

There are some key issues that
~~are going to~~ have to be solved
before this can proceed. — mainly
issues with closed basin & the
metropolitan district. We will probably
need an Intergovernmental Agreement
in regards to the district

Master Development Drainage Plan
Wolf Ranch Development

City of Colorado Springs, Colorado

RAM
2/11/05

Prepared For:

Norwood Development Group
4065 Sinton Road Suite 200
Colorado Springs, CO 80907

Prepared By:

Kiowa Engineering Corporation
1604 South 21st Street
Colorado Springs, Colorado 80904

Project Number 03094
July 2004
November 2004

WOLF RANCH MASTER DEVELOPMENT DRAINAGE UPDATE

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*in regards to
the bridge*

**WOODMEN HEIGHTS NO 1
ANNEXATION AGREEMENT**

THIS ANNEXATION AGREEMENT (this "Agreement"), dated this 23rd day of July, 2004, is between the City of Colorado Springs, a home rule city and Colorado municipal corporation (the "City"), and The Robert W. Kinzie Revocable Living Trust and The Evelyn M. Kinzler Revocable Living Trust (collectively referred to as "Owners" or the "Property Owners").

**I.
INTRODUCTION**

The Owners own all of the real property located in El Paso County, Colorado, identified and described in the legal description attached hereto as **Exhibit A** (the "Property").

The growth of the Colorado Springs metropolitan area makes it likely that the Property will experience development in the future and the Property is identified in the City Annexation Plan as recommended for annexation. Subject to the terms and conditions set forth herein, both the City and the Owners wish to annex the Property into the City to ensure its orderly development. In consideration of the mutual covenants contained in this Agreement, the receipt and sufficiency of which are acknowledged by each of the parties, the City and the Owners agree as follows.

**II
ANNEXATION**

The Owners have petitioned the City for annexation of the Property as set forth in **Exhibit A**. The annexation will become effective upon final approval by the City Council and the recording of the annexation plat and annexation ordinance with the El Paso County Clerk and Recorder.

All references to the Property or to the Owners' Property are to the Property described in **Exhibit A** except as otherwise indicated.

**III.
LAND USE**

A Master Plan for the Property, Woodmen Heights Master Plan, has been proposed and submitted to the City for approval. Owners will comply with the approved Master Plan or an amended Master Plan approved in accord with applicable provisions of the Code of the City of Colorado Springs 2001, as amended or recodified ("City Code").

**IV.
ZONING**

A. Zoning. The City Planning and Community Development Department of the City agrees to recommend that the initial zone for the Owners' Property shall be Agricultural (A) upon annexation. While zoned A, a development plan shall be required for any use requiring a building permit except for agricultural uses. Owners acknowledge and understand that the City Council determines what is an appropriate zone for the Property, and this recommendation does not bind the Planning Commission or City Council to adopt an Agricultural zone for the Property.

B. Rezoning. Rezoning shall conform to the Master Plan, as approved or as amended by the City in the future. Rezoning in accord with the land uses reflected on the Master Plan will occur prior to actual development of the site.

**V.
PUBLIC FACILITIES**

A. Street / Traffic. The Owners agree to construct, at the Owners' expense (unless provided by the Woodmen Road Metropolitan District as defined below (V 1.b.)) those street and/or traffic

Vollmer Road may be reduced to match the ultimate design of Vollmer Road as determined by El Paso County

4. Black Forest Road. The Owners will be responsible for dedicating one-half (1/2) of the necessary right-of-way for, and constructing Black Forest Road so that Black Forest Road has four (4) lanes and meets City standards for a principal arterial road with a total right-of-way of one hundred twenty feet (120') from its intersection with Woodmen Road north to the northern boundary of the Property. Owners or the District (as defined in Section XII of this Agreement) will be entitled to cost recovery for the costs to construct and improve the west one-half (1/2) of Black Forest Road from owners having frontage on said road in accord with Section 7.7.705.B. of the City Code (Subdivision Regulations).

5. Black Forest Road Cottonwood Creek Crossing. Owners acknowledge that there is a need to construct the Black Forest Road bridge or box culvert, as applicable, across Cottonwood Creek. The Owners, either directly or through the Districts, shall construct the bridge or box culvert over Cottonwood Creek prior to the expiration of the second phase of the development but in any case prior to December 31, 2011. The City commits to acquire the necessary right-of-way and easements necessary for the construction of the bridge through the development process and/or through its powers of eminent domain. The owners will be eligible for reimbursement as applicable, per Section 7.7.1001-1006 (Arterial Roadway Bridges) of the City Code. City participation or reimbursement for the costs of construction of the bridge or box culvert for the Black Forest Road Cottonwood Creek crossing will not be allowed.

6. Construction of Internal Public Street Network to Serve Property. It is recognized that there may be a need for certain Owners to construct portions of the internal public street network, as illustrated on the approved Woodmen Heights Master Plan, that are not adjacent to their property. In order to accommodate this situation, Owners shall dedicate the full right-of-way for any internal public streets, as illustrated on the approved Master Plan, and a temporary construction easement as reasonably required to complete construction of those internal roads, at any time requested by the City or by an Owner that intends to commence development. Additionally, Owners who incur costs associated with the design and construction of internal public streets within the Property shall be eligible for Cost Recovery from Owners having frontage on said street in accord with Section 7.7.705.B. of the City Code (Subdivision Regulations).

B. Marksheffel Road Sand Creek Crossing. The Owners shall construct the Marksheffel Road bridge or box culvert, as applicable, across Sand Creek at their expense. The owners will be eligible for fifty percent (50%) reimbursement for the construction cost of the bridge or box culvert, as applicable, per section 7.7.1001-1006 (Arterial Roadway Bridges) of the City Code.

C. Traffic Control Devices and Street Lights. As required herein, the Owners shall pay for installation of traffic and street signs, striping, and traffic control devices, permanent barriers, and street lights, together with all associated conduit for all streets within or contiguous to the Property as mutually determined necessary by the parties, and in accord with uniformly applied criteria set forth by the City. The City agrees that the traffic signal at the intersection of Woodmen Road and Marksheffel Road may be installed by the Woodmen Road Metro District rather than by Owners, but Owners will remain responsible for that traffic signal if the District does not fund it. Streetlights will be required on collector and larger streets or at intersections for public safety as reasonably determined necessary by the City and Utilities. Traffic signals will be installed only after the intersection warrants such signals, as outlined in the Manual on Uniform Traffic Control Devices in use at the time or another nationally accepted standard. Once the intersection meets the outlined criteria, the City will notify the Owners in writing and the Owners will install the traffic signal within one hundred eighty (180) days after receipt of that notice. The Owners will be responsible for all components of the traffic signal, except the City will supply the controller equipment and cabinet (the reasonable costs therefor to be reimbursed by the Owners). If not provided by the District, the Owners will be responsible for purchasing and installing Intelligent Transportation Systems (ITS) for transit and smart bus stops in the development and along adjacent arterials to the development. This includes Woodmen Road. The level of ITS infrastructure will be determined as the level of transit service develops in the area; however, after the initial installation of the ITS, the Owners shall have no obligation for operating, maintaining, repairing or upgrading such systems. The City shall be solely responsible for further operating, maintenance, repair and upgrading of the ITS.

Kiowa Engineering Corporation

December 1, 2004

Mr. Tim Mitros
Subdivision Engineering
City of Colorado Springs
30 South Nevada, Suite 700
Colorado Springs, Colorado 80903

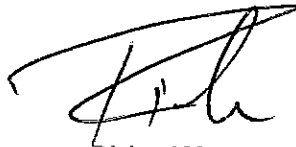
RE: Wolf Ranch Master Development Drainage Plan, Colorado Springs, Colorado (Kiowa Project No. 03094)

Dear Tim:

Accompanying this letter is a revised copy of the MDDP for the above referenced project. I have also returned your review copy for your files as requested. As a result of this submittal, I would request on behalf of the developer that a drainage board item be scheduled to present and discuss the closing of the basin and the exemption of this site from drainage fee assessment. Please let me know at your earliest convenience when the drainage board item can be scheduled.

If Kiowa can be of any further assistance, please do not hesitate to contact us.

Sincerely,
KIOWA ENGINEERING CORPORATION



Richard N. Wray, P.E.
Principal

Cc: Ralph Braden, Norwood Development
RNW/rnw
1201rnw1

ENGINEER'S STATEMENT:

The attached master development drainage plan and report were prepared under my direction and supervision and are correct to the best of my knowledge and belief. Said drainage report has been prepared according to the criteria established by the City/County for drainage reports and said report is in conformity with the master plan of the drainage basin. I accept responsibility for any liability caused by any negligent acts, errors or omissions on my part in preparing this report.

Kiowa Engineering Corporation, 1604 South 21st Street, Colorado Springs, Colorado 80904

Richard N. Wray
Registered Engineer # 19310

Date

DEVELOPER'S STATEMENT:

I, the Developer, have read and will comply with all of the requirements specified in this drainage report and plan.

BY: _____
Date

ADDRESS: Norwood Development Group
4065 Sinton Road Suite 200
Colorado Springs, CO 80907

CITY OF COLORADO SPRINGS

Filed in accordance with Section ~~15.3-906~~ ^{7.7.906} of the Code of the City of Colorado Springs, ~~1980~~, as amended.
2001

City Engineer

Dated

PROJECT DESCRIPTION

Wolf Ranch Development is a master planned community located in northeast Colorado Springs. The master development plan includes open space, parks, drainage, residential, office and commercial uses. The development covers approximately 1800 acres. The development is located bordered by Black Forest Road on the east, Old Ranch Road on the north, the Cordera development on the west and Cowpoke Road on the south. The location of the site is presented on Figure 1.

The property subject to development is located in portions of Sections 30 and 31 Township 12 South, Range 65 West of the 6th Principal Meridian and Section 6 Township 13 South Range 65 West of the 6th Principal Meridian. The development subject to master drainage planning has a segment of Cottonwood Creek that passes through the southern portion of the site as well as a major sub-tributary designated as Tributary Four in this report. The property lies completely within the Cottonwood Creek basin.

PREVIOUS REPORTS

The following reports and plans were reviewed in the process of preparing this master development drainage plan:

1. Soil Survey for El Paso County, Colorado, dated June 1981.
2. "City of Colorado Springs/El Paso County Drainage Criteria Manual", prepared by City of Colorado Springs, El Paso County, dated May 1987, revised 1996.
3. Cottonwood Creek Drainage Basin Planning Study (DBPS) prepared by URS, Inc., dated 1994.
4. Cottonwood Creek Drainage Basin Planning Study prepared by Ayres Associates, Inc. dated June 2000.
5. Westcreek at Wolf Ranch Subdivision Master Development Drainage Plan and Final Drainage Report for Westcreek at Wolf Ranch Filings Nos. 1, 2, 3, 4 and 5, prepared by Rockwell Consulting, dated September 2003.
6. Westcreek at Wolf Ranch Subdivision Master Development Drainage Plan and Final Drainage Report for Westcreek at Wolf Ranch Filings Nos. 6, 7, 8, 9, 10, 11 and 12 and Research Parkway at Wolf Ranch Filings 1, 2, and 3, prepared by Rockwell Consulting, dated December 2003.
7. HEC-1 Flood Hydrograph Package User's Manual, prepared by US Army Corps of Engineers Hydrologic Engineering Center, dated June 1998.
8. Prudent Line for Rural Areas in El Paso County Criteria prepared by Ayres Associates dated June 2000.

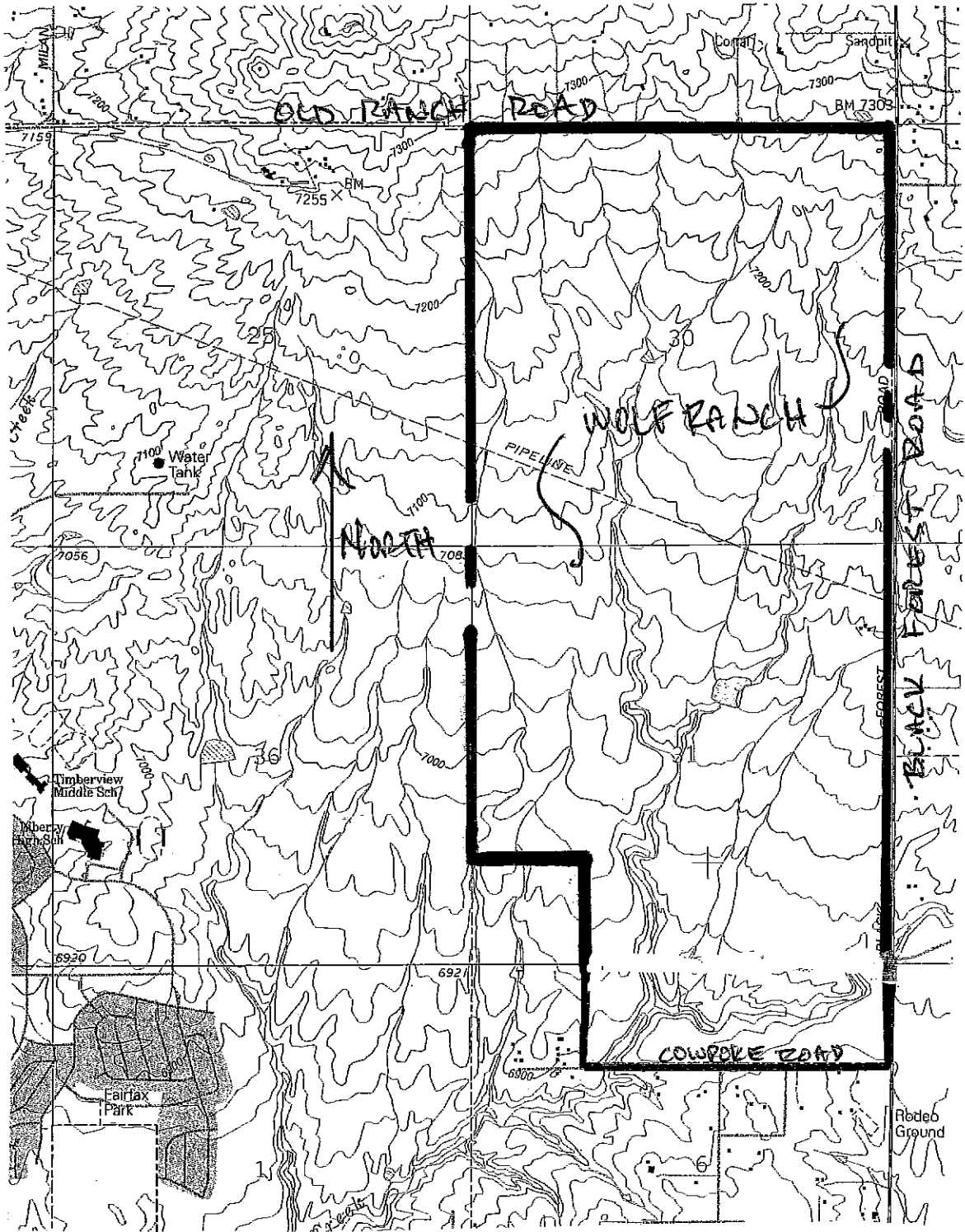


FIGURE 1
VICINITY MAP

References 3 and 4 were prepared for the overall Cottonwood Creek Drainage basin and were used to establish the selected drainageway improvements for the basin. The City adopted the studies and used them in the establishment of the drainage and bridge fees for the basin. The primary difference between these two studies was that in Reference 4 the prudent line concept was incorporated into the DBPS as the preferred alternative channel design for the upper portions of Cottonwood Creek and for Tributary Four as well. The drainage fee was modified in Reference 4 to account for the land costs associated with the creation of a prudent line setback. No channel improvements other than grade control structures were recommended for Cottonwood Creek and Tributary Four for the reaches within the Wolf Ranch development. The peak discharges summarized in Reference 4 were applied in the design of bank improvements and grade controls for the portion of Cottonwood Creek that passes through the southern portion of the development.

References 5 and 6 were used to establish the proposed major drainage structures within the Filings covered by these master development drainage plans and final drainage reports. Storm sewer outfall sewers and detention basins shown recommended in these studies were considered when the hydrologic models were developed for this MDDP.

The purpose of this MDDP is to develop the hydrologic model of the onsite and offsite watersheds related to the Master Planned area. It is also the focus of this MDDP to evaluate the storm sewer infrastructure to be constructed as part of the Westcreek and greater Wolf Ranch developments, and to establish the size, type, and location of the major drainageway facilities for Wolf Ranch. It should however be expected that modifications in the size and location of the major drainageway facilities as shown herein might occur depending upon the actual development of the land within the Wolf Ranch property. In particular the location of the regional detention basins may be shifted as alternatives are analyzed as part of the land development process.

HYDROLOGY

The offsite and onsite hydrology for the site was estimated using the methods outlined in the City/County Storm Drainage Criteria Manual. Topography for the site was compiled at a two-foot contour interval and a horizontal scale of one inch to 400-feet. This topography was used to verify the onsite sub-basin boundaries. Offsite sub-basin boundaries were determined using the above referenced reports, the City of Colorado Springs FIMS mapping base, and the USGS quadrangle maps for the area. Field inspections were also carried out in order to confirm or refine subdivision limits.

Existing and developed condition peak discharges for the sub-basins and design points along the major drainageway associated with Tributary Four and Cottonwood Creek shown on the Hydrologic Sub-basin Map were determined for the 5-year and 100-year recurrence intervals. The 24-hour storm duration was modeled using a Type IIA rainfall distribution. The total 24-hour rainfall depth was 2.5 and 4.4 inches for the 5- and 100-year frequencies, respectively. No area reduction factor was applied to the rainfall distribution and total depths.

Soils within the Wolf Ranch are mostly classified into hydrologic soils group B as shown in Reference 1. A small amount of hydrologic soil group A exists along the west-bank of Tributary Four in the southern portion of the development. For the purposes of modeling the developed conditions, all soils within the development were assumed to be hydrologic soil group B. Presented on Figure 2 are the hydrologic soil types that can be found within the Wolf Ranch development.

Land uses within the development were determined using the master development plan for Wolf Ranch. The development land will be of mixed uses. The land uses were used in the establishment of the curve numbers (CN values) that were input to the HEC-1 model. For the existing development condition and CN value of 61 was used for all of existing sub-basins within the development. Presented on Figure 3 is the hydrologic land use map for Wolf Ranch and their associated CN-values.

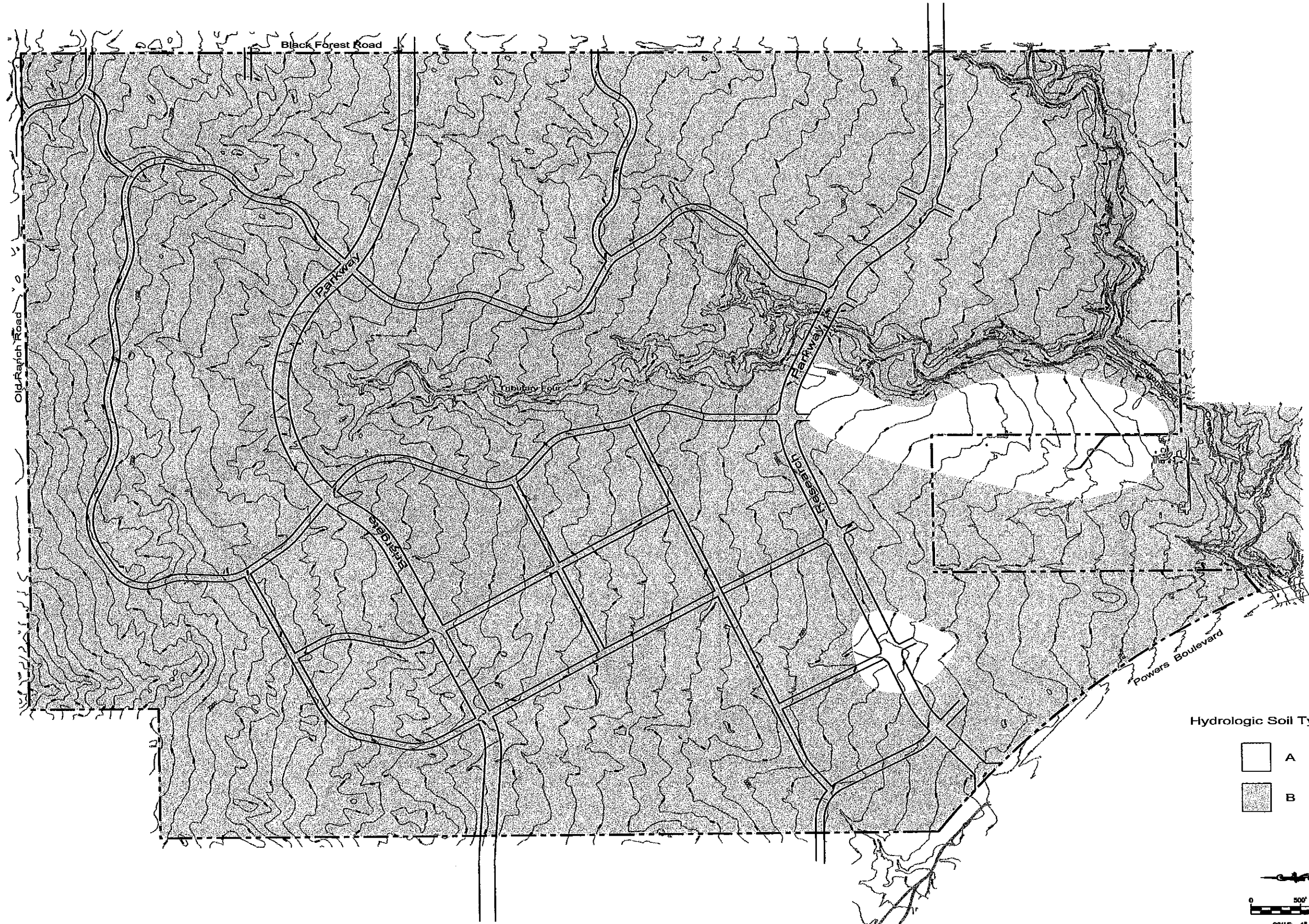
The time of concentration for each of the sub-basins modeled was estimated. The time of concentration was computed from a combination of overland flow, channel and pipe flow for each sub-basin. The time lag for each sub-basin was computed by reducing the time of concentration by 60 percent. The time lag was input to the HEC-1 model.

The Muskingum-Cunge routing technique was used to route the sub-basin hydrographs between design points. The majority of the routing elements were trapezoidal channel sections. Within the Westcreek portion of the development storm sewers were modeled. The longitudinal slope of each routing element was determined using the topographic mapping described above.

Hydrologic flow charts were prepared and are contained within Appendix A of this report. These flow charts were used to compile the HEC-1 model.

EXISTING MAJOR SUB-WATERSHED DESCRIPTIONS

The study area was divided into eight major sub-watersheds. These sub-watersheds are noted in the hydrologic analysis by using the designations A through H. The sub-basins were coded accordingly (i.e., A-1, A-2, B-1, etc). The sub-basins for the existing condition are presented on Figure 4.



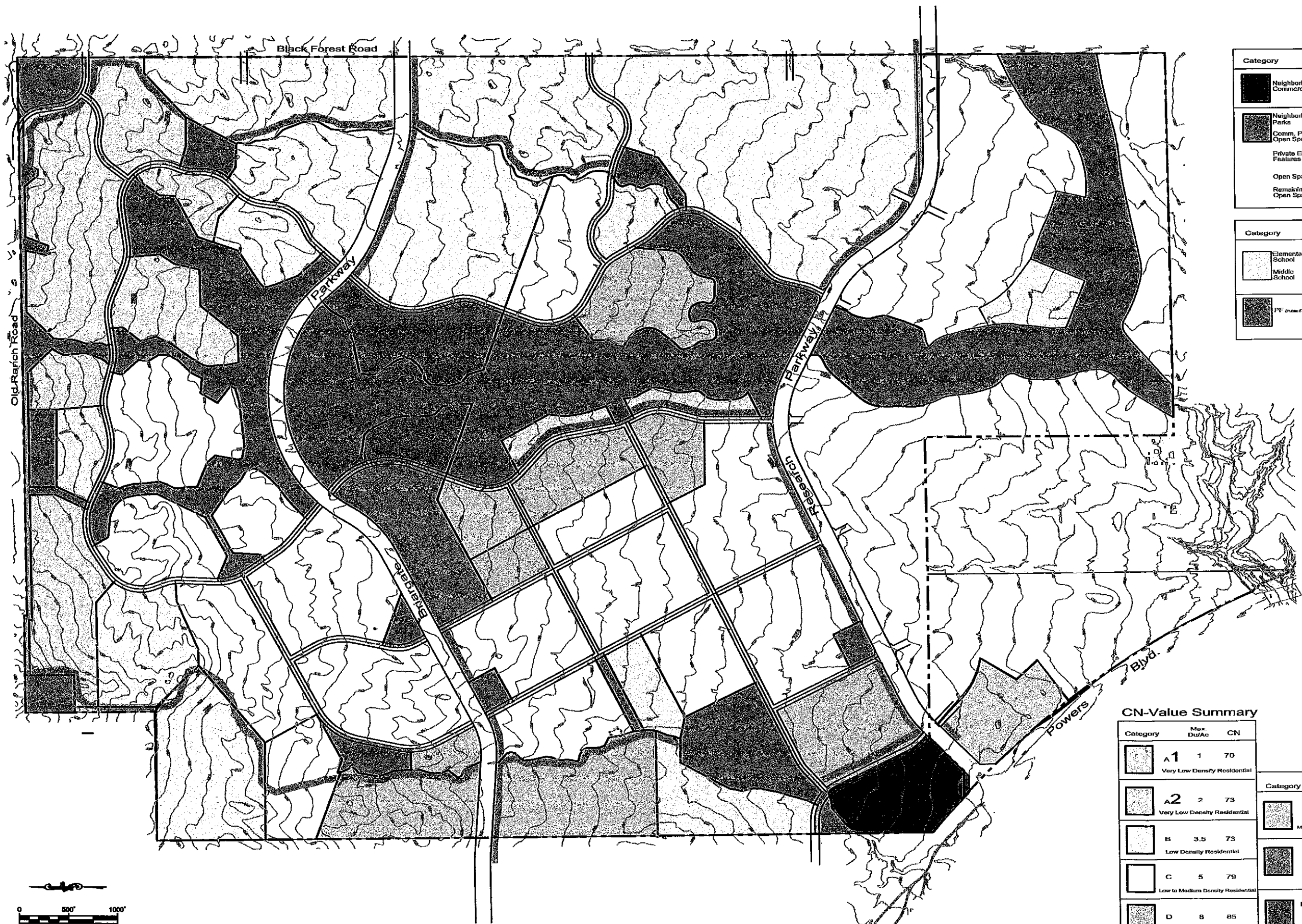
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 1604 South 21st Street
 Colorado Springs, Colorado
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WOLF RANCH
MASTER DEVELOPMENT DRAINAGE PLAN
HYDROLOGIC SOILS MAP
 COLORADO SPRINGS, COLORADO

Project No.:	03094
Date:	01-04
Design:	RHW
Drawn:	EAK
Check:	RHW
Revisions:	

SHEET

Fig. 2

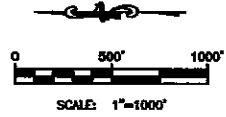


Category	CN
Neighborhood Commercial	92
Neighborhood Parks Comm. Parks/ Open Space	61
Private Entry Features	
Open Space	
Remaining Open Space	

Category	CN
Elementary School	75
Middle School	80
PF (Paved Facility)	70

CN-Value Summary

Category	Max. Du/Ac	CN
A1 Very Low Density Residential	1	70
A2 Very Low Density Residential	2	73
B Low Density Residential	3.5	73
C Low to Medium Density Residential	5	79
D Medium Density Residential	8	85
E Medium to High Density Residential	12	88
F High Density Residential	25	92
Mixed Use	Up to 25.00	92



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WOLF RANCH
MASTER DEVELOPMENT DRAINAGE PLAN
HYDROLOGIC LANDUSE MAP
 COLORADO SPRINGS, COLORADO

Project No.:	03084
Date:	01-04
Design:	RNW
Drawn:	EAK
Check:	RNW
Revisions:	

SHEET
Fig. 3

As shown on Figure 4 the "A" basins discharge to an existing concrete box culvert under Powers Boulevard. The sub-watershed drains a total of .42 square miles at its outfall point along the west boundary of the development. Slopes along the major drainageway range from 3 to 5 percent. Soils are entirely hydrologic soil group B. There is a portion of sub-basin A-1 that lies offsite from Wolf Ranch. The offsite portion of sub-basin A-1 is presently developed into large rural lots ranging in size from 5 to 40 acres. The watershed is well vegetated with native grasses. A small portion of sub-basin A-1 is forested.

The "B" basins discharge to an existing 54-inch reinforced concrete storm sewer that is within Research Parkway west of Powers Boulevard. The sub-watershed drains a total of .15 square miles at its outfall point at Powers Boulevard. Slopes along the major drainageway range from 2 to 5 percent. Soils are entirely hydrologic soil group B. Sub-watershed B lies entirely within Wolf Ranch. The watershed is well vegetated with native grasses.

The "C" basins discharge to an existing 72-inch reinforced concrete storm sewer that is under Powers Boulevard near the southwest corner of the property. The sub-watershed drains a total of .25 square miles at its outfall point at Powers Boulevard. Slopes along the major drainageway range from 2 to 5 percent. Soils are predominantly hydrologic soil group B however a small portion of type A soil exists within sub-basin C-1. Sub-watershed C lies entirely within Wolf Ranch. Most of sub-basin C-2 lies within the Westcreek subdivision Filings 1 through 3. The watershed is well vegetated with native grasses.

The "D" basins discharge to Cottonwood Creek within an offsite property just upstream of Powers Boulevard. The sub-watershed drains a total of .36 square miles at its outfall point at Cottonwood Creek. Slopes along the major drainageway range from 2 to 5 percent. Soils are predominantly hydrologic soil group B. Sub-watershed D lies mostly within Wolf Ranch however sub-basin D-3 lies within the Goetsch property that lies south of Wolf Ranch. The watershed is well vegetated with native grasses. The major drainageway within sub-basin D-3 is stable and has no improvements such as grade controls or bank lining. The drainageway is poorly defined where it enters Cottonwood Creek.

The "E" basins discharge to the Cottonwood Creek drainageway through an offsite property just upstream of Powers Boulevard. The sub-watershed drains a total of .32 square miles at its outfall point at Cottonwood Creek. Slopes along the major drainageway range from 2 to 5 percent. Soils are entirely hydrologic soil group B.

Approximately 60-percent of sub-watershed E lies within Wolf Ranch however 40 percent lies within the Goetsch property south of Wolf Ranch. The watershed is well vegetated with native grasses. The major drainageway within sub-basin E-2 is stable and has no improvements such as grade controls or bank lining. A stock pond exists along the drainageway within the Goetsch property.

"F" basins discharge to Cottonwood Creek approximately 4,000 feet upstream of the bridge over Powers Boulevard. The sub-watershed drains a total of 2 square miles at its outfall point. Slopes along the major drainageway range from 2 to 4 percent. Soils are mostly classified as hydrologic soil group B however a small area of Type A soil exist along the west overbank of Tributary Four south of Research Parkway. There is a portion of sub-watershed F that is offsite from Wolf Ranch. The offsite portion of the sub-watershed (i.e., sub-basins F-1 though F-7) is presently developed into large rural lots ranging in size from 5 to 40 acres. The watershed is well vegetated with native grasses. A small portion of the upper watershed is forested. The major drainageway in the F sub-watershed is Tributary 4. There are presently no improvements along the drainageway in the form of bank lings or grade controls. The low flow channel and some segments of the 100-year floodplain that have cross-section that is well incised.

The "G" basins discharge to Cottonwood Creek approximately 500 feet upstream of the outfall of sub-watershed F. The sub-watershed drains a total of .32 square miles at its outfall point. Slopes along the major drainageway range from 2 to 3 percent. Soils are entirely hydrologic soil group B. A portion of sub-watershed G lies offsite from Wolf Ranch. The offsite portion of the sub-watershed (i.e., sub-basin G-1) is presently developed into large rural lots ranging in size from 2.5 to 5 acres. The watershed is well vegetated with native grasses.

The "H" basin discharges to Cottonwood Creek just downstream of Black Forest Road. This sub-watershed drains a total of .093 square miles at its outfall point. Slopes along the watershed range from 2 to 6 percent. Soils are entirely hydrologic soil group B. The sub-watershed is well vegetated with native grasses.

It was assumed in this report that the portions of the A- and F-basins that lie north of Old Ranch Road will not develop to any higher land use densities than exist today. If more dense development would occur north of Old Ranch Road, it has been further assumed that detention would be required so that the peak discharges flowing onto the Wolf Ranch development would not be increased over the existing condition rates calculated in this report.

DEVELOPED MAJOR SUB-WATERSHEDS

The study area was divided into nine major sub-watersheds. These sub-watersheds are noted in the hydrologic analysis by using the designations A through J. The sub-basins were coded accordingly (i.e., A-1, A-2, B-1, etc). The sub-basins for the developed condition existing condition are presented on Figure 5. For the most part the developed condition sub-watershed boundaries cover similar areas as compared to existing sub-watersheds. The sub-basin divides were determined using the master development plan so that basin divides and key design points could be evaluated at future major roads. Some minor sub-basin rerouting and diversions have occurred. The curve-numbers were revised for the developed conditions. The developed curve numbers ranged from 72 to 90. The time of concentration values and resulting time lags were evaluating using developed flow paths and storm sewers where applicable.

HYDROLOGY RESULTS

Presented of Figures 4 and 5 are the peak discharges that resulted from the hydrology analysis for sub-basins as well as at key design points within the development. Presented on Table 1 is a comparison of the DBPS discharges summarized in Reference 4 at each common design point. The variances in the peak discharges are largely the result of the differences between the HEC-1 model developed in the Reference 4 and this MDDP. A greater degree of sub-basin delineation has been applied in this MDDP that can cause differences in peak discharges. Differences if the sub-basin area can also produce variances between this MDDP and the DBPS. The input and output for the HEC-1 computer model for the existing and developed hydrologic analyses are contained within Appendix A of this report. There was no analysis conducted in this MDDP for the main stem of Cottonwood Creek. Peak discharges data shown on Table 1 that was obtained derived from the DBPS were applied in this MDDP for the estimation of the 100-year flood plain for Cottonwood Creek and the sizing selective of bank linings.

At design point A the primary difference between the 100-year peak discharge reported in Reference 4 and this MDDP is due to the larger basin area applied in this MDDP for the developed condition. A modestly lower curve number was applied in this MDDP compared to Reference 4. The lower curve number yields a lower unit discharge at design point A for the MDDP hydrology (i.e., 1,490 cubic feet per second/square mile (DBPS) versus 1,270 cubic feet per second/square (MDDP)). This result is consistent with the application of a lower curve number.

At design point F located at the confluence of Tributary Four and Cottonwood Creek the variance in the peak discharges is also the result of a larger area applied in the

TABLE 1:
COMPARISON OF 100-YEAR PEAK DISCHARGES
DEVELOPED CONDITION WITHOUT DETENTION
WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN

DESIGN POINT (cfs)	DBPS (REFERENCE 4)		MDDP (KIOWA)	
	Q5 (cfs)	Q100 (cfs)	Q5 (cfs)	Q100 (cfs)
A	n/r	553	206 270	722 930
F	n/r	1,450	360 310	1,870 1650
COTTONWOOD CREEK AT POWERS BOULEVARD	n/r	2,730 (1)	ne	ne
COTTONWOOD CREEK UPSTREAM OF TRIBUTARY FOUR	n/r	860 (1)	ne	ne

(1) Source: Cottonwood Creek DBPS, Ayres Associates, June 2000 (reference 4)
n/r = not reported in this MDDP
ne = no estimate made in this MDDP

MDDP and differing curve number. The unit discharges compare well between the DBPS and this MDDP, (i.e., 760 cubic feet per second/square mile (DBPS) versus 810 cubic feet per second/square (MDDP)).

REGIONAL DETENTION HYDROLOGY

Detention storage was determined through an iterative process where an initial volume was calculated based on the changes of SCS curve numbers between the existing and developed condition. The initial volume was refined using the HEC-1 model resulting in the storage volumes summarized in this report. The proposed development condition was modeled with sufficient detention storage so that the flow rates were maintained to historic levels at each outfall point along the development's southern and western boundaries. The implementation of detention storage will have the affect of reducing the size of major drainageway facilities that may lie downstream of a detention basin. Detention will extend the time and duration of peak discharges but significantly reduce the magnitude of the peak flow rates for the 5- and 100-year recurrence intervals.

Presented on Figure 6 are the locations and hydraulic characteristics of six detention basins that are proposed within the Wolf Ranch development. Each detention basin would be built with an outlet structure that would control the 5-year and 100-year discharges from the detention basin to historic levels at the discharge points from the property. Detention basins within sub-watershed A, E/D, DB18, DV19 and G will have additional storage attributed to water quality. Onsite detention is recommended for the development that may occur within sub-watersheds H and J since no site with the physical attributes for a detention basin exists. Detention basins A, DB18, DB19 and DB28 have been sited to take into account a roadway embankment that could be integrated into the design of the detention basin. Presented on Table 2 are peak flow comparisons at the discharge point of each sub-watershed for the existing, developed and detained hydrologic conditions.

At design point A an "allowable" discharge of 553 cubic feet per second was determined in Reference 4. The allowable discharge at Design Point A represents the maximum release rate from a developed A watershed and would be within the hydraulic capacity of the Fairfax Detention Basin. The Fairfax detention basin lies downstream of Powers Boulevard and is a regional detention basin that receives runoff from sub-watershed A. The discharge in the detained condition at design point A is 165 cubic feet per second well below the allowable discharge stated in Reference 4. The existing condition peak discharge estimated herein is 160 cubic feet per second.

TABLE 2:
COMPARISON OF EXISTING, FUTURE AND DETAINED CONDITIONS PEAK DISCHARGES
WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN

DESIGN POINT	LOCATION	EXISTING CONDITION		FUTURE CONDITION		DETAINED CONDITION	
		Q5 (cfs)	Q100 (cfs)	Q5 (cfs)	Q100 (cfs)	Q5 (cfs)	Q100 (cfs)
A	at West Property Line	11	157	250	854	34	166
A5	at Cross Creek Drive	N/A	N/A	254	862	34	165
A6	at existing stock pond	12	142	199	631	200	632
A3	at Briargate Boulevard	N/A	N/A	155	509	155	509
C	at Cottonwood Creek	8	94	114	328	114	328
D	at Cottonwood Creek	10	107	55	179	N/A	N/A
D2 (1)	at south property line	10	103	57	173	13	156
E	at Cottonwood Creek	11	124	111	334	N/A	N/A
E2 (1)	at south property line	6	66	116	336	13	156
F	Tributary 4 at Cottonwood Creek	49	661	321	1,740	114	600
F28	Tributary 4 at Research Parkway	55	664	323	1,719	112	558
F22	Tributary 4 1,000' south of Briargat	49	570	116	828	47	238
G	at Cottonwood Creek	13	155	120	489	11	140
H-1	at Research Parkway	5	41	17	63	17	63
H-2	at Cottonwood Creek	3	36	25	96	25	96

(1) Detained design points D2 and E2 combine the discharges for existing basins E-1 and design point D2

The input and output for the HEC-1 computer model for the detained hydrologic analysis is contained within Appendix A of this report.

HYDRAULICS

The sizing of the major drainageway conveyances, storm sewer outfall lines and roadway culverts was accomplished using the discharge data produced for the detained hydrologic condition. Presented on Figure 6 are the sizes for each of the major roadway crossings. Roadway culverts were determined using the Federal Highways Administration HY-8 Culvert Analysis program. The input and output for the culvert analyses are contained within Appendix B. Storm sewers shown on Figure 6 were determined using normal flow equations and a minimum slope of 2 percent. The major storm sewers were modeled in the HEC-1 analysis.

With the exception of the Cottonwood Creek and Tributary Four drainageways the open channels shown on Figure 6 were sized using normal depth equations. For grass-lined channels a maximum 100-year velocity of five feet per second was assumed. For channels lined with riprap a maximum 100-year design velocity of nine feet per second was applied. The spacing of grade control along open channels, including Cottonwood Creek and Tributary Four was determined using an assumption that the longitudinal slope would degrade to one-half of the existing longitudinal slope.

Presented on plan and profiles PP1 through PP6 contained within Appendix C are the proposed drainageway improvements for the segments of Tributary Four and Cottonwood Creek within the development. Grade controls would be sloping boulder or soil cement drops with a maximum drop height of six vertical feet. A typical section of a boulder sloping drop is included with the plan and profiles. The drop structure would provide for the control of the 5-year as well as the 100-year discharge through the drop. Selective riprap bank lining is proposed along Cottonwood Creek and Tributary Four. The locations proposed for bank lining are shown on the plan and profiles. A typical bank section and sloping drop has been provided for on the detail sheet PP7 as well.

Presented on the plan and profile drawings is the 100-year floodplain and profile for Cottonwood Creek and Tributary Four. The 100-year water surface was determined using the U. S. Army Corps of Engineers HEC-2 water surface profile program. The hydrology used to determine the floodplain and profile was the developed condition without detention. The 100-year velocity along Cottonwood Creek through the Wolf Ranch development ranges 4 to 10 feet per second. The 100-year velocity for Tributary Four ranges from 6 to 10 feet per second. These velocity ranges were used when determining the average riprap size needed for the selective linings.

Also presented on the plan and profiles is a proposed erosion setback for Cottonwood Creek and Tributary Four. This setback was determined using the “prudent line” methodology for erosion resistant banks conditions as outlined in Reference 8. This setback was determined in order to define the location of the encroachment limits for the Cottonwood Creek and Tributary Four corridors. This setback was determined since the banks will only be selectively lined and therefore some allowance for lateral migration of the stream channel could occur. Using the methodology outlined in Reference 8, the calculated setback ranges from 60 to 140 feet for Tributary Four. The location of the erosion setback denotes the limits of encroachment fill that would be associated with land development activities with the exception of roadway and utility crossings. The potential for vertical degradation will be limited by the drop structures. The use of the prudent line criteria is appropriate for the segments of Tributary Four and Cottonwood Creek within the property and is consistent with the Cottonwood Creek Drainage Basin Planning Study (Reference 4). The calculations associated with determining the location of the erosion setback are included within Appendix B.

FLOODPLAIN STATEMENT

Floodplains for the 100-year existing condition have been delineated for Cottonwood Creek within the Colorado Springs and El Paso County Flood Insurance Study (FIS). Cottonwood Creek is the only drainageway within the Wolf Ranch development that has been studied by FEMA.

Shown on Figure 7 is the project site superimposed on the Flood Insurance Study FIRM panel for this area of El Paso County. Portions of the Wolf Creek property lie within a 100-year floodplain and floodway as depicted in the in the City of Colorado Springs and El Paso County Flood Insurance Study (FIS), prepared by the Federal Emergency Management Agency (FEMA).

PROPOSED FACILITIES

Detention

The primary conclusion of this MDDP is that regional detention will be required to maintain the historic flow conditions at the development’s west and south property lines. It is proposed to construct six detention basins within the development. Three of the detention basins lie within the Tributary Four watershed. The remaining three lie within sub-watersheds A, E/D and G. Onsite detention is recommended for sub-watersheds H and J. As discussed above, the detention basins shown on Figure 6 collectively act to reduce the 100-year peak discharge to at or below historic conditions. Detention basin

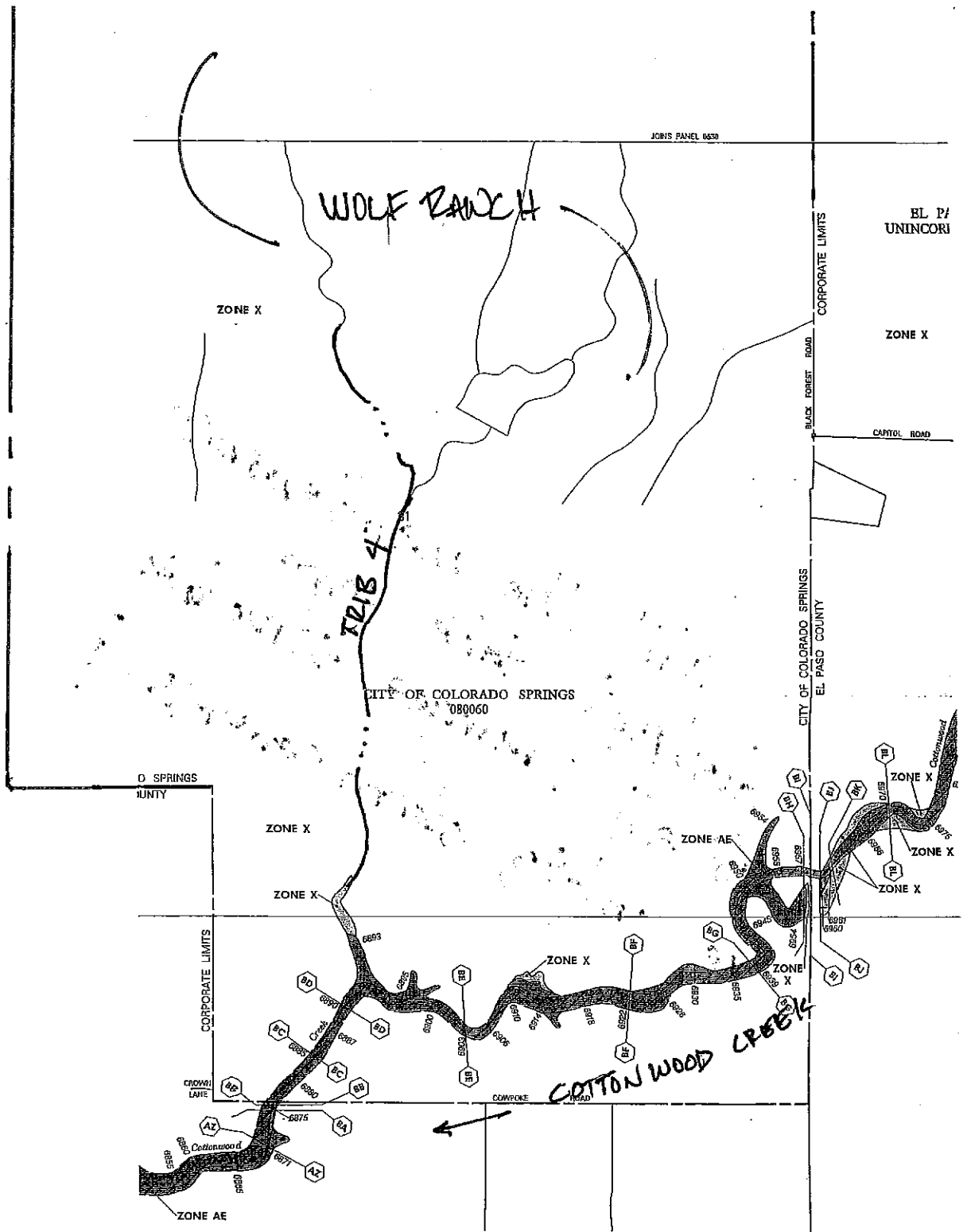


FIGURE 7
FLOODLAIN INFORMATION

E/D will be constructed with the Westcreek II subdivision. It is the intent of this MDDP to incorporate water quality storage and discharge control features for all of the detention basins except detention basin F28 that lies upstream of proposed Research Parkway embankment. Detention basin E/D should be designed with a constructed wetland bottom due to the presence of high groundwater and existing wetland vegetation. The HEC-1 models incorporating these storage facilities are contained within Appendix A of this report. The storage and outflow data for each of the detention basins are presented on Figure 6. Each detention basin will be designed to be in conformance with the City/County storm drainage technical criteria. Each detention basin will be required to have an emergency spillway. Easements or tracts dedicated for access and maintenance will be established at each detention basin site. Maintenance responsibility for each of the detention basins will be with a metropolitan district that will be formed for the area encompassed by the Wolf Ranch development.

How would that work?

Drainageways

The City of Colorado Springs, El Paso County Drainage Criteria Manual was used in the development of the typical sections and plans for the major drainageways within the Cross Creek Development. The City/County storm drainage criteria manual was supplemented by other criteria with more specific application. These were:

1. Urban Storm Drainage Criteria Manual, Volumes I, II, and III prepared by the Urban Drainage and Flood Control District.

The recommended channel sections for each reach of drainageway have been presented on Figure 6 at the rear of this report. Maintenance of the major drainageways including Cottonwood Creek and Tributary Four will be with a metropolitan district that will be formed for the area encompassed by the Wolf Ranch development.

The City of Colorado Springs adopted a streamside overlay zone for many of the natural watercourses that lie within the City in 2001. This zone was established in order to restrict encroachment of fill associated with development into the natural flood zones of a particular drainageway and to promote the preservation of the natural floodplain zones that may exist. Because of the prudent line assumption that has been advanced for Cottonwood Creek, Cottonwood Creek was exempted from the streamside overlay regulations and criteria. Tributary Four does not lie within a designated streamside overlay zone.

Drop and Check Structures

Drop structures have been sited along the Cottonwood Creek, and Tributary Four drainageways in order to maintain the channel invert at a stable gradient or to reduce the slope of the channel gradient so that lower velocities result along the drainageways. When determining the location of drop structures a degraded slope of no more than one-half of the existing slope was assumed. In the case of Cottonwood Creek the design slope ranged from 1.5 percent to 2 percent. In the case of Tributary Four the design slope applied was 1.25 percent. This assumption allows for the design to accommodate future channel degradation without modifying the existing channel section. The drops are designed to allow for a maximum drop of six feet and will have a sloping face of four to one.

Check structures are needed along the invert of some of the natural and smaller improved drainageways shown on Figure 6. The check will allow for a three-foot degradation of the invert prior to undermining a given check. These checks will be constructed of either riprap or concrete. A typical check structure detail has been presented on detail sheet PP7. The interval between checks is shown for each drainageway on Figure 6.

As with the detention basins and major drainageways the responsibility for maintenance will be dedicated to a metropolitan district to be formed for the area encompassed by the Wolf Ranch development.

?

Roadway Crossings

Summarized on Figure 6 are the size, type and location of roadway crossings along the major drainageways. The location of future arterials and collector streets was obtained from the development plan for Wolf Ranch. A 100-year headwater to depth ratio of 1.1 was assumed in the sizing of the major roadway culverts. The maintenance of roadway culverts under the public right-of-ways will be the responsibility of the City of Colorado Springs.

The existing crossings at Cowpoke Road and Black Forest Road are proposed to remain as they have sufficient capacity to pass the 100-year discharge without overtopping. These crossings are maintained by the El Paso County Department of Transportation. El Paso County recently extended the culvert at Black Forest Road and installed some additional riprap outlet protection. The bridge at Cowpoke Road will probably need replacement if Cowpoke Road is improved in the future.

As part of the annexation agreement for the Wolf Ranch property the Black Forest Road culvert will be required to be rebuilt by the developer of Wolf Ranch when traffic levels on Black Forest Road warrant the widening of the roadway.

be removed
when Tull Blvd is extended
across Cottonwood Creek
and Cowpoke
is realigned

DBPS SAYS
17
this is a bridge?

Are you planning to do anything with these culverts? If not, I would state it in this report.

Several culverts exist under Old Ranch Road at this time. These culverts range in size from 18-inches to 48-inches and are all corrugated metal pipe. The culverts have adequate capacity to convey the existing five-year flow under the roadway without overtopping. Some of the culverts have a 100-year capacity. It was assumed in the hydrologic analysis that the areas north of Old Ranch Road will not produce runoff greater than the existing condition rates calculated in this report. The majority of the area north of Old Ranch Road is developed. If a more dense land use takes place in the future detention would be required so as to not increase the rates of runoff to the Wolf Ranch property.

Trails

Trails for access to the detention basins and major drainageways need to be incorporated into the design of the improvements. For the Wolf Ranch a multi-purpose trail is proposed that is aligned along the Tributary Four. This trail will have to be accommodated at each of the roadway crossings by either an at grade or sub-grade crossing. Where practical, this trail can accommodate maintenance access to the channel and the detention basins. If the trail encroaches into a 100-year floodplain, the trail design should take into account hydraulic considerations, utilities in the area and access to dedicated parks and roadway crossings. Maintenance access to the drainageway and to existing utilities within the drainageway corridor can offer a multiple use aspect to a trail project.

Maintenance and Revegetation

Maintenance of drainageway facilities is essential in preventing long term degradation of the drainageway and overbank areas. Along the drainageway, clearing of debris and dead vegetation should be considered within the low flow area of the creek and its tributaries. On the overbanks, limited maintenance of the existing vegetative cover is recommended. Yearly clearing of trash and debris at roadway crossings is also recommended to ensure the design capacity of the crossing, and to enhance the crossings for trail users if a trail exists. Caution should be taken when clearing culverts of sediment so as not to leave the dredged soil within the channel or overbank area. This disturbs the native vegetation and creates a potential water quality concern if the dredged material is subsequently washed into the drainageway by natural erosion. For those reaches of drainageways that are designated for selective lining and the floodplain preservation, maintenance activities should be carried out while minimizing the disturbances to native vegetation.

The proposed detention basins will also require annual maintenance. The outlet structures will need to be cleared and the entry channel and forebays cleared of debris or silt. For those detention basin where water quality storage has been incorporated into the design, the clearing of sediment from the water quality pools will need to be carried out on a yearly basis as well, minimum.

Right-of-Way

It will be required for the main drainageways within the development that pass through the basin to be within dedicated tracts, easements or right-of-ways. For those segments of the drainageway where floodplain preservation is the recommended plan, a combination of open space dedication (such as park-land and greenbelts), in combination with a more narrow dedicated maintenance right-of-way along the low flow area of the drainageway should be obtained through the land development process. Land dedication will be required for the detention basins. The dedication of easements and right-of-way for the drainageways and detention basins would be accomplished at the time of development planning and/or platting of the parcels that lie adjacent to or upstream of the stormwater facility.

- who would own

DRAINAGE BASIN FEES

It is the intent of the developer to request that the developable land within the Wolf Ranch property be exempted from the assessment of drainage fees associated with the Cottonwood Creek basin and in essence "close" the basin. As such the developable acreage subject to fee assessment that has been is estimated at 1,484 acres would be removed from the Cottonwood basin. Additionally, the drainageway improvements identified in the DBPS for the portion of Cottonwood Creek within the property and for Tributary Four would not be subject to reimbursement. The land associated with the erosion control setback will also not be subject to reimbursement through the Cottonwood Creek basin fee system.

Do you have an estimate of what that amount is?

A formal presentation to the Drainage Board will be conducted wherein the recalculation of the basins fees will be discussed and revised accordingly based upon the recommendation of the Drainage Board. It is understood that the City will not provide a final approval of the MDDP until the revised fees for the basin have been resolved and reestablished.

and the In addition, the Cottoncreek DBPS will need to be updated per the outcome of this action.

APPENDIX A
HYDROLOGIC CALCULATIONS

WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN
 WEIGHTED CN-VALUES
 FUTURE DEVELOPMENT CONDITIONS

A-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
A-1	38.2	61	0	0	0	38.2	0	0	0	61.0
A-3	96.0	61	85	73	0	7.3	31.1	57.6	0	76.0
A-4	55.1	79	0	0	0	55.1	0	0	0	79.0
A-5	71.3	80	85	61	0	26.7	28.6	16	0	77.7
A-6	23.7	79	85	0	0	20.5	3.2	0	0	79.8
A-7	32.0	70	79	0	0	2.8	29.2	0	0	78.2
A-9	43.1	79	61	70	0	21.4	11.2	10.5	0	72.1
A-10	5.5	61	0	0	0	5.5	0	0	0	61.0
A-11	51.8	61	73	79	0	2.7	0.9	48.2	0	78.0

WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN
 WEIGHTED CN-VALUES
 FUTURE DEVELOPMENT CONDITIONS

C-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
C-1	29.4	79	0	0	0	29.4	0	0	0	79.0
C-2	70.4	79	88	0	0	58.0	12.4	0	0	80.6
C-3	35.2	79	0	0	0	35.2	0	0	0	79.0

WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN
 WEIGHTED CN-VALUES
 FUTURE DEVELOPMENT CONDITIONS

B-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
B-1	25.6	92	85	73	0	25.6	0	0	0	92.0

WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN
 WEIGHTED CN-VALUES
 FUTURE DEVELOPMENT CONDITIONS

D-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
D-1	39.4	79	70	0	0	35.5	3.9	0	0	78.1
D-2	23.0	79	0	0	0	23.0	0	0	0	79.0
D-3	15.4	61	0	0	0	15.4	0	0	0	61.0

WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN
 WEIGHTED CN-VALUES
 FUTURE DEVELOPMENT CONDITIONS

E-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
E-1	25.8	79	85	0	0	13.9	11.9	0	0	81.8
E-2	33.3	79	0	0	0	33.3	0	0	0	79.0
E-3	63.7	61	0	0	0	63.7	0	0	0	61.0
E-4	27.1	79	0	0	0	27.1	0	0	0	79.0
E-5	25.6	79	0	0	0	25.6	0	0	0	79.0
E-6	30.6	79	0	0	0	30.6	0	0	0	79.0

WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN
 WEIGHTED CN-VALUES
 FUTURE DEVELOPMENT CONDITIONS

F-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
F-1 to F-7										data taken from prior program compilations
F-8	57.8	61	70	73	0	11.6	17.3	28.9	0	69.7
F-9	27.5	61	70	75	0	8.3	13.7	5.5	0	68.2
F-10	11.5	61	70	75	0	5.2	1.2	5.2	0	68.8
F-11	29.4	61	70	0	0	5.9	23.5	0	0	68.2
F-12	37.8	61	70	0	0	3.7	34.1	0	0	69.1
F-13	9	61	70	0	0	9.0	0	0	0	60.7
F-14	82.6	61	70	73	0	0.0	0	82.6	0	73.0
F-15	13.4	61	70	73	0	2.7	6.7	4	0	69.1
F-16	17.3	61	70	73	0	3.5	3.4	10.38	0	69.9
F-17	24.3	61	70	73	0	23.1	0	1.2	0	61.6
F-18	63	61	73	79	0	17.9	17.9	25.2	0	69.7

F-19	65.3	61	73	79	0	20.9	0	44.4	0	73.2
F-21	50.6	85	88	92	0	12.6	12.6	25.3	0	89.1
F-22	41	61	92	0	0	36.9	4.1	0	0	64.1
F-23	19.8	0	73	0	0	0.0	19.8	0	0	73.0
F-24	57	0	73	79	0	0.0	40	17	0	74.8
F-25	57	0	73	79	0	0.0	51	6	0	73.6
F-26	34	0	79	85	0	0.0	17	17	0	82.0
F-27	129	61	73	85	92	90.0	6	6	27	69.2
F-28	24	61	73	85	92	12.0	0	12	0	73.0
F-29	16	61	73	85	92	8.0	0	8	0	73.0
F-30	14	61	75	85	92	2.8	11.2	0	0	72.2
F-31	60	61	73	85	92	40.0	20	0	0	65.0

WOLF RANCH MASTER DEVELOPMENT DRAINAGE PLAN
 WEIGHTED CN-VALUES
 FUTURE DEVELOPMENT CONDITIONS

G-BASINS

SUB-BASIN NUMBER	BASIN AREA (AC)	CN-VALUES				AREAS				WEIGHTED CN-VALUE
		CN 1	CN 2	CN3	CN4	AREA 1	AREA 2	AREA 3	AREA 4	
G-1										data taken from prior program compilations
G-2	22.4	73	0	0	0	22.4	0	0	0	73.0
G-3	113.3	73	75	0	0	111.9	1.4	0	0	73.0
G-4	59.9	61	79	92	0	0.2	57.3	2.4	0	79.5
G-5	43.5	61	79	0	0	5.6	37.9	0	0	76.7

Wolf Ranch Master Development Drainage Plan
Time of Concentration
A-basins

Basin	Slope			Length			Run Coef. (5-year)	Velocity			T _c		T _c	Basin	
	O'land	Chan. 1	Chan. 2	O'land	Chan. 1	Chan. 2		O'land	Chan. 1	Chan. 2	Chan. 1	Chan. 2			
A-1	9.0 %	6.1 %	0 %	1,000 lf	1,650 lf	0 lf	0.20	8.0 ft/sec	8.0 ft/sec	0.0 ft/sec	1536 sec.	206 sec.	0 sec.	29.0 min.	A-1
A-3	6.0 %	2.1 %	0 %	300 lf	3,200 lf	0 lf	0.45	8.0 ft/sec	5.0 ft/sec	0.0 ft/sec	696 sec.	640 sec.	0 sec.	22.3 min.	A-3
A-4	2.0 %	4.1 %	3 %	300 lf	850 lf	1,650 lf	0.50	2.0 ft/sec	8.0 ft/sec	8.0 ft/sec	926 sec.	106 sec.	206 sec.	20.6 min.	A-4
A-5	2.0 %	3.1 %	1 %	300 lf	2,050 lf	1,120 lf	0.60	2.0 ft/sec	8.0 ft/sec	5.0 ft/sec	771 sec.	256 sec.	224 sec.	20.9 min.	A-5
A-6	2.0 %	1.6 %	0 %	300 lf	1,550 lf	0 lf	0.50	2.0 ft/sec	5.0 ft/sec	5.0 ft/sec	926 sec.	310 sec.	0 sec.	20.6 min.	A-6
A-7	2.0 %	2.0 %	0 %	100 lf	2,000 lf	0 lf	0.50	2.0 ft/sec	4.0 ft/sec	10.0 ft/sec	534 sec.	500 sec.	0 sec.	17.2 min.	A-7
A-9	2.0 %	2.0 %	0 %	300 lf	2,300 lf	0 lf	0.45	2.0 ft/sec	4.0 ft/sec	10.0 ft/sec	1003 sec.	575 sec.	0 sec.	26.3 min.	A-9
A-10	5.0 %	0.0 %	0 %	550 lf	0 lf	0 lf	0.20	5.0 ft/sec	4.0 ft/sec	10.0 ft/sec	1386 sec.	0 sec.	0 sec.	23.1 min.	A-10
A-11	4.7 %	3.4 %	0 %	300 lf	1,252 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	813 sec.	313 sec.	0 sec.	18.8 min.	A-11

Equations:

$$\text{Time of Concentration (Overland)} = 1.87(1.1 - C_2)L^{0.5} S^{-0.333}$$

C₂ = Runoff coefficient for five-year flow

L = Length of overland flow in feet

S = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{(0.5 \log S + 0.2)})$$

S = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_n^{2/3} S^{1/2}$$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Wolf Ranch Master Development Drainage Plan
Time of Concentration
B-basins

Basin	Slope			Length			Run Coef (5-year)	Velocity			T _c			Basin	
	Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		T _c
B-1	2.0 %	2.0 %	0 %	100 lf	1,850 lf	0 lf	0.90	2.0 ft/sec	4.0 ft/sec	0.0 ft/sec	178 sec.	463 sec.	0 sec.	10.7 min.	B-1

Equations:

$$\text{Time of Concentration (Overland)} = 1.47(1.1 - C_s)L^{0.5} S^{-0.333}$$

C_s = Runoff coefficient for five-year flow

L = Length of overland flow in feet

S = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{(0.51 \log S + 0.3)})$$

S = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_n^{2/3} S^{1/2}$$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Wolf Ranch Master Development Drainage Plan
Time of Concentration
C-basins

Basin	Slope			Length			Run Coef. (5-year)	Velocity			T _c			Basin	
	Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		
C-1	2.0 %	3.0 %	0 %	100 lf	1,950 lf	0 lf	0.60	2.0 ft/sec	4.0 ft/sec	0.0 ft/sec	445 sec.	488 sec.	0 sec.	15.5 min.	C-1
C-2	3.0 %	4.0 %	0 %	100 lf	650 lf	3,450 lf	0.55	2.0 ft/sec	4.0 ft/sec	6.0 ft/sec	428 sec.	163 sec.	0 sec.	9.8 min.	C-2
C-3	2.5 %	2.0 %	0 %	100 lf	2,650 lf	0 lf	0.55	2.0 ft/sec	4.0 ft/sec	0.0 ft/sec	455 sec.	663 sec.	0 sec.	18.6 min.	C-3

Equations:

$$\text{Time of Concentration (Overland)} = 1.87(1.1 - C_3)L^{0.5} S^{-0.333}$$

C_3 = Runoff coefficient for five-year flow

L = Length of overland flow in feet

S = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{(0.5 \log S + 0.3)})$$

S = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_h^{2/3} S^{1/2}$$

Slope (S) = Slope of the channel

n = Manning's number

R_h = Hydraulic Radius (Reynold's Number)

Wolf Ranch Master Development Drainage Plan
Time of Concentration
D-basins

Basin	Slope			Length			Run Coef (5-year)	Velocity			T _c			Basin	
	O'land	Chan 1	Chan 2	O'land	Chan 1	Chan 2		O'land	Chan 1	Chan 2	O'land	Chan 1	Chan 2		
D-1	2.0 %	2.0 %	0 %	100 lf	2,350 lf	0 lf	0.55	2.0 ft/sec	4.0 ft/sec	0.0 ft/sec	490 sec.	588 sec.	0 sec.	18.0 min.	D-1
D-2	2.0 %	3.0 %	0 %	100 lf	1,350 lf	0 lf	0.55	2.0 ft/sec	6.0 ft/sec	0.0 ft/sec	490 sec.	225 sec.	0 sec.	11.9 min.	D-2
D-3	4.0 %	2.6 %	0 %	800 lf	1,920 lf	0 lf	0.20	7.0 ft/sec	4.0 ft/sec	0.0 ft/sec	1800 sec.	480 sec.	0 sec.	38.0 min.	D-3

Equations:

$$\text{Time of Concentration (Overland)} = 1.48(1.1 - C_s)L^{0.5} S^{-0.333}$$

C_s = Runoff coefficient for five-year flow

L = Length of overland flow in feet

S = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{(0.5 \log S + 0.3)})$$

S = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_h^{2/3} S^{1/2}$$

Slope (S) = Slope of the channel

n = Manning's number

R_h = Hydraulic Radius (Reynold's Number)

Wolf Ranch Master Development Drainage Plan
Time of Concentration
E-basins

Basin	Slope			Length			Run Coef (5-year)	Velocity			T _c			Basin	
	O'land	Chan. 1	Chan. 2	O'land	Chan. 1	Chan. 2		O'land	Chan. 1	Chan. 2	O'land	Chan. 1	Chan. 2		
E-1	2.0 %	2.0 %	0 %	100 lf	1,700 lf	0 lf	0.60	2.0 ft/sec	4.0 ft/sec	0.0 ft/sec	445 sec.	425 sec.	0 sec.	14.5 min.	E-1
E-2	3.0 %	3.0 %	0 %	100 lf	2,250 lf	0 lf	0.55	2.0 ft/sec	6.0 ft/sec	0.0 ft/sec	428 sec.	375 sec.	0 sec.	13.4 min.	E-2
E-3	3.0 %	2.0 %	0 %	700 lf	3,150 lf	0 lf	0.25	2.0 ft/sec	5.0 ft/sec	0.0 ft/sec	1750 sec.	630 sec.	0 sec.	39.7 min.	E-3
E-4	2.0 %	2.0 %	0 %	100 lf	2,150 lf	0 lf	0.55	2.0 ft/sec	6.0 ft/sec	0.0 ft/sec	490 sec.	358 sec.	0 sec.	14.1 min.	E-4
E-5	3.0 %	3.0 %	0 %	100 lf	1,700 lf	0 lf	0.55	2.0 ft/sec	6.0 ft/sec	0.0 ft/sec	428 sec.	283 sec.	0 sec.	11.9 min.	E-5
E-6	2.0 %	2.0 %	0 %	100 lf	2,200 lf	0 lf	0.50	2.0 ft/sec	4.0 ft/sec	0.0 ft/sec	534 sec.	550 sec.	0 sec.	18.1 min.	E-6

Equations:

$$\text{Time of Concentration (Overland)} = 1.47(1.1 - C_5)L^{0.4} S^{-0.333}$$

C₅ = Runoff coefficient for five-year flow

L = Length of overland flow in feet

S = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{(0.5 \log S + 0.3)})$$

S = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_n^{2/3} S^{1/2}$$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Wolf Ranch Master Development Drainage Plan
Time of Concentration
F-basins

Basin	Slope			Length			Run Coef (5-year)	Velocity			T _c			Basin	
	Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		Overland	Chan. 1	Chan. 2	Overland	Chan. 1	Chan. 2		T _c
F-8	6.7 %	4.4 %	0 %	298 lf	2,323 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	720 sec.	581 sec.	0 sec.	21.7 min.	F-8
F-9	6.3 %	4.0 %	0 %	300 lf	927 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	737 sec.	232 sec.	0 sec.	16.1 min.	F-9
F-10	6.7 %	5.0 %	0 %	300 lf	600 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	722 sec.	150 sec.	0 sec.	14.5 min.	F-10
F-11	5.7 %	4.1 %	0 %	300 lf	918 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	762 sec.	230 sec.	0 sec.	16.5 min.	F-11
F-12	4.0 %	3.3 %	0 %	300 lf	1,290 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	857 sec.	323 sec.	0 sec.	19.7 min.	F-12
F-13	7.3 %	5.2 %	0 %	300 lf	498 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	702 sec.	125 sec.	0 sec.	13.8 min.	F-13
F-14	3.7 %	3.1 %	3 %	300 lf	1,081 lf	1,730 lf	0.40	4.0 ft/sec	4.0 ft/sec	8.0 ft/sec	880 sec.	270 sec.	216 sec.	22.8 min.	F-14
F-15	5.8 %	3.7 %	0 %	300 lf	931 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	758 sec.	233 sec.	0 sec.	16.5 min.	F-15
F-16	2.6 %	2.6 %	0 %	300 lf	1,085 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	990 sec.	271 sec.	0 sec.	21.0 min.	F-16
F-17	3.7 %	3.4 %	3 %	300 lf	945 lf	990 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	880 sec.	236 sec.	124 sec.	20.7 min.	F-17
F-18	3.3 %	3.5 %	0 %	300 lf	1,465 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	914 sec.	366 sec.	0 sec.	21.3 min.	F-18
F-19	4.5 %	5.9 %	4 %	300 lf	654 lf	1,155 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	824 sec.	159 sec.	144 sec.	18.8 min.	F-19
F-21	3.3 %	2.3 %	0 %	300 lf	2,420 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	914 sec.	605 sec.	0 sec.	25.3 min.	F-21
F-22	4.1 %	3.5 %	0 %	300 lf	1,705 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	850 sec.	426 sec.	0 sec.	21.3 min.	F-22
F-23	4.0 %	4.8 %	2 %	300 lf	414 lf	890 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	857 sec.	104 sec.	111 sec.	17.9 min.	F-23
F-24	4.0 %	2.1 %	0 %	300 lf	2,765 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	857 sec.	691 sec.	0 sec.	25.8 min.	F-24
F-25	2.0 %	2.8 %	0 %	300 lf	2,270 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	1080 sec.	568 sec.	0 sec.	27.5 min.	F-25
F-26	4.7 %	2.7 %	0 %	300 lf	1,250 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	813 sec.	313 sec.	0 sec.	18.8 min.	F-26
F-27	2.7 %	3.8 %	2 %	300 lf	1,650 lf	4,150 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	977 sec.	413 sec.	519 sec.	31.8 min.	F-27
F-28	3.3 %	4.7 %	0 %	300 lf	1,950 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	914 sec.	488 sec.	0 sec.	23.4 min.	F-28
F-29	2.7 %	4.3 %	0 %	300 lf	655 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	977 sec.	164 sec.	0.0 ft/sec	19.0 min.	F-29
F-30	3.3 %	4.1 %	0 %	300 lf	680 lf	0 lf	0.40	5.0 ft/sec	4.0 ft/sec	0.0 ft/sec	914 sec.	170 sec.	0.0 ft/sec	18.1 min.	F-30
F-31	3.3 %	5.0 %	3 %	300 lf	1,600 lf	1,110 lf	0.40	5.0 ft/sec	4.0 ft/sec	8.0 ft/sec	914 sec.	400 sec.	139 sec.	24.2 min.	F-31

Equations:

$$\text{Time of Concentration (Overland)} = 1.87(1.1 - C_3)L^{0.5} S^{-0.533}$$

C₃ = Runoff coefficient for five-year flow

L = Length of overland flow in feet

S = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{(0.51 \log S + 0.3)})$$

S = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_n^{2/3} S^{1/2}$$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Wolf Ranch Master Development Drainage Plan
Time of Concentration
G-basins

Basin	Slope			Length			Run Coef. (5-year)	Velocity			TC			T _T	Basin
	O'land	Chan. 1	Chan. 2	O'land	Chan. 1	Chan. 2		O'land	Chan. 1	Chan. 2	O'land	Chan. 1	Chan. 2		
G-2	3.5 %	2.9 %	0 %	284 lf	1,796 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	872 sec.	449 sec.	0 sec.	22.0 min.	G-2
G-3	3.0 %	2.6 %	0 %	263 lf	3,376 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	883 sec.	844 sec.	0 sec.	28.8 min.	G-3
G-4	3.2 %	2.6 %	0 %	249 lf	1,780 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	841 sec.	445 sec.	0 sec.	21.4 min.	G-4
G-5	2.7 %	4.1 %	0 %	300 lf	1,900 lf	0 lf	0.40	4.0 ft/sec	4.0 ft/sec	0.0 ft/sec	977 sec.	475 sec.	0 sec.	24.2 min.	G-5

Equations:

$$\text{Time of Concentration (Overland)} = 1.87(1.1 - C_5)L^{0.5} S^{-0.333}$$

C_5 = Runoff coefficient for five-year flow

L = Length of overland flow in feet

S = Slope of flow path in percent

$$\text{Velocity (Road)} = 10(10^{(0.5 \log S + 0.3)})$$

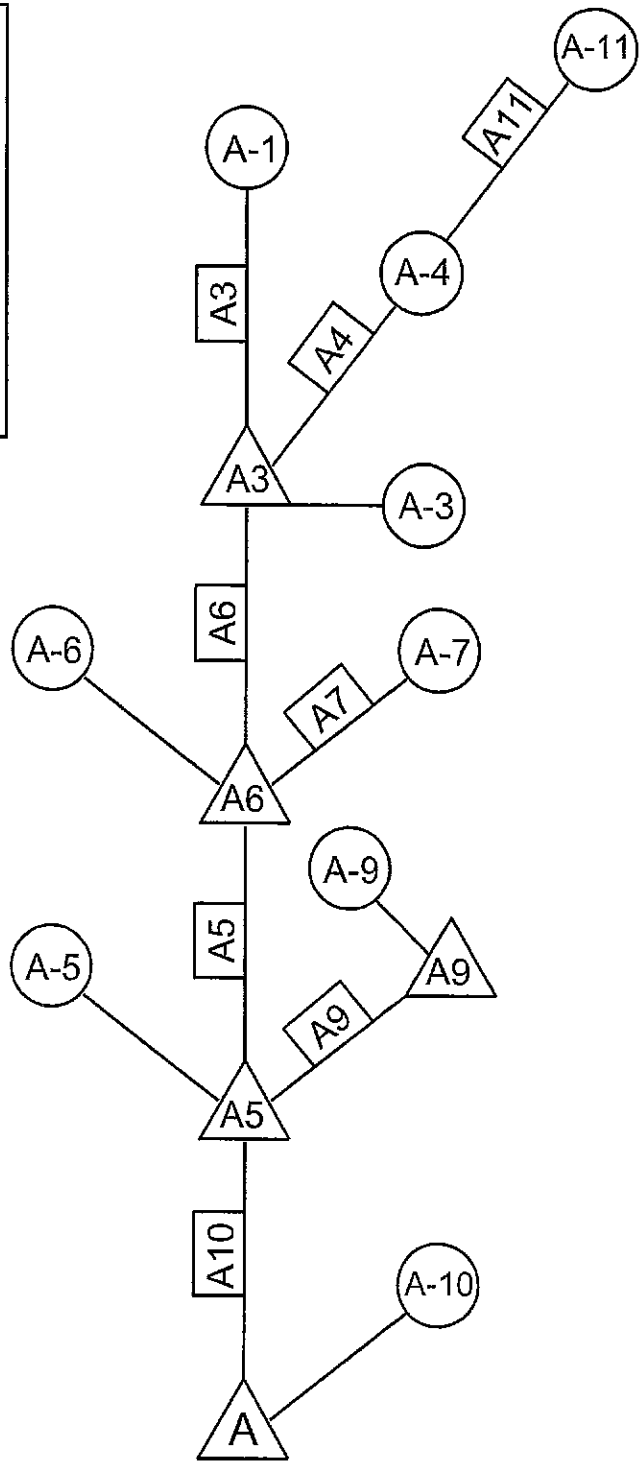
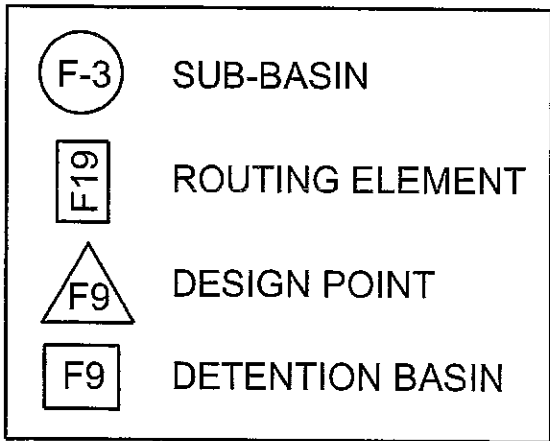
S = Slope of flow path in percent

$$\text{Velocity (Channel)} = (1.49/n)R_n^{2/3} S^{1/2}$$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)



HEC1 FLOW SCHEMATIC
DEVELOPED CONDITION 'A' BASINS

Kiowa Engineering Corporation

1604 South 21st Street
Colorado Springs, Colorado
80904-4208
(719) 630-7342

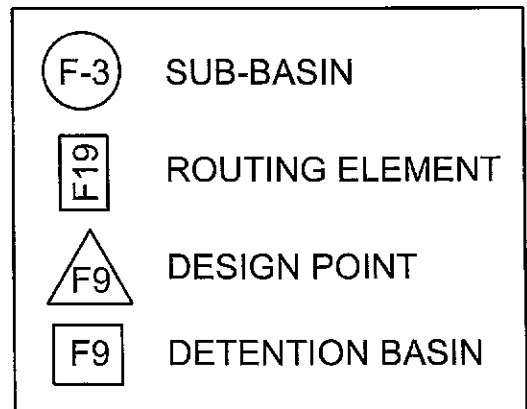
WOLF RANCH
HYDROLOGIC MODEL SCHEMATIC
COLORADO SPRINGS, COLORADO

FIGURE A

PROJECT NO.: 03094
DATE: 01/29/04
DESIGN: RNW
REVISIONS:



HEC1 FLOW SCHEMATIC
DEVELOPED CONDITION 'B' BASINS



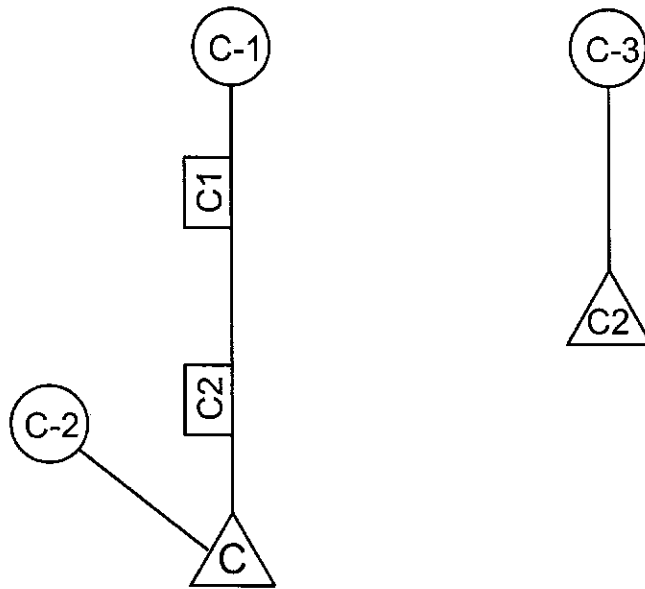
Kiowa Engineering Corporation

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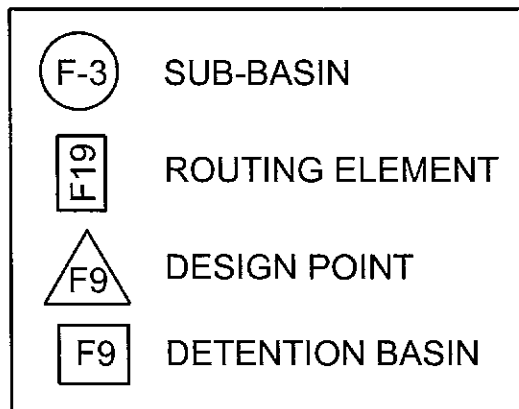
WOLF RANCH
HYDROLOGIC MODEL SCHEMATIC
COLORADO SPRINGS, COLORADO

FIGURE B

PROJECT NO.: 03094
DATE: 01/29/04
DESIGN: RNW
REVISIONS:



HEC1 FLOW SCHEMATIC
DEVELOPED CONDITION 'C' BASINS



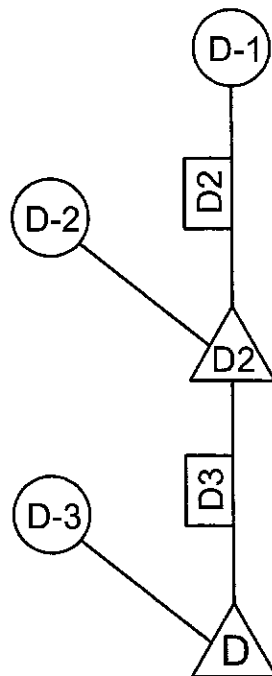
Kiowa Engineering Corporation

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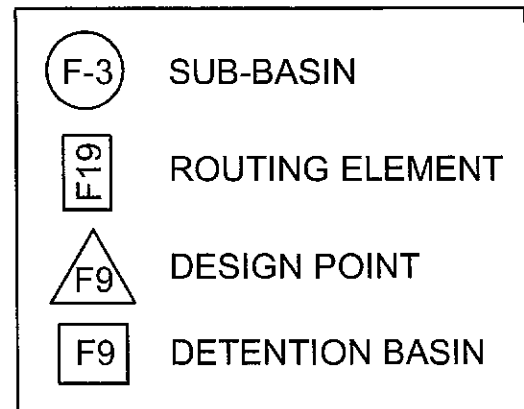
WOLF RANCH
HYDROLOGIC MODEL SCHEMATIC
COLORADO SPRINGS, COLORADO

FIGURE C

PROJECT NO.: 03094
DATE: 01/29/04
DESIGN: RNW
REVISIONS:



HEC1 FLOW SCHEMATIC
DEVELOPED CONDITION 'D' BASINS



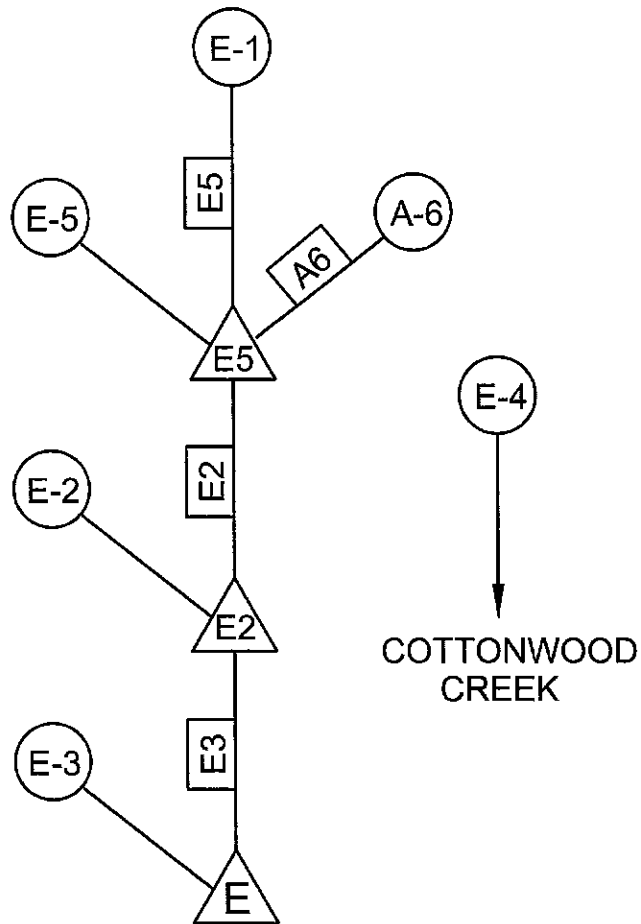
Kiowa Engineering Corporation

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 Colorado Springs, Colorado
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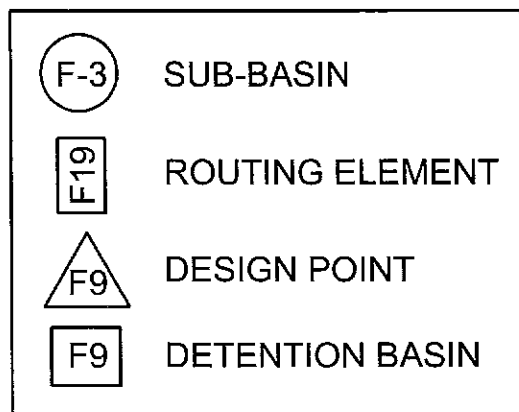
WOLF RANCH
 HYDROLOGIC MODEL SCHEMATIC
 COLORADO SPRINGS, COLORADO

FIGURE D

PROJECT NO.: 03094
 DATE: 01/29/04
 DESIGN: RNW
 REVISIONS:



HEC1 FLOW SCHEMATIC
DEVELOPED CONDITION 'E' BASINS



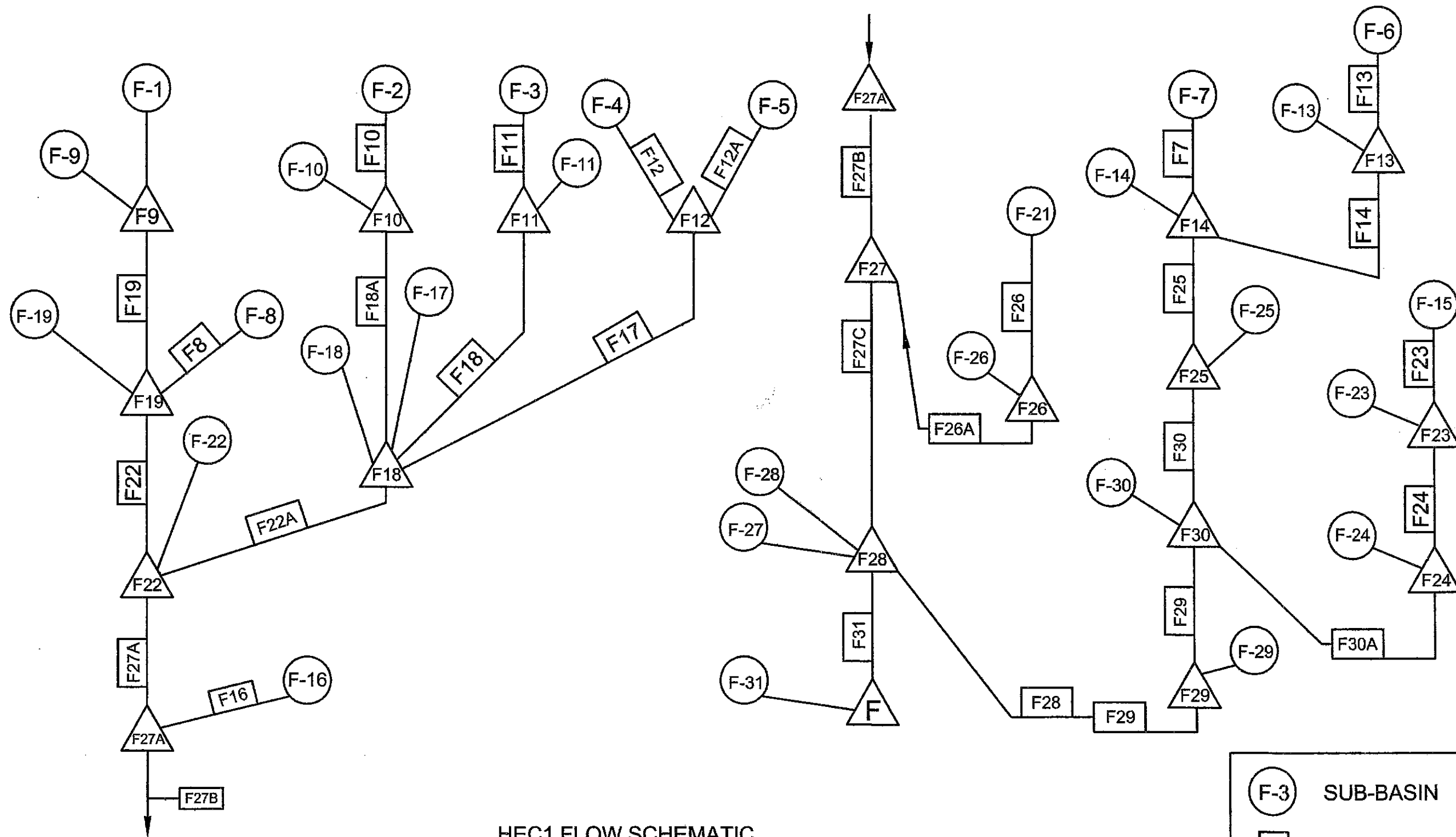
Kiowa Engineering Corporation

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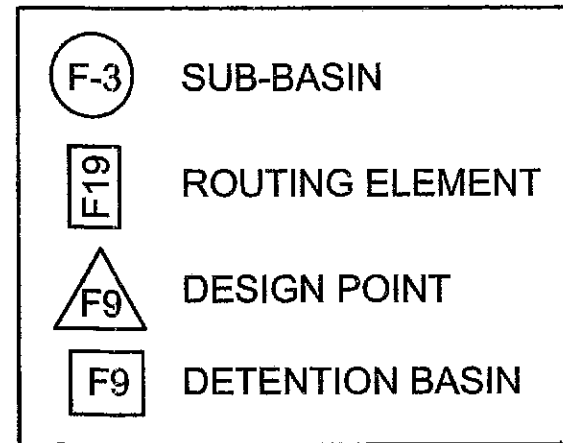
WOLF RANCH
 HYDROLOGIC MODEL SCHEMATIC
 COLORADO SPRINGS, COLORADO

FIGURE E

PROJECT NO.: 03094
 DATE: 01/29/04
 DESIGN: RNW
 REVISIONS:



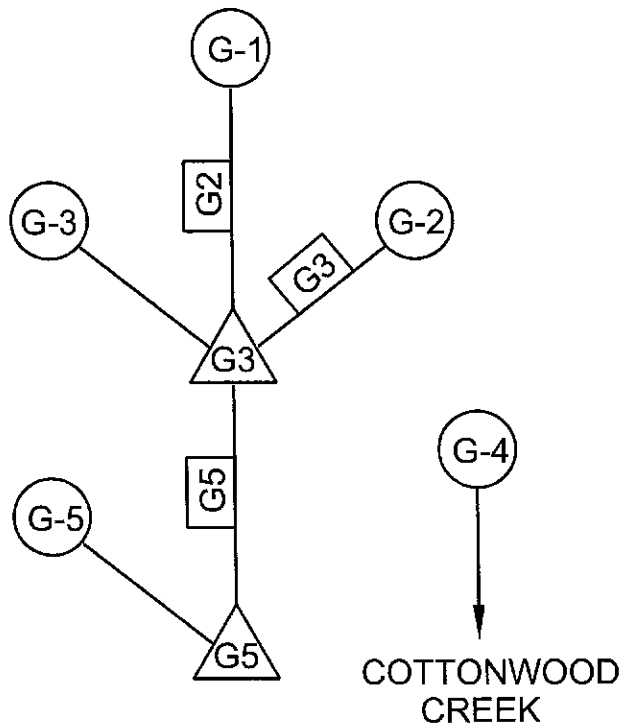
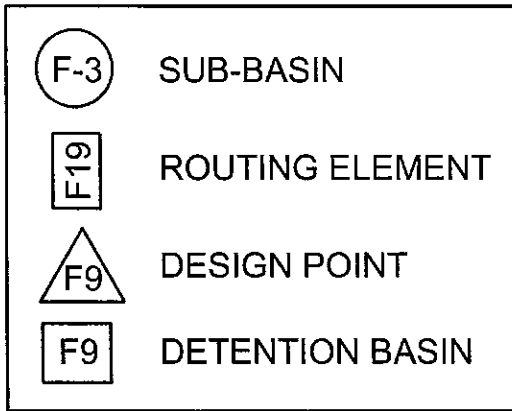
HEC1 FLOW SCHEMATIC
DEVELOPED CONDITION 'F' BASINS



Kiowa Engineering Corporation
 1604 South 21st St.
 Colorado Springs, Colorado
 80904-4208
 (719) 590-7342

WOLF RANCH
 HYDROLOGIC MODEL SCHEMATIC
 FIGURE F
 COLORADO SPRINGS, COLORADO

Project No.:	03004
Scale:	
Date:	05/09/04
Design:	RHW
Drawn:	JLN
Check:	RHW
Revised:	



HEC1 FLOW SCHEMATIC
DEVELOPED CONDITION 'G' BASINS

<p><u>Kiowa Engineering Corporation</u> 1604 South 21st Street Colorado Springs, Colorado 80904-4208 (719) 630-7342</p>	<p>WOLF RANCH HYDROLOGIC MODEL SCHEMATIC COLORADO SPRINGS, COLORADO FIGURE G</p>	<p>PROJECT NO.: 03094 DATE: 02/17/04 DESIGN: RNW REVISIONS:</p>
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HEC-1 INPUT & OUTPUT
EXISTING DEVELOPMENT CONDITIONS

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1*****
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*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* U.S. ARMY CORPS OF ENGINEERS
* JUN 1998
* HYDROLOGIC ENGINEERING CENTER
* VERSION 4.1
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
* RUN DATE 25FEB04 TIME 18:18:07
* (916) 756-1104
*
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*****

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A-BASINS
EXISTING

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X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1
PAGE 1

HEC-1 INPUT

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1 ID Wolf Ranch Master Development Drainage Plan
2 ID A Basins, existing development condition PN

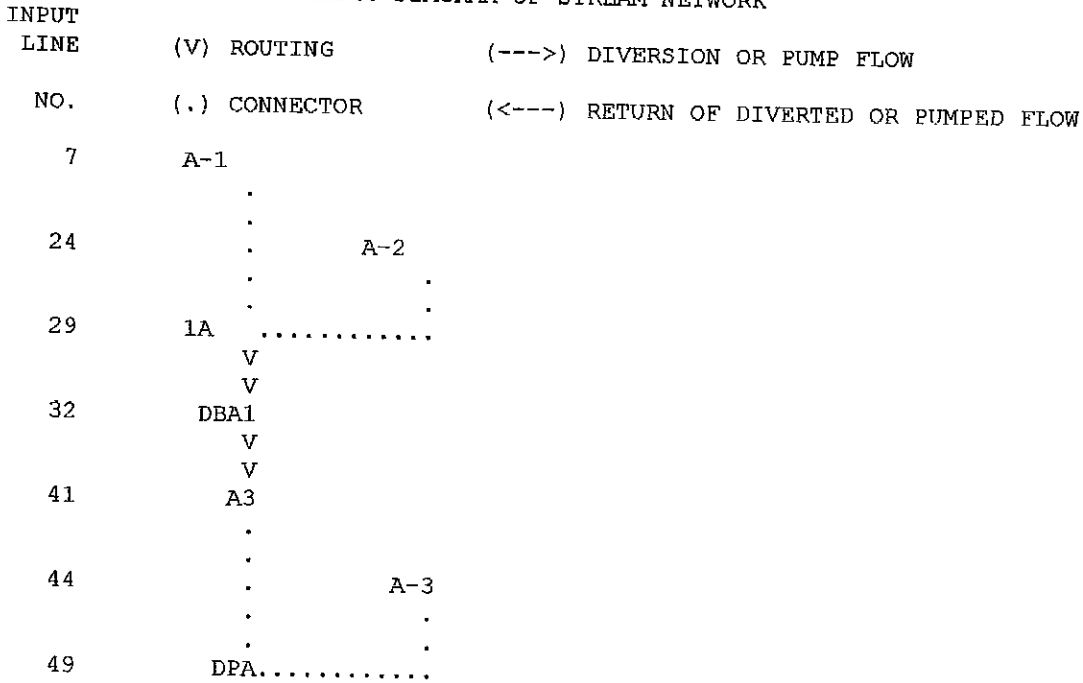
J3094

ABASINE.DAT	3	ID	5-year and 100 Year, 24 hr Type IIA Storm fn				
		*DIAGRAM					
	4	IT	5	0	0	300	
	5	IO	5	0			
	6	JR	PREC	.56	1.0		
	7	KK	A-1				
	8	KM	SCS RUNOFF FOR SUB-BASIN A-1				
	9	BA	.1819				
	10	IN	15				
	11	PB	4.4				
	12	PC	0.0000	0.0005	0.0015	0.0030	0.0045 0.0060 0.0080
0.0100	0.0120	0.0143					
	13	PC	0.0165	0.0188	0.0210	0.0233	0.0255 0.0278 0.0320
0.0390	0.0460	0.0530					
	14	PC	0.0600	0.0750	0.1000	0.4000	0.7000 0.7250 0.7500
0.7650	0.7800	0.7900					
	15	PC	0.8000	0.8100	0.8200	0.8250	0.8300 0.8350 0.8400
0.8450	0.8500	0.8550					
	16	PC	0.8600	0.8638	0.8675	0.8713	0.8750 0.8788 0.8825
0.8863	0.8900	0.8938					
	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115 0.9148 0.9180
0.9210	0.9240	0.9270					
	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400 0.9425 0.9450
0.9475	0.9500	0.9525					
	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650 0.9675 0.9700
0.9725	0.9750	0.9775					
	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850 0.9863 0.9875
0.9888	0.9900	0.9913					
	21	PC	0.9925	0.9938	0.9950	0.9963	0.9975 0.9988 1.0000
	22	LS	0	61			
	23	UD	0.36				
	24	KK	A-2				
	25	KM	RUNOFF FOR SUB-BASIN A-2				
	26	BA	.1098				
	27	LS	0	61			
	28	UD	.29				
	29	KK	1A				
	30	KM	DESIGN POINT 1A COMBINE RUNOFF FROM A-1 AND A-2				
	31	HC	2				
	32	KK	DBA1				
	33	KM	ROUTE DP 1A THROUGH EXISTING STOCK POND DBA1				
	34	RS	1	ELEV	7040		1
	35	SA	0.16	0.34	0.56	0.77	
	36	SE	7040	7041	7042	7043	
	37	SS	7041	60	0.49	1.5	
	38	ST	7041	60	0.49	1.5	
	39	SW	0	10	70	90	
	40	SE	7043	7041	7041	7043	
	41	KK	A3				
BASIN A-3	42	KM	ROUTE OUTFLOW FROM EXISTING STOCK POND DBA1 THROUGH SUB-				

LINE
 ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

44 KK A-3
 45 KM RUNOFF FOR SUB-BASIN A-3
 46 BA .1318
 47 LS 0 61
 48 UD 0.28
 49 KK DPA
 50 KM DESIGN POINT A COMBINE RUNOFF from A3 AND SUB-BASIN A-3
 51 HC 2
 52 ZZ

1
 SCHEMATIC DIAGRAM OF STREAM NETWORK



(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

1*****

 * *
 * *
 * FLOOD HYDROGRAPH PACKAGE (HEC-1) *
 * U.S. ARMY CORPS OF ENGINEERS *
 * JUN 1998 *
 * HYDROLOGIC ENGINEERING CENTER *
 * VERSION 4.1 *
 * 609 SECOND STREET *


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*
*      DAVIS, CALIFORNIA 95616      *
* RUN DATE 25FEB04 TIME 18:18:07 *
*      (916) 756-1104      *
*
*
*
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Wolf Ranch Master Development Drainage Plan
A Basins, existing development condition PN 03094
5-year and 100 Year, 24 hr Type IIA Storm fn

ABASINE.DAT

```

5 IO      OUTPUT CONTROL VARIABLES
          IPRNT      5 PRINT CONTROL
          IPLOT      0 PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMIN      5 MINUTES IN COMPUTATION INTERVAL
          IDATE     1 0 STARTING DATE
          ITIME     0000 STARTING TIME
          NQ        300 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE    2 0 ENDING DATE
          NDTIME    0055 ENDING TIME
          ICENT     19 CENTURY MARK

          COMPUTATION INTERVAL .08 HOURS
          TOTAL TIME BASE 24.92 HOURS

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ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME    ACRE-FEET
SURFACE AREA      ACRES
TEMPERATURE       DEGREES FAHRENHEIT

```

```

JP        MULTI-PLAN OPTION
          NPLAN      1 NUMBER OF PLANS

```

```

JR        MULTI-RATIO OPTION
          RATIOS OF PRECIPITATION
          .56      1.00

```

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO
ECONOMIC COMPUTATIONS

FLows IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
TIME TO PEAK IN HOURS

EIR CONDITIONS
B-BASINS

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
609 SECOND STREET *
*
DAVIS, CALIFORNIA 95616 *
* RUN DATE 16JAN04 TIME 15:41:35 *
(916) 756-1104 *
*
*****
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION.

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT
PAGE 1

```

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Wolf Ranch Master Development Drainage Plan
2 ID B basins existing development condition PN 03094
3 TD 5-year and 100 Year, 24 hr Type IIA Storm FN bbas-e.dat
*DIAGRAM
4 IT 5 0 0 300
5 IO 4 0
6 JR PREC .56 1.0
7 KK B-1
8 RA RUNOFF FOR 302-BASIN 01
9 BA .1505
10 IN 15
11 PB 4.4
12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120
0.0143
13 PC 0.0165 0.0188 0.0210 0.0233 0.0255 0.0278 0.0320 0.0390 0.0460
)

```

0.7900	14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800
0.8550	15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500
0.8938	16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900
0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240
0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500
0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750
0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900
	21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000		
	22	LS	0	61							
	23	UD	0.50								
	24	ZZ									

1 .

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT
 LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
 7 B-1

{***} RUNOFF ALSO COMPUTED AT THIS LOCATION

1*****

```

*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
* HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* RUN DATE 16JAN04 TIME 15:41:35 *
* (916) 756-1104 *
*
*

```


Wolf Ranch Master Development Drainage Plan
 B basins existing development condition PN 03094
 5-year and 100 Year, 24 hr Type IIA Storm EN bbas-e.dat

5 IO OUTPUT CONTROL VARIABLES
 IPKNT 4 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0 HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK
 COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 24.92 HOURS

PRECIPITATION OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT +	A-1	.18	1 FLOW TIME	7. 6.33	85. 6.25
HYDROGRAPH AT +	A-2	.11	1 FLOW TIME	5. 6.25	59. 6.17
2 COMBINED AT +	DPA1	.29	1 FLOW TIME	12. 6.33	142. 6.25
ROUTED TO +	DBA1	.29	1 FLOW TIME	8. 6.75	116. 6.33
				** PEAK STAGES IN FEET **	
				1 STAGE	7041.41 7043.50
				TIME	6.75 6.33
ROUTED TO +	A3	.29	1 FLOW TIME	8. 6.92	113. 6.42
HYDROGRAPH AT +	A-3	.13	1 FLOW TIME	6. 6.25	72. 6.17
2 COMBINED AT +	DPA	.42	1 FLOW TIME	11. 6.75	157. 6.42

1
STATION DBA1
BREACH FORMATION)

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING

PLAN 1	INITIAL VALUE	SPILLWAY CREST	TOP
OF DAM			
7041.00	ELEVATION 7040.00	7041.00	
0.	STORAGE 0.	0.	
0.	OUTFLOW 0.	0.	

TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS
6.75	.00	.56	7041.41	.41	0.	8.	18.58
6.33	.00	1.00	7043.50	2.50	2.	116.	19.00

*** NORMAL END OF HEC-1 ***

EXISTING CONDITIONS
C-BASINS

```

I*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
609 SECOND STREET *
*
DAVIS, CALIFORNIA 95616 *
* RUN DATE 16JAN04 TIME 15:41:52 *
(916) 756-1104 *
*
*****
*****

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X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

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NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT
PAGE 1

```

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Wolf Ranch Master Development Drainage Plan
2 ID C Basins existing development condition PN 03094
3 ID 5-year and 100 Year, 24 hr Type TTA Storm FN cbas-e.dat
*DIAGRAM
4 TF 5 2 2 300
5 IO 4 0
6 JR PREC .56 1.0
7 KK C-1
8 KM RUNOFF FOR SUBSYSTEM C)
9 BA .1508
10 IN 15
11 PB 4.4
12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120
0.0143
13 PC 0.0165 0.0188 0.0210 0.0233 0.0255 0.0278 0.0320 0.0390 0.0460
0.0530

```


0.7900	14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800
0.8550	15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500
0.8938	16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900
0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240
0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500
0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750
0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900
	21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000		
	22	LS	0	61							
	23	UD	0.46								
	24	KK	C3								
	25	RM	RUNOFF SUB-BASIN C-1 TO DPC								
	26	RD	37.00	0.032	0.04			TBAP	1.0	4	
	27	KK	C-2								
	28	RM	RUNOFF FOR SUB-BASIN C-2								
	29	BA	0.0991								
	30	LS	0	61							
	31	UD	0.43								
	32	KK	DPC								
	33	RM	COMBINE RUNOFF FROM C3 AND C-1								
	34	HC	2								
	35	ZZ									

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

```

  7      C-1
        V
        V
  24     C3
        .
        .
  27     .      C-2
        .
        .
  32     DPC.....
  
```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* U.S. ARMY CORPS OF ENGINEERS
* JUN 1998
* HYDROLOGIC ENGINEERING CENTER
* VERSION 4.1
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
* RUN DATE 16JAN04 TIME 15:41:52
* (916) 756-1104
*
*****
*****
  
```

Wolf Ranch Master Development Drainage Plan
 C Basins existing development condition PN 03094
 5-year and 100 Year, 24 hr Type IIA Storm FN cbas-e.dat

5 IO OUTPUT CONTROL VARIABLES
 IPRNT 4 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK

 COMPUTATION INTERVAL .08 HOURS
 TOTAL FLOW BASIN 24.22 ACRES

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRES-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION 3
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .56 1.00

*** **
 *** **

 * *
 7 KK * C-1 *
 * *

RUNOFF FOR SUBBASIN C1

10 IN TIME DATA FOR INPUT TIME SERIES
 JXMIN 15 TIME INTERVAL IN MINUTES
 JXDATE 1 0 STARTING DATE
 JXTIME 0 STARTING TIME

SUBBASIN RUNOFF DATA

9 BA SUBBASIN CHARACTERISTICS
 TAREA .15 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.40 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN
 .00 .00 .00 .00 .00 .00 .00 .00

.00 .00 .00 .00 .00 .00 .00 .00

22 LS SCS LOSS RATE
STRTL 1.28 INITIAL ABSTRACTION
CRVNBR 61.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

23 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .44 LAG

UNIT HYDROGRAPH
28 END-OF-PERIOD ORDINATES

66.	12.	37.	76.	122.	146.	150.	139.	120.	92.
4.	50.	38.	29.	22.	16.	12.	9.	7.	5.
	3.	2.	2.	1.	1.	1.	0.	0.	

*** **
*** **

* *
24 KK * D2 *
* *

ROUTE FLOW FROM SUB-BASIN D-1 TP DP D2

HYDROGRAPH ROUTING DATA

26 RD MUSKINGUM-CUNGE CHANNEL ROUTING
L 5470. CHANNEL LENGTH
S .0270 SLOPE
N .040 CHANNEL ROUGHNESS COEFFICIENT
CA .00 CONTRIBUTING AREA
SHAPE TRAP CHANNEL SHAPE
WD 10.00 BOTTOM WIDTH OR DIAMETER
Z 10.00 SIDE SLOPE

*** **
*** **

* *
27 KK * D-2 *
* *

RUNOFF FROM Sub-basin D-2

SUBBASIN RUNOFF DATA

29 BA SUBBASIN CHARACTERISTICS
TAREA .17 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.40 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00 .00 .00 .00 .00 .00 .00 .00 .00 .00

2. 39. 28. 20. 14. 10. 7. 5. 4. 3.
 2. 1. 1. 0.

*** **

 * *
 32 KK * DPD2 *
 * *

COMBINE RUNOFF from D-2 AND D2

34 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

 * *
 35 KK * D3 *
 * *

ROUTE FLOW FROM DP D2 TO DP D

HYDROGRAPH ROUTING DATA

37 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 3000. CHANNEL LENGTH
 S .0350 SLOPE
 N .040 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z 10.00 SIDE SLOPE

*** **

 * *
 38 KK * D-3 *
 * *

RUNOFF FROM Sub-basin D-3

SUBBASIN RUNOFF DATA

40 BA SUBBASIN CHARACTERISTICS
 TAREA .05 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.40 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

5.	54.	41.	32.	25.	19.	14.	11.	8.	6.
0.	4.	3.	2.	2.	1.	1.	1.	1.	0.

*** **

```

*****
*
24 KK *      C3 *
*
*****

```

ROUTE SUB-BASIN C-1 TO DP C

HYDROGRAPH ROUTING DATA

```

26 RD      MUSKINGUM-CUNGE CHANNEL ROUTING
           L      3700.  CHANNEL LENGTH
           S      .0320  SLOPE
           N      .040   CHANNEL ROUGHNESS COEFFICIENT
           CA     .00    CONTRIBUTING AREA
           SHAPE  TRAP   CHANNEL SHAPE
           WD     10.00  BOTTOM WIDTH OR DIAMETER
           Z      4.00  SIDE SLOPE

```

*** **

```

*****
*
27 KK *      C-2 *
*
*****

```

RUNOFF FOR SUB-BASIN C-2

SUBBASIN RUNOFF DATA

```

29 BA      SUBBASIN CHARACTERISTICS
           TAREA   .10  SUBBASIN AREA

```

PRECIPITATION DATA

```

11 PB      STORM      4.40  BASIN TOTAL PRECIPITATION
12 PI      INCREMENTAL PRECIPITATION PATTERN
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.10 .10 .00 .01 .01 .01 .01 .01 .10 .10
.00 .00 .10 .10 .01 .01 .01 .01 .01 .01

```


COMBINE RUNOFF from C3 AND C-1

34 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

1 ***

COMPUTATIONS PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	C-1	.15	1	FLOW	58.
				TIME	6.50
ROUTED TO					
+	C3	.15	1	FLOW	59.
				TIME	6.83
HYDROGRAPH AT					
+	C-2	.10	1	FLOW	41.
				TIME	6.50
2 COMBINED AT					
+	DPC	.25	1	FLOW	94.
				TIME	6.67

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

VOLUME	ISTAQ	ELEMENT	DT	PEAK	TIME TO	VOLUME	DT	INTERPOLATED TO	
								COMPUTATION INTERVAL	PEAK
(IN)			(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)
		FOR PLAN = 1	RATIO= .00						
.19		C3 MANE	2.00	5.79	406.00	.18	5.00	5.43	410.00

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1490E+01 EXCESS= .0000E+00 OUTFLOW= .1481E+01 BASIN STORAGE=
 .1603E-01 PERCENT ERROR= -.5

		FOR PLAN = 1	RATIO= .00						
1.02		C3 MANE	2.50	58.59	390.00	1.02	5.00	58.59	390.00

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8231E+01 EXCESS= .0000E+00 OUTFLOW= .8223E+01 BASIN STORAGE=
 .2816E-01 PERCENT ERROR= -.2

*** NORMAL END OF HEC-1 ***

*East
D Basins
2-1009R*

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
* CALIFORNIA 95616 *
* RUN DATE 11MAR04 TIME 12:41:53 *
(916) 756-1104 *
*
*****
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1
PAGE 1

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Wolf Ranch Master Development Drainage Plan									
2	ID	D Basins existing development conditions PN 03094									
3	ID	5-year and 100 Year, 24 hr Type IIA Storm FN dbas-e.dat									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	4	0								
6	JR	PREC	.48	.61	.70	.93	1.0				
7	KK	D-1									
8	KM	RUNOFF FOR Sub-basin D-1									
9	BA	.1503									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143
13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270

18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	61								
23	UD	0.44									
24	KK	D2									
25	KM	ROUTE FLOW FROM SUB-BASIN D-1 TP DP D2									
26	RD	5470	0.027	0.04		TRAP		10			
27	KK	D-2									
28	KM	RUNOFF FROM Sub-basin D-2									
29	BA	.1660									
30	LS	0	61								
31	UD	0.37									
32	KK	DPD2									
33	KM	COMBINE RUNOFF from D-2 AND D2									
34	HC	2									
35	KK	D3									
36	KM	ROUTE FLOW FROM DP D2 TO DP D									
37	RD	3000	0.035	0.04		TRAP		10		10	
38	KK	D-3									
39	KM	RUNOFF FROM Sub-basin D-3									
40	BA	.0450									
41	LS	0	61								
42	UD	0.12									

1 HEC-1 INPUT

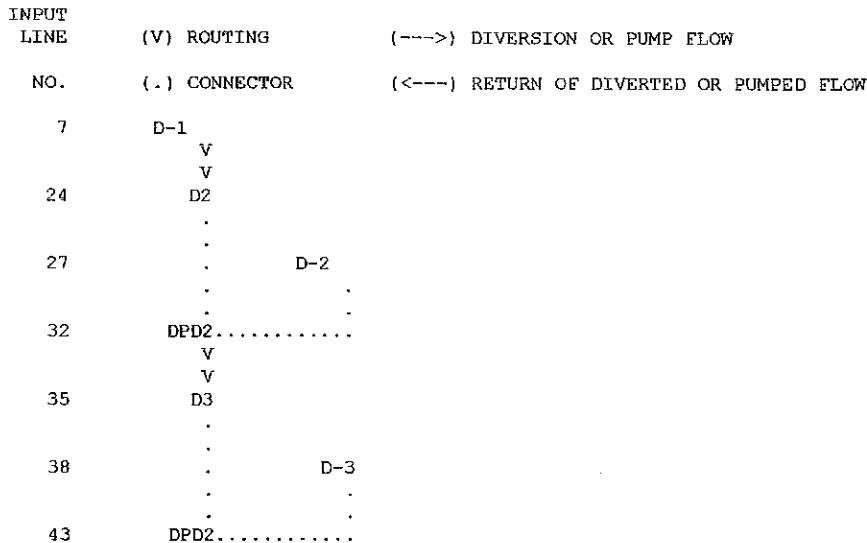
PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43	KK	DPD2									
44	KM	COMBINE RUNOFF from D-3 AND D3									
45	HC	2									
46	ZZ										

1

SCHEMATIC DIAGRAM OF STREAM NETWORK



(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

1*****

```

*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
CORPUS OF ENGINEERS
* JUN 1998
ENGINEERING CENTER
* VERSION 4.1
SECOND STREET
*
CALIFORNIA 95616
* RUN DATE 11MAR04 TIME 12:41:53
(916) 756-1104
*
*****
*****

```

Wolf Ranch Master Development Drainage Plan
 D Basins existing development conditions PN 03094
 5-year and 100 Year, 24 hr Type IIA Storm FN dbas-e.dat

```

5 IO      OUTPUT CONTROL VARIABLES
          IPRNT      4  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMN        5  MINUTES IN COMPUTATION INTERVAL
          IDATE      1  0  STARTING DATE
          ITIME      0000 STARTING TIME
          NQ         300 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE     2  0  ENDING DATE
          NDTIME     0055 ENDING TIME
          ICENT      19  CENTURY MARK

          COMPUTATION INTERVAL .08 HOURS
          TOTAL TIME BASE     24.92 HOURS

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME    ACRE-FEET
SURFACE AREA      ACRES
TEMPERATURE       DEGREES FAHRENHEIT

JP        MULTI-PLAN OPTION
          MPLAN      1  NUMBER OF PLANS

JR        MULTI-RATIO OPTION
          RATIOS OF PRECIPITATION
          .48      .61      .70      .93      1.00

```

*** **

```

*****
*
7 KK    *   D-1  *
*
*****

```

RUNOFF FOR Sub-basin D-1

*** **

43 KK
 * DPD2 *

COMBINE RUNOFF from D-3 AND D3

45 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION					
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	
				.48	.61	.70	.93	1.00	
HYDROGRAPH AT									
+	D-1	.15	1	FLOW TIME	2. 6.58	9. 6.42	18. 6.42	49. 6.33	60. 6.33
ROUTED TO									
+	D2	.15	1	FLOW TIME	2. 7.33	9. 7.00	20. 6.67	49. 6.67	59. 6.67
HYDROGRAPH AT									
+	D-2	.17	1	FLOW TIME	2. 6.50	11. 6.33	22. 6.33	61. 6.25	75. 6.25
2 COMBINED AT									
+	DPD2	.32	1	FLOW TIME	4. 7.33	14. 6.92	33. 6.67	84. 6.50	103. 6.50
ROUTED TO									
+	D3	.32	1	FLOW TIME	3. 7.67	15. 7.17	31. 6.92	88. 6.67	103. 6.67
HYDROGRAPH AT									
+	D-3	.05	1	FLOW TIME	1. 6.08	6. 6.08	12. 6.08	30. 6.08	36. 6.08
2 COMBINED AT									
+	DPD2	.36	1	FLOW TIME	4. 7.67	16. 7.17	32. 6.92	92. 6.67	107. 6.67

*** NORMAL END OF HEC-1 ***

Ex Condition
E Basins
2 -> 100yr

```

1*****
*****
*
*
*   FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
*   JUN 1998 *
ENGINEERING CENTER *
*   VERSION 4.1 *
SECOND STREET *
*
CALIFORNIA 95616 *
*   RUN DATE 11MAR04 TIME 12:43:42 *
(916) 756-1104 *
*
*****
*****

```

```

*
*   U.S. ARMY
*   HYDROLOGIC
*   609
*   DAVIS,

```

```

X   X   XXXXXXXX   XXXXX   X
X   X   X           X   X   XX
X   X   X           X           X
XXXXXXXX   XXXX   X           XXXXX   X
X   X   X           X           X
X   X   X           X   X           X
X   X   XXXXXXXX   XXXXX   XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1
PAGE 1

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Wolf Ranch master Development Drainage Plan									
2	ID	E Basins existing development condition PN 03094									
3	ID	5-year and 100 Year, 24 hr Type IIA Storm FN ebas-e.dat									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	4	0								
6	JR	PREC	.48	.61	.70	.93	1.0				
7	KK	E-1									
8	KM	RUNOFF FOR SUB-BASIN E-1									
9	BA	.1640									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143
13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270

18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	61								
23	UD	0.44									
24	KK	E2									
25	KM	ROUTE FLOW FROM SUB-BASIN E-1 TO DP E									
26	RD	3050	.035	0.04		TRAP	10	5			
27	KK	E-2									
28	KM	RUNOFF FOR SUB-BASIN E-2									
29	BA	.1520									
30	LS	0	61								
31	UD	0.44									
32	KK	DPE									
33	KM	COMBINE RUNOFF FROM E2 AND E-2									
34	HC	2									
35	ZZ										

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE      (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.       (.) CONNECTOR  (<---) RETURN OF DIVERTED OR PUMPED FLOW

  7      E-1
         V
         V
  24      E2
         .
         .
  27      .      E-2
         .
         .
  32      DPE.....

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
CORPS OF ENGINEERS
* JUN 1998
ENGINEERING CENTER
* VERSION 4.1
SECOND STREET
*
CALIFORNIA 95616
* RUN DATE 11MAR04 TIME 12:43:42
(916) 756-1104
*
*****

```

```

*
* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,
*

```

Wolf Ranch master Development Drainage Plan
E Basins existing development condition PN 03094
5-year and 100 Year, 24 hr Type IIA Storm FN ebas-e.dat

5 IO OUTPUT CONTROL VARIABLES

IPRNT	4	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK

 COMPUTATION INTERVAL .09 HOURS
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .48 .61 .70 .93 1.00

*** **

 * *
 7 KK * E-1 *
 * *

RUNOFF FOR SUB-BASIN E-1

10 IN TIME DATA FOR INPUT TIME SERIES
 JXMIN 15 TIME INTERVAL IN MINUTES
 JXDATE 1 0 STARTING DATE
 JXTIME 0 STARTING TIME

SUBBASIN RUNOFF DATA

9 BA SUBBASIN CHARACTERISTICS
 TAREA .16 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.40 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.10	.00	.01	.01	.01	.01	.01	.10	.10	.10

OPERATION	STATION	AREA	PLAN		RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5
					.48	.61	.70	.93	1.00
HYDROGRAPH AT									
+	E-1	.16	1	FLOW	2.	10.	19.	53.	66.
				TIME	6.58	6.42	6.42	6.33	6.33
ROUTED TO									
+	E2	.16	1	FLOW	2.	10.	19.	53.	66.
				TIME	6.92	6.67	6.58	6.50	6.50
HYDROGRAPH AT									
+	E-2	.15	1	FLOW	2.	9.	18.	49.	61.
				TIME	6.58	6.42	6.42	6.33	6.33
2 COMBINED AT									
+	DPE	.32	1	FLOW	3.	18.	35.	99.	124.
				TIME	6.92	6.58	6.50	6.42	6.42

1
 *** NORMAL END OF HEC-1 ***

EX-Conditions
 "F" Basins

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
609 SECOND STREET *
*
DAVIS, CALIFORNIA 95616 *
* RUN DATE 16JAN04 TIME 17:45:26 *
(916) 756-1104 *
*
*****
*****
  
```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 PAGE 1 HEC-1 INPUT

```

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Wolf Ranch Master Development Drainage Plan
2 ID F Basins Existing Development Condition PN 03094
3 ID 5-year and 100 Year, 24 hr Type IIA Storm FN fbas-e.dat
*DIAGRAM
4 IT 5 0 0 300
5 IO 4 0
6 JR PREC .56 1.0
7 KK F-1
8 KM RUNOFF SUB-BASIN F-1
9 BA .1659
10 IN 1t
11 EP 4.4'
0.0143 12 EC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120
5
0.0530 13 EC 0.0165 0.0188 0.0210 0.0233 0.0255 0.0278 0.0320 0.0390 0.0460
  
```

0.7900	14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800
0.8550	15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500
0.8938	16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900
0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240
0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500
0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750
0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900
	21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000		
	22	LS									
	23	UD	0.20								
	24	KK	1-8								
	25	KM	ROUTE FLOW FROM F-1 THROUGH F-8								
	26	RD	4620	0.04	0.04		TRAP	6		3	
	27	KK	F-8								
	28	KM	SCS RUNOFF F-8								
	29	BA	.1499								
	30	LS	0	61							
	31	UD	.22								
	32	KK	1F								
	33	KM	COMBINE RUNOFF FROM F-1 AND F-8								
	34	HC	2								
	35	KK	F-2								
	36	KM	SCS RUNOFF F-2								
	37	BA	.0424								
	38	LS	0	61							
	39	UD	.19								
	40	KK	F-3								
	41	KM	SCS RUNOFF F-3								
	42	BA	.0942								
	43	LS	0	61							
	44	UD	.22								

1
PAGE 2

HEC-1 INPUT

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

45	KK	2F									
46	KM	COMBINE RUNOFF FROM F-2 AND F-3									
47	HC	2									
48	KK	2F-5F									
49	KM	ROUTE FLOW FROM 2F THROUGH F-9									
50	RD	3087	0.036	0.04		TRAP	6			3	
51	KK	F-9									
52	KM	SCS RUNOFF F-9									
53	BA	.1953									
54	LS	0	61								
55	UD	.27									
56	KK	5F									
57	KM	COMBINE RUNOFF FROM 2F AND F-9									
58	HC	2									
59	KK	POND1									
60	KM	ROUTE FLOW THROUGH POND1									
61	RS	1	ELEV	7133						1	

62	SA	0.41	0.58	0.76	0.86				
63	SE	7133	7134	7135	7136				
64	ST	7133	10	0.50	1.5				
65	SS	7133	10	0.50	1.5				
66	SW	0	50	60	70	125			
67	SE	7136	7135	7133	7133	7136			
68	KK	F-4							
69	KM	SCS RUNOFF F-4							
70	BA	.2681							
71	LS	0	61						
72	UD	.28							
73	KK	F-5							
74	KM	SCS RUNOFF F-5							
75	BA	.1073							
76	LS	0	61						
77	UD	.24							
78	KK	3F							
79	KM	COMBINE RUNOFF FROM F-4 AND F-5							
80	HC	2							
81	KK	3F-6F							
82	KM	ROUTE FLOW FROM 3F THROUGH F-10							
83	RD	3790	0.034	0.04		TRAP	10	10	
84	KK	F-10							
85	KM	SCS RUNOFF F-10							
86	BA	.0883							
87	LS	0	61						
88	UD	.28							

1
PAGE 3

HEC-1 INPUT

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

89	KK	6F							
90	KM	COMBINE RUNOFF FROM 3F AND F-10							
91	HC	2							
92	KK	8F							
93	KM	COMBINE RUNOFF FROM 5F AND 6F							
94	HC	2							
95	KK	8F-9F							
96	KM	ROUTE FLOW FROM 8F TO 9F							
97	RD	1706	0.034	0.04		TRAP	6	2	
98	KK	F9							
99	KM	COMBINE RUNOFF FROM 1F AND 9F							
100	HC	2							
101	KK	F12							
102	KM	ROUTE FLOW FROM 8F 9F TO 8F F12							
103	RC	.04	0.035	0.04	5200	0.022			
104	RX	0	20	33	37	43	47	60	80
105	RY	7014	7004	7004	7000	7000	7004	7004	7014
106	KK	F-6							
107	KM	SCS RUNOFF F-6							
108	BA	.0310							
109	LS	0	61						
110	UD	.19							
111	KK	F-7							
112	KM	SCS RUNOFF F-7							
113	BA	.0782							
114	LS	0	61						

115 UD .19
 116 KK 4F
 117 KM COMBINE RUNOFF FROM F-6 AND F-7
 118 HC 2
 119 KK 4F-7F
 120 KM ROUTE FLOW FROM 4F THROUGH F-11
 121 RD 3610 0.06 0.04 TRAP 10 10
 122 KK F-11
 123 KM SCS RUNOFF F-11
 124 BA .1136
 125 LS 0 61
 126 UD .16
 127 KK 7F
 128 KM COMBINE RUNOFF FROM 4F AND F-11
 129 HC 2

1
 PAGE 4

HEC-1 INPUT

LINE
 ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

130 KK 7F-10F
 131 KM ROUTE FLOW FROM 7F THROUGH F-14
 132 RD 4970 0.023 0.04 TRAP 6 3
 133 KK F-14
 134 KM SCS RUNOFF F-14
 135 BA .1493
 136 LS 0 61
 137 UD .30
 138 KK F-13 1
 139 KM RUNOFF SUB-BASIN F-13
 140 BA .1169
 141 LS 0 61
 142 UD .44
 143 KK F14
 144 KM COMBINE RUNOFF FROM 7F, F-13, AND F-14
 145 HC 3
 146 KK DBF13
 147 KM ROUTE FLOW FROM DP F14 THROUGH POND DBF13
 148 RS 1 ELEV 7026 1
 149 SA 1.97 2.35 2.83 3.21 3.66 4.0 4.33
 150 SE 7026 7027 7028 7029 7030 7031 7032
 151 ST 7029 40 0.50 1.5
 152 SS 7029 40 0.50 1.5
 153 SW 0 0 1.20 1.50
 154 SE 7032 7029 7029 7032
 155 KK F15
 156 KM ROUTE FLOW FROM POND DB F13 TO DP F15
 157 RS 1 STOR -1
 158 RC .04 0.035 0.04 1194 0.5
 159 RX 0 20 33 37 43 47 60 80
 160 RY 7014 7004 7004 7000 7000 7004 7004 7014
 161 KK F-15
 162 KM RUNOFF SUB-BASIN F-15
 163 BA .0321
 164 LS 0 61
 165 UD .11
 166 KK DPF15
 167 KM COMBINE RUNOFF FROM F15 AND SUB-BASIN F-15

168	HC	2	
169	KK	F-12	
170	KM	SCS RUNOFF F-12	
171	BA	.2471	
172	LS	0	61
173	UD	.33	

1
PAGE 5

HEC-1 INPUT

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

174	KK	F12							
175	KM	COMBINE RUNOFF FROM F12, DP F12 AND F-12							
176	HC	3							
177	KK	F16							
178	KM	ROUTE FLOW FROM DP F12 TO DP F16							
179	BC	.04 0.035 0.04 2091 0.02							
180	RX	0 20 33 37 43							
181	RY	7014 7004 7004 7000 7000 7004 60 80							
182	KK	F-16							
183	KM	RUNOFF SUB-BASIN F-16							
184	BA	.0570							
185	LS	0 61							
186	UD	.09							
187	KK	DPF16 1							
188	KM	COMBINE RUNOFF FROM F16 AND F-16							
189	HC	2							
190	KK	F17							
191	KM	ROUTE FLOW FROM DP F16 TO DP F17							
192	RD	1950 0.025 0.04 TRAP 20 3							
193	KK	F-17							
194	KM	RUNOFF SUB-BASIN F-17							
195	BA	.0520							
196	LS	0 61							
197	UD	.37							
198	KK	DPF							
199	KM	COMBINE RUNOFF FROM F17 AND SUB-BASIN F-17							
200	HC	2							
201	ZZ								

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
7	F-1	
	V	
	V	
24	1-8	
	.	
27	.	F-8
	.	.
	.	.
32	1F.....	
	.	
	.	
35	.	F-2
	.	.
	.	.
40	.	E-3

45
	.	2F.....	.	.
	.	√	.	.
	.	V	.	.
48	.	2F-5F	.	.

51	.	.	F-9	.

56	.	5F.....	.	.
	.	√	.	.
	.	V	.	.
59	.	POND1	.	.

68	.	.	F-4	.

73	.	.	.	F-5

78	.	.	3F.....	.
	.	.	√	.
	.	.	V	.
81	.	.	3F-6F	.

84	.	.	.	F-10

89	.	.	6F.....	.

92	.	8F.....	.	.
	.	√	.	.
	.	V	.	.
95	.	8F-9F	.	.

98	.	F9.....	.	.
	.	V	.	.
	.	V	.	.
101	.	E12	.	.

106	.	F-6	.	.

111	.	.	F-7	.

116	.	4F.....	.	.
	.	√	.	.
	.	V	.	.
119	.	4F-7F	.	.

122	.	.	F-11	.

127	.	7F.....	.	.
	.	√	.	.
	.	V	.	.
130	.	7F-10F	.	.

133	.	.	F-14	.


```

138      .           .           .           F-13
      .           .           .           .
143      .           F14.....
      .           V
      .           V
146      .           DBF13
      .           V
      .           V
155      .           F15
      .           .
      .           .
161      .           .           F-15
      .           .           .
166      .           DPF15.....
      .           .
      .           .
169      .           .           F-12
      .           .           .
      .           .           .
174      F12.....
      .           V
      .           V
177      F16
      .           .
      .           .
182      .           F-16
      .           .
      .           .
187      DPF16.....
      .           V
      .           V
190      F17
      .           .
      .           .
193      .           F-17
      .           .
      .           .
198      DPF.....

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	F-1	.17	1	FLOW TIME	10. 6.17 110. 6.08
ROUTED TO					
+	1-8	.17	1	FLOW TIME	9. 6.42 110. 6.25
HYDROGRAPH AT					
+	F-8	.15	1	FLOW TIME	9. 6.17 93. 6.17
2 COMBINED AT					
+	1F	.32	1	FLOW TIME	14. 6.42 186. 6.17
HYDROGRAPH AT					

+	F-2	.04	1	FLOW TIME	3. 6.17	29. 6.08
	HYDROGRAPH AT					
+	F-3	.09	1	FLOW TIME	5. 6.17	59. 6.17
	2 COMBINED AT					
+	2F	.14	1	FLOW TIME	8. 6.17	87. 6.08
	ROUTED TO					
+	2F-5F	.14	1	FLOW TIME	9. 6.33	85. 6.25
	HYDROGRAPH AT					
+	E-9	.20	1	FLOW TIME	10. 6.25	111. 6.17
	2 COMBINED AT					
+	5F	.33	1	FLOW TIME	18. 6.33	192. 6.17
	ROUTED TO					
+	POND1	.33	1	FLOW TIME	18. 6.33	192. 6.17
	** PEAK STAGES IN FEET **					
	1			STAGE TIME	7134.09 7.17	7136.25 6.17
	HYDROGRAPH AT					
+	F-4	.27	1	FLOW TIME	13. 6.25	147. 6.17
	HYDROGRAPH AT					
+	F-5	.11	1	FLOW TIME	5. 6.33	52. 6.25
	2 COMBINED AT					
+	3F	.38	1	FLOW TIME	17. 6.25	196. 6.17
	ROUTED TO					
+	3F-6F	.38	1	FLOW TIME	18. 6.42	196. 6.33
	HYDROGRAPH AT					
+	E-10	.09	1	FLOW TIME	4. 6.25	49. 6.17
	2 COMBINED AT					
+	6F	.46	1	FLOW TIME	22. 6.42	235. 6.33
	2 COMBINED AT					
+	8F	.80	1	FLOW TIME	37. 6.42	407. 6.25
	ROUTED TO					
+	8F-9F	.80	1	FLOW TIME	36. 6.50	398. 6.33
	2 COMBINED AT					
+	F9	1.11	1	FLOW TIME	49. 6.50	570. 6.25
	ROUTED TO					
+	F12	1.11	1	FLOW TIME	48. 6.75	566. 6.42

HYDROGRAPH AT						
+	F-6	.03	1	FLOW TIME	2. 6.17	21. 6.08
HYDROGRAPH AT						
+	F-7	.08	1	FLOW TIME	5. 6.17	54. 6.08
2 COMBINED AT						
+	4F	.11	1	FLOW TIME	7. 6.17	75. 6.08
ROUTED TO						
+	4F-7F	.11	1	FLOW TIME	6. 6.50	74. 6.25
HYDROGRAPH AT						
+	F-11	.11	1	FLOW TIME	8. 6.08	86. 6.08
2 COMBINED AT						
+	7F	.22	1	FLOW TIME	10. 6.42	133. 6.17
ROUTED TO						
+	7F-10F	.22	1	FLOW TIME	11. 6.50	130. 6.33
HYDROGRAPH AT						
+	F-14	.15	1	FLOW TIME	7. 6.25	77. 6.17
HYDROGRAPH AT						
+	F-13	.12	1	FLOW TIME	4. 6.50	47. 6.33
3 COMBINED AT						
+	F14	.49	1	FLOW TIME	20. 6.50	244. 6.33
ROUTED TO						
+	DBF13	.49	1	FLOW TIME	0. .00	29. 7.67
** PEAK STAGES IN FEET **						
1. STAGE . 7027.97 7030.28						
TIME 24.92 7.67						
ROUTED TO						
+	F15	.49	1	FLOW TIME	0. .00	29. 7.75
** PEAK STAGES IN FEET **						
1. STAGE 7000.00 7000.20						
TIME .00 7.67						
HYDROGRAPH AT						
+	F-15	.03	1	FLOW TIME	3. 6.08	27. 6.00
2 COMBINED AT						
+	DBF15	.52	1	FLOW TIME	3. 6.08	31. 7.75
HYDROGRAPH AT						
+	F-12	.25	1	FLOW TIME	11. 6.33	123. 6.25
3 COMBINED AT						
+	F12	1.88	1	FLOW TIME	55. 6.75	664. 6.42

ROUTED TO
 + F16 1.88 1 FLOW 48. 643.
 TIME 6.83 6.42

** PEAK STAGES IN FEET **
 1 STAGE 7001.13 7004.59
 TIME 6.83 6.42

HYDROGRAPH AT
 + F-16 .06 1 FLOW 5. 53.
 TIME 6.08 6.00

2 COMBINED AT
 + DPF16 1.94 1 FLOW 49. 650.
 TIME 6.83 6.42

ROUTED TO
 + F17 1.94 1 FLOW 48. 644.
 TIME 7.00 6.50

HYDROGRAPH AT
 + F-17 .05 1 FLOW 2. 24.
 TIME 6.42 6.25

2 COMBINED AT
 + DPF 1.99 1 FLOW 49. 661.
 TIME 7.00 6.50

1
 1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION POND1
 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	STORAGE	7133.00	7133.00	7133.00
	OUTFLOW	0.	0.	0.

TIME OF FAILURE HOURS	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
.00	.56	7134.09	1.09	1.	6.	19.08	7.17
.00	1.00	7136.25	3.25	2.	29.	19.25	6.17

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DBF13
 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	STORAGE	7026.00	7026.00	7026.00
	OUTFLOW	0.	0.	0.

TIME OF FAILURE HOURS	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
.00	.56	7027.97	.00	5.	0.	.00	.00

.00	1.00	7030.28	1.28	12.	29.	18.42	7.67
-----	------	---------	------	-----	-----	-------	------

*** NORMAL END OF HEC-1 ***

G-BASINS
Existing Condition

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1*****
*****
*
*
*   FLOOD HYDROGRAPH PACKAGE (HEC-1) *
U.S. ARMY CORPS OF ENGINEERS *
*   JUN 1998 *
HYDROLOGIC ENGINEERING CENTER *
*   VERSION 4.1 *
609 SECOND STREET *
*
DAVIS, CALIFORNIA 95616 *
*   RUN DATE 19JAN04 TIME 09:36:27 *
(916) 756-1104 *
*
*****
*****

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```

X   X XXXXXXX XXXXX   X
X   X X   X   X   XX
X   X X   X   X   X
XXXXXXX XXXX   X   XXXXX X
X   X X   X   X   X
X   X X   X   X   X
X   X XXXXXXX XXXXX   XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT
PAGE 1

```

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1          ID          Wolf Ranch Master Development Drainage Plan
2          ID          G Basins Existing development conditions PN 03094
3          ID          5-year and 100 Year, 24 hr Type TIA Storm FN Gbas-e.dat
          *DIAGRAM
4          IT          5          0          0          300
5          IO          4          0
6          JR          PREC          .56          1.0
7          KK          G-1
8          KM          RUNOFF -- Sub-basin G-1
9          BA          .0808
10         IN          15
11         PB          4.4
0.0143    12         PC          0.0000  0.0005  0.0015  0.0030  0.0045  0.0060  0.0080  0.0100  0.0120
0.0530    13         PC          0.0165  0.0188  0.0210  0.0233  0.0255  0.0278  0.0320  0.0390  0.0460

```

0.7900	14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800
0.8550	15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500
0.8938	16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900
0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240
0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500
0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750
0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900
	21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000		
	22	LS	0	61							
	23	UD	0.22								
	24	KK	G2								
	25	KM	ROUTE FLOW from SUB-BASIN G-1 TO DP G2								
	26	RD	3700	0.028	0.04		TRAP	10	10		
	27	KK	G-2								
	28	KM	RUNOFF - Sub-basin G-2								
	29	BA	.171								
	30	LS	0	61							
	31	UD	0.31								
	32	KK	DPG2								
	33	KM	COMBINE RUNOFF from G2 AND SUB-BASIN G-2								
	34	HC	2								
	35	KK	G3								
	36	KM	ROUTE FLOW from DP G2 TO DP G								
	37	RD	1850	0.028	0.04		TRAP	10	10		
	38	KK	G-3								
	39	KM	RUNOFF - Sub-basin G-3								
	40	BA	.068								
	41	LS	0	61							
	42	UD	0.44								

1
PAGE 2

HEC-1 INPUT

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43	KK	DPG									
44	KM	COMBINE RUNOFF from G3 AND SUB-BASIN G-3									
45	HC	2									
46	ZZ										

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

```

7      G-1
      V
      V
24     G2
      .
      .
27     .      G-2
      .
      .
32     DPG2.....
      V
      V

```

```

35      G3
      .
38      .      G-3
      .
43      DPG.....

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION


```

*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
609 SECOND STREET *
*
DAVIS, CALIFORNIA 95616 *
* RUN DATE 19JAN04 TIME 09:36:27 *
(916) 756-1104 *
*
*

```


Wolf Ranch Master Development Drainage Plan
G Basins Existing development conditions PN 03094
5-year and 100 Year, 24 hr Type IIA Storm FN Gbas-e.dat

```

5 IO      OUTPUT CONTROL VARIABLES
          IPRNT      4 PRINT CONTROL
          IPLOT      0 PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMIN      5 MINUTES IN COMPUTATION INTERVAL
          IDATE      1 0 STARTING DATE
          ITIME      0000 STARTING TIME
          NQ         300 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE     2 0 ENDING DATE
          NDTIME     0055 ENDING TIME
          ICENT      19 CENTURY MARK

          COMPUTATION INTERVAL .08 HOURS
          TOTAL TIME BASE 24.92 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME     KCFT-Feet
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

```

JP        MULTI-PLAN OPTION
          NPLAN      1 NUMBER OF PLANS

```

```

JR        MULTI-RATIO OPTION
          RATIOS OF PRECIPITATION
          .56      1.00

```


28 UD

SCS DIMENSIONLESS UNITGRAPH
TLAG .47 LAG

	UNIT HYDROGRAPH 30 END-OF-PERIOD ORDINATES									
47.	7.	19.	40.	65.	83.	88.	85.	75.	63.	
3.	35.	27.	21.	16.	12.	9.	7.	5.	4.	
0.	2.	2.	1.	1.	1.	1.	1.	0.	0.	
1										

COMPUTATIONS PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	H-1	.04	1	FLOW	5.
				TIME	41.
					6.00
					6.00
HYDROGRAPH AT					
+	H-2	.09	1	FLOW	3.
				TIME	36.
					6.50
					6.42

*** NORMAL END OF HEC-1 ***

31 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .31 LAG

UNIT HYDROGRAPH
21 END-OF-PERIOD ORDINATES

37.	31.	101.	196.	234.	221.	178.	118.	78.	54.
1.	25.	17.	12.	8.	5.	4.	3.	2.	1.
	0.								

*** **
*** **

* *
32 KK * DPG2 *
* *

COMBINE RUNOFF from G2 AND SUB-BASIN G-2

34 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **
*** **

* *
35 KK * G3 *
* *

ROUTE FLOW from DP G2 TOA DP G

HYDROGRAPH ROUTING DATA

37 RD MUSKINGUM-CUNGE CHANNEL ROUTING

L	1850.	CHANNEL LENGTH
S	.0280	SLOPE
N	.040	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	10.00	BOTTOM WIDTH OR DIAMETER
Z	10.00	SIDE SLOPE

*** **
*** **

* *
38 KK * G-3 *
* *

RUNOFF - Sub-basin G-3

SUBBASIN RUNOFF DATA

42 UD SCS DIMENSIONLESS UNITGRAPH

		UNIT HYDROGRAPH							
		28 END-OF-PERIOD ORDINATES							
30.	6.	17.	35.	55.	66.	68.	63.	54.	42.
2.	22.	17.	13.	10.	7.	6.	4.	3.	2.
	1.	1.	1.	1.	0.	0.	0.	0.	

*** **

43 KK *****
 * *
 * DPG *
 * *

COMBINE RUNOFF from G3 AND SUB-BASIN G-3

45 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

1

COMPUTATIONS PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	G-1	.08	1	FLOW TIME	5. 6.17
ROUTED TO					
+	G2	.08	1	FLOW TIME	6. 6.58
HYDROGRAPH AT					
+	G-2	.17	1	FLOW TIME	8. 6.33
2 COMBINED AT					
+	DPG2	.25	1	FLOW TIME	11. 6.58
ROUTED TO					
+	G3	.25	1	FLOW TIME	11. 6.75
HYDROGRAPH AT					
+	G-3	.07	1	FLOW TIME	2. 6.50
2 COMBINED AT					
+	DPG	.32	1	FLOW TIME	13. 6.75

*** NORMAL END OF HEC-1 ***

*H-Basins
Existing Conditions*

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
609 SECOND STREET *
*
DAVIS, CALIFORNIA 95616 *
* RUN DATE 19JAN04 TIME 10:16:18 *
(916) 756-1104 *
*
*****
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X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

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NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT
PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Wolf Ranch master Development Drainage Plan									
2	ID	H Basins Existing Development Conditions PN 03094									
3	ID	5-year and 100 Year, 24 hr Type IIA Storm FN hbas-e.dat									
	*DIAGRAM										
4	IT	5	0	0	000						
5	IO	4	0								
6	JR	PREC	.56	1.0							
7	KK	H-1									
8	KA	RUNOFF FROM SUB-BASIN 'A-1									
9	BA	.0370									
10	IN	15									
11	FB	4.4									
0.0143	12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120
0.0530	13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460

0.7900	14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800
0.8550	15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500
0.8938	16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900
0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240
0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500
0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750
0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900
	21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000		
	22	LS	0	61							
	23	UD	0.05								
	24	KK	H-2								
	25	RM									
	26	EA	.0931								
	27	LS	0	61							
	28	UD	.47								
	29	BB									

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
 7 H-1
 .
 .
 24 . H-2

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
609 SECOND STREET *
*
DAVIS, CALIFORNIA 95616 *
* RUN DATE 19JAN04 TIME 10:16:18 *
(916) 756-1104 *
*
*****
*****

```

Wolf Ranch master Development Drainage Plan
 H Basins Existing Development Conditions PN 03094
 5-year and 100 Year, 24 hr Type IIA Storm FN hbas-e.dat

5 IO OUTPUT CONTROL VARIABLES
 IPRNT 4 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL

IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-Feet
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .56 1.00

*** **
 *** **

 * *
 7 KK * H-1 *
 * *

RUNOFF FROM SUB-BASIN H-1

10 IN TIME DATA FOR INPUT TIME SERIES
 JXMIN 15 TIME INTERVAL IN MINUTES
 JXDATE 1 0 STARTING DATE
 JXTIME 0 STARTING TIME

SUBBASIN RUNOFF DATA

9 BA SUBBASIN CHARACTERISTICS
 AREA .04 SUBBASIN AREA

PRECIPITATION DATA

11 PB STORM 4.40 BASIN TOTAL PRECIPITATION

12 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.10	.10	.00	.01	.01	.01	.01	.01	.01	.10
.00	.00	.10	.10	.01	.01	.01	.01	.01	.01

**HEC-1 INPUT & OUTPUT
DEVELOPED CONDITIONS**

A-BASINS DEVELOPED

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
*
CALIFORNIA 95616 *
* RUN DATE 19NOV04 TIME 11:51:16 *
756-1104 *
*
*****
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND 'EC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1
PAGE 1

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Wolf Ranch, Master Developed Drainage Plan									
2	ID	A Basins, future development condition									
3	ID	5-year and 100 Year, 24 hr Type IIA Storm									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	5	0								
6	JR	PREC	.56	1.0							
7	KK	A-1									
8	KM	RUNOFF FROM SUB-BASIN A-1									
9	BA	.060									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143
13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270


```

71      KM  DESIGN POINT A6 COMBINE RUNOFF FROM SUB-BASIN A-6, A6 AND A7
72      HC      3

73      KK  A5
74      KM  ROUTE FLOW FROM DESIGN POINT A6 TO DP A5
75      RD  2200 .011 .04 TRAP 10 4

76      KK  A-9
77      KM  RUNOFF FROM SUB-BASIN A-9
78      BA  .0673
79      LS  0 72.1
80      UD  .263

81      KK  A9
82      KM  ROUTE FLOW FROM SUB-BASIN A-9 TO DESIGN POINT A5
83      RD  500 .02 .016 CIRC 3.5

```

1
PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

84      KK  A-5
85      KM  RUNOFF FROM SUB-BASIN A-5
86      BA  .1114
87      LS  0 77.7
88      UD  .209

89      KK  DPA5
90      KM  DESIGN POINT A5 COMBINE RUNOFF FROM SUB-BASIN A-5, A5 AND A9
91      HC      3

92      KK  A10
93      KM  ROUTE FLOW FROM DESIGN POINT A5 TO DESIGN POINT A
94      RD  720 .021 .04 TRAP 15 4

95      KK  A-10
96      KM  RUNOFF FROM SUB-BASIN A-10
97      BA  .0086
98      LS  0 61
99      UD  .231

100     KK  DPA
101     KM  DESIGN POINT A COMBINE RUNOFF SUB-BASIN A-10 AND A10
102     HC      2
103     ZZ

```

1

SCHMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE  (V) ROUTING      (--->) DIVERSION OR PUMP FLOW

NO.   (.) CONNECTOR   (<---) RETURN OF DIVERTED OR PUMPED FLOW

 7     A-1
      V
      V
24     A3
      .
      .
27     .             A-11
      .             V
      .             V
32     .             A11
      .             .
      .             .
35     .             .             A-4
      .             .
      .             .
40     .             DPA4.....
      .             V
      .             V

```

```

43      .           A4
      .           .
      .           .
46      .           .           A-3
      .           .           .
      .           .           .
51      DPA3.....
      V
      V
54      A6
      .
      .
57      .           A-7
      .           V
      .           V
62      .           A7
      .           .
      .           .
65      .           .           A-6
      .           .           .
      .           .           .
70      DPA6.....
      V
      V
73      A5
      .
      .
76      .           A-9
      .           V
      .           V
81      .           A9
      .           .
      .           .
84      .           .           A-5
      .           .           .
      .           .           .
89      DPA5.....
      V
      V
92      A10
      .
      .
95      .           A-10
      .           .
      .           .
100     DPA.....

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
*
CALIFORNIA 95616 *
* RUN DATE 19NOV04 TIME 11:51:16 *
756-1104 *
*
*****
*****

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*
* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,
* (916)
*

```

Wolf Ranch, Master Developed Drainage Plan
 A Basins, future development condition
 5-year and 100 Year, 24 hr Type IIA Storm

5 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK

 COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .56 1.00

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	A-1	.06	1	FLOW	3.
				TIME	32.
					6.25
					6.17
ROUTED TO					
+	A3	.06	1	FLOW	3.
				TIME	31.
					6.75
					6.42
HYDROGRAPH AT					
+	A-11	.08	1	FLOW	45.
				TIME	140.
					6.08
					6.08
ROUTED TO					
+	A11	.08	1	FLOW	44.
				TIME	138.
					6.08
					6.08
HYDROGRAPH AT					
+	A-4	.09	1	FLOW	49.
				TIME	149.
					6.08
					6.08
2 COMBINED AT					
+	DEA4	.17	1	FLOW	92.
				TIME	288.
					6.08
					6.08

ROUTED TO						
+	A4	.17	1	FLOW TIME	91. 6.08	286. 6.08
HYDROGRAPH AT						
+	A-3	.15	1	FLOW TIME	64. 6.08	223. 6.08
3 COMBINED AT						
+	DPA3	.38	1	FLOW TIME	155. 6.08	509. 6.08
ROUTED TO						
+	A6	.38	1	FLOW TIME	154. 6.17	491. 6.17
HYDROGRAPH AT						
+	A-7	.05	1	FLOW TIME	30. 6.08	90. 6.08
ROUTED TO						
+	A7	.05	1	FLOW TIME	29. 6.08	89. 6.08
HYDROGRAPH AT						
+	A-6	.04	1	FLOW TIME	22. 6.08	66. 6.08
3 COMBINED AT						
+	DPA6	.46	1	FLOW TIME	199. 6.17	631. 6.08
ROUTED TO						
+	A5	.46	1	FLOW TIME	196. 6.25	623. 6.17
HYDROGRAPH AT						
+	A-9	.07	1	FLOW TIME	19. 6.17	76. 6.17
ROUTED TO						
+	A9	.07	1	FLOW TIME	18. 6.17	76. 6.17
HYDROGRAPH AT						
+	A-5	.11	1	FLOW TIME	57. 6.08	184. 6.08
3 COMBINED AT						
+	DPA5	.64	1	FLOW TIME	254. 6.25	862. 6.17
ROUTED TO						
+	A10	.64	1	FLOW TIME	249. 6.25	848. 6.17
HYDROGRAPH AT						
+	A-10	.01	1	FLOW TIME	0. 6.17	5. 6.17
2 COMBINED AT						
+	DPA	.65	1	FLOW TIME	250. 6.25	854. 6.17

*** NORMAL END OF HEC-1 ***

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1*****
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*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
U.S. ARMY CORPS OF ENGINEERS
* JUN 1998
HYDROLOGIC ENGINEERING CENTER
* VERSION 4.1
609 SECOND STREET
*
DAVIS, CALIFORNIA 95616
* RUN DATE 03FEB04 TIME 11:18:38
(916) 756-1104
*
*****
*****

```

*B' BASINS
FUTURE CONDITIONS*

```

X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1
PAGE 1

HEC-1 INPUT

```

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Wolf Ranch Master Development Drainage Plan
2 ID B basins future development condition PN 03094
3 ID 5-year and 100 Year, 24 hr Type IIA Storm FN bbas-f.dat
*DIAGRAM
4 IT 5 0 0 300
5 IO 5 0
6 JR PREC .56 1.0
7 KK B-1
8 KM RUNOFF FOR SUB-BASIN B-1
9 BA .0400
10 IN 15
11 PB 4.4
12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100
0.0120 0.0143
13 PC 0.0165 0.0188 0.0210 0.0233 0.0255 0.0278 0.0320 0.0390
0.0460 0.0530
14 PC 0.0600 0.0750 0.1000 0.4000 0.7000 0.7250 0.7500 0.7650
0.7800 0.7900
15 PC 0.8000 0.8100 0.8200 0.8250 0.8300 0.8350 0.8400 0.8450
0.8500 0.8550
16 PC 0.8600 0.8638 0.8675 0.8713 0.8750 0.8788 0.8825 0.8863
0.8900 0.8938

```


0.9240	0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210
0.9500	0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475
0.9750	0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725
0.9900	0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888
		21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000	
		22	LS	0	92						
		23	UD	.1070							
		24	ZZ								

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT
 LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
 7 B-1

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
609 SECOND STREET *
*
DAVIS, CALIFORNIA 95616 *
* RUN DATE 03FEB04 TIME 11:18:38 *
(916) 756-1104 *
*
*****
*****

```

Wolf Ranch Master Development Drainage Plan
 B basins future development condition PN 03094
 5-year and 100 Year, 24 hr Type IIA Storm FN bbas-f.dat

5 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE- FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS


```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
CORPS OF ENGINEERS
* JUN 1998
ENGINEERING CENTER
* VERSION 4.1
SECOND STREET
*
CALIFORNIA 95616
* RUN DATE 03FEB04 TIME 11:12:55
(916) 756-1104
*
*****
*****

```

*C' Basins
Developed
Conditions*

```

*
* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,
*
*

```

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

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DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1
PAGE 1

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Wolf Ranch Master Development Drainage Plan									
2	ID	C basins future development condition PN 03094									
3	ID	5-year and 100 Year, 24 hr Type IIA Storm FN Cbas-f.dat									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	5	0								
6	JR	PREC	.56	1.0							
7	KK	C-1									
8	KM	RUNOFF FOR SUB-BASIN C-1									
9	BA	.0460									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143
13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270

18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	79								
23	UD	.1550									
24	KK	C1									
25	KM	ROUTE FLOW FROM SUB-BASIN C-1 TO C2									
26	RD	2500	0.02	.013			CIRC	4.0			
27	KK	C2									
28	KM	ROUTE FLOW FROM C1 TO DP C									
29	RD	1450	0.02	.013			CIRC	6.0			
30	KK	C-2									
31	KM	RUNOFF FROM SUB-BASIN C-2									
32	BA	.1110									
33	LS	0	80.8								
34	UD	.098									
35	KK	DPC									
36	KM	DESIGN POINT C COMBINE RUNOFF FROM SUB-BASIN C-2 AND C2									
37	HC	2									
38	KK	C-3									
39	KM	RUNOFF FROM SUB-BASIN C-3									
40	BA	.0550									
41	LS	0	79								
42	UD	.186									
43	ZZ										

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT
 LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

```

  7      C-1
        V
        V
  24     C1
        V
        V
  27     C2
        .
        .
  30     .      C-2
        .      .
        .      .
  35     DPC.....
        .
        .
  38     .      C-3
  
```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
CORPS OF ENGINEERS
* JUN 1998
ENGINEERING CENTER
* VERSION 4.1
SECOND STREET
*
CALIFORNIA 95616
*
* RUN DATE 03FEB04 TIME 11:12:55
(916) 756-1104
  
```

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*
*
* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,
*
  
```

* * *

Wolf Ranch Master Development Drainage Plan
C basins future development condition PN 03094
5-year and 100 Year, 24 hr Type IIA Storm FN Cbas-f.dat

5 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .56 1.00

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	C-1	.05	1	FLOW	30.
				TIME	6.08
					86.
ROUTED TO					
+	C1	.05	1	FLOW	29.
				TIME	6.08
					86.
ROUTED TO					
+	C2	.05	1	FLOW	27.
				TIME	6.08
					84.
HYDROGRAPH AT					
+	C-2	.11	1	FLOW	94.
				TIME	6.00
					253.

2 COMBINED AT
 + DPC .16 1 FLOW 114. 328.
 TIME 6.00 6.00

HYDROGRAPH AT
 + C-3 .05 1 FLOW 33. 100.
 TIME 6.08 6.08

1

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

VOLUME	ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO COMPUTATION INTERVAL	
								PEAK (CFS)	TIME TO PEAK (MIN)
.81		C1 MANE	1.50	29.12	367.50	.81	5.00	28.61	365.00

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1995E+01 EXCESS= .0000E+00 OUTFLOW= .1995E+01 BASIN STORAGE= .2215E-03
 PERCENT ERROR= .0

2.29		C1 MANE	1.75	86.16	364.00	2.29	5.00	85.58	365.00
------	--	---------	------	-------	--------	------	------	-------	--------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5624E+01 EXCESS= .0000E+00 OUTFLOW= .5624E+01 BASIN STORAGE= .2322E-03
 PERCENT ERROR= .0

.81		C2 MANE	1.25	28.40	367.50	.81	5.00	26.94	365.00
-----	--	---------	------	-------	--------	-----	------	-------	--------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1990E+01 EXCESS= .0000E+00 OUTFLOW= .1990E+01 BASIN STORAGE= .1307E-03
 PERCENT ERROR= .0

2.29		C2 MANE	1.27	84.87	366.20	2.29	5.00	84.05	365.00
------	--	---------	------	-------	--------	------	------	-------	--------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5620E+01 EXCESS= .0000E+00 OUTFLOW= .5620E+01 BASIN STORAGE= .1300E-03
 PERCENT ERROR= .0

*** NORMAL END OF HEC-1 ***


```

24      KK      D2
25      KM      ROUTE FLOW FROM SUB-BASIN D-1 TO DP D2
26      RD      1230  0.01  .013          CIRC      4.5

27      KK      D-2
28      KM      RUNOFF FROM SUB-BASIN D-2
29      BA      .0360
30      LS      0      79
31      UD      .119

32      KK      DPD2
33      KM      DESIGN POINT D2 COMBINE RUNOFF FROM SUB-BASIN D-2 AND D2
34      HC      2

35      KK      D3
36      KM      ROUTE FLOW FROM DP D2 TO DP D
37      RD      3100  .026  .040          TRAP      4.0      4

38      KK      D-3
39      KM      RUNOFF FROM SUB-BASIN D-3
40      BA      .0240
41      LS      0      61
42      UD      .380

```

1
PAGE 2

HEC-1 INPUT

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43      KK      DPD
44      KM      DESIGN POINT D COMBINE RUNOFF FROM SUB-BASINS D-3 AND D2
45      HC      2
46      ZZ

```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE      (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.      (.) CONNECTOR    (<---) RETURN OF DIVERTED OR PUMPED FLOW

7        D-1
        V
        V
24       D2
        .
        .
27       .      D-2
        .
        .
32       DPD2.....
        V
        V
35       D3
        .
        .
38       .      D-3
        .
        .
43       DPD.....

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

1*****

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*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
* CALIFORNIA 95616 *
* RUN DATE 03FEB04 TIME 16:50:52 *
(916) 756-1104 *
*
* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,

```


* * *

Wolf Ranch Master Development Drainage Plan
D basins future development condition PN 03094
5-year and 100 Year, 24 hr Type IIA Storm FN Dbas-f.dat

5 IO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN 5 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 300 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 2 0 ENDING DATE
NDTIME 0055 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-Feet
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION

NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION

RATIOS OF PRECIPITATION
.56 1.00

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	D-1	.06	1	FLOW	36.
				TIME	6.08
					109.
ROUTED TO					
+	D2	.06	1	FLOW	34.
				TIME	6.08
					107.
HYDROGRAPH AT					
+	D-2	.04	1	FLOW	25.
				TIME	6.00
					73.
2 COMBINED AT					
+	DD2	.10	1	FLOW	57.
				TIME	6.08
					173.
ROUTED TO					
+	D3	.10	1	FLOW	55.
				TIME	6.17
					170.
HYDROGRAPH AT					

```

+           D-3      .02    1  FLOW      1.    11.
              TIME      6.42   6.25

  2 COMBINED AT
+           DPD      .12    1  FLOW     55.   179.
              TIME      6.17   6.17
1

```

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

VOLUME	ISTAQ	ELEMENT	DT	PEAK	TIME TO	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		
								PEAK	TIME TO	
			(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
	FOR PLAN = 1	RATIO=	.00							
.77	D2	MANE	1.50	34.98	366.00	.77	5.00	33.89	365.00	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2544E+01 EXCESS= .0000E+00 OUTFLOW= .2544E+01 BASIN STORAGE= .1572E-03
PERCENT ERROR= .0

2.22	FOR PLAN = 1	RATIO=	.00							
	D2	MANE	1.40	108.18	366.18	2.22	5.00	107.31	365.00	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7337E+01 EXCESS= .0000E+00 OUTFLOW= .7336E+01 BASIN STORAGE= .1466E-03
PERCENT ERROR= .0

.79	FOR PLAN = 1	RATIO=	.00							
	D3	MANE	1.50	55.48	372.00	.79	5.00	54.65	370.00	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4107E+01 EXCESS= .0000E+00 OUTFLOW= .4109E+01 BASIN STORAGE= .3421E-02
PERCENT ERROR= -.1

2.24	FOR PLAN = 1	RATIO=	.00							
	D3	MANE	1.75	171.92	367.50	2.25	5.00	169.71	370.00	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1174E+02 EXCESS= .0000E+00 OUTFLOW= .1175E+02 BASIN STORAGE= .3457E-02
PERCENT ERROR= -.1

*** NORMAL END OF HEC-1 ***

```

*****
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
CORPS OF ENGINEERS
* JUN 1998
ENGINEERING CENTER
* VERSION 4.1
SECOND STREET
*
CALIFORNIA 95616
* RUN DATE 05FEB04 TIME 14:01:38
(916) 756-1104
*****
*****

```

E BASIN
DEVELOPED CONDITIONS

```

* U.S. ARMY
HYDROLOGIC
* 609
* DAVIS,
*
*

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1
PAGE 1

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Wolf Ranch Master Development Drainage Plan									
2	ID	E basins future development condition PN 03094									
3	ID	5-year and 100 Year, 24 hr Type IIA Storm FN Dbas E dat									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	5	0								
6	JR	PREC	.56	1.0							
7	KK	E-1									
8	KM	RUNOFF FOR SUB-BASIN E-1									
9	BA	.0403									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143
13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270

18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	81.8								
23	UD	.1450									
24	KK	E5									
25	KM	ROUTE FLOW FROM SUB-BASIN E-1 TO DP E5									
26	RD	360	.010	.035		TRAP	10	4			
27	KK	E-6									
28	KM	RUNOFF FROM SUB-BASIN E-6									
29	BA	.0478									
30	LS	0	79								
31	UD	.181									
32	KK	E6									
33	KM	ROUTE FLOW FROM SUB-BASIN E-6 TO DP E5									
34	RD	1450	.010	.013		CIRC	3				
35	KK	E-5									
36	KM	RUNOFF FROM SUB-BASIN E-5									
37	BA	.0400									
38	LS	0	79								
39	UD	.119									
40	KK	DPE5									
41	KM	DESIGN POINT E5 COMBINE RUNOFF FROM SUB-BASIN E-5, E6 AND E5									
42	HC	3									

HEC-1 INPUT

1
PAGE 2

LINE	ID	1	2	3	4	5	6	7	8	9	10
43	KK	E2									
44	KM	ROUTE FLOW FROM DESIGN POINT E5 TO DP E2									
45	RD	1850	.010	.013		CIRC	4.5				
46	KK	E-2									
47	KM	RUNOFF FROM SUB-BASIN E-2									
48	BA	.0520									
49	LS	0	79								
50	UD	.134									
51	KK	DPE2									
52	KM	DESIGN POINT E2 COMBINE RUNOFF FROM SUB-BASIN E-2 AND E2									
53	HC	2									
54	KK	E3									
55	KM	ROUTE FLOW FROM DP E2 TO DP E									
56	RD	3150	.010	.040		TRAP	10	4			
57	KK	E-3									
58	KM	RUNOFF FROM SUB-BASIN E-3									
59	BA	.0095									
60	LS	0	61								
61	UD	.397									
62	KK	DPE									
63	KM	DESIGN POINT E COMBINE RUNOFF FROM SUB-BASIN E-3 AND E3									
64	HC	2									
65	KK	E-4									
66	KM	RUNOFF FROM SUB-BASIN E-4									
67	BA	.0423									
68	LS	0	79								
69	UD	.141									
70	ZZ										

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE NO.	(V) ROUTING (.) CONNECTOR	(--->) DIVERSION OR PUMP FLOW (<---) RETURN OF DIVERTED OR PUMPED FLOW
7	E-1	
	V	
	V	
24	E5	
	.	
	.	
27	.	E-6
	.	V
	.	V
32	.	E6
	.	.
	.	.
35	.	E-5
	.	.
	.	.
40	DPE5.....	
	V	
	V	
43	E2	
	.	
	.	
46	.	E-2
	.	.
	.	.
51	DPE2.....	
	V	
	V	
54	E3	
	.	
	.	
57	.	E-3
	.	.
	.	.
62	DPE.....	
	.	
	.	
65	.	E-4

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
*
CALIFORNIA 95616 *
* RUN DATE 05FEB04 TIME 14:01:38 *
(916) 756-1104 *
*
*****
*****

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* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,

Wolf Ranch Master Development Drainage Plan
D basins future development condition PN 03094
5-year and 100 Year, 24 hr Type IIA Storm FN Dbas-f.dat


```

HYDROGRAPH AT
+           E-2      .05      1  FLOW      34.      102.
          TIME      6.08      6.00

  2 COMBINED AT
+           DPE2     .18      1  FLOW     116.     336.
          TIME      6.08      6.08

ROUTED TO
+           E3       .18      1  FLOW     111.     330.
          TIME      6.25      6.17

HYDROGRAPH AT
+           E-3     .01      1  FLOW      0.       4.
          TIME     6.42      6.33

  2 COMBINED AT
+           DPE     .19      1  FLOW     111.     334.
          TIME      6.25      6.17

HYDROGRAPH AT
+           E-4     .04      1  FLOW     28.      81.
          TIME      6.08      6.00
1

```

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

VOLUME	ISTAQ	ELEMENT	DT	PEAK	TIME TO	VOLUME	INTERPOLATED TO			
							DT	COMPUTATION INTERVAL	PEAK	TIME TO
			(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
	FOR PLAN = 1	RATIO= .00								
.96	E5	MANE	1.74	31.18	364.81	.96	5.00	31.15	365.00	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2065E+01 EXCESS= .0000E+00 OUTFLOW= .2065E+01 BASIN STORAGE= .2915E-03
PERCENT ERROR= .0

2.53	FOR PLAN = 1	RATIO= .00								
	E5	MANE	1.31	85.18	361.81	2.53	5.00	82.96	365.00	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5440E+01 EXCESS= .0000E+00 OUTFLOW= .5439E+01 BASIN STORAGE= .3190E-03
PERCENT ERROR= .0

.81	FOR PLAN = 1	RATIO= .00								
	E6	MANE	1.50	28.88	367.50	.81	5.00	27.61	365.00	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2073E+01 EXCESS= .0000E+00 OUTFLOW= .2073E+01 BASIN STORAGE= .1962E-03
PERCENT ERROR= .0

2.29	FOR PLAN = 1	RATIO= .00								
	E6	MANE	1.75	85.53	365.75	2.29	5.00	85.12	365.00	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5844E+01 EXCESS= .0000E+00 OUTFLOW= .5843E+01 BASIN STORAGE= .1744E-03
PERCENT ERROR= .0

F-BASINS DEVELOPMENT

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1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
CORPS OF ENGINEERS
* JUN 1998
ENGINEERING CENTER
* VERSION 4.1
SECOND STREET
*
CALIFORNIA 95616
* RUN DATE 19NOV04 TIME 12:35:23
756-1104
*
*****
*****

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X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

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DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT
PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10	
1	ID	Wolf Ranch Master Development Drainage Plan										
2	ID	F basins future development conditions PN 03094										
3	ID	5-year and 100 year, 24hr Type IIA Storm										
	*DIAGRAM											
4	IT	5	0	0	300							
5	IO	5	0									
6	JR	PREC	.56	1.0								
7	KK	F-8										
8	KM	RUNOFF FOR SUB-BASIN F-8										
9	BA	.0630										
10	IN	15										
11	PB	4.4										
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143	
13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530	
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900	
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550	
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938	
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270	

71	KM	COMBINE FLOW FROM SUB-BASIN F-10 AND RF10
72	HC	2
73	KK	RF-18A
74	KM	ROUTE FLOW FROM DESIGN POINT DP F10 TO DESIGN POINT F18
75	RD	1800 0.037 0.04 TRAP 10 6
76	KK	F-3
77	KM	RUNOFF FOR SUB-BASIN F-3
78	BA	.0942
79	LS	0 61
80	UD	.22
81	KK	RF-11
82	KM	ROUTE FLOW FROM SUB-BASIN F-3 TO DESIGN POINT F11
83	RD	950 0.038 0.04 TRAP 10 6

HEC-1 INPUT

LINE	ID1.....2.....3.....4.....5.....6.....7.....8.....9.....10
84	KK	F-11
85	KM	RUNOFF FOR SUB-BASIN F-11
86	BA	.0460
87	LS	0 68.2
88	UD	.17
89	KK	DPF11
90	KM	COMBINE FLOW FROM SUB-BASIN F-11 AND RF-11
91	HC	2
92	KK	RF-18
93	KM	ROUTE FLOW FROM DESIGN POINT F11 TO DESIGN POINT F18
94	RD	1800 0.037 0.04 TRAP 10 6
95	KK	F-4
96	KM	RUNOFF FOR SUB-BASIN F-4
97	BA	.2681
98	LS	0 61
99	UD	.28
100	KK	RF-12
101	KM	ROUTE FLOW FROM SUB-BASIN F-4 TO DESIGN POINT F12
102	RD	1150 0.044 0.04 TRAP 10 6
103	KK	F-5
104	KM	RUNOFF FOR SUB-BASIN F-5
105	BA	.1073
106	LS	0 61
107	UD	.34
108	KK	RF-12A
109	KM	ROUTE FLOW FROM SUB-BASIN F-5 TO DESIGN POINT F12
110	RD	1600 0.035 0.04 TRAP 10 6
111	KK	F-12
112	KM	RUNOFF FOR SUB-BASIN F-12
113	BA	.0590
114	LS	0 69.1
115	UD	.20
116	KK	DPF12
117	KM	COMBINE FLOW FROM SUB-BASIN RF-12, RF-12A, AND F-12
118	HC	3
119	KK	RF-17
120	KM	ROUTE FLOW FROM DESIGN POINT F-12 TO DESIGN POINT F18
121	RD	1900 0.028 0.04 TRAP 10 6
122	KK	F-17

123 KM RUNOFF FOR SUB-BASIN F-17
 124 BA .0380
 125 LS 0 61.6
 126 UD .21

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

127 KK F-18
 128 KM RUNOFF FOR SUB-BASIN F-18
 129 BA .0980
 130 LS 0 69.7
 131 UD .21

132 KK DPF18
 133 KM COMBINE FLOW FROM SUB-BASINS F-18 AND F17, AND RF-18A, RF-18 AND RF-17
 134 HC 5

135 KK RF-22A
 136 KM ROUTE FLOW FROM DESIGN POINT F-18 TO DESIGN POINT F22
 137 RD 1800 0.027 0.04 TRAP 10 6

138 KK F-22
 139 KM RUNOFF FOR SUB-BASIN F-22
 140 BA .0640
 141 LS 0 64.1
 142 UD .21

143 KK DPF22
 144 KM COMBINE FLOW FROM SUB-BASIN F-22, RF-22 AND RF-22A
 145 HC 3

146 KK RF-27A
 147 KM ROUTE FLOW FROM DESIGN POINT F-22 TO DESIGN POINT F27A
 148 RD 500 0.029 0.04 TRAP 10 6

149 KK F-16
 150 KM RUNOFF FOR SUB-BASIN F-16
 151 BA .0270
 152 LS 0 69.9
 153 UD .21

154 KK RF-16
 155 KM ROUTE FLOW FROM SUB-BASIN F-16 TO DESIGN POINT F27A
 156 RD 2000 0.030 0.04 TRAP 10 6

157 KK DPF27A
 158 KM COMBINE FLOW FROM RF-16 AND FR-27A
 159 HC 2

160 KK RF-27B
 161 KM ROUTE FLOW FROM DESIGN POINT F27A TO DESIGN POINT F27
 162 RD 3150 0.020 0.04 TRAP 10 6

163 KK F-21
 164 KM RUNOFF FOR SUB-BASIN F-21
 165 BA .0790
 166 LS 0 89.1
 167 UD .25

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

168 KK RF-26
 169 KM ROUTE FLOW FROM SUB-BASIN 26 TO DESIGN POINT F26
 170 RD 1300 .028 .04 TRAP 10 6

275 KK RF-29
 276 KM ROUTE FLOW FROM DESIGN POINT F30 TO DESIGN POINT F29
 277 RD 2350 0.027 0.04 TRAP 6 3

 278 KK F-29
 279 KM RUNOFF FOR SUB-BASIN F-29
 280 BA .0250
 281 LS 0 73.0
 282 UD .19

 283 KK DPF29
 284 KM COMBINE FLOW FROM RF-29 AND F-29
 285 HC 2

 286 KK RF-28
 287 KM ROUTE FLOW FROM DESIGN POINT F29 TO DESIGN POINT F28
 288 RD 750 0.015 0.04 TRAP 20 3
 HEC-1 INPUT

1
PAGE 8

LINE	ID	1	2	3	4	5	6	7	8	9	10
289	KK	F-28									
290	KM	RUNOFF FOR SUB-BASIN F-28									
291	BA	.042									
292	LS	0 73.0									
293	UD	.23									
294	KK	F-27									
295	KM	RUNOFF FOR SUB-BASIN F-27									
296	BA	.213									
297	LS	0 69.2									
298	UD	.32									
299	KK	DPF28									
300	KM	COMBINE FLOW FROM RF-27C, RF-28, F-28 AND F-27									
301	HC	4									
302	KK	RF-31									
303	KM	ROUTE FLOW FROM DESIGN POINT F28 TO DESIGN POINT F									
304	RD	3500 0.023 0.04 TRAP 100 3									
305	KK	F-31									
306	KM	RUNOFF FOR SUB-BASIN F-31									
307	BA	.0810									
308	LS	0 65.0									
309	UD	.24									
310	KK	DP F									
311	KM	COMBINE FLOW FROM RF-31 AND F-31									
312	HC	2									
313	ZZ										

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE NO.	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
7	F-8	
	V	
	V	
24	RF-8	
	.	
	.	
27	F-1	
	V	
	V	
32	RF-9	
	.	

35	.	.	F-9	.	
	
40	.	DPF9.....	.	.	
	.	V	.	.	
	.	V	.	.	
43	.	RF-19	.	.	
	
46	.	.	F-19	.	
	
51	DPF19.....	.	.	.	
	V	.	.	.	
	V	.	.	.	
54	RF-22	.	.	.	
	
57	.	F-2	.	.	
	.	V	.	.	
	.	V	.	.	
62	.	RF-10	.	.	
	
65	.	.	F-10	.	
	
70	.	DPF10.....	.	.	
	.	V	.	.	
	.	V	.	.	
73	.	RF-18A	.	.	
	
76	.	.	F-3	.	
	.	.	V	.	
	.	.	V	.	
81	.	.	RF-11	.	
	
84	.	.	.	F-11	
	
89	.	.	DPF11.....	.	
	.	.	V	.	
	.	.	V	.	
92	.	.	RF-18	.	
	
95	.	.	.	F-4	
	.	.	.	V	
	.	.	.	V	
100	.	.	RF-12	.	
	
103	.	.	.	F-5	
	.	.	.	V	
	.	.	.	V	
108	.	.	.	RF-12A	
	
111	F-12

116	.	.	.	DPF12.....	.
	.	.	.	V	.
	.	.	.	V	.
119	.	.	.	RF-17	.

122	F-17

127	F-18
132	.	DPF18
	.	V
135	.	V
	.	RF-22A
138	.	.	F-22

143	DPF22
	V
	V
146	RF-27A
149	.	F-16
	.	V
	.	V
154	.	RF-16

157	DPF27A
	V
	V
160	RF-27B
163	.	F-21
	.	V
	.	V
168	.	RF-26

171	.	.	F-26

176	.	DPF26
	.	V
	.	V
179	.	RF-26A

182	DPF27
	V
	V
185	RF-27C
188	.	F-7
	.	V
	.	V
193	.	RF-7

196	.	.	F-14

201	.	.	.	F-6	.	.	.
	.	.	.	V	.	.	.
	.	.	.	V	.	.	.
206	.	.	.	RF-13	.	.	.

209	F-13	.	.

214	.	.	.	DPF13.....
	.	.	.	V
217	.	.	.	V
	.	.	.	RF-14

220	.	DPF14.....	.	.
	.	V	.	.
	.	V	.	.
223	.	RF-25	.	.

226	.	.	F-25	.

231	.	DPF25.....	.	.
	.	V	.	.
	.	V	.	.
234	.	RF-30	.	.

237	.	.	F-15	.
	.	.	V	.
	.	.	V	.
242	.	.	RF-23	.

245	.	.	.	F-23

250	.	.	DPF23.....	.
	.	.	V	.
	.	.	V	.
253	.	.	RF-24	.

256	.	.	.	F-24

261	.	.	DPF24.....	.
	.	.	V	.
	.	.	V	.
264	.	.	RF-30A	.

267	.	.	.	F-30

272	.	DPF30.....	.	.
	.	V	.	.
	.	V	.	.
275	.	RF-29	.	.

278	.	.	F-29	.

283	.	DPF29.....	.	.
	.	V	.	.
	.	V	.	.
286	.	RF-28	.	.

289	.	.	F-28	.

294	.	.	.	F-27

299	.	DPF28.....	.	.
	.	V	.	.

302 V
RF-31
.
305 . F-31
.
310 DP F.....

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

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1*****
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*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
* CALIFORNIA 95616 *
* RUN DATE 19NOV04 TIME 12:35:23 *
756-1104 *
*
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*****

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*
* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,
* (916)
*

Wolf Ranch Master Development Drainage Plan
F basins future development conditions PN 03094
5-year and 100 year, 24hr Type IIA Storm

5 IO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 5 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 300 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 2 0 ENDING DATE
NDTIME 0055 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-Feet
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
.56 1.00

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	F-8	.06	1	FLOW TIME	15. 6.17 69. 6.08
ROUTED TO					
+	RF-8	.06	1	FLOW TIME	15. 6.25 67. 6.17
HYDROGRAPH AT					
+	F-1	.17	1	FLOW TIME	10. 6.17 110. 6.08
ROUTED TO					
+	RF-9	.17	1	FLOW TIME	10. 6.25 106. 6.17
HYDROGRAPH AT					
+	F-9	.04	1	FLOW TIME	10. 6.08 50. 6.08
2 COMBINED AT					
+	DPF9	.21	1	FLOW TIME	18. 6.17 152. 6.08
ROUTED TO					
+	RF-19	.21	1	FLOW TIME	17. 6.33 148. 6.17
HYDROGRAPH AT					
+	F-19	.10	1	FLOW TIME	38. 6.08 144. 6.08
3 COMBINED AT					
+	DPF19	.37	1	FLOW TIME	56. 6.25 338. 6.17
ROUTED TO					
+	RF-22	.37	1	FLOW TIME	55. 6.33 326. 6.17
HYDROGRAPH AT					
+	F-2	.04	1	FLOW TIME	3. 6.17 29. 6.08
ROUTED TO					
+	RF-10	.04	1	FLOW TIME	3. 6.25 28. 6.17
HYDROGRAPH AT					
+	F-10	.02	1	FLOW TIME	5. 6.08 22. 6.08
2 COMBINED AT					
+	DPF10	.06	1	FLOW TIME	6. 6.17 48. 6.08
ROUTED TO					
+	RF-18A	.06	1	FLOW TIME	6. 6.25 47. 6.17
HYDROGRAPH AT					
+	F-3	.09	1	FLOW	5. 59.

				TIME	6.17	6.17
ROUTED TO						
+	RF-11	.09	1	FLOW	5.	58.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-11	.05	1	FLOW	11.	53.
				TIME	6.08	6.08
2 COMBINED AT						
+	DPF11	.14	1	FLOW	13.	102.
				TIME	6.17	6.08
ROUTED TO						
+	RF-18	.14	1	FLOW	13.	102.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-4	.27	1	FLOW	13.	147.
				TIME	6.25	6.17
ROUTED TO						
+	RF-12	.27	1	FLOW	13.	144.
				TIME	6.33	6.25
HYDROGRAPH AT						
+	F-5	.11	1	FLOW	5.	52.
				TIME	6.33	6.25
ROUTED TO						
+	RF-12A	.11	1	FLOW	5.	51.
				TIME	6.50	6.33
HYDROGRAPH AT						
+	F-12	.06	1	FLOW	13.	66.
				TIME	6.17	6.08
3 COMBINED AT						
+	DPF12	.43	1	FLOW	24.	236.
				TIME	6.25	6.25
ROUTED TO						
+	RF-17	.43	1	FLOW	24.	234.
				TIME	6.42	6.25
HYDROGRAPH AT						
+	F-17	.04	1	FLOW	3.	25.
				TIME	6.17	6.08
HYDROGRAPH AT						
+	F-18	.10	1	FLOW	24.	110.
				TIME	6.17	6.08
5 COMBINED AT						
+	DPF18	.77	1	FLOW	58.	476.
				TIME	6.25	6.17
ROUTED TO						
+	RF-22A	.77	1	FLOW	57.	474.
				TIME	6.33	6.25
HYDROGRAPH AT						
+	F-22	.06	1	FLOW	7.	51.
				TIME	6.17	6.08
3 COMBINED AT						
+	DPF22	1.21	1	FLOW	116.	828.
				TIME	6.33	6.25
ROUTED TO						

+	RF-27A	1.21	1	FLOW TIME	113. 6.33	824. 6.25
	HYDROGRAPH AT					
+	F-16	.03	1	FLOW TIME	7. 6.17	31. 6.08
	ROUTED TO					
+	RF-16	.03	1	FLOW TIME	6. 6.25	29. 6.25
	2 COMBINED AT					
+	DPF27A	1.24	1	FLOW TIME	119. 6.33	853. 6.25
	ROUTED TO					
+	RF-27B	1.24	1	FLOW TIME	117. 6.50	838. 6.33
	HYDROGRAPH AT					
+	F-21	.08	1	FLOW TIME	79. 6.08	184. 6.08
	ROUTED TO					
+	RF-26	.08	1	FLOW TIME	79. 6.17	179. 6.17
	HYDROGRAPH AT					
+	F-26	.05	1	FLOW TIME	39. 6.08	105. 6.08
	2 COMBINED AT					
+	DPF26	.13	1	FLOW TIME	112. 6.17	280. 6.08
	ROUTED TO					
+	RF-26A	.13	1	FLOW TIME	110. 6.25	272. 6.17
	2 COMBINED AT					
+	DPF27	1.37	1	FLOW TIME	185. 6.42	1044. 6.33
	ROUTED TO					
+	RF-27C	1.37	1	FLOW TIME	180. 6.50	1045. 6.33
	HYDROGRAPH AT					
+	F-7	.08	1	FLOW TIME	5. 6.17	54. 6.08
	ROUTED TO					
+	RF-7	.08	1	FLOW TIME	5. 6.25	53. 6.17
	HYDROGRAPH AT					
+	F-14	.13	1	FLOW TIME	42. 6.17	162. 6.08
	HYDROGRAPH AT					
+	F-6	.03	1	FLOW TIME	2. 6.17	21. 6.08
	ROUTED TO					
+	RF-13	.03	1	FLOW TIME	2. 6.25	21. 6.17
	HYDROGRAPH AT					
+	F-13	.01	1	FLOW TIME	1. 6.08	11. 6.08

2 COMBINED AT						
+	DPF13	.05	1	FLOW TIME	2. 6.25	30. 6.08
ROUTED TO						
+	RF-14	.05	1	FLOW TIME	2. 6.92	30. 6.33
3 COMBINED AT						
+	DPF14	.25	1	FLOW TIME	45. 6.17	210. 6.17
ROUTED TO						
+	RF-25	.25	1	FLOW TIME	44. 6.33	209. 6.25
HYDROGRAPH AT						
+	F-25	.09	1	FLOW TIME	27. 6.17	106. 6.17
2 COMBINED AT						
+	DPF25	.34	1	FLOW TIME	66. 6.25	303. 6.25
ROUTED TO						
+	RF-30	.34	1	FLOW TIME	66. 6.33	303. 6.25
HYDROGRAPH AT						
+	F-15	.02	1	FLOW TIME	6. 6.08	26. 6.08
ROUTED TO						
+	RF-23	.02	1	FLOW TIME	5. 6.17	24. 6.17
HYDROGRAPH AT						
+	F-23	.03	1	FLOW TIME	12. 6.08	44. 6.08
2 COMBINED AT						
+	DPF23	.05	1	FLOW TIME	15. 6.17	68. 6.08
ROUTED TO						
+	RF-24	.05	1	FLOW TIME	15. 6.25	65. 6.17
HYDROGRAPH AT						
+	F-24	.09	1	FLOW TIME	32. 6.17	115. 6.17
2 COMBINED AT						
+	DPF24	.14	1	FLOW TIME	44. 6.25	180. 6.17
ROUTED TO						
+	RF-30A	.14	1	FLOW TIME	42. 6.25	172. 6.17
HYDROGRAPH AT						
+	F-30	.02	1	FLOW TIME	8. 6.08	30. 6.08
3 COMBINED AT						
+	DPF30	.50	1	FLOW TIME	110. 6.33	488. 6.25
ROUTED TO						
+	RF-29	.50	1	FLOW TIME	108. 6.42	489. 6.25

HYDROGRAPH AT						
+	F-29	.03	1	FLOW	9.	35.
				TIME	6.08	6.08
2 COMBINED AT						
+	DPF29	.53	1	FLOW	111.	510.
				TIME	6.42	6.25
ROUTED TO						
+	RF-28	.53	1	FLOW	111.	494.
				TIME	6.42	6.25
HYDROGRAPH AT						
+	F-28	.04	1	FLOW	14.	53.
				TIME	6.17	6.08
HYDROGRAPH AT						
+	F-27	.21	1	FLOW	38.	183.
				TIME	6.25	6.17
4 COMBINED AT						
+	DPF28	2.15	1	FLOW	323.	1719.
				TIME	6.42	6.33
ROUTED TO						
+	RF-31	2.15	1	FLOW	317.	1711.
				TIME	6.58	6.42
HYDROGRAPH AT						
+	F-31	.08	1	FLOW	10.	64.
				TIME	6.17	6.17
2 COMBINED AT						
+	DP F	2.23	1	FLOW	321.	1740.
				TIME	6.58	6.42
1						

*** NORMAL END OF HEC-1 ***

G-BASINS DEVELOPED

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*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
*
CALIFORNIA 95616 *
* RUN DATE 21MAY04 TIME 12:44:02 *
756-1104 *
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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND 'EC1KW.

THE DEFINITIONS OF VARIABLES -RTIME- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1
PAGE 1

HEC-1 INPUT

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1	ID Wolf Ranch Master Development Drainage Plan
2	ID G Basins Future developed condition PN 03094
3	ID 5-year and 100 Year, 24 hr Type IIA Storm FN Gbas-f.dat
	*DIAGRAM
4	IT 5 0 0 300
5	IO 4 0
6	JR PREC .56 1.0
7	KK G-1
8	KM RUNOFF - Sub-basin G-1
9	BA .0808
10	IN 15
11	PB 4.4
12	PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120 0.0143
13	PC 0.0165 0.0188 0.0210 0.0233 0.0255 0.0278 0.0320 0.0390 0.0460 0.0530
14	PC 0.0600 0.0750 0.1000 0.4000 0.7000 0.7250 0.7500 0.7650 0.7800 0.7900
15	PC 0.8000 0.8100 0.8200 0.8250 0.8300 0.8350 0.8400 0.8450 0.8500 0.8550
16	PC 0.8600 0.8638 0.8675 0.8713 0.8750 0.8788 0.8825 0.8863 0.8900 0.8938
17	PC 0.8975 0.9013 0.9050 0.9083 0.9115 0.9148 0.9180 0.9210 0.9240 0.9270

18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	61								
23	UD	0.22									
24	KK	G2									
25	KM	ROUTE FLOW from SUB-BASIN G-1 TO DP G3									
26	RD	3200	0.027	0.04		TRAP	10			4	
27	KK	G-2									
28	KM	RUNOFF - Sub-basin G-2									
29	BA	.035									
30	LS	0	73								
31	UD	0.22									
32	KK	G3									
33	KM	ROUTE FLOW from SUB-BASIN G-2 TO DP G3									
34	RD	2730	0.024	0.04		TRAP	10			4	
35	KK	G-3									
36	KM	RUNOFF - Sub-basin G-3									
37	BA	.177									
38	LS	0	73								
39	UD	0.29									
40	KK	DPG3									
41	KM	COMBINE RUNOFF from G2, G3 AND SUB-BASIN G-3									
42	HC	3									

1
PAGE 2

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43	KK	G5									
44	KM	ROUTE FLOW from DP G3 TO DP G5									
45	RD	2200	0.02	.013		CIRC	4.5				
46	KK	G-5									
47	KM	RUNOFF - Sub-basin G-5									
48	BA	.153									
49	LS	0	78.4								
50	UD	0.26									
51	KK	DPG									
52	KM	COMBINE RUNOFF from G5 AND SUB-BASIN G-5									
53	HC	2									
54	ZZ										

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT

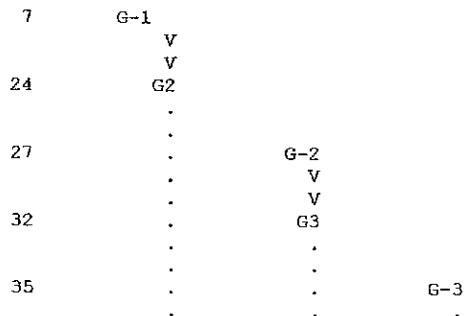
LINE

(V) ROUTING (--->) DIVERSION OR PUMP FLOW

NO.

(.) CONNECTOR

(<---) RETURN OF DIVERTED OR PUMPED FLOW



```

40      DPG3.....
      V
      V
43      G5
      .
46      .          G-5
      .
51      DPG.....

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(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

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1*****
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*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
CALIFORNIA 95616 *
* RUN DATE 21MAY04 TIME 12:44:02 *
756-1104 *
*
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*****

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*
* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,
* (916)
*

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	G-1	.08	1	FLOW TIME	5. 6.17 50. 6.17
ROUTED TO					
+	G2	.08	1	FLOW TIME	4. 6.58 50. 6.25
HYDROGRAPH AT					
+	G-2	.04	1	FLOW TIME	12. 6.17 45. 6.08
ROUTED TO					
+	G3	.04	1	FLOW TIME	12. 6.33 44. 6.25
HYDROGRAPH AT					
+	G-3	.18	1	FLOW TIME	50. 6.17 200. 6.17
3 COMBINED AT					
+	DPG3	.29	1	FLOW TIME	57. 6.25 278. 6.25
ROUTED TO					

+	G5	.29	1	FLOW TIME	55. 6.33	277. 6.25
HYDROGRAPH AT						
+	G-5	.15	1	FLOW TIME	74. 6.17	230. 6.17
2 COMBINED AT						
+	DPG	.45	1	FLOW TIME	120. 6.17	489. 6.17
1						

*** NORMAL END OF HEC-1 ***

H-J Basins Developed

```

*****
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* CORPS OF ENGINEERS
* JUN 1998
* ENGINEERING CENTER
* VERSION 4.1
* SECOND STREET
* CALIFORNIA 95616
* RUN DATE 21MAY04 TIME 15:11:47
* 756-1104
*
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*
* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,
* (916)
*

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1
PAGE 1

HEC-1 INPUT

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1	ID Wolf Ranch master Development Drainage Plan
2	ID H AND J Basins developed conditions PN 03094
3	ID 5-year and 100 Year, 24 hr Type IIA Storm FN hjbas-f.dat
	*DIAGRAM
4	IT 5 0 0 300
5	IO 4 0
6	JR PREC .56 1.0
7	KK H-1
8	KM RUNOFF FROM SUB-BASIN H-1
9	BA .0370
10	IN 15
11	PB 4.4
12	PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120 0.0143
13	PC 0.0165 0.0188 0.0210 0.0233 0.0255 0.0278 0.0320 0.0390 0.0460 0.0530
14	PC 0.0600 0.0750 0.1000 0.4000 0.7000 0.7250 0.7500 0.7650 0.7800 0.7900
15	PC 0.8000 0.8100 0.8200 0.8250 0.8300 0.8350 0.8400 0.8450 0.8500 0.8550
16	PC 0.8600 0.8638 0.8675 0.8713 0.8750 0.8788 0.8825 0.8863 0.8900 0.8938
17	PC 0.8975 0.9013 0.9050 0.9083 0.9115 0.9148 0.9180 0.9210 0.9240 0.9270

18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	0.9525
19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	0.9775
20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	0.9913
21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
22	LS	0	73								
23	UD	0.10									
24	KK	H-2									
25	KM		RUNOFF FROM SUB-BASIN H-2								
26	BA	.0700									
27	LS	0	73								
28	UD	.20									
29	KK	J-1									
30	KM		RUNOFF FROM SUB-BASIN J-1								
31	BA	.0250									
32	LS	0	79								
33	UD	.10									
34	KK	J-2									
35	KM		RUNOFF FROM SUB-BASIN J-2								
36	BA	.0530									
37	LS	0	77								
38	UD	.15									
39	ZZ										

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE NO.	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
7	H-1	
	.	
24	.	H-2
	.	.
29	.	J-1
	.	.
34	.	J-2
	.	.

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
CORPS OF ENGINEERS
* JUN 1998
ENGINEERING CENTER
* VERSION 4.1
SECOND STREET
*
CALIFORNIA 95616
* RUN DATE 21MAY04 TIME 15:11:47
756-1104
*
*****
*****

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*
*
* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,
* (916)
*

```

Wolf Ranch master Development Drainage Plan
H AND J Basins developed conditions PN 03094
5-year and 100 Year, 24 hr Type IIA Storm FN hjbas-f.dat

**HEC-1 INPUT & OUTPUT
DEVELOPED CONDITIONS WITH DETENTION**

A-BASINS DETAINED

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
* CALIFORNIA 95616 *
* RUN DATE 19NOV04 TIME 15:02:01 *
756-1104 *
*
*****
*****

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X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1
PAGE 1

HEC-1 INPUT

LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
1	ID	Wolf Ranch, Master Developed Drainage Plan									
2	ID	A Basins, future development condition									
3	ID	5-year and 100 Year, 24 hr Type IIA Storm									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	5	0								
6	JR	PREC	.56	1.0							
7	KK	A-1									
8	KM	RUNOFF FROM SUB-BASIN A-1									
9	BA	.060									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143
13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270


```

71      KM  DESIGN POINT A6 COMBINE RUNOFF FROM SUB-BASIN A-6, A6 AND A7
72      HC      3

73      KK      A5
74      KM  ROUTE FLOW FROM DESIGN POINT A6 TO DP A5
75      RD  2200  .011  .04      TRAP      10      4

76      KK  A-9
77      KM  RUNOFF FROM SUB-BASIN A-9
78      BA  .0673
79      LS   0      72.1
80      UD  .263

81      KK      A9
82      KM  ROUTE FLOW FROM SUB-BASIN A-9 TO DESIGN POINT A5
83      RD  500   .02   .016      CIRC      3.5

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1
PAGE 3

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

84      KK  A-5
85      KM  RUNOFF FROM SUB-BASIN A-5
86      BA  .1114
87      LS   0      77.7
88      UD  .209

89      KK  DPA5
90      KM  DP A5 COMBINE RUNOFF FROM SUB-BASIN A-5, A5 AND A9 THIS IS INFLOW
91      KM  TO DETENTION BASIN A
92      HC      3

93      KK  DBA
94      KM  ROUTE DP A5 THROUGH DETENTION BASIN A
95      RS   1      ELEV      100
96      SV   0      4      10      20      40      60
97      SE  100      102      104      106      108      110
98      SQ   0      10      35      80      230      500

99      KK  A10
100     KM  ROUTE FLOW FROM DESIGN POINT A5 TO DESIGN POINT A
101     RD  720   .021   .04      TRAP      15      4

102     KK  A-10
103     KM  RUNOFF FROM SUB-BASIN A-10
104     BA  .0086
105     LS   0      61
106     UD  .231

107     KK  DPA
108     KM  DESIGN POINT A COMBINE RUNOFF SUB-BASIN A-10 AND A10
109     HC      2
110     ZZ

```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO.        (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

7          A-1
          V
          V
24         A3
          .
          .
27         .      A-11
          .      V
          .      V
32         .      A11

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.
.
35 . . . . . A-4
.
.
40 . . . . . DPA4.....
.
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.
.
43 . . . . . A4
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.
.
46 . . . . . A-3
.
.
.
.
51 . . . . . DPA3.....
.
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.
.
54 . . . . . A6
.
.
.
.
57 . . . . . A-7
.
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.
.
62 . . . . . A7
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.
.
.
65 . . . . . A-6
.
.
.
.
70 . . . . . DPA6.....
.
.
.
.
73 . . . . . A5
.
.
.
.
76 . . . . . A-9
.
.
.
.
81 . . . . . A9
.
.
.
.
84 . . . . . A-5
.
.
.
.
89 . . . . . DPA5.....
.
.
.
.
93 . . . . . DBA
.
.
.
.
99 . . . . . A10
.
.
.
.
102 . . . . . A-10
.
.
.
.
107 . . . . . DPA.....

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION


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*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
*
* CALIFORNIA 95616 *

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*
*
* U.S. ARMY
* HYDROLOGIC
* 609
* DAVIS,

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* RUN DATE 19NOV04 TIME 15:02:01 *
 756-1104 *
 * *

Wolf Ranch, Master Developed Drainage Plan
 A Basins, future development condition
 5-year and 100 Year, 24 hr Type IIA Storm

5 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK
 COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-Feet
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .56 1.00

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	A-1	.06	1	FLOW	3.
				TIME	32.
					6.25
					6.17
ROUTED TO					
+	A3	.06	1	FLOW	3.
				TIME	31.
					6.75
					6.42
HYDROGRAPH AT					
+	A-11	.08	1	FLOW	45.
				TIME	140.
					6.08
					6.08
ROUTED TO					

+	A11	.08	1	FLOW TIME	44. 6.08	139. 6.08
	HYDROGRAPH AT					
+	A-4	.09	1	FLOW TIME	49. 6.08	149. 6.08
	2 COMBINED AT					
+	DPA4	.17	1	FLOW TIME	93. 6.08	288. 6.08
	ROUTED TO					
+	A4	.17	1	FLOW TIME	91. 6.08	286. 6.08
	HYDROGRAPH AT					
+	A-3	.15	1	FLOW TIME	64. 6.08	223. 6.08
	3 COMBINED AT					
+	DPA3	.38	1	FLOW TIME	155. 6.08	509. 6.08
	ROUTED TO					
+	A6	.38	1	FLOW TIME	154. 6.17	489. 6.17
	HYDROGRAPH AT					
+	A-7	.05	1	FLOW TIME	30. 6.08	90. 6.08
	ROUTED TO					
+	A7	.05	1	FLOW TIME	29. 6.08	89. 6.08
	HYDROGRAPH AT					
	A-6	.04	1	FLOW TIME	22. 6.08	66. 6.08
	3 COMBINED AT					
+	DPA6	.46	1	FLOW TIME	200. 6.17	632. 6.08
	ROUTED TO					
+	A5	.46	1	FLOW TIME	196. 6.25	626. 6.17
	HYDROGRAPH AT					
+	A-9	.07	1	FLOW TIME	19. 6.17	76. 6.17
	ROUTED TO					
+	A9	.07	1	FLOW TIME	18. 6.17	76. 6.17
	HYDROGRAPH AT					
+	A-5	.11	1	FLOW TIME	57. 6.08	184. 6.08
	3 COMBINED AT					
+	DPA5	.64	1	FLOW TIME	254. 6.25	865. 6.17
	ROUTED TO					
+	DBA	.64	1	FLOW TIME	34. 7.17	165. 6.83

** PEAK STAGES IN FEET **

1	STAGE	103.90	107.13
	TIME	7.17	6.83

ROUTED TO

A10	.64	1	FLOW	34.	165.
			TIME	7.25	6.83

HYDROGRAPH AT

+	A-10	.01	1	FLOW	0.	5.
				TIME	6.17	6.17

2 COMBINED AT

+	DPA	.65	1	FLOW	34.	166.
				TIME	7.25	6.83

1

*** NORMAL END OF HEC-1 ***

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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
*
* RUN DATE 06JUL04 TIME 14:18:28 *
*
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*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

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X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Wolf Ranch Master Development Drainage Plan									
2	ID	E and D basins future development condition pn 03094									
3	ID	5-year and 100 year, 24hr Type IIA Storm FN:E&D-DET.DAT									
4	IT	5	0	0	300						
5	IO	5	0								
6	JR	PREC	.56	1.0							
7	KK	E-1									
8	KM	RUNOFF FOR SUB-BASIN E-1									
9	BA	.0403									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143
13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530


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54      KK      D-1
55      KM      RUNOFF FOR SUB-BASIN D-1
56      BA      .0620
57      LS      0      78.1
58      UD      .180

59      KK      D2
60      KM      ROUTE FLOW FROM SUB-BASIN D-1 TO DP D2
61      RD      1230      0.01      .013      CIRC      4.5

62      KK      D-2
63      KM      RUNOFF FROM SUB-BASIN D-2
64      BA      .0360
65      UD      .119

66      KK      DPD2
67      KM      DESIGN POINT D2 COMBINE RUNOFF FROM SUB-BASIN D-2 AND D2
68      HC      2

69      KK      DPE-D
70      KM      DESIGN POINT DPED COMBINE DP 2 AND DP E2
71      KM      THIS IS THE INFLOW TO DETENTION BASIN E-D
72      HC      2

73      KK      DBE-D
74      KM      DESIGN POINT DPED INTO DETENTION BASIN E-D
75      KM      THIS IS THE OUTFLOW FROM DETENTION BASIN E-D
76      RS      1      ELEV      -1
77      SQ      0      2.2      11      15      109.2      162.9      179.9      509
78      SE      6952      6954.25      6954.5      6956.33      6957      6958      6959      6960
79      SA      0      1.5      2.08      3.04      3.59      3.86      4      4.2
80      SE      6952      6953      6954      6955      6957      6959      6960      6961
81      ZZ

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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 06JUL04 TIME 14:18:28 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****

```

Wolf Ranch Master Development Drainage Plan
E and D basins future development condition pn 03094
5-year and 100 year, 24hr Type IIA Storm FN:E&D-DET.DAT

5 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0055 ENDING TIME
 ICENT 19 CENTURY MARK

 COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .56 1.00

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00
HYDROGRAPH AT					
+	E-1	.04	1	FLOW	32.
				TIME	6.08
					86.
					6.00
ROUTED TO					
+	E5	.04	1	FLOW	31.
				TIME	6.08
					83.
					6.08
HYDROGRAPH AT					

+	E-6	.05	1	FLOW TIME	29. 6.08	87. 6.08
ROUTED TO						
+	E6	.05	1	FLOW TIME	28. 6.08	85. 6.08
HYDROGRAPH AT						
+	E-5	.04	1	FLOW TIME	28. 6.00	82. 6.00
3 COMBINED AT						
+	DPE5	.13	1	FLOW TIME	85. 6.08	241. 6.08
ROUTED TO						
+	E2	.13	1	FLOW TIME	82. 6.08	240. 6.08
HYDROGRAPH AT						
+	E-2	.05	1	FLOW TIME	34. 6.08	102. 6.00
2 COMBINED AT						
+	DPE2	.18	1	FLOW TIME	116. 6.08	336. 6.08
HYDROGRAPH AT						
+	D-1	.06	1	FLOW TIME	36. 6.08	109. 6.08
ROUTED TO						
+	D2	.06	1	FLOW TIME	34. 6.08	107. 6.08
HYDROGRAPH AT						
+	D-2	.04	1	FLOW TIME	23. 6.00	71. 6.00
2 COMBINED AT						
+	DPD2	.10	1	FLOW TIME	56. 6.08	171. 6.08
2 COMBINED AT						
+	DPE-D	.28	1	FLOW TIME	172. 6.08	507. 6.08
ROUTED TO						
+	DBE-D	.28	1	FLOW TIME	13. 7.25	156. 6.33

** PEAK STAGES IN FEET **

1 1 STAGE 6955.33 6957.87
 TIME 7.25 6.33

*** NORMAL END OF HEC-1 ***

F BASINS DETAINED

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
*
CALIFORNIA 95616 *
* RUN DATE 19NOV04 TIME 15:55:15 *
756-1104 *
*
*****
*****

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1
PAGE 1

HEC-1 INPUT

LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
1	ID	Wolf Ranch Master Development Drainage plan									
2	ID	F-Basins future developed condition with detention PN 03094									
3	ID	5-year and 100 Year, 24 hr Type IIA Storm FN: f-DET.dat									
	*DIAGRAM										
4	IT	5	0	0	300						
5	IO	5	0								
6	JR	PREC	.56	1.0							
7	KK	F-8									
8	KM	RUNOFF FOR SUB-BASIN F-8									
9	BA	.0630									
10	IN	15									
11	PB	4.4									
12	PC	0.0000	0.0005	0.0015	0.0030	0.0045	0.0060	0.0080	0.0100	0.0120	0.0143
13	PC	0.0165	0.0189	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	0.0530
14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	0.7900
15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	0.8550
16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	0.8938
17	EC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	0.9270

HEC-1 INPUT

LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
124	KK	DPF12									
125	KM	COMBINE FLOW FROM SUB-BASIN RF-12 RF-12A, AND F-12									
126	HC	3									
127	KK	RF-17									
128	KM	ROUTE FLOW FROM DESIGN POINT F-12 TO DETENTION BASIN DB 18									
129	RD	1600	0.020	0.04		TRAP	15		4		
130	KK	F-17									
131	KM	RUNOFF FOR SUB-BASIN F-17									
132	BA	.0380									
133	LS	0	61.6								
134	UD	.21									
135	KK	F-18									
136	KM	RUNOFF FOR SUB-BASIN F-18									
137	BA	.0980									
138	LS	0	69.7								
139	UD	.21									
140	KK	F-16									
141	KM	RUNOFF FOR SUB-BASIN F-16									
142	BA	.0270									
143	LS	0	69.9								
144	UD	.21									
145	KK	RF-16									
146	KM	ROUTE FLOW FROM SUB-BASIN F-16 TO DETENTION BASIN DB 18									
147	RD	600	0.020	.013		CIRC	2				
148	KK	DPF18									
149	KM	COMBINE FLOW FROM SUB-BASINS F-18, F17, RF-18A, RF-18, RF-17, AND RF-16									
150	KM	THIS IS INFLOW TO DETENTION BASIN F-18									
151	HC	6									
152	KK	DBF18									
153	KM	ROUTE DPF18 THROUGH DETENTION BASIN F-18									
154	KM	THIS IS OUTFLOW FROM DETENTION BASIN F-18									
155	RS	1	ELEV	7140							
156	SV	0	1	4	11	23.5	41				
157	SE	7140	7142	7144	7146	7148	7150				
158	SQ	0	10	55	100	200	300				
159	KK	RF-22A									
160	KM	ROUTE FLOW FROM DESIGN POINT DPF18 TO DESIGN POINT F22									
161	RD	1800	0.027	0.04		TRAP	10		6		
162	KK	F-22									
163	KM	RUNOFF FOR SUB-BASIN F-22									
164	BA	.0640									
165	LS	0	64.1								
166	UD	.21									

HEC-1 INPUT

LINE	ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10
167	KK	DPF22									
168	KM	COMBINE FLOW FROM SUB-BASIN F-22, RF-22 AND RF-22A									
169	HC	3									
170	KK	RF-27									
171	KM	ROUTE FLOW FROM DESIGN POINT DPF22 TO DESIGN POINT F27									
172	RD	3700	0.020	0.04		TRAP	50		3		


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173      KK      F-21
174      KM      RUNOFF FOR SUB-BASIN F-21
175      BA      .0790
176      LS      0      89.1
177      UD      .25

178      KK      RF-26
179      KM      ROUTE FLOW FROM SUB-BASIN F21 TO DESIGN POINT F26
180      RD      1350      .018      .013      CIRC      4

181      KK      F-26
182      KM      RUNOFF FOR SUB-BASIN F-26
183      BA      .0520
184      LS      0      82.0
185      UD      .19

186      KK      DPF26
187      KM      COMBINE FLOW FROM RF-26 AND F-26
188      HC      2

189      KK      RF-26A
190      KM      ROUTE FLOW FROM DESIGN POINT F26 TO DESIGN POINT F27
191      RD      1700      0.022      .013      CIRC      4.5

192      KK      DRF27
193      KM      COMBINE FLOW FROM RF-27B AND RF-26A
194      HC      2

195      KK      RF-27C
196      KM      ROUTE FLOW FROM DESIGN POINT F27 TO DESIGN POINT F28
197      RD      1400      0.019      0.04      TRAP      50      3

198      KK      F-7
199      KM      RUNOFF FOR SUB-BASIN F-7
200      BA      .0782
201      LS      0      61
202      UD      .19

203      KK      RF-7
204      KM      ROUTE FLOW FROM SUB-BASIN F-7 TO DESIGN POINT F14
205      RD      1200      0.033      0.04      TRAP      10      6
                                     HEC-1 INPUT

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1
PAGE 6

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

206      KK      F-14
207      KM      RUNOFF FOR SUB-BASIN F-14
208      BA      .1290
209      LS      0      73.0
210      UD      .23

211      KK      F-6
212      KM      RUNOFF FOR SUB-BASIN F-6
213      BA      .0310
214      LS      0      61
215      UD      .19

216      KK      RF-13
217      KM      ROUTE FLOW FROM SUB-BASIN F-6 TO DESIGN POINT F13
218      RD      800      0.038      0.04      TRAP      10      6

219      KK      F-13
220      KM      RUNOFF FOR SUB-BASIN F-13
221      BA      .0140
222      LS      0      60.7
223      UD      .14

224      KK      DPF13

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277 KK F-30
 278 KM RUNOFF FOR SUB-BASIN F-30
 279 BA .0220
 280 LS 0 72.2
 281 UD .18

 282 KK DPF30
 283 KM COMBINE FLOW FROM RF-30, RF-30A AND F-30
 284 HC 3

 285 KK RF-29
 286 KM ROUTE FLOW FROM DESIGN POINT F30 TO DESIGN POINT F29
 287 RD 2350 0.027 0.04 TRAP 6 3
 HEC-1 INPUT

1
PAGE 8

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
288	KK F-29
289	KM RUNOFF FOR SUB-BASIN F-29
290	BA .0250
291	LS 0 73.0
292	UD .19
293	KK DPF29
294	KM COMBINE FLOW FROM RF-29 AND F-29
295	HC 2
296	KK RF-28
297	KM ROUTE FLOW FROM DESIGN POINT F29 TO DESIGN POINT F28
298	RD 750 0.015 0.04 TRAP 20 3
299	KK F-28
300	KM RUNOFF FOR SUB-BASIN F-28
301	BA .042
302	LS 0 73.0
303	UD .23
304	KK F-27
305	KM RUNOFF FOR SUB-BASIN F-27
306	BA .213
307	LS 0 69.2
308	UD .32
309	KK DPF28
310	KM COMBINE FLOW FROM RF-27C, RF-28, F-28 AND F-27
311	KM THIS IS INFLOW TO DETENTION BASIN F-28
312	HC 4
313	KK DBF28
314	KM ROUTE DPF28 THROUGH DETENTION BASIN F-28
315	KM THIS IS OUTFLOW FROM DETENTION BASIN F-28
316	RS 1 ELEV 6960
317	SV 0 .74 2.72 6.20 10.81 15.88 21.44 27.56 34.39 42.08
318	SV 50.72 60.39 71.09 82.91 95.94 110.43
319	SE 6960 6962 6964 6966 6968 6970 6972 6974 6976 6978
320	SE 6980 6982 6984 6986 6988 6990
321	SQ 0 10 55 100 200 300 550 560 570 580
322	SQ 590 600 610 620 630 640
323	KK RF-31
324	KM ROUTE FLOW FROM DPF TO DESIGN POINT F
325	RD 3500 0.023 0.04 TRAP 20 3
326	KK F-31
327	KM RUNOFF FOR SUB-BASIN F-31
328	BA .081
329	LS 0 65.0
330	UD .24

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
331	KK UP F
332	KM COMBINE FLOW FROM RE-31 AND F-31
333	HC 2
334	ZZ

1

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
CORPS OF ENGINEERS *
* JUN 1998 *
ENGINEERING CENTER *
* VERSION 4.1 *
SECOND STREET *
*
CALIFORNIA 95616 *
* RUN DATE 19NOV04 TIME 15:55:15 *
756-1104 *
*
*****
*****
  
```

Wolf Ranch Master Development Drainage plan
 F-Basins future developed condition with detention PN 03094
 5-year and 100 Year, 24 hr Type IIA Storm FN: f-DET.dat

```

5 IO OUTPUT CONTROL VARIABLES
    IPRNT      5 PRINT CONTROL
    IPLOT      0 PLOT CONTROL
    QSCAL      0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
    NMIN      5 MINUTES IN COMPUTATION INTERVAL
    IDATE     1 0 STARTING DATE
    ITIME     0000 STARTING TIME
    NQ        300 NUMBER OF HYDROGRAPH ORDINATES
    NDDATE    2 0 ENDING DATE
    NDTIME    0055 ENDING TIME
    ICENT     19 CENTURY MARK

    COMPUTATION INTERVAL .08 HOURS
    TOTAL TIME BASE 24.92 HOURS
  
```

```

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE- FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT
  
```

```

JP MULTI-PLAN OPTION
    NPLAN      1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
  
```

RATIOS OF PRECIPITATION
 .56 1.00

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN		RATIOS APPLIED TO PRECIPITATION	
					RATIO 1	RATIO 2
					.56	1.00
HYDROGRAPH AT						
+	F-8	.06	1	FLOW	15.	69.
				TIME	6.17	6.08
ROUTED TO						
+	RF-8	.06	1	FLOW	14.	68.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-1	.17	1	FLOW	10.	110.
				TIME	6.17	6.08
ROUTED TO						
+	RF-3	.17	1	FLOW	10.	106.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-9	.04	1	FLOW	10.	50.
				TIME	6.08	6.08
2 COMBINED AT						
+	DPF9	.21	1	FLOW	18.	152.
				TIME	6.17	6.08
ROUTED TO						
+	RF-19	.21	1	FLOW	17.	147.
				TIME	6.33	6.17
HYDROGRAPH AT						
+	F-19	.10	1	FLOW	38.	144.
				TIME	6.08	6.08
3 COMBINED AT						
+	DPF19	.37	1	FLOW	53.	337.
				TIME	6.25	6.17
ROUTED TO						
+	DBF19	.37	1	FLOW	19.	89.
				TIME	6.67	6.58
				** PEAK STAGES IN FEET **		
				1 STAGE	7142.42	7145.52
				TIME	6.67	6.58
ROUTED TO						
+	RF-22	.37	1	FLOW	19.	89.
				TIME	6.83	6.67
HYDROGRAPH AT						
+	F=2	.04	1	FLOW	3.	29.
				TIME	6.17	6.08
ROUTED TO						
+	RF-10	.04	1	FLOW	3.	28.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-10	.02	1	FLOW	5.	22.

				TIME	6.08	6.08
2 COMBINED AT						
+	DPF10	.06	1	FLOW	6.	48.
				TIME	6.17	6.08
ROUTED TO						
+	RF-18A	.06	1	FLOW	6.	47.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-3	.09	1	FLOW	5.	59.
				TIME	6.17	6.17
ROUTED TO						
+	RF-11	.09	1	FLOW	5.	58.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-11	.05	1	FLOW	11.	53.
				TIME	6.08	6.08
2 COMBINED AT						
+	DPF11	.14	1	FLOW	13.	102.
				TIME	6.17	6.08
ROUTED TO						
+	RF-18	.14	1	FLOW	13.	102.
				TIME	6.25	6.17
HYDROGRAPH AT						
+	F-4	.27	1	FLOW	13.	147.
				TIME	6.25	6.17
ROUTED TO						
+	RF-12	.27	1	FLOW	13.	144.
				TIME	6.33	6.25
HYDROGRAPH AT						
+	F-5	.11	1	FLOW	5.	52.
				TIME	6.33	6.25
ROUTED TO						
+	RF-12A	.11	1	FLOW	5.	51.
				TIME	6.50	6.33
HYDROGRAPH AT						
+	F-12	.06	1	FLOW	13.	66.
				TIME	6.17	6.08
3 COMBINED AT						
+	DPF12	.43	1	FLOW	24.	236.
				TIME	6.25	6.25
ROUTED TO						
+	RF-17	.43	1	FLOW	24.	235.
				TIME	6.42	6.25
HYDROGRAPH AT						
+	F-17	.04	1	FLOW	3.	25.
				TIME	6.17	6.08
HYDROGRAPH AT						
+	F-18	.10	1	FLOW	24.	110.
				TIME	6.17	6.08
HYDROGRAPH AT						
+	F-16	.03	1	FLOW	7.	31.
				TIME	6.17	6.08
ROUTED TO						

+	RF-16	.03	1	FLOW TIME	7. 6.17	30. 6.06
6 COMBINED AT						
+	DPF18	.80	1	FLOW TIME	64. 6.25	509. 6.17
ROUTED TO						
+	DPF18	.80	1	FLOW TIME	26. 6.83	141. 6.75
** PEAK STAGES IN FEET **						
1	STAGE	7142.70	7146.83			
	TIME	6.83	6.75			
ROUTED TO						
+	RF-22A	.80	1	FLOW TIME	26. 6.92	141. 6.83
HYDROGRAPH AT						
+	F-22	.06	1	FLOW TIME	7. 6.17	51. 6.08
3 COMBINED AT						
+	DPF22	1.24	1	FLOW TIME	47. 6.83	238. 6.75
ROUTED TO						
+	RF-27	1.24	1	FLOW TIME	47. 7.00	237. 6.83
HYDROGRAPH AT						
+	F-21	.08	1	FLOW TIME	79. 6.08	184. 6.08
ROUTED TO						
+	RF-26	.08	1	FLOW TIME	77. 6.17	180. 6.08
HYDROGRAPH AT						
+	F-26	.05	1	FLOW TIME	39. 6.08	105. 6.08
2 COMBINED AT						
+	DPF26	.13	1	FLOW TIME	115. 6.08	285. 6.08
ROUTED TO						
+	RF-26	.13	1	FLOW TIME	111. 6.17	279. 6.08
2 COMBINED AT						
+	DPF27	1.37	1	FLOW TIME	111. 6.17	295. 6.42
ROUTED TO						
+	RF-27	1.37	1	FLOW TIME	109. 6.17	294. 6.42
HYDROGRAPH AT						
+	F-7	.08	1	FLOW TIME	5. 6.17	54. 6.08
ROUTED TO						
+	RF-7	.08	1	FLOW TIME	5. 6.25	53. 6.17
HYDROGRAPH AT						
+	F-14	.13	1	FLOW TIME	42. 6.17	162. 6.08

HYDROGRAPH AT						
+	F-6	.03	1	FLOW TIME	2. 6.17	21. 6.08
ROUTED TO						
+	RF-13	.03	1	FLOW TIME	2. 6.25	21. 6.17
HYDROGRAPH AT						
+	F-13	.01	1	FLOW TIME	1. 6.08	11. 6.08
2 COMBINED AT						
+	DPF13	.05	1	FLOW TIME	2. 6.25	30. 6.08
ROUTED TO						
+	RF-14	.05	1	FLOW TIME	2. 6.92	30. 6.33
3 COMBINED AT						
+	DPF14	.25	1	FLOW TIME	45. 6.17	210. 6.17
ROUTED TO						
+	RF-25	.25	1	FLOW TIME	44. 6.33	209. 6.25
HYDROGRAPH AT						
+	F-25	.09	1	FLOW TIME	27. 6.17	106. 6.17
2 COMBINED AT						
+	DPF25	.34	1	FLOW TIME	66. 6.25	303. 6.25
ROUTED TO						
+	RF-30	.34	1	FLOW TIME	67. 6.33	304. 6.25
HYDROGRAPH AT						
+	F-15	.02	1	FLOW TIME	6. 6.08	26. 6.08
ROUTED TO						
+	RF-23	.02	1	FLOW TIME	5. 6.17	25. 6.08
HYDROGRAPH AT						
+	F-23	.03	1	FLOW TIME	12. 6.08	44. 6.08
2 COMBINED AT						
+	DPF23	.05	1	FLOW TIME	16. 6.17	69. 6.08
ROUTED TO						
+	RF-24	.05	1	FLOW TIME	15. 6.25	66. 6.17
HYDROGRAPH AT						
+	F-24	.09	1	FLOW TIME	32. 6.17	115. 6.17
2 COMBINED AT						
+	DPF24	.14	1	FLOW TIME	44. 6.25	181. 6.17
ROUTED TO						
+	RF-30	.14	1	FLOW TIME	42. 6.25	173. 6.17

HYDROGRAPH AT						
+	F-30	.02	1	FLOW	8.	30.
				TIME	6.08	6.08
3 COMBINED AT						
+	DPF30	.50	1	FLOW	112.	490.
				TIME	6.33	6.25
ROUTED TO						
+	RF-29	.50	1	FLOW	109.	486.
				TIME	6.42	6.25
HYDROGRAPH AT						
+	F-29	.03	1	FLOW	9.	35.
				TIME	6.08	6.08
2 COMBINED AT						
+	DPF29	.53	1	FLOW	112.	507.
				TIME	6.42	6.25
ROUTED TO						
+	RF-28	.53	1	FLOW	112.	489.
				TIME	6.42	6.25
HYDROGRAPH AT						
+	F-28	.04	1	FLOW	14.	53.
				TIME	6.17	6.08
HYDROGRAPH AT						
+	F-27	.21	1	FLOW	38.	183.
				TIME	6.25	6.17
4 COMBINED AT						
+	DPF28	2.15	1	FLOW	231.	983.
				TIME	6.33	6.25
ROUTED TO						
+	DFE28	2.15	1	FLOW	112.	558.
				TIME	6.75	6.67
				** PEAK STAGES IN FEET **		
				1 STAGE	6966.24	6973.52
				TIME	6.75	6.67
ROUTED TO						
+	RF-31	2.15	1	FLOW	112.	578.
				TIME	6.92	6.50
HYDROGRAPH AT						
+	F-31	.08	1	FLOW	10.	64.
				TIME	6.17	6.17
2 COMBINED AT						
+	DF F	2.23	1	FLOW	114.	600.
				TIME	6.92	6.50

1

*** NORMAL END OF HEC-1 ***

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1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
609 SECOND STREET *
*
DAVIS, CALIFORNIA 95616 *
* RUN DATE 21MAY04 TIME 13:22:20 *
(916) 756-1104 *
*
*****
*****

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G BASINS DETAINED

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT
PAGE 1

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LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10 /
1 ID Wolf Ranch Master Development Drainage Plan
2 ID G Basins Future developed condition with detention PN
03094
3 ID 5-year and 100 Year, 24 hr Type IIA Storm FN G-det.dat
*DIAGRAM
4 IT 5 0 0 300
5 IO 4 0
6 JR PREC .56 1.0
7 KK G-1
8 KM RUNOFF - Sub-basin G-1
9 BA .0808
10 IN 15
11 PB 4.4
0.0143 12 PC 0.0000 0.0005 0.0015 0.0030 0.0045 0.0060 0.0080 0.0100 0.0120

```

0.0530	13	PC	0.0165	0.0188	0.0210	0.0233	0.0255	0.0278	0.0320	0.0390	0.0460	
0.7900	14	PC	0.0600	0.0750	0.1000	0.4000	0.7000	0.7250	0.7500	0.7650	0.7800	
0.8550	15	PC	0.8000	0.8100	0.8200	0.8250	0.8300	0.8350	0.8400	0.8450	0.8500	
0.8938	16	PC	0.8600	0.8638	0.8675	0.8713	0.8750	0.8788	0.8825	0.8863	0.8900	
0.9270	17	PC	0.8975	0.9013	0.9050	0.9083	0.9115	0.9148	0.9180	0.9210	0.9240	
0.9525	18	PC	0.9300	0.9325	0.9350	0.9375	0.9400	0.9425	0.9450	0.9475	0.9500	
0.9775	19	PC	0.9550	0.9575	0.9600	0.9625	0.9650	0.9675	0.9700	0.9725	0.9750	
0.9913	20	PC	0.9800	0.9813	0.9825	0.9838	0.9850	0.9863	0.9875	0.9888	0.9900	
	21	PC	0.9925	0.9938	0.9950	0.9963	0.9975	0.9988	1.0000			
	22	LS	0	61								
	23	UD	0.22									
	24	KK	G2									
	25	KM		ROUTE FLOW from SUB-BASIN G-1 TO DP G3								
	26	RD	3200	0.027	0.04		TRAP	10		4		
	27	KK	G-2									
	28	KM		RUNOFF - Sub-basin G-2								
	29	BA	.035									
	30	LS	0	73								
	31	UD	0.22									
	32	KK	G3									
	33	KM		ROUTE FLOW from SUB-BASIN G-2 TO DP G3								
	34	RD	2730	0.024	0.04		TRAP	10		4		
	35	KK	G-3									
	36	KM		RUNOFF - Sub-basin G-3								
	37	BA	.177									
	38	LS	0	73								
	39	UD	0.29									
	40	KK	DPG3									
	41	KM		COMBINE RUNOFF from G2, G3 AND SUB-BASIN G-3								
	42	HC	3									

1
PAGE 2

HEC-1 INPUT

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43	KK	G5									
44	KM		ROUTE FLOW from DP G3 TO DP G5								
45	RD	2200	0.02	.013			CIRC		4.5		
46	KK	G-5									
47	KM		RUNOFF - Sub-basin G-5								
48	BA	.153									
49	LS	0	78.4								
50	UD	0.26									
51	KK	DPG									
52	KM		COMBINE RUNOFF from G5 AND SUB-BASIN G-5								
53	HC	2									
54	KK	DB G									
55	KM		DESIGN POINT G NTO DETENTION BASIN G								
56	KM		THIS IS THE OUTFLOW FROM DETENTION BASIN G								
57	RS	1	ELEV	0							
58	SQ	0	10	15	130	220	250				
59	SE	0	2	4	6	8	10				
60	SV	0	5.0	9.3	17.0	24.6	33.0				

1

61 ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE      (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.       (.) CONNECTOR  (<---) RETURN OF DIVERTED OR PUMPED FLOW

  7      G-1
        V
        V
  24      G2
        .
        .
  27      .      G-2
        .      V
        .      V
  32      .      G3
        .      .
        .      .
  35      .      .      G-3
        .      .      .
        .      .      .
  40      DPG3.....
        V
        V
  43      G5
        .
        .
  46      .      G-5
        .      .
        .      .
  51      DPG.....
        V
        V
  54      DB G

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
U.S. ARMY CORPS OF ENGINEERS *
* JUN 1998 *
HYDROLOGIC ENGINEERING CENTER *
* VERSION 4.1 *
609 SECOND STREET *
*
DAVIS, CALIFORNIA 95616 *
* RUN DATE 21MAY04 TIME 13:22:20 *
(916) 756-1104 *
*
*****
*****

```

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	RATIO 2
				.56	1.00

HYDROGRAPH AT

+	G-1	.08	1	FLOW TIME	5. 6.17	50. 6.17
ROUTED TO						
+	G2	.08	1	FLOW TIME	4. 6.58	50. 6.25
HYDROGRAPH AT						
+	G-2	.04	1	FLOW TIME	12. 6.17	45. 6.08
ROUTED TO						
+	G3	.04	1	FLOW TIME	12. 6.33	44. 6.25
HYDROGRAPH AT						
+	G-3	.18	1	FLOW TIME	50. 6.17	200. 6.17
3 COMBINED AT						
+	DPG3	.29	1	FLOW TIME	57. 6.25	278. 6.25
ROUTED TO						
+	G5	.29	1	FLOW TIME	55. 6.33	277. 6.25
HYDROGRAPH AT						
+	G-5	.15	1	FLOW TIME	74. 6.17	230. 6.17
2 COMBINED AT						
+	DPG	.45	1	FLOW TIME	120. 6.17	489. 6.17
ROUTED TO						
+	DB G	.45	1	FLOW TIME	11. 8.25	140. 6.67
** PEAK STAGES IN FEET **						
	1			STAGE TIME	2.54 8.25	6.22 6.67

1

*** NORMAL END OF HEC-1 ***

000000

APPENDIX B

HYDRAULIC CALCULATIONS

BASIN 'A' HYDRAULICS

PRELIMINARY DETENTION BASIN SIZES

- Detention Basin "A"

- historic data $Q_5 = \frac{11}{39}$ $Q_{100} = \frac{157}{244}$

$TBA = .42 \text{ SM} = 270 \text{ Ac}$

$CN = 61$ RUNOFF $5 \text{ yr} = .2''$
 $100 \text{ yr} = 1.02''$

- "Developed": $Q_5 = \frac{206}{221} \text{ cfs}$ $Q_{100} = \frac{722}{584} \text{ cfs}$

$TBA = .57 \text{ SM} = 365 \text{ Ac}$

Wtd CN = $[61(62) + .15(76) + .08(79) + .05(78.2) + .03(71.8)$
 $+ .067(72.1) + .111(77.2) + .001(61)]$

$\div (.57) = 73.9 \text{ } \approx 74$

RUNOFF: $5 \text{ yr} = .6''$
 $100 \text{ yr} = 1.90''$

- RAINFALL 5-year = 2.5"
 100-year = 4.4"

- Existing 'A' BASIN VOLUME

$Vol(5) = 270 \text{ Ac} (.2/12) = 4.5 \text{ AF}$

$Vol(100) = 270 \text{ Ac} (1.02/12) = 23.0 \text{ AF}$

- DEVELOPED 'A' BASIN VOLUME

$Vol(5) = 365 (.6/12) = 18.6 \text{ AF}$

$Vol(100) = 365 (1.90/12) = 57.8 \text{ AF}$

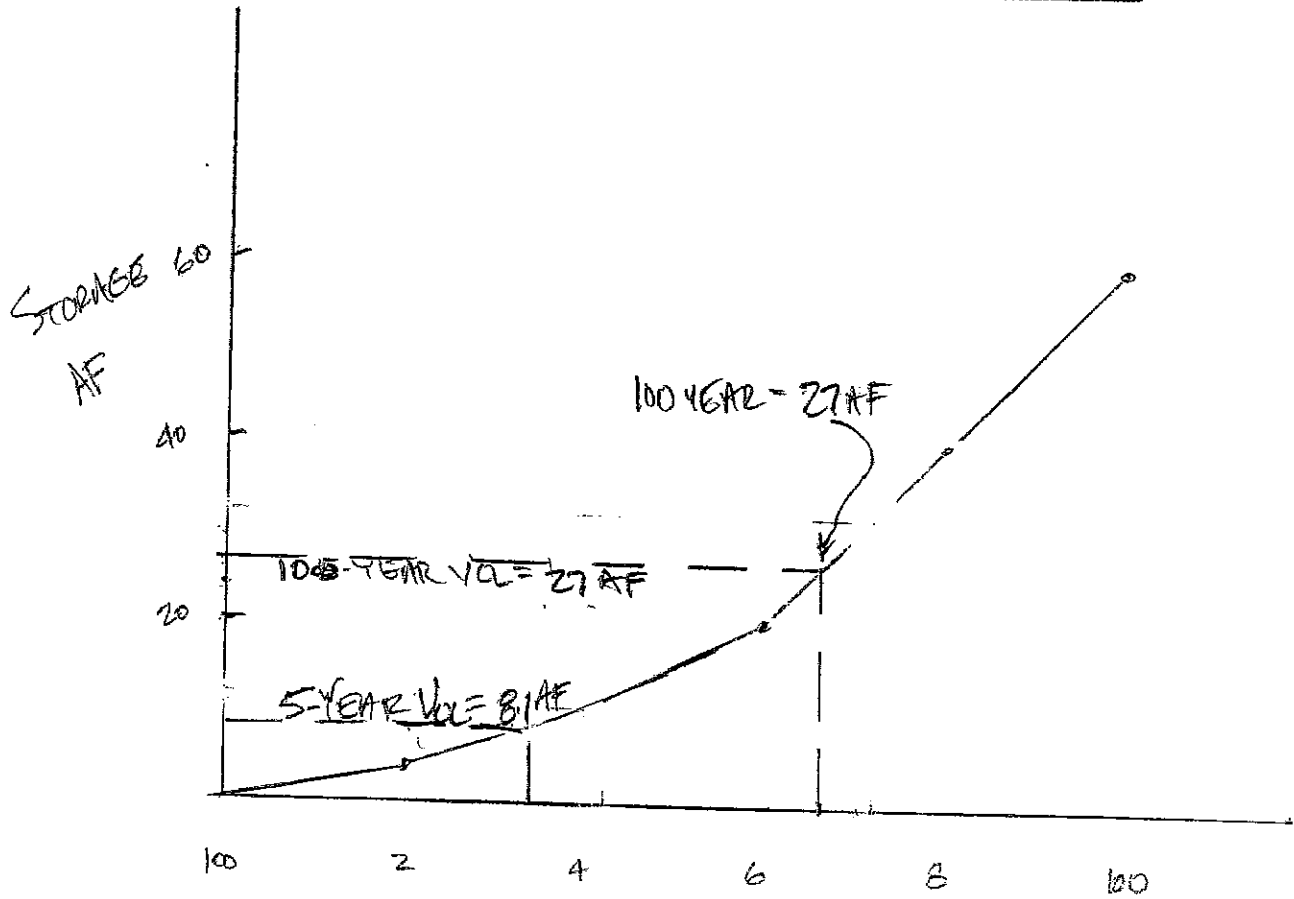
$\Delta = 14.1 \text{ AF } 5 \text{ YEAR}$
 $34.8 \text{ AF} = 100 \text{ YR}$

Detention Basin 'A'

DETAINED FLOW

$Q_{100} = 28 \text{ cfs}$

$Q_{100} = 166 \text{ cfs}$



W/LQ \approx 5-YEAR

TOTAL $V_{100} = 32 \text{ AF} + 12 = \underline{\underline{44 \text{ AF}}}$

OUTLET CULVERT FROM
DET. BASIN A Q = 166 cfs¹

CURRENT DATE: 05-14-2004
CURRENT TIME: 14:35:17

FILE DATE: 05-14-2004
FILE NAME: A5

***** FHWA CULVERT ANALYSIS *****
***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	97.00	200.02	1 RCB	5.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

***** SUMMARY OF CULVERT FLOWS (CFS) FILE: A5 DATE: 05-14-2004 *****

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
101.21	17	17	0	0	0	0	0	0	1
101.91	34	34	0	0	0	0	0	0	1
102.49	51	51	0	0	0	0	0	0	1
103.01	68	68	0	0	0	0	0	0	1
103.49	85	85	0	0	0	0	0	0	1
103.95	102	102	0	0	0	0	0	0	1
104.42	119	119	0	0	0	0	0	0	1
104.91	136	136	0	0	0	0	0	0	1
105.43	153	153	0	0	0	0	0	0	1
105.86	166	166	0	0	0	0	0	0	1
110.00	261	261	0	0	0	0	0	0	1

***** SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: A5 DATE: 05-14-2004 *****

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
101.21	0.00	17	0	0.00
101.91	0.00	34	0	0.00
102.49	0.00	51	0	0.00
103.01	0.00	68	0	0.00
103.49	0.00	85	0	0.00
103.95	0.00	102	0	0.00
104.42	0.00	119	0	0.00
104.91	0.00	136	0	0.00
105.43	0.00	153	0	0.00
105.86	0.00	166	0	0.00

<1> TOLERANCE (FT) = 0.010
<2> TOLERANCE (%) = 1.000

CURRENT DATE: 05-14-2004
 CURRENT TIME: 14:35:17

FILE DATE: 05-14-2004
 FILE NAME: A5

 ***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
 BOTTOM WIDTH (FT) 10.00
 SIDE SLOPE H/V (X:1) 4.0
 CHANNEL SLOPE V/H (FT/FT) 0.025
 MANNING'S N (.01-0.1) 0.035
 CHANNEL INVERT ELEVATION (FT) 97.00
 CULVERT NO.1 OUTLET INVERT ELEVATION 97.00 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	97.00	0.000	0.00	0.00
17.00	97.42	0.931	3.44	0.66
34.00	97.63	0.962	4.33	0.98
51.00	97.79	0.977	4.92	1.23
68.00	97.92	0.987	5.38	1.44
85.00	98.04	0.994	5.76	1.63
102.00	98.15	0.999	6.08	1.79
119.00	98.25	1.003	6.36	1.95
136.00	98.34	1.007	6.61	2.09
153.00	98.42	1.010	6.84	2.22
166.00	98.49	1.012	7.00	2.32

 ***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE	GRAVEL
EMBANKMENT TOP WIDTH (FT)	20.00
CREST LENGTH (FT)	100.00
OVERTOPPING CREST ELEVATION (FT)	110.00

BASIN 'A'

OUTFALL CHANNELS.

- Try to achieve Velocity 5-year 5fps or less
- 100 year Velocity < 7 fps for grasslined

OUTFALL
- Channel A3

$$Q_5 = 3 + 64 = 67 \text{ cfs}$$

$$Q_{100} = \text{SB A1} + \text{SB A3}$$

$$Q_{100} = 32 + 223 = 255 \text{ cfs}$$

conservative

- Existing slope DP A1 → A3

$$L = 3700' \quad \Delta H = 7228 - 7086 = 142'$$

$$\text{Slope} = 142/3700 = 3.8\%$$

@ slope = 3.8% $V_5 = 6.5 \text{ fps}$ no good.

if slope = 1.7% $V_5 = 4.9 \text{ mph}$

$V_{100} = 7.0 \text{ (ps.) mph}$) SEE 2 + 3 of 3

Required grade control:

$$L = 3700' \quad \Delta S = .038 - .017 = .021$$

$$H = 77.7' \quad \text{See 7B}$$

w/ 3' each check / drop = 26 checks

$$\text{Spacing} = 3700/26 = \underline{\underline{142'}}$$

Wolf Ranch MDDP
Swale Capacity Calculation

Zof3

Structure A3: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	67 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	1.7 %
Depth of Flow	1.10 ft	Manning's Roughness Coef.	0.035

Channel Area	15.8 sf
Channel Wetted Perimeter	19.1 ft
Hydraulic Radius	0.83 ft

Channel Flow Velocity	4.9 ft/sec
Channel Flow Capacity	78 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	2.2 ft
Top Width	27.8 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d\sqrt{1+z^2}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

Wolf Ranch MDDP

Swale Capacity Calculation

Structure A3: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	255 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	1.7 %
Depth of Flow	2.10 ft	Manning's Roughness Coef.	0.035

Channel Area	38.6 sf
Channel Wetted Perimeter	27.3 ft
Hydraulic Radius	1.41 ft

Channel Flow Velocity	7.0 ft/sec
Channel Flow Capacity	270 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	3.3 ft
Top Width	36.6 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d*(1+z²)^{0.5}

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R_n^{2/3} S^{1/2}

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR_n^{2/3} S^{1/2}

Freeboard = 1.0 + 0.025(v)d^{0.33}

OUTFALL CHANNEL AB.

Flow ranges Δ AB \rightarrow ^{SB} AB

$$Q_5 = 112 + 22 = 134 \text{ cfs}$$

$$Q_{100} = 371 + 66 = 437 \text{ cfs}$$

Existing Slope AB \rightarrow AB

$$L = 1600' \quad \Delta H = 7086 - 7036 = 50'$$

$$S = 50/1600 = .03125 \%$$

$$V_5 @ S = .03125\% \quad 6.9 \text{ is no good}$$

$$@ \text{ Slope} = 1.4\%$$

$$V_5 = 4.9 \text{ fps is ok}$$

$$V_{100} = 7.1 \text{ (ps, close, is ok)}$$

Required grade control.

$$L = 1600' \quad \Delta S = .03125 - .014 = .01725$$

$$H \& \text{ drops} = 1600(.01725) = 27.6', \text{ say } 27$$

w/ 3' each, need 9 drops/checks

$$\text{Spacing } 1600/27 = 60'$$

Spacing is way to close.

If sloping boulder drops used, 6' drop each

∴ spacing increased to 120'

need 14 drops

Still to close:

go to riprap side slopes.

make $V_s = 7$ fps

w/ BW = 10', slope = 2.790

Surpuser $\left\{ \begin{array}{l} V_s = 6.9 \text{ fps.} \\ V_{100} = 9.5 \\ d_{100} = 3.7 \text{ (w/ FB)} \end{array} \right.$
 3+484

Riprap size

$$\frac{V_s^{1.7}}{1.36} = \frac{9.5(.027)^{1.7}}{1.36} = 3.8 \text{ Type L, close to M, use M.}$$

Required grade control

$$\Delta S = .03125 - .027 = .00425$$

$$\text{Total H} = .00425(1600) = 6.8, \text{ say } 6$$

\therefore need 2 x 3' drops

$$\text{Spacing} = 1600 / 2 = 800'$$

3/4

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure A6: Riprap channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	134 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	2.7 %
Depth of Flow	1.35 ft	Manning's Roughness Coef.	0.035

Channel Area	20.8 sf
Channel Wetted Perimeter	21.1 ft
Hydraulic Radius	0.98 ft

Channel Flow Velocity	6.9 ft/sec
Channel Flow Capacity	144 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.54 ft
Top Width	30.3 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b+2d*(1+z²)^{0.5}

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R_n^{2/3} S^{1/2}

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR_n^{2/3} S^{1/2}

Freeboard = 1.0+0.025(v)d^{0.33}

Wolf Ranch MDDP Swale Capacity Calculation

Structure A6: Riprap channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	437 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	2.7 %
Depth of Flow	2.40 ft	Manning's Roughness Coef.	0.035

Channel Area	47.0 sf
Channel Wetted Perimeter	29.8 ft
Hydraulic Radius	1.58 ft

Channel Flow Velocity	9.5 ft/sec
Channel Flow Capacity	446 cfs
Capacity Check	Okay

Freeboard	1.3 ft
Swale Depth	3.72 ft
Top Width	39.7 ft

Equations:

$$\text{Area (A)} = b(d)$$

$$b = \text{width}$$

$$d = \text{depth}$$

$$\text{Perimeter (P)} = b + 2d(1+z^2)^{0.5}$$

$$z = \text{side slope}$$

$$\text{Hydraulic Radius} = A/P$$

$$\text{Velocity} = (1.49/n)R_n^{2/3} S^{1/2}$$

$$\text{Slope (S)} = \text{Slope of the channel}$$

$$n = \text{Manning's number}$$

$$R_n = \text{Hydraulic Radius (Reynold's Number)}$$

$$\text{Flow} = (1.49/n)AR_n^{2/3} S^{1/2}$$

$$\text{Freeboard} = 1.0 + 0.025(v)d^{0.33}$$

OUTFALL CHANNEL A5

Flow range A6 + SB A5

$$Q_5 = 157 + 57 = 214 \text{ cfs}$$

$$Q_{100} = 498 + 184 = 682 \text{ cfs}$$

Existing slope A6 \rightarrow use of detention basin 'A'

$$\Delta H = 7036 - 6994 = 42' \quad L = 1750'$$

$$\text{Slope} = 42/1750 = .024'/1'$$

Use riprap:

$$\begin{aligned} \text{e Slope} = 2.4\% \quad V_5 = 7.1 \text{ fps close to de} \\ V_{100} = 10.0 \text{ fps} \end{aligned} \left. \begin{array}{l} \\ \\ \end{array} \right\} \begin{array}{l} \text{see} \\ 295 \text{ of } 3 \end{array}$$

$$\text{Riprap Size} = \frac{10(.024)^{.17}}{1.36} = 3.9 \text{ use } \underline{\text{Type 'M'}}$$

Wolf Ranch MDDP
Swale Capacity Calculation

Structure A5: Riprap channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	214 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.4 %
Depth of Flow	1.45 ft	Manning's Roughness Coef.	0.035

Channel Area	30.2 sf
Channel Wetted Perimeter	27.0 ft
Hydraulic Radius	1.12 ft

Channel Flow Velocity	7.1 ft/sec
Channel Flow Capacity	214 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.65 ft
Top Width	36.2 ft

Equations:

$$\text{Area (A)} = b(d)$$

$$b = \text{width}$$

$$d = \text{depth}$$

$$\text{Perimeter (P)} = b + 2d(1+z^2)^{0.5}$$

$$z = \text{side slope}$$

$$\text{Hydraulic Radius} = A/P$$

$$\text{Velocity} = (1.49/n)R_n^{2/3} S^{1/2}$$

$$\text{Slope (S)} = \text{Slope of the channel}$$

$$n = \text{Manning's number}$$

$$R_n = \text{Hydraulic Radius (Reynold's Number)}$$

$$\text{Flow} = (1.49/n)AR_n^{2/3} S^{1/2}$$

$$\text{Freeboard} = 1.0 + 0.025(v)d^{0.33}$$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure A5: Riprap channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	682 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.4 %
Depth of Flow	2.70 ft	Manning's Roughness Coef.	0.035

Channel Area	69.7 sf
Channel Wetted Perimeter	37.3 ft
Hydraulic Radius	1.87 ft

Channel Flow Velocity	10.0 ft/sec
Channel Flow Capacity	697 cfs
Capacity Check	Okay

Freeboard	1.3 ft
Swale Depth	4.05 ft
Top Width	47.4 ft

Equations:

Area (A) = b(d)
 b = width
 d = depth

Perimeter (P) = b + 2d*(1+z²)^{0.5}
 z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R_n^{2/3} S^{1/2}

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR_n^{2/3} S^{1/2}

Freeboard = 1.0 + 0.025(v)d^{0.33}

Channel #10

$Q_5 = 28 \text{ cfs}$
 $Q_{100} = 165 \text{ cfs}$ } outlet side of detention basin 'A'

$L = 400'$ design slope = $12/400 = 3.0\%$

design for Q_{100} only

$V_{100} = 7.6 \text{ fps}$ from swale calcs (see 2/2)

$$VS^{.17} / 1.36 = \frac{7.6(603)^{.17}}{1.36} = 3.07 \text{ use Type 'L'}$$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure A10: Riprap channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	165 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	3.0 %
Depth of Flow	1.45 ft	Manning's Roughness Coef.	0.035

Channel Area	22.9 sf
Channel Wetted Perimeter	22.0 ft
Hydraulic Radius	1.04 ft

Channel Flow Velocity	7.6 ft/sec
Channel Flow Capacity	174 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.66 ft
Top Width	31.3 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d*(1+z²)^{0.5}

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R_n^{2/3} S^{1/2}

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR_n^{2/3} S^{1/2}

Freeboard = 1.0 + 0.025(v)d^{0.33}

Outfall Storm Sewers

Assume all Storm Sewers @ 2.0% PEP

Outfall Storm Sewer A4

$Q_{100} = 509 \text{ cfs (DP A3)}$

@ 2.4%, $Q = 520 \text{ cfs for } 60" \text{ PEP} \therefore \underline{\underline{\text{ok}}}$

Storm Sewer A7

$Q_{100} = 90 \text{ cfs}$

@ 2.0%, $Q = 94 \text{ cfs for } 36" \text{ PEP} \therefore \underline{\underline{\text{ok}}}$

Storm Sewer A9

$Q_{100} = 76 \text{ cfs}$

use 1.0% since grade may be a problem

\therefore @ 1.3%, $Q = 73 \text{ cfs for } 36" \text{ PEP} \therefore \underline{\underline{\text{ok}}}$

Storm Sewer Segment 'A3' TO Braggate Blvd.

$Q_{100} = 223 \text{ cfs}$

18" @ 2.4% $Q_{full} = 223 \text{ cfs} \therefore \underline{\underline{\text{ok}}}$

Storm Sewer A4-1 @ DP A4-1

$Q_{100} = 288 \text{ cfs}$

@ 2.0%, 54" PEP $Q_{full} = 292 \text{ cfs} \therefore \underline{\underline{\text{ok}}}$

Storm Sewer A-11 @ SB A-11

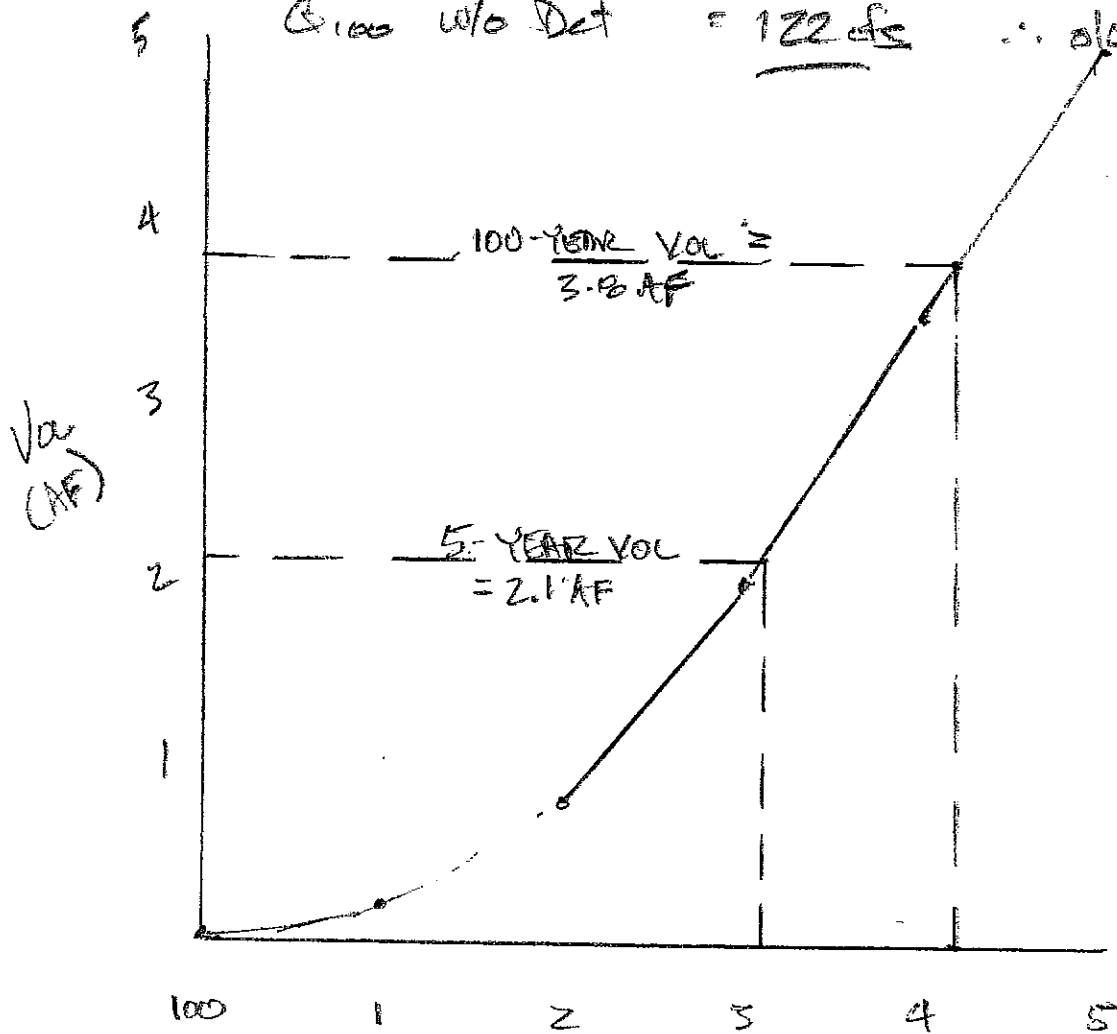
$$Q_{100} = 140 \text{ cfs}$$

$$42" \text{ RCP @ } 2.0\% \text{ } C_{op} = 142 \text{ cfs } \underline{\underline{si \text{ } dc}}$$

May not need to detain because ex 54" rep has adequate capacity to pickup 100 year developed flow:

$Q_{coop} \text{ 54" Rep @ 1.0\%} = 200 \text{ cfs}$

$Q_{100} \text{ w/o Det} = \underline{122 \text{ cfs}} \therefore \text{ok.}$



W/ WQ = 5 YEAR VOL

TOTAL VOL = 3.8 + 2.1 = 5.9 AF

Detention "Basin" E/D

- Historic Data:

$$BA = .164 \text{ SM (SIS'E')} + .32 \text{ SM (DP DZ)} = .48 \text{ SM} = 307 \text{ A}$$

$$CN = 61 \quad \text{Runoff } S_{5r} = .2'' \quad 100yr = 1.02''$$

D Basin Ex $Q_5 = 10$; $Q_{100} = 103$ E-BASIN Ex; $Q_5 = 6$ $Q_{100} = 66$

- Developed Data: Total E/D: $Q_5 = 16$ $Q_{100} = 169$

$$BA = .10 \text{ SM (DP'DZ')} + .18 \text{ (DP'E2)} = .28 \text{ SM} = 179 \text{ Ac}$$

$$CN = \frac{.04(81.8) + .04(79) + .062(78.1) + .052(79) + .036(79)}{.28} = 79.2$$

- Empty E/D Basin Volume of Runoff

$$Vol(5) = 307 (.2/12) = 5.2 \text{ AF}$$

$$Vol(100) = 307 (1.02/12) = 26.1 \text{ AF}$$

- Developed E/D Volume of Runoff

$$\text{Runoff } S_{5\text{-year}} = .84'' \quad 100\text{-year} = 2.29''$$

$$Vol 5 = 179 (.84/12) = 12.5 \text{ AF}$$

$$Vol 100 = 179 (2.29/12) = 34.2 \text{ AF}$$

- Required Storage

$$\Delta Vol 5 = 12.5 - 5.2 = 7.3 \text{ AF}$$

$$\Delta Vol 100 = 34.2 - 26.1 = 8.1 \text{ AF}$$

- Required Storage Volume

Vol 5-year = $18.6 - 4.5 = 14.1$ AF

Vol 100-year = $57.8 - 23.0 = 34.8$ AF

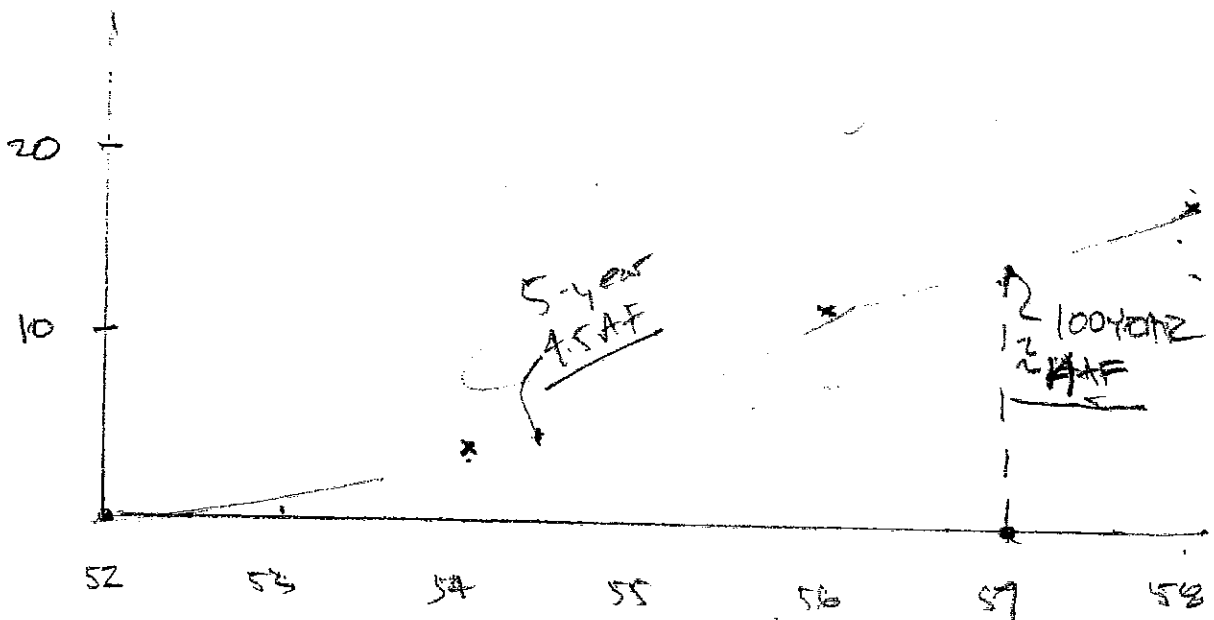
Above values are conservative & do not include channel storage due to routing.

- INFLOW TO DET. BASIN

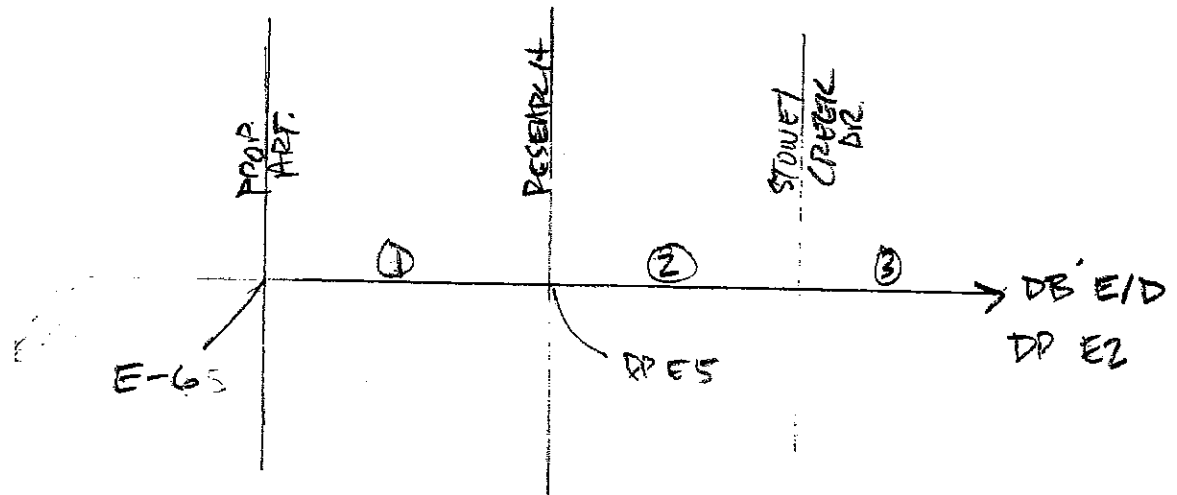
$Q_5 = 173$ cfs $Q_{100} = 509$ cfs

- Allowable Release Rates

$Q_5 = 16$ cfs $Q_{100} = 169$ cfs.



'E/D' BASIN HYDRAULICS
Outfall Storm Sewer Sizing
 East Outfall to Detention Basin 'E/D'



Flow Summary

	Q _s	Q ₁₀₀
c E-6	29	87
c DP ES	85	241
c Stony Creek	95	270
c DB E/D	116	336

Segment 1 EG to Research Parkway

En grade slope along prop Road = $40/300 = .03\%$

use 2.5% \dot{i} pick up 100-year

\therefore 36" RCP @ 2% = 94 cfs \therefore 0.6

Segment 2 Research to Stony Creek $Q_{100} = 241$ cfs
 use slope of Pony Creek Street $4/140 = .029\%$
 use slope of 2.4%

\therefore 48" DEP @ $2.4\% = 227$ cfs. probability ok since slope can probably be made steeper than 2.4%

Segment 3 Stony Creek to DB ED

$Q_{100} = 270$

use slope from DB to int of Abby Rd & Pony Creek
 elev @ DB = 52.0 est. elev of int. @ intersection = 60
 \therefore slope = $60 - 52 / 350 = .023\%$

- check Pony Creek $6/330 = .019\%$, use $.018\%$

60" DEP @ $.018 = Q = 349$; too much

54" DEP @ $.018 = 264$ cfs, probability ok (Seg 3A)

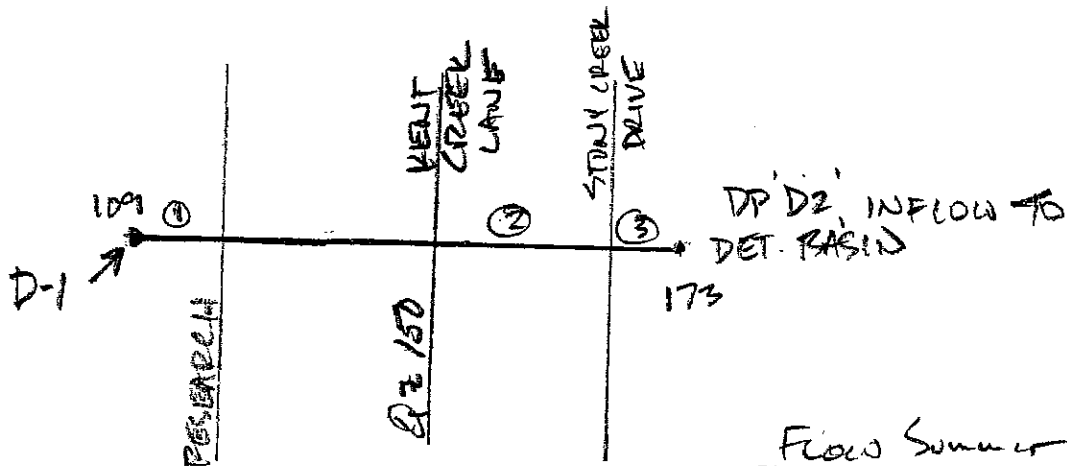
Seg 3b (Abby Road Lane) $Q = 336$

54" @ $2.3\% Q = 305$ cfs no good

60" @ $2.3\% Q = 404$ ok

Outfall Storm Sewer Sizing

Wet outfall to Detention Basin E/D



Flow Summary

e D-1	36	109
e DP D2	57	173

Segment 1 : $Q = 109$ cfs

assume minimum slope of 2% across Research

∴ Need 42" RCP $Q = 142$ cfs ←

36" RCP $Q = 94$ cfs ∴ no good

Segment 2 : Kent Creek Drive to Stony Creek $Q = 150$ cfs.

use slope of Connet Lane, 2%

48" RCP @ 2% = 203 cfs ; ample. ←

42" RCP @ 2% = 140 ∴ no good

Segment 3:

Stoney Creek to Rd. Basin E/D

$$Q = 170 \text{ cfs}$$

Bottom of Pond @ 52 ± . L = 160'

appears the slope will be 2 2/120 = .0167% say
.016

$$48'' \text{ dia } Q @ 1.5\% = 182 \text{ cfs } \therefore \text{ok.}$$

RAIN F HYDRAULICS

Tramway Culverts (See HYB results)

- DP F9 $Q_{100} = 152 \text{ cfs}$ $L = 80'$
 $H_w/D = 4.2/4 = 1.05 \therefore \text{ok } 4' \times 6' \text{ CRC}$

- SB F8 $Q_{100} = 64 \text{ cfs}$ $L = 80'$
 $H_w/D = 3.8/4 = .95 \therefore \text{ok } 48" \text{ RCP}$

DP F10 $Q_{100} = 48 \text{ cfs}$ $L = 80'$
 $H_w/D = 3.3/3.5 = .94 \therefore \text{ok } 42" \text{ RCP}$

DP F11 $Q_{100} = 102 \text{ cfs}$ $L = 80'$
 $H_w/D = 4.25/4 = 1.06 \therefore \text{ok } 4' \times 4' \text{ CRC}$

DP F12 $Q_{100} = 236 \text{ cfs}$ $L = 80'$
 $H_w/D = 4/4 = 1 \therefore \text{ok } 4' \times 10' \text{ CRC}$

SB F15 $Q_{100} = 4 \text{ cfs}$ use 18" RCP

DP F13 $Q_{100} = 30 \text{ cfs}$ $L = 80'$
 $H_w/D = 2.7/3 = .9 \therefore \text{ok use } 36" \text{ RCP}$

~~SB F20 (Briarpatch Blvd)~~ $Q_{100} = 140 \text{ cfs}$ $L = 160'$
 ~~$H_w/D = 3.7/4 = 1.0 \therefore \text{ok use } 4' \times 6' \text{ CRC}$~~

Roadway Culverts Contd.

DB 19 : This is outlet of Det. Basin 19 $L = 240' \pm$
 $Q_{100} \text{ out} = 89 \text{ cfs.}$

Assume Hw depth of 7' can be obtained
 w/ 42" RCP, $Hw/D = 6.6/3.5 = 1.9.$

6.6' Hw depth consistent w/ DB 19 Hw requirements.

DB 18 : This is outlet of Det. Basin 18, $L = 240' \pm$
 $Q_{100} \text{ out} = 141 \text{ cfs}$

Assume Hw depth $\approx 7'$, same as DB 19
 w/ 48" RCP, $Hw = 7.5' \therefore \text{OK.}$

$Hw/D = 7.5/4 = 1.88$

DP F23 : $Q_{100} = 169 \text{ cfs}$ $L = 160'$
 (Briargate)

$Hw/D = 3.8/4 = .95 \therefore \text{use } 48" \text{ RCP.}$

DP F14 : $Q_{100} = 210 \text{ cfs}$ $L = 160'$

$Hw/D = 4.35/4 = 1.08 \therefore \text{OK use } 4' \times 8' \text{ CBL}$

DP F24 : $Q_{100} = 181 \text{ cfs}$ $L = 80'$

$Hw/D = 3.9/4 = .98 \therefore \text{OK use } 4' \times 8' \text{ CBL}$

DP F25: $Q_{100} = 303 \text{ cfs}$ $L = 80'$
 $HW/D = 4.75/5 = .94 \therefore \text{ok}$ $5' \text{H} \times 10' \text{W} \text{CBL}$

DP F30: $Q_{100} = 490 \text{ cfs}$ $L = 80'$
 $HW/D = 6.6/6 = 1.10 \therefore \text{ok}$ use $6' \times 10' \text{ CBL}$

DP F28: This is outlet from Det Basin DB 28 e $L = 240' \pm$
Research Parkway
Assume HW depth of $16'$ to match HEC-1
 $Q_{100} = 563 \text{ cfs}$
w/ $4' \times 8' \text{ CBL}$ $HW = 16.5' \therefore \text{ok}$
use $4' \times 8' \text{ CBL}$

AT DT F9 upper collector

CURRENT DATE: 05-19-2004
CURRENT TIME: 13:11:37

FILE DATE: 05-19-2004
FILE NAME: F9

***** FHWA CULVERT ANALYSIS *****
***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCB	6.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (CFS) FILE: F9 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
100.91	16	16	0	0	0	0	0	0	1
101.45	32	32	0	0	0	0	0	0	1
101.90	48	48	0	0	0	0	0	0	1
102.31	64	64	0	0	0	0	0	0	1
102.69	80	80	0	0	0	0	0	0	1
103.05	96	96	0	0	0	0	0	0	1
103.38	112	112	0	0	0	0	0	0	1
103.72	128	128	0	0	0	0	0	0	1
104.05	144	144	0	0	0	0	0	0	1
104.23	152	152	0	0	0	0	0	0	1
110.00	334	334	0	0	0	0	0	0	OVERTOPPING

How/D = 1005 : : 0e

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F9 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
100.91	0.00	16	0	0.00
101.45	0.00	32	0	0.00
101.90	0.00	48	0	0.00
102.31	0.00	64	0	0.00
102.69	0.00	80	0	0.00
103.05	0.00	96	0	0.00
103.38	0.00	112	0	0.00
103.72	0.00	128	0	0.00
104.05	0.00	144	0	0.00
104.23	0.00	152	0	0.00

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

PRINT DATE: 05-19-2004
CURRENT TIME: 13:11:37

FILE DATE: 05-19-2004
FILE NAME: F9

***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
BOTTOM WIDTH (FT) 10.00
SIDE SLOPE H/V (X:1) 6.0
CHANNEL SLOPE V/H (FT/FT) 0.020
MANNING'S N (.01-0.1) 0.035
CHANNEL INVERT ELEVATION (FT) 98.40
CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
16.00	98.83	0.808	2.99	0.53
32.00	99.03	0.830	3.72	0.78
48.00	99.18	0.840	4.21	0.97
64.00	99.31	0.847	4.58	1.13
80.00	99.42	0.852	4.88	1.27
96.00	99.52	0.856	5.14	1.40
112.00	99.61	0.859	5.36	1.51
128.00	99.69	0.862	5.57	1.62
144.00	99.77	0.865	5.75	1.71
152.00	99.81	0.866	5.83	1.76

***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE PAVED
EMBANKMENT TOP WIDTH (FT) 30.00
CREST LENGTH (FT) 100.00
OVERTOPPING CREST ELEVATION (FT) 110.00

CURRENT DATE: 05-19-2004
 CURRENT TIME: 13:20:42

FILE DATE: 05-19-2004
 FILE NAME: SB8

 ***** FHWA CULVERT ANALYSIS *****
 ***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCP	4.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

 SUMMARY OF CULVERT FLOWS (CFS) FILE: SB8 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
101.59	16	16	0	0	0	0	0	0	1
102.36	32	32	0	0	0	0	0	0	1
103.04	48	48	0	0	0	0	0	0	1
103.65	64	64	0	0	0	0	0	0	1
104.28	80	80	0	0	0	0	0	0	1
104.97	96	96	0	0	0	0	0	0	1
105.78	112	112	0	0	0	0	0	0	1
106.73	128	128	0	0	0	0	0	0	1
107.82	144	144	0	0	0	0	0	0	1
108.42	152	152	0	0	0	0	0	0	1
110.00	171	171	0	0	0	0	0	0	OVERTOPPING

 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: SB8 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
101.59	0.00	16	0	0.00
102.36	0.00	32	0	0.00
103.04	0.00	48	0	0.00
103.65	0.00	64	0	0.00
104.28	0.00	80	0	0.00
104.97	0.00	96	0	0.00
105.78	0.00	112	0	0.00
106.73	0.00	128	0	0.00
107.82	0.00	144	0	0.00
108.42	0.00	152	0	0.00

<1> TOLERANCE (FT) = 0.010

<2> TOLERANCE (%) = 1.000

CURRENT DATE: 05-19-2004
CURRENT TIME: 13:20:42

FILE DATE: 05-19-2004
FILE NAME: SB8

***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
BOTTOM WIDTH (FT) 10.00
SIDE SLOPE H/V (X:1) 6.0
CHANNEL SLOPE V/H (FT/FT) 0.020
MANNING'S N (.01-0.1) 0.035
CHANNEL INVERT ELEVATION (FT) 98.40
CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
16.00	98.83	0.808	2.99	0.53
32.00	99.03	0.830	3.72	0.78
48.00	99.18	0.840	4.21	0.97
64.00	99.31	0.847	4.58	1.13
80.00	99.42	0.852	4.88	1.27
96.00	99.52	0.856	5.14	1.40
112.00	99.61	0.859	5.36	1.51
128.00	99.69	0.862	5.57	1.62
144.00	99.77	0.865	5.75	1.71
152.00	99.81	0.866	5.83	1.76

***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE PAVED
EMBANKMENT TOP WIDTH (FT) 30.00
CREST LENGTH (FT) 100.00
OVERTOPPING CREST ELEVATION (FT) 110.00

DP F10 Upper Collector

CURRENT DATE: 05-19-2004
 CURRENT TIME: 13:25:46

FILE DATE: 05-19-2004
 FILE NAME: F10

 ***** FHWA CULVERT ANALYSIS *****
 ***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
	1	100.00	98.40	80.02	1 RCP	3.50	3.50	.012
2								
3								
4								
5								
6								

 SUMMARY OF CULVERT FLOWS (CFS) FILE: F10 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
100.99	6	6	0	0	0	0	0	0	1
101.43	12	12	0	0	0	0	0	0	1
101.77	18	18	0	0	0	0	0	0	1
102.13	24	24	0	0	0	0	0	0	1
102.45	30	30	0	0	0	0	0	0	1
102.74	36	36	0	0	0	0	0	0	1
103.02	42	42	0	0	0	0	0	0	1
103.30	48	48	HW/D0 = 94	0	0	0	0	0	1
103.58	54	54	0	0	0	0	0	0	1
103.88	60	60	0	0	0	0	0	0	1
110.00	134	134	0	0	0	0	0	0	OVERTOPPING

 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F10 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
100.99	0.00	6	0	0.00
101.43	0.00	12	0	0.00
101.77	0.00	18	0	0.00
102.13	0.00	24	0	0.00
102.45	0.00	30	0	0.00
102.74	0.00	36	0	0.00
103.02	0.00	42	0	0.00
103.30	0.00	48	0	0.00
103.58	0.00	54	0	0.00
103.88	0.00	60	0	0.00

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

CURRENT DATE: 05-19-2004
 CURRENT TIME: 13:25:46

FILE DATE: 05-19-2004
 FILE NAME: F10

 ***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
 BOTTOM WIDTH (FT) 10.00
 SIDE SLOPE H/V (X:1) 6.0
 CHANNEL SLOPE V/H (FT/FT) 0.020
 MANNING'S N (.01-0.1) 0.035
 CHANNEL INVERT ELEVATION (FT) 98.40
 CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
6.00	98.64	0.769	2.15	0.30
12.00	98.76	0.798	2.72	0.45
18.00	98.85	0.812	3.11	0.57
24.00	98.93	0.821	3.41	0.67
30.00	99.00	0.828	3.65	0.75
36.00	99.07	0.833	3.86	0.83
42.00	99.12	0.837	4.04	0.90
48.00	99.18	0.840	4.21	0.97
54.00	99.23	0.843	4.35	1.03
60.00	99.28	0.845	4.49	1.09

 ***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH (FT)	30.00
CREST LENGTH (FT)	100.00
OVERTOPPING CREST ELEVATION (FT)	110.00

CURRENT DATE: 05-19-2004
 CURRENT TIME: 13:46:47

FILE DATE: 05-19-2004
 FILE NAME: F11

 ***** FHWA CULVERT ANALYSIS *****
 ***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCB	4.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

 SUMMARY OF CULVERT FLOWS (CFS) FILE: F11 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
100.93	11	11	0	0	0	0	0	0	1
101.48	22	22	0	0	0	0	0	0	1
101.94	33	33	0	0	0	0	0	0	1
102.36	44	44	0	0	0	0	0	0	1
102.75	55	55	0	0	0	0	0	0	1
103.11	66	66	0	0	0	0	0	0	1
103.46	77	77	0	0	0	0	0	0	1
103.80	88	88	0	0	0	0	0	0	1
104.15	99	99	0	0	0	0	0	0	1
104.25	102	102	0	0	0	0	0	0	1
110.00	223	223	0	0	0	0	0	0	OVERTOPPING

 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F11 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
100.93	0.00	11	0	0.00
101.48	0.00	22	0	0.00
101.94	0.00	33	0	0.00
102.36	0.00	44	0	0.00
102.75	0.00	55	0	0.00
103.11	0.00	66	0	0.00
103.46	0.00	77	0	0.00
103.80	0.00	88	0	0.00
104.15	0.00	99	0	0.00
104.25	0.00	102	0	0.00

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

CURRENT DATE: 05-19-2004
 CURRENT TIME: 13:46:47

FILE DATE: 05-19-2004
 FILE NAME: F11

 ***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
 BOTTOM WIDTH (FT) 10.00
 SIDE SLOPE H/V (X:1) 6.0
 CHANNEL SLOPE V/H (FT/FT) 0.020
 MANNING'S N (.01-0.1) 0.035
 CHANNEL INVERT ELEVATION (FT) 98.40
 CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
11.00	98.74	0.795	2.65	0.43
22.00	98.91	0.819	3.31	0.63
33.00	99.04	0.830	3.76	0.79
44.00	99.14	0.838	4.10	0.93
55.00	99.24	0.843	4.38	1.04
66.00	99.32	0.848	4.62	1.15
77.00	99.40	0.851	4.83	1.25
88.00	99.47	0.854	5.01	1.33
99.00	99.54	0.857	5.18	1.42
102.00	99.55	0.857	5.23	1.44

 ***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE PAVED
 EMBANKMENT TOP WIDTH (FT) 30.00
 CREST LENGTH (FT) 100.00
 OVERTOPPING CREST ELEVATION (FT) 110.00

F23 BRIDGE BLDG 1

CURRENT DATE: 05-21-2004
 CURRENT TIME: 09:22:08

FILE DATE: 05-19-2004
 FILE NAME: F23

 ***** FHWA CULVERT ANALYSIS *****
 ***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	96.80	160.03	1 RCP	4.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

 FILE: F23 CULVERT HEADWATER ELEVATION (FT) DATE: 05-19-2004

DISCHARGE	1	2	3	4	5	6	ROADWAY
0	100.00	0.00	0.00	0.00	0.00	0.00	110.00
8	101.07	0.00	0.00	0.00	0.00	0.00	110.09
15	101.53	0.00	0.00	0.00	0.00	0.00	110.14
23	101.90	0.00	0.00	0.00	0.00	0.00	110.18
30	102.27	0.00	0.00	0.00	0.00	0.00	110.22
38	102.61	0.00	0.00	0.00	0.00	0.00	110.25
45	102.92	0.00	0.00	0.00	0.00	0.00	110.28
53	103.22	0.00	0.00	0.00	0.00	0.00	110.31
60	103.50	0.00	0.00	0.00	0.00	0.00	110.34
68	103.79	0.00	0.00	0.00	0.00	0.00	110.37
69	103.84	0.00	0.00	0.00	0.00	0.00	110.37

2
 HW/D = 95

CURRENT DATE: 05-19-2004
CURRENT TIME: 13:52:24

FILE DATE: 05-19-2004
FILE NAME: F12

***** FHWA CULVERT ANALYSIS *****
***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCB	10.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (CFS) FILE: F12 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
100.85	24	24	0	0	0	0	0	0	1
101.35	48	48	0	0	0	0	0	0	1
101.77	72	72	0	0	0	0	0	0	1
102.15	96	96	0	0	0	0	0	0	1
102.51	120	120	0	0	0	0	0	0	1
102.84	144	144	0	0	0	0	0	0	1
103.15	168	168	0	0	0	0	0	0	1
103.45	192	192	0	0	0	0	0	0	1
103.75	216	216	0	0	0	0	0	0	1
104.00	236	236	0	0	0	0	0	0	1
110.00	557	557	0	0	0	0	0	0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F12 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
100.85	0.00	24	0	0.00
101.35	0.00	48	0	0.00
101.77	0.00	72	0	0.00
102.15	0.00	96	0	0.00
102.51	0.00	120	0	0.00
102.84	0.00	144	0	0.00
103.15	0.00	168	0	0.00
103.45	0.00	192	0	0.00
103.75	0.00	216	0	0.00
104.00	0.00	236	0	0.00

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

CURRENT DATE: 05-19-2004
 CURRENT TIME: 13:52:24

FILE DATE: 05-19-2004
 FILE NAME: F12

 ***** CULVERT # 1 *****

 PERFORMANCE CURVE FOR 1 BARREL(S)

Q (cfs)	HWE (ft)	TWE (ft)	ICH (ft)	OCH (ft)	FLOW TYPE	CCE (ft)	FCE (ft)	TCE (ft)	VO (fps)
0	100.00	98.40	0.00	-1.60	0-NF	0.00	100.00	0.00	0.00
24	100.85	98.93	0.85	0.69	6-FF	0.00	0.00	0.00	7.19
48	101.35	99.18	1.35	0.88	6-FF	0.00	0.00	0.00	10.34
72	101.77	99.36	1.77	1.07	6-FF	0.00	0.00	0.00	10.73
96	102.15	99.52	2.15	1.25	6-FF	0.00	0.00	0.00	11.71
120	102.51	99.65	2.51	1.45	6-FF	0.00	0.00	0.00	12.34
144	102.84	99.77	2.84	1.66	6-FF	0.00	0.00	0.00	12.85
168	103.15	99.88	3.15	1.87	6-FF	0.00	0.00	0.00	13.38
192	103.45	99.98	3.45	2.10	6-FF	0.00	0.00	0.00	13.79
216	103.75	100.08	3.75	2.35	6-FF	0.00	0.00	0.00	14.18
236	104.00	100.15	4.00	2.56	6-FF	0.00	0.00	0.00	14.46

El. inlet face invert 100.00 ft El. outlet invert 98.40 ft
 El. inlet throat invert 0.00 ft El. inlet crest 0.00 ft

***** SITE DATA ***** CULVERT INVERT *****
 INLET STATION (FT) 100.00
 INLET ELEVATION (FT) 100.00
 OUTLET STATION (FT) 180.00
 OUTLET ELEVATION (FT) 98.40
 NUMBER OF BARRELS 1.00
 SLOPE (V-FT/H-FT) 0.0200
 CULVERT LENGTH ALONG SLOPE (FT) 80.02

***** CULVERT DATA SUMMARY *****
 BARREL SHAPE BOX
 BARREL SPAN 10.00 FT
 BARREL RISE 4.00 FT
 BARREL MATERIAL CONCRETE
 BARREL MANNING'S N 0.012
 INLET TYPE CONVENTIONAL
 INLET EDGE AND WALL SQUARE EDGE (30-75 DEG. FLARE)
 INLET DEPRESSION NONE

CURRENT DATE: 05-19-2004
 CURRENT TIME: 13:52:24

FILE DATE: 05-19-2004
 FILE NAME: F12

 ***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
 BOTTOM WIDTH (FT) 10.00
 SIDE SLOPE H/V (X:1) 6.0
 CHANNEL SLOPE V/H (FT/FT) 0.020
 MANNING'S N (.01-0.1) 0.035
 CHANNEL INVERT ELEVATION (FT) 98.40
 CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
24.00	98.93	0.821	3.41	0.67
48.00	99.18	0.840	4.21	0.97
72.00	99.36	0.850	4.73	1.20
96.00	99.52	0.856	5.14	1.40
120.00	99.65	0.861	5.47	1.56
144.00	99.77	0.865	5.75	1.71
168.00	99.88	0.868	6.00	1.85
192.00	99.98	0.872	6.22	1.98
216.00	100.08	0.874	6.42	2.09
236.00	100.15	0.876	6.58	2.18

 ***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE PAVED
 EMBANKMENT TOP WIDTH (FT) 30.00
 CREST LENGTH (FT) 100.00
 OVERTOPPING CREST ELEVATION (FT) 110.00

DP F13 upper local roadway

PRINT DATE: 05-19-2004
 CURRENT TIME: 14:17:54

FILE DATE: 05-19-2004
 FILE NAME: F13

 ***** FHWA CULVERT ANALYSIS *****
 ***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCP	3.00	3.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

 SUMMARY OF CULVERT FLOWS (CFS) FILE: F13 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
100.78	4	4	0	0	0	0	0	0	1
101.12	7	7	0	0	0	0	0	0	1
101.39	11	11	0	0	0	0	0	0	1
101.66	14	14	0	0	0	0	0	0	1
101.91	18	18	0	0	0	0	0	0	1
102.14	21	21	0	0	0	0	0	0	1
102.35	25	25	0	0	0	0	0	0	1
102.56	28	28	0	0	0	0	0	0	1
102.67	30	30	0	0	0	0	0	0	1
102.96	35	35	0	0	0	0	0	0	1
110.00	100	100	0	0	0	0	0	0	1

HWID= .9

 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F13 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
100.78	0.00	4	0	0.00
101.12	0.00	7	0	0.00
101.39	0.00	11	0	0.00
101.66	0.00	14	0	0.00
101.91	0.00	18	0	0.00
102.14	0.00	21	0	0.00
102.35	0.00	25	0	0.00
102.56	0.00	28	0	0.00
102.67	0.00	30	0	0.00
102.96	0.00	35	0	0.00

<1> TOLERANCE (FT) = 0.010

<2> TOLERANCE (%) = 1.000

CURRENT DATE: 05-19-2004
 (RENT TIME: 14:17:54

FILE DATE: 05-19-2004
 FILE NAME: F13

 ***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
 BOTTOM WIDTH (FT) 10.00
 SIDE SLOPE H/V (X:1) 6.0
 CHANNEL SLOPE V/H (FT/FT) 0.020
 MANNING'S N (.01-0.1) 0.035
 CHANNEL INVERT ELEVATION (FT) 98.40
 CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
3.50	98.58	0.744	1.78	0.22
7.00	98.67	0.776	2.27	0.33
10.50	98.74	0.793	2.61	0.42
14.00	98.79	0.804	2.87	0.49
17.50	98.85	0.811	3.08	0.56
21.00	98.90	0.817	3.27	0.62
24.50	98.94	0.822	3.43	0.67
28.00	98.98	0.826	3.57	0.73
30.00	99.00	0.828	3.65	0.75
35.00	99.06	0.832	3.83	0.82

 ***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE PAVED
 EMBANKMENT TOP WIDTH (FT) 30.00
 CREST LENGTH (FT) 100.00
 OVERTOPPING CREST ELEVATION (FT) 110.00

DB19 OUTLET OF
DETENTION BASIN¹

CURRENT DATE: 05-19-2004
CURRENT TIME: 16:28:35

FILE DATE: 05-19-2004
FILE NAME: DB19

***** FHWA CULVERT ANALYSIS *****
***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	95.20	240.05	1 RCP	3.50	3.50	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (CFS) FILE: DB19 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
101.29	10	10	0	0	0	0	0	0	1
101.90	20	20	0	0	0	0	0	0	1
102.45	30	30	0	0	0	0	0	0	1
102.93	40	40	0	0	0	0	0	0	1
103.39	50	50	0	0	0	0	0	0	1
103.88	60	60	0	0	0	0	0	0	1
104.42	70	70	0	0	0	0	0	0	1
105.05	80	80	0	0	0	0	0	0	1
105.76	90	90	0	0	0	0	0	0	1
106.57	100	100	0	0	0	0	0	0	1
110.00	134	134	0	0	0	0	0	0	1

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: DB19 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
101.29	0.00	10	0	0.00
101.90	0.00	20	0	0.00
102.45	0.00	30	0	0.00
102.93	0.00	40	0	0.00
103.39	0.00	50	0	0.00
103.88	0.00	60	0	0.00
104.42	0.00	70	0	0.00
105.05	0.00	80	0	0.00
105.76	0.00	90	0	0.00
106.57	0.00	100	0	0.00

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

CURRENT DATE: 05-19-2004
CURRENT TIME: 16:28:35

FILE DATE: 05-19-2004
FILE NAME: DB19

***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
BOTTOM WIDTH (FT) 10.00
SIDE SLOPE H/V (X:1) 6.0
CHANNEL SLOPE V/H (FT/FT) 0.020
MANNING'S N (.01-0.1) 0.035
CHANNEL INVERT ELEVATION (FT) 95.20
CULVERT NO.1 OUTLET INVERT ELEVATION 95.20 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	95.20	0.000	0.00	0.00
10.00	95.53	0.791	2.56	0.41
20.00	95.68	0.816	3.22	0.60
30.00	95.80	0.828	3.65	0.75
40.00	95.91	0.836	3.98	0.88
50.00	96.00	0.841	4.26	0.99
60.00	96.08	0.845	4.49	1.09
70.00	96.15	0.849	4.70	1.19
80.00	96.22	0.852	4.88	1.27
90.00	96.28	0.855	5.04	1.35
100.00	96.34	0.857	5.20	1.43

***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE PAVED
EMBANKMENT TOP WIDTH (FT) 30.00
CREST LENGTH (FT) 100.00
OVERTOPPING CREST ELEVATION (FT) 110.00

DB 18. outlet of
detection basin 1

CURRENT DATE: 05-19-2004
CURRENT TIME: 16:33:00

FILE DATE: 05-19-2004
FILE NAME: DB18

***** FHWA CULVERT ANALYSIS *****
***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
	1	100.00	95.20	240.05	1 RCP	4.00	4.00	.012
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (CFS) FILE: DB18 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
101.53	15	15	0	0	0	0	0	0	1
102.27	30	30	0	0	0	0	0	0	1
102.92	45	45	0	0	0	0	0	0	1
103.50	60	60	0	0	0	0	0	0	1
104.08	75	75	0	0	0	0	0	0	1
104.70	90	90	0	0	0	0	0	0	1
105.41	105	105	0	0	0	0	0	0	1
106.24	120	120	0	0	0	0	0	0	1
107.19	135	135	0	0	0	0	0	0	1
107.53	140	140	0	0	0	0	0	0	1
110.00	171	171	0	0	0	0	0	0	1

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: DB18 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
101.53	0.00	15	0	0.00
102.27	0.00	30	0	0.00
102.92	0.00	45	0	0.00
103.50	0.00	60	0	0.00
104.08	0.00	75	0	0.00
104.70	0.00	90	0	0.00
105.41	0.00	105	0	0.00
106.24	0.00	120	0	0.00
107.19	0.00	135	0	0.00
107.53	0.00	140	0	0.00

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

CURRENT DATE: 05-19-2004
 CURRENT TIME: 16:33:00

FILE DATE: 05-19-2004
 FILE NAME: DB18

 ***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
 BOTTOM WIDTH (FT) 10.00
 SIDE SLOPE H/V (X:1) 6.0
 CHANNEL SLOPE V/H (FT/FT) 0.020
 MANNING'S N (.01-0.1) 0.035
 CHANNEL INVERT ELEVATION (FT) 95.20
 CULVERT NO.1 OUTLET INVERT ELEVATION 95.20 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	95.20	0.000	0.00	0.00
15.00	95.61	0.806	2.93	0.51
30.00	95.80	0.828	3.65	0.75
45.00	95.95	0.839	4.13	0.94
60.00	96.08	0.845	4.49	1.09
75.00	96.18	0.851	4.79	1.23
90.00	96.28	0.855	5.04	1.35
105.00	96.37	0.858	5.27	1.46
120.00	96.45	0.861	5.47	1.56
135.00	96.53	0.863	5.65	1.66
140.00	96.55	0.864	5.70	1.69

 ***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE PAVED
 EMBANKMENT TOP WIDTH (FT) 30.00
 CREST LENGTH (FT) 100.00
 OVERTOPPING CREST ELEVATION (FT) 110.00

CURRENT DATE: 05-21-2004
 CURRENT TIME: 09:22:08

FILE DATE: 05-19-2004
 FILE NAME: F23

 ***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
 BOTTOM WIDTH (FT) 10.00
 SIDE SLOPE H/V (X:1) 6.0
 CHANNEL SLOPE V/H (FT/FT) 0.020
 MANNING'S N (.01-0.1) 0.035
 CHANNEL INVERT ELEVATION (FT) 96.80
 CULVERT NO.1 OUTLET INVERT ELEVATION 96.80 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	96.80	0.000	0.00	0.00
7.50	97.08	0.779	2.32	0.35
15.00	97.21	0.806	2.93	0.51
22.50	97.32	0.819	3.34	0.64
30.00	97.40	0.828	3.65	0.75
37.50	97.48	0.834	3.91	0.85
45.00	97.55	0.839	4.13	0.94
52.50	97.62	0.842	4.32	1.02
60.00	97.68	0.845	4.49	1.09
67.50	97.73	0.848	4.65	1.16
69.00	97.74	0.849	4.68	1.18

 ***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE PAVED
 EMBANKMENT TOP WIDTH (FT) 30.00
 CREST LENGTH (FT) 100.00
 OVERTOPPING CREST ELEVATION (FT) 110.00

CURRENT DATE: 05-19-2004
 (CURRENT TIME: 17:00:28

FILE DATE: 05-19-2004
 FILE NAME: F14

 ***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
 BOTTOM WIDTH (FT) 10.00
 SIDE SLOPE H/V (X:1) 6.0
 CHANNEL SLOPE V/H (FT/FT) 0.020
 MANNING'S N (.01-0.1) 0.035
 CHANNEL INVERT ELEVATION (FT) 96.80
 CULVERT NO.1 OUTLET INVERT ELEVATION 96.80 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	96.80	0.000	0.00	0.00
22.00	97.31	0.819	3.31	0.63
44.00	97.54	0.838	4.10	0.93
66.00	97.72	0.848	4.62	1.15
88.00	97.87	0.854	5.01	1.33
110.00	98.00	0.859	5.34	1.50
132.00	98.11	0.863	5.61	1.64
154.00	98.22	0.866	5.86	1.77
176.00	98.32	0.870	6.08	1.89
198.00	98.41	0.872	6.27	2.01
210.00	98.45	0.874	6.37	2.06

 ***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE PAVED
 EMBANKMENT TOP WIDTH (FT) 30.00
 CREST LENGTH (FT) 100.00
 OVERTOPPING CREST ELEVATION (FT) 110.00

CURRENT DATE: 05-21-2004
 CURRENT TIME: 09:29:06

FILE DATE: 05-19-2004
 FILE NAME: F24

 ***** FHWA CULVERT ANALYSIS *****
 ***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
	1	100.00	98.40	80.02	1 RCB	8.00	4.00	.012
2								
3								
4								
5								
6								

 SUMMARY OF CULVERT FLOWS (CFS) FILE: F24 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
100.84	19	19	0	0	0	0	0	0	1
101.34	38	38	0	0	0	0	0	0	1
101.76	57	57	0	0	0	0	0	0	1
102.13	76	76	0	0	0	0	0	0	1
102.49	95	95	0	0	0	0	0	0	1
102.82	114	114	0	0	0	0	0	0	1
103.13	133	133	0	0	0	0	0	0	1
103.43	152	152	0	0	0	0	0	0	1
103.72	171	171	0	0	0	0	0	0	1
103.86	180	180	0	0	0	0	0	0	1
110.00	445	445	0	0	0	0	0	0	OVERTOPPING

 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F24 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
100.84	0.00	19	0	0.00
101.34	0.00	38	0	0.00
101.76	0.00	57	0	0.00
102.13	0.00	76	0	0.00
102.49	0.00	95	0	0.00
102.82	0.00	114	0	0.00
103.13	0.00	133	0	0.00
103.43	0.00	152	0	0.00
103.72	0.00	171	0	0.00
103.86	0.00	180	0	0.00

<1> TOLERANCE (FT) = 0.010
 <2> TOLERANCE (%) = 1.000

CURRENT DATE: 05-21-2004
CURRENT TIME: 09:29:06

FILE DATE: 05-19-2004
FILE NAME: F24

***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
BOTTOM WIDTH (FT) 10.00
SIDE SLOPE H/V (X:1) 6.0
CHANNEL SLOPE V/H (FT/FT) 0.020
MANNING'S N (.01-0.1) 0.035
CHANNEL INVERT ELEVATION (FT) 98.40
CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
19.00	98.87	0.814	3.16	0.59
38.00	99.09	0.834	3.92	0.86
57.00	99.25	0.844	4.42	1.06
76.00	99.39	0.851	4.81	1.24
95.00	99.51	0.856	5.12	1.39
114.00	99.62	0.860	5.39	1.52
133.00	99.72	0.863	5.62	1.65
152.00	99.81	0.866	5.83	1.76
171.00	99.90	0.869	6.03	1.87
180.00	99.93	0.870	6.11	1.91

***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE PAVED
EMBANKMENT TOP WIDTH (FT) 30.00
CREST LENGTH (FT) 100.00
OVERTOPPING CREST ELEVATION (FT) 110.00

CURRENT DATE: 05-21-2004
 CURRENT TIME: 09:25:45

FILE DATE: 05-21-2004
 FILE NAME: F25

 ***** FHWA CULVERT ANALYSIS *****
 ***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCB	10.00	5.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

 SUMMARY OF CULVERT FLOWS (CFS) FILE: F25 DATE: 05-21-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
101.24	31	31	0	0	0	0	0	0	1
101.60	62	62	0	0	0	0	0	0	1
102.10	93	93	0	0	0	0	0	0	1
102.54	124	124	0	0	0	0	0	0	1
102.97	155	155	0	0	0	0	0	0	1
103.36	186	186	0	0	0	0	0	0	1
103.73	217	217	0	0	0	0	0	0	1
104.09	248	248	0	0	0	0	0	0	1
104.43	279	279	0	0	0	0	0	0	1
104.74	306	306	0	0	0	0	0	0	1
110.00	663	663	0	0	0	0	0	0	OVERTOPPING

 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F25 DATE: 05-21-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
101.24	0.00	31	0	0.00
101.60	0.00	62	0	0.00
102.10	0.00	93	0	0.00
102.54	0.00	124	0	0.00
102.97	0.00	155	0	0.00
103.36	0.00	186	0	0.00
103.73	0.00	217	0	0.00
104.09	0.00	248	0	0.00
104.43	0.00	279	0	0.00
104.74	0.00	306	0	0.00

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

CURRENT DATE: 05-21-2004
CURRENT TIME: 09:25:45

FILE DATE: 05-21-2004
FILE NAME: F25

***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
BOTTOM WIDTH (FT) 10.00
SIDE SLOPE H/V (X:1) 6.0
CHANNEL SLOPE V/H (FT/FT) 0.020
MANNING'S N (.01-0.1) 0.035
CHANNEL INVERT ELEVATION (FT) 98.40
CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
31.00	99.01	0.829	3.69	0.77
62.00	99.29	0.846	4.53	1.11
93.00	99.50	0.855	5.09	1.37
124.00	99.67	0.861	5.52	1.59
155.00	99.82	0.866	5.87	1.78
186.00	99.96	0.871	6.17	1.95
217.00	100.08	0.874	6.43	2.10
248.00	100.19	0.877	6.67	2.24
279.00	100.30	0.880	6.88	2.37
306.00	100.38	0.882	7.05	2.47

***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE PAVED
EMBANKMENT TOP WIDTH (FT) 30.00
CREST LENGTH (FT) 100.00
OVERTOPPING CREST ELEVATION (FT) 110.00

CURRENT DATE: 05-21-2004
 CURRENT TIME: 09:33:34

FILE DATE: 05-19-2004
 FILE NAME: F30

 ***** FHWA CULVERT ANALYSIS *****
 ***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	98.40	80.02	1 RCB	10.00	6.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

 SUMMARY OF CULVERT FLOWS (CFS) FILE: F30 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
101.88	50	50	0	0	0	0	0	0	1
102.20	100	100	0	0	0	0	0	0	1
102.88	150	150	0	0	0	0	0	0	1
103.52	200	200	0	0	0	0	0	0	1
104.09	250	250	0	0	0	0	0	0	1
104.63	300	300	0	0	0	0	0	0	1
105.15	350	350	0	0	0	0	0	0	1
105.66	400	400	0	0	0	0	0	0	1
106.18	450	450	0	0	0	0	0	0	1
106.60	490	490	0	0	0	0	0	0	1
110.00	753	753	0	0	0	0	0	0	OVERTOPPING

 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: F30 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
101.88	0.00	50	0	0.00
102.20	0.00	100	0	0.00
102.88	0.00	150	0	0.00
103.52	0.00	200	0	0.00
104.09	0.00	250	0	0.00
104.63	0.00	300	0	0.00
105.15	0.00	350	0	0.00
105.66	0.00	400	0	0.00
106.18	0.00	450	0	0.00
106.60	0.00	490	0	0.00

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

CURRENT DATE: 05-21-2004
 CURRENT TIME: 09:33:34

FILE DATE: 05-19-2004
 FILE NAME: F30

 ***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
 BOTTOM WIDTH (FT) 10.00
 SIDE SLOPE H/V (X:1) 6.0
 CHANNEL SLOPE V/H (FT/FT) 0.020
 MANNING'S N (.01-0.1) 0.035
 CHANNEL INVERT ELEVATION (FT) 98.40
 CULVERT NO.1 OUTLET INVERT ELEVATION 98.40 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	98.40	0.000	0.00	0.00
50.00	99.20	0.841	4.26	0.99
100.00	99.54	0.857	5.20	1.43
150.00	99.80	0.865	5.81	1.75
200.00	100.01	0.872	6.29	2.02
250.00	100.20	0.878	6.68	2.25
300.00	100.36	0.882	7.01	2.45
350.00	100.51	0.886	7.31	2.64
400.00	100.65	0.889	7.57	2.81
450.00	100.78	0.892	7.80	2.97
490.00	100.87	0.894	7.98	3.09

 ***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE	PAVED
EMBANKMENT TOP WIDTH (FT)	30.00
CREST LENGTH (FT)	100.00
OVERTOPPING CREST ELEVATION (FT)	110.00

DB 28 Reservoir Parkway
 Outlet from det. basin

CURRENT DATE: 05-19-2004
 CURRENT TIME: 18:03:27

FILE DATE: 05-19-2004
 FILE NAME: DB28

 ***** FHWA CULVERT ANALYSIS *****
 ***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	95.20	240.05	1 RCB	8.00	4.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

 SUMMARY OF CULVERT FLOWS (CFS) FILE: DB28 DATE: 05-19-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
102.03	60	60	0	0	0	0	0	0	1
103.20	120	120	0	0	0	0	0	0	1
104.23	180	180	0	0	0	0	0	0	1
105.33	240	240	0	0	0	0	0	0	1
106.62	300	300	0	0	0	0	0	0	1
108.18	360	360	0	0	0	0	0	0	1
110.04	420	420	0	0	0	0	0	0	1
112.25	480	480	0	0	0	0	0	0	1
114.97	540	540	0	0	0	0	0	0	1
116.45	570	570	0	0	0	0	0	0	1
120.00	636	636	0	0	0	0	0	0	OVERTOPPING

 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: DB28 DATE: 05-19-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
102.03	0.00	60	0	0.00
103.20	0.00	120	0	0.00
104.23	0.00	180	0	0.00
105.33	0.00	240	0	0.00
106.62	0.00	300	0	0.00
108.18	0.00	360	0	0.00
110.04	0.00	420	0	0.00
112.25	0.00	480	0	0.00
114.97	0.00	540	0	0.00
116.45	0.00	570	0	0.00

<1> TOLERANCE (FT) = 0.010

<2> TOLERANCE (%) = 1.000

CURRENT DATE: 05-19-2004
RENT TIME: 18:03:27

FILE DATE: 05-19-2004
FILE NAME: DB28

***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
BOTTOM WIDTH (FT) 10.00
SIDE SLOPE H/V (X:1) 6.0
CHANNEL SLOPE V/H (FT/FT) 0.020
MANNING'S N (.01-0.1) 0.035
CHANNEL INVERT ELEVATION (FT) 95.20
CULVERT NO.1 OUTLET INVERT ELEVATION 95.20 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	95.20	0.000	0.00	0.00
60.00	96.08	0.845	4.49	1.09
120.00	96.45	0.861	5.47	1.56
180.00	96.73	0.870	6.11	1.91
240.00	96.96	0.877	6.61	2.20
300.00	97.16	0.882	7.01	2.45
360.00	97.34	0.886	7.36	2.67
420.00	97.50	0.890	7.66	2.87
480.00	97.65	0.894	7.94	3.06
540.00	97.79	0.897	8.19	3.23
570.00	97.85	0.899	8.30	3.31

***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE PAVED
EMBANKMENT TOP WIDTH (FT) 30.00
CREST LENGTH (FT) 100.00
OVERTOPPING CREST ELEVATION (FT) 120.00

CUTANER DESIGN - BASIN 'F'

Design guidelines.

Side Tributaries : Try to get 5-year velocity ≤ 5 fps or less for grasslined.

Try to get 100-year velocity ≤ 7 fps for grasslined / w riprap invert. > 7 fps, need \neq riprap sides.

- Since perimeter of Wolf Ranch is low density (i.e., 2.5 ac and greater lots), natural drainage ways could be left as is. Check structure @ most along steep sections.

"Net. Drainage"	Ex. Slope	τ @ 1' depth (l)
SB F-B	.104	2.5
SB F-B	.031	1.5
F9	.057	3.6
F10	.04	2.5
F11	.038	2.4
F12	.042	2.6
F12A	.034	2.2
F13	.05	3.1
F7	.031	1.9
F14	.042	2.6

$\tau = 8.65 = 8.5$ for $d=1'$

- Channel SB F-8 $Q_{100} = 69 \text{ cfs}$ $T = 2.5 @ 12"$
 69 cfs would be $< 12"$ deep $\therefore T < 2.5$
recommend leave as is.

~~Channel SB F-20 $T < 2.1$ allowable for gravel lined
leave as is.~~

- Channel F9 $Q_{100} = 152 \text{ cfs}$
drainage way is very wide, $> 50 \text{ BW}$
 $\therefore T < 3.6$ leave as is.

- Channel F10: $Q_{100} = 48 \text{ cfs}$ $T = 2.5 \text{ pcf}$
low flow, $T < 2.5$ leave as is.

- Channel F11: $Q_{100} = 102 \text{ cfs}$ $T = 2.4 \text{ pcf}$
 $d < 12"$ $\therefore T < 2.4$
leave as is.

- Channel F12: $Q_{100} = 144 \text{ cfs}$ $T = 2.6 \text{ pcf}$
very broad flow path, $>> 50'$
 $\therefore d < 12"$, $T < 2.6$ leave as is

- Channel 12A: $Q_{100} = 51 \text{ cfs}$ $T = 2.2 \text{ pcf}$
very broad flow path; $>> 50'$
 $\therefore d < 12"$, $T < 2.2 \text{ pcf}$
leave as is.

- channel F13 : $Q_{100} = 21 \text{ cfs}$ $\tau = 3.1$
 very low flow; may be a roadside swale.
 w/ $d = .5$ (dc for 21 cfs) $\tau = 1.55 \text{ psf}$
 \therefore leave as is or grasslined swale.

Improved drainage ways

- F8 (to confluence w/ F13)
 Q_5 range $15 \rightarrow 25 \text{ cfs}$
 Q_{100} range $69 \text{ cfs} \rightarrow 80 \text{ cfs}$
 Slope = $.037\%$
 - area has broad flow path; cutting through low density residential
 \therefore use BW 15'
 V_{50} Velocity = 4.2 fps \therefore dc for gravel
 100% = 6.1 fps need riprap invert
 No grade control proposed.
- F14
 $Q_5 = 18 \rightarrow 56$
 $Q_{100} = 152 \rightarrow 338 \text{ cfs}$ $S = .035\%$
 Fairly defined flowpath. use BW = 20'
 $e S = .035$, $V_5 = 5.2 \text{ fps}$ \therefore no good.
 Flatter w/ grade control.
 $e S = 2.5\%$ $V_5 = 4.8 \text{ ok}$, $V_{100} = 8 \text{ fps}$ \therefore no good
 flatten to 1.8% $V_5 = 4$ $V_{100} = 7.2 \text{ ok}$
 $\underline{\underline{3}}$

F19 cont'd.

Grade control. Design Slope = 1.8% $L = 1850'$
 Ex Slope = 3.5%
 $\therefore \Delta H = 1850 (.035 - .018) = 31.5'$ See 32
 Assume 6' of drop into DB forebay(s)
 $\therefore 3.2 \cdot L = 26'$ 9 drops / sheets
 Spacing @ 3' each $1850 / 9 = 205'$
spacing @ 200' int.

F18A : $Q_5 = 16$ $L = 1100'$
 $Q_{100} = 48$
 wide flow path. use $BW = 15'$
 Slope ex. = $.05'/1'$
 100 year velocity w/ 15' BW = $5.9'$ / sec
 5 year velocity = $3.1'$ / sec
No grade control required

F18 : $Q_5 = 13$, $Q_{100} = 102$ @ $1/4$. $L = 1500'$
 $Q_5 = F_{10} + F_{11} = 6 + 13 = 19$ cfs
 $Q_{100} = 48 + 102 = 150$ cfs.
 Slope = $50 / 1500 = .033'/1'$
 Assume 6' of drop can be achieved in DB forebay(s)
 $\therefore \Delta H = 50 - 6 = 44$
 $\therefore S = 44 / 1500 = .029'/1'$ $V_5 = 3.7$ fps
 $V_{100} = 6.4$ fps \therefore ok

F17

$$Q_s = 24 \text{ cfs} + \text{SBF17} = 24 + 3 = 27 \text{ cfs} \quad L = 1600'$$

$$Q_{100} = 236 \text{ cfs} + 25 \text{ cfs} = 261 \text{ cfs}$$

$$S = 54/1600 = .034\%$$

Assume 6' of drop into DB Forebays.

$$\therefore S_{eff} = 54 - 6 / 1600 = .03\%$$

@ Slope = .03%, V_{100} w/ 15' BW = 8.5 fpc.
 no grade.

Flatten with grade control:

$$@ S = .02\%, \quad V_{100} = 7.1 \text{ fpc} \therefore \frac{dV}{dL}$$

$$V_5 = 3.5 \text{ fpc} \therefore \frac{dV}{dL}$$

Required grade control:

$$\Delta S = .035 - .02 = .01 \times L = 16'$$

@ 3' / drop, need 3.1 drops, say 3

$$L_{seg} = 1600/3 = 533'$$

F16

This would be piped to DB18

$$Q_{100} = 31 \text{ cfs}$$

w/ 2% Storm Sewer Slope need 24" RCP.

Lower Portion, F14/F7

$$Q_5 = R_{F14} + R_{F7} = 5 + 2 = 7 \text{ cfs}$$

$$Q_{100} = 53 + 30 = 83 \text{ cfs} \quad L = 750'$$

$$S = 46.24 / 750' = .029' / 1'$$

w/ 10' BW, $S = 2.9\%$ $V_5 = 3 \text{ fps} \therefore \text{ok}$

$$V_{100} = 7.1 \text{ fps} \therefore \text{ok}$$

No grade control required.

F23

$$Q_5 = 6 \rightarrow 16$$

$$Q_{100} = 26 \rightarrow 69$$

$$L = 1050'$$

$$S = 28 / 1050 = .027' / 1'$$

w/ 10' BW, $V_5 = 3.5 \text{ fps} \therefore \text{ok}$

$$V_{100} = 5.7 \text{ fps} \therefore \text{ok}$$

no grade control req'd.

F24

$$Q_5 = 16 \rightarrow 44$$

$$Q_{100} = 69 \rightarrow 181$$

$$L = 2200'$$

$$S = 60 / 2200 = .027' / 1'$$

w/ 15' BW, $V_5 = 4.5 \text{ fps}$ $V_{100} = 7.1 \therefore \text{ok}$

no grade control req'd.

F25

$Q_5 = 45 \rightarrow 66$

$L = 2400'$

$Q_{100} = 210 \rightarrow 303$

$S = 66/2400 = .028\%$

w/BW = 20', S = .028, $V_{100} = 8.2$ ft/sec

Try S = .018, $V_{100} = 6.9$ ft/sec

$V_5 =$

Need Grade control

$\Delta S = .028 - .018 = .01 \times L = 24'$

w/ 3' per GC, need 8 drop/checks

Spacing @ 300' int.

F30

$Q_5 = 66$

$L = 900'$

$Q_{100} = 303$

$S = 28/900 = .031\%$

Use same section as F25

Speed = 1.8% for $V_{100} < 7$ fps.

$\therefore (.031 - .018)900 = 11.7'$ say 12

Need 4, 3' GC/drops

Spacing $900/4 = 225'$

F29 $Q_5 = 112$ $Q_{100} = 480$ $L = 750'$
 $S = \frac{30 - 00}{750} = .04' / 11$

try $BW = 20'$, $Velocity_{100} = 10.5$ fps + no good.
 cut to 2%, still need riprap. $V_{100} = 8.2$ fps.
 go with riprap swale.

GC: $\Delta S = .04 - .02 = .02 \times L = 15'$
 ∴ need 5, 3' drops @ 150' interval. to close.
 use 2- 6' sloping drops.

∴ Slope of channel = $750 (.04 - X) = 12'$ Riprap Size
 $X = .024' / 1$ $V_{S=1.36} = 8.8 (.024)^{.17}$
 $= 3.4'$

~~F21 $Q_5 = 45 \rightarrow 120$ $L = 1750'$ Type "L"
 $Q_{100} = 140 \rightarrow 313$
 $S = 60 / 1750 = .029' / 1$~~

~~Try $BW = 20'$ @ $S = .029$, $V_{100} = 8.2$ + no good
 w/ $S = 1.8\%$ $V_{100} = 6.9$ fps ∴ ok~~

~~GC: $(.029 - .018) 1750 = .011 (1750) = 19.25$~~

~~seg 21:~~

~~w/ 3' / 66, need 7 drops : Int = $1750 / 7 = 250'$~~

F22 $Q_5 = 20 + \frac{1}{2} \overset{SB}{F22} = 20 + \frac{1}{2}(7) = 24 \text{ cfs}$
 $Q_{100} = 89 + \frac{1}{2} \overset{SB}{F22} = 89 + \frac{1}{2}(5) = 115 \text{ cfs}$
 $L = 1850' \quad S = 60/1850 = .032'/1'$

Try $BW = 15'$, $S = .032'/1'$, $V_{100} = 6.5 \text{ ft/s} < \underline{ok}$ $V_5 =$
 no gc required

F22A $Q_5 = 26 + \frac{1}{2} \overset{SB}{F22} = 30 \text{ cfs}$
 $Q_{100} = 141 + \frac{1}{2} \overset{SB}{F22} = 167 \text{ cfs}$
 $L = 2050' \quad S = 60/2050 = .029'/1'$

Try $20'$ BW, $S = .029'/1'$ $V_{100} = 6.7 \text{ ft/s} < \underline{ok}$
 $V_5 = 3.2 \text{ ft/s} < \underline{ok}$
 No GC req'd.

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F8: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	25 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	3.7 %
Depth of Flow	0.40 ft	Manning's Roughness Coef.	0.035

Channel Area 6.6 sf
Channel Wetted Perimeter 18.3 ft
Hydraulic Radius 0.36 ft

Channel Flow Velocity	4.2 ft/sec
Channel Flow Capacity	28 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.48 ft
Top Width	26.8 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b+2d*(1+z²)^{0.5}

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R_n^{2/3} S^{1/2}

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR_n^{2/3} S^{1/2}

Freeboard = 1.0+0.025(v)d^{0.33}



**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F8: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	80 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	3.7 %
Depth of Flow	0.75 ft	Manning's Roughness Coef.	0.035

Channel Area 13.5 sf
 Channel Wetted Perimeter 21.2 ft
 Hydraulic Radius 0.64 ft

Channel Flow Velocity	6.1 ft/sec
Channel Flow Capacity	82 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.89 ft
Top Width	30.1 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d*(1+z²)^{0.5}

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R_n^{2/3} S^{1/2}

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR_n^{2/3} S^{1/2}

Freeboard = 1.0 + 0.025(v)d^{0.33}

Wolf Ranch MDDP
Swale Capacity Calculation

Structure F19: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	56 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	1.8 %
Depth of Flow	0.65 ft	Manning's Roughness Coef.	0.035

Channel Area 14.7 sf
Channel Wetted Perimeter 25.4 ft
Hydraulic Radius 0.58 ft

Channel Flow Velocity	4.0 ft/sec
Channel Flow Capacity	58 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.74 ft
Top Width	33.9 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d\sqrt{1+z^2}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F19: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	338 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	1.8 %
Depth of Flow	1.80 ft	Manning's Roughness Coef.	0.035

Channel Area	49.0 sf
Channel Wetted Perimeter	34.8 ft
Hydraulic Radius	1.41 ft

Channel Flow Velocity	7.2 ft/sec
Channel Flow Capacity	351 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	3.02 ft
Top Width	44.1 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d(1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F18A: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	6 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	5.0 %
Depth of Flow	0.20 ft	Manning's Roughness Coef.	0.035

Channel Area	3.2 sf
Channel Wetted Perimeter	16.6 ft
Hydraulic Radius	0.19 ft

Channel Flow Velocity	3.1 ft/sec
Channel Flow Capacity	10 cfs
Capacity Check	Okay

Freeboard	1.0 ft
Swale Depth	1.25 ft
Top Width	25.0 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

Wolf Ranch MDDP
Swale Capacity Calculation

Structure F18A: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	48 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	5.0 %
Depth of Flow	0.55 ft	Manning's Roughness Coef.	0.035

Channel Area 9.5 sf
Channel Wetted Perimeter 19.5 ft
Hydraulic Radius 0.48 ft

Channel Flow Velocity	5.9 ft/sec
Channel Flow Capacity	56 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.67 ft
Top Width	28.4 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d \sqrt{1+z^2}^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.53}$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F18: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	19 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.9 %
Depth of Flow	0.40 ft	Manning's Roughness Coef.	0.035

Channel Area 6.6 sf
Channel Wetted Perimeter 18.3 ft
Hydraulic Radius 0.36 ft

Channel Flow Velocity	3.7 ft/sec
Channel Flow Capacity	24 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.47 ft
Top Width	26.7 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b+2d*(1+z²)^{0.5}

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R_n^{2/3} S^{1/2}

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR_n^{2/3} S^{1/2}

Freeboard = 1.0+0.025(v)d^{0.33}

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F18: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	150 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.9 %
Depth of Flow	1.15 ft	Manning's Roughness Coef.	0.035

Channel Area	22.5 sf
Channel Wetted Perimeter	24.5 ft
Hydraulic Radius	0.92 ft

Channel Flow Velocity	6.9 ft/sec
Channel Flow Capacity	155 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.33 ft
Top Width	33.6 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d \sqrt{1+z^2}^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F17: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	27 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.0 %
Depth of Flow	0.50 ft	Manning's Roughness Coef.	0.035

Channel Area	8.5 sf
Channel Wetted Perimeter	19.1 ft
Hydraulic Radius	0.44 ft

Channel Flow Velocity	3.5 ft/sec
Channel Flow Capacity	30 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.57 ft
Top Width	27.6 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)^{0.33}$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F17: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	261 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.0 %
Depth of Flow	1.70 ft	Manning's Roughness Coef.	0.035

Channel Area 37.1 sf
Channel Wetted Perimeter 29.0 ft
Hydraulic Radius 1.28 ft

Channel Flow Velocity	7.1 ft/sec
Channel Flow Capacity	263 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.91 ft
Top Width	38.3 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d*(1+z²)^{0.5}

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R_n^{2/3} S^{1/2}

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR_n^{2/3} S^{1/2}

Freeboard = 1.0 + 0.025(v)d^{0.33}

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F14: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	7 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	2.9 %
Depth of Flow	0.30 ft	Manning's Roughness Coef.	0.035

Channel Area 3.4 sf
Channel Wetted Perimeter 12.5 ft
Hydraulic Radius 0.27 ft

Channel Flow Velocity	3.0 ft/sec
Channel Flow Capacity	10 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.35 ft
Top Width	20.8 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n) R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n) A R_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)^{0.33}$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F14: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	83 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	2.9 %
Depth of Flow	0.95 ft	Manning's Roughness Coef.	0.029

Channel Area 13.1 sf
Channel Wetted Perimeter 17.8 ft
Hydraulic Radius 0.74 ft

Channel Flow Velocity	7.1 ft/sec
Channel Flow Capacity	93 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.13 ft
Top Width	27.0 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d(1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

Wolf Ranch MDDP
Swale Capacity Calculation

Structure F23: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	16 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	2.7 %
Depth of Flow	0.40 ft	Manning's Roughness Coef.	0.035

Channel Area	4.6 sf
Channel Wetted Perimeter	13.3 ft
Hydraulic Radius	0.35 ft

Channel Flow Velocity	3.5 ft/sec
Channel Flow Capacity	16 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.46 ft
Top Width	21.7 ft

Equations:

$$\text{Area (A)} = b(d)$$

$$b = \text{width}$$

$$d = \text{depth}$$

$$\text{Perimeter (P)} = b + 2d(1+z^2)^{0.5}$$

$$z = \text{side slope}$$

$$\text{Hydraulic Radius} = A/P$$

$$\text{Velocity} = (1.49/n)R_n^{2/3} S^{1/2}$$

$$\text{Slope (S)} = \text{Slope of the channel}$$

$$n = \text{Manning's number}$$

$$R_n = \text{Hydraulic Radius (Reynold's Number)}$$

$$\text{Flow} = (1.49/n)AR_n^{2/3} S^{1/2}$$

$$\text{Freeboard} = 1.0 + 0.025(v)d^{0.33}$$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F23: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	69 cfs	Channel Side Slope	4:1
Bottom Width	10.0 ft	Channel Longitudinal Slope	2.7 %
Depth of Flow	0.95 ft	Manning's Roughness Coef.	0.035

Channel Area 13.1 sf
Channel Wetted Perimeter 17.8 ft
Hydraulic Radius 0.74 ft

Channel Flow Velocity	5.7 ft/sec
Channel Flow Capacity	75 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	2.09 ft
Top Width	26.7 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d*(1+z²)^{0.5}

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R_n^{2/3} S^{1/2}

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR_n^{2/3} S^{1/2}

Freeboard = 1.0 + 0.025(v)d^{0.33}

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F24: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	44 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.7 %
Depth of Flow	0.60 ft	Manning's Roughness Coef.	0.035

Channel Area	10.4 sf
Channel Wetted Perimeter	19.9 ft
Hydraulic Radius	0.52 ft

Channel Flow Velocity	4.5 ft/sec
Channel Flow Capacity	47 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.70 ft
Top Width	28.6 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d\sqrt{1+z^2}^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F24: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	181 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.7 %
Depth of Flow	1.30 ft	Manning's Roughness Coef.	0.035

Channel Area	26.3 sf
Channel Wetted Perimeter	25.7 ft
Hydraulic Radius	1.02 ft

Channel Flow Velocity	7.1 ft/sec
Channel Flow Capacity	186 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.49 ft
Top Width	34.9 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)^{0.33}$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F25: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	66 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	1.8 %
Depth of Flow	0.70 ft	Manning's Roughness Coef.	0.035

Channel Area 16.0 sf
Channel Wetted Perimeter 25.8 ft
Hydraulic Radius 0.62 ft

Channel Flow Velocity	4.1 ft/sec
Channel Flow Capacity	66 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.79 ft
Top Width	34.3 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d*(1+z²)^{0.5}

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R_n^{2/3} S^{1/2}

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR_n^{2/3} S^{1/2}

Freeboard = 1.0 + 0.025(v)d^{0.33}

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F25: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	303 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	1.8 %
Depth of Flow	1.70 ft	Manning's Roughness Coef.	0.035

Channel Area	45.6 sf
Channel Wetted Perimeter	34.0 ft
Hydraulic Radius	1.34 ft

Channel Flow Velocity	6.9 ft/sec
Channel Flow Capacity	316 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.91 ft
Top Width	43.3 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F29: Riprap channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	490 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	2.4 %
Depth of Flow	2.00 ft	Manning's Roughness Coef.	0.035

Channel Area 56.0 sf
Channel Wetted Perimeter 36.5 ft
Hydraulic Radius 1.53 ft

Channel Flow Velocity	8.8 ft/sec
Channel Flow Capacity	491 cfs
Capacity Check	Okay

Freeboard	1.3 ft
Swale Depth	3.28 ft
Top Width	46.2 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d\sqrt{1+z^2}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

Wolf Ranch MDDP
Swale Capacity Calculation

Structure F22: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	24 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	3.2 %
Depth of Flow	0.40 ft	Manning's Roughness Coef.	0.035

Channel Area 6.6 sf
Channel Wetted Perimeter 18.3 ft
Hydraulic Radius 0.36 ft

Channel Flow Velocity	3.9 ft/sec
Channel Flow Capacity	26 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.47 ft
Top Width	26.8 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d \sqrt{1+z^2}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F22: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	115 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	3.2 %
Depth of Flow	0.95 ft	Manning's Roughness Coef.	0.035

Channel Area 17.9 sf
 Channel Wetted Perimeter 22.8 ft
 Hydraulic Radius 0.78 ft

Channel Flow Velocity	6.5 ft/sec
Channel Flow Capacity	115 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.11 ft
Top Width	31.9 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n) R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n) A R_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure F22A: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	30 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	2.9 %
Depth of Flow	0.40 ft	Manning's Roughness Coef.	0.035

Channel Area 8.6 sf
Channel Wetted Perimeter 23.3 ft
Hydraulic Radius 0.37 ft

Channel Flow Velocity	3.7 ft/sec
Channel Flow Capacity	32 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.47 ft
Top Width	31.8 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

Wolf Ranch MDDP
Swale Capacity Calculation

Structure F22A: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	167 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	2.9 %
Depth of Flow	1.05 ft	Manning's Roughness Coef.	0.035

Channel Area 25.4 sf
Channel Wetted Perimeter 28.7 ft
Hydraulic Radius 0.89 ft

Channel Flow Velocity	6.7 ft/sec
Channel Flow Capacity	170 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.22 ft
Top Width	37.8 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b+2d*(1+z²)^{0.5}

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R_n^{2/3} S^{1/2}

Slope (S) = Slope of the channel

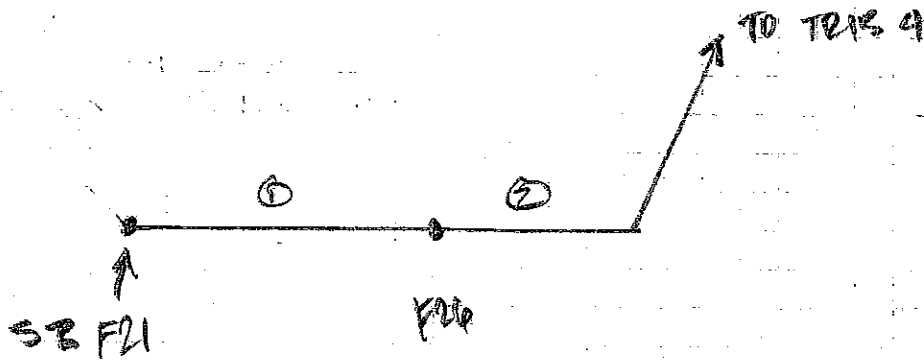
n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR_n^{2/3} S^{1/2}

Freeboard = 1.0+0.025(v)d^{0.33}

OUTFALL STORM SEWER, BASIN 'F'



Flow Summary

Q_{100}

e SB F21	184 cfs	→ 235	1/2 to DP F26
e DP F26	285 cfs		
e DP F27	294 cfs		
Segment ①	$Q_{100} = 184$ cfs		

assume 1.8% Pipe Slope ∴ 48" RCP, $Q_{full} = 193$ cfs

Segment ② $Q_{100} = 294$ cfs → 285 e Trib 4
 Should be able to steeper slope to 2.5 → 3%
 ∴ 54" @ 2.2% ≈ $Q_{full} = 292$ cfs ∴ ok

~~Segment ③ $Q_{100} = 110$ → 113 cfs~~

~~SB F21 @ 2.0% Q_{full} to 42" RCP = 119 cfs ok~~

~~SB to SB 20 1/2" $Q = 70$ cfs. 36" RCP @ 2.0 = 94 cfs ok~~

6-Basin DETENTION

Total Area @ DP G : = .32 sm = 205 Ac

$Q_5 \text{ Ex} = 13 \text{ cfs}$

$Q_{100} \text{ Ex} = 155 \text{ cfs}$

CN = 61

Runoff = .2" 5 year
1.02" 100 year

- DEVELOPED

$Q_5 = 80 \text{ cfs}$ $Q_{100} = 305$

Drainage Area: .45 sm @ DP G = 288 Ac

Wtd CN: $\frac{.08(61) + .035(73) + .172(73) + .153(78.4)}{.45} = 72.0$

\therefore Runoff = 5 year = .53" 100 year = 1.75"

- Existing Volume of Runoff

5-year : (205 Ac) .2" / 12 = 3.4 Ac-ft

100 year (205 Ac) 1.02" / 12 = 17.4 Ac-ft

- Developed Runoff Volume :

5-year = 288 Ac (.53 / 12) = 12.7 AF

100-year = 288 (1.75 / 12) = 42.0 AF

- Required Storage Volume in Basin

5 year = 12.7 - 3.4 = 9.3 AF ←

100 year = 42.0 - 17.4 = 24.6 AF ←

Place single detection basin @ DP G3

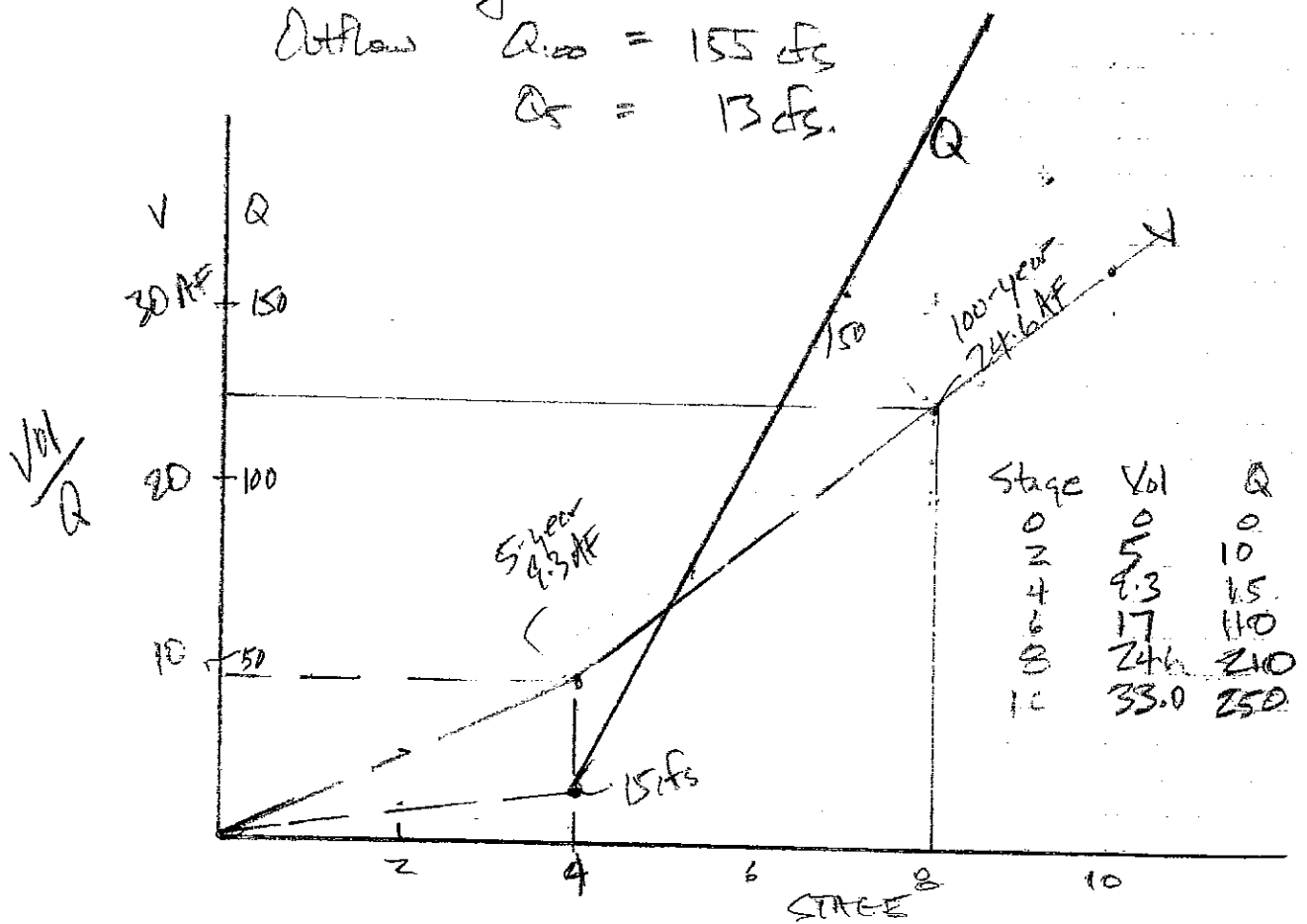
Need to reduce 100 year flow to \approx

$Q_{100} @ DP G3 = 273 cfs$ $\times DP G = 429 cfs$
 $SB G-5 Q_{100} = 230 cfs$

Required @ DP G = 155 cfs ; can't be done so will need det in SB G-5

Size single facility @ DP G.

Outflow $Q_{100} = 155 cfs$
 $Q_5 = 13 cfs$



G-Basin Hydraulics

Outfall Channels

Use same criteria as previous basins.

G3

$$Q_5 = 12 + 1/2(63) = 12 + 25 = 37 \text{ cfs}$$

$$Q_{100} = 45 + 100 = 145 \text{ cfs}$$

$$L = 3150' \quad S = \frac{164.82}{3150} = .026'/1$$

w/ TSW = 15', S = .026 $V_{100} = 6.5 \text{ fps}$ is ok
 $V_5 = 4.2 \text{ fps}$ is ok

No grade control required.

G2

$$Q_5 = 5861 + 1/2(63) = 5 + 25 = 30 \text{ cfs}$$

$$Q_{100} = 50 + 100 = 150 \text{ cfs}$$

$$L = 3250' \quad S = (166.82)/3250 = .026'/1$$

w/ 15' TSW; S = .026' $V_{100} = 6.7 \text{ fps}$ is ok
 $V_5 = 4.0 \text{ fps}$ is ok

No grade control Req'd.

Q5 $Q_5 = 57 + \frac{1}{2}(6 \cdot 5) = 57 + 37 = 94 \text{ cfs}$ $L = 1850'$
 $Q_{100} = 278 + \frac{1}{2}(6 \cdot 5) = 278 + 115 = 393 \text{ cfs}$
 $S = 50 / 1850 = .027 \%$

try $BWD = w/ S = .027 \%$ $V_{100} = 8.6 \text{ fps}$, too high
 use $S = .02$ $V > 8'$
 $w/ S = 1.5 \%$ $V_{100} = 7.0 \text{ fps} \therefore ok$
 $V_5 = 4.5 \text{ fps} \therefore ok$

Grate control req'd.

$\Delta S = .027 - .015 = .012 \%$ $\times L = 22.2'$
 w each drop = 3', 8' checks say 24
 spacing $1850 / 8 = 230'$ interval

Wolf Ranch MDDP
Swale Capacity Calculation

Structure G3: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	37 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.6 %
Depth of Flow	0.55 ft	Manning's Roughness Coef.	0.035

Channel Area	9.5 sf
Channel Wetted Perimeter	19.5 ft
Hydraulic Radius	0.48 ft

Channel Flow Velocity	4.2 ft/sec
Channel Flow Capacity	40 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.64 ft
Top Width	28.1 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d(1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

Wolf Ranch MDDP
Swale Capacity Calculation

Structure G3: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	145 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.6 %
Depth of Flow	1.15 ft	Manning's Roughness Coef.	0.035

Channel Area	22.5 sf
Channel Wetted Perimeter	24.5 ft
Hydraulic Radius	0.92 ft

Channel Flow Velocity	6.5 ft/sec
Channel Flow Capacity	146 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.32 ft
Top Width	33.6 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d \cdot (1 + z^2)^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n) R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n) A R_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

Wolf Ranch MDDP
Swale Capacity Calculation

Structure G2: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	30 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.6 %
Depth of Flow	0.50 ft	Manning's Roughness Coef.	0.035

Channel Area	8.5 sf
Channel Wetted Perimeter	19.1 ft
Hydraulic Radius	0.44 ft

Channel Flow Velocity	4.0 ft/sec
Channel Flow Capacity	34 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	1.58 ft
Top Width	27.6 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d \sqrt{1 + z^2}^{0.5}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n)R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n)AR_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.33}$

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure G2: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	150 cfs	Channel Side Slope	4:1
Bottom Width	15.0 ft	Channel Longitudinal Slope	2.6 %
Depth of Flow	1.20 ft	Manning's Roughness Coef.	0.035

Channel Area	23.8 sf
Channel Wetted Perimeter	24.9 ft
Hydraulic Radius	0.95 ft

Channel Flow Velocity	6.7 ft/sec
Channel Flow Capacity	158 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	2.38 ft
Top Width	34.0 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b+2d*(1+z²)^{0.5}

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R_n^{2/3} S^{1/2}

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR_n^{2/3} S^{1/2}

Freeboard = 1.0+0.025(v)d^{0.33}

Wolf Ranch MDDP
Swale Capacity Calculation

Structure G5: Grasslined channel 5-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	94 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	1.5 %
Depth of Flow	0.95 ft	Manning's Roughness Coef.	0.035

Channel Area	22.6 sf
Channel Wetted Perimeter	27.8 ft
Hydraulic Radius	0.81 ft

Channel Flow Velocity	4.5 ft/sec
Channel Flow Capacity	103 cfs
Capacity Check	Okay

Freeboard	1.1 ft
Swale Depth	2.06 ft
Top Width	36.5 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = b + 2d*(1+z²)^{0.5}

z = side slope

Hydraulic Radius = A/P

Velocity = (1.49/n)R_n^{2/3} S^{1/2}

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = (1.49/n)AR_n^{2/3} S^{1/2}

Freeboard = 1.0 + 0.025(v)d^{0.33}

**Wolf Ranch MDDP
Swale Capacity Calculation**

Structure G5: Grasslined channel 100-year

Trapezoidal Channel Capacity Calculation (Values to be Input)			
Design Flow	393 cfs	Channel Side Slope	4:1
Bottom Width	20.0 ft	Channel Longitudinal Slope	1.5 %
Depth of Flow	2.05 ft	Manning's Roughness Coef.	0.035

Channel Area	57.8 sf
Channel Wetted Perimeter	36.9 ft
Hydraulic Radius	1.57 ft

Channel Flow Velocity	7.0 ft/sec
Channel Flow Capacity	407 cfs
Capacity Check	Okay

Freeboard	1.2 ft
Swale Depth	3.27 ft
Top Width	46.2 ft

Equations:

Area (A) = b(d)

b = width

d = depth

Perimeter (P) = $b + 2d \sqrt{1 + z^2}$

z = side slope

Hydraulic Radius = A/P

Velocity = $(1.49/n) R_n^{2/3} S^{1/2}$

Slope (S) = Slope of the channel

n = Manning's number

R_n = Hydraulic Radius (Reynold's Number)

Flow = $(1.49/n) A R_n^{2/3} S^{1/2}$

Freeboard = $1.0 + 0.025(v)d^{0.13}$

Pipe Alternatives, Reach G5

$Q_{100} = 277$ c Research to 393 f
DB 9

use RCP ; $S = 2.2\%$ same as channel.

$W/S = 2.2\%$ 60" RCP $Q_{full} = 386$ cfs

G3 e Briarcliff Blvd.

CURRENT DATE: 05-24-2004
 CURRENT TIME: 17:31:53

Q=277 cfs

FILE DATE: 05-24-2004
 FILE NAME: G3

 ***** FHWA CULVERT ANALYSIS *****
 ***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	96.80	160.03	1 RCB	10.00	5.00	.012	CONVENTIONAL
2								
3								
4								
5								
6								

 SUMMARY OF CULVERT FLOWS (CFS) FILE: G3 DATE: 05-24-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
100.94	28	28	0	0	0	0	0	0	1
101.49	56	56	0	0	0	0	0	0	1
101.96	84	84	0	0	0	0	0	0	1
102.37	112	112	0	0	0	0	0	0	1
102.77	140	140	0	0	0	0	0	0	1
103.14	168	168	0	0	0	0	0	0	1
103.48	196	196	0	0	0	0	0	0	1
103.81	224	224	0	0	0	0	0	0	1
104.13	252	252	0	0	0	0	0	0	1
104.41	277	277	0	0	0	0	0	0	1
110.00	663	663	0	0	0	0	0	0	1
			0	0	0	0	0	0	1

Handwritten note: $H_w/D = 1.08$ or 1.0

 0 OVERTOPPING

 SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: G3 DATE: 05-24-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
100.94	0.00	28	0	0.00
101.49	0.00	56	0	0.00
101.96	0.00	84	0	0.00
102.37	0.00	112	0	0.00
102.77	0.00	140	0	0.00
103.14	0.00	168	0	0.00
103.48	0.00	196	0	0.00
103.81	0.00	224	0	0.00
104.13	0.00	252	0	0.00
104.41	0.00	277	0	0.00

 <1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

CURRENT DATE: 05-24-2004
CURRENT TIME: 17:31:53

FILE DATE: 05-24-2004
FILE NAME: G3

***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
BOTTOM WIDTH (FT) 10.00
SIDE SLOPE H/V (X:1) 6.0
CHANNEL SLOPE V/H (FT/FT) 0.020
MANNING'S N (.01-0.1) 0.035
CHANNEL INVERT ELEVATION (FT) 96.80
CULVERT NO.1 OUTLET INVERT ELEVATION 96.80 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	96.80	0.000	0.00	0.00
28.00	97.38	0.826	3.57	0.73
56.00	97.64	0.844	4.40	1.05
84.00	97.84	0.853	4.95	1.30
112.00	98.01	0.859	5.36	1.51
140.00	98.15	0.864	5.70	1.69
168.00	98.28	0.868	6.00	1.85
196.00	98.40	0.872	6.26	2.00
224.00	98.51	0.875	6.49	2.13
252.00	98.61	0.878	6.69	2.25
277.00	98.69	0.880	6.87	2.36

***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE PAVED
EMBANKMENT TOP WIDTH (FT) 30.00
CREST LENGTH (FT) 100.00
OVERTOPPING CREST ELEVATION (FT) 110.00

OUTLET DIS G
54" RCP

CURRENT DATE: 07-02-2004
CURRENT TIME: 14:59:59

FILE DATE: 07-02-2004
FILE NAME: DBGOUT

***** FHWA CULVERT ANALYSIS *****
***** HY-8, VERSION 3.2 *****

C U L V #	SITE DATA			CULVERT SHAPE, MATERIAL, INLET				
	INLET ELEV. (FT)	OUTLET ELEV. (FT)	CULVERT LENGTH (FT)	BARRELS SHAPE MATERIAL	SPAN (FT)	RISE (FT)	MANNING n	INLET TYPE
1	100.00	95.00	80.16	1 RCP	4.50	4.50	.012	CONVENTIONAL
2								
3								
4								
5								
6								

SUMMARY OF CULVERT FLOWS (CFS) FILE: DBGOUT DATE: 07-02-2004

ELEV (FT)	TOTAL	1	2	3	4	5	6	ROADWAY	ITR
100.00	0	0	0	0	0	0	0	0	1
101.42	15	15	0	0	0	0	0	0	1
102.06	30	30	0	0	0	0	0	0	1
102.64	45	45	0	0	0	0	0	0	1
103.18	60	60	0	0	0	0	0	0	1
103.67	75	75	0	0	0	0	0	0	1
104.14	90	90	0	0	0	0	0	0	1
104.63	105	105	0	0	0	0	0	0	1
105.16	120	120	0	0	0	0	0	0	1
105.75	135	135	0	0	0	0	0	0	1
105.95	140	140	0	0	0	0	0	0	1
110.00	213	213	0	0	0	0	0	0	OVERTOPPING

SUMMARY OF ITERATIVE SOLUTION ERRORS FILE: DBGOUT DATE: 07-02-2004

HEAD ELEV (FT)	HEAD ERROR (FT)	TOTAL FLOW (CFS)	FLOW ERROR (CFS)	% FLOW ERROR
100.00	0.00	0	0	0.00
101.42	0.00	15	0	0.00
102.06	0.00	30	0	0.00
102.64	0.00	45	0	0.00
103.18	0.00	60	0	0.00
103.67	0.00	75	0	0.00
104.14	0.00	90	0	0.00
104.63	0.00	105	0	0.00
105.16	0.00	120	0	0.00
105.75	0.00	135	0	0.00
105.95	0.00	140	0	0.00

<1> TOLERANCE (FT) = 0.010 <2> TOLERANCE (%) = 1.000

REPORT DATE: 07-02-2004
REPORT TIME: 14:59:59

FILE DATE: 07-02-2004
FILE NAME: DBGOUT

***** TAILWATER *****

***** REGULAR CHANNEL CROSS SECTION *****
BOTTOM WIDTH (FT) 50.00
SIDE SLOPE H/V (X:1) 2.0
CHANNEL SLOPE V/H (FT/FT) 0.025
MANNING'S N (.01-0.1) 0.035
CHANNEL INVERT ELEVATION (FT) 95.00
CULVERT NO.1 OUTLET INVERT ELEVATION 95.00 FT

***** UNIFORM FLOW RATING CURVE FOR DOWNSTREAM CHANNEL

FLOW (CFS)	W.S.E. (FT)	FROUDE NUMBER	VEL. (FPS)	SHEAR (PSF)
0.00	95.00	0.000	0.00	0.00
15.00	95.15	0.862	1.93	0.24
30.00	95.23	0.922	2.53	0.37
45.00	95.30	0.958	2.97	0.47
60.00	95.36	0.984	3.33	0.55
75.00	95.41	1.005	3.63	0.63
90.00	95.45	1.022	3.90	0.71
105.00	95.50	1.036	4.14	0.78
120.00	95.54	1.049	4.37	0.84
135.00	95.58	1.060	4.57	0.90
140.00	95.59	1.063	4.63	0.92

***** ROADWAY OVERTOPPING DATA *****

ROADWAY SURFACE GRAVEL
EMBANKMENT TOP WIDTH (FT) 25.00
CREST LENGTH (FT) 100.00
OVERTOPPING CREST ELEVATION (FT) 110.00

H/T Basin Hydraulics

H-1 attall to Cottonwood Creek,
 $Q_{100} = 63 \text{ cfs}$

Assume 2% of Storm Sewer
 \therefore Need 30" pipe @ 2.4%

H-2: direct discharge to creek via ^{outside} detention basin outlet structures.

V-1 : "

V-2 : "

Bank Line Estimation: Tributary 4

Per page 12 of the criteria, use method outlined in 3.3.

$$Eros. \text{ Setback} = 2 (BH + ID) + VW$$

This is for erosion resistant materials. Our plan would be to line the outside ponds creating a "eros. resistant" bank.

Assume ID = 2' at all XSECS.

XSEC	Max BH	ID	VW	ESetback
1	22'	2	95	140'
2	36'	2	65	140
3	22	2	95	140
4	22'	2	70	115 120
5	12'	2	85	130 115
6	16	2	80	115
11	16	2	55	115
12	16	2	140	175
13	22	2	75	125
14	12	2	60	90
15	14	2	65	100
16	12	2	60	90
17	10	2	45	70
18	10	2	50	75
19	10	2	35	60
20	10	2	35	60

PROJECT LINE: COTTONWOOD

Same "erosion-resistant" assumption as Trib 4

<u>XSEC</u>	<u>MAX H</u>	<u>ID (I)</u>	<u>VW</u>	<u>EROS. SB</u>
1050.1	8'	4'	55	80
50.2	16'	4'	95'	135
50.3	20'	4'	80'	130
50.4	16'	4'	85'	125
50.5	32"	4'	70	140
60.1	28	4	140'	200
60.2	10'	↓	80'	110
60.3	14		90'	125
60.4	32'		55'	130
60.5	18		70	115
60.6	24		90'	145
60.7	18		40'	85

(1) Assume contact 4' for Cottonwood; w/ gabriestral in place.

NC	0.020	0.020	0.045	0.100	0.300	0	0	0	0	0
	POWERS BOULEVARD									
X1	1040.1	14	1120	1204	0	0	0	0	0	0
GR	6860	1000	6838	1055	6836	1072	6824	1100	6822	1108
GR	6820	1120	6814	1130	6814	1140	6816	1165	6818	1204
GR	6826	1240	6834	1276	6840	1310	6846	1350		
QT	1	2733								
X1	1040.2	10	1055	1078	550	550	550	0	0	0
GR	6864	1000	6824	1055	6822	1060	6824	1068	6826	1078
GR	6828	1105	6830	1118	6838	1165	6850	1198	6854	1210
X1	1040.3	14	1195	1333	675	675	675	0	0	0
GR	6870	1000	6862	1045	6854	1150	6852	1170	6840	1195
GR	6838	1222	6834	1230	6836	1240	6838	1262	6840	1333
GR	6842	1355	6850	1410	6860	1423	6870	1462		
X1	1040.4	10	1127	1250	525	525	525	0	0	0
GR	6878	1000	6870	1050	6862	1127	6850	1155	6848	1180
GR	6846	1238	6862	1250	6872	1295	6874	1310	6876	1380
X1	1040.5	12	1142	1195	550	550	550	0	0	0
GR	6884	1000	6878	1050	6862	1115	6858	1142	6856	1165
GR	6854	1170	6852	1172	6854	1180	6856	1195	6860	1215
GR	6876	1230	6880	1290						
	COWPOKE ROAD									
X1	1050.1	12	1058	1160	785	785	785	0	0	0
GR	6898	1000	6890	1030	6880	1058	6874	1080	6868	1095
GR	6868	1105	6872	1112	6876	1140	6884	1160	6892	1200
GR	6894	1215	6896	1232						

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PAGE 2

X1	1050.2	11	1124	1215	400	400	400	0	0	0
GR	6904	1000	6894	1072	6886	1090	6884	1110	6880	1124
GR	6876	1148	6872	1162	6874	1178	6880	1215	6898	1230
GR	6910	1290								
X1	1050.3	8	1090	1175	405	405	405	0	0	0
GR	6910	1000	6882	1090	6880	1120	6878	1150	6880	1158
GR	6886	1175	6900	1195	6912	1275				
QT	1	857								
X1	1050.4	13	1100	1160	540	540	540	0	0	0
GR	6920	1000	6914	1035	6896	1050	6892	1075	6912	1090
GR	6912	1100	6892	1112	6890	1120	6890	1135	6892	1160
GR	6900	1205	6912	1228	6920	1278				
X1	1050.5	15	1262	1380	490	490	490	0	0	0

GR	6930	1000	6924	1045	6923	1065	6924	1080	6926	1110
GR	6926	1142	6920	1190	6912	1262	6904	1290	6902	1302
GR	6900	1318	6900	1358	6904	1366	6910	1380	6922	1405

CSAGRICULTURAL

X1	1060.1	11	1107	1275	580	580	580	0	0	0
GR	6934	1000	6924	1075	6922	1088	6922	1107	6910	1123
GR	6908	1130	6910	1140	6910	1253	6914	1275	6924	1293
GR	6934	1345								

X1	1060.2	11	1100	1215	428	428	428	0	0	0
GR	6940	1000	6930	1085	6922	1100	6916	1140	6912	1155
GR	6914	1160	6916	1180	6918	1205	6920	1215	6930	1228
GR	6934	1268								

X1	1060.3	15	1065	1245	562	562	562	0	0	0
GR	6944	1000	6942	1025	6940	1065	6922	1098	6920	1108
GR	6922	1118	6924	1152	6926	1192	6932	1220	6934	1245
GR	6934	1300	6936	1320	6942	1340	6944	1362	6950	1410

X1	1060.4	8	1052	1136	443	443	443	0	0	0
GR	6950	1000	6948	1018	6932	1052	6930	1082	6926	1092
GR	6928	1100	6940	1136	6950	1153				

X1	1060.5	9	1026	1115	517	517	517	0	0	0
GR	6960	1000	6958	1015	6950	1026	6938	1032	6936	1040
GR	6938	1048	6940	1097	6950	1115	6956	1150		

X1	1060.6	10	1070	1111	300	300	300	0	0	0
GR	6962	1000	6950	1030	6946	1045	6942	1070	6938	1076
GR	6937	1090	6938	1105	6940	1111	6954	1145	6960	1203

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X1	1060.7	10	1103	1153	314	314	314	0	0	0
GR	6970	1000	6968	1060	6966	1078	6950	1103	6942	1118
GR	6941	1121	6942	1124	6948	1128	6950	1153	6966	1170

BLACK FOREST ROAD

X1	1070.1	9	1155	1167	196	196	196	0	0	0
GR	6976	1000	6974	1135	6972	1145	6950	1155	6946	1158
GR	6946	1162	6950	1167	6972	1184	6974	1219		

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SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	HL	OLOSS	BANK	ELEV
-------	-------	-------	------	-------	----	----	----	-------	------	------

Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 1

0

CCHV= .100 CEHV= .300

*SECNO 1040.100

3720 CRITICAL DEPTH ASSUMED

POWERS BOULEVARD

1040.10	5.80	6819.80	6819.80	6810.00	6821.61	1.81	.00	.00	6820.00
3477.	0.	3409.	68.	0.	315.	7.	0.	0.	6818.00
.00	.00	10.82	9.35	.000	.045	.020	.000	6814.00	1120.34
.018826	0.	0.	0.	0	20	0	.00	91.76	1212.09

0

*SECNO 1040.200

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

1040.20	7.85	6829.85	6829.85	.00	6831.81	1.96	6.92	.05	6824.00
2733.	283.	1332.	1118.	24.	138.	88.	4.	1.	6826.00
.01	12.02	9.68	12.67	.020	.045	.020	.000	6822.00	1046.95
.008293	550.	550.	550.	3	14	0	.00	70.09	1117.04

0

*SECNO 1040.300

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

1040.30	6.59	6840.59	6840.59	.00	6841.66	1.07	8.34	.09	6840.00
2733.	2.	2723.	9.	0.	327.	2.	8.	3.	6840.00
.04	4.37	8.32	4.67	.020	.045	.020	.000	6834.00	1193.78
.020369	675.	675.	675.	16	10	0	.00	145.69	1339.46

0

*SECNO 1040.400

1040.40	4.85	6850.85	6850.76	.00	6852.34	1.49	10.55	.12	6862.00
2733.	0.	2733.	0.	0.	279.	0.	12.	4.	6862.00
.05	.00	9.79	.00	.000	.045	.000	.000	6846.00	1153.02
.019828	525.	525.	525.	7	19	0	.00	88.62	1241.64

0

*SECNO 1040.500

7185 MINIMUM SPECIFIC ENERGY

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SECNO	DEPTH	CWSEL	CRISW	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

3720 CRITICAL DEPTH ASSUMED

1040.50	7.75	6859.75	6859.75	.00	6861.39	1.64	8.82	.05	6858.00
2733.	80.	2203.	450.	10.	226.	35.	15.	5.	6856.00
.07	7.75	9.77	12.82	.020	.045	.020	.000	6852.00	1130.21
.013225	550.	550.	550.	5	14	0	.00	83.52	1213.73

0

*SECNO 1050.100
 7185 MINIMUM SPECIFIC ENERGY
 3720 CRITICAL DEPTH ASSUMED
 COWPOKE ROAD

1050.10	7.79	6875.79	6875.79	.00	6877.70	1.91	12.70	.08	6880.00
2733.	0.	2733.	0.	0.	246.	0.	20.	7.	6884.00
.09	.00	11.10	.00	.000	.045	.000	.000	6868.00	1073.45
.020229	785.	785.	785.	11	5	0	.00	65.06	1138.51

0

*SECNO 1050.200

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 2.01

1050.20	8.75	6880.75	.00	.00	6881.40	.64	3.57	.13	6880.00
2733.	3.	2730.	0.	1.	424.	0.	23.	7.	6880.00
.10	2.67	6.44	2.04	.020	.045	.020	.000	6872.00	1121.36
.005004	400.	400.	400.	4	0	0	.00	94.27	1215.63

0

*SECNO 1050.300

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = .53

1050.30	5.59	6883.59	.00	.00	6885.13	1.55	3.46	.27	6882.00
2733.	33.	2700.	0.	4.	270.	0.	26.	8.	6886.00
.11	8.24	10.00	.00	.020	.045	.000	.000	6878.00	1084.90
.017840	405.	405.	405.	3	0	0	.00	83.26	1168.16

0

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SECNO	DEPTH	CWSEL	CRISW	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*SECNO 1050.400

3265 DIVIDED FLOW

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = .39

1050.40	3.23	6893.23	6892.88	.00	6893.89	.66	8.66	.09	6912.00
857.	30.	803.	25.	5.	123.	4.	29.	9.	6892.00
.14	5.62	6.55	5.79	.020	.045	.020	.000	6890.00	1067.31
.011827	540.	540.	540.	11	11	0	.00	64.28	1166.92

0

*SECNO 1050.500

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

1050.50	2.19	6902.19	6902.19	.00	6903.11	.92	8.13	.08	6912.00
857.	0.	857.	0.	0.	111.	0.	30.	10.	6910.00
.16	.00	7.70	.00	.000	.045	.000	.000	6900.00	1300.88
.024976	490.	490.	490.	8	14	0	.00	61.49	1362.37

0

*SECNO 1060.100

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 1.61

CSAGRICULTURAL									
1060.10	3.40	6911.40	.00	.00	6911.68	.27	8.50	.06	6922.00
857.	0.	857.	0.	0.	205.	0.	32.	11.	6914.00
.19	.00	4.17	.00	.000	.045	.000	.000	6908.00	1121.14
.009631	580.	580.	580.	6	0	0	.00	139.55	1260.69

0

*SECNO 1060.200

3301 HV CHANGED MORE THAN HVINS

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SECNO	DEPTH	CWSEL	CRISW	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = .66

1060.20	4.98	6916.98	.00	.00	6917.87	.89	6.01	.18	6922.00
857.	0.	857.	0.	0.	113.	0.	34.	12.	6920.00
.21	.00	7.55	.00	.000	.045	.000	.000	6912.00	1133.46
.022335	428.	428.	428.	4	0	0	.00	58.80	1192.26

0

*SECNO 1060.300

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 1.58

1060.30	5.04	6925.04	.00	.00	6925.44	.40	7.52	.05	6940.00
857.	0.	857.	0.	0.	169.	0.	36.	13.	6934.00
.24	.00	5.07	.00	.000	.045	.000	.000	6920.00	1092.43
.008900	562.	562.	562.	5	0	0	.00	80.29	1172.72

0

*SECNO 1060.400

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

1060.40	5.44	6931.44	6931.44	.00	6932.51	1.07	6.19	.20	6932.00
857.	0.	857.	0.	0.	103.	0.	37.	14.	6940.00
.26	.00	8.30	.00	.000	.045	.000	.000	6926.00	1060.38
.025000	443.	443.	443.	4	8	0	.00	49.95	1110.32

0

*SECNO 1060.500

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 1.44

1060.50	4.70	6940.70	.00	.00	6941.24	.54	8.68	.05	6950.00
857.	0.	857.	0.	0.	145.	0.	38.	14.	6950.00
.28	.00	5.90	.00	.000	.045	.000	.000	6936.00	1030.65
.012051	517.	517.	517.	6	0	0	.00	67.63	1098.27

0

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SECNO	DEPTH	CWSEL	CRISW	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*SECNO 1060.600

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 2.07

1060.60	5.48	6942.48	.00	.00	6942.80	.32	1.53	.02	6942.00
---------	------	---------	-----	-----	---------	-----	------	-----	---------

857.	1.	824.	32.	1.	180.	7.	40.	15.	6940.00
.30	1.50	4.57	4.31	.020	.045	.020	.000	6937.00	1067.01
.002606	300.	300.	300.	4	0	0	.00	50.01	1117.02

0

*SECNO 1060.700

3301 HV CHANGED MORE THAN HVINS

3685 20 TRIALS ATTEMPTED WSEL,CWSEL

3693 PROBABLE MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

1060.70	6.50	6947.50	6947.50	.00	6949.56	2.05	2.03	.52	6950.00
857.	0.	857.	0.	0.	75.	0.	41.	15.	6950.00
.31	.00	11.50	.00	.000	.045	.000	.000	6941.00	1107.68
.027701	314.	314.	314.	20	11	0	.00	19.99	1127.67

0

*SECNO 1070.100

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

BLACK FOREST ROAD

1070.10	6.81	6952.81	6952.81	.00	6955.14	2.33	4.62	.08	6950.00
857.	13.	814.	29.	2.	66.	3.	41.	15.	6950.00
.31	7.38	12.39	9.58	.020	.045	.020	.000	6946.00	1153.72
.020333	196.	196.	196.	1	8	0	.00	15.45	1169.17

0

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THIS RUN EXECUTED 7/12/ 4 16:41:24

 HEC2 RELEASE DATED SEP 88 UPDATED APR 1989

ERROR CORR - 01,02
 MODIFICATION -

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

COTTONWOOD CREEK FILENAM

SUMMARY PRINTOUT TABLE 150

SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRWS	EG	10*KS	VCH	AREA	.01K
* 1040.100	.00	.00	.00	6814.00	3477.00	6819.80	6819.80	6821.61	188.26	10.82	322.37	253.41

*	1040.200	550.00	.00	.00	6822.00	2733.00	6829.85	6829.85	6831.81	82.93	9.68	249.36	300.12
*	1040.300	675.00	.00	.00	6834.00	2733.00	6840.59	6840.59	6841.66	203.69	8.32	329.32	191.49
	1040.400	525.00	.00	.00	6846.00	2733.00	6850.85	6850.76	6852.34	198.28	9.79	279.09	194.09
*	1040.500	550.00	.00	.00	6852.00	2733.00	6859.75	6859.75	6861.39	132.25	9.77	270.96	237.65
*	1050.100	785.00	.00	.00	6868.00	2733.00	6875.79	6875.79	6877.70	202.29	11.10	246.24	192.16
*	1050.200	400.00	.00	.00	6872.00	2733.00	6880.75	.00	6881.40	50.04	6.44	424.93	386.36
*	1050.300	405.00	.00	.00	6878.00	2733.00	6883.59	.00	6885.13	178.40	10.00	274.10	204.62
*	1050.400	540.00	.00	.00	6890.00	857.00	6893.23	6892.88	6893.89	118.27	6.55	132.11	78.80
*	1050.500	490.00	.00	.00	6900.00	857.00	6902.19	6902.19	6903.11	249.76	7.70	111.33	54.23
*	1060.100	580.00	.00	.00	6908.00	857.00	6911.40	.00	6911.68	96.31	4.17	205.41	87.33
*	1060.200	428.00	.00	.00	6912.00	857.00	6916.98	.00	6917.87	223.35	7.55	113.46	57.34
*	1060.300	562.00	.00	.00	6920.00	857.00	6925.04	.00	6925.44	89.00	5.07	169.14	90.84
*	1060.400	443.00	.00	.00	6926.00	857.00	6931.44	6931.44	6932.51	250.00	8.30	103.29	54.20
*	1060.500	517.00	.00	.00	6936.00	857.00	6940.70	.00	6941.24	120.51	5.90	145.30	78.07
*	1060.600	300.00	.00	.00	6937.00	857.00	6942.48	.00	6942.80	28.06	4.57	188.29	161.79
*	1060.700	314.00	.00	.00	6941.00	857.00	6947.50	6947.50	6949.56	277.01	11.50	74.54	51.49

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	SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRISW	EG	10*KS	VCH	AREA	.01K
*	1070.100	196.00	.00	.00	6946.00	857.00	6952.81	6952.81	6955.14	203.33	12.39	70.59	60.10

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COTTONWOOD CREEK FILENAM

SUMMARY PRINTOUT TABLE 150

SECNO	Q	CWSEL	DIFWSP	DIFWSX	DIFKWS	TOPWID	XLCH
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*	1040.100	3477.00	6819.80	.00	.00	9.80	91.76	.00
*	1040.200	2733.00	6829.85	.00	10.05	.00	70.09	550.00
*	1040.300	2733.00	6840.59	.00	10.73	.00	145.69	675.00
	1040.400	2733.00	6850.85	.00	10.26	.00	88.62	525.00
*	1040.500	2733.00	6859.75	.00	8.90	.00	83.52	550.00
*	1050.100	2733.00	6875.79	.00	16.04	.00	65.06	785.00
*	1050.200	2733.00	6880.75	.00	4.97	.00	94.27	400.00
*	1050.300	2733.00	6883.59	.00	2.83	.00	83.26	405.00
*	1050.400	857.00	6893.23	.00	9.64	.00	64.28	540.00
*	1050.500	857.00	6902.19	.00	8.96	.00	61.49	490.00
*	1060.100	857.00	6911.40	.00	9.22	.00	139.55	580.00
*	1060.200	857.00	6916.98	.00	5.58	.00	58.80	428.00
*	1060.300	857.00	6925.04	.00	8.05	.00	80.29	562.00
*	1060.400	857.00	6931.44	.00	6.40	.00	49.95	443.00
*	1060.500	857.00	6940.70	.00	9.26	.00	67.63	517.00
*	1060.600	857.00	6942.48	.00	1.77	.00	50.01	300.00
*	1060.700	857.00	6947.50	.00	5.03	.00	19.99	314.00
*	1070.100	857.00	6952.81	.00	5.31	.00	15.45	196.00

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1*****
* WATER SURFACE PROFILES *
* VERSION OF SEPTEMBER 1988 *
* ERROR: 01,02 *
* UPDATED: 4 APRIL 1989 *
* RUN DATE 7/12/ 4 TIME 16:39:20 *
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* U.S. ARMY CORPS OF ENGINEERS *
* THE HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616-4687 *
* (916) 756-1104, (916) 551-1748 *
*****

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X . X XXXXXXX XXXXX XXXXX
X X X X X X X
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END OF BANNER

1 7/12/ 4 16:39:20

PAGE 1

THIS RUN EXECUTED 7/12/ 4 16:39:20

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*****
HEC2 RELEASE DATED SEP 88 UPDATED APR 1989

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ERROR CORR - 01,02
MODIFICATION -

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T1 TRIBUTARY FOUR WOLF RANCH MDDP KIOWA ENGINEERING PN 03094
T2 100-YEAR FREQUENCY DEVELOPED W/O DETETNION X-SECTIONS L TO R UPSTREA
T3 FILENAME TRIB4.DAT

```

J1	ICHECK	INQ	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FQ
	0	2	0	0	.02	0	0	0	6878	0
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	1	0	-1	0	0	0	0	0	0	0

QT 1 1870

QT 1 1830

NORTH RESEARCH PARKWAY

X1	9	23	1086	1149	162	162	162	0	0	0
GR	6983	1000	6982	1006	6980	1018	6978	1033	6976	1059
GR	6974	1076	6972	1081	6970	1086	6968	1090	6966	1095
GR	6964	1104	6963	1112	6964	1119	6966	1141	6968	1146
GR	6970	1149	6972	1151	6974	1154	6976	1156	6978	1159
GR	6980	1161	6982	1163	6983	1164				

X1	10	20	1017	1091	411	411	411	0	0	0
GR	6990	1000	6988	1005	6986	1008	6984	1012	6982	1014
GR	6980	1017	6978	1019	6976	1024	6974	1029	6972	1037
GR	6970	1048	6972	1055	6974	1070	6976	1076	6978	1083
GR	6980	1091	6982	1099	6986	1110	6988	1126	6990	1141

X1	11	31	1048	1132	407	407	407	0	0	0
GR	7004	1000	7002	1012	7000	1018	7002	1022	7004	1025
GR	7006	1033	7008	1038	6990	1048	6988	1056	6986	1064
GR	6984	1074	6982	1081	6980	1087	6980	1090	6981	1099
GR	6980	1107	6978	1115	6978	1118	6980	1123	6982	1124
GR	6984	1126	6986	1127	6988	1129	6990	1132	6992	1135
GR	6994	1139	6996	1143	6998	1146	7000	1153	7002	1164
GR	7004	1173								

QT 1 1160

X1	12	29	1077	1291	585	585	585	0	0	0
GR	7020	1000	7018	1015	7016	1034	7014	1048	7012	1061
GR	7010	1077	7008	1096	7006	1112	7004	1134	7004	1181
GR	7002	1198	7000	1216	7000	1238	7002	1268	7004	1275
GR	7006	1279	7008	1282	7010	1291	7012	1304	7014	1325

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GR	7015	1332	7014	1340	7013	1345	7014	1346	7016	1351
GR	7018	1356	7020	1362	7021	1380	7020	1409		

X1	13	23	1018	1195	443	443	443	0	0	0
GR	7028	1000	7026	1003	7024	1008	7022	1013	7020	1018
GR	7018	1022	7016	1025	7014	1041	7012	1046	7010	1053
GR	7008	1063	7007	1077	7008	1093	7010	1119	7012	1157
GR	7014	1168	7016	1177	7018	1186	7020	1195	7022	1202
GR	7024	1213	7026	1224	7028	1237				

X1	14	22	1037	1135	634	634	634	0	0	0
GR	7042	1000	7040	1009	7038	1022	7036	1033	7034	1034
GR	7032	1036	7030	1037	7028	1038	7026	1041	7024	1048

GR	7022	1066	7023	1092	7024	1114	7026	1121	7028	1127
GR	7030	1135	7032	1144	7034	1176	7036	1191	7038	1201
GR	7040	1248	7042	1263						
X1	15	26	1112	1197	438	438	438	0	0	0
GR	7054	1000	7053	1017	7053	1043	7052	1068	7050	1070
GR	7048	1074	7046	1081	7044	1086	7044	1097	7042	1106
GR	7040	1112	7038	1118	7036	1127	7035	1139	7034	1154
GR	7035	1177	7036	1188	7038	1192	7040	1197	7042	1211
GR	7044	1225	7046	1246	7046	1291	7047	1310	7050	1358
GR	7054	1392								
X1	16	18	1161	1259	352	352	352	0	0	0
GR	7060	1000	7054	1057	7053	1104	7052	1159	7050	1161
GR	7042	1173	7040	1177	7041	1200	7042	1222	7044	1233
GR	7046	1244	7048	1252	7050	1259	7052	1267	7054	1280
GR	7056	1296	7058	1315	7060	1335				
X1	17	18	1067	1163	382	382	382	0	0	0
GR	7068	1000	7064	1034	7060	1067	7058	1079	7056	1087
GR	7054	1092	7052	1097	7050	1101	7049	1111	7048	1125
GR	7049	1137	7050	1144	7054	1152	7060	1163	7062	1180
GR	7064	1209	7066	1243	7068	1285				
X1	18	21	1165	1261	416	416	416	0	0	0
GR	7076	1000	7074	1020	7073	1042	7072	1080	7072	1136
GR	7072	1153	7070	1165	7068	1173	7060	1182	7058	1185
GR	7057	1189	7056	1195	7057	1214	7058	1228	7060	1232
GR	7066	1243	7068	1249	7070	1261	7072	1277	7074	1297
GR	7076	1307								
X1	19	27	1178	1337	480	480	480	0	0	0
GR	7088	1000	7086	1038	7084	1080	7083	1096	7083	1101
GR	7083	1140	7082	1175	7080	1178	7072	1190	7070	1198
GR	7069	1206	7068	1217	7069	1223	7070	1227	7074	1235
GR	7076	1240	7078	1248	7079	1277	7078	1314	7079	1326
GR	7080	1337	7084	1371	7085	1382	7086	1395	7086	1473
GR	7087	1505	7088	1531						

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PAGE 4

TRIBUTARY FOUR LIMITS										
X1	20	19	1054	1085	363	363	363	0	0	0
GR	7094	1000	7090	1024	7086	1040	7084	1044	7076	1054
GR	7075	1057	7074	1060	7075	1074	7076	1085	7078	1089
GR	7080	1093	7082	1096	7084	1100	7086	1104	7088	1108
GR	7090	1116	7092	1128	7093	1140	7094	1153		

1

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SECNO	DEPTH	CWSEL	CRIWS	WSELK	EG	HV	HL	OLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

*PROF 1

CCHV# .100 CEHV= .300

*SECNO 1.000

TRIBUTARY FOUR

1.00	5.35	6895.35	.00	6878.00	6896.62	1.27	.00	.00	6900.00
1870.	0.	1870.	0.	0.	207.	0.	0.	0.	6900.00
.00	.00	9.03	.00	.000	.045	.000	.000	6890.00	1017.65
.020013	0.	0.	0.	0	0	8	.00	75.20	1092.84

0

*SECNO 2.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

2.00	5.24	6905.24	6905.24	.00	6906.60	1.36	8.88	.03	6910.00
1870.	0.	1870.	0.	0.	200.	0.	2.	1.	6910.00
.01	.00	9.36	.00	.000	.045	.000	.000	6900.00	1094.85
.021833	425.	425.	425.	4	8	0	.00	73.82	1168.67

0

*SECNO 3.000

3.00	3.65	6913.65	.00	.00	6914.74	1.08	8.11	.03	6920.00
1870.	0.	1870.	0.	0.	224.	0.	4.	1.	6920.00
.03	.00	8.36	.00	.000	.045	.000	.000	6910.00	1013.17
.020447	384.	384.	384.	2	0	0	.00	93.63	1106.80

0

*SECNO 4.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

4.00	4.09	6924.09	6924.09	.00	6925.39	1.30	9.29	.07	6930.00
1870.	0.	1870.	0.	0.	204.	0.	6.	2.	6930.00
.04	.00	9.16	.00	.000	.045	.000	.000	6920.00	1041.68
.022526	433.	433.	433.	3	8	0	.00	79.41	1121.09

0

*SECNO 5.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

5.00	5.16	6933.16	6933.16	.00	6934.43	1.27	8.28	.00	6940.00
1870.	0.	1870.	0.	0.	207.	0.	8.	3.	6940.00
.05	.00	9.05	.00	.000	.045	.000	.000	6928.00	1056.89
.023082	363.	363.	363.	5	11	0	.00	83.68	1140.56

0

1

SECNO	DEPTH	CWSEL	CRIWS	WSELK	EG	HV	HL	OLOSS	BANK	ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT	
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA	
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST	

*SECNO 6.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

6.00	4.69	6948.69	6948.69	.00	6950.17	1.47	15.16	.06	6960.00
1870.	0.	1870.	0.	0.	192.	0.	11.	4.	6960.00
.07	.00	9.74	.00	.000	.045	.000	.000	6944.00	1023.65
.022331	668.	668.	668.	3	11	0	.00	66.82	1090.47

0

*SECNO 7.000

7.00	5.48	6957.48	6957.41	.00	6958.75	1.27	8.57	.02	6960.00
1870.	0.	1870.	0.	0.	206.	0.	13.	5.	6960.00
.08	.00	9.06	.00	.000	.045	.000	.000	6952.00	1218.02
.021726	389.	389.	389.	5	11	0	.00	77.88	1295.91

0

*SECNO 8.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

SOUTH RESEARCH PARKWAY

8.00	4.33	6965.33	6965.33	.00	6966.89	1.56	6.86	.08	6970.00
1870.	0.	1870.	0.	0.	187.	0.	14.	5.	6970.00
.09	.00	10.01	.00	.000	.045	.000	.000	6961.00	1051.55
.021184	320.	320.	320.	3	15	0	.00	61.12	1112.67

0

*SECNO 9.000

NORTH RESEARCH PARKWAY

9.00	5.51	6968.51	.00	.00	6969.82	1.31	2.90	.03	6970.00
1830.	0.	1830.	0.	0.	200.	0.	15.	6.	6970.00
.09	.00	9.17	.00	.000	.045	.000	.000	6963.00	1088.98
.015283	162.	162.	162.	2	0	0	.00	57.79	1146.77

0

*SECNO 10.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

10.00	6.10	6976.10	6976.10	.00	6977.79	1.69	7.30	.12	6980.00
1830.	0.	1830.	0.	0.	175.	0.	16.	6.	6980.00
.11	.00	10.44	.00	.000	.045	.000	.000	6970.00	1023.75
.020892	411.	411.	411.	2	8	0	.00	52.61	1076.35

0

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SECNO	DEPTH	CWSEL	CRIWS	WSELK	EG	HV	HL	OLOSS	BANK	ELEV
-------	-------	-------	-------	-------	----	----	----	-------	------	------

Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

```

*SECNO 11.000
  11.00   6.06  6984.06   .00   .00  6985.53   1.48   7.72   .02  6990.00
  1830.   0.   1830.   0.   0.   188.   0.   18.   7.   6990.00
    .12   .00   9.75   .00   .000   .045   .000   .000  6978.00  1073.69
  .017284  407.   407.   407.   3     0     0     .00   52.34  1126.03
  
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0

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*SECNO 12.000
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3301 HV CHANGED MORE THAN HVINS
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7185 MINIMUM SPECIFIC ENERGY
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3720 CRITICAL DEPTH ASSUMED
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  12.00   2.75  7002.75  7002.75   .00  7003.71   .95  11.50   .05  7010.00
  1160.   0.   1160.   0.   0.   148.   0.   20.   7.   7010.00
    .14   .00   7.84   .00   .000   .045   .000   .000  7000.00  1191.61
  .024520  585.   585.   585.   10    14    0     .00   79.02  1270.63
  
```

0

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*SECNO 13.000
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  13.00   3.97  7010.97   .00   .00  7011.57   .61   7.83   .03  7020.00
  1160.   0.   1160.   0.   0.   185.   0.   22.   8.   7020.00
    .16   .00   6.26   .00   .000   .045   .000   .000  7007.00  1049.61
  .013353  443.   443.   443.   5     0     0     .00   87.76  1137.38
  
```

0

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*SECNO 14.000
```

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7185 MINIMUM SPECIFIC ENERGY
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3720 CRITICAL DEPTH ASSUMED
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  14.00   3.09  7025.09  7025.09   .00  7026.10   1.00  11.19   .12  7030.00
  1160.   0.   1160.   0.   0.   144.   0.   25.   9.   7030.00
    .18   .00   8.04   .00   .000   .045   .000   .000  7022.00  1044.18
  .024389  634.   634.   634.   10    15    0     .00   73.65  1117.82
  
```

0

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*SECNO 15.000
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7185 MINIMUM SPECIFIC ENERGY
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3720 CRITICAL DEPTH ASSUMED
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  15.00   3.13  7037.13  7037.13   .00  7038.17   1.04  10.47   .01  7040.00
  1160.   0.   1160.   0.   0.   142.   0.   26.  10.   7040.00
    .19   .00   8.18   .00   .000   .045   .000   .000  7034.00  1121.90
  .023422  438.   438.   438.   4     5     0     .00   68.37  1190.27
  
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SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	HL	GLOSS	BANK	ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT	
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA	
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST	

```

*SECNO 16.000
 16.00  3.92  7043.92  .00  .00  7044.77  .86  6.58  .02  7050.00
 1160.  0.  1160.  0.  0.  156.  0.  27.  11.  7050.00
 .21  .00  7.42  .00  .000  .045  .000  .000  7040.00  1170.13
 .015269  352.  352.  352.  5  0  0  .00  62.42  1232.54

```

0

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*SECNO 17.000
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
 17.00  3.71  7051.71  7051.71  .00  7053.01  1.30  7.04  .13  7060.00
 1160.  0.  1160.  0.  0.  127.  0.  28.  11.  7060.00
 .22  .00  9.15  .00  .000  .045  .000  .000  7048.00  1097.58
 .022673  382.  382.  382.  3  11  0  .00  49.84  1147.42

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0

```

*SECNO 18.000
 18.00  4.00  7060.00  .00  .00  7061.07  1.07  8.04  .02  7070.00
 1160.  0.  1160.  0.  0.  140.  0.  30.  12.  7070.00
 .23  .00  8.31  .00  .000  .045  .000  .000  7056.00  1182.00
 .016680  416.  416.  416.  5  0  0  .00  50.01  1232.00

```

0

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*SECNO 19.000
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
 19.00  4.46  7072.46  7072.46  .00  7073.89  1.43  9.13  .11  7080.00
 1160.  0.  1160.  0.  0.  121.  0.  31.  12.  7080.00
 .25  .00  9.60  .00  .000  .045  .000  .000  7068.00  1189.31
 .021908  480.  480.  480.  10  8  0  .00  42.62  1231.92

```

0

```

*SECNO 20.000
TRIBUTARY FOUR LIMITS
 20.00  4.78  7078.78  .00  .00  7080.09  1.31  6.18  .01  7076.00
 1160.  18.  1108.  35.  5.  119.  8.  32.  13.  7076.00
 .26  3.66  9.34  4.49  .050  .045  .050  .000  7074.00  1050.53
 .013610  363.  363.  363.  4  0  0  .00  40.02  1090.55

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THIS RUN EXECUTED 7/12/ 4 16:39:20

HEC2 RELEASE DATED SEP 88 UPDATED APR 1989

ERROR CORR - 01,02
MODIFICATION -

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

FILENAME TRIB4.DAT

SUMMARY PRINTOUT TABLE 150

	SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRWS	EG	10*KS	VCH	AREA	.01K
	1.000	.00	.00	.00	6890.00	1870.00	6895.35	.00	6896.62	200.13	9.03	207.07	132.18
*	2.000	425.00	.00	.00	6900.00	1870.00	6905.24	6905.24	6906.60	218.33	9.36	199.69	126.56
	3.000	384.00	.00	.00	6910.00	1870.00	6913.65	.00	6914.74	204.47	8.36	223.76	130.78
*	4.000	433.00	.00	.00	6920.00	1870.00	6924.09	6924.09	6925.39	225.26	9.16	204.15	124.60
*	5.000	363.00	.00	.00	6928.00	1870.00	6933.16	6933.16	6934.43	230.82	9.05	206.68	123.08
*	6.000	668.00	.00	.00	6944.00	1870.00	6948.69	6948.69	6950.17	223.31	9.74	192.07	125.14
	7.000	389.00	.00	.00	6952.00	1870.00	6957.48	6957.41	6958.75	217.26	9.06	206.48	126.87
*	8.000	320.00	.00	.00	6961.00	1870.00	6965.33	6965.33	6966.89	211.84	10.01	186.81	128.48
	9.000	162.00	.00	.00	6963.00	1830.00	6968.51	.00	6969.82	152.83	9.17	199.56	148.03
*	10.000	411.00	.00	.00	6970.00	1830.00	6976.10	6976.10	6977.79	208.92	10.44	175.29	126.61
	11.000	407.00	.00	.00	6978.00	1830.00	6984.06	.00	6985.53	172.84	9.75	187.74	139.20
*	12.000	585.00	.00	.00	7000.00	1160.00	7002.75	7002.75	7003.71	245.20	7.84	148.03	74.08
	13.000	443.00	.00	.00	7007.00	1160.00	7010.97	.00	7011.57	133.53	6.26	185.37	100.39
*	14.000	634.00	.00	.00	7022.00	1160.00	7025.09	7025.09	7026.10	243.89	8.04	144.27	74.28
*	15.000	438.00	.00	.00	7034.00	1160.00	7037.13	7037.13	7038.17	234.22	8.18	141.84	75.80
	16.000	352.00	.00	.00	7040.00	1160.00	7043.92	.00	7044.77	152.69	7.42	156.26	93.88
*	17.000	382.00	.00	.00	7048.00	1160.00	7051.71	7051.71	7053.01	226.73	9.15	126.83	77.04

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	SECNO	XLCH	ELTRD	ELLC	ELMIN	Q	CWSEL	CRWS	EG	10*KS	VCH	AREA	.01K
	18.000	416.00	.00	.00	7056.00	1160.00	7060.00	.00	7061.07	166.80	8.31	139.62	89.82

*	19.000	480.00	.00	.00	7068.00	1160.00	7072.46	7072.46	7073.89	219.08	9.60	120.83	78.37
	20.000	363.00	.00	.00	7074.00	1160.00	7078.78	.00	7080.09	136.10	9.34	131.11	99.43

1

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PAGE 11

FILENAME TRIB4.DAT

SUMMARY PRINTOUT TABLE 150

	SECNO	Q	CWSEL	DIFWSP	DIFWSX	DIFKWS	TOPWID	XLCH
	1.000	1870.00	6895.35	.00	.00	17.35	75.20	.00
*	2.000	1870.00	6905.24	.00	9.89	.00	73.82	425.00
	3.000	1870.00	6913.65	.00	8.42	.00	93.63	384.00
*	4.000	1870.00	6924.09	.00	10.44	.00	79.41	433.00
*	5.000	1870.00	6933.16	.00	9.07	.00	83.68	363.00
*	6.000	1870.00	6948.69	.00	15.53	.00	66.82	668.00
	7.000	1870.00	6957.48	.00	8.79	.00	77.88	389.00
*	8.000	1870.00	6965.33	.00	7.85	.00	61.12	320.00
	9.000	1830.00	6968.51	.00	3.18	.00	57.79	162.00
*	10.000	1830.00	6976.10	.00	7.59	.00	52.61	411.00
	11.000	1830.00	6984.06	.00	7.96	.00	52.34	407.00
*	12.000	1160.00	7002.75	.00	18.70	.00	79.02	585.00
	13.000	1160.00	7010.97	.00	8.21	.00	87.76	443.00
*	14.000	1160.00	7025.09	.00	14.13	.00	73.65	634.00
*	15.000	1160.00	7037.13	.00	12.04	.00	68.37	438.00
	16.000	1160.00	7043.92	.00	6.78	.00	62.42	352.00
*	17.000	1160.00	7051.71	.00	7.79	.00	49.84	382.00
	18.000	1160.00	7060.00	.00	8.29	.00	50.01	416.00

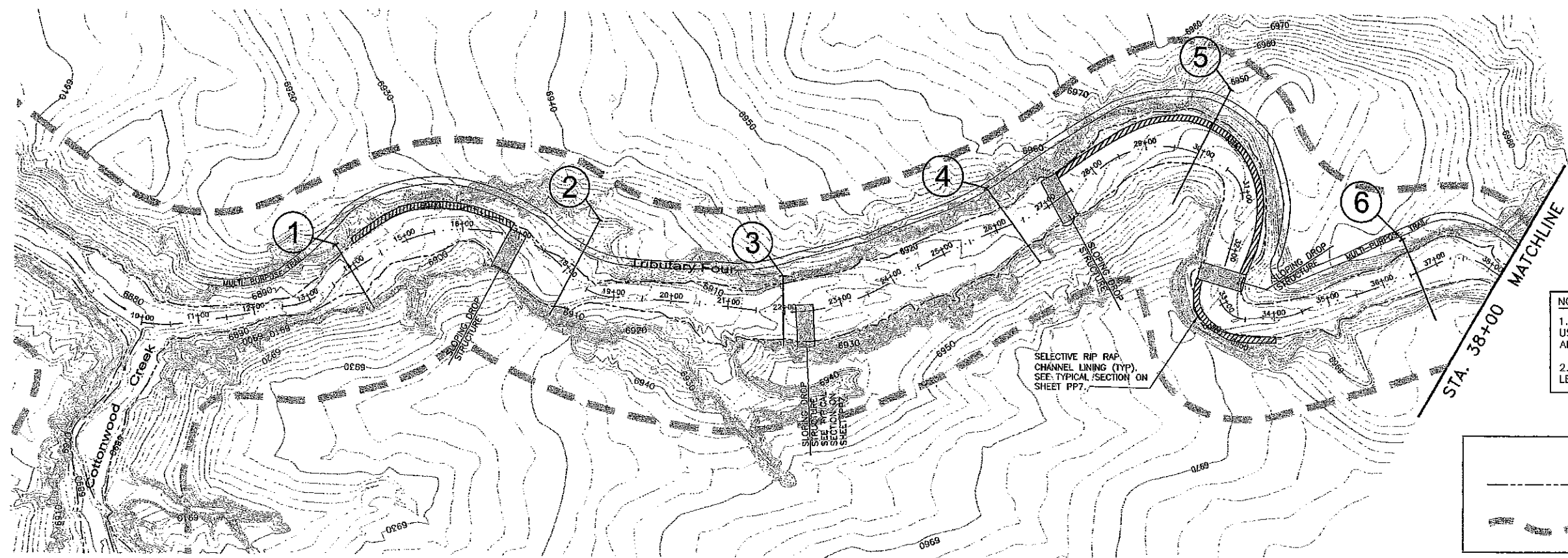
*	19.000	1160.00	7072.46	.00	12.46	.00	42.62	480.00
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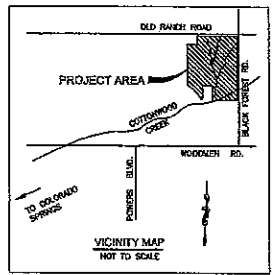
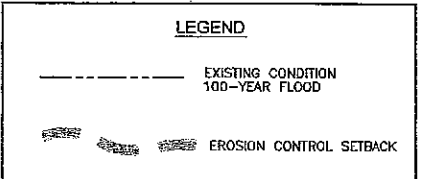
APPENDIX C

PLAN AND PROFILES



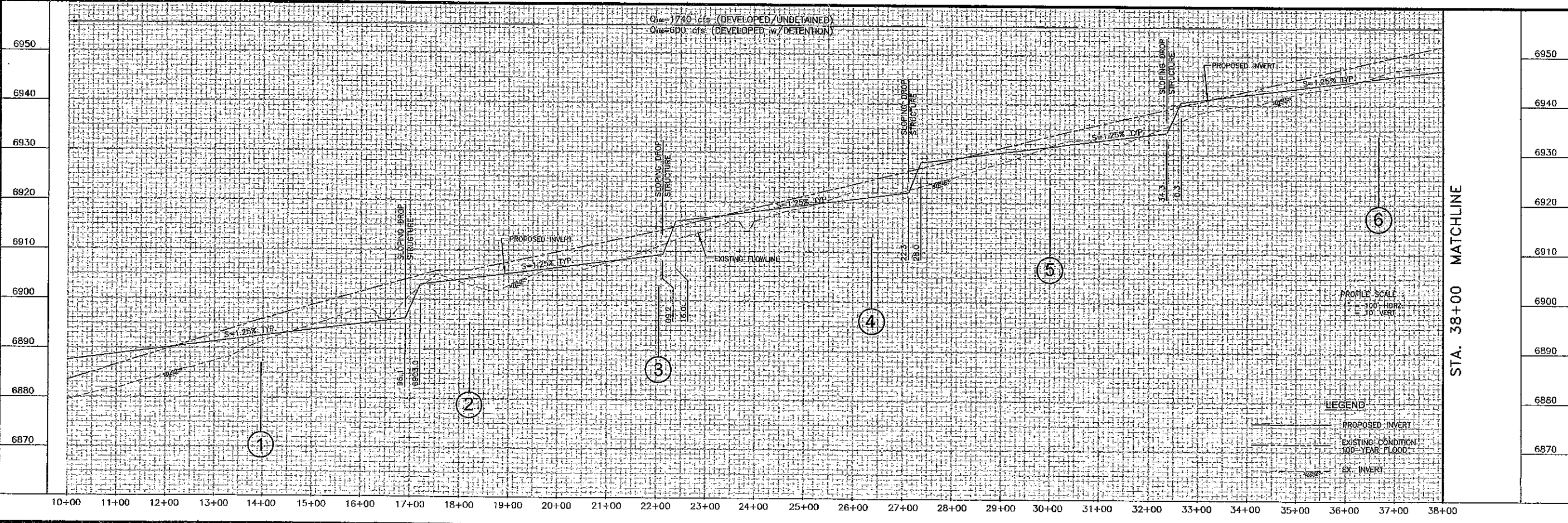
NOTES :

1. FLOODPLAIN SHOWN DETERMINED USING THE 100-YEAR DEVELOPED AND UNDETAINED.
2. CROSS-SECTIONS ORIENTED LEFT-TO-RIGHT FACING UPSTREAM.



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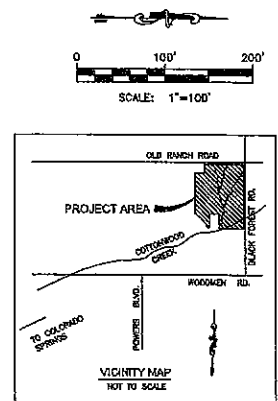
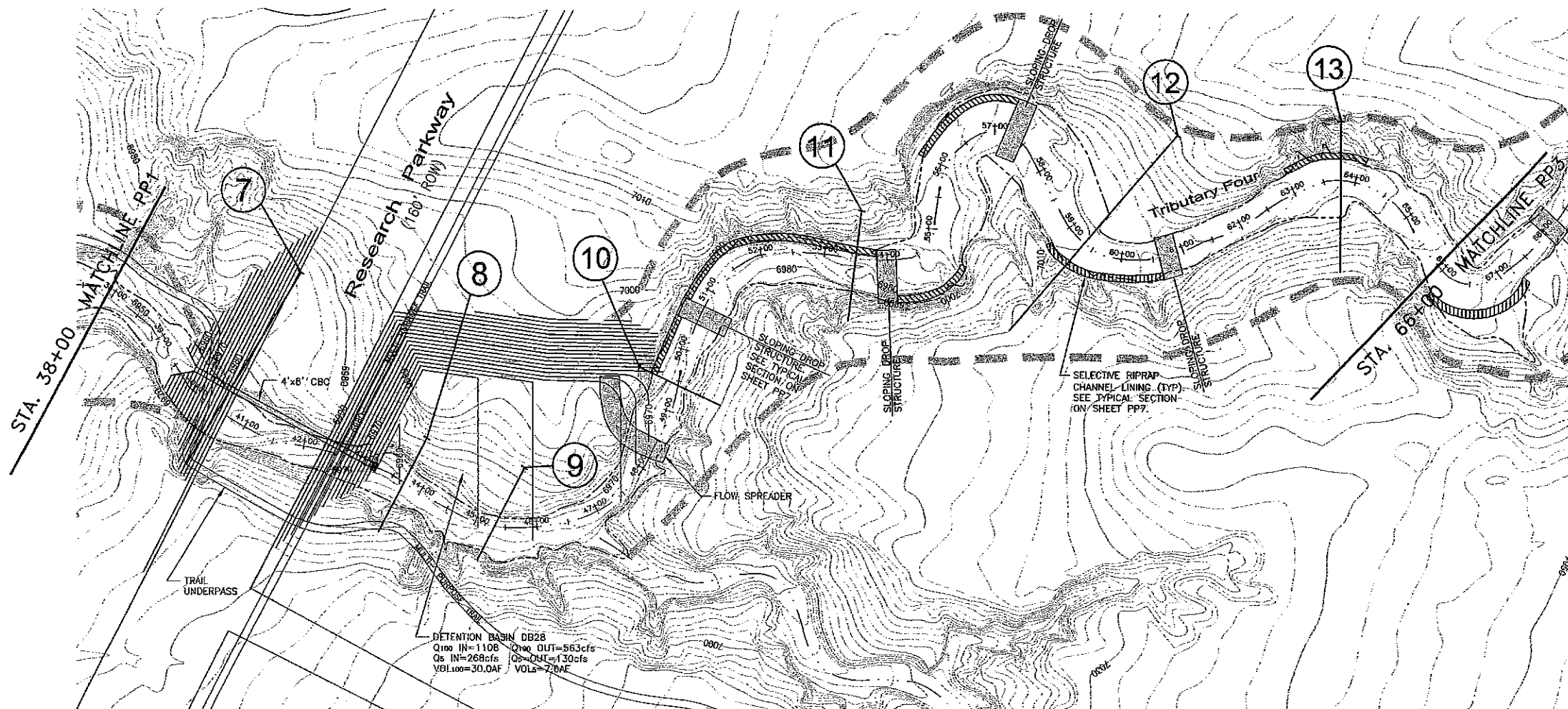
WOLF RANCH
MASTER DEVELOPMENT DRAINAGE PLAN
TRIBUTARY FOUR
PLAN & PROFILE
 COLORADO SPRINGS, COLORADO



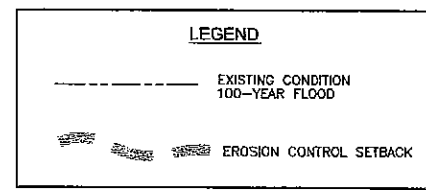
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 Date: 02/13/04
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 Drawn: JLN
 Check: RNW
 Revisions:

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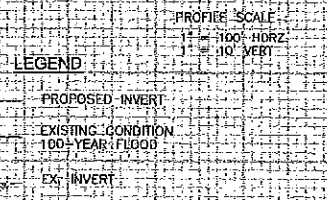
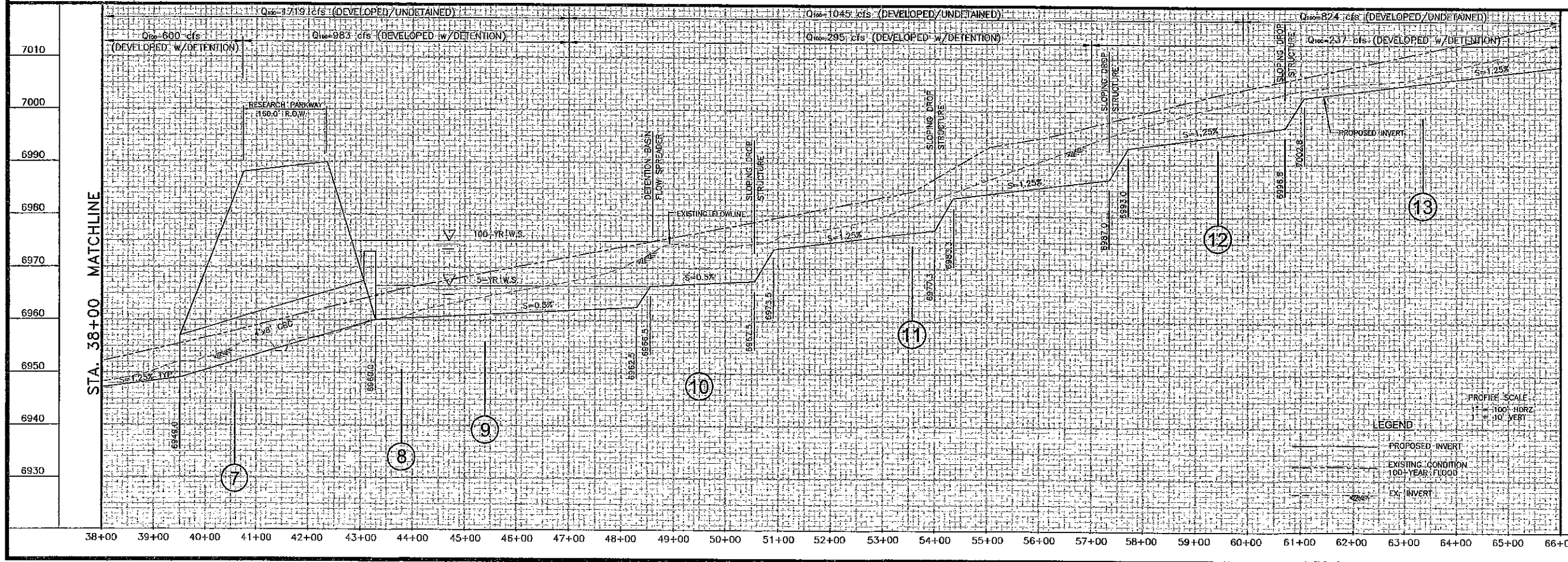
03094 p1-3.dwg/Dec 01, 2004



- NOTES:
1. FLOODPLAIN SHOWN DETERMINED USING THE 100-YEAR DEVELOPED AND UNDETAINED.
 2. CROSS-SECTIONS ORIENTED LEFT-TO-RIGHT FACING UPSTREAM.



DETENTION BASIN DB28
 $Q_{100} IN = 1108$ $Q_{100} OUT = 563 cfs$
 $Q_5 IN = 268 cfs$ $Q_5 OUT = 130 cfs$
 $VOL_{100} = 30.0 AF$ $VOL_5 = 7.6 AF$



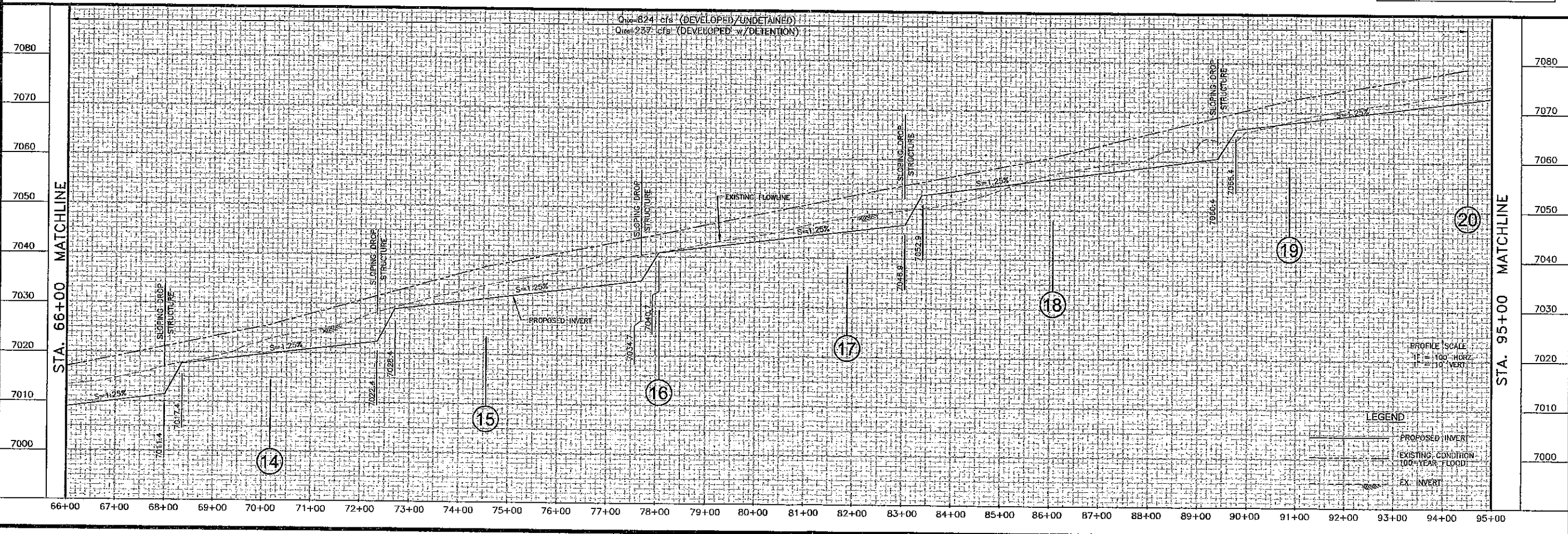
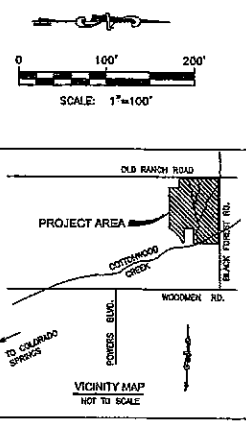
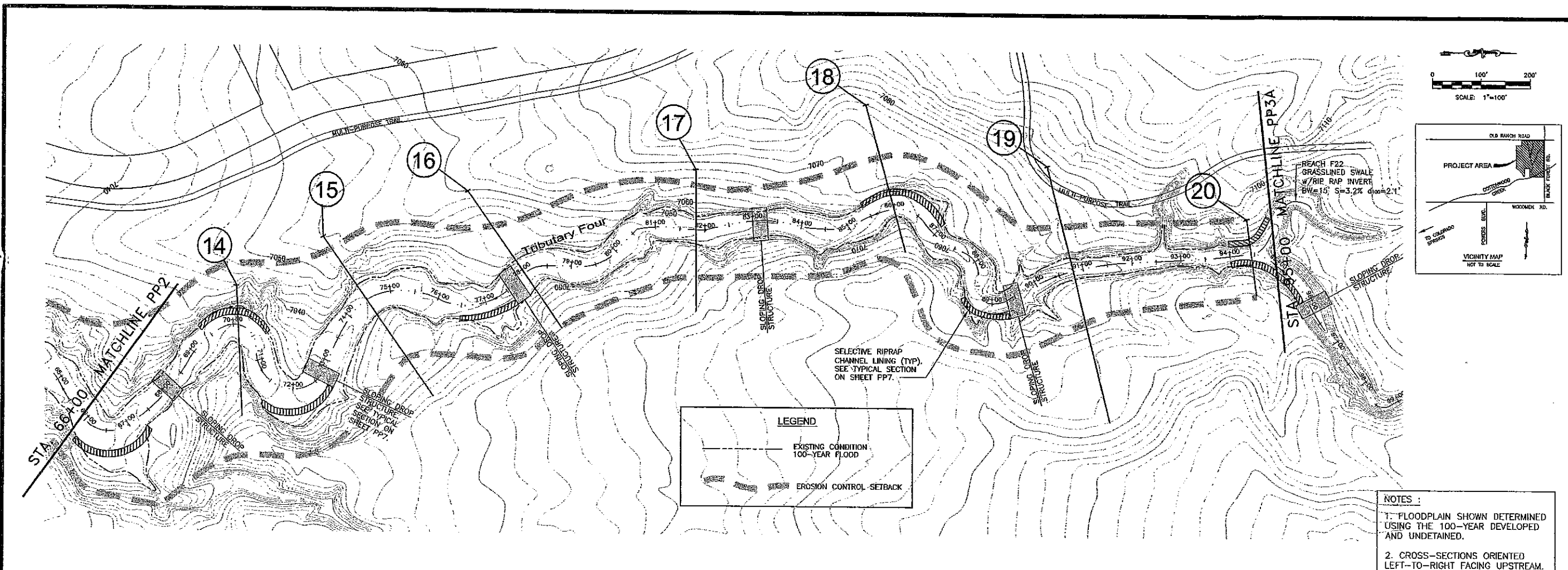
PROFILE SCALE
 1" = 100' HORIZ.
 1" = 10' VERT.

WOLF RANCH
 MASTER DEVELOPMENT DRAINAGE PLAN
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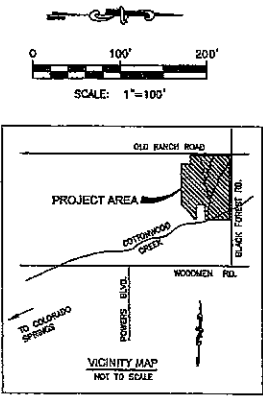
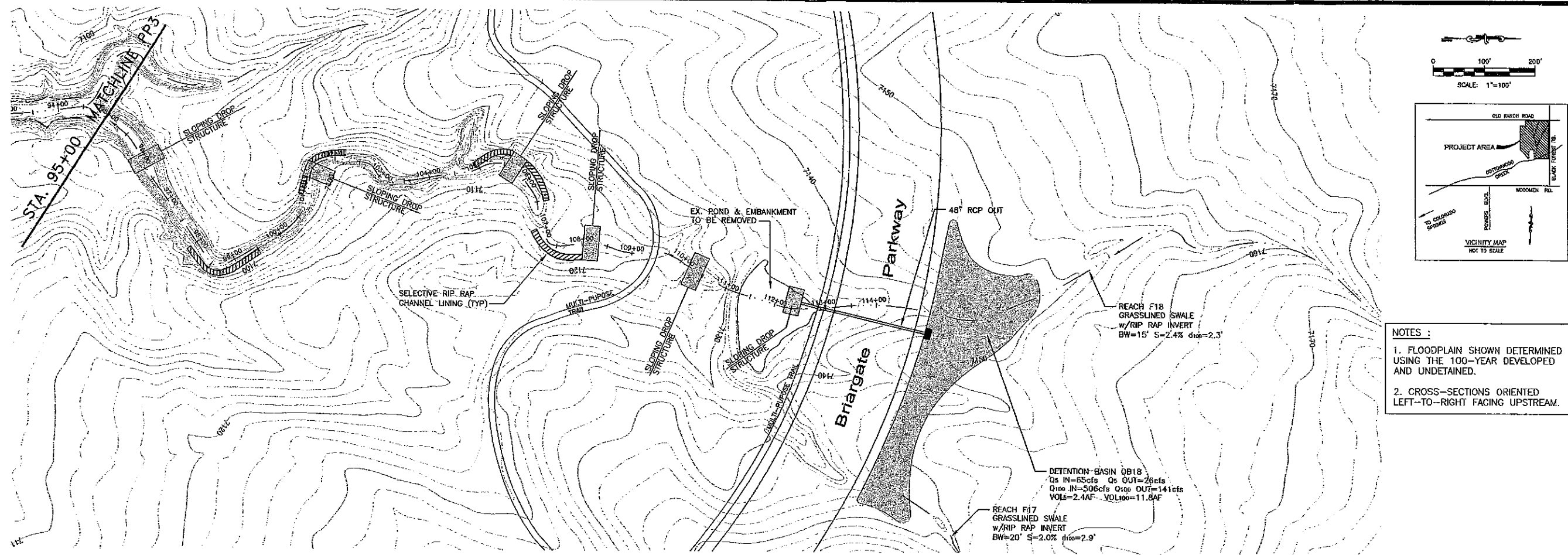
WOLF RANCH
MASTER DEVELOPMENT DRAINAGE PLAN
TRIBUTARY FOUR
PLAN & PROFILE
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PP3
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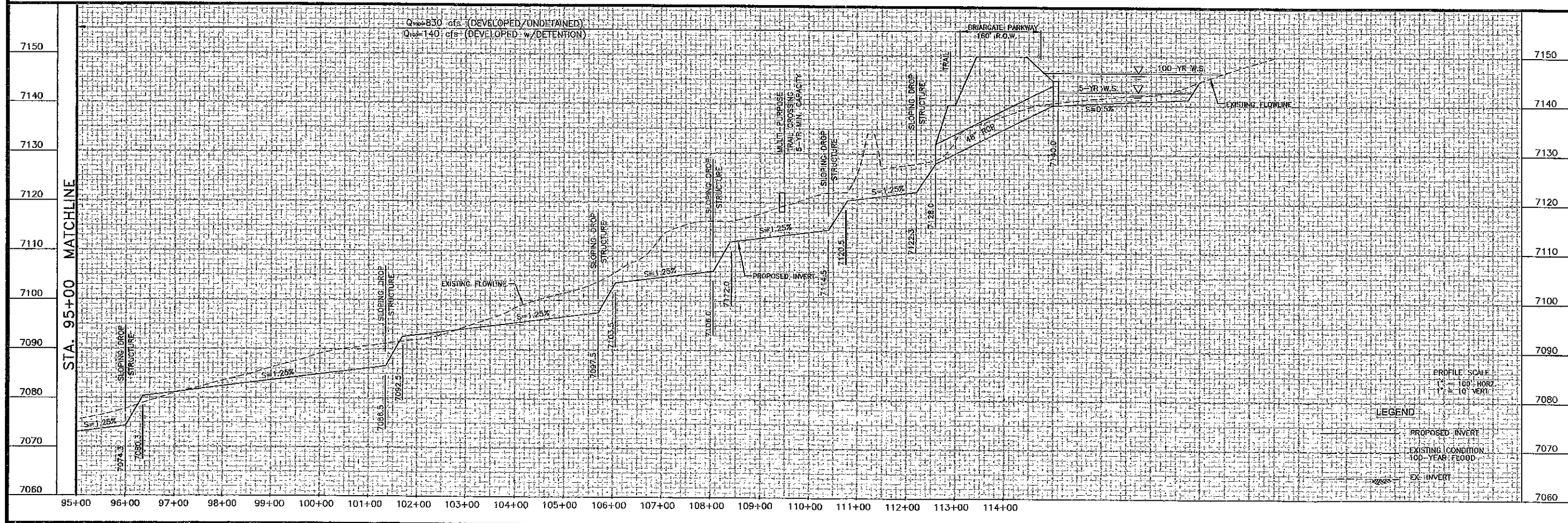
03094_pp1-3.dwg/04c 01, 2004



- NOTES :**
1. FLOODPLAIN SHOWN DETERMINED USING THE 100-YEAR DEVELOPED AND UNDETAINED.
 2. CROSS-SECTIONS ORIENTED LEFT-TO-RIGHT FACING UPSTREAM.

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TRIBUTARY FOUR
PLAN & PROFILE
 COLORADO SPRINGS, COLORADO



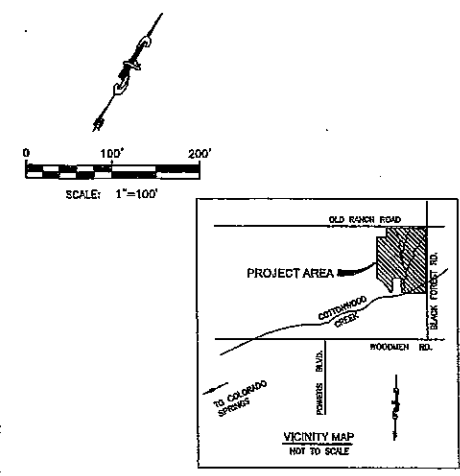
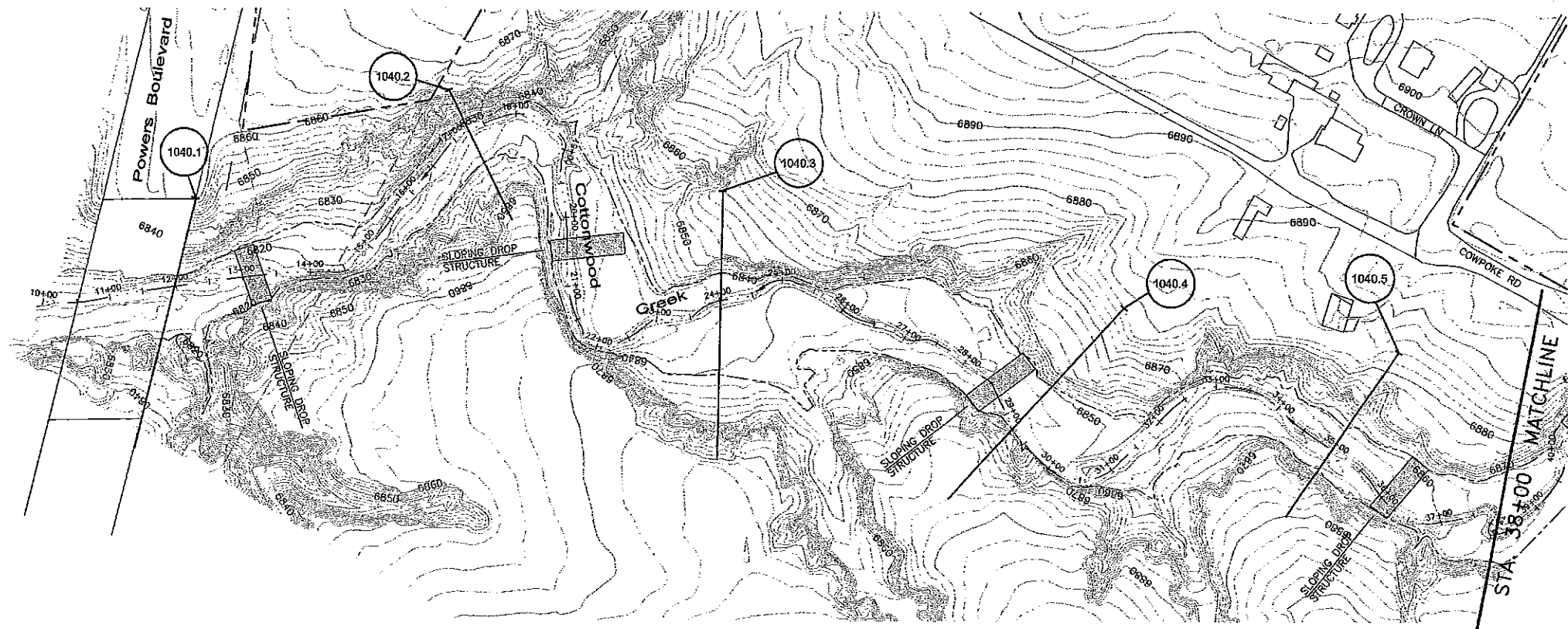
PROFILE SCALE:
 1" = 100' HORZ.
 1" = 10' VERT.

LEGEND

— PROPOSED INVERT
 - - - EXISTING CONDITION
 --- 100-YEAR FLOOD
 --- EX-INVERT

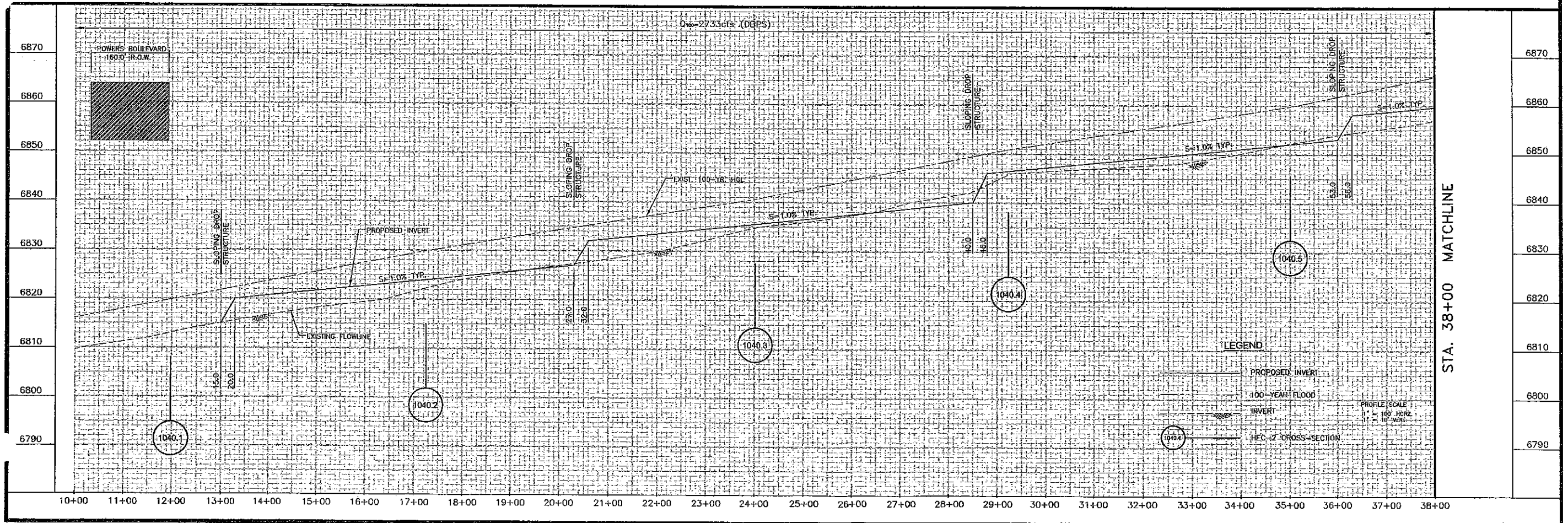
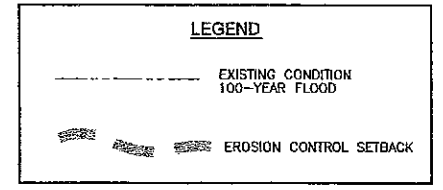
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 OF X SHEETS



NOTES:

- FLOODPLAIN SHOWN DETERMINED USING THE 100-YEAR DEVELOPED AND UNDETAILED.
- CROSS-SECTIONS ORIENTED LEFT-TO-RIGHT FACING UPSTREAM.



LEGEND

- PROPOSED INVERT
- 100-YEAR FLOOD
- INVERT
- HEC-2 CROSS-SECTION

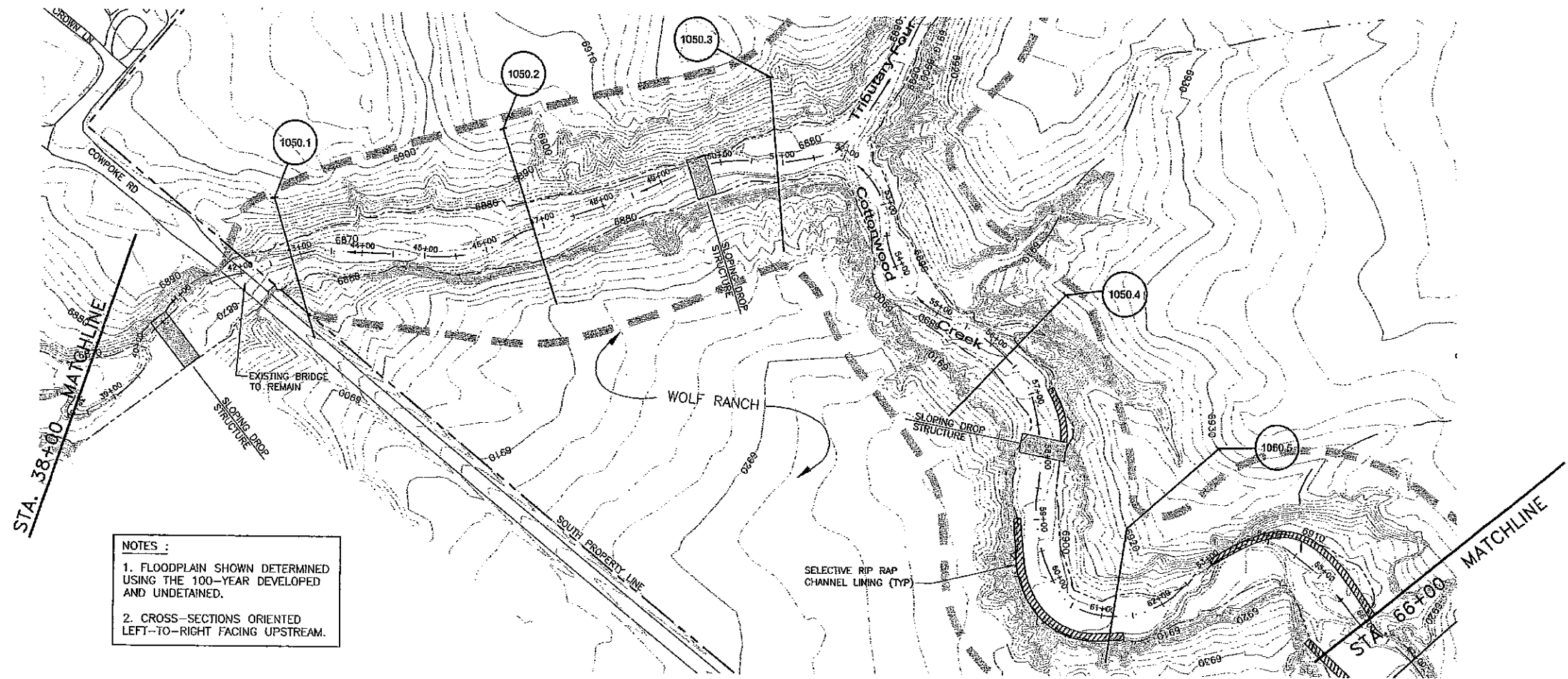
PROFILE SCALE:
 1" = 100' HORIZ.
 1" = 10' VERT.

WOLF RANCH
MASTER DEVELOPMENT DRAINAGE PLAN
COTTONWOOD CREEK
PLAN & PROFILE
 COLORADO SPRINGS, COLORADO

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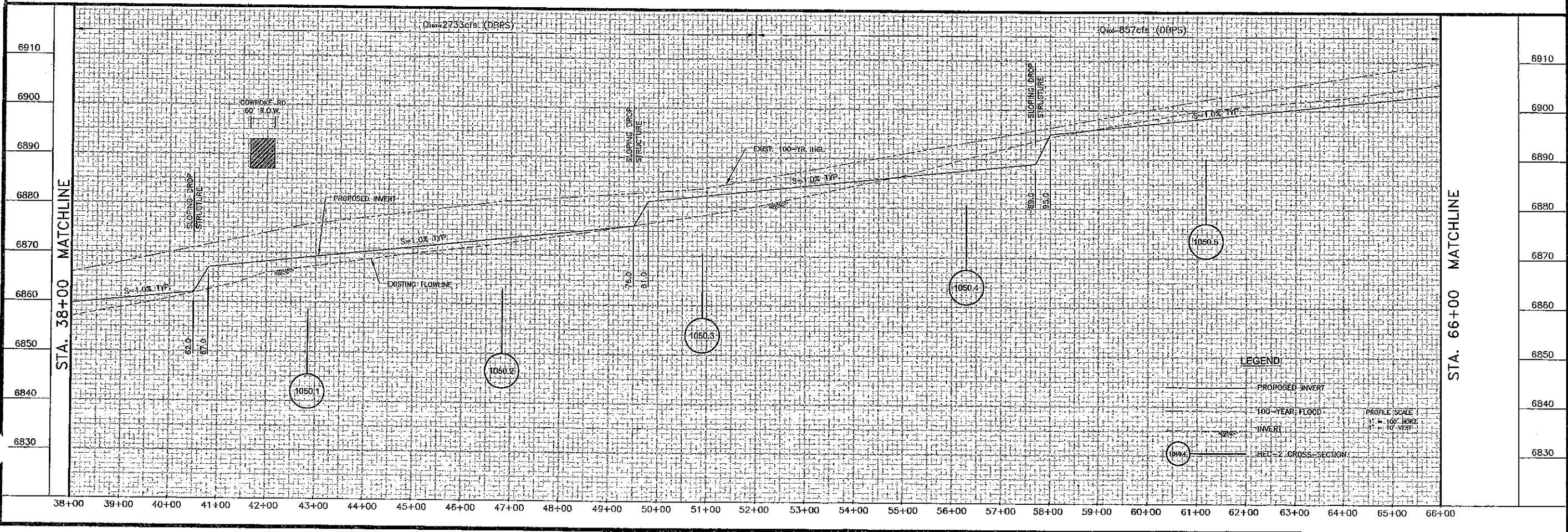
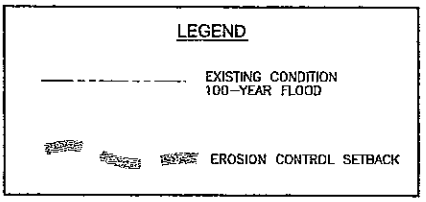
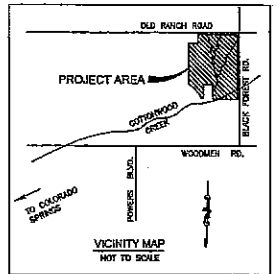
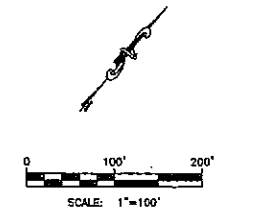
SHEET
PP4
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NOTES :

1. FLOODPLAIN SHOWN DETERMINED USING THE 100-YEAR DEVELOPED AND UNDETAINED.
2. CROSS-SECTIONS ORIENTED LEFT-TO-RIGHT FACING UPSTREAM.



LEGEND:

- PROPOSED INVERT
- 100-YEAR FLOOD
- EXIST. 100-YR. FLD.
- INVERT
- HEC-2 CROSS-SECTION

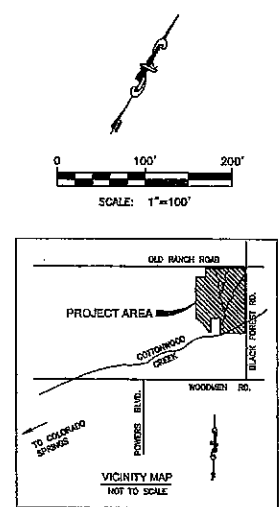
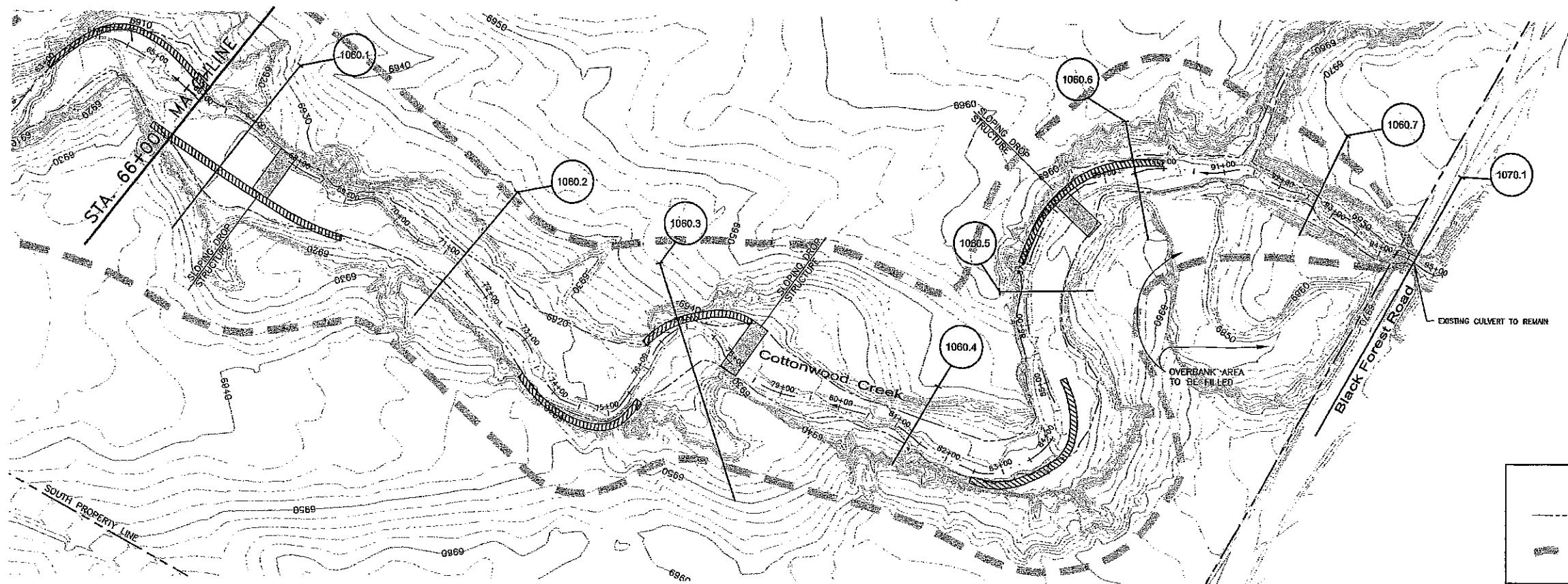
PROFILE SCALE:
 1" = 100' HORIZ.
 1" = 10' VERT.

WOLF RANCH
MASTER DEVELOPMENT DRAINAGE PLAN
COTTONWOOD CREEK
PLAN & PROFILE
 COLORADO SPRINGS, COLORADO

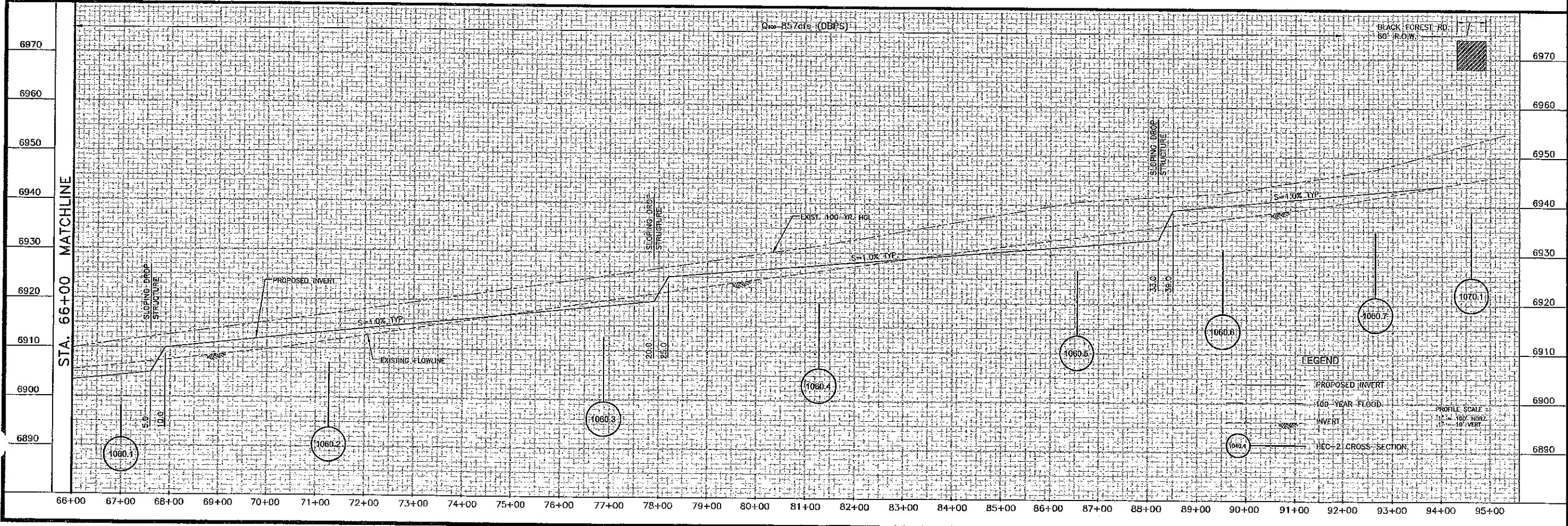
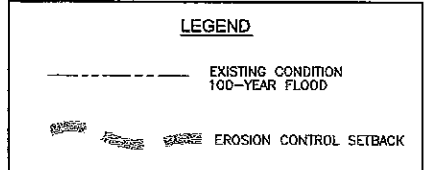
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 Revisions:

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- NOTES :**
1. FLOODPLAIN SHOWN DETERMINED USING THE 100-YEAR DEVELOPED AND UNDETAINED.
 2. CROSS-SECTIONS ORIENTED LEFT-TO-RIGHT FACING UPSTREAM.



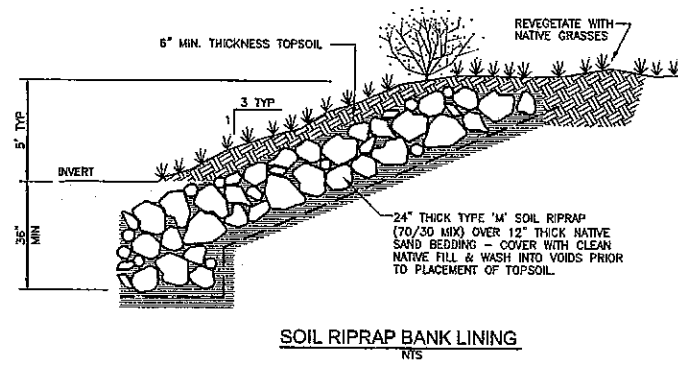
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WOLF RANCH
MASTER DEVELOPMENT DRAINAGE PLAN
COTTONWOOD CREEK
PLAN & PROFILE
 COLORADO SPRINGS, COLORADO

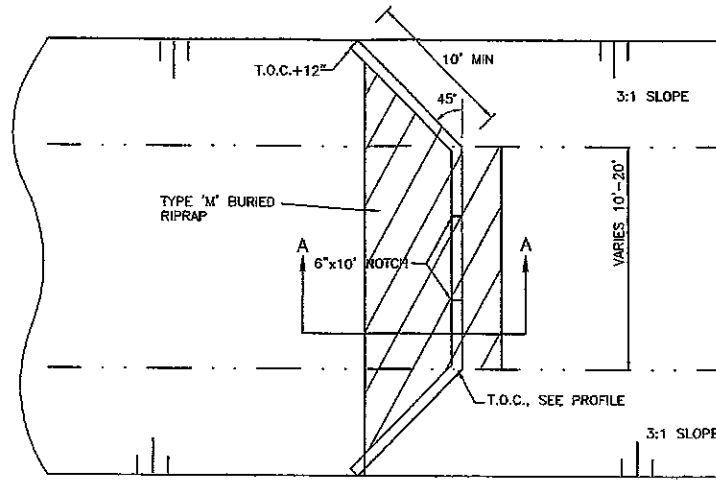
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PP6
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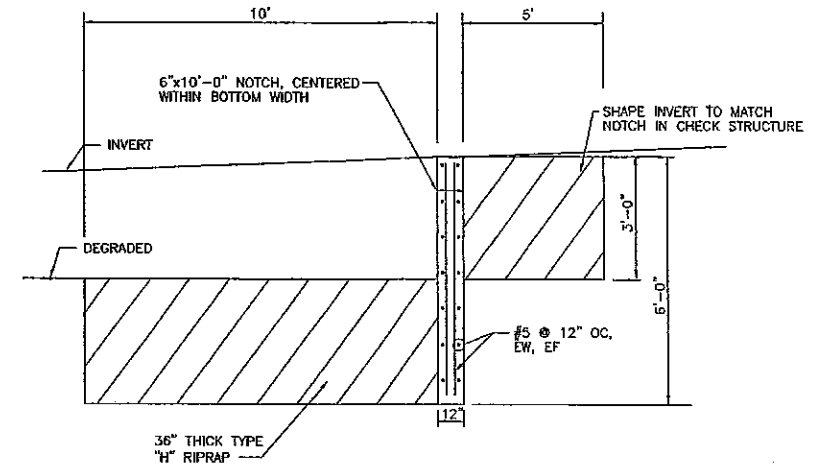
03094 p06-6.dwg/Dec 01, 2004



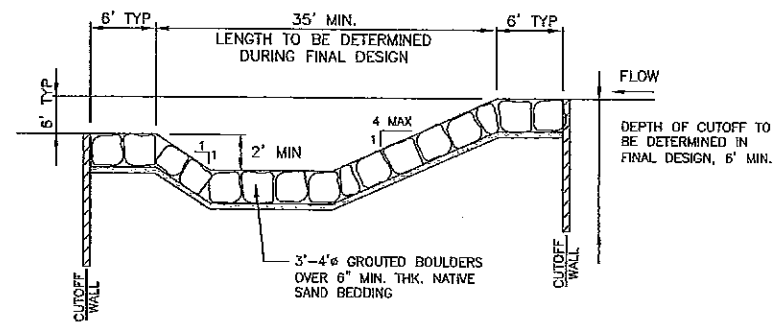
SOIL RIPRAP BANK LINING
N.T.S.



TYPICAL CHECK STRUCTURE PLAN



CHECK STRUCTURE SECTION A-A



**TYPICAL GROUT SLOPING
BOULDER DROP SECTION**
SCALE : N.T.S.

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WOLF RANCH
MASTER DEVELOPMENT DRAINAGE PLAN
TYPICAL DRAINAGEWAY DETAILS
COLORADO SPRINGS, COLORADO

Project No.:	03094
Date:	11/19/04
Design:	RNW
Drawn:	JLN
Check:	RNW
Revisions:	