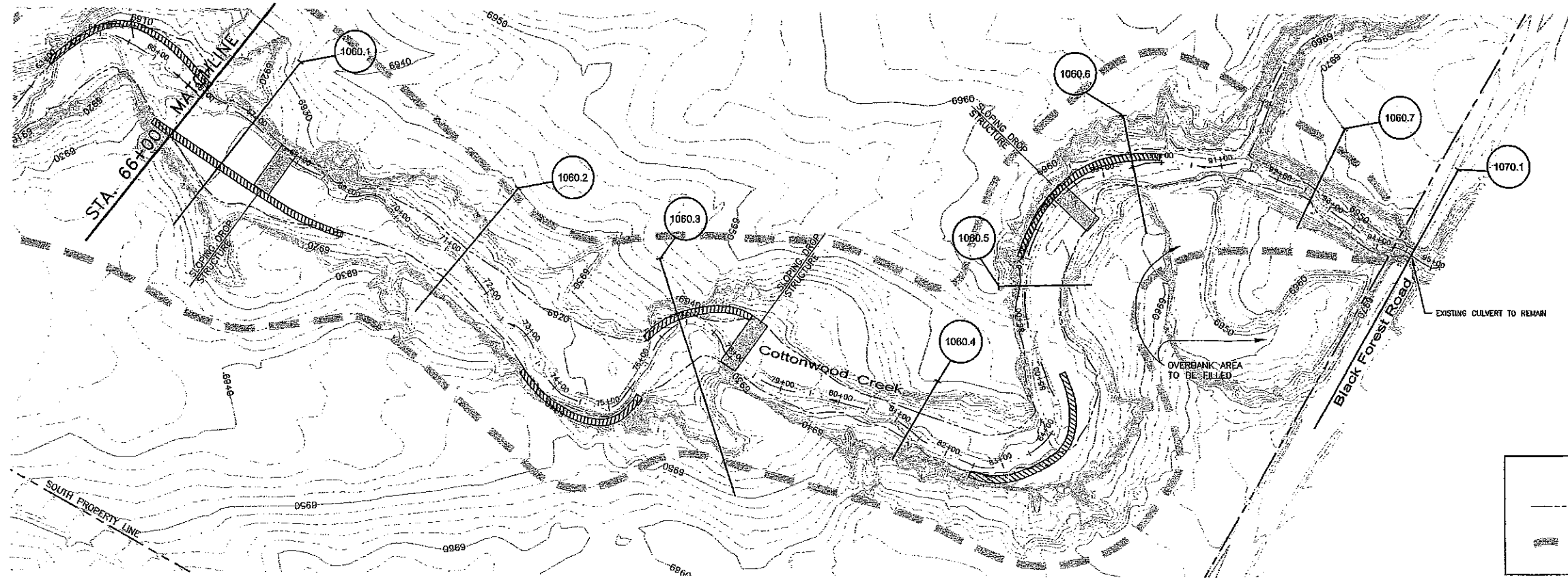


**WOLF RANCH**  
**MASTER DEVELOPMENT DRAINAGE PLAN**  
**COTTONWOOD CREEK**  
**PLAN & PROFILE**  
**COLORADO SPRINGS, COLORADO**

**Kiowa Engineering Corporation**  
 1604 South 21st St.  
 Colorado Springs, Colorado  
 80904 - 4208  
 (719) 690-7342

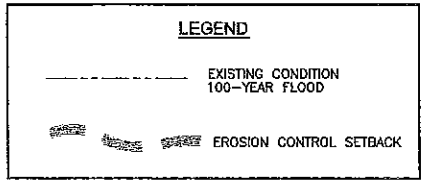
Project No.:	03094
Date:	01/29/04
Design:	RNW
Drawn:	JLN
Check:	RNW
Revisions:	

SHEET  
**PP5**  
 OF 8 SHEETS



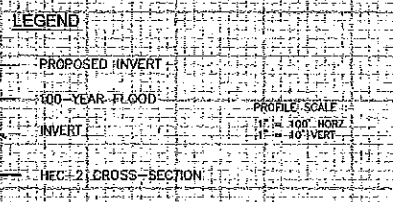
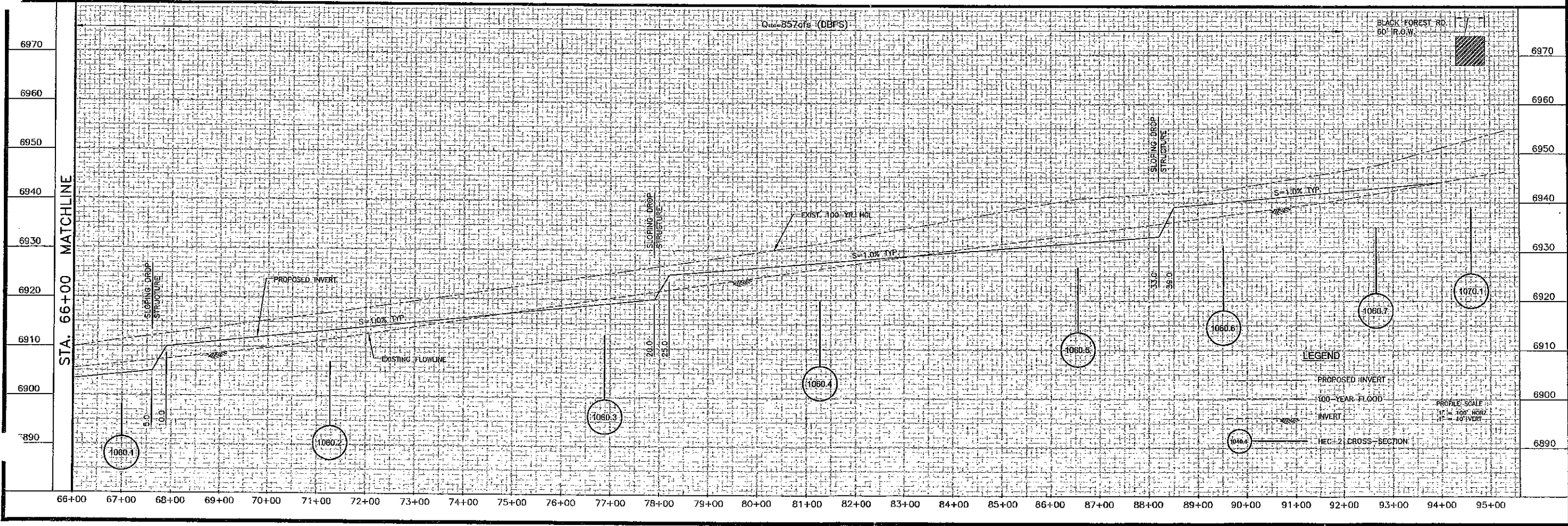
**NOTES :**

1. FLOODPLAIN SHOWN DETERMINED USING THE 100-YEAR DEVELOPED AND UNDETAINED.
2. CROSS-SECTIONS ORIENTED LEFT-TO-RIGHT FACING UPSTREAM.



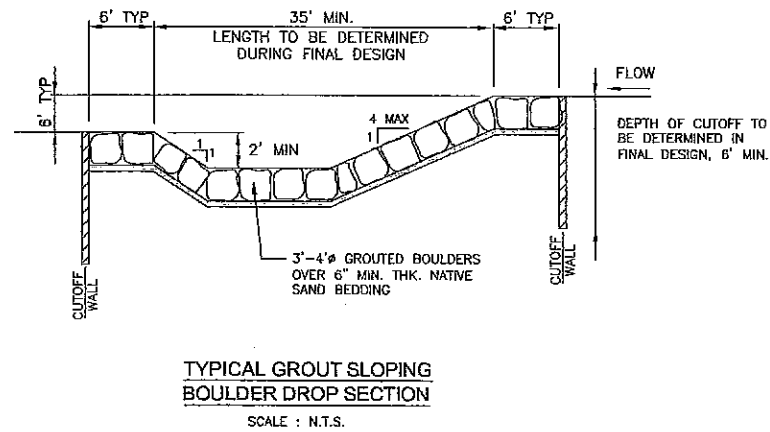
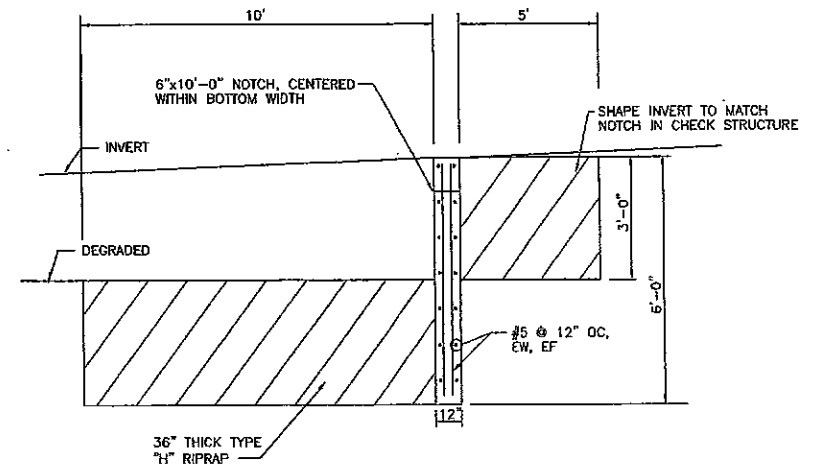
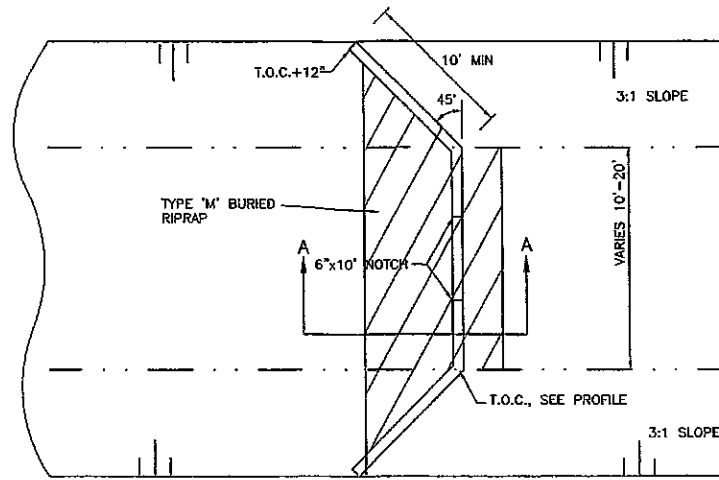
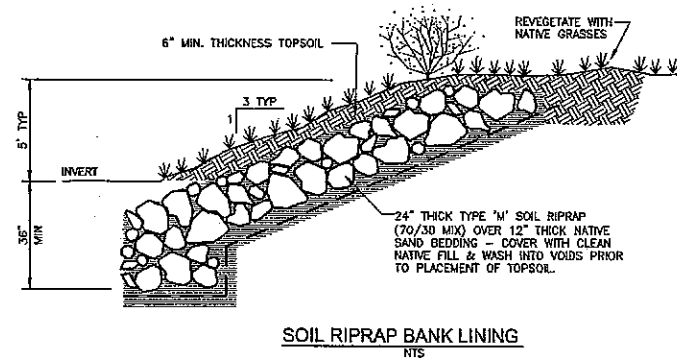
**Kiowa Engineering Corporation**  
 1804 South 21st St.  
 Colorado Springs, Colorado  
 80904 - 4208  
 [719] 630-7342

**WOLF RANCH**  
**MASTER DEVELOPMENT DRAINAGE PLAN**  
**COTTONWOOD CREEK**  
**PLAN & PROFILE**  
 COLORADO SPRINGS, COLORADO



Project No.:	03094
Date:	01/29/04
Design:	RNW
Drawn:	JLN
Check:	RNW
Revisions:	

SHEET  
**PP6**  
 OF X SHEETS



Kiowa Engineering Corporation  
1604 South 27th St.  
Colorado Springs, Colorado  
80904-4208  
(719) 690-7342

WOLF RANCH  
MASTER DEVELOPMENT DRAINAGE PLAN  
TYPICAL DRAINAGEWAY DETAILS  
COLORADO SPRINGS, COLORADO

Project No.:	03094
Date:	11/19/04
Design:	RNW
Drawn:	JLN
Check:	RNW
Revisions:	